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**USER'S MANUAL FOR GENERALIZED ILSGLD-ILS
GLIDE SLOPE PERFORMANCE PREDICTION:
MULTIPATH SCATTERING**

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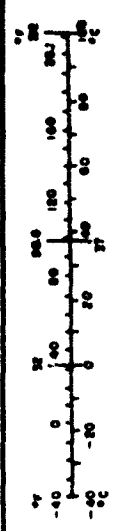
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17. Abstract This manual presents the computer program package for the generalized ILSGLD scattering model. The text includes a complete description of the program itself as well as a brief description of the ILS system and antenna patterns. The program listings are included as appendixes, and contain both input-generation programs and output-plotting programs. For a technical mathematical analysis of the system see the FAA report, "ILS Glide Slope Performance Prediction: Multipath Scattering." The present report is a partial revision of part II of report FAA-RD-74-157B. The revisions include the treatment of scattering from randomly oriented rectangular surfaces.			
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PREFACE

This document is a companion document to the Federal Aviation Administration report, "ILS Glide Slope Performance Prediction: Multipath Scattering," and contains the computer program for applying the model developed in the aforementioned report. The computational program may be used to predict the performance of new ILS glide slope systems, or modified existing systems. The manual contains a complete description of the glide slope system, the program listings, and step-by-step instructions for running the computer program.

METRIC CONVERSION FACTORS

Approximate Conversions to Metric Measures				Approximate Conversions from Metric Measures			
Symbol	When You Know	Multiply by	To Find	Symbol	When You Know	Multiply by	To Find
LENGTH							
in	inches	2.5	centimeters	cm	centimeters	0.04	inches
ft	feet	30	centimeters	cm	centimeters	0.4	inches
yd	yards	0.9	meters	m	meters	3.3	yards
mi	miles	1.6	kilometers	km	kilometers	1.1	miles
						0.6	miles
AREA							
sq ft	square feet	0.9	square centimeters	cm ²	square centimeters	1.2	square inches
sq yd	square yards	0.8	square meters	m ²	square meters	1.2	square yards
sq mi	square miles	2.6	square kilometers	km ²	square kilometers	0.4	square miles
ac	acres	0.4	hectares	ha	hectares (10,000 m ²)	2.5	acres
MASS (weight)							
oz	ounces	28	grams	g	grams	0.035	ounces
lb	pounds	0.45	kilograms	kg	kilograms	2.2	pounds
	short tons (2000 lb)	0.9	tonnes	t	tonnes	1.1	short tons
VOLUME							
cup	cup	5	milliliters	ml	milliliters	0.03	fluid ounces
tblsp	tablespoons	15	milliliters	ml	milliliters	0.5	tablespoons
fl oz	fluid ounces	30	milliliters	ml	milliliters	1.06	fluid ounces
c	cup	0.24	liters	l	liters	0.24	quarts
qt	quarts	0.97	liters	l	liters	0.95	quarts
gal	gallons	3.8	liters	l	liters	3.8	gallons
cu ft	cubic feet	0.03	cubic meters	m ³	cubic meters	0.03	cubic feet
cu yd	cubic yards	0.76	cubic meters	m ³	cubic meters	1.3	cubic yards
TEMPERATURE (exact)							
F	Fahrenheit temperature	5/9 (after subtracting 32)	Celsius temperature	C	Celsius temperature	9/5 (then add 32)	Fahrenheit temperature



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1. INTRODUCTION: DEFINITION OF INSTRUMENT LANDING SYSTEM

In a previous report,* a computer program (ILSGLD) was written to simulate certain terrain conditions which affect the glide slope portion of the Instrument Landing System (ILS). The ILSGLD model was developed to treat one-dimensional terrain variations. This report describes a generalized version of ILSGLD which treats two-dimensional ground plane variations, and which is able also to simulate the effects of scattering from planar, randomly oriented rectangular surfaces. A technical mathematical analysis of the system is described in a separate report.**

The ILS is used to provide signals for the safe navigation of landing aircraft during periods of low cloud cover and other conditions of restricted visual range. Separate systems are used to communicate vertical and horizontal information; the vertical system is called the "glide slope." This system operates by the transmission of an RF carrier, amplitude modulated by two audio frequencies, and beamed to approaching airborne receivers. In an instrumented aircraft, the glide slope receiver serves to demodulate the RF signal, amplify and isolate the corresponding audio signals and derive a signal to drive the ILS vertical display in the cockpit. The pilot, by reading the display, can determine if he is on course, above or below the glide path. These signals must be strong enough to cover a radius of 15 miles in front of the antenna.

* "ILS Glide Slope Performance Prediction," FAA RD 74-157B, Part II. 9/74.

** FAA, ILS Glide Slope Performance Prediction: Multipath Scattering, In Preparation.

The directional information is determined by the relative strengths of the transmitted sideband signals. The audio frequency modulations, which are fixed at 90 and 150 Hz, are radiated in different angular patterns with respect to the intended glidepath. The "course" is defined as the locus of points where the amplitudes of the two modulations are equal. The display of a difference of the amplitudes (90 and 150 Hz) of the sidebands is referred to as the Course Deviation Indication. Thus, the CDI is the pilot's indication as to what his deviation is relative to the glidepath. The CDI is measured in microamperes. The actual course generated by any particular ILS installation will deviate from the ideal because of irregularities in the terrain. The deviation of the CDI caused by these irregularities, from the ideal receiver reading at that point in space (e.g., on the glidepath a CDI reading other than 0) is the derogation effect.

The glide slope system transmits an asymmetrical pattern by beaming a "carrier plus sideband" pattern and a "sideband only" pattern, the composite of which gives the desired effect.

2. ANTENNA PATTERNS

The proper angular variation of the transmitted 90 and 150 Hz modulation is achieved by the radiation of the two independent sideband patterns by the transmitting antenna. One pattern, the "carrier plus sideband" (C+S) signal, is radiated in a symmetrical pattern; the other pattern, the "sideband-only" (SO) signal, is radiated in an "anti-symmetrical" pattern relative to the prescribed glide angle (see Figure 1).

The C+S signal is composed of a carrier wave and paired sideband waves at 90 and 150 Hz. The sideband amplitudes are equal and represent a 40 percent modulation of the carrier wave (or a "depth of modulation" of 0.4) at both frequencies. The SO wave is a carrier wave that is equally modulated at 90 and 150 Hz to the extent that it retains no pure carrier component.

The spatial modulation pattern obtained by combining the symmetrical C+S pattern with the "anti-symmetrical" SO pattern is illustrated in Figure 1. At a given receiver point the total signal is the C+S carrier plus the combined sideband amplitudes of the C+S and SO patterns. The sideband amplitudes are phased so that above the glide path the 90 Hz amplitudes add and the 150 Hz amplitudes subtract, while below the glide path, the 90 Hz amplitudes subtract and the 150 Hz amplitudes add.

Any angular deviation of the airplane's receiver from the correct course results in a "Difference in Depth of Modulation" (DDM) between the 150 and 90 Hz signals. Since the strength of C+S and SO signals fall off at the same rate with distance from the transmitting antenna, the DDM is independent of range.

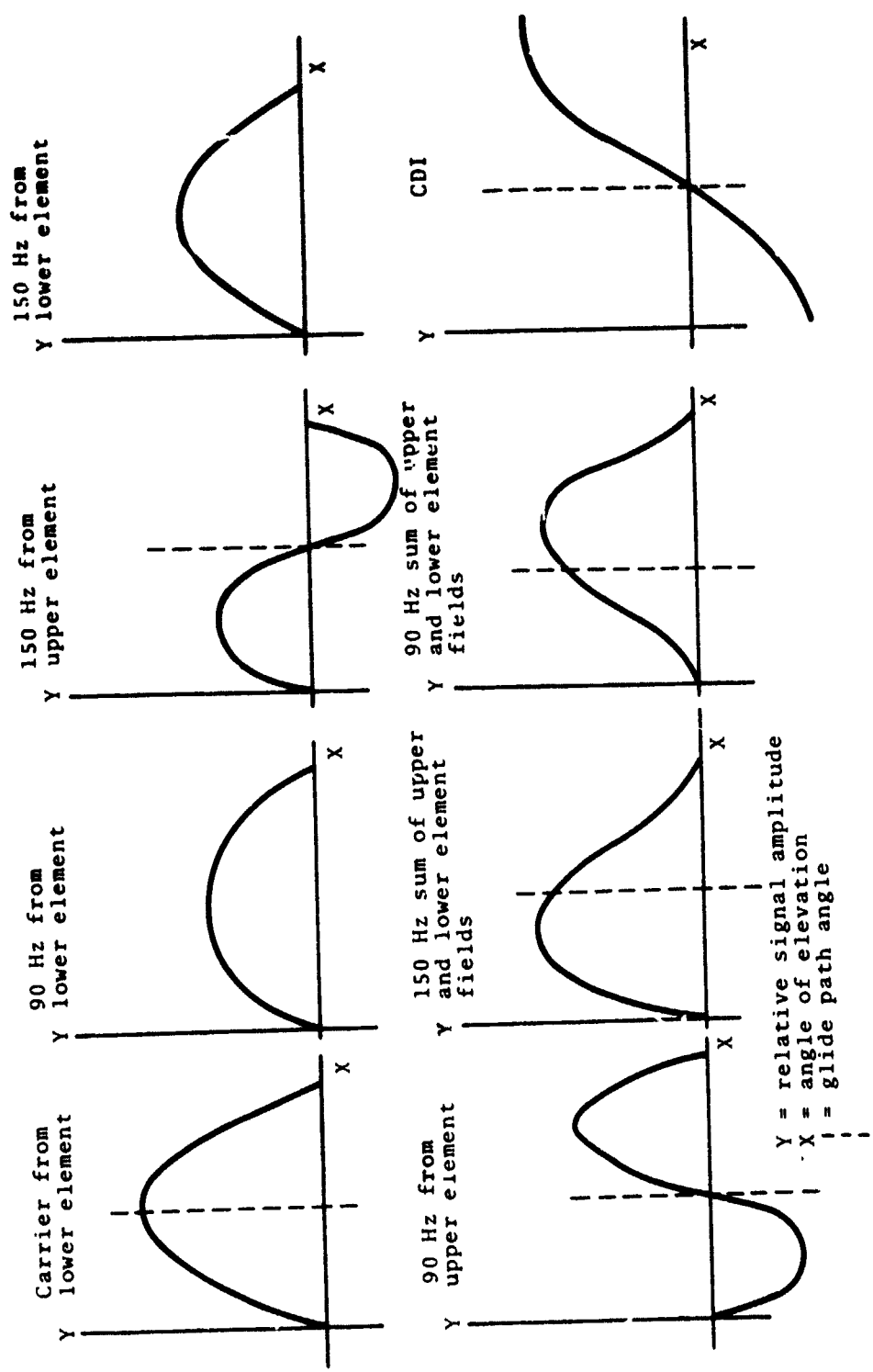


FIGURE 1. ANTENNA PATTERNS FOR NULL REFERENCE ANTENNA

The antenna patterns are generated by using arrays of one or more elements in combination with the ground as reflector. The effect of an ideal ground plane on a single element is as though there was an "image" element located below the ground and radiating equal power to the real element but with opposite phase. In a glide slope array there will be two or more elements radiating different signals to give the desired combined antenna pattern. (Note that this means that a glide slope array is defined by giving, for each element, its location and complex amplitude of the carrier and sidebands.) However, the real ground is not an ideal plane. This has the effect of distorting the element patterns and results in a derogation of the glide slope system performance.

The extended glideslope derogation simulation package consists of five programs. They are:

- FMAKE.F4 Used to generate input files for the simulation.
- ILSVEN.F4 Simulates the one-dimensional-variation ground. Takes input prepared by FMAKE. Outputs the complex field intensities at the various receiver locations.
- MOLE.F4 Simulates the scattering from a rectangular planar surface with arbitrary orientation. Takes as input the data output from ILSVEN. Outputs a new set of fields.
- GLDCDI.F4 Simulates the effects of the receiver, including CDI determination and dynamic smoothing from the instrumentation.
- GLDPLT.F4 Produces graphical presentations of the CDI results from the simulation. Takes as input the data file

output from GLDCDI. Outputs graphs of various forms as determined by the user.

The inputs and operation of these programs will be given in the following sections.

The basic procedure is to prepare the input with FMAKE. The ground effects are determined by running ILSVEN. The output is a data file containing the antenna descriptors, the receiver locations and the complex field intensities for the carrier and sidebands. If desired GLDCDI may be run at this point to produce the CDI's that would be produced by this ground configuration, antenna system, and flight path. If additional scatterers are involved such as buildings or hills, they may be represented as rectangular surfaces and the derogation effects added with MOLE. MOLE may be used as often as needed to include any number of scattering surfaces. After all surfaces have been included GLDCDI is run to generate the CDI file for input to the graphing program. GLDPLT is then run to generate the graphs required.

3. GROUND EFFECT SIMULATION WITH ILSVEN

The ILSVEN program simulates the effects of a non-planar ground on the glide slope antenna system.

The program uses a ground description, an antenna description and a set of spatial coordinates for the receiver locations as input. The program calculates the outputs for each receiver location, the complex values of the fields for carrier and sidebands that would be received at that location. This represents the summation of the direct fields from each antenna element and the fields from each antenna element scattered from the parts of the ground "plane." Additionally the fields that would be produced by an ideal ground plane are included. This allows comparison with flights that do not have a simple ideal CDI along the flight path, for example, flights at right angles to the glide path such as are used to determine the course width.

The ILSVEN simulation makes certain simplifying assumptions. They include:

- a. Perfectly reflecting ground surface
- b. Far-field scattering--all scattering from points on the ground surface is assumed independent of all other points; thus multiple reflections and near-field interactions are ignored
- c. Noise-free environment
- d. Relative field strengths--the absolute field strengths involved are not calculated. Thus, while the CDI's can be calculated in microamperes, the absolute electric field intensities are not ascertained,

e. Geometric shadowing--the shadowing of one portion of the ground on another is done by straight ray approximations assuming a total cutoff with no diffraction, and

f. Antenna elements are assumed to be simple dipoles.

3.1 METHOD OF SIMULATION

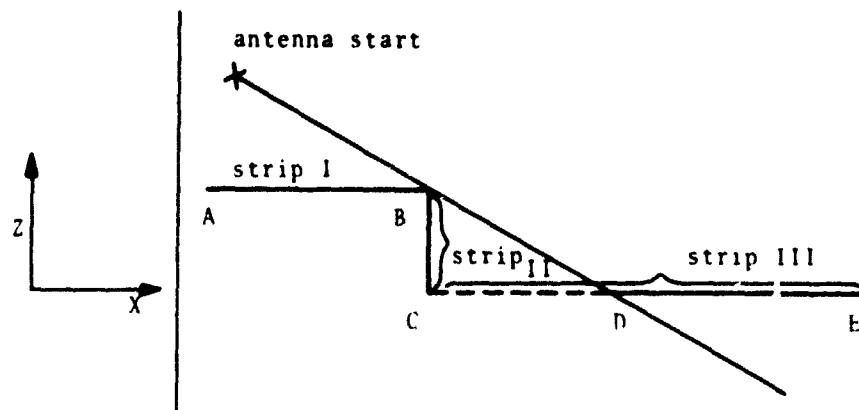
An antenna element is described by giving its x , y - and z -coordinates and the complex amplitudes of its radiated amplitude at the three frequencies (carrier, 150 and 90 Hz sidebands). The ground is broken up into strips; these strips have an infinite width and a finite length. The infinite extent is parallel to the y -axis, that is at a right angle to the runway centerline. Thus, a ground strip is described by giving the x and z -coordinates of the leading and trailing edges of the strip. A receiver location is described by giving its x -, y - and z -coordinates.

The basic part of the simulation consists of calculating the field at a receiver location. This field is caused by the power radiated from an element and reflected from a strip. The receiver field can be expressed as a complex gain factor times the radiated antenna field. This gain factor is expressed as a double integral over the strip. The integration along the infinite extent (y axis direction) was approximated by using the stationary phase method. The resulting single integral is solved by a modified trapezoid rule. The trapezoid rule is used with the spacing between sample points adjusted for the derivative of the integrand.

Thus, for a given receiver location, the program takes an antenna element and calculates the "gain factor" for each ground strip, multiplies by the radiated power, and sums the three complex

field intensities for all ground strips. The direct field of the element at the receiver is then added. This process is repeated for all elements, giving the total field at the receiver. For comparison purposes the fields resulting from an ideal ground plane are calculated. The location of the receiver (x-, y-, z- and t coordinates) are output along with the six complex field intensity numbers. This is then repeated for each receiver location in the input file.

If the terrain is sufficiently irregular, part of the energy radiated toward a point on the ground may be intercepted by another piece of the ground closer to the antenna. This shadowing is complex including, as it does, diffraction as well as reflection. This is approximated in the simulation by using ray optics; that is, the shadow is assumed to have no diffraction at the edges and a zero field amplitude inside of the shadow. The program does this by assuming the ground is continuous; i.e., the far edge of one strip is the near edge of the next, and keeping track of the "furthest" (in angular sense) edge. If part (or all) of the next strip is "below" that edge, then that part (or all) will not be included in the trapezoid integration. For example in the sketch below:



all of strip I, none of strip II and that part of strip III between D and E will be included in the integration.

For the receiver antenna a "semi" directional antenna is assumed; that is, only the incident fields from the front half-sphere around the receiver are included. This is as though an omni-directional antenna was used but blocked by the fuselage from receiving signals from the direction of the tail. This is done in the program by stopping the summation of fields over the ground strips at a point directly below the receiver.

The back half-plane is assumed to be an ideal flat horizontal reflector of infinite extent. The field from this is included by adding the "gain factor" for this as an initial strip to that calculated by integrating over the "real" strips.

3.2 OPERATION

ILSVEN assumes the ground description is a file called GRND.DAT, and that the receiver locations are in a file called PATH.DAT. The user starts the program and then inputs the name of the file containing the antenna description. The simulation will be run, and the output will be found in file STRIP.DAT.

4. ADDITION OF SCATTERERS WITH MOLE

MOLE is used to include the derogation effects of finite scatterers. This would include sides of buildings and other man-made objects composed of flat rectangular surfaces. In addition portions of the ground surface such as hills can be simulated if they may be represented by rectangular pieces. The program takes as input a file generated by ILSVEN. This contains the antenna and flight path descriptions along with the complex fields scattered from the ground for both the non-planar ground simulated and for the ideal ground case. The program adds to these fields the fields resulting from scattering from the piece being simulated and outputs a new data file containing the input data with revised values for the complex fields. The output file being in the same format as the input file allows this output to be used as the input for another run of the MOLE program. This permits the user to continue to add in the effects of as many scatterers as desired.

The simulation makes certain simplifying assumptions. They include those explained for ILSVEN. In addition, the ground surface for the MOLE simulation is assumed to be the ideal flat horizontal ground plane. Thus the multiple reflections from the antenna element to ground to scatterer, and from scatterer to ground to receiver, are done using a simple ground plane.

To operate the program the user will have previously run ILSVEN to simulate the terrain involved. When MOLE is run, the program will request:

INPUT FILE NAME:

The user types in the name of the file output from ILSVEN. This is initially named STRIP.DAT, but may have been renamed by the user if there is more than one simulation to be done.

The program will then request:

OUTPUT FILE NAME:

The user then types in the name to be given to the file to be output from MOLE. This file will contain the modified filed values in addition to the antenna and flight path data from the input.

The program will then read in the piece description data from unit 20. (Normally, it is a disk file FOR20.DAT.) These data are in free-field general FORTRAN format (3G). The data consist of the x-, y-, and z-coordinates for the four corners of the rectangle, one set of coordinates per line. The corners are described in the order that they would be scanned in traveling around the perimeter of the rectangle in a clockwise direction. In this sense, the rectangle is assumed to be facing the user. For example, the coordinates:

0.0.0,
1.0.0,
1.0.1, and
0.0.1,

describe a square, one foot on a side, situated on the centerline of the runway oriented with one side on the centerline on the ground, and one side vertical at the origin. The "front" of the square is facing in the positive y-direction. See figure example (Figure 2).

The program will then execute the simulation, output the new file, and terminate. Multiple runs, scatterers and input cases may be set up using the usual batch control features.

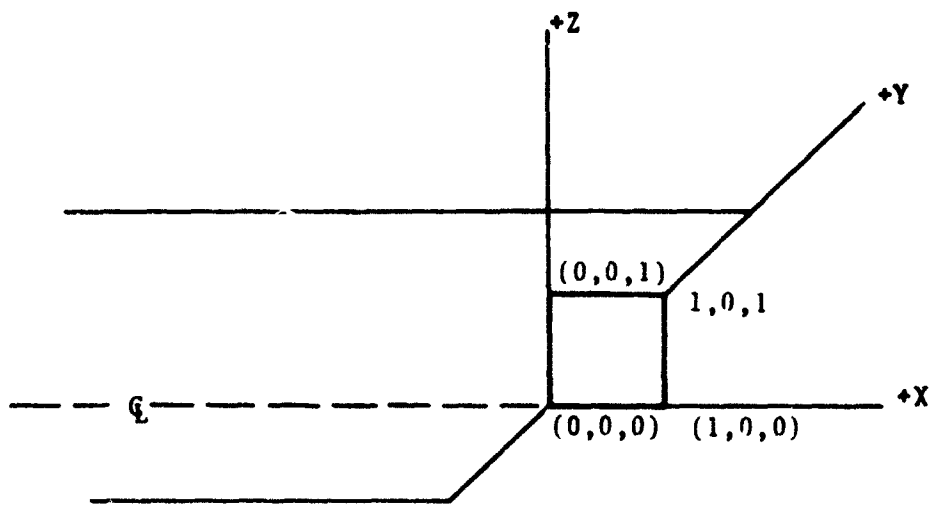


FIGURE 2. REPRESENTATION OF SQUARE SCATTERER

5. CDI DETERMINATION USING GLDCDI

The output files from ILSVEN and MOLE contain the complex field intensities for the carrier and sidebands for the cases simulated. For analysis purposes the user would usually wish to see the CDI's produced. The difference between these and the correct CDI's is the derogation that would affect the pilot in the case being studied. This CDI generation is done by GLDCDI. The program will calculate the CDI for both the static case and for a dynamic case using the smoothing time constant input in FMAKE.

To operate the program the user runs GLDCDI. The program will request:

INPUT FILE NAME:

The user then types in the name of the file (generated by ILSVEN or MOLE). The program will then request:

OUTPUT FILE NAME:

The user then types in the name of the file to be used for the output file. The program will then execute and terminate. The output file contains the CDI's static and dynamic for both the simulation and the ideal ground case. The various CDI's may be graphic using GLDPLT.

6. FMAKE PROGRAM DESCRIPTION

FMAKE is a file generation program used to create input files for ILSVEN. It is designed to be used interactively. The user starts by running the program. The program will respond by typing:

INPUT SWITCH:

The user then types in a single character switch, followed by a <CR>, for the file he wishes to generate. The program will then respond with a request for the input required for that file. If a blank is used as the input switch the program will terminate. If any character other than those explained below are used, an error message will be given. After each file is generated, the program will return to the switch input point thus allowing the user to generate the data files for many simulation runs in one sitting.

(N.B. All units are in feet unless otherwise stated)

6.1 SWITCH: Y

For this switch (Y), the program will type:

INPUT YO, LAMBDA:

The user then inputs in free field format the y-offset (i.e., the y-coordinate) of the antenna elements and the wavelength of the carrier, followed by a <CR>. The y-offset is the distance from the base of the antenna to the centerline of the runway. As this information is required for both the antenna description and the flight path, it is input with a separate switch to avoid repetition.

6.2 SWITCH: G

This switch (G) is used to input the ground description.

The program will respond with:

INPUT GROUND FILE NAME:

The user then inputs a <five(5) character name for the ground description file, followed by a <CR>. ILSGLD requires the ground file to be called GRND.DAT. (The .DAT extension is a system default.) FMAKE allows the user to generate several ground files with different names at one sitting. Then by using system renaming commands, a single batch job may be set up that will run many simulations without further user interactions.

The program will then type:

INPUT GROUND LABEL.

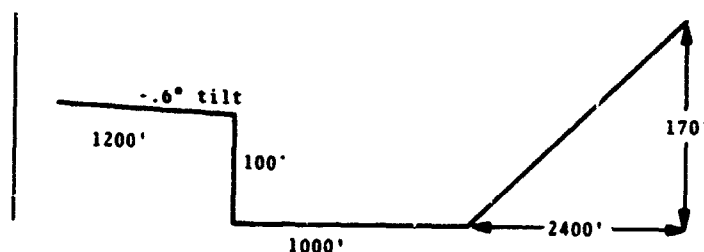
The user then inputs up to 40 characters to be used as a label for this ground description. The label is carried in the ground description file and will be placed in the output file by ILSGLD. It allows the GLDPLT program to label the plots with the ground description. This is necessary if a batch job generates plots from more than one simulation.

The program will then type:

INPUT GROUND SEGMENTS. STARTING FROM ANTENNA GIVE CONSECUTIVELY EITHER X AND Z INCREMENTS OR THE LENGTH AND ANGLE FROM HORIZONTAL IN DEGREES, SEPARATED BY A ZERO. HIT CARRIAGE RETURN FOR END OF DATA, OR IF THERE ARE NO MORE STRIPS.

The user inputs ground strip end points in either Cartesian or polar increments using two or three fields respectively. They are input in floating free field format followed by a <CR>. The first point is taken relative to the origin and is the near edge of the closest strip to the antenna. The second point is the far edge of the first strip and the near edge of the second strip.

This second point is relative to the first. This will continue for additional strips until a <CR> is hit with no data, at which point the program will return to the switch input. For example to input this profile:



The input would be

```
0.,0.  
1200., 0., -.6  
0., -100.  
2400., 170.
```

There is a maximum of 20 strips allowed in both FMAKE and ILSGLD. This is determined by array sizes and could be changed if desired.

6.3 SWITCH: P

This is used to generate a flight path file. The program will respond:

INPUT FLIGHT PATH FILE NAME:

The user then inputs a five (5) character file name (the name must be exactly 5 characters). ILSGLD requires the flight path to be in

a file called PATH.DAT (for explanation of multiple files see SWITCH:G). The program will then type:

INPUT FLIGHT PATH TITLE:

The user then inputs a title, using up to 40 characters, for the flight path. This is used as a label on the plots output by GLDPLT. The program will then type:

INPUT FLIGHT PATH TYPE:

The user has a choice of two flight path types, linear or hyperbolic. For a linear flight path, type a <CR>; for a hyperbolic path type a 'G' followed by a <CR>. When it is a linear flight the program will respond:

INPUT X0, Y0, Z0:

The user then inputs the x-, y-, and z-coordinates of the first receiver point in free field floating point format followed by a <CR>. The program will respond:

INPUT XF, YF, ZF:

The user then inputs the final receiver location in the same way. The program then types:

INPUT # OF POINTS, VELOCITY, TIME CONSTANT:

The user then inputs the total number of receiver locations desired in integer free field format, followed by the velocity of the aircraft in feet/sec. in floating point free field and the time constant in seconds (usually 0.4) used for the "inertia" of the receiver in dynamic simulation. The program will then generate the data file and return to the SWITCH POINT.

The actual ideal surface of zero CDI is a hyperboloid of two sheets whose axis of rotation is parallel to the z-axis and passes through the antenna. For comparison purposes it is convenient to

have the aircraft travel along this surface and see how the real CDI deviated from 0. If the glide path is used for linear flight in the near field (between threshold and antenna) large CDI's will occur because of the hyperbolic shape. The program will allow the user to generate a hyperbola which is the intersection of the 0 CDI surface and the plane containing the runway centerline parallel to the z-axis. To do this the user types a 'G' for the flight path type. The program will respond:

INPUT XO, XF, H:

The user inputs these in floating point free field format followed by a <CR>. XO is the x-coordinate of the initial receiver point (YO is zero and ZO is specified by the hyperboloid), XF is the x-coordinate of the final receiver point. H is the height of the main carrier element in the antenna array. The program will then respond:

INPUT # OF POINTS, VELOCITY, TIME CONSTANT

These are input as above. The program will generate the file and return to the switch point.

6.4 SWITCH: A

This switch is used to generate the antenna description file. The program will respond:

INPUT ANTENNA FILE NAME:

The user inputs the 5 character file name. The program will type:

INPUT ANTENNA DESCRIPTION:

The user inputs a <40 character antenna description to be used as a plot label. The program will then type:

INPUT ELEMENT VALUES:

The user then types in, in free field floating format, a maximum of 8 fields followed by a <CR>. The fields have the following use:

<u>field #</u>	<u>use</u>
1	x-coordinate of element (usually 0)
2	z-coordinate of element (height)
3	real amplitude of carrier
4	imaginary amplitude of carrier
5	real amplitude of 150 Hz side band
6	imaginary amplitude of 150 Hz side band
7	real amplitude of 90 Hz side band
8	imaginary amplitude of 90 Hz side band

This element inputting is repeated for each element. After the last element is input an extra carriage return is typed. No y-coordinate is input for the elements. This is because nominally all the elements have the same y offset (the value input as Y0 under switch:Y). However, a small offset correction is applied for near field correction. An explanation of this correction may be found in part I (see discussion preceding Eq. (33)). This is automatically done by the program. As the first element input is assumed to have the correct offset, it will always have a value of Y0. Thus the main carrier element should be input first, for example, a null reference antenna was input as follows:

```
INPUT SWITCH: Y
INPUT Y0, LAMBDA: 300., 3.
```

7. GLDPLT PROGRAM DESCRIPTION

GLDPLT is a plotting output program to graph the CDI information from GLDCDI. The user runs GLDPLT which then types:

INPUT FILE NAME AND AXIS TYPE:

The user then types in a 5 character (left-justified and blank filled to 5 characters) and two integer fields in free field format. The first integer is the switch for x-axis type and the second integer is the switch for the y-axis. The y-switch has two values, 1 and 2, the x-switch has three 1, 2, and 3; any other values will terminate the program.

The switches have the following use:

y-switch=1 this plots the static CDI values

y-switch=2 this plots the dynamic CDI values

x switch=1 this uses the altitude angle, in degrees measured from the origin of the receiver point as x-coordinate

x-switch=2 this uses the x-coordinate of the receiver as the x-axis

x-switch=3 uses the time in seconds, at the receiver point, as the x-coordinate.

After the input, a plot is generated and the program returns to the input and asks for the data for the next plot. The user can give the same file name to plot the data differently, or a new file name can be given. This would be done when multiple runs were done before plotting, the output file from each simulation run carrying its own name.

INPUT SWITCH: A

INPUT ANTENNA FILE NAME: NULL

INPUT ANTENNA DESCRIPTION

NULL REFERENCE ANTENNA

INPUT ELEMENT VALUES

0., 15., 1., 0., .4, 0., .4, 0.

0., 30., 0., 0., -.12, 0., .12, 0.

APPENDIX A ILSVEN

```

1      DIMENSION ILABL(8)
2      DIMENSION IPTDAT(33)
3      COMMON /PLKT/ NRP,RXNN,RXNY,RXF,RXLY,RVNN,RVNY,RVFT,RVLY,
4      1R2NN,R2MX,R2FT,R2LY,R3NN,R3MX,R3FT,R3LY,
5      2A1NN,A1MX,A1FT,A1LY,ARNN,ARMX,ARFT,ARLY,
6      3ADIN,ADIN,ADIF,ADIL,
7      4ADRN,ADRX,ADRF,ADRL
8      EQUIVALENCE (IPTDAT(1),NRP)
9      IMPLICIT COMPLEX (C)
10     DIMENSION X(20),Y(20),Z(20)
11     DIMENSION CF1(20),CF2(20),CF3(20)
12     IMPLICIT DOUBLE PRECISION (D)
13     COMMON /REC/RX,RV,RZ,RT,NSIZE
14     REAL LAMBDA
15     COMMON /GROUND/ K,X1(20),Z1(20),X2(0/20),Z2(0/20),IEL
16     COMMON /ANT/AX,AY,AZ,LAMBDA,DAK,DPI
17     COMMON /VAL/ HR,HI
18
19     C      THIS VALUE OF TWO PI IS INITIALIZED THIS WAY TO AVOID USING
20     C BLOCK DATA
21     C      DPI=6.2831853071795864769
22
23     C      THIS OPENS THE OUTPUT FILE
24     C      CALL OFILE(1,'STRIP')
25
26     C      THIS SUBROUTINE OPENS THE FLIGHT PATH FILE AND RETURNS WITH
27     C THE FLIGHT PATH PLOT LABEL (ILABL) AND TIME CONSTANT (TAU)
28     C THE FILE WAS SET UP WITH JOYRAX SO THIS SUBROUTINE AND INPUT ARE
29     C USED TO FACILITATE MODIFICATIONS
30     C      CALL IP(ILABL,TAU)
31     1000  FORMAT(8A9,F)
32     WRITE(1,1000) ILABL,TAU
33
34     C      THIS SECTION INITIALIZES SOME CONSTANTS
35     C      NRP=0
36
37     C      THIS SECTION INPUTS THE GROUND STRIPS DESCRIPTIONS
38     C      CALL IFILE(20,'GRND')
39     READ(20,1000) ILABL
40     WRITE(1,1000) ILABL
41     READ(20) K,X1,Z1,X2,Z2
42     CALL RELEAD (20)
43
44     C      THIS SECTION INPUTS THE ANTENNA FILE NAME TO BEUSED
45     C AND THEN INPUTS THE ANTENNA ELEMENT DESCRIPTIONS
46     WRITE(5,2001)
47     2001  FORMAT(' INPUT ANTENNA FILE NAME:',8)
48     READ(5,2001) ILBL
49     2000  FORMAT(A9)
50     CALL IFILE(20,ILBL)
51     READ(20,1000) ILABL
52     WRITE(1,1000) ILABL
53     READ(20) LAMBDA,NEL,(X(I),Y(I),Z(I),CF1(I),CF2(I),CF3(I),I=1,NEL)

```

```

94      WRITF(1) LAMBDA,NEL,(X(1),Y(1),Z(1),CF1(1),CF2(1),CF3(1),I=1,NEL)
95      CALL RELEAS (20)
96      SORT2L=1./SORT(2.*LAMBDA)
97      TEMP2=LAMBDA
98      DAK=DP1/DBLE(LAMBDA)
99      SAK=SNGL(DAK)
100     C
101     C      THIS IS THE MAIN LOOP FOR THE SIMULATION, THE RECEIVER
102     C LOCATION IS READ IN BY INPUT, THE DATA IS IN COMMON 'REC'
103     C THE INPUT BEING DONE BY JOVRAX, IF THERE ARE NO MORE RECEIVER
104     C POINTS THE SUBROUTINE RETURNS TO 200.
105     C201 CALL INPUT(S200)
106     C
107     C      THIS SECTION INITIALIZES THE COMPLEX AMPLITUDES FOR
108     C THE RECEIVED FIELD AS FOLLOWS:
109     C      CFR1 CARRIER WITH 'REAL' GROUND
110     C      CFR2 150 MHZ SIDEBAND WITH 'REAL' GROUND
111     C      CFR3 90MHZ SIDEBAND WITH 'REAL' GROUND
112     C      CFS1 CARRIER WITH 'IDEAL' FLAT GROUND PLANE
113     C      CFS2 150MHZ WITH 'IDEAL' GROUND
114     C      CFS3 90 MHZ WITH 'IDEAL' GROUND
115     C      CFR1=(0.,0.)
116     C      CFR2=(0.,0.)
117     C      CFR3=(0.,0.)
118     C      CFS1=(0.,0.)
119     C      CFS2=(0.,0.)
120     C      CFS3=(0.,0.)
121     C      R2=SQRT(RX*RX+RZ*RZ)
122     C
123     C      THIS LOOP IS OVER THE ELEMENTS OF THE ANTENNA
124     C THE COMPLEX FIELDS ARE SUMMED IN CFR1,CFR2 ETC.
125     C      DO 3 IEL=1,NEL
126     C
127     C      THESE ARE THE LOCATION COORDINATES OF THE ANTENNA ELEMENTS
128     C AND CONSTANTS USED IN THE STRIP INTEGRATION
129     C      AX=X(IEL)
130     C      AY=Y(IEL)
131     C      AZ=Z(IEL)
132     C      DELX=RX-AX
133     C      DELY=RY-AY
134     C      DELZ=RZ-AZ
135     C      DR=DSQRT(DELX*DELX+DELY*DELY+DELZ*DELZ)
136     C      R=SNGL(DR)
137     C      DR=DR*DAK
138     C      IL=DR/DP1
139     C
140     C      THIS SECTION INITIALIZES HR AND HI TO INCLUDE THE
141     C SEMI-INFINITE REAR GROUND PLANE
142     C      TEMP2=DR*DBLE(FLOAT(IL))*DP1
143     C      TEMP2=AB
144     C      F1=SQRT(TEMP*TEMP+AY*AY)
145     C      F2=-RX*TEMP/(R2*F1)
146     C      TC=SQRT(1.+AY*AY/(TEMP*TEMP))

```

ILSVEN.F4

F40

V27(36P)

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11:04

```
107      TD=TC*AZ
108      R1=R2*TC
109      S=SQRT((1./R2+1./AZ)/(TC*TC*TC))
110      G=RX/(TD*TD*R1-R1*S)
111      TEMP=SAK*F1
112      SF=SIN(TEMP)
113      FC=COS(TEMP)
114      TEMP=AZ*G/DAK/F2
115      C
116      C      HR AND HI ARE THE REAL AND IMAGINARY PARTS OF THE COMPLEX
117      C 'GAIN' FACTOR OF THE GROUND SURFACE SCATTERING TO THE RECEIVER
118      C LOCATION
119      HR=-TEMP*(SF*FC/(DAK*TD))
120      HI=TEMP*(FC-SF/(DAK*TC))
121      C
122      C      THIS SUBROUTINE SUMS THE 'GAIN' FACTOR FOR EACH STRIP OF
123      C THE GROUND SURFACE
124      CALL SCAT
125      C
126      C      THIS SECTION INCLUDES THE EFFECT OF THE DIRECT RADIATION FROM
127      C THE ANTENNA ELEMENT AT THE RECEIVER
128      HR=HR*SQRT2L
129      HI=HI*SQRT2L
130      TEMP=DELX/(R*RI)
131      SF=SIN(TEMP2)
132      FC=COS(TEMP2)
133      C
134      C      CTEMP IS THE COMPLEX GAIN FACTOR INCLUDING ALL RADIATION FROM
135      C THIS ELEMENT
136      CTEMP=CMPLX(-TEMP*SF+HR-HI,TEMP*FC+HR+HI)*.9/LAMBDA
137      C
138      C      THIS SECTION ACCUMULATES THE FIELDS OF THE VARIOUS FREQUENCIES
139      CFS1=CFS1+CTEMP*CF1(IPL)
140      CFS2=CFS2+CTEMP*CF2(IPL)
141      CFS3=CFS3+CTEMP*CF3(IEL)
142      ALPH=SAK*.9*AZ/R2/R
143      CTEMP=TEMP*.9/LAMBDA*CMPLX(-SF,FC)*
144      1CMPLX(1,-COS(ALPH)),-SIN(ALPH))
145      CFR1=CFR1+CTEMP*CF1(IEI)
146      CFR2=CFR2+CTEMP*CF2(IEI)
147      CFR3=CFR3+CTEMP*CF3(IPL)
148      3      CONTINUE
149      WRITE(1,2003) RX,RV,RZ,RY,CFR1,CFR2,CFR3,CFS1,CFS2,CFS3
150      2003  FORMAT(4F,/,6E13.6,/,AE13.6)
151      GO TO 201
152      C
153      C      THIS IS THE TERMINATION SECTION. THE INITIAL RECORD ON
154      C THE OUTPUT FILE IS WRITTEN AND THE PROGRAM TERMINATES.
155      200  CALL RELEAS (1)
156      CALL EXIT
157      STOP
158      END
```


FILE	20	20																		
IL	20	102																		
ILAM	1	22	22	30	40	51	52													
ILC	40	20																		
INPUT	00																			
IPYDGT	2	0																		
I	15	41																		
LAMDA	14	14	93	94	96	97	98	130	143											
MA	23	24	25																	
MD	3	0	29																	
MSIR	13																			
OFFIC	24																			
PLST	3																			
R	26	130	142																	
R1	100	110																		
R2	21	103	109	100	170															
REC	13																			
RELEASE	42	55	125																	
RT	13	149																		
RTTY	3																			
RTY	3																			
RTM	3																			
RTM	3																			
RM	13	81	92	105	110	140														
RMT	3																			
RML	3																			
RMM	3																			
RMM	3																			
RY	13	93	140																	
RVTY	3																			
RVTY	3																			
RYM	3																			
RYM	3																			
RZ	13	81	94	142	140															
RZTY	3																			
RZLY	3																			
RZM	3																			
RZM	3																			
S	102	110																		
SAN	20	111	142																	
SCAT	124																			
SF	112	119	120	131	136	143														
SIN	112	131	143																	
SMGL	20	24																		
SMST	20	21	124	126	129															
SMSTL	24	120	129																	
TAU	30	32																		
TC	106	107	170	170																
TD	107	117	119	120																
TEMP	108	104	109	126	111	112	113	114	119	120	120	130	143							
TEMP2	22	102	121	132																
VAL	17																			
X	10	53	54	89																
X1	19	41																		
X2	19	41																		
Y	10	53	54	90																
Z	10	53	54	91																
Z1	19	41																		
Z2	19	41																		
3P	85	140																		
200P	87	155																		
201P	85	151																		
1000P	21	12	39	40	41	52														
2000P	40	40																		
2011P	40	47																		
2003P	149	150																		

ILSVEN.FA

F40

V27(36P)

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11:09

```

1
2
3
4
5
6
7
SUBROUTINE INPUT(S)
COMMON /REC/ RX(4),NSIZE
IF(NSIZE .LE. 0) RETURN 1
CALL JOVNI(1,RX,4,0)
NSIZE=NSIZE-1
RETURN
END

```

CONSTANTS

```

0 0000000000000001 1 0000000000000004 7 0000000000000000

```

COMMON

```

RX /REC /-0 NSIZE /REC /-4

```

SUBPROGRAMS

JOVNI

SCALARS

```

INPUT 36 NSIZE 4

```

ARRAYS

```

RX 0

```

```

INPUT 1
JOVNI 4
NSIZE 2 3 5
REC 2 4
RX 2

```

IL9VER.F4

F40

V27(360)

22-APR-76

11:09

```
1 C
2 C THIS SUBROUTINE SUMS THE EFFECTS OF THE STRIPS THAT MAKE
3 C UP THE GROUND SURFACE. THERE ARE 'K' STRIPS DESCRIBED IN COMMON
4 C GROUND AS FOLLOWS:
5 C X1(I) THE X-COORDINATE OF THE LEADING EDGE OF THE I'TH STRIP
6 C Z1(I) THE Z-COORDINATE OF THE LEADING EDGE OF THE I'TH STRIP
7 C X2(I) THE X-COORDINATE OF THE ENDING EDGE OF THE I'TH STRIP
8 C Z2(I) THE Z-COORDINATE OF THE ENDING EDGE OF THE I'TH STRIP
9 C
10 C SUBROUTINE SCAT
11 C COMMON /SEC/ RX,RY,RZ
12 C COMMON /ANT/AX,AY,AZ
13 C COMMON /GROUND/ N,X1(20),Z1(20),X2(20),Z2(20),IEL
14 C COMMON /SEC/ XX1,ZZ1,XX2,ZZ2,N
15 C
16 C THESE ARE INITIAL VALUES FOR THE PARAMETERS USED IN SHADOWING
17 C SLOPE=-1.
18 C PHIE=-1.
19 C
20 C THIS IS THE LOOP OVER THE STRIPS
21 C DO 1 I=1,K
22 C
23 C THESE ARE THE VALUES TO BE USED IN THE STRIP
24 C INTEGRATION SUBROUTINE
25 C XX1 LEADING X-COORDINATE
26 C ZZ1 LEADING Z-COORDINATE
27 C XX2 TRAILING X-COORDINATE
28 C ZZ2 TRAILING Z-COORDINATE
29 C
30 C XX1=X1(I)
31 C ZZ1=Z1(I)
32 C XX2=X2(I)
33 C ZZ2=Z2(I)
34 C
35 C THIS IS A TEST TO SEE IF THE SUMMATION OVER THE GROUND
36 C STRIPS HAS REACHED THE RECEIVER LOCATION. IF IT HAS THE SUMMATION
37 C IS STOPPED. THIS IS TO GIVE THE EFFECT OF FORWARD LOCKING RECEIVER
38 C ANTENNA PATTERN.
39 C IF (XX1 .GE. RX) GO TO 6
40 C
41 C IF THE RECEIVER IS LOCATED OVER THE MIDDLE PORTION OF A STRIP
42 C THE STRIP WILL BE INTEGRATED ONLY UP TO THE VALUE OF THE
43 C RECEIVER X-COORDINATE
44 C IF (XX2 .LE. RX) GO TO 5
45 C ZZ2=ZZ1+(RX-XX1)*(ZZ2-ZZ1)/(XX2-XX1)
46 C XX2=RX
47 C
48 C CONTINUE
49 C
50 C THIS SECTION DOES THE SHADOWING. IF PART OR ALL OF THE STRIP
51 C IS IN THE SHADOW OF A PREVIOUS STRIP, THIS STRIP WILL BE ELIMINATED
52 C OR MASKED TO GIVE THE EFFECT OF SHADOWING.
53 C DEL=XX2-AX
54 C IF (DELX .LE. 0.) GO TO 3
55 C PHIE=(AZ-ZZ2)/DELX
56 C IF (SLOPE .LT. P.) GO TO 3
```

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```

04      IF(PWIC .GE. SLOPE) GO TO 1
05      PWID=(A2-ZZ1)/(XZ1-AZ)
06      IF(PWID .LE. SLOPE) GO TO 3
07      IF(XZ1 .EQ. XZ2) GO TO 4
08      A=(ZP2-ZZ1)/(XZ2-XZ1)
09      B=ZS1-A*(XZ1-AZ)
10      ZS1=(A2-B)/(A-SLOPE)+AZ
11      ZZ1=SLOPE*(XZ1-AZ)+A2
12
13      C
14      C THIS SUBROUTINE WILL INTEGRATE OVER THE STRIP THE
15      C COMPLEX 'GAIN' EFFECT OF THIS STRIP WILL BE ADDED TO M1 AND M2
16      C IN COMMON 'VALL'
17      3 CALL SUBR
18      SLOPE=PWIC
19      1 CONTINUE
20      6 RETN
21      END

```

CONSTANTS

P 281488888888

COMMON

M1	/REC	/=0	M2	/REC	/=1	M3	/REC	/=2	M4	/ANT	/=0	M5	/ANT	/=1	
M6	/ANT	/=2	M7	/GROUND/=0	M8	/GROUND/=1	M9	/GROUND/=2	M10	/GROUND/=3	M11	/GROUND/=4	M12	/GROUND/=5	
M13	/GROUND/=6	M14	/GROUND/=7	M15	/GROUND/=8	M16	/GROUND/=9	M17	/GROUND/=10	M18	/GROUND/=11	M19	/GROUND/=12	M20	/GROUND/=13
M21	/SEG	/=3	M22	/SEG	/=4	M23	/SEG	/=5	M24	/SEG	/=6	M25	/SEG	/=7	

SUBPROGRAMS

SUB

SCALARS

SCAT	143	SLOPE	144	PWIC	145	1	146	2	147
XZ1	0	ZZ1	1	XZ2	2	ZZ2	3	A	148
DELX	147	AZ	0	A2	2	PWID	149	TEL	150
4	152	M1	1	M2	2	M3	3	M4	4
5	4	M5	5	M6	6	M7	7	M8	8

ARRAYS

M1	1	M2	2	M3	3	M4	4	M5	5
----	---	----	---	----	---	----	---	----	---

A	58	59	68							
ANT	11									
AX	11	52	55	59	68	61				
AY	11									
AZ	11	52	55	68	61					
B	59	62								
DELX	58	51	52							
GROUND	12									
I	22	28	29	38	31					
TEL	12									
K	12	22								
N	13									
PH1B	55	56								
PH1E	17	52	54	67						
REC	18									
RX	18	37	42	43	44					
RY	18									
RZ	18									
SCAT	9									
SEC	13									
SLOPE	14	53	54	56	68	61	67			
SUN	66									
X1	12	28								
X2	12	38								
XX1	13	28	37	43	55	57	58	59	68	61
XX2	13	38	42	43	44	58	57	58		
Z1	12	29								
Z2	12	31								
Z21	13	29	43	55	58	59	61			
Z22	13	31	43	52	58					
1P	28	54	68							
3P	51	53	56	66						
4P	57	61								
9P	42	45								
6P	37	69								


```

1      C
2      C      THIS SUBROUTINE INTEGRATES OVER THE SURFACE STRIP DEFINED
3      C BY X1,Z1,X2,Z2 IN COMMON 'SEG', TO GIVE THE FIELD EFFECT
4      C OF THE ANTENNA ELEMENT IN COMMON 'ANT' AT RECEIVER DEFINED
5      C IN COMMON 'REC'. THE VARIABLES ARE AS FOLLOWS:
6      C      AX      ANTENNA X-COORDINATE
7      C      AY      ANTENNA Y-COORDINATE
8      C      AZ      ANTENNA Z-COORDINATE
9      C      LAMBDA  WAVELENGTH OF CARRIER
10     C      AK      TWO*PI/LAMBDA
11     C      DPI     TWO*PI (DOUBLE PRECISION)
12     C      RX      RECEIVER X-COORDINATE
13     C      RY      RECEIVER Y-COORDINATE
14     C      RZ      RECEIVER Z-COORDINATE
15     C      HR      REL PART OF 'GAIN' FACTOR
16     C      HI      IMAGINARY PART OF 'GAIN' FACTOR
17     C      X1      LEADING EDGE OF STRIP'S X-COORDINATE
18     C      Z1      LEADING Z-COORDINATE
19     C      X2      TRAILING EDGE X-COORDINATE
20     C      Z2      TRAILING Z-COORDINATE
21     C THE INTEGRATION IS PERFORMED BY A MODIFIED TRAPIZOID RULE.
22     C THE SPACING BETWEEN POINTS ALONG THE VARIABLE OF INTEGRATION
23     C IS VARIED BY THE RATE OF CHANGE OF THE INTEGRAND.
24     C      SUBROUTINE SUM
25     C      COMMON /SEG/ X1,Z1,X2,Z2,N
26     C      DOUBLE PRECISION A1,A2,B1,B2,XL,AY2
27     C      REAL JR,J1,JOR,J01,JNR,JN1
28     C      REAL LAMBDA
29     C      DOUBLE PRECISION AK,DPI,DR
30     C      COMMON /ANT/AX,AY,AZ,LAMBDA,AK,DPI
31     C      COMMON /REC/RX,RY,RZ
32     C      COMMON /VAL/HR,HI
33     C      REAL L3,L10
34     C
35     C      THIS IS THE INITIALIZATION SECTION
36     C      AY2=DOUBLE(AY)*DOUBLE(AY)
37     C      AKK=8NGL(AK)
38     C      SF=Z2-Z1
39     C      CL=X2-X1
40     C
41     C      XMAX IS THE LENGTH ALONG THE SURFACE OF THE STRIP
42     C      XMAX=SQRT(SE*SE+CE*CE)
43     C
44     C      THESE ARE THE SIN AND COS OF THE ANGLE THE STRIP MAKES WITH
45     C A HORIZONTAL PLANE
46     C      SE=SE/XMAX
47     C      CE=CE/XMAX
48     C      JR=0.
49     C      J1=0.
50     C
51     C      XL IS THE VARIABLE OF INTEGRATION. IT IS THE DISTANCE
52     C LONG THE SURFACE OF THE STRIP STARTING FROM THE LEADING EDGE
53     C      XL=0.

```

ILSVEN.F4

F48

V27(36P)

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11:05

```

94          NX=1
95          IT=0
96          C
97          C THESE ARE THE LOWER AND UPPER BOUNDS FOR THE SPACING BETWEEN
98          C POINTS ALONG THE VARIABLE OF INTEGRATION
99          L3= LAMBDA/24,
100         L10=20.*LAMBDA
101         A1=RX-X1
102         A2=RF-Z1
103         B1=X1
104         B2=Z1-A2
105         A=A1
106         TEMP=A2
107         A= SQRT(A*A+TEMP*TEMP)
108         B=B1
109         TEMP=B2
110         B= SQRT(B*B+TEMP*TEMP)
111         TEMPA=A*B
112         DR=DSQRT(DBLE(TEMP)*DBLE(TEMP)+DBLE(A*Y*Y))
113         C=DR
114         DR=DR*AK
115         I=DR/DPI
116         F=DR*DBLE(FLOAT(I))*DPI
117         C=C/TEMP
118         D=C*B
119         R=C*A
120         S=SQRT((1./A+1./B)/C/C/C)
121         G=A1/D/D/R/R/S
122         TEMP=G/(AKK*D)
123         CF=COS(F)
124         SF=SIN(F)
125         J0R=G*CF-TEMP*SF
126         J0I=G*SF+TEMP*CF
127         AP=(A1*CE-A2*SE)/A
128         BP=(B1*CE+B2*SE)/B
129
130          C
131          C FP IS THE DERIVATIVE OF THE PHASE FUNCTION
132          C OF THE INTEGRAND
133          FP=ABS((AP*BP)/C)
134
135          C
136          C DL IS DELTA XL
137          DL=L3/FP
138          IF(DL .GT. L10) DL=L10
139          IF(DL .LT. L3) DL=L3
140          XL=XL+DL
141
142          C
143          C THIS IS THE LOOP OVER THE SURFACE OF THE STRIP. XL IS
144          C INCREMENTED BY DL (OF VARIABLE SIZE UNTIL THE END OF THE STRIP
145          C IS REACHED (XMAX)
146          C CONTINUE
147
148          C
149          C THIS SECTION CALCULATE VARIOUS TERMS USED IN EVALUATING THE
150          C INTEGRAND. THE AMPLITUDE AND PHASE FUNCTION

```

```

107 C ARE EVALUTATED SEPARATELY. THE DERIVATIVE OF THE PHASE FUNCTION
108 C IS EVALUATED TO DETERMINE THE SIZE FOR DELTA X
109 DLSE=DL*SE
110 DLCE=DL*CE
111 A1=A1-DLCE
112 A2=A2-DLSE
113 B1=B1-DLCE
114 B2=B2-DLSE
115 A=A1
116 TEMP=A2
117 A= SORT(A*A+TEMP*TEMP)
118 B=B1
119 TEMP=B2
120 B= SORT(B*B+TEMP*TEMP)
121 TEMP=A*B
122 DR=DSORT(DBLE(TEMP)*DBLE(TEMP)+DBLE(A*A))
123 C=SNGL(DR)/TEMP
124 DR=DR*AK
125 I=DR/DPI
126 C
127 C THIS IS THE PHASE ANGLE *MODULO TWO P *
128 F=DR*DBLE(FLOAT(I))*DPI
129 D=C*R
130 R=C*A
131 S=SQRT((1./A+1./B)/C)/C
132 G=A1/(D*D*R+S)
133 C
134 C THIS IS THE AMPLITUDE FUNCTION
135 TEMP=G/(AK*D)
136 CF=COS(F)
137 SF=SIN(F)
138 C
139 C THIS IS THE REAL PART OF THE INTEGRAND FOR THE
140 C INTEGRATION VARIABLE VALUE OF XL
141 JNR=G*CF-TEMP*SF
142 C
143 C THIS IS THE IMAGINARY PART
144 JNI=G*SF+TEMP*CF
145 TEMP=DL
146 C
147 C THESE ARE THE REAL AN IMAGINARY PARTS OF THE THE SUMMATION
148 C OF THE TRAPIZOIDS MAKING UP THE APPROXIMATION TO THE INTEGRAL
149 JR=JR+(JNR*JNR)*TEMP
150 JI=JI+(JNI*JNI)*TEMP
151 IF(IT.NE.0) GO TO 2
152 JDR=JNR
153 JDI=JNI
154 AP=(A1*CE-A2*SE)/A
155 BP=(B1*CE+B2*SE)/B
156 C
157 C FP IS THE DERIVATIVE OF THE PHASE FUNCTION
158 FP=ABS((AP*BP)/C)
159 C

```

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```

168 C DL IS DELTA X AND IS LIMITED BY THE ROUNDS LI-LI2
169 DL=LI/PP
170 IF(DL .GT. LI2) DL=LI2
171 IF(DL .LT. LI) DL=LI
172 AX=DX+1
173
174 C
175 C THE VARIABLE OF INTEGRATION IS INCREMENTED AND IF THE END OF THE
176 C STRIP IS REACHED THE LAST TRAPEZOID IS ADDED
177 XL=XL+DL
178 IF(XL .GT. XMAX) GO TO 1
179 DL=XMAX-DL-XL
180 XL=XMAX
181 IT=0
182 GO TO 1
183
184 C
185 C THIS SECTION ADDS THE FIELD EFFECT FROM THE STRIP TO THE
186 C TOTAL FIELD SUM AND TEM SUBROUTINE TERMINATES
187 CONTINUE
188
189 N=AX
190 TEMPO=(Z1-A2)*CE-X1*SE)/2.
191 HR=HR+JR*TEMP
192 MI=MI+JI*TEMP
193 RETURN
194 END

```

CONSTANTS

P 2896P*28*278

COMMON

X1	/SEC	/+2	Z1	/SEC	/+1	X2	/SEC	/+2	Z2	/SEC	/+3	N	/SEC	/+4
AX	/ANT	/+8	AY	/ANT	/+1	AZ	/ANT	/+2	LAMBDA	/ANT	/+3	AK	/ANT	/+4
DP1	/ANT	/+6	RX	/REC	/+8	RY	/REC	/+1	RB	/REC	/+2	HR	/VAL	/+8
MI	/VAL	/+1												

SUBPROGRAMS

DBLE	DFM.2	SNDL	SORT	DSORT	DFI.2	DFMN.2	DFD.2	IDINT	FLOAT	DFS.8	DFD.6	COS	SIN	DFN.4
DFM.6	DF4.4	DFD.4	ABS	DFAM.2	DFS.2									

SCALARS

BLM	1864	AMP	1865	AY	1	AKK	1867	AK	4
CE	1870	B2	3	Z1	1	CI	1871	X2	2
X1	8	XMAX	1872	JR	1873	J1	1874	XL	1875
X2	1877	IT	11PR	LS	1181	LAMBDA	3	LI2	1182
A1	1183	RX	B	A2	1189	R2	2	B1	1187
B2	1111	AZ	P	A	1113	TEMP	1114	B	1119
DP	1116	C	1122	I	1121	DP1	8	F	1122
D	1123	R	1124	S	1128	G	1126	CF	1127
XF	1138	JDR	1131	JDI	1132	AP	1133	BR	1134
PP	1139	DL	1136	LBE	1137	OLCE	1140	JNR	1141

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JN1	1142	N	4	HR	8	MI	1	AX	8
PI	1								

A	69	67	71	79	80	87	119	117	121	130	131	134		
A1	26	61	65	81	87	111	119	132	134					
A2	29	62	66	87	112	116	124							
ABS	92	198												
AA	29	38		74	124									
AAK	37	82	139											
AAV	39													
AP	87	92	194	198										
AR	39													
AV	38	36	72	122										
AVZ	26	36												
AZ	39	64	179											
B	69	78	71	78	80	80	118	120	121	129	131	138		
B1	26	63	68	88	113	118	129							
B2	26	64	69	88	114	119	129							
BP	88	92	195	198										
C	73	77	78	79	88	92	123	129	138	131	138			
CE	35	42	47	87	88	118	124	129						
CF	85	85	86	136	141	144								
COB	83	126												
D	78	81	82	129	132	135								
DALE	36	72	76	122	128									
DL	95	96	97	98	189	118	149	161	162	163	168	178		
DLCE	118	111	113											
DLSE	109	112	114											
DP1	29	38	75	74	125	128								
DR	29	72	73	74	79	76	122	123	124	128	188			
OSONT	72	122												
F	76	83		128	136	137								
FLOAT	76	128	84	128	136	137								
FP	92	95	198	161										
G	81	82	85	86	132	138	141	144						
HI	32	181												
HR	32	188												
I	78	76	125	128										
IT	95	191	172											
J1	27	49	198	181										
JMI	27	144	198	193										
JNR	27	141	149	182										
JOT	27	86	198	193										
JOR	27	85	149	192										
JR	27	48	149	188										
L10	32	68	96	162										
L3	33	59	95	87	161	163								
LAMBDA	28	39	59	68										
N	28	178												
NX	94	184	178											
R	79	81	138	132										
REC	31													
RX	31	61												
RY	31													
RZ	31	62												
S	88	81	131	132										
SE	38	42	46	87	88	189	194	199	179					
SEC	25													
SM	84	85	86	137	141	144								
SMAL	37	123												
SBRT	42	67	78	88	117	128	131							
SUM	24													
TEMP	46	67	69	78	71	72	77	82	85	86	116	117	119	128
VAL	111	122	123	139	141	144	149	149	198	179	188	181		
X1	32													
X2	29	39	61	63	179									
X3	29	39												
X4	26	93	98	188	169		171							
XMAX	42	44	47	168	169	178								
Z1	28	38	62	64	178									
Z2	28	38												
1P	183	189	173											
2P	191	177												

APPENDIX B MOLE

```

1      DIMENSION ILABL(6)
2      DIMENSION IPTDAT(33)
3      COMMON /PLXT/ NR0,RX0N,RXMX,RXFT,RXLT,RV0N,RVMX,RVFT,RVLT,
4      1R0N,R0MX,R0FT,R0LT,RT0N,RTMX,RTFT,RTL,
5      2A0N,A0MX,A0FT,A0LT,ARMN,ARMX,ARFT,ARLT,
6      3ADN,ADIX,ADIF,ADIL,
7      4ADRN,ADRX,ADRF,ADRL
8      EQUIVALENCE (IPTDAT(1),NR0)
9      IMPLICIT COMPLEX (C)
10     DIMENSION X(20),Y(20),Z(20)
11     DIMENSION CF1(20),CF2(20),CF3(20)
12     IMPLICIT DOUBLE PRECISION (D)
13     COMMON /REC/RX,RY,RZ,RY,NSIZE
14     REAL LAMDA
15     COMMON /ANT/AX,AY,AZ,LAMDA,DAK,OPI
16     COMMON /VAL/ NR,N1
17     COMMON /GRND/ P(3,4),N(3)
18
19     C
20     C THIS VALUE OF TWO PI IS INITIALIZED THIS WAY TO AVOID USING
21     C BLOCK DATA
22     OPI=6.2831853071795864749
23     WRITE(5,2001)
24     2001 FORMAT(' INPUT FILE NAME:',S)
25     READ(5,2000) ILOL
26     2000 FORMAT(A5)
27     CALL IFILE(21,ILOL)
28     WRITE(5,2002)
29     2002 FORMAT(' OUTPUT FILE NAME:',S)
30     READ(5,2000) ILOL
31     CALL OFILE(1,ILOL)
32     4000 READ(20,4000) ((P(I,J),I=1,3),J=1,4)
33     FORMAT(4I30,/)
34     READ(21,1000) ILABL,TAU
35     WRITE(1,1000) ILABL
36     DO 3 I=1,2
37     READ(21,1000) ILABL
38     3 WRITE(1,1000) ILABL
39     1000 FORMAT(9A5,F)
40     READ(21) LAMDA,NEL,(X(I),Y(I),Z(I),CF1(I),CF2(I),CF3(I),I=1,NEL)
41     WRITE(1) LAMDA,NEL,(X(I),Y(I),Z(I),CF1(I),CF2(I),CF3(I),I=1,NEL)
42     DAK=OPI/DOUBLE(LAMDA)
43     201 READ(21,2009,END=200) RX,RY,RZ,RY,
44     1CFR1,CFR2,CFR3,CFR4,CFR5,CFR6
45     2009 FORMAT(4F,/,0E13,0,/,0E13,0)
46     2005 READ(5,3000) P
47     3000 FORMAT(30)
48     DO 5 I=1,NEL
49     AX=X(I)
50     AY=Y(I)
51     AZ=Z(I)
52     CTEMP=(0.,0.)
53     CALL INTR2(CTEMP)
54     CT=CTEMP*CF1(I)

```

```

94      CFR3=CFR1*CT
95      CFS1=CFR1*CT
96      CT=CTEMP*CF2(1)
97      CFR2=CFR2*CT
98      CFS2=CFR2*CT
99      CT=CTEMP*CF3(1)
00      CFS3=CFR3*CT
01      CFR3=CFR3*CT
02      S      CONTINUE
03      WRITE(1,2005) RX,RV,RZ,RY,CFR1,CFR2,CFR3,CFS1,CFS2,CFS3
04      GO TO 201
05
06      C      THIS IS THE TERMINATION SECTION. THE INITIAL RECORD ON
07      C THE OUTPUT FILE IS WRITTEN AND THE PROGRAM TERMINATES.
08      200  CALL RELEAS (1)
09      CALL EXIT
10      STOP
11      END
    
```

CONSTANTS

R	203622077325	1	158842855861	2	000000000025	3	000000000001	4	000000000000
S	000000000000								

COMMON

NRP	/PLXT	/+0	RXNX	/PLXT	/+1	RXNY	/PLXT	/+2	RXYT	/PLXT	/+3	RZLT	/PLXT	/+4
RXNY	/PLXT	/+5	RXNY	/PLXT	/+6	RZLT	/PLXT	/+7	RZLT	/PLXT	/+8	RZNY	/PLXT	/+9
RZNY	/PLXT	/+10	RZNY	/PLXT	/+11	RZNY	/PLXT	/+12	RZNY	/PLXT	/+13	RZNY	/PLXT	/+14
RTFT	/PLXT	/+15	RTFT	/PLXT	/+16	RTFT	/PLXT	/+17	RTFT	/PLXT	/+18	RTFT	/PLXT	/+19
RTFT	/PLXT	/+20	RTFT	/PLXT	/+21	RTFT	/PLXT	/+22	RTFT	/PLXT	/+23	RTFT	/PLXT	/+24
ADIX	/PLXT	/+25	ADIX	/PLXT	/+26	ADIX	/PLXT	/+27	ADIX	/PLXT	/+28	ADIX	/PLXT	/+29
ADIX	/PLXT	/+30	ADIX	/PLXT	/+31	ADIX	/PLXT	/+32	ADIX	/PLXT	/+33	ADIX	/PLXT	/+34
ADIX	/PLXT	/+35	ADIX	/PLXT	/+36	ADIX	/PLXT	/+37	ADIX	/PLXT	/+38	ADIX	/PLXT	/+39
ADIX	/PLXT	/+40	ADIX	/PLXT	/+41	ADIX	/PLXT	/+42	ADIX	/PLXT	/+43	ADIX	/PLXT	/+44
ADIX	/PLXT	/+45	ADIX	/PLXT	/+46	ADIX	/PLXT	/+47	ADIX	/PLXT	/+48	ADIX	/PLXT	/+49
ADIX	/PLXT	/+50	ADIX	/PLXT	/+51	ADIX	/PLXT	/+52	ADIX	/PLXT	/+53	ADIX	/PLXT	/+54
ADIX	/PLXT	/+55	ADIX	/PLXT	/+56	ADIX	/PLXT	/+57	ADIX	/PLXT	/+58	ADIX	/PLXT	/+59
ADIX	/PLXT	/+60	ADIX	/PLXT	/+61	ADIX	/PLXT	/+62	ADIX	/PLXT	/+63	ADIX	/PLXT	/+64
ADIX	/PLXT	/+65	ADIX	/PLXT	/+66	ADIX	/PLXT	/+67	ADIX	/PLXT	/+68	ADIX	/PLXT	/+69
ADIX	/PLXT	/+70	ADIX	/PLXT	/+71	ADIX	/PLXT	/+72	ADIX	/PLXT	/+73	ADIX	/PLXT	/+74
ADIX	/PLXT	/+75	ADIX	/PLXT	/+76	ADIX	/PLXT	/+77	ADIX	/PLXT	/+78	ADIX	/PLXT	/+79
ADIX	/PLXT	/+80	ADIX	/PLXT	/+81	ADIX	/PLXT	/+82	ADIX	/PLXT	/+83	ADIX	/PLXT	/+84
ADIX	/PLXT	/+85	ADIX	/PLXT	/+86	ADIX	/PLXT	/+87	ADIX	/PLXT	/+88	ADIX	/PLXT	/+89
ADIX	/PLXT	/+90	ADIX	/PLXT	/+91	ADIX	/PLXT	/+92	ADIX	/PLXT	/+93	ADIX	/PLXT	/+94
ADIX	/PLXT	/+95	ADIX	/PLXT	/+96	ADIX	/PLXT	/+97	ADIX	/PLXT	/+98	ADIX	/PLXT	/+99
ADIX	/PLXT	/+100	ADIX	/PLXT	/+101	ADIX	/PLXT	/+102	ADIX	/PLXT	/+103	ADIX	/PLXT	/+104

SUBPROGRAMS

FORBE.	JOFF	ALPHO.	ALPHI.	IFILE	OFILE	ALLTD.	FLOUT.	FLIRT.	GINNR.	OBLE	DFD.2	END.	INTR2	CFM.2
RELEAS	EXIT													

SCALARS

NPI	6	ILBL	486	I	487	J	410	TAU	411
LAMBDA	3	NEL	412	DAK	4	RX	8	RY	1
RE	2	RT	5	CFR1	413	CFR2	415	CFR3	417
CFR1	421	CFR2	423	CFR3	425	AK	8	AY	1
AS	2	CTEMP	427	CT	431	NRP	8	RXNX	1
RXNY	2	RTFT	3	RZLT	4	RXNY	9	RXNY	6
RZNY	2	RTFT	3	RZNY	11	RZNY	12	RZNY	13
ADIX	7	RTFT	16	ADIX	16	ADIX	17	ADIX	20
ADIX	14	ADIX	22	ADIX	23	ADIX	24	ADIX	25
ADIX	21	ADIX	22	ADIX	23	ADIX	24	ADIX	25

MOLE.F4 F40

V2713001

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ARMX 26
 ADIF 33
 ADRL 40

ARPT 27
 ADIL 34
 NS12C 4

ARLT 30
 ARDN 35
 W 1

ADIL 34
 ARDN 36
 NI 1

ADIX 32
 ARNV 37

ARRAYS

ILABL 423
 CFI 537

IPYDGY 8
 CP2 607

P 443
 CP3 697

V 447
 P 8

2 513
 4 14

ADIF	3													
ADIL	3													
ADIX	3													
ADIN	3													
ADRY	3													
ADRL	3													
ADRN	3													
ADRX	3													
ALTY	2													
ALTY	3													
ALPM	3													
ALNK	3													
AMT	19													
ARPT	3													
ARLT	2													
ARNN	3													
ARMX	3													
AX	19	40												
AY	19	49												
AZ	19	50												
CF1	11	39	48	51										
CF2	11	39	48	56										
CF3	11	39	48	59										
CFR1	42	54	63											
CFR2	42	57	63											
CFR3	42	61	63											
CFR4	42	62	63											
CFR5	42	60	63											
CFR6	42	60	63											
CFR7	42	60	63											
CFR8	42	60	63											
CT	33	54	55	56	57	58	59	60	61					
CTEND	31	52	53	56	59									
DAK	19	41												
DBLE	51													
DPT	18	21	41											
EXIT	69													
GRND	17													
NI	16													
NI	16													
NI	16													
LC	20	39	39	40	47	48	48	50	53	56	59			
IL JL	1	33	34	36	37									
ILLL	24	24	29	30										
INTRP	52													
IPYDGY	2	0												
J	21													
LAMBDA	14	19	39	40	41									
N	17													
NEL	39	40	47											
NSP	3	0												
NS12C	13													
OFFLINE	38													
P	17	31	45											
PLKY	3													

REC	13			
RELEAS	68			
RT	13	42	63	
RYPT	3			
RYLT	3			
RYMN	3			
RYMX	3			
RX	13	42	63	
RXPT	3			
RXLT	3			
RXMN	3			
RXXM	3			
RY	13	42	63	
RYPT	3			
RYLT	3			
RYMN	3			
RYMX	3			
RZ	13	42	63	
RZPT	3			
RZLT	3			
RZMN	3			
RZMX	3			
TAU	33			
VAL	16			
X	18	39	48	48
Y	18	39	48	49
Z	18	39	48	50

3P	35	37			
5P	47	62			
202P	42	68			
201P	42	64			
1000P	33	34	36	37	38
2000P	24	25	29		
2001P	22	23			
2002P	27	28			
2003P	42	44	63		
3000P	45	46			
4000P	31	32			

HOLE,F4 F48 V27(248) 22-APR-76 13:53

```

1      SUBROUTINE NORMAL(V1,V2,V3,V4,R)
2      DIMENSION V1(1),V2(1),V3(1),V4(1)
3      Z1=V2(1)-V1(1)
4      Z2=V3(1)-V1(1)
5      V1=V2(2)-V1(2)
6      V2=V3(2)-V1(2)
7      Z1=V2(3)-V1(3)
8      Z2=V3(3)-V1(3)
9      X=V1(2)-V2(2)
10     Y=Z1(2)-Z2(2)
11     Z=X10V2-V1(2)
12     R=SQRT(X*X+Y*Y+Z*Z)
13     V4(1)=X/R
14     V4(2)=Y/R
15     V4(3)=Z/R
16     RETURN
17     END

```

GLOBAL DUMMIES

V1 133 V2 134 V3 135 V4 136 R 137

SUBPROGRAMS

 SORT

SCALARS

NORMAL 141 X1 142 X2 143 Y1 144 Y2 145
Z1 146 Z2 147 X 148 Y 149 Z 150

ARRAYS

V1 133 V2 134 V3 135 V4 136

NORMAL	1								
R	1								
SORT	12								
V1	1	2	3	4	5	6	7	8	
V2	1	2	3	4	5	6	7	8	
V3	1	2	3	4	5	6	7	8	
V4	1	2	13	14	15				
X	9	12	13						
X1	1	12	13						
X2	4	12	13						
Y	10	12	14						
Y1	9	9	11						
Y2	6	9	11						
Z	11	12	15						
Z1	7	9	12						
Z2	0	9	10						

HOLE,F4 F43

V27(368)

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```

1      DOUBLE PRECISION FUNCTION DIST(X,Y)
2      DIMENSION X(1),Y(1)
3      DOUBLE PRECISION R,TEMP
4      R=0.
5      DO 1 I=1,3
6      TEMP=X(I)-Y(I)
7      R=R+TEMP*TEMP
8      DIST=DSORT(R)
9      RETURN
10     END

```

GLOBAL DUMMIES

X	56	Y	57
---	----	---	----

SUBPROGRAMS

DFM,2	DFAM,2	DSORT
-------	--------	-------

SCALARS

DIST	68	R	62	I	64	TEMP	65
------	----	---	----	---	----	------	----

ARRAYS

X	56	Y	57
---	----	---	----

DIST	1	8		
DSORT	8	5		
I	5	6		
R	3	4	7	8
TEMP	3	6	7	
X	1	2	6	
Y	1	2	6	

1P	5	7
----	---	---

```

1 SUBROUTINE INTR2(CTEMP)
2 DATA DX,DY/23.,.40./
3 DIMENSION XTA(3),ETA(3)
4 DOUBLE PRECISION D10,D20,R10,R20
5 COMPLEX A,B
6 DOUBLE PRECISION D01,D02
7 COMPLEX CTEMP,CCT,CCX,CCY,CCX0
8 REAL N,LAMBDA,N1,N2,N3
9 COMMON /SRNO/ P(3,4),N(3)
10 EQUIVALENCE (N(1),N1),(N(2),N2),(N(3),N3)
11 DOUBLE PRECISION DAK,DP1
12 COMMON /REC/ XR,YR,ZR
13 COMMON /ANT/XA,YA,ZA,LAMBDA,DAK,DP1
14 EQUIVALENCE (P(1),P(1,1)),(P(2),P(1,2)),(P(3),P(2,1))
15 EQUIVALENCE (P(4),P(2,4)),(P(5),P(3,1)),(P(6),P(3,4))
16 LOGICAL TEST
17 DATA TEST/.TRUE./
18 IF(TEST) CALL NORMAL(P(1),P(2),P(1,4),N(1),TEMP)
19 TEST=.FALSE.
20 ZAR=Z.A
21 TP1=SNGL(DP1)
22 AK=SNGL(DAK)
23 CTEMP=(0.,0.)
24 DELX=0
25 DCG=PI*IST(0(1,1),0(1,2))
26 IX=DGG/DELX
27 IF(IX .LT. 0) IX=-IX
28 IF(IX .LT. 1) IX=1
29 IX=(IX+1)/2*2
30 DELX=DGG/FLOAT(IX)
31 XTA(1)=(P(1,2)-P(1,1))/DGG
32 XTA(2)=(P(2,2)-P(2,1))/DGG
33 XTA(3)=(P(3,2)-P(3,1))/DGG
34 DCGY=XTA(1)*DELX
35 DCGY=XTA(2)*DELX
36 DCGY=XTA(3)*DELX
37 DCG1=PI*IST(P(1,1),P(1,4))
38 DELZ=0
39 IZ=DG1/DELZ
40 IF(IZ .LT. 0) IZ=-IZ
41 IF(IZ .LT. 1) IZ=1
42 IZ=(IZ+1)/2*2
43 DELZ=DG1/FLOAT(IZ)
44 ETA(1)=(P(2,4)-P(1,1))/DGG
45 ETA(2)=(P(3,4)-P(2,1))/DGG
46 ETA(3)=(P(3,4)-P(3,1))/DGG
47 DCG1=ETA(1)*DELZ
48 DCG1=ETA(2)*DELZ
49 DCG1=ETA(3)*DELZ
50 DO 1 IXX=1,IX
51 FX=FLOAT(IXX)-.5
52 XS=P(1,1)+FX*DCGX
53 YS=P(2,1)+FX*DCGY

```

```

94 ZS=P(3,1)-PK=DC6Z
95 DO 2 IZ=1,17
96 FZ=FLOAT(IZ)-.5
97 XS=XS-FZ*DB1X
98 YS=YS-FZ*DB1Y
99 ZS=ZS-FZ*DB1Z
100 CC6=XR-XS
101 CC7=YS-YA
102 TEMP=VR-VS
103 TEMP2=ZR-ZS
104 TEMP3=ZR-ZS
105 DR1=ABLE(CC6*CC6)*ABLE(TEMP*TEMP)
106 DR2=DR1*ABLE(TEMP3*TEMP3)
107 DR1=DR1*ABLE(TEMP2*TEMP2)
108 R12=DR1
109 R22=DR2
110 R1P=NSORT(DR1)
111 R2P=NSORT(DR2)
112 R1=R1P
113 R2=R2P
114 TEMP=VS-YA
115 TEMP2=ZS-ZA
116 TEMP3=ZS-ZA
117 DR1=ABLE(CC7*CC7)*ABLE(TEMP*TEMP)
118 DR2=DR1*ABLE(TEMP3*TEMP3)
119 DR1=DR1*ABLE(TEMP2*TEMP2)
120 D12=DR1
121 D22=DR2
122 D1P=NSORT(DR1)
123 D2P=NSORT(DR2)
124 D1=D1P
125 D2=D2P
126 F1P=42*XS*(VR-VS)+(41*YS+NS*(ZS-ZA))*(XR-XS)
127 F2P=F1P+NS*(XR-XS)*ZA
128 COSA1=(XTA(1)*CC7+XTA(2)*(YS-YA)+XTA(3)*(ZS-ZA))/D1
129 COSA2=(XTA(1)*CC7+XTA(2)*(YS-YA)+XTA(3)*(ZS-ZA))/D2
130 COSG1=(XTA(1)*CC6+XTA(2)*(VR-VS)+XTA(3)*(ZR-ZS))/R1
131 COSG2=(XTA(1)*CC6+XTA(2)*(VR-VS)+XTA(3)*(ZR-ZS))/R2
132 COSB1=(ZTA(1)*CC7+ZTA(2)*(YS-YA)+ZTA(3)*(ZS-ZA))/D1
133 COSB2=(ZTA(1)*CC7+ZTA(2)*(YS-YA)+ZTA(3)*(ZS-ZA))/D2
134 COSD1=(ZTA(1)*CC6+ZTA(2)*(VR-VS)+ZTA(3)*(ZR-ZS))/R1
135 COSD2=(ZTA(1)*CC6+ZTA(2)*(VR-VS)+ZTA(3)*(ZR-ZS))/R2
136 CM=COSA-COSG
137 CM1=COSA1-COSG1
138 CM2=COSA2-COSG2
139 CM3=COSA1-COSG1
140 C=COSB-COSD
141 C1=COSB1-COSD1
142 C2=COSB2-COSD2
143 C3=COSB1-COSD1
144 D1P=Z1P*AK
145 D2P=Z2P*AK
146 R1P=R1P*AK

```

```

107 R20=R20*QAN
108 ID=010/DPI
109 D1=010=0BLE(FLOAT(ID))=DPI
110 ID=020/DPI
111 D2=020=0BLE(FLOAT(ID))=DPI
112 ID=R10/DPI
113 R1=010=0BLE(FLOAT(ID))=DPI
114 ID=R20/DPI
115 R2=020=0BLE(FLOAT(ID))=DPI
116 TEMP=F10*SIN(AK*CM=DELX*.5)*SIN(AK*C=DELZ*.5)/(CM*C=012=0R12)
117 CTENP=CTENP+TEMP*CEXP(CMPLX(R.,D1=0P1))
118 TEMP=F10*SIN(AK*CM1=DELX*.5)*SIN(AK*C1=DELZ*.5)/(CM1*C1=012=0R22)
119 CTENP=CTENP+TEMP*CEXP(CMPLX(R.,D1=0P2))
120 TEMP=F20*SIN(AK*CM2=DELX*.5)*SIN(AK*C2=DELZ*.5)/(CM2*C2=022=0R12)
121 CTENP=CTENP+TEMP*CEXP(CMPLX(R.,D2=0P1))
122 TEMP=F20*SIN(AK*CM3=DELX*.5)*SIN(AK*C3=DELZ*.5)/(CM3*C3=022=0R22)
123 CTENP=CTENP+TEMP*CEXP(CMPLX(R.,D2=0P2))
124 2 CONTINUE
125 1 CONTINUE
126 CTENP=CTENP*2./(TP1+TP1)
127 ICC=1X=1E
128 RETURN
129 END
    
```

CONSTANTS

0 0000000000 1 P2PPPE00000 2 P0002000001 3 0000000000

GLOBAL DUMMIES

CTEMP 1341

COMMON

P	/GRND	/+0	N	/GRND	/+14	YR	/REC	/+0	YR	/REC	/+1	BR	/REC	/+2
KA	/ANT	/+0	YA	/ANT	/+1	ZA	/ANT	/+2	LAMBDA	/ANT	/+3	BAK	/ANT	/+4
DPI	/ANT	/+0	NI	/GRND	/+14	Y2	/CNC	/+15	N3	/GRND	/+16	P11	/GRND	/+0
P12	/GRND	/+3	P21	/GRND	/+1	P24	/GRNC	/+12	P31	/GRND	/+2	P34	/GRNC	/+13

SUBPROGRAMS

NORMAL	ENGL	DIST	D	IFIX	FLOAT	DBLE	DFA.2	DFAH.0	DSORT	DFMH.2	DFD.2	IQINT	DFM.0	DEF.0
R.H	CEXP	CMPLX	CFM.0	CFD.4										

SCALARS

INTR2	1347	OK	1350	NY	1351	TEST	1352	P11	0
P12	3	TEMP	1353	ZA2	1354	Z0	2	TP1	1355
DPI	6	AK	1356	YAK	4	CTENP	1341	DELX	1357
D00	1360	IX	1361	YCPX	1362	D00Y	1363	D00Z	1364
D01	1365	DEL2	1366	IZ	1367	OC1X	1370	D01Y	1371
D01Z	1372	IXX	1373	FX	1374	Y0	1375	Y0	1376
Z0	1377	IZZ	1400	FZ	1401	CC6	1400	YR	0

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CC7	1483	XA	P	YR	1	TEMP2	1484	ZR	2
TEMP3	1485	DR1	1486	782	1418	R12	1412	R22	1413
418	1414	R2P	1416	R1	1428	R2	1421	YA	1
Q12	1422	D22	1423	718	1424	Q28	1426	D1	1438
Q2	1431	F18	1432	"2	15	Y1	14	Y3	16
F2P	1433	COSA	1434	COSA1	1439	CCSG	1436	COSG1	1437
COS6	144P	COSB1	1441	COSB	1442	CCSC1	1443	CM	1444
CM1	1445	CM2	1446	CM3	1447	C	1450	C1	1451
C2	1452	C3	1453	17	1454	ICC	1455	LAMBDA	3
P21	1	P24	12	P31	2	P34	13		

ARRAYS

XTA	1456	ZTA	1461	P	2	N	14
-----	------	-----	------	---	---	---	----

A	5									
AK	22	116	118	120	122					
ANT	13									
B	5									
C	188	116								
C1	181	118								
C2	182	120								
C3	183	122								
CEB	88	95	98	91	94	95				
CC7	61	77	98	99	92	93				
CCY	7									
CCX	7									
CCNO	7									
CCY	7									
CEXP	117	119	121	123						
CM	96	116								
CM1	97	118								
CM2	98	120								
CM3	99	122								
CMPLX	117	119	121	123						
COSA	88	96	97							
COSA1	89	98	99							
COSB	92	108	121							
COSB1	93	102	123							
COSO	94	108	122							
COSD1	95	101	123							
COSG	98	96	98							
COSG1	91	97	99							
CTEMP	1	7	23	117	119	121	123	126		
D	25									
D1	84	88	92	129	117	119				
D18	4	82	84	124	128	129				
D12	88	116	118							
D2	85	83	85	111	121	123				
D28	4	83	85	125	118	111				
D22	81	128	122							
DAK	11	13	22	124	105	106	127			
DBLE	65	66	67	77	78	79	109	111	113	115
DELX	24	26	28	34	35	36	110	118	120	122
DEL2	38	39	43	47	48	49	116	118	120	122
D68	25	26	30	31	32	33				
DC1	34	32								
DC2	39	33								
DC3	36	34								
D41	37	39	43	44	49	46				
DC1X	47	37								
DC1Y	48	38								
DC1Z	49	39								
DC1T	25	37								
OP1	11	13	21	120	100	112	111	112	113	115
DR1	6	65	66	67	68	78	77	78	79	82
DR2	6	66	69	71	78	81	43			
DSGRY	78	71	82	83						

APPENDIX C GLDCDI

```

1      DIMENSION I(LABL(8))
2      DIMENSION IPTDAT(33)
3      COMMON /PLXT/ NRP,RXHN,RXNX,RXFT,RXLY,RVHN,RVNX,RVFT,RVLY,
4      1RXHN,RXNX,RZFT,RZLY,RTHN,RTNX,RTFT,RTLY,
5      2A1HN,A1NX,A1FT,A1LY,ARMN,ARMX,ARFT,ARLY,
6      3ADIN,ADIX,ADIE,ADIL,
7      4ADRN,ADRX,ADRF,ADRL,
8      EQUIVALENCE (IPTDAT(1),NRP)
9      IMPLICIT COMPLEX (C)
10     DIMENSION X(20),Y(20),Z(20)
11     DIMENSION CF1(20),CF2(20),CF3(20)
12     IMPLICIT DOUBLE PRECISION (D)
13     COMMON /REC/RX,RV,RZ,RT,NSIZE
14     REAL LAMBDA
15     COMMON /GROUND/ K,X1(20),Z1(20),X2(0/20),Z2(0/20),IEL
16     COMMON /ANT/AX,AY,AZ,LAMBDA,DAK,OPI
17     COMMON /VAL/ NR,NI
18
19     C
20     C      THIS VALUE OF TWO PI IS INITIALIZED THIS WAY TO AVOID USING
21     C BLOCK DATA
22     C
23     2001 FORMAT(' INPUT FILE NAME:',S)
24     READ(9,2001) I(LBL)
25     2000 FORMAT(A9)
26     CALL IFILE(20,I(LBL))
27     WRITE(9,2002)
28     2002 FORMAT(' OUTPUT FILE NAME:',S)
29     READ(9,2000) I(LBL)
30     CALL OFILE(1,I(LBL))
31     WRITE(1) IPTDAT
32     READ(20,1000) I(LABL,TAU)
33     WRITE(1,1000) I(LABL)
34     DO 3 I=1,2
35     READ(20,1000) I(LABL)
36     WRITE(1,1000) I(LABL)
37     1000 FORMAT(8A9,F)
38     READ(20) LAMBDA,NEL,(X(I),Y(I),Z(I),CF1(I),CF2(I),CF3(I),I=1,NEL)
39     READ(20,2003,END=200) RX,RV,RZ,RT,
40     1CFR1,CFR2,CFR3,CFS1,CFS2,CFS3
41     2003 FORMAT(4F,/,6E13.6,/,6E13.6)
42     C
43     C      AFTER THE FIELDS HAVE BEEN ACCUMULATED FOR ALL THE ELEMENTS
44     C THE CDI'S ARE CALCUATED
45     C      ACOR CDI FOR THE GROUND SURFACE
46     C      ACDI CDI FOR 'IDEAL' GROUND PLANE
47     ACDR=0.97,14*REAL((CFR2-CFR3)/CFR1)
48     ACDI=0.97,14*REAL((CFS2-CFS3)/CFS1)
49     C
50     C      NCRP IS THE COUNT OF THE RECEIVERPOINTS
51     NCRP=NRP+1
52     IF(NRP .NE. 1) GO TO 4
53     C

```

```

94 C THIS SECTION INITIALIZES THE MAXIMUM AND MINIMUM VALUES
95 C OF THE VARIOUS RANGE AND DOMAIN VARIABLES, THESE ARE
96 C USED IN THE PLOTTING PROGRAM TO SCALE THE PLOTS. AFTER THE
97 C RUN IS FINISHED THEY WILL BE OUTPUT IN PLACE OF THE
98 C INITIAL DUMMY RECORD
99 ADDI=ACDI
100 ADDR=ACDR
101 TB=RT
102 ADIX=ACDI
103 ADIN=ACDI
104 ADIF=ACDI
105 ADRX=ACDR
106 ADR=ACDR
107 ADRF=ACDR
108 RXFT=RX
109 RYFT=RY
110 RZFT=RZ
111 RTFT=RT
112 AIFT=ACDI
113 ARFT=ACDR
114 RXMN=RX
115 RXMX=RX
116 RYMN=RY
117 RYMX=RY
118 RZMN=RZ
119 RZMX=RZ
120 RTMN=RT
121 RTMX=RT
122 AIMX=ACDI
123 AIMN=ACDI
124 ARMX=ACDR
125 ARMN=ACDR
126
127 C THIS SECTION UPDATES THE MAXIMUM AND MINIMUM VALUES
128 C
129 CONTINUE
130 RXL=RX
131 RYL=RY
132 RZL=RZ
133 RTL=RT
134 AILT=ACDI
135 ARLT=ACDR
136 IF(RX .LT. RXMN) RXMN=RX
137 IF(RX .GT. RXMX) RXMX=RX
138 IF(RY .LT. RYMN) RYMN=RY
139 IF(RY .GT. RYMX) RYMX=RY
140 IF(RZ .LT. RZMN) RZMN=RZ
141 IF(RZ .GT. RZMX) RZMX=RZ
142 IF(RT .LT. RTMN) RTMN=RT
143 IF(RT .GT. RTMX) RTMX=RT
144 IF(ACDI .GT. AIMX) AIMX=ACDI
145 IF(ACDI .LT. AIMN) AIMN=ACDI
146 IF(ACDR .GT. ARMX) ARMX=ACDR
147 IF(ACDR .LT. ARMN) ARMN=ACDR

```

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```

107          CD=EXP((T0-RT)/TAU)
108          C
109          C THIS SECTION SIMULATE THE EFFECT OF THE ELECTRICAL AND
110          C MECHANICAL 'INERTIA' OF THE ILS
111          C RECEIVER SYSTEM FOR DYNAMIC SIMULATION
112          T0=RY
113          ADD1=CON*(ADD1-ACD1)+ACD1
114          ADDR=CON*(ADDR-ACDR)+ACDR
115          IF(ADDI .LT. ADIN) ADI=ADDD
116          IF(ADDI .GT. ADIN) ADI=ADDD
117          ADI=ADDD
118          IF(ADDP .LT. ADRN) ADRN=ADDP
119          IF(ADDP .GT. ADRN) ADRN=ADDP
120          ADRN=ADDP
121          C
122          C THIS IS THE OUTPUT OF THE REAL AND 'IDEAL' , STATIC
123          C AND DYNAMIC CDI'S WITHIN THE RECEIVER COORDINATES
124          WRITE(1,2003) R ,RY,R2,R*,ACD1,ACDR,ADDD,ADRN
125          2003 FORMAT(8F)
126          GO TO 201
127          C
128          C THIS IS THE TERMINATION SECTION. THE INITIAL RECORD ON
129          C THE OUTPUT FILE IS WRITTEN AND THE PROGRAM TERMINATES.
130          200 CALL RELEAS (1)
131          ENCODE (0,2006,ILABL(1)) I,BL
132          2006 FORMAT(A9,'.DAT')
133          CALL OFFLINE FILE(1,25,1,ILABL(1))
134          WRITE(101) IPTDAT
135          CALL RELEAS (1)
136          CALL EXIT
137          STOP
138          END

```

CONSTANTS

#	203622877325	1	198842859861	2	800000000024	3	800000000001	4	212694443696
5	800000000031								

COMMON

WRP	/PLXT	/+0	R2MN	/PLXT	/+1	R2MX	/PLXT	/+2	R2FT	/PLXT	/+3	R2LT	/PLXT	/+4
R2MN	/PLXT	/+5	R2MX	/PLXT	/+6	R2FT	/PLXT	/+7	R2LT	/PLXT	/+8	R2MN	/PLXT	/+9
R2MX	/PLXT	/+10	R2FT	/PLXT	/+11	R2LT	/PLXT	/+12	R2MN	/PLXT	/+13	R2MX	/PLXT	/+14
R2FT	/PLXT	/+15	R2LT	/PLXT	/+16	A1MN	/PLXT	/+17	A1MX	/PLXT	/+18	A1FT	/PLXT	/+19
A1LT	/PLXT	/+20	A1MN	/PLXT	/+21	A1MX	/PLXT	/+22	A1FT	/PLXT	/+23	A1LT	/PLXT	/+24
ADIN	/PLXT	/+25	ADIX	/PLXT	/+26	ADIF	/PLXT	/+27	ADIL	/PLXT	/+28	ADRN	/PLXT	/+29
ADRN	/PLXT	/+30	ADRT	/PLXT	/+31	ADRL	/PLXT	/+32	RA	/REC	/+33	RY	/REC	/+34
R2	/REC	/+35	RT	/REC	/+36	R2	/REC	/+37	K	/GROUND	/+38	X1	/GROUND	/+39
X1	/GROUND	/+40	X2	/GROUND	/+41	E2	/GROUND	/+42	TEL	/GROUND	/+43	A2	/ANT	/+44
AT	/ANT	/+45	A2	/ANT	/+46	LAMBDA	/ANT	/+47	DAK	/ANT	/+48	DP1	/ANT	/+49
WR	/VAL	/+50	WI	/VAL	/+51	IPTDAT	/PLXT	/+52						

SUBPROGRAMS

SLB001,F4 F40 V27(300) 22-APR-76 11104

FORMC. VADOR.	JOFF DEFINE	ALPHO. RECNO.	ALPHI. RANAC.	IFILE EXIT	OFILE	QINWP.	FLOUT.	FLIRT.	END.	REAL	CF0.2	EXP	CFM.2	RELEASE
SCALARS														
DP1	6		ILBL	967		TAU	970		1	991		LAMBDA	3	
NEL	972		RI	0		RY	1		R2	2		RT	3	
CFR1	373		CFR2	978		CFR3	977		CFB1	681		CFB2	683	
CFB3	689		ACDR	687		ACD1	610		WRP	0		ADD1	611	
ADDR	612		T0	613		ADIX	32		ADIN	31		ADIF	33	
ADRR	30		ADRN	33		ADRF	37		ARFT	3		ARFT	7	
ARPT	13		RYFT	17		ARFT	23		ARFT	27		ARWR	1	
RYWR	2		RYWR	9		RYWR	6		RYWR	11		RYWR	12	
RYWR	15		RYWR	16		RYWR	22		RYWR	21		RYWR	20	
ARWR	29		RYLT	4		RYLT	10		RYLT	14		RYLT	13	
ARLT	24		ARLT	30		CON	614		ADIL	34		ADRL	40	
NSLKE	4		R	0		ILL	120		AS	0		AY	1	
AR	2		DAK	4		WR	0		WI	1				
ARRAYS														
ILABL	616		IPTDAT	0		X	626		V	692		Z	676	
CF1	722		CF2	772		CF2	1042		X1	1		Z1	22	
W2	91		Z2	76										

ACD1	40	59	62	63	64	72	82	83	93	103	104	113	124	
ACDR	47	60	65	66	67	73	84	85	94	105	106	114	124	
ADD1	39	113	115	116	117	124								
ADDR	60	114	119	119	120	124								
ADIF	3	64												
ADIL	3	117												
ADIN	3	63	115											
ADIR	3	62	116											
ADRF	3	67												
ADRL	3	120												
ADRN	3	66	118											
ADRW	3	65	119											
ARFT	3	72												
ARLT	3	93												
ARWR	3	81	184											
ARWR	3	82	183											
ARWR	10													
ARWR	3	73												
ARWR	3	94												
ARWR	3	85	186											
ARWR	3	84	185											
AX	16													
AY	16													
AZ	16													
CF1	11	30												
CF2	11	30												
CF3	11	30												
CFR1	39	47												
CFR2	39	47												
CFR3	39	47												
CFB1	39	48												
CFB2	39	48												
CFB3	39	48												
CON	107	113	114											
DAK	16													
DEFINE	133													
DP1	16	21												
EXIT	136													
EXP	107													
GROUND	15													
WI	17													
WR	17													
I	34	30	133											
ILL	15													
IFILE	26													
ILABL	1	37	33	35	36	131	133							
ILBL	24	24	29	30	131									
IPTDAT	2	8	31	134										
X	10													
LAMBDA	14	16	30											
NEL	30													
WRP	3	6	91	92										
NSLKE	13													

OFFICE	30												
PLAT	3												
REAL	47	44											
REC	13												
RELEASE	130	135											
RT	13	39	61	71	80	81	92	101	102	107	118	124	
RTPT	3	71											
RTLT	3	92											
RTMN	3	87	102										
RTME	3	81	121										
RX	13	39	60	74	75	89	95	96	124				
RHPT	3	58											
RHLT	3	89											
RHMN	3	74	95										
RHME	3	75	96										
RY	13	39	69	76	77	90	97	98	124				
RYPT	3	69											
RYLT	3	97											
RYMN	3	74	97										
RYME	3	77	98										
RZ	13	39	70	78	79	91	99	100	124				
RZPT	3	72											
RZLT	3	91											
RZMN	3	74	120										
RZME	3	79	99										
Y0	41	107	112										
YAJ	30	127											
VAL	17												
X	10	30											
X1	19												
X2	19												
Y	10	30											
Z	10	30											
Z1	19												
Z2	19												
30	34	36											
40	52	60											
203P	30	137											
201P	30	126											
1002P	32	33	35	36	37								
2002P	24	25	70										
2001P	22	21											
2002P	27	24											
2003P	124	125											
2009P	30	41											
2004P	11	172											

APPENDIX D GLDPLT

GLDPLT.F4

F40

V27(362)

22-APR-76

11:04

```
1 DIMENSION ITYPE(3,2)
2 DATA ITYPE/'STATI', 'C VAL', 'UES', 'DYNAM', 'IC VA', 'LUES'/
3 DATA PID,PRD/'COID', 'THEOD'/
4 DIMENSION SPACE(4), IAX(2,3)
5 DATA SPACE/1.,2.,2.5,5./
6 DATA IAX/'DEGRE', 'ES', ' FEET', ' ', 'SECON', 'OS'/
7 DATA PRX,PRY,PRZ,PRT,PAI,PAR/
8 'RX', 'RY', 'RZ', 'RT', 'COI', 'THEO'/
9 DIMENSION IPTDAT(33)
10 COMMON /PTXXN/NRP, RXMN, RXXM, RXFT, RXLT, RYMN, RYMX, RYFT, RYLT,
11 'RZMN, RZMX, RZFT, RZLT, RTMN, RTMX, RTFT, RTLT,
12 2AIMN, AIMX, AIFT, AILT, ARMN, ARMX, ARFT, ARLT,
13 3ADIN, ADIX, ADIF, ADIL, ADRN, ADRX, ADRF, ADRL
14 EQUIVALENCE (IPTDAT(1), NRP)
15 DIMENSION ILABL(8)
16 DATA XLEN, YLEN, ITIC/20.,8.,21/
17 DIMENSION DY1(2000)
18 DIMENSION DX(2000), DY(2000)
19 NAMELIST /FREQ/ YLENG, YDEL, YSC, DMIN, DMAX, DEL, IP, XSC
20 CALL PLOTS(1BUF, 360, 16)
21 WRITE(9, 1006)
22 1006 FORMAT(' INPUT FILE NAME AND AXIS TYPES:', S)
23 READ(5, 1005) NAME, ISX, ISY, BOUND
24 1005 FORMAT(A9, 1, 1, F)
25 IF (ISY .LT. 1) GO TO 204
26 IF (ISY .GT. 2) GO TO 204
27 IF (ISX .LT. 1) GO TO 204
28 IF (ISX .GT. 3) GO TO 204
29 CALL PLOT(0., -12., -3)
30 CALL PLOT(0., 1., -3)
31 I=0
32 CALL IFILE(20, NAME)
33 READ(20) IPTDAT
34 WRITE(3, 1002) NRP
35 1002 FORMAT(' THERE ARE', I9, ' RECEIVER POINTS', /)
36 WRITE(3, 1003)
37 1003 FORMAT(14X, 'MIN', 9X, 'MAX', 9X, 'FIRST', 8X, 'LAST', /)
38 1004 FORMAT(1X, A5, 1X, 4F12.4)
39 WRITE(3, 1004) PRX, RXMN, RXXM, RXFT, RXLT
40 WRITE(3, 1004) PRY, RYMN, RYMX, RYFT, RYLT
41 WRITE(3, 1004) PRZ, RZMN, RZMX, RZFT, RZLT
42 WRITE(3, 1004) PRT, RTMN, RTMX, RTFT, RTLT
43 WRITE(3, 1004) PAI, AIMN, AIMX, AIFT, AILT
44 WRITE(3, 1004) PAR, ARMN, ARMX, ARFT, ARLT
45 WRITE(3, 1004) PID, ADIN, ADIX, ADIF, ADIL
46 WRITE(3, 1004) PRD, ADRN, ADRX, ADRF, ADRL
47 GASD00,
48 GASU00,
49 GACN00,
50 DO 7 I|=1,3
51 READ(20, 100) ILABL
52 WRITE(3, 101) ILABL
53 101 FORMAT(1X, 8A5)
```

GLDPLT.F4

F40

V27(360)

22-APR-76

11:04

```

94      100  FORMAT(8A5)
95      CALL SYM90L(0..0..2,1,LABL,90..40)
96      7    CALL PLOT(.3,0..-3)
97      CALL SYM90L(0..0..2,1,TYPE(1,15'),90..15)
98      CALL PLOT(2..0..-3)
99      1    READ(20,1000,END=2) X,Y,Z,T,C,R,CD,RD
100     1000  FORMAT(8F)
101     TEMP=SQRT(X*X+Y*Y)
102     IF((TEMP .LT. 3500.) .OR. (TEMP .GT. 2P720.)) GO TO 60
103     GASU=GASU+C
104     GASD=GASD+CD
105     GACN=GACN+1.
106     60    CONTINUE
107     I=I+1
108     GO TO (300,301) 15V
109     300   CONTINUE
110     DY(I)=C
111     71    DY1(I)=R
112     GO TO 302
113     301   DY(I)=CD
114     DY1(I)=RD
115     302   CONTINUE
116     GO TO (200,201,202) 15X
117     200   DX(I)=ATAN2(Z, SQRT(X*X+Y*Y))*97.2053
118     GO TO 199
119     201   DX(I)=X
120     GO TO 199
121     202   DX(I)=Y
122     GO TO 199
123     199   IF(I .NE. 1) GO TO 198
124     DMIN=DX(I)
125     DMAX=DX(I)
126     198   DMIN=AMIN1(DMIN,DX(I))
127     DMAX=AMAX1(DMAX,DX(I))
128     1001  FORMAT(5X,3F)
129     IF( I .LT. 2000) GO TO 1
130     2    IF( I .LT. 2) GO TO 3
131     YLENG=AMAX1(AINX,ABS(BOUND),-AIMN,0.)
132     IF(ARS(BOUND) .LT. 1.F-4) GO TO 10
133     YDEL=YLENG
134     GO TO 11
135     10   YLENG=AMAX1(YLENG,ARMX,-ARMN)
136     YDEL=FLOAT(IFIX(YLENG/YLEN))
137     YLENG=YDEL*YLEN
138     11   CALL AXISS(0..0.,-YLENG,YLENG,YDEL,YLEN,
139     1'MICROAMPERES',12,0,0.,YSC)
140     IP=IP[X(ALOG10(DMAX-DMIN))-1]
141     POW=18.9*IP
142     DO 120 J=1,4
143     DEL=SPACE(J)*POW
144     IT=IFIX(DMAX/DEL-1.)+1-IFIX(DMIN/DEL)
145     IF(IT .LT. ITIC) GO TO 121
146     120   CONTINUE

```

```

127 121 DMIN=FLOAT(IFIE DMIN/DEL 1)DEL
128 DMAX=FLOAT(IFIEI DMIN/DEL 1)DEL
129 IP=IP+1
130 IF(IP.LT. 8) IP=8
131 CALL ATN3(0.,IP,DMAX,DMIN,DEL,ILEN,1001,1001,7,IP,0.,ASC)
132 CALL PLOT(0.,ILEN,IP-3)
133 CALL PLOT(ILEN,IP-2)
134 WRITE(9,PGED)
135 CALL PLOT(DM11-DMIN/ASC,DY11/ASC,3)
136 WRITE(3,1001) DM11,DY11,DY11
137 GASOGASDP=7/6ACN/150.
138 GASOGASDP=7/6ACN/150.
139 WRITE(3,1007) GASU,GASD,GACN
122 1007 FORMAT(' STATIC MEAN ANGLE ERROR=',E,
121 1) ' DYNAMIC MEAN ANGLE ERROR=',E,10X,'COUNT=',F6.0)
122 DO 4 J=2,1
123 WRITE(3,1001) DM(J),DY(J),DY(J)
124 4 CALL PLOT(DM(J)-DMIN/ASC,DY(J)/ASC,2)
125 IF(ROUND(LT. 0) GO TO 8
126 IS=8
127 CALL PLOT(DM(J)-DMIN/ASC,DY(J)/ASC,3)
128 DO 6 J=2,1
129 CALL PLOT(DM(J)-DMIN/ASC,DY(J)/ASC,15)
130 6 IS=8-15
131 8 CALL PLOT(ILEN-2,IP-3)
132 GO TO 3
133 704 CALL PLOT(3.,0.,000)
134 CALL EXIT
135 STOP
136 EN*

```

CONSTANTS

8	000000000000	1	000000000000	2	200000000000	3	200000000000	4	201400000000
5	200000000000	6	170611463146	7	200000000000	12	200000000000	11	177463146314
12	000000000000	13	272600000000	14	217973000000	15	214669400000	16	206712271430
17	204400000000	20	103643734277	21	466210351236	22	406332042644	23	426444020100
24	000000000000	25	210000000000	26	17961463146	27	000000000000	30	000000000000
31	000000000000	32	22054614631	33	210000000000	34	203500000000	35	202600000000
36	000000000000	37							

COMMON

QBP	/PTXN /-0	RYM	/PTXN /-1	QYX	/PTXN /-2	QYF	/PTXN /-3	QYLT	/PTXN /-4
RYM	/PTXN /-5	RYM	/PTXN /-6	QYF	/PTXN /-7	QYLT	/PTXN /-8	QYM	/PTXN /-11
QYX	/PTXN /-2	QYF	/PTXN /-13	QYLT	/PTXN /-14	RYM	/PTXN /-15	RYM	/PTXN /-16
QYF	/PTXN /-9	RYT	/PTXN /-20	QYX	/PTXN /-21	QYM	/PTXN /-22	QYF	/PTXN /-23
QYLT	/PTXN /-24	QYX	/PTXN /-25	QYM	/PTXN /-26	QYF	/PTXN /-27	QYLT	/PTXN /-28
QYM	/PTXN /-31	QYF	/PTXN /-32	QYLT	/PTXN /-33	QYX	/PTXN /-34	QYM	/PTXN /-35
QYF	/PTXN /-36	QYLT	/PTXN /-37	QYX	/PTXN /-40	IP'DA'	/PTXN /-8		

SUBPROGRAMS

GLOPLT.F4 F48 V29(30P) 22-APR-76 11:04

FORSE, SORT	.JOBFF ATAN2	ALLIO. AMINI	PLOYS AMAX1	ALPHO. ABS	ALPHI. FLOAT	INTO. IFIX	INTI. AXIS2	FLOUT. ALOG1P	FLIRT. EXP2.2	PLOT NMLST,	IFILE EXIT	DINMR.	SYMBOL	END.
SCALARS														
PID	1230		PRD	1231		PRX	1232		PRY	1233		PRE	1234	
PRY	1235		PAI	1236		PAR	1237		XLEN	1240		VLEN	1241	
ITIC	1242		YLENG	1243		VDEL	1244		YBC	1249		DMIN	1246	
OMAX	1247		DEL	1250		IP	1251		XBC	1252		IBUF	1253	
NAME	1254		ISX	1255		ISY	1256		BOUND	1257		I	1260	
WRP	0		RKMN	1		RKMX	2		RKFT	3		RKLT	4	
RYMN	5		RYMX	6		RYFT	7		RILT	18		RMN	11	
RPMX	12		RFTY	13		RFLT	14		RTMN	15		RTMX	16	
RFTY	17		RTLT	20		AIMN	21		AIMX	22		AIFT	23	
AILT	24		ARMN	25		ARMX	26		ARFT	27		ARLT	28	
ADIN	31		ADIX	32		ADIF	33		ADIL	34		ADRN	35	
ADRX	36		ADRF	37		ADRL	40		CASD	1261		GABU	1262	
GAGN	1263		II	1264		X	1265		Y	1266		Z	1267	
T	1270		C	1271		R	1272		CD	1273		RD	1274	
TEMP	1275		POW	1276		J	1277		IT	1300		ISH	1301	
ARRAYS														
ITYPE	1302		SPACE	1310		IAX	1314		IPTDAT	0		ILABL	1322	
OY1	1332		DX	9292		DY	11192							

ABS	91	92																		
ADIF	10	45																		
ADIL	10	45																		
ADIN	10	45																		
ADIX	10	45																		
ADRF	10	46																		
ADRL	10	46																		
ADRN	10	46																		
ADRX	10	46																		
AIFT	10	43																		
AILT	10	43																		
AIMN	10	43	91																	
AIMX	10	43	91																	
ALOG10	108																			
AMAX1	87	91	95																	
AMINI	86																			
ARFT	10	44																		
ARLT	10	44																		
ARMN	10	44	95																	
ARMX	10	44	95																	
ATAN2	77																			
AXIS3	98	111																		
BOUND	23	91	92	125																
C	59	63	70																	
CO	59	64	73																	
DEL	19	123	104	107	100	111														
DMAX	19	85	87	100	104	100	111													
DMIN	19	84	86	100	104	107	111	115	124	127	129									
DX	10	77	79	81	84	85	86	87	115	116	123	124	127	129						
DY	10	70	73	115	110	123	124													
DY1	17	71	74	116	123	127	129													
EXIT	134																			
FLOAT	96	107	108																	
FRED	19	114																		
GACH	49	65	117	110	119															
GASO	47	64	110	119																
GASU	40	63	117	119																
I	31	67	70	71	73	74	77	79	81	83	84	85	86	87						
	89	70	122	128																
IAX	4	A	111																	
IBUF	20																			
IFILE	32																			
IFIX	96	100	104	107	100															
II	50																			
ILABL	15	51	52	55																
IP	19	102	107	100	110	111														
IPYDAT	9	14	33																	
ISW	126	120	130																	
ISX	23	27	28	26	111															
ISY	23	25	26	57	60															
IT	174	105																		
ITIC	10	105																		
ITYPE	1	2	57																	

J	102	103	122	123	124	128	129							
NAME	23	32												
MBP	10	14	34											
PAI	7	43												
PAR	7	44												
PID	3	45												
PLOT	20	30	56	90	112	113	119	124	127	129	131	133		
PLOT%	20													
POW	101	103												
PRO	3	46												
PRT	7	42												
PRX	7	39												
PRY	7	40												
PRZ	7	41												
PTXHX	10													
R	50	71												
RO	50	74												
RTPT	10	42												
RTLT	10	42												
RTMN	10	42												
RTMX	10	42												
RYPT	10	39												
RKLT	10	39												
RKMN	10	39												
RKMX	10	39												
RYPT	10	40												
RYLT	10	42												
RYMN	10	42												
RYMX	10	40												
REPT	10	41												
RELT	10	41												
REMN	10	41												
REMX	10	41												
SPACE	4	5	103											
SORT	61	77												
SYMBOL	55	57												
T	50	81												
TEMP	61	62												
X	50	61	77	70										
XLEN	10	111	113	131										
XSC	10	111	115	124	127	129								
Y	50	61	77											
YOEL	10	93	96	97	98									
YLEN	10	96	97	98	112									
YLENG	10	91	93	95	96	97	98							
YSC	10	90	115	124	127	129								
Z	50	77												

1P	59	89							
2P	59	90							
3P	21	90	132						
4P	122	124							
5P	128	132							
7P	58	54							
8P	125	131							
10P	92	95							
11P	94	98							
60P	62	66							
100P	51	54							
101P	52	53							
122P	102	106							
121P	105	107							
100P	83	86							
199P	78	80	82	83					
202P	76	77							
201P	76	79							
202P	76	81							
204P	25	26	27	28	133				
300P	68	69							
301P	68	73							
302P	72	75							
1000P	59	60							
1001P	88	116	123						
1002P	34	35							
1003P	34	37							
1004P	38	39	40	41	42	43	44	45	46
1005P	23	24							
1006P	21	22							
1007P	119	120							

```

1 SURROUTINE AXIS3(XB,YB,AMAX,AMIN,DELA,AINCH,BCC,NCR,NDEC,PWR,DELN)
2 DIMENSION BCC(1)
3 HT = .10
4 DELA=SIGN(DELA,(AMAX-AMIN))
5 W1=0.
6 W2=0.
7 W3 = 0.
8 NEXP = 0
9 NCH=ABS(NCR)
10 IF(PWR,NE,0.) NEXP = 6
11 CINCH=ABS(AINCH)
12 IF(ABS(AMAX-AMIN)+ABS(DELX).LT.1.E-5) GO TO 38
13 IF((AMAX-AMIN)/(DELX+1.E-5).GT.3.*CINCH) DELX = (AMAX-AMIN)/CINCH
14 IF(NCR.LT.0) W3 = 1.
15 NUM=FIX((AMAX-AMIN)/DELX+1.9)
16 ANC=CINCH/FLOAT(NUM-1)
17 IF(AINCH.LT.0.)GO TO 5
18 W2=1.
19 GO TO 10
20 W1=1.
21 CALL PLOT(XB,YB,3)
22 DELN=DELX/10.**PWR/ANC
23 ANUM=AMIN-DELX
24 X=P.
25 Y=0.
26 XM=0.
27 DO 40 I=1,NUM
28 ANUM=ANUM+DELX
29 II=0
30 IF(ABS(ANUM)/10.**II.LT.1.)GO TO 27
31 II=II+1
32 GO TO 25
33 IF(ANUM.LT.0.)II=II+1
34 IF(ABS(ANUM).LT.1.) II=II+1
35 IMORE=NDEC+1
36 II=II+IMORE
37 IF(FIX(W1)+1.E0.1) HT = AMIN1(HT ,ANC,FLOAT(II+2))
38 CENTER = FLOAT(II)*HT/(1.+W1)
39 OFF = .05
40 XC = X - CENTER + W2*(W3*(.30+CENTER) - .15)
41 IF(XC.LT.XM)XM=XC
42 YC = Y - W1*(HT + .15 - W3*(HT+.13)) - W2*OFF
43 CALL PLOT(XB+X,YB+Y,2)
44 CALL PLOT(XB+X+.1*W2,YB+Y+.1*W1,3)
45 CALL PLOT(XB+X-.1*W2,YB+Y-.1*W1,2)
46 CALL NUMBER(XB+XC,YB+YC,HT,ANUM,0.,NDEC)
47 CALL PLOT(XB+X,YB+Y,3)
48 X=X+ANC*W1
49 Y=Y+ANC*W2
50 CONTINUE
51 BST = (CINCH - FLOAT(NCH*NEXP)*.12)/2.
52 XXC = W1*(XB + BST) + W2*(XB + XM + OFF + W3*(2.*CENTER+.44))
53 YYC = W1*(YB + YC - .17 + W3*(HT + .22) ) + W2*(YB + BST)

```


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34 CALL SYMROL(XXC,YYC,,12,BCD,90,042,NCM)
35 IF(PWR,EO,0) RETURN
36 CALL WHERE(XO,YO,XXCX)
37 CALL SYMROL(XO,YO,,12,5H+10,90,042,9)
38 CALL WHERE(XO,YO,XXCX)
39 X = YO + (XXC-.00-YO)*42
40 Y = YO + (YYC-.00-YO)*41
41 CALL NUMBER(X,Y,,09,PWR,90,042,-1)
42 RETURN
43 SE DELM = 1.E-3*10.00PWR/CINCH
44 N=NCM/5
45 WRITE(5,1000) AMAX,AMIN,DELA,PWR,(BCD(1),10L,N)
46 1000 FORMAT(1H0,27MINBUFFICIENT RANGE FOR AXIS ,
47 1/,1X,4G,/,1X,13A5)
48 CALL EXIT
49 RETURN
50 ENN

```

CONSTANTS

P	179631463146	1	167406111564	2	160517426542	3	8174631-631	4	000000000003
5	201400000000	6	174631463146	7	177463146314	10	24463146314	11	000000000002
12	000000000000	13	175753412172	14	177722436560	15	76934121727	16	176782436560
17	201244036540	20	000000000000	21	000000000005	22	75907534121	23	175940907534

GLOBAL DUMMIES

XO	696	YO	697	AMAX	660	AMIN	661	DELA	662
AINCM	663	BCD	664	NCR	665	NDEC	666	PWR	667
DELM	678								

SUBPROGRAMS

SIGN	IA05	ABS	IFIX	FLOAT	PLOT	EXP3.2	EXP2.2	AMIN1	NUMBER	SYMBOL	WHERE	ALL10.	ALPHO.	ALPH1.
EXIT														

SCALARS

AXIS3	673	WT	674	DELN	675	DELA	662	AMAX	660
AMIN	661	W1	676	W2	677	W3	700	NEXP	701
NCH	702	NCR	665	PWR	667	CINCH	703	AINCM	663
NCH	704	ANC	705	XO	696	YO	697	DELN	670
ANUM	706	X	707	Y	710	XH	711	I	712
II	713	INORE	714	NDEC	666	CENTER	715	OFF	716
XC	717	YC	720	BST	721	XXC	722	YYC	723
XO	724	YO	729	XXCX	726	N	707		

ARRAYS

BCD	664
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APPENDIX E FMAKE

FMAKE.F4

F40

V27(360)

22-APR-76

11:04

