# Testing of Small and Large Sign Support Systems FOIL Test Numbers: 92F040 

U.S.Department of Transportation

## Federal Highway Administration

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Technical Report Documentation Page

15. Supplementary Notes

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18. Abstract

This test report contains the results of a crash test performed at the Federal Outdoor Impact Laboratory (FOIL) in McLean, Virginia. The test was performed on a small sign support system at $60 \mathrm{mi} / \mathrm{h}(96.6 \mathrm{~km} / \mathrm{h})$, test 92 F 040 . The vehicle used for this test was a 1986 Honda Civic. The purpose of this test was to evaluate the high-speed safety performance of a triple-legged 12 -gauge $1.75-i n(44.4-\mathrm{mm})$ square tube sign support. The performance evaluation was based on the latest requirements for breakaway supports as specified in Volume 54, Number 3 of the Federal Register dated January 5, 1989. These criteria specify, in part, that the occupant change in velocity must be $16 \mathrm{ft} / \mathrm{s}$ ( $4.9 \mathrm{~m} / \mathrm{s}$ ) or less, that the significant test article stub height remaining after impact be no more than 4 in ( 101.6 mm ), and that there can be no occupant compartment intrusion. The test results indicate that the square tube sign support system does not meet all of the applicable safety criteria for the high-speed test in strong soil as specified by the FHWA.
17. Key Words

Acceleration, occupant impact ve?ocity, strong soil, square tube, vehicle, FOIL.

## 18. Distribution Statement

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|  |  | S1* (M | DERN ME | HO) | ONV | $10 N F A O T$ | 35 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| APPROXIMATE CONVERSIONS TO SI UNITS |  |  |  |  | APPROXIMATE CONVERSIONS FROM SI UNITS |  |  |  |  |
| Symbol | When You Know | Multiply By | To Find | Symbol | Symbol | When You Know | Multiply By | To Find Sy | Symbal |
|  |  | LENGTH |  |  |  |  | LENGTH |  |  |
| in | inches | 25.4 | millimeters |  | mm | millimeters | 0.039 | inches | in |
| H | fagt | 0.305 | molers | m | m | meters | 328 | feel | $1 t$ |
| yd | yands | 0.914 | meters | m | m | meters | 1.09 | yards | yod |
| mi | miles | 1.61 | hilomelers | km | km | kilometers | 0.621 | miles | mı |
|  |  | AREA |  |  |  |  | AREA |  |  |
| in ${ }^{2}$ | square inchos | 645.2 | square millimeters | $\mathrm{mm}^{2}$ | $\mathrm{mm}^{2}$ | square millimeters | 0.0016 | square inchos | $1 \mathrm{n}^{2}$ |
| $\dagger^{+}$ | square teet | 0.093 | square meters | $m^{2}$ | $\mathrm{m}^{7}$ | square meters | 10.764 | square teot | $\mathrm{H}^{2}$ |
| yof | square yards | 0836 | square melers | $\mathrm{m}^{2}$ | $\mathrm{m}^{2}$ | square meters | 1195 | square yards | $\mathrm{ac}^{\text {c }}$ |
| ac | acres | 0.405 | heclares | ha | ha | heclares | 247 | acres | $\mathrm{mi}^{2}$ |
| $m r^{2}$ | square miles | 2.59 | square kilometers | $\mathrm{km}^{2}$ | km ${ }^{2}$ | square kilometers | 0.386 | square milos |  |
|  |  | VOLUME |  |  |  |  | VOLUME |  |  |
| flaz | fluid ounces | 2957 | millititers | ml | ml | millititers | 0.034 | flud ounces | $\mathrm{H}_{\mathrm{O}}$ |
| gal | gallons | 3.785 | liters | 1 | , | liters | 0.264 | gations | gal |
| $\mathrm{l}^{3}$ | cubic feet | 0.028 | cubic melers | $\mathrm{m}^{3}$ | $\mathrm{m}^{3}$ | cubic metors | 35.71 | cubic toet | is |
| $y 0^{\circ}$ | cubic yards | 0.765 | cubic meters | $\mathrm{m}^{3}$ | $\mathrm{m}^{3}$ | cubic meters | 1.307 | cubic yauds | $y^{\prime \prime}$ |
| NOTE: Volumes greater than 10001 shall be shown in $m^{3}$. |  |  |  |  |  |  |  |  |  |
|  |  | MASS |  |  |  |  | MASS |  |  |
| O2 | ounces | 28.35 | grams |  | $\theta$ | grams | 0.035 | ounces | 02 |
| lb | pounds | 0.454 | kulograms | kg | kg | kilograms | 2.202 | pounds | 16 |
| T | short lons (2000 lb) | 0.907 | megagrams | Mg | Mg | megagrams | 1.103 | short tons (2000 Ib) | T |
| TEMPERATURE (exact) |  |  |  |  | TEMPERATURE (exact) |  |  |  |  |
| ${ }^{\circ} \mathrm{F}$ | Fahrenhen temperature | $\begin{aligned} & 5(F-32) / 9 \\ & \text { or }(F-32) 1.8 \end{aligned}$ | Calcius temperature | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{C}$ | Celcius temperature | $1.8 \mathrm{C}+32$ | Fahrenteit temperature | ${ }^{\circ} \mathrm{F}$ |
|  | ILL | IMINATION |  |  | ILLUMINATION |  |  |  |  |
| $\begin{aligned} & \text { Ic } \\ & \text { fi } \end{aligned}$ | foot-candles foot-Lamberts | $\begin{aligned} & 10.76 \\ & 3.426 \end{aligned}$ | lux candela/m ${ }^{2}$ | $\mathrm{cd} / \mathrm{m}^{2}$ | $1 \times$ $\mathrm{cd} / \mathrm{m}^{2}$ | lux candola/m $\mathrm{m}^{2}$ | $\begin{aligned} & 0.0929 \\ & 0.2919 \end{aligned}$ | foot-candles foot-Lamberts | Ic |
|  | FORCE and PRESSURE or STRESS |  |  |  | FORCE and PRESSURE or STRESS |  |  |  |  |
| lbl | poundiorco | 4.45 | newtons | N | $N$ | newtons | 0.225 | prundlorce | lbl |
| pSı | poundiorce per square inch | 689 | kilopascals | kPa | kPa | kilopascals | 0145 | poundtorco per square inch | psi |

- Sl is the symbol for the International System of Units. Appropriate
rounding should be made to comply with Sectorn 4 of ASTM E380.


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## 1. SCOPE

This test report contains the results of a crash test performed at the Federal Outdoor Impact Laboratory (FOIL) in McLean, Virginia. The test was performed on a small sign support system at $60 \mathrm{mi} / \mathrm{h}(96.6 \mathrm{~km} / \mathrm{h})$, test 92 FO 0 . The vehicle used for this test was a 1986 Honda Civic. The purpose of this test was to evaluate the high-speed safety performance of the sign support system. The sign support system consisted of three small square tube posts inserted in three larger square tube anchors. The sign posts were $1-3 / 4$-in ( $44.4-\mathrm{mm}$ ) square tube inserted into 2 -in ( $50.8-\mathrm{mm}$ ) square tube anchors. The anchors were installed in strong soil. The performance evaluation was based on the latest requirements for breakaway supports as specified in Volume 54, Number 3 of the Federal Register dated January 5, 1989. These criteria specify, in part, that the occupant change in velocity must be $16 \mathrm{ft} / \mathrm{s}$ ( $4.9 \mathrm{~m} / \mathrm{s}$ ) or less, that the significant test article stub height remaining after impact be no more than 4 in ( 101.6 mm ), and that there can be no occupant compartment intrusion.

## 2. TEST MATRIX

The test was performed on a small sign support system. The test speed was $60 \mathrm{mi} / \mathrm{h}(96.6 \mathrm{~km} / \mathrm{h})$. The sign was buried in NCHRP Report Number 230, S-1 strong soil ${ }^{(1)}$. A summary of the test conditions is presented in table 1 .

| Table 1. Test matrix. |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Test Number | Test Date | Test Vehicle | Test Weight (1b) | Test Speed (mi/h) | Test <br> Article Description | Impact Location |
| 92F040 | 12-16-92 | ' 86 Honda Civic | $\begin{array}{r} 1850 \\ 839 \mathrm{~kg} \\ \hline \end{array}$ | $\begin{gathered} 60 \\ 96.6 \mathrm{~km} / \mathrm{h} \\ \hline \end{gathered}$ | 3 leg steel square tube | center |

## 3. VEHICLE

The test vehicle was a 1986 Honda Civic two door hatchback with a manual transmission. Prior to the test, the vehicles' fluids were drained and its inertial properties measured. The vehicle was stripped of certain components which made space for the installation of test equipment. The vehicle was ballasted with a data acquisitions system, transducers, a brake system and weight plates (if necessary) to bring its inertial weight to approximately $185010(839 \mathrm{~kg})$. The actual weight of the test vehicle was $1850 \mathrm{lb}(839 \mathrm{~kg})$. After ballasting, the vehicles' inertial properties were remeasured.

## 4. SIGN SUPPORT

The sign support system consisted of three square tube posts embedded $3 \mathrm{ft}(0.9 \mathrm{~m})$ in NCHRP Report $230 \mathrm{~S}-1$ strong soil. Each leg consisted of a l-3/4-in ( $44.4-\mathrm{mm}$ ) 12 -gauge perforated square tube inserted into a 2 -in ( $50.8-\mathrm{mm}$ ) 12 -gauge perforated square tube anchor. The splice was 9 in ( 228.6 mm ) long with 8 in ( 203.2 mm ) below ground. The square tubes were spliced using two $3 / 8$-in ( $9.5-\mathrm{mm}$ ) diameter corner bolts at ground level. The posts were spaced $1.75 \mathrm{ft}(0.53 \mathrm{~m})$ apart with a $2.5-\mathrm{ft}$ by $5.5-\mathrm{ft}$ ( $0.76-\mathrm{m}$ by $1.68-\mathrm{m}$ ) aluminum sign blank attached. Figure $l$ presents a sketch
of the sign support system. The sign system was assembled then placed in a trench in the strong soil. Soil was placed in the trench around the sign posts in 6 -in ( $152.4-\mathrm{mm}$ ) lifts. During each lift the soil was moistened and compacted. This procedure was repeated until the final grade was reached.

## 5. TEST RESULTS - TEST $92 F 040$

The test vehicle was accelerated to $59.2 \mathrm{mi} / \mathrm{h}(86.8 \mathrm{ft} / \mathrm{s}(95.5 \mathrm{~km} / \mathrm{h})$ ) prior to impacting the sign support. The centerline of the test vehicle was aligned with the center sign post.

The bumper made contact with all three sign posts but did not significantly collapse. The three square tube sign posts bent around the front end of the test vehicle. The three square tube posts buckled 0.014 s after contact. The vehicle begins to ridedown the sign posts but the square tube fractured at the impact point on the posts approximately 0.028 s into the impact event. The square tube anchors did not plow through the strong soil during impact. The square tube anchors were pulled up slightly by the vehicle. The anchors of the center and right posts fractured at the bottom of the splice, where the inserted smaller tube ends inside the larger anchor. The left post fractured 1 in ( 25.4 mm ) above ground just above the corner bolts that spliced the two pieces of square tube. The vehicle broke through the square tube posts and pushed on the remaining sign posts rotating the top of the sign down towards the vehicle. The sign made contact with the roofwindshield joint at 0.080 s . The impact of the sign on the roof and windshield caused severe denting of the roof and shattered the windshield. The roof attained its maximum crush at approximately 0.108 s . The sign rebounded off the roof and slid down off the front end of the vehicle and briefly impaled the ground in front of the test vehicle. The vehicle struck the sign again and launched it up and away from the test vehicle. The vehicle's brakes were applied and the vehicle came to a stop prior to colliding with the FOIL catch fence. The sign stub remaining at the location of impact consisted of three $24-\mathrm{in}(609.6-\mathrm{mm})$ square tube sections bent over, laying flat on the ground. The six corner bolts did not fracture or tear through the perforated square tube during impact.

Damage to the vehicle consisted of damage to the parking lights and a small dent in the front end header panel. No damage to the bumper or headlights was recorded after the test. The most damage was imparted to the windshield and roof of the vehicle. The roof dented in approximately 6 in ( 152.4 mm ) and the windshield was shattered. The occupant compartment was not intact after the test.

Damage to the sign system consisted of three collapsed $1.75-\mathrm{in}$ ( $44.4-\mathrm{mm}$ ) square tube posts and three fractured $2-i n(50.8-\mathrm{mm}$ ) square tube anchors. None of the square tube sign material could be reused. The sign panel and six corner bolts were in usable condition after the test. The sign panel and top of the posts collapsed the occupant compartment.

The occupant impact velocity using the $2-\mathrm{ft}(0.6-\mathrm{m})$ flail space model outlined in NCHRP Report Number 230, was determined to be $8.1 \mathrm{ft} / \mathrm{s}(2.5 \mathrm{~m} / \mathrm{s})$. The occupant impact velocity was reached 0.2805 s into the crash event. The ridedown acceleration was 2.5 g 's. The peak acceleration ( 300 Hz data) for the impact event was 25.4 g 's (peak force $47.0 \mathrm{kips}(209.1 \mathrm{kN})$ ). Because the sign system had secondary impact with the vehicle after the occupant had traversed the flail space, the vehicle change in velocity is greater than the occupant impact velocity. The calculated vehicle change in velocity by integration of the acceleration trace was $10.6 \mathrm{ft} / \mathrm{s}(3.2 \mathrm{~m} / \mathrm{s})$.

Photographs during the impact event are presented in figure 2. A summary of the impact conditions and the test results is presented in figure 3. Figures 4 through 7 are plots of data collected during the test. Pre- and post-test photographs of the vehicle and sign support system are presented in figures 8 through 10.

## 6. CONCLUSION

The test results indicate that the small sign support system does not meet all of the applicable criteria for the high-speed test in strong soil. The occupant impact velocity was $8.1 \mathrm{ft} / \mathrm{s}(2.5 \mathrm{~m} / \mathrm{s})$ which is less than or equal to the $16-\mathrm{ft} / \mathrm{s}(4.9-\mathrm{m} / \mathrm{s})$ limit specified by the FHWA and the significant test article stub height remaining after the test was 1.75 in ( 44.4 mm ) which is less than or equal to the 4 -in (101.6-mm) limit. However the impact between the sign panel/posts and the roof and windshield, caused severe collapse of the vehicle's roof and shattered the windshield. The occupant compartment was severely damaged and could put an occupant at a higher risk of injury.


Figure 1. Sketch of small sign support.

0.032 s

Test photographs during impact, test 92F040.

0.010 s

0.050 s


Figure 3. Summary of test 92F040.

## TEST NO. 92F040



Figure 4. Acceleration versus time, $X$-axis, test 92 F040.
TEST NO. 92F040

$1 \mathrm{ft}=0.305 \mathrm{~m}$

Figure 5. Velocity versus time, X-axis, test $92 \mathrm{FO40}$.

TEST NO. $92 F 040$


Figure 6. Force versus displacement, $X$-axis, test 92 F040.

TEST NO. 92F040

$1 \mathrm{ft}=0.305 \mathrm{~m}$
Figure 7. Occupant velocity and relative displacement versus time, X-axis, test 92 F040.




## 7. REFERENCES

(1) Jarvis D. Michie, Recommended Procedures for the Safety Performance Evaluation of Highway Appurtenances, National Cooperative Highway Research Program Report Number 230, March 1981.

