# ANALYSIS OF PREDICTED AIRCRAFT WAKE VORTEX TRANSPORT AND COMPARISON WITH EXPERIMENT 

Volume II -- Appendixes



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Technical Report Documentation Page



## PREFACE

This document represents the final report of Contract DOT-TSC-593 and covers the period 2 April to 2 December 1973.

This study was performed by personnel at the Lockheed Missles \& Space Company, Inc., Huntsville Research \& Engineering Center, Huntsville, Alabama. The project engineer and principal investigator for this study was Dr. M.R. Brashears of the Fluid Mechanics Applications Group.

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Appendix A
SUMMARY OF AIRCRAFT FLYBYS

This appendix summarizes aircraft information for the test days of interest. The first priority flybys are those recorded on 17 and 18 October 1972 and 1 November 1972. However, predictive vortex tracks have been generated for most of the runs shown in this appendix. The wind speed and direction are the unaveraged values recorded at the 140 -foot level on the tower corresponding to the time of aircraft passage.

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| 曷 | $\begin{array}{\|l\|l} \hline \infty \\ \underset{\sim}{2} \\ \dot{0} \end{array}$ | $\begin{array}{\|l\|l} \tilde{N} \\ \infty \\ \infty \end{array}$ | $\begin{array}{\|l\|l} \hline \stackrel{\circ}{2} \\ \dot{\infty} \end{array}$ | $\begin{array}{\|l\|l} \hline \stackrel{\circ}{\ddot{0}} \\ \ddot{\circ} \end{array}$ | $$ | $\begin{aligned} & \vec{n} \\ & \stackrel{\theta}{\circ} \end{aligned}$ | $\begin{array}{\|l\|l} \hline \stackrel{R}{2} \\ \ddot{0} \\ \hline 0 \end{array}$ | $\begin{aligned} & \hline \underset{o}{0} \\ & \dot{0} \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \stackrel{\circ}{\circ} \end{aligned}$ | $\begin{aligned} & \mathrm{y} \\ & \underset{\sim}{\circ} \end{aligned}$ | N ※̈ O | $\begin{aligned} & \text { ٌ } \\ & \underset{\sim}{\circ} \end{aligned}$ |
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| $$ | $\begin{array}{\|l} \hline \stackrel{\tilde{\omega}}{\dot{\circ}} \end{array}$ | $\begin{aligned} & \text { N } \\ & \stackrel{y}{0} \end{aligned}$ | $\begin{aligned} & \text { } \\ & \stackrel{\infty}{\vdots} \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \text { O} \\ & \stackrel{\rightharpoonup}{\circ} \end{aligned}$ | $\begin{aligned} & \text { \#̈ } \\ & \stackrel{3}{\theta} \end{aligned}$ | $\begin{aligned} & \stackrel{\sim}{n} \\ & \stackrel{0}{-} \end{aligned}$ | $\begin{aligned} & \stackrel{\ddot{U}}{\ddot{ت}} \end{aligned}$ | $\stackrel{\circ}{\square}$ | $\stackrel{\text { 年 }}{\rightrightarrows}$ | $\stackrel{9}{⿻}$ | $\stackrel{\text { H }}{\underset{\sim}{\#}}$ |
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|  | $\stackrel{\underset{1}{1}}{\stackrel{\rightharpoonup}{9}}$ |  | $\stackrel{\underset{1}{\mathrm{D}}}{1}$ |  | $\stackrel{N}{\square}$ |  | $\underset{\sim}{\mathrm{I}}$ | $\underset{\underset{\sim}{\mathrm{I}}}{\underset{\sim}{2}}$ |  | $\stackrel{7}{1}$ |  | $\stackrel{\rightharpoonup}{\square}$ |
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| $\underbrace{\text { O }}_{\substack{\dot{0} \\ \text { ¢ }}}$ | $\pm$ | $\cong$ | $\cong$ | $\approx$ | $\xlongequal{ }$ | $\stackrel{\infty}{\sim}$ | $\stackrel{\infty}{\sim}$ | $\stackrel{\infty}{\sim}$ | $\stackrel{\infty}{\sim}$ | $\stackrel{\infty}{\sim}$ | $\stackrel{\infty}{\sim}$ | $\stackrel{\infty}{\sim}$ |
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| cid |  |  |  | $\tilde{\text { Ha }}^{\infty}$ | Fio |  | $\underset{\sim}{\underset{M}{A}} \stackrel{\rightharpoonup}{2}$ |  | $\underset{\substack{\mathrm{A}}}{\text { N }}$ | $\stackrel{\text { H̀ }}{\hat{M}}$ | $\underset{M}{\underset{\sim}{A} n}$ | 㔖号 |
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|  | $\stackrel{\stackrel{\rightharpoonup}{+}}{\stackrel{+}{+}}$ | $\tilde{N}$ <br> $\stackrel{\sim}{\circ}$ | $\begin{aligned} & \stackrel{0}{\circ} \\ & \stackrel{0}{\circ} \end{aligned}$ | $\stackrel{\sim}{n}$ <br> $\stackrel{\sim}{i}$ | $\left\lvert\, \begin{gathered} n \\ \ddot{\ddot{o}} \\ \ddot{o} \end{gathered}\right.$ | $\begin{array}{\|l\|} \hline \stackrel{O}{\circ} \\ \ddot{\circ} \end{array}$ | $\begin{aligned} & N \\ & \underset{\ddot{\theta}}{\sim} \end{aligned}$ | $\stackrel{0}{\ddot{0}}$ | $\begin{aligned} & \bar{\sim} \\ & \text { ®̈ } \end{aligned}$ | $\left\lvert\, \begin{aligned} & n \\ & \stackrel{n}{\infty} \\ & \ddot{\infty} \end{aligned}\right.$ | $\begin{array}{\|} \underset{\sim}{\underset{\sim}{0}} \\ \ddot{\circ} \end{array}$ | $\left\lvert\, \begin{aligned} & \tilde{N} \\ & \substack{\infty \\ \infty \\ \infty} \end{aligned}\right.$ |
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|  | $\stackrel{\infty}{\vdots}$ | $\stackrel{\infty}{1}$ | $\stackrel{\infty}{1}$ | $\underset{\sim}{1}$ | $\stackrel{\infty}{\square}$ | $\underset{\substack{\infty \\ \underset{\sim}{1} \\ \hline}}{ }$ | $\frac{\infty}{\vdots}$ | $\stackrel{\infty}{\stackrel{\infty}{\square}}$ | $\stackrel{\infty}{1}$ | $\frac{\infty}{1}$ | $\stackrel{\infty}{\square}$ | $\stackrel{\infty}{\square}$ |
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| 品志品 | $\stackrel{\stackrel{\rightharpoonup}{\mathrm{o}}}{\stackrel{1}{\mathrm{~m}}}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{\hat{m}}^{N} \end{aligned}$ | $\hat{o}_{\mathrm{D}}^{\mathrm{m}}$ |  | $\stackrel{\hat{a}}{\mathrm{~m}}^{\mathrm{in}}$ | $\underset{\substack{\stackrel{N}{\circ} \\ \stackrel{1}{2} \\ \hline}}{ }$ | $\begin{array}{\|c} \hat{O} \\ \vdots \\ i \end{array}$ | $\hat{0}_{\substack{\infty}}$ | $\stackrel{\text { oñ }}{\substack{0 \\ \hline}}$ | $\left\lvert\, \begin{aligned} & \text { Bo } \\ & \text { Do } \\ & \text { in } \end{aligned}\right.$ | $\begin{aligned} & \text { Noे } \\ & \text { in } \end{aligned}$ | ®o ¢ N |
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| Configuration | $\begin{aligned} & \text { Run } \\ & \text { Label } \end{aligned}$ | Aircraft Displacement from owe (ft) | Aircraft Altitude Abreast of Tower <br> (it) | Aircraft Weight (1000 1b) | Aircraft Speed (knots) | Temp. <br> ( ${ }^{\circ} \mathrm{C}$ ) | Initial Wind Speed (mph) | Initial Wind Angle (deg from true N ) true $N$ ) | Final Wind Speed (mph) | $\begin{gathered} \text { Final } \\ \text { Wind } \\ \text { Angle } \\ \text { (deg from } \\ \text { true N) } \\ \hline \end{gathered}$ | Aircraft Heading (deg from mag. N) | $\begin{gathered} \text { Month- } \\ \text { Day } \\ \text { (1972) } \end{gathered}$ | $\begin{aligned} & \text { Time } \\ & \text { (EDT) } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Holding, level flight, all engines same power | $\begin{gathered} \text { B707 } \\ 13 \end{gathered}$ | 257 | 215 | 237 | 220 | 6 | 5 | 20 | 6 | 350 | 130 | 10-18 | 09:33 |
| Holding, level flight, all engines same power | $\begin{gathered} \mathrm{B} 707 \\ 14 \end{gathered}$ | 288 | 231 | 236 | 225 | 6 | 6 | 20 | 9 |  | 130 | 10-18 | 09:37 |
| Holding, level fight, all engines same power | $\begin{gathered} \mathrm{B} 707 \\ 15 \end{gathered}$ | 248 | 195 | 235 | 220 | 6 | 8 |  | 8 | 10 | 130 | 10-18 | 09:41 |
| Landing, outboard engine away from tower at idle (Vortex 2) | $\begin{gathered} \mathrm{B} 707 \\ 16 \end{gathered}$ | 275 | 221 | 234 | 145 | 6 | 10 |  | 7 | 10 | 130 | 10-18 | 09:45 |
| Landing, outboard engine away from tower at idle (Vortex 2) | $\begin{gathered} \mathrm{B} 707 \\ 17 \end{gathered}$ | 271 | 191 | 233 | 145 | 6 | 10 |  | 8 |  | 130 | 10-18 | 09:50 |
| Landing, outboard engine away from tower at idle (Vortex 2) | $\begin{gathered} \mathrm{B} 707 \\ 18 \end{gathered}$ | 275 | 209 | 231 | 209 | 6 | 8 |  | 9 |  | 130 | 10-18 | 09:54 |
| Landing, outboard engine toward tower at idle (Vortex 1) | $\begin{gathered} \text { B707 } \\ 19 \end{gathered}$ | 249 | 196 | 230 | 145 | 6 | 9 |  | 8 |  | 128 | 10-18 | 09:57 |
| Landing, outboard engine toward tower at idle (Vortex 1) | $\begin{gathered} \text { B707 } \\ 20 \end{gathered}$ | 252 | 156 | 229 | 145 | 6 | 8 |  | 8 |  | 130 | 10-18 | 10:02 |
| Landing, outboard engine toward tower at idle (Vortex 1) | $\begin{gathered} 8707 \\ 21 \end{gathered}$ | 278 | 150 | 227 | 145 | 6 | 8 |  |  |  | 127 | 10-18 | 10:06 |
| Take off, swoop, full power | $\begin{gathered} \mathrm{B} 707 \\ 22 \end{gathered}$ | 277 | 182 | 226 | 170 | 7 | 4 |  | 6 | 350 | 130 | 10-18 | 10:10 |
| Take off, swoop, full power | $\begin{gathered} \mathrm{B} 707 \\ 23 \end{gathered}$ | 269 | 161 | 225 | 170 | 7 | 8 | 10 | 6 |  | 130 | 10-18 | 10:15 |
| Take off, swoop, full power | $\begin{gathered} \mathrm{B} 707 \\ 24 \end{gathered}$ | 270 | 158 | 223 | 172 | 7 | 6 | 20 |  |  | 130 | 10-18 | 10:22 |


|  | $\sqrt[\ddot{\ddot{Z}}]{\square}$ | $\begin{aligned} & \underset{7}{7} \\ & \hline \end{aligned}$ | $\begin{gathered} \underset{\sim}{\sharp} \\ \end{gathered}$ | $\stackrel{\infty}{\underset{\rightrightarrows}{=}}$ | $\stackrel{N}{\rightrightarrows}$ | $\begin{aligned} & \stackrel{0}{7} \\ & = \end{aligned}$ | $\stackrel{7}{\rightrightarrows}$ | $\begin{aligned} & \text { 等 } \end{aligned}$ | $\stackrel{\stackrel{\circ}{\square}}{\underset{7}{7}}$ |
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|  | N | $\stackrel{\stackrel{\circ}{*}}{\sim}$ | $\stackrel{\infty}{\sim}$ | $\underset{\sim}{N}$ | $\stackrel{\sim}{\sim}$ | $\underset{\sim}{N}$ | － | $\stackrel{\text { n }}{\sim}$ | $\underset{\sim}{\text { N }}$ |
| 号运 | $\underset{\mathrm{m}}{\mathrm{C}}$ | $\begin{aligned} & \text { No웅 } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \hat{N} \\ & \tilde{M} \\ & \end{aligned}$ |  | $\begin{aligned} & \text { ion } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \text { No } \\ & \text { op } \\ & \text { in } \end{aligned}$ | $\stackrel{\rightharpoonup}{\dot{m}} \overline{\mathrm{o}}$ | $\begin{aligned} & \hat{N} \\ & \hat{0} \tilde{m} \\ & i \end{aligned}$ | $\stackrel{\text { Noेm }}{\substack{\text { m }}}$ |
|  |  |  |  |  |  |  |  |  |  |


| Configuration | Run Label | Aircraft Displacement from Tower <br> (ft) | Aircraft Altitude Abreast of Tower <br> (ft) | Aircraft Weight (1000 1b) | Aircraft Speed (knots) | Temp. <br> ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{aligned} & \text { Initial } \\ & \text { Wind } \\ & \text { Speed } \\ & \text { (mph) } \end{aligned}$ | Initial Wind Angle (deg from true N$)$ | Final <br> Wind <br> Speed <br> (mph) | Final <br> Wind <br> Angle (deg from true N) | Aircraft Heading (deg from mag. N) | $\begin{gathered} \begin{array}{c} \text { Month- } \\ \text { Day } \end{array} \\ \text { (1972) } \end{gathered}$ | $\begin{aligned} & \text { Time } \\ & \text { (EST) } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Holding, level lifght, all ergines same power | $\begin{gathered} B 707 \\ 34 \end{gathered}$ | 257 | 191 | 264 | 225 | 6 | 7 |  |  |  | 130 | 11-1 | 07:36 |
| Holding, level flight, all engines same power | $\begin{gathered} 8707 \\ 35 \end{gathered}$ | 303 | 205 | 263 | 218 | 6 | 6 |  | 6 | 350 | 130 | 11-1 | 07:40 |
| Landing, level flight, all engines same power | $\begin{gathered} 8707 \\ 36 \end{gathered}$ | 276 | 212 | 262 | 150 | 6 | 7 |  | 7 |  | 126 | 11-1 | 07:44 |
| Landing, level flight, all engines same power | $\begin{gathered} \text { B707 } \\ 37 \end{gathered}$ | 294 | 197 | 261 | 148 | 5 | 5 | 350 |  |  | 128 | 11-1 | 07:49 |
| Landing, outboard <br> engine away from tower <br> at idle (Vortex 2) | $\begin{gathered} \mathrm{B} 707 \\ 38 \end{gathered}$ | 276 | 204 | 258 | 148 | 5 | 5 | 310 |  |  | 130 | 11-1 | 07:58. |
| Landing, outboard <br> engine away from tower <br> at idle (Vortex 2) | $\begin{gathered} \text { B707 } \\ 39 \end{gathered}$ | 278 | 229 | 256 | 146 | 6 |  |  | 7 |  | 130 | 11-1 | 08:08 |
| Landing, outboard engine toward tower at idle (Vortex 1) | $\begin{gathered} \mathrm{B707} \\ 40 \end{gathered}$ | 298 | 218 | 254 | 148 | 5 | 9 | 330 | 8 |  | 126 | 11-1 | 08:07 |
| tanding, outboard engine toward tower at idle (Vortex 1) | $\begin{gathered} \mathrm{B707} \\ 41 \end{gathered}$ | 276 | 216 | 250 | 143 | 5 |  |  | 7 | 350 | 128 | 11-1 | 08:12 |
| Takeoff, level flight, all engines same power | $\underset{42}{\mathrm{~B} 707}$ | 241 | 200 | 250 | 145 | 5 | 7 |  | 5 |  | 130 | 11-1 | 08: 18 |
| Take off, level flight, all engines same power | $\begin{gathered} \mathrm{B} 707 \\ 43 \end{gathered}$ | 269 | 219 | 249 | 148 | 5 | 6 |  | 6 |  | 130 | 11-1 | 08:23 |
| Take off, swoop, kull power | $\begin{gathered} \mathrm{B} 707 \\ 44 \end{gathered}$ | 263 | 145 | 248 | 158 | 6 |  |  |  |  | 130 | 11-1 | 08:27 |
| Take off, swoop, full power | $\begin{gathered} \text { B707 } \\ 45 \end{gathered}$ | 250 | 180 | 246 | 158 | 5 | 7 |  | 5 |  | 130 | 11-1 | 08:32 |
| Holding, level flight, all engines same power | $\begin{gathered} B 707 \\ 46 \end{gathered}$ | 251 | 240 | 230 | 218 | 6 | 2 |  | 4 |  | 128 | 11-1 | 09:31 |
| Holding, level flight, all engines same power | $\begin{gathered} B 707 \\ 47 \end{gathered}$ | 250 | 190 | 229 | 210 | 5 | 2 |  | 2 |  | 126 | 11-1 | 09:36 |


| Configuration | Run Label | Aircraft Displacement from Tower (ft) | Aircraft Altitude Abreast of Tower (ft) | $\begin{aligned} & \text { Aircraft } \\ & \text { Weight } \\ & (1000 \mathrm{lb}) \end{aligned}$ | Aircraft Speed (knots) | Temp. <br> $\left({ }^{\circ} \mathrm{C}\right)$ | Initial Wind Speed (mph) | Initial Wind Angle (deg from true $N$ ) | Final Wind Speed (mph) | Final <br> Wind <br> Angle <br> (deg from <br> true N) | Aircraft Heading (deg from mag. N) | $\begin{gathered} \text { Month- } \\ \text { Day } \\ (1972) \end{gathered}$ | Time <br> (EST) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Landing, level flight. all engines same power | $\begin{gathered} B 707 \\ 48 \end{gathered}$ | 277 | 215 | 228 | 137 | 5 | 2 |  | 4 | 350 | 128 | 11-1 | 09:40 |
| Landing, level flight, all engines same power | $\begin{gathered} \mathrm{B} 707 \\ 49 \end{gathered}$ | 272 | 206 | 227 | 134 | 6 | 4 |  |  |  | 126 | 11-1 | 09:44 |
| Landing, outboard engine away from tower at idle (Vortex 2) | $\begin{gathered} \mathrm{B} 707 \\ 50 \end{gathered}$ | 240 | 201 | 226 | 133 | 7 | 2 |  |  |  | 128 | 11-1 | 09:48 |
| Landing, outboard engine away from tower at idle (Vortex 2) | $\begin{gathered} \text { B707 } \\ 51 \end{gathered}$ | 278 | 219 | 223 | 135 | 6 | 3 |  | 4 |  | 130 | 11-1 | 09:58 |
| Landing, outboard engine toward tower a idle (Vortex 1) | $\begin{gathered} B 707 \\ 52 \end{gathered}$ | 256 | 219 | 221 | 134 | 6 |  |  | 4 |  | 127 | 11-1 | 10:03 |
| Landing, outboard engine toward tower at idle (Vortex 1) | $\begin{gathered} \text { B707 } \\ 53 \end{gathered}$ | 239 | 212 | 219 | 131 | 6 | 2 |  | 3 |  | 126 | 11-1 | 10:07 |
| Take off, level flight, all engines same power | $\begin{gathered} \mathrm{B} 707 \\ 54 \end{gathered}$ | 285 | 184 | 218 | 135 | 7 | 5 |  |  |  | 127 | 11-1 | 10:12 |
| Take off, level flight, all engines same power | $\begin{gathered} \mathrm{B} 707 \\ 55 \end{gathered}$ | 270 | 213 | 216 | 134 | 6 | 4 | 340 |  | * | 127 | 11-1 | 10:17 |
| Take off, swoop, full power | $\begin{gathered} \text { B707 } \\ 56 \end{gathered}$ | 285 | $164^{\circ}$ | 215 | 132 | 7 |  |  |  |  | 1264 | 11-1 | 10:23 |
| Take off, swoop, full power | $\begin{gathered} \text { B707 } \\ 57 \end{gathered}$ | 281 | 162 | 213 | 135 | 6 | 5 |  | 12 |  | 128 | 11-1 | 10:27 |
| Holding, level flight, all engines same power | $\begin{gathered} \text { B707 } \\ 58 \end{gathered}$ | 271 | 177 | 202 | 198 | 6 | 4 | 340 | 3 |  | 128 | 11-1 | 11:12 |
| Holding, level flight, all engines same power | $\begin{gathered} \text { B707 } \\ 59 \end{gathered}$ | 293 | 206 | 201 | 185 | 6 |  |  |  |  | 130 | 11-1 | 11:16 |
| Landing, level flight, all engines same power | $\begin{gathered} B 707 \\ 60 \end{gathered}$ | 340 | 206 | 200 | 131 | 6 |  |  | 4 |  | 128 | 11-1 | 11:20 |
| Landing, level flight, all engines same power | $\begin{gathered} \text { B707 } \\ 61 \end{gathered}$ | 273 | 220 | 199 | 124 | 7 |  |  |  |  | 130 | 11-1 | 11:25 |
| Holding, level flight, all engines same power | $\begin{gathered} \mathrm{B} 707 \\ 63 \end{gathered}$ | 250 | 150 | 192 | 290 | 6 |  |  |  |  | 130 | 11-1 | 11:33 |

## Appendix B

PROBABLE STABILITY CONDITIONS PREVALENT DURING SELECTED NAFEC FLYBYS

AT ATLANTIC CITY, N.J.
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Near neutral atmospheric buoyancy or stability conditions are likely to prevail $80 \%$ of the time at any given station. At night, during and very shortly after sunrise, an inversion layer usually exists in the surface boundary layer (region of shear stress almost constant with height). Thus, the near neutral conditions would tend toward the stable state during this period. This effect is due to a massive heat exchange by horizontal convection in the upper atmosphere as opposed to a negative to very small positive temperature rise in the surface boundary region. In its relatively non-dynamic state, the surface boundary layer will only experience a large temperature rise when the surface itself is well exposed to an appreciable solar radiation flux. Shortly after sunrise the neutral conditions will tend more toward the unstable state due to the surface heating and the resultant vertical convective processes. Heat exchange at higher altitudes is mostly a function of mass exchange due to horizontal pressure gradients and the earth's rotation and are relatively independent of the surface characteristics when the region of interest is confined to such a small scale as an airport. Radiosonde data taken at these higher altitudes will exhibit lapse rates which somewhat arbitrarily reverse signs and cover a somewhat larger variation in magnitudes.

In Lissaman, etal.(Ref. 5), the Pasquill classes were categorized in terms of various lapse rates. In addition, a qualitative description of meteorological conditions likely to be present during the various' Pasquill defined degrees of stability are given.

The tables presented in this appendix define the classes which would exist under the Pasquill criteria during the periods of interest (if the necessary data are available). The classes are suggested for: (1) the general meteorological conditions (from NOAA surface weather tables); (2) the lapse rate from 23 to 140 feet (from NAFEC tower data); (3) the lapse rate from approximately 200 to approximately 4000 feet (from radiosonde data); and (4) the lapse rate from 140 to approximately 200 feet (from NAFEC tower data in conjunction with the radiosonde data).

General meteorological conditions indicate that the expected stabilities for a given time of day were present in each case with the possible exception of the unusual trend of 17 October 1972. The tendency of the buoyancy conditions to remain more nearly neutral throughout the morning than normal may be explained by the air mass modification created by the impending frontal passage. The sharp temperature contrasts of 17 October and 18 October support this argument.

The lapse rates from 23 to 140 feet appear to be anomalous in magnitude and, in some cases, sign for all periods of interest. This phenomenon is possibly due to instrument error or high degree of inaccuracy.

As discussed previously, the lapse rates from approximately 200 to approximately 4000 feet do not give a true picture of stability. Even if linear trends of temperature change with height were exhibited these trends would most probably be inapplicable to the vertical region of interest.

Although the lapse rates between 140 feet and approximately 200 feet would be of value in establishing the conditions applicable to the vortex problem, the values computed are unrealistic due to the possible inaccuracy of the tower data and the fact that the lowest level radiosonde measurement is unreliable most of the time.

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| General Meteorological Conditions |  |  |  |  |  |  |
|  | $\begin{array}{ll} 8 & 8 \\ \ddot{-} & \ddot{9} \\ - & \ddot{m} \\ 1 & 1 \end{array}$ | $\begin{aligned} & \circ \\ & \hline-1 \\ & \dot{4} \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\sim} \\ & \stackrel{\sim}{\sim} \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{0} \\ & \stackrel{\rightharpoonup}{\circ} \\ & i \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 \\ & 0 \\ & 0 \\ & i \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{0} \\ & 0 \\ & i \end{aligned}$ |
| $\begin{aligned} & \stackrel{\rightharpoonup}{M} \\ & \stackrel{N}{\sim} \\ & \underset{\sim}{\circ}= \end{aligned}$ | $\begin{array}{ll} 0 & N \\ \hdashline & N \\ \infty & 1 \end{array}$ |  | $\underset{\sim}{\sim}$ | $\begin{gathered} \underset{1}{\prime} \\ \alpha \end{gathered}$ |  |  |


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| $\begin{aligned} & \stackrel{N}{N} \\ & \underset{\sim}{N} \\ & \stackrel{O}{\sigma} \end{aligned}$ | $\underset{\sigma}{ \pm}$ | $\begin{aligned} & 0 \\ & 1 \\ & 1 \\ & \sigma \end{aligned}$ |  |  | $\begin{aligned} & \underset{\sim}{1} \\ & 1 \end{aligned}$ |  |


| B <br> 0 <br> 0 <br> $\vdots$ <br> 1 <br> 0 <br> 0 <br>  |  |  |  |  |  |
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| $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & \vdots \\ & H \\ & 0 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ |  |  |  |  |  |
|  | $\begin{aligned} & 0 \\ & \stackrel{0}{0} \\ & i \end{aligned}$ | $\begin{aligned} & 0 \\ & \stackrel{0}{\infty} \\ & \infty \\ & i \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{0} \\ & \dot{\circ} \\ & i \end{aligned}$ | $\begin{aligned} & \stackrel{0}{i} \\ & \stackrel{i}{i} \end{aligned}$ |  |
|  | $\stackrel{\rightharpoonup}{\square}$ |  |  |  |  |




Appendix C
DESCRIPTION OF OUTPUT PLOTS OF WAKE VORTEX TRANSPORT COMPUTER PROGRAM

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Following is a brief description of the output plots (SC-4020) for the wake vortex transport computer program. The output consists of 14 pages of plots shown on pages $C-3$ through $C-16$. The first page represents a summary of input flags as used for analysis of Run 4 on 18 October 1972, and also the first portion of the wind field input description. All input flags are defined via comment cards in the computer program and are given in Appendix $D$ for easy reference. The wind field is defined by specifying the number of altitudes to be used in the curve fitting algorithm followed by a table defining the wind speed for both the horizontal and vertical versus altitude. This table is concluded on the second page. Next is the specified reference speed and altitude along with the exponent defining the power law curve fit required to represent the wind field over a continuous height. Following this is a temperature-altitude table for stability and density calculations. Page C-5 defines the variables for the temperature-altitude curve fit, the wind shear model parameters, the buoyancy model parameters, and a description of the ground wind array and sensor type. Page C-6 lists aircraft information required for the transport calculations and some of the basic quantities calculated in the program.

The display of the vortex tracks is initiated in the plot on page C-7. This plot is a cross sectional vortex track of altitude versus lateral distance referenced to the centerline of the aircraft flight path. Each plotting symbol indicates a time as defined by the user specified time increment. Page C-8 represents a cross sectional vortex track corresponding to the desired experimental condition. The current setup represents the NAFEC conditions with the lateral distance coordinate referenced to the NAFEC tower. The plotting characters initiating at the simulated aircraft are predicted values with the asterisks and $X$ s representing the starboard and port vortices, respectively. The measured vortex position as determined from the photographs are shown superimposed on the predicted tracks with the $S$ and $P$ corresponding to the starboard and port vortices, respectively. The solid line represents constant time lines and can be calibrated by the caption at the top of the plot.

Page C-9 is a time versus altitude track comparing predicted and photographic measurement. In the case for no wind shear, equal circulation and level flight, the starboard and port predictive tracks are identical as indicated by the double plotting character. Here again the $S$ and $P$ represent starboard and port vortex position obtained by measurement. Next is the reduced ground wind track comparing predicted and measured vortex positions. The lines represent predicted vortex position versus time with the $S$ and $P$ referring to photographic measurement and $R$ and $L$ referring to ground wind measurement of the right and left vortex, respectively. Page C-Il is the induced velocity (predicted) as a function of time for each ground wind sensor including a specified sensor response. The peaks are the predictive points shown in the previous plot. The remaining plots relate to either the wind field or the atmospheric characterization.

The plot on page $C-12$ is the measured (symbols) wind velocity for the five tower levels and the line through the data is the least square power law representation of the wind profile. Page C-13 shows the variation of wind direction with altitude for both the measured (symbols) and the least square quadratic representation (solid line) of the data. Pages C-14 and C-15 show the component wind profile for the lateral and longitudinal directions, respectively, for both the measured data and that calculated from the least square information of the previous two plots. The final plot (page C-16) represents temperature, pressure and density profiles for the altitude range of interest computed from the temperature data measured on the tower and the recorded surface pressure measured by NOAA,

RUN 48707 WIND PROFILE

| sinfut |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| ISIM | $=$ | \$1 |  |  |  |
| STIME | $=$ | . $000000505+00$ |  |  |  |
| FTIME | $=$ | . $16090900 \mathrm{E}+03$ |  |  |  |
| OTIME | $=$ | -20000000E+01 |  |  |  |
| JPRINT | $=$ | +1 |  |  |  |
| SpEED | $=$ | - $21250000 \mathrm{E}+03$ |  |  |  |
| WEIGHT | $=$ | -24700000E+96 |  |  |  |
| WSFAN | $=$ | . $14580009 \mathrm{E}+03$ |  |  |  |
| Ifloti | $=$ | +1 |  |  |  |
| IPLOT2 | $=$ | +3 |  |  |  |
| Ifunch | $=$ | +1 |  |  |  |
| LINE | $=$ | +1 |  |  |  |
| OTLINE | $=$ | .60000000E+01 |  |  |  |
| ISCALE | $=$ | +1 |  |  |  |
| YR | = | . $400000950+03$ |  |  |  |
| YL | $=$ | -.60000000E+03 |  |  |  |
| $2 T$ | $=$ | .25000000E+03 |  |  |  |
| FHIN | $=$ | -. 30000000E+02 |  |  |  |
| PMAX | $=$ | . $300050008+02$ |  |  |  |
| SENO |  |  |  |  |  |
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| Vor | $=$ | . $00000000 \mathrm{E}+00$ |  |  |  |
| ISIGHT | $=$ | +0 |  |  |  |
| SENC |  |  |  |  |  |
| SWIMDS |  |  |  |  |  |
| JWIND | $=$ | +3 |  |  |  |
| SWINDT | = | . $000000005+00$ |  |  |  |
| WINCD | $=$ | . $00000000 \mathrm{E}+00$ |  |  |  |
| NW | = | +5 |  |  |  |
| ALT | = | . $23000000 \mathrm{E}+02$, | . $45000000 \mathrm{E}+02$, | . $70000009 E+02$, | -10000000E+03, |
|  |  | . $14000000 \mathrm{E}+03$, | . 20000000E+03, | . O00000000E+00, | . $000000008+00$, |
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| PRESSG | $=$ | . $102630008+04$ |  |  |  |
| JTEMP | $=$ | +2 |  |  |  |
| NA | $=$ | +5 |  |  |  |
| ALTIT | $=$ | . 23009000E+02, | . $45000000 \mathrm{ta2}$, | . $70000000 \mathrm{E}+02$, | .10000000E+03, |
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| tehp | $=$ | . $29000000 \mathrm{E}+01$, | . 28000000E+01, | . $290000005+01$, | . $280000000+01$. |
|  |  | .27000000E+01, | . 20000000E+02, | .20000000E+02, | .20000000E+02, |
|  |  | .20000000E+02, | . 20000000E+02, | .20000000E+02, | .20000000E+02, |
|  |  | .20000000E+02, | . 20000000E+02, | . 20000000E+02, | .20000000E+02, |
|  |  | . $200000005+02$, | .20000000E+02, | . 20000000E+02, | .20000000E+02, |


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|  |  | .20000000E+02, | . $200000050 \mathrm{E}+52$, | . $25000000 \mathrm{E}+02$, | . $20000500 \mathrm{E}+02$, |
|  |  | .20900000E+52, | .200005005+02 |  |  |
| NPOLYT | $=$ | +1 |  |  |  |
| COEFT | $=$ | . $00000000 \mathrm{E}+00$, | . $00000000 \mathrm{e}+00$, | . $000000050+00$, | . $00000005 \mathrm{t}+00$, |
|  |  | . $00000005 \mathrm{E}+00$, | . $000900008+00$, | . $05005050 \mathrm{C}+00$, | . $000000005+09$, |
|  |  | . $00000000 \mathrm{E}+50$ |  |  |  |
| JFOTEN | $=$ | +1 |  |  |  |
|  |  |  | , |  |  |
| SENC |  |  |  |  |  |
| \$SHEAR |  |  |  |  |  |
| NROWS | $=$ | +0 | . |  |  |
| NCOLS | $=$ | +1 |  |  |  |
| HEIGHT | $=$ | . $00000000 \mathrm{E}+50$ |  |  |  |
| WIDTH | $=$ | . $00000000 \mathrm{E}+00$ |  |  |  |
| F | $=$ | .00000000E+00, | . $00000000 \mathrm{E}+60$, | . $00000000 \mathrm{E}+05$, | .00000000E +00 |
| SENO |  |  |  |  |  |
| sbuoy |  |  |  |  |  |
| SMIX | $=$ | . $000000008+00$ |  |  |  |
| ZCHECK | $=$ | . $500000008+03$ | - |  |  |
| 2CHEX = .SODOD00203 |  |  |  |  |  |
| SEND |  |  |  |  |  |
| SSENSOR |  |  |  |  |  |
| KSEN | $=$ | $+0$ |  |  |  |
| NSEN | = | +12 |  |  |  |
| YSEN | $=$ | . $55000000 \mathrm{E}+03$, | . $45000000 \mathrm{E}+03$, | . 350000000e+03, | .25000000E+03, |
|  |  | . $150000000+03$, | . $50000000 \mathrm{E}+52$, | -. 50000000E+02, | -. $15000000 \mathrm{t}+03$, |
|  |  | -. $25000000 \mathrm{E}+63$, | -. $35000000 \mathrm{E}+03$, | -.45000000E+03, | -.55000000E+03, |
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| ZSEN | $=$ | .60000000E+01, | . $600000005+01$, | . $60000000 \mathrm{E}+01$, | .60000000E+01, |
|  |  | .60000000E+01, | .60000000E+91, | . $60000000 \mathrm{E}+01$, | . $600000500 \mathrm{E}+01$, |
|  |  | .60000000E+01, | .60000000E+01, | .60000000E+01, | . $600000008+01$, |
|  |  | .00000000E+00, | . $000000000+00$, | .00000000E+00, | .050000000E+00 |
| PHI | $\underline{\square}$ | .27000000E +03 , | . $27000000 \mathrm{E}+03$, | . $27000000 \mathrm{E}+03$, | .27000000E+03, |
|  |  | .27000000et03, | .27000000E+03, | .27000000E+03, | . $27000000 \mathrm{E}+03$, |
|  |  | .27000000E+03, | . $270000005+03$, | .270000008+03, | .27000000E+03, |
|  |  | .27000000E +03 , | . $270000005+03$, | . $27090000 \mathrm{E}+03$, | .27000000E+03 |
| theta | $=$ | . $90000000 \mathrm{E}+02$, | . $90000000 \mathrm{E}+02$, | .99000000E+02, | .90000000E+02, |
|  |  | . $90000000 \mathrm{E}+02$, | . $900000008+02$, | .90000000E+02, | . $90000000 \mathrm{E}+02$, |
|  |  | .90000000E +02 , | . $90000000 \mathrm{E}+02$, | . $900000000 \mathrm{t}+02$, | . $900000000 \mathrm{E}+02$, |
|  |  | . $900000000 \mathrm{E}+02$, | . $90000000 \mathrm{E}+02$, | .90000000E+02, | . $90000000 \mathrm{E}+02$ |
| ISENS | $=$ | +0, | +0, | + 0 , | +0, |
|  |  | \$3, | 43. | 43, | 43, |
|  |  | +3, | +3, | +3, | +3, |
|  |  | +3, | +3, | 43, | +3 |

3END
run cata carc
CONFIGURATION LaNDING，outboarg engine abay froh tower at icle
AIRCRAFT TYPE IS B7GT
RUN NUMBER 4
AIRCRAFT CISFLACEMENT FROH TOWER 273 FT
aIrcraft al tituce abreast of tower 294 ft
ATRCRAFT WEIGHT 261000．FOUNCS
AIRSFEEC 244.9 FT／SEC
temperature 5 degrees $C$（not usec）
INITIAL WINC SFEEC 7 MFH （NOT USED）
Initial hind angle o degrees true（not used）
FINAL WINC SFEEC 5 MFH （NOT USEC）
FINAL WIND ANGLE 10 CEGREES TRUE（NOT USED）
alrcraft heacing 130 cegrees magnetic
HONTH 10 CAY 18 HOUR 7 HINUTE 59 LOCAL TIME

```
.NUTFUT
SPEEC = -.24490500E+03
WEIGHT = .261000SOE +56
WSFRN = .14200000E+03
SENC
sm.og
HSPR = .40058082E+01
CFOWER = .62449599E+00
COEF = -.44856098E+02, .32959656E+00, .25889222E-03, .12560241E+02,
    .00000000E+00, .000000000E+00, .00000000E+00, .00000000E+00,
    .000000000E+00
```


## SEND

GABHA IN FT＊\＃2／SEC $=3.84819925+03$
EDOY VISCOSITY INFI就／SEC $=5.06600792-01$
TEMPERATURE IN RANKINE $=4.96429741+02$
DENSITY IN SLUGS／FT中胡 $=2.48317368-03$
ACOUSTIC VELOCITY IN FT／SEC $=1.0922000$ THOS
STAB：LITYINI／SEC\＄ $2=0.00000000$
INITIAL PARAMETER （OIMENSIONLESS）$=0.00000000$



C-6


RUN 4 B707
FIRST TIME FOR S IS 22 FIRST IIME FOR F IS 38


C-8





C-12



C-14



C-16

Appendix D
DESCRIPTION OF INPUT REQUIREMENTS FOR LOCKHEED WAKE VORTEX TRANSPORT COMPUTER PROGRAM

This Appendix presents a summary of input namelist and input flag requirements for using the Lockheed Wake Vortex transport computer program.



D-2


| - |  | N |  | 4 | 1 l |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\omega \omega \omega \geq 0$ | z 2 | $\checkmark$ |  | $z$ | - |  |  |  |
| IEI m m | $0<0$ | 0 | $\cdots$ | - | + |  |  | $\geq 2$ |
|  | $\cdots 0$ | d | $z$ | 4 | $\checkmark$ |  |  | $\cdots$ |
|  | $\cdots \mathrm{n}$ | - | - | 6 | 0 | e | 1 | HEE |
|  | 를 | - | - | 0 | $\cdots$ | $>$ | 2 | N0. |

[^0]\[

$$
\begin{aligned}
& \begin{array}{l}
\text { NAMELIST IVORT) } \\
\text { VORTEX ALTITUDF ABOVE GROUNA } \\
\text { FLAG } \\
\text { ISIGHT }=O \text { PHOTOGRAPHIC INPUT IS NDT USED TO } \\
\text { ISIGHT }=1 \text { THETERMINE YORTEX STARTING POSITION } \\
\text { USEDTST PHOTOGRAPHIC YNPUT CARD IS } \\
\text { POSITION DETERMINE VORTEX STARTING }
\end{array}
\end{aligned}
$$
\]





[^1]


[^2]

Appendix E
SUMMARY OF LINE PRINTER OUTPUT OF LOCKHEED WAKE VORTEX TRANSPORT COMPUTER PROGRAM

## LINE PRINTER OUTPUT

Print out on Page E-7
(1) Title from title card
(2) Standard aircraft chosen; not printed if standard aircraft not chosen
(3) Namelist INPUT

The printing of variable STIME does not reflect the effect of the selection of first Photographic Input Card used to determine the vortex starting position.

The printing of variables SPEED, WEIGHT and WSPAN reflects the effect of (2) but does not reflect the overriding of the Run Data Card, if selected.
(4) Namelist VORT
(5) Namelist WINDS

Print out on Page E-8
(5) Continuation of Namelist WINDS

The printing of variables ALTR, WSPR, CPOWER, COEF and COEFT does not reflect the least squares computations.
(6) Namelist SHEAR
(7) Namelist BUOY

Print out on Page E-9
(8) Namelist SENSOR
(49) Altitude in feet of port vortex
(50) Horizontal position in feet of starboard vortex relative to tower
(51) Same as (47)
(52) Horizontal position in feet of port vortex relative to tower
(53) Same as (49)
(54) Rate of change in feet per second of the horizontal position of the sta rboard vortex
(55) Rate of change in feet per second of the altitude of the starboard
(56) Rate of change in feet per second of the horizontal position of the (57) Rate of change in feet per second of the altitude of the port vortex
(58) Distance between vortex centers in feet
(59) Horizontal separation between vortex centers in feet
(60) Altitude difference between vortex centers in feet
(61) Tilt angle in degrees from horizontal of line through vortex centers. Positive is in the counterclockwise direction.
(62) Same as (61) but in radians
(63) Rate of change of angle described in (61). Units are degrees per
(64) Same as (63) but units are radians per second
(65) Difference in circulation between the two vortices in square feet
(66) Cross flight path windspeed in feet per second
(67) Wind velocity component in direction ground wind sensor is pointed at sensor location in feet per second.
(68) Orthogonal wind velocity components in feet per second at sensor
69) The magnitude of the wind velocity in feet per second

Print out on Page E-13
Information from photographic data cards.
(70) Time in seconds from vortex creation for the following observed positions.
(71) Same as (50) except this is observed
(72) Same as (51) except this is observed
(73) Same as (52) except this is observed
(74) Same as (53) except this is observed
(75) Same as 58 except computed from observed position
(76) Same as (59) except computed from observed position
(77) Same as 60 except computed from observed position
(78) Same as (61) except computed from observed position
(79) Same as (62) except computed from observed position
(80) Same as (54) except computed from observed positions before and after
(81) Same as (55) except computed from observed positions before and after
(82) Same as (56) except computed from observed positions before and after
(83) Same as (57) except computed from observed positions before and after
(84) Same as (63) except computed from observed positions before and after
(85) Same as (64) except computed from observed positions before and after
(86) Difference in circulation between the two vortices necessary to cause the angular rate (84).
(87) Same as (66) except computed from observed positions before and after

Print out on Page E-14
Information from Ground Wind Data Cards
(88) Position from tower of ground sensor (in feet)
(89) Time in seconds from vortex creation when starboard vortex passes over ground sensor
(90) Time in seconds from vortex creation when port vortex passes over ground sensor
(91) Same as (80) except computed from positions observed by the ground sensor
(92) Same as (82) except computed from positions observed by the ground sensor
(93) Cubic curve fit coefficients of cross flight path wind profile. Program does not use this curve fit.
$V_{\text {wind }}=-2.13-0.236 \mathrm{H}+1.731 * 10^{-3} \mathrm{H}^{2}-4.644 * 10^{-6} \mathrm{H}^{3}$
0.511 is the standard deviation of the points from the cubic curve.





E-11
SGAMMA IN FTH2/5FC = 3.44867923403
(3) EDNY VISCCSITY IN FTOOTISEC $=4.74849720-01$ (41) DENSTTY TN SLUGS/FTW03 E $2.47358737-03$
(44) INTTIAL PARAMETER (DTMENSIDNLESSI = 0.0000000n






PORT DISPLACEMENT
2 5FPARATION 5.00
-2.00
-5.00
-9.75
$\circ$
$\stackrel{\circ}{\circ}$
$\stackrel{\circ}{0}$



PMOTEGEADH.C DATA TIME FROM VORTEX GFNERATION 1
STARANARO RISOLACEMENT OFZ AND HEIGMT 100
STAROGAF VORTEX TRANSPORT VELOCITY Y COMPONENT -
PMOTOGOAPH.- MATA TIME FRON VORTEX GFNERATION is 2 2n

PHOTOGRAPH. C GATA TIMF FROM VORTEX GFNERATION IS 27
PORT DISPLACEMEMT - 12 AND HEIGHT E4
$Z$ SFPARATION $5.00 \quad$ ANGLE FROM HORIZONTAL $Z$ COMPONENT
$Z$ COMPONENT
RUNWAY WIND VELOCITY
CROSS RUNWAY WIND VELOCITY

PORT DISPLACEMENT -68 AND HEIGHT 73
$Z$ SEPARATION $3 . O D \quad$ ANGLE FROM HORIZONTAL
2.400-02

8
$\stackrel{8}{6}$


Appendix $F$
FLOW CHARTS FOR LOCKHEED WAKE VORTEX TRANSPORT COMPUTER PROGRAM
$\square$
1

I


Following is a detailed flow chart of the Lockheed Wake Vortex Trans port Computer Program. A simple block flow chart is presented at the conclusion of this Appendix to aid the user in establishing the general calling sequences.










F-10

Appendix G
SUMMARY OF PREDICTED WAKE VORTEX TRACKS AND COMPARISON WITH EXPERIMENT


## LIST OF RUNS PROVIDED IN THIS APPENDIX

| Aircraft Type | Run Number | Date (1972) | Page |
| :---: | :---: | :---: | :---: |
| DC6 | 79 | 19 August |  |
|  | 81 |  |  |
|  | 83 |  |  |
| , | 84 |  |  |
| $\dagger$ | 85 | $\dagger$ |  |
| B747 | 1 | 16 September |  |
| 1 | 2 |  |  |
|  | 3 |  |  |
|  | 4 |  |  |
|  | 5 |  |  |
|  | 6 |  |  |
|  | 7 |  |  |
|  | 8 |  |  |
|  | 9 |  |  |
|  | 10 |  |  |
|  | 11 |  |  |
|  | 12 |  |  |
|  | 15 |  |  |
|  | 16 |  |  |
|  | 17 | $\dagger$ |  |
|  | 27 | 17 September |  |
|  | 30 |  |  |
|  | 31 | I |  |
|  | 33 | $\dagger$ |  |
|  | 55 | 17 October |  |
|  | 56 |  |  |
|  | 57 |  |  |
|  | 58 |  |  |
|  | 59 |  |  |
| + | 60 |  |  |
| 7 | 63 | $\downarrow$ |  |
| B707 | 6 | 18 October |  |
| 1 | 7 |  |  |
|  | 8 |  |  |
|  | 9 |  |  |
|  | 10 |  |  |
|  | 13 |  |  |
|  | 15 |  |  |
|  | 18 |  |  |
| , | 20 |  |  |
| $\checkmark$ | 21 | $\dagger$ |  |

## LIST OF RUNS (Concluded)

| Aircraft Type | Run Number | Date (1972) | Page |
| :---: | :---: | :---: | :---: |
| B707 | 26 | 18 October |  |
| 1 | 29 | 18 October |  |
|  | 31 |  |  |
|  | 32 | $\dagger$ |  |
|  | 34 | 1 November |  |
|  | 35 |  |  |
|  | 37 |  |  |
|  | 40 |  |  |
|  | 41 |  |  |
|  | 42 |  |  |
| 1 | 43 |  |  |
| $\dagger$ | 46 | $\gamma$ |  |




$$
\mathrm{G}-4
$$




FIRST TIME FOR 5 IS 16
FIRST TIME FOR F IS 26


$G-10$











































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$$
\mathrm{G}-77
$$



















































RUN $37 \quad$ B707
FIRST TIME FOR S IS 30



















Appendix H
REPORT OF INVENTIONS
$\qquad$

After a diligent review of the work performed under this contract, no new innovation, discovery, improvement or invention was made.


[^0]:    

[^1]:    
    

[^2]:    
    

[^3]:    otsplacement from toner in feet