```

1      DIMENSION IDUM(2)
2      DATA IDUM(2)/',.DAT'/'
3      COMMON XX,YY,ZZ,TT
4      DIMENSION ILABL(8)
5      DIMENSION X(20),Y(20),Z(20)
6      IMPLICIT COMPLEX (C)
7      DIMENSION C1(20),C2(20),C3(20)
8      COMMON /GROUND/ K,X1(20),Z1(20),X2(0/20),Z2(0/20),IEL
9
10     C      THIS SECTION ACCEPTS THE INPUT OF THE SWITCH (ONE CHARACTER) TO
11     C DETERMINE WHAT KIND OF FILE TO GENERATE,
12     C      <BLANK> TO END THE PROGRAM
13     C      Y      TO SET ANTENNA OFFSET AND TRANSMISSION WAVELENGTH
14     C      G      FOR GROUND DESCRIPTION
15     C      P      FOR FLIGHT PATH
16     C      A      FOR ANTENNA DESCRIPTION
17     C      WRITE(5,1013)
18     C      READ(5,1009) NAME
19     C      IF(NAME .EQ. ' ') GO TO 3
20     C      IF(NAME .EQ. 'Y') GO TO 20
21     C      IF(NAME .EQ. 'G') GO TO 21
22     C      IF(NAME .EQ. 'P') GO TO 22
23     C      IF(NAME .EQ. 'A') GO TO 23
24     C      WRITE(5,1012)
25     C      GO TO 2
26
27     C      THIS IS THE INPUT FOR THE ANTENNA OFFSET AND FOR THE
28     C TRANSMISSION WAVELENGTH, BOTH ARE IN FEET AND ARE FLOATING POINT.
29     C      WRITE(5,1011)
30     C      READ(5,1021) Y0,RL
31     C      GO TO 2
32
33     C      THIS SECTION IS FOR GROUND DESCRIPTION
34     C      WRITE(5,1014)
35
36     C      THIS IS TO INPUT THE FILE NAME FOR GROUND DESCRIPTION
37     C      READ(5,105) IDUM(1)
38     C      WRITE(5,104)
39
40     C      THIS IS TO INPUT THE PLOT LABEL FOR GROUND DESCRIPTION
41     C      READ(5,105) ILABL
42     C      WRITE(5,100)
43
44     C      THIS IS THE INPUT FOR THE GROUND STRIP EDGE COORDINATES
45     C      R      DELTA X-COORDINATE FOR CARTESIAN AND
46     C      RANGE FOR POLAR COORDINATES
47     C      ZZ      DELTA Y-COORDINATE FOR CARTESIAN AND
48     C      USUALLY ZERO FOR POLAR COORDINATES
49     C      THETA   ZERO FOR CARTESIAN COORDINATES AND
50     C      THE ELEVATION ANGLE FOR POLAR
51     C      THIS IS THE INPUT FOR THE STARTING EDGE OF THE FIRST STRIP
52     C      READ(5,101,END=2) P,ZZ,THETA
53     C      X2(0)=R+COSD(THETA)-ZZ*SIND(THETA)

```

FNAGE.F4

F4B

V27(36B)

22-APR-76

11184

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94      Z2(8)=R*SIND(THETA)+Z2*COSD(THETA)
95      K=8
96      WRITE(5,102)
97      C
98      C      THIS IS THE INPUT LOOP FOR THE REST OF THE STRIP EDGES, THE
99      C EDGES ARE THE TRAILING EDGE OF THE PREVIOUS STRIP AND THE
100     C LEADING EDGE OF THE NEXT. THE LOOP WILL CONTINUE TO A MAXIMUM OF
101     C TWENTY STRIPS OR UNTIL BOTH 'R' AND 'Z2' ARE ZERO.
102     11  READ(5,101,END=2) R,Z2,THETA
103     63  IF(R.NE.0.) GO TO 5
104     64  IF(Z2.NE.0.) GO TO 5
105     65  IF(K.EQ.20) GO TO 2
106     66  GO TO 4
107     67  5  K=K+1
108     68  X1(K)=X2(K-1)
109     69  Z1(K)=Z2(K-1)
110     70  X2(K)=X2(K-1)+R*COSD(THETA)-Z2*SIND(THETA)
111     71  Z2(K)=Z2(K-1)+R*SIND(THETA)+Z2*COSD(THETA)
112     72  IF(K.LT.20) GO TO 6
113     73  WRITE(5,103)
114     74  GO TO 4
115     75  6  WRITE(5,102)
116     76  GO TO 11
117     77  C
118     78  C      THIS OPENS A FILE FOR THE GROUND DESCRIPTION, OUTPUTS IT
119     C IN BINARY AND CLOSES THE FILE. FLOW THEN RETURNS TO THE SWITCH POINT.
120     80  4  CALL OFILE(20,IOUM(1))
121     81  WRITE(20,105) ILABL
122     82  WRITE(20) K,X1,Z1,X2,Z2
123     83  CALL RELEAS(20)
124     84  GO TO 2
125     85  C
126     86  C      THIS IS THE SECTION TO GENERATE A FLIGHT PATH FILE.
127     87  22 WRITE(5,1019)
128     88  C
129     89  C      THIS INPUTS THE FLIGHT PATH FILE NAME
130     90  READ(5,105) IOUM(1)
131     91  C
132     92  C      THIS IS TO CREATE THE FILE IF ONE DOES NOT ALREADY EXIST.
133     C THIS IS NECESSARY AS JOVRAX DOES NOT CREATE FILES.
134     94  CALL OFILE(20,IOUM(1))
135     95  CALL RELEAS(20)
136     96  C
137     97  C      THIS IS TO OPEN THE FILE FOR JOVVRA
138     98  CALL JOVSET(1,IOUM(1),NSIZE)
139     99  WRITE(5,1003)
140    100  C
141    101  C      THIS IS TO INPUT THE FLIGHT PATH PLOT LABEL AND OUTPUT IT TO
142    102  C THE FILE
143    103  C
144    104  READ(5,105) ILABL
145    105  CALL JOVNO(1,ILABL,8,8)
146    106  WRITE(5,1008)

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```
107 C
108 C THIS SWITCH IS TO SELECT EITHER STRIGHT LINE FLIGHT OR
109 C HYPERBOLIC. 'C' INPUT WILL SELECT HYPERBOLIC ANYTHING ELSE WILL
110 C GIVE STRIGHT LINE.
111 READ(9,1009) I
112 IF(I .NE. 'C') GO TO 12
113 C
114 C THIS IS THE HYPERBOLIC FLIGHT SECTION
115 WRITE(9,1010)
116 C
117 C THIS IS THE INPUT TO DESCRIBE THE FLIGHT
118 C X0 STARTING X-COORDINATE
119 C XF ENDING X-COORDINATE
120 C H HEIGHT OF MAIN ELEMENT USED TO DETERMINE GLIDE ANGLE
121 C AND HEIGHT ABOVE GROUND OF ZERO CDI SURFACE AT CLOSEST
122 C APPROACH
123 READ(9,1011) X0,XF,H
124 WRITE(9,1006)
125 C
126 C THIS INPUT IS FOR THE FLIGHT PATH QUANTIZATION PARAMETERS
127 C NK IS THE NUMBER OF POINTS ALONG THE FLIGHT PATH
128 C V IS THE VELOCITY (FT./SEC.) OF THE AIRCRAFT
129 C TAU IS THE TIME CONSTANT (SEC.) FOR THE DYNAMIC CDI
130 READ(9,1007) NK,V,TAU
131 IF(NK .LE. 0) GO TO 22
132 CALL JOVMD(1,TAU,1,0)
133 C
134 C THIS LOOP GENERATES THE COORINATES OF THE POINTS ALONG THE
135 C HYPERBOLA AND OUTPUTS THEM TO THE FLIGHT PATH FILE
136 A1=RL*RL*.25-H*H-Y0*Y0
137 A2=1./((1.-4.*H*H/RL/RL)
138 DX=(XF-X0)/FLOAT(NK-1)
139 XX=X0
140 YY=0.
141 TT=0.
142 XOL=XX
143 ZOL=SQRT((A1-XX*XX)*A2)
144 DO 13 I=1,NK
145 ZZ=SQRT((A1-XX*XX)*A2)
146 TEMP=XX-XOL
147 TEMP2=ZZ-ZOL
148 TT=TT+SQRT(TEMP*TEMP-TEMP2*TEMP2)/V
149 CALL JOVMD(1,XX,4,P)
150 XOL=XX
151 ZOL=ZZ
152 XX=XX+DX
153 CONTINUE
154 GO TO 14
155 C
156 C THIS SECTION IS FOR STRIGHT LINE FLIGHT
157 CONTINUE
158 WRITE(9,1004)
159 C
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160 C THESE INPUTS ARE TO DESCRIBE THE FLIGHT PATH
161 C XX STARTING X-COORDINATE (FEET)
162 C YY STARTING Y-COORDINATE (FEET)
163 C ZZ STARTING Z-COORDINATE (FEET)
164 C XF ENDING X-COORDINATE (FEET)
165 C YF ENDING Y-COORDINATE (FEET)
166 C ZF ENDING Z-COORDINATE
167 C NK NUMBER OF POINTS ALONG THE FLIGHT PATH
168 C V VELOCITY OF AIRCRAFT (FEET/SEC.)
169 C TAU TIME CONSTANT FOR DYNAMIC COI (SEC)
170 READ(5,101) XX,YY,ZZ
171 WRITE(5,1005)
172 READ(5,101) XF,YF,ZF
173 WRITE(5,1006)
174 READ(5,1007) NK,V,TAU
175 IF(NK.LE.0) GO TO 22
176 CALL JOVHO(1,TAU,1,0)
177 FN=NK-1
178 DX=(XF-XX)/FN
179 DY=(YF-YY)/FN
180 DZ=(ZF-ZZ)/FN
181 DT=SQRT(DX*DX+DY*DY+DZ*DZ)/V
182 TT=0.
183 C
184 C LOOP TO GENERATE X-,Y-, AND Z-COORDINATES AND OUTPUT THEM
185 C TO THE FLIGHT PATH FILE
186 DO 1 I=1,NK
187 CALL JOVHO(1,XX,4,0)
188 XX=XX+DX
189 YY=YY+DY
190 ZZ=ZZ+DZ
191 TT=TT+DT
192 C
193 C THIS CLOSSES THE FLIGHT PATH FILE AND RETURNS TO SWITCH POINT
194 CALL JOVREL(1)
195 GO TO 2
196 C
197 C THIS SECTION IS TO GENERATE ANTENNA DESCRIPTION FILE
198 N=0
199 WRITE(5,107)
200 C
201 C INPUT FOR ANTENNA FILE NAME
202 READ(5,2000) ILBL
203 WRITE(5,108)
204 C
205 C INPUT FOR ANTENNA PLOT LABEL
206 READ(5,105) ILABL
207 N=1
208 C
209 C THIS IS THE INPUT FOR ELEMENT DESCRIPTION
210 C X(I) X-COORDINATE OF I'TH ELEMENT (FEET)
211 C Z(I) Z-COORDINATE OF I'TH ELEMENT (FEET)
212 C C(I) COMPLEX AMPLITUDE OF CARRIER COMPONENT OF I'TH ELEMENT

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213 C C2(I) COMPLEX AMPLITUDE OF 150 HZ SIDEBAND OF I'TH ELEMENT
214 C C3(I) COMPLEX AMPLITUDE OF 90 HZ SIDEBAND OF I'TH ELEMENT
215 C THE PROGRAM WILL LOOP THRU 10 FOR ADDITIONAL ELEMENTS UNTIL A
216 C ZERO IS ENCOUNTERED FOR Z(N)
217 WRITE(9,1017)
218 10 READ(5,2001) X(N),Z(N),C1(N),C2(N),C3(N)
219 IF( Z(N) .EQ. 0) GO TO 9
220 C
221 C THIS SECTION DETERMINES THE Y OFFSET OF EACH ELEMENT. THIS
222 C IS NOMINALLY Y0 BUT THERE IS A SMALL CHANGE (LESS THEN ONE WAVELENGTH)
223 C FOR NEAR FIELD CORRECTION PURPOSES
224 SW=SIGN(1.,Z(N)-Z(1))
225 IF(N .NE. 1) GO TO 15
226 Y(1)=Y0
227 F=SQRT(Y0*Y0+Z(1)*Z(1))
228 GO TO 16
229 15 XB=Y0-SQRT(F*F-Z(N)*Z(N))
230 IF(XB=SW .LT. 0.) GO TO 17
231 10 XP=Y0-SQRT((F+RL)*(F+RL)-Z(N)*Z(N))
232 IF(XP=SW .LT. 0.) GO TO 18
233 F=F+RL*SW
234 XB=XP
235 GO TO 19
236 17 F=F-RL*SW
237 GO TO 15
238 18 Y(N)=Y0-XB
239 16 CONTINUE
240 N=N+1
241 GO TO 10
242 C
243 C THIS SECTION OUTPUTS THE ANTENNA DESCRIPTION TO THE FILE
244 C AND ON THE LINE PRINTER. CLOSSES THE FILE AND RETURNS TO THE SWITCH
245 C POINT
246 9 NEL=N-1
247 CALL OFILE(20,1LRL)
248 WRITE(20,105) I(LABL)
249 WRITE(20) RL,NEL,(X(I),Y(I),Z(I),C1(I),C2(I),C3(I),I=1,NEL)
250 WRITE(3,1016) I(LABL)
251 WRITE(3,2001) (X(I),Y(I),Z(I),C1(I),C2(I),C3(I),I=1,NEL)
252 CALL RELEAS(20)
253 GO TO 2
254 C
255 C THIS IS THE PROGRAM TERMINATION POINT
256 3 CALL EXIT
257 STOP
258 1012 FORMAT(' UNKNOWN SWITCH,')
259 1013 FORMAT(' INPUT SW(YCM),S)
260 1014 FORMAT(' INPUT GROUND FILE NAME:',S)
261 1015 FORMAT(' INPUT FLIGHT PATH FILE NAME!',S)
262 1017 FORMAT(' INPUT ELEMENT VALUES.,',/)
263 1016 FORMAT(2X,0A5)
264 104 FORMAT(' INPUT GROUND LABEL',/)
265 105 FORMAT(0A5)

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266 100 FORMAT(' INPUT GROUND SEGMENTS. STARTING FROM ANTENNA.'//
267 1' GIVE CONSECUTIVELY EITHER X AND Z INCREMENTS, OR THE'//
268 2' LENGTH AND ANGLE FROM HORIZONTAL IN DEGREES, SEPARATED'//
269 3' BY A ZERO. HIT CARRIAGE RETURN FOR END OF DATA.'//
270 4' OR IF THERE ARE NO MORE STRIPS.'//' 0',S)
271 101 FORMAT(3F)
272 103 FORMAT(' ONLY 20 GROUND SEGMENTS ALLOWED. COMPUTATION WILL'//
273 1' PROCEED WITH DATA ALREADY OBTAINED.'//)
274 102 FORMAT(' 0',S)
275 1003 FORMAT(' INPUT FLIGHT PATH TITLE'//)
276 1000 FORMAT(' INPUT FLIGHT PATH TYPE'//)
277 1000 FORMAT(A1)
278 1010 FORMAT(' INPUT XP,XF,M1'//,S)
279 1011 FORMAT(' INPUT Y0,LAMBDA1'//,S)
280 1004 FORMAT(' INPUT X0,Y0,201'//,S)
281 1005 FORMAT(' INPUT XF,YF,2F1'//,S)
282 1006 FORMAT(' INPUT # OF PRINTS, VELOCITY, TIME CONSTANT'//,S)
283 1007 FORMAT(1,2F)
284 107 FORMAT(' INPUT ANTENNA FILE NAME'//,S)
285 2000 FORMAT(A5)
286 100 FORMAT(' INPUT ANTENNA DESCRIPTION'//)
287 2001 FORMAT(0F)
288 ENH

```

CONSTANTS

P	20100402P10	1	94900402010P	7	435004020100	3	501004020100	4	405004020100
S	000000000024	6	0000000000201	7	200000000010	10	000000000000	11	000000000004
12	201400000000								

COMMON

XX	/,COMMON/+0	YY	/,COMMON/+1	ZZ	/,COMMON/+2	TT	/,COMMON/+3	K	/GROUND/+0
X1	/GROUND/+1	Z1	/GROUND/+25	X2	/GROUND/+51	Z2	/GROUND/+76	IEL	/GROUND/+123

SUBPROGRAMS

FORSE.	.JOBFF	END.	COSD	SIND	OF,LE	SINWR.	RELEAS	JOVSET	JOVNO	FLOAT	SORT	JOVREL	SIGN	EXIT
ALPH0.	ALPH1.	FLPUT.	FLIRT.	INT0.	INT1.									

SCALARS

NAME	1410	Y0	1411	PL	1412	R	1413	Z0	2
THETA	1414	K	P	4512E	1415	I	1416	HD	1417
XF	1420	M	1421	VE	1422	V	1423	TAU	1424
A1	1425	A2	1426	ZK	1427	XX	0	YT	1
YT	3	XDL	1430	ZOL	1431	TEMP	1430	TEMP2	1433
YF	1434	ZF	1435	FK	1436	DY	1437	DE	1440
NY	1441	N	1442	L0L	1443	S	1444	F	1445
XP	1446	NEL	1447	IEL	123				

ARRAYS

