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Testing of Small and Large Sign Support Systems FOIL Test Number: 92F026



U.S. Department of Transportation

Federal Highway Administration

Research and Development Turner-Fairbank Highway Research Center 6300 Georgetown Pike McLean, Virginia 22101-2296

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SI* (MODERN METRIC) CONVERSION FACTORS									
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	square inch								

SI is the symbol for the International System of Units Appropriate rounding should be made to comply with Section 4 of ASTM E380.

(Revised August 1992)

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1. SCOPE

This test report contains the results of a crash test performed at the Federal Outdoor Impact Laboratory (FOIL) in McLean, Virginia. The test was performed on a small sign support system at 60 mi/h (26.8 m/s), test 92F026. The vehicle used for this test was the FOIL reusable bogie vehicle. The purpose of this test was to evaluate the high-speed safety performance of a 5-in (127.0-mm) diameter wood post sign support system. The performance evaluation was based on the latest requirements for breakaway supports as specified in Volume 54, Number 3 of the Federal Register dated January 5, 1989. These criteria specify, in part, that the occupant change in velocity must be 16 ft/s (4.9 m/s) or less, that the significant test article stub height remaining after impact be no more than 4 in (101.6 mm), and that there can be no occupant compartment intrusion.

2. TEST MATRIX

The test was performed on a small sign support system. The test speed was 60 mi/h (26.8 m/s). The sign was buried in NCHRP Report Number 230, S-2 weak soil⁽¹⁾. A summary of the test conditions is presented in table 1.

Table 1. Test matrix.									
Test Number	Test Date	Test Vehicle	Test Weight lb	Test Speed mi/h	Test Article Description	Impact Location			
92F026	8-31-92	FOIL Bogie	1850	60	wood post in soilcrete/weak soil	center			

3. VEHICLE

The test vehicle was the FOIL reusable breakaway bogie. Frontal crush of the bogie vehicle which simulates the crush of an actual vehicle was accomplished using multiple cartridges of an expendable aluminum honeycomb material in a sliding nose. After the test, the honeycomb material is replaced and the vehicle reused. The honeycomb was set up to represent the crush characteristics of a 1979 Volkswagen Rabbit's left quarter point.^[2] Figure 1 is a sketch of the 60-mi/h (26.8-m/s) honeycomb configuration used for test 92F026. A sweeper plate was attached to bogie vehicle such that it would hang down to a height of 4 in (101.6 mm) above the ground. The sweeper plate was constructed of a section of steel angle welded to a 1/4-in (6.4-mm) steel plate then attached to the bogie using two 3/8-in (9.5-mm) bolts. The sweeper plate was designed as a sacrificial element to simulate the performance of an automobile's undercarriage. The function of the sweeper plate is to determine stub height compliance by the test article. Four wooden 6-ft (1.8-m) four by fours were attached to the bogie vehicle to protect it from damage. The bogie vehicle was ballasted with a data acquisitions system, transducers, a brake system and weight plates (if necessary) to bring its inertial weight to approximately 1850 lb (839 kg). The actual weight of the bogie was 1850 1b (839 kg).



Figure 1. Sketch of bogie honeycomb configuration.

4. SIGN SUPPORT

The sign support system consisted of one 5-in (127.0-mm)-diameter wood post 15.5 ft (4.7 m) long. The post dimension was taken from the tapered tip of the sign post. The actual diameter of the sign post at the impact height was 6.5 in (165.1 mm). The wood post was made from pressure treated southern yellow pine. Two 2-in (50.8-mm) holes were drilled in the sign post, one 6 in (152.4 mm) and one 18 in (457.2 mm) above ground level. A gain was cut from 4 ft 3 in (1.3 m) above ground to the top of the post. The gain provided a flat area for sign panel attachment. The sign panel used was a 1/8 in (3.2 mm) thick aluminum sheet measuring 5 ft (1.5 m) high by 4 ft (1.2 m)wide. Three feet six inches (1.1 m) of the sign post was cast in an 18-in (457.2-mm) diameter soilcrete foundation. The soilcrete foundation was embedded 3.5 ft (1.1 m) deep in NCHRP Report 230 S-2 weak soil (sand). Soilcrete is a mixture of 9 parts native soil and one part portland cement. Because the test was performed in weak soil (sand), sand was used as the native soil. The sign panel was installed 7 ft (2.1 m) above ground. The whole sign support system was assembled and a hole was dug in the weak soil. An 18-in (457.2-mm) form was placed in the hole and the sign post was inserted in the form. A 12-in (304.8-mm) long 2 by 4 was nailed to the base of the sign post to inhibit the sign post from rotating inside the soilcrete. The soilcrete mixture was placed inside the form in 6-in (152.4-mm) lifts and compacted simultaneously with the hole in the weak soil being backfilled in 6-in (152.4-mm) lifts and compacted until the final grade was reached. Figure 2 is a drawing of the sign support system.

5. TEST RESULTS - TEST 92F026

The test vehicle was accelerated to 59.5 mi/h (87.2 ft/s (26.6 m/s)) prior to impacting the sign support. The centerline of the bogie vehicle was aligned with the centerline of the wood sign post.

The honeycomb nose made contact with the wood post and began to collapse. The nose made contact 17.5 in (444.5 mm) above ground on the upper hole. The wood post began to fracture simultaneously at the upper and lower hole. Fracture initiated 0.014 s after initial contact and was complete 0.034 s after impact. The post fractured vertically below the lower hole and between the lower and upper hole. The eighth cartridge of honeycomb had started to crush when the post began to fracture. The eighth cartridge of honeycomb requires approximately 20,000 lb (89 kN) to initiate crush. The bogie passed underneath the sign post without further contact. The bogie vehicle's sweeper plate passed over the remaining stub of the wood post without contact. The stub was measured after the test and was 4 in (101.6 mm) high.

Damage to the bogie vehicle consisted of crushed honeycomb. The damage was to expendable material and not to structural members of the bogie. The measured honeycomb crush after the test was recorded to be 16.1 in (408.9 mm). None of the sign components would have impaled an actual automobile's occupant compartment.

Damage to the sign consisted of a fractured wooden sign post. The soilcrete foundation did not move during the crash test. The sign panel was in good condition after the test.

The occupant impact velocity using the 2-ft (0.6-m) flail space model outlined in NCHRP Report Number 230, was determined to be 6.1 ft/s (1.9 m/s). The occupant impact velocity was reached 0.389 s into the crash event. The 10-ms ridedown acceleration was determined to be 0.8 g's. The peak force

(300 Hz data) for the impact event was 16.1 g's (29.7 kips (132 kN)). The sign post-bogic contact was short and therefore the vehicle change in velocity is equal to the occupant impact velocity, 6.1 ft/s (2.2 m/s). Photographs during the impact event are presented in figure 3. A summary of the impact conditions and the test results is presented in figure 4. Figures 5 through 8 are plots of data collected during the test. Pre- and post-test photographs of the vehicle and sign support system are presented in figures 9 through 12.

6. CONCLUSION

The test results indicate that the small sign support system meets all of the applicable criteria for the high-speed test in weak soil. There was no occupant compartment intrusion, no significant stub remaining after the test, and the occupant impact velocity was 6.1 ft/s (1.9 m/s) which is less than or equal to the 16 ft/s (4.9 m/s) limit specified by the FHWA.



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Figure 2. Sketch of small sign support.

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Figure 3. Test photographs during impact, test 92F026.



4-in STUB IN SOILCRETE FOUNDATION



Test number
Date August 31, 1992
Test vehicle
Vehicle weight
Test articleSmall Sign Support
Material5-in diameter wood 1-Leg, 1-Hit Embedment depth
Panel typesheet
Height 12 ft
Foundation 10-in-dia. soilcrete foundation in S-2 Weak Soil
Impact speed
Impact angle0 degrees
Impact location

Vehicle ana	llysis:	Observed	<u>Design/Limit</u>
Longitudina Occupant De Ridedown Ac	l: lta V at 2 ft celeration	6.1 ft/s 0.8 g's	≤16 ft/s 15/20 g′s
Lateral: Occupant De Ridedown Ac	lta V at 1 ft celeration	no contact no contact	no spec no spec
Peak 50 mse Longit Latera	c acceleration udinal l		2.9 g's NA
Vehicle Dam	age (TAD) (VD1)	• • • • • • • • • • • • • • • • • • •	NA NA
Honeycomb c	rush	•••••	16.1 in
Vehicle vel	ocity change		6.1 ft/s
Exit angle.	•••••••••••••••••••••••••••••••••••••••		O degrees

1 in = 25.4 mm 1 ft = 0.305 m 1 1

1 1b = 0.454 kg

Figure 4. Summary of test 92F026.



TEST NO. 92F026

Figure 5. Acceleration versus time, X-axis, test 92F026.

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Acceleration (g's)



1 ft = 0.305 m

Figure 6. Velocity versus time, X-axis, test 92F026.

Q

(ft/g)

Velocity



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 $1 \ 1bf = 4.45 \ N$ 1 ft = 0.305 m

Figure 7. Force versus displacement, X-axis, test 92F026.

TEST NO. 92F026





Figure 8. Occupant velocity and relative displacement versus time, X-axis, test 92F026.

<u>نام</u>

disp (ft)

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Occupant velocity (ft/s)

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Figure 10. Additional pretest photographs of test 92F026.



Figure 11. Post-test photographs of test 92F026.

Figure 12. Additional post-test photographs of test 92F026.

8. REFERENCES

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- Jarvis D. Michie, Recommended Procedures for the Safety Performance Evaluation of Highway Appurtenances, National Cooperative Highway Research Program Report Number 230, March 1981.
- (2) Charles R. Hott, Christopher M. Brown, Nick Totani and Allen G. Hansen, Crush Characteristics of the "Breakaway" Bogie, Report No. FHWA-RD-89-107, Federal Highway Administration, Washington, DC, July 1990.