

ARIZONA DEPARTMENT OF TRANSPORTATION

REPORT NUMBER: FHWA-AZ88-202-III

SMALL SIGN SUPPORT ANALYSIS

Phase II
Static, Pendulum and Full-Scale Crash Test Programs
Volume II (Appendices)

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Prepared for:

Arizona Department of Transportation 206 South 17th Avenue Phoenix, Arizona 85007 in cooperation with U.S. Department of Transportation Federal Highway Administration The contents of this report reflect the views of the authors who are responsible for the facts and the accuracy of the data presented herein. The contents do not necessarily reflect the official views or policies of the Arizona Department of Transportation or the Federal Highways Administration. This report does not constitute a standard, specification, or regulation. Trade or manufacturer's names which may appear herein are cited only because they are considered essential to the objectives of the report. The U.S. Government and the State of Arizona do not endorse products or manufacturers.

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test results of alternative small sign support systems for Arizona Department of Transportation (ADOT). The tests were conducted and evaluated in accordance with the recommendations of NCHRP Report 230 and the 1985 AASHTO "Standard Specifications for Structural Supports for Highway Signs, Luminaires and Traffic Signals."

Results of this research indicate that three-3 lb/ft or (based on energy based analysis) two-4 lb/ft 80 ksi Marion steel u-post supports and stubs assembled using a 4 in. nested splice (support assembled behind the stub) with 1/2 in. spacers and grade 9 bolts, nuts and washers will meet the evaluation criteria. It also is apparent from the results of this study that a slip-base retrofit for a sign support system with up to three P2 Uni-Strut posts will meet the evaluation criteria.

In all cases, tests were conducted in NCHRP Report 230 (2) Classification Sl (STRONG) soil. In cases where installation in a "weak" soil is anticipated, further evaluation is required.

This report is one of three reports prepared in the subject project. The other two are:

Small Sign Support Analysis: Phase I - Crash Test Program Phase III - Benefit/Cost Analysis

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FIELD BOLT SUMMARY TABLES

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Table A.1. Results of 72 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 3 Inch Back to Back Splice in Critical Configuration (Grade 5 Field Bolts).

 	1		2 00		BENDING	TEST	
Dist to	length () bolt A gauge () arm (in)	(in) in)	1.38 12.00	Back	ON 3 lb/: to back	; gr 5 bc	lts
LOAD (lbs)	 Ch.#1	Tip Defl	Total Defl	At G	AIN auge /in)	STRE (ks	
Appl Total	(mV)	(in)	(in)	Obs.	•	Base	Gauge
floor 60 60 32 92 32 124 32 156 32 188 32 220 32 252 32 284 32 316 16 332 16 348	1.951 2.686 2.807 3.101 3.309 3.513 3.724 3.928 4.123 4.323 4.519 4.615 4.696	0.77 0.43 0.45 0.50 0.48 0.46 0.32 0.53 0.32 0.33	0.00 0.77 1.19 1.64 2.14 2.62 3.09 3.55 3.87 4.40 4.72 5.05	•	0.037 0.277 0.404 0.532 0.660 0.788 0.915 1.043 1.171 1.299 1.363 1.427	1.89 12.44 18.06 23.69 29.32 34.94 40.57 46.19 51.82 57.44 60.25 63.07	1.11 3.37 8.87 12.76 16.57 20.51 24.33 27.97 31.71 35.37 37.17 38.68

^{*} Nominal yield stress

Table A.2. Results of 72 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 3 Inch Nested Splice in Critical Configuration (Grade 5 Field Bolts).

Splice length (in) 3.00 Dist to bolt A (in) 1.50 MARION 3 lb/ft - 80 ksi * Dist to gauge (in) 11.75 Nested; gr 5 bolts Moment arm (in) 72.06 Critical orientation Critical orientation STRAIN STRESS LOAD Tip Total At Gauge (ksi) (lbs) Ch.#1 Defl Defl (uin/in) Obs @ Appl Total (mV) (in) (in) Obs. Calc. Base Gauge Calc. Ca
Dist to bolt A (in) 1.50
LOAD
(lbs) Ch.#1 Defl Defl (uin/in) Obs @ Appl Total (mV) (in) (in) Obs. Calc. Base Gauge floor 1.851
Appl Total (mV) (in) (in) Obs. Calc. Base Gauge
floor 1.851 DL 1.927 0.00 0.037 0.037 1.90 1.11 60 60 2.324 0.90 0.90 0.283 0.277 12.42 8.50 32 92 2.534 0.50 1.39 0.414 0.405 18.03 12.41 48 140 2.743 0.51 1.90 0.544 0.597 26.45 16.31 32 172 2.945 0.50 2.40 0.669 0.725 32.06 20.07 32 204 3.141 0.49 2.89 0.791 0.853 37.67 23.72 32 236 3.350 0.54 3.43 0.921 0.981 43.28 27.62 32 268 3.542 0.52 3.95 1.040 1.109 48.89 31.19
DL 1.927 0.00 0.037 0.037 1.90 1.11 60 60 2.324 0.90 0.90 0.283 0.277 12.42 8.50 32 92 2.534 0.50 1.39 0.414 0.405 18.03 12.41 48 140 2.743 0.51 1.90 0.544 0.597 26.45 16.31 32 172 2.945 0.50 2.40 0.669 0.725 32.06 20.07 32 204 3.141 0.49 2.89 0.791 0.853 37.67 23.72 32 236 3.350 0.54 3.43 0.921 0.981 43.28 27.62 32 268 3.542 0.52 3.95 1.040 1.109 48.89 31.19
60
60
32
48 140 2.743 0.51 1.90 0.544 0.597 26.45 16.31 32 172 2.945 0.50 2.40 0.669 0.725 32.06 20.07 32 204 3.141 0.49 2.89 0.791 0.853 37.67 23.72 32 236 3.350 0.54 3.43 0.921 0.981 43.28 27.62 32 268 3.542 0.52 3.95 1.040 1.109 48.89 31.19
32 172 2.945 0.50 2.40 0.669 0.725 32.06 20.07 32 204 3.141 0.49 2.89 0.791 0.853 37.67 23.72 32 236 3.350 0.54 3.43 0.921 0.981 43.28 27.62 32 268 3.542 0.52 3.95 1.040 1.109 48.89 31.19
32
32 236 3.350 0.54 3.43 0.921 0.981 43.28 27.62 32 268 3.542 0.52 3.95 1.040 1.109 48.89 31.19
32 268 3.542 0.52 3.95 1.040 1.109 48.89 31.19
48 316 3.848 0.93 4.88 1.230 1.300 57.30 36.89
16 332 3.946 0.33 5.21 1.291 1.364 60.11 38.72
16 348 4.053 0.48 5.69 1.357 1.428 62.91 40.71
16 364 4.148 0.50 6.19 1.416 1.492 65.72 42.48
16 380 4.250 0.54 6.73 1.479 1.556 68.53 44.38

^{*} Nominal yield stress

Table A.3. Results of 72 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 3 Inch Face to Face Splice in Critical Configuration (Grade 5 Field Bolts).

!	~ 1.				ř	BENDING	TEST	!	
ĺ	Dist to	length (in bolt A (in bolt A (in bolt)) gauge (in arm (in))	(in) ln)	1.75 8.25	MARION 3 lb/ft - 80 ksi * Face to face; gr 5 bolts Critical orientation				
			7 40 00 10 40 60 av	ഡ വർഷം അം ഓ വ	STRAIN STRESS				
)AD			Total		auge	[(k		
•	bs)	Ch.#1	Defl	Defl		/in)	_	Obs @	
Appl	Total	(mV)	(in)	(in)	Obs.	Calc.	Base	Gauge	
	floor								
	DL	2.129		0.00	0.041		1.91	1.23	
60	60	1.667	0.97	0.97	0.329	0.297	12.51	9.87	
32	92	1.434	0.55	1.51	0.474	0.434	18.17	14.22	
32	124	1.223	0.50	2.02	0.605	0.570	23.82	18.16	
32	156	1.010	0.53	2.55	0.738	0.707	29.48	22.15	
32	188	0.805	0.54	3.08	0.866	0.843	35.13	25.98	
32	220	0.571	0.63	3.71	1.012	0.980	40.78	30.35	
16	236	0.486	0.26	3.97	1.065	1.048	43.61	31.94	
16	252	0.371	0.31	4.28	1.136	1.117	46.44	34.09	
16	268	0.275	0.28	4.56	1.196	1.185	49.27	35.88	
16	284	0.196	0.25	4.81	1.245	1.253	52.09	37.36	
16	300	0.098	0.33	5.13	1.306	1.321	54.92	39.19	
16	316	0.008	0.35	5.48	1.362	1.390	57.75	40.87	
16	332	-0.096	0.45	5.93	1.427	1.458	60.58	42.82	

^{*} Nominal yield stress

Table A.4. Results of 72 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 3 Inch Back to Back Splice in Non-critical Configuration (Grade 5 Field Bolts).

			<i></i>								
1						BENDING	TEST	1			
İ	•	length (i			MARION 3 1b/ft - 80 ksi *						
į	Dist to	gauge (i	in)	7.88	Bacl	k to back;	; gr 5 bo	1ts			
i	Moment	arm (in)		72.38	Non	Non-critical orientation					
İ											
1					STRAIN STRESS						
[LC)AD		Tip	Total	At (Gauge	(ks	i)			
j (1	.bs)	Ch.#1	Defl	Defl		n/in)		0bs @			
Appl	Total	(mV)	(in)	(in)	Obs.	Calc.	Base	Gauge			
						ab 45 45 97 88 98 98 98 98					
1	floor	**									
1	DL	8.242		0.00	0.042		1.89				
60	60	7.848	0.74	0.74	0.287		1	8.62			
32	92	7.661	0.38		0.404		18.09	12.12			
32	124	7.471	0.39		•		23.73	15.67			
32	156	7.266	0.41		0.650		29.36	19.50			
32	188	7.068	0.43		1		35.00	23.20			
32	220	6.878	0.46		0.892		40.63	26.76			
32	252	6.653	0.55		1.032		46.27	30.96			
32	284	6.446	0.50		•		51.90	34.83			
32	316	6.252	0.51		•		57.54				
32	348	6.052	0.67		1.406		63.17	42.19			
16	364	5.980	0.66	5.66	1.451	1.598	65.99	43.54			

^{*} Nominal yield stress

^{**} Strain gauge malfunction - data omitted

Table A.5. Results of 72 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 3 Inch Nested Splice in Non-critical Configuration (Grade 5 Field Bolts).

!	C-14	1 /	\	2 00		BENDING	TEST		
-	Dist to	length (i bolt A o gauge (i arm (in)	(in) in)	1.50	. 1	ON 3 lb/m Mested; gr critical	r 5 bolts		
•	OAD	Ch.#1	Tip Defl	Total Defl	At (RAIN Gauge n/in)	STRE (ks		1
App1	Total	(mV)	(in)	(in)	Obs.	Calc.	Base	Gauge	
 60 32	floor DL 60 92	1.949 2.059 1.652 1.444	0.92 0.58	0.00 0.92 1.49	0.037 0.291 0.420	0.277	1.90 1.90 12.46	1.11 8.72 12.61	
32	124 156	1.221	0.50	2.01	0.420 0.559 0.691	0.533	23.73 29.37	16.77 20.74	
32	188 220	0.696	0.75	3.26 3.79	0.886	0.789	35.00	26.59 30.62	 -
32	252 284	0.277 0.073	0.51	4.29 4.81	1.147	1.045 1.173	46.27 51.91	34.42 38.23	
32 32	316 348	-0.125 -0.323	0.56	5.37 5.99	1.398 1.521	1.301 1.430	57.54 63.18	41.93 45.63	
16	364	-0.422	0.46	6.45	1.583	1.494	66.00	47.48	İ

^{*} Nominal yield stress

Table A.6. Results of 72 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 3 Inch Face to Face Splice in Non-critical Configuration (Grade 5 Field Bolts).

Splice length (in)	3 00		BENDING	TEST	
Dist to bolt A	(in)	1.31		ON 3 1b/f		
Dist to gauge (in)	7.75	Face	to face;	; gr 5 b	olts
Moment arm (in)	7	2.19	Non-	critical	orienta	tion
]				
				RAIN		ESS.
LOAD		otal		Gauge	(K	si)
(lbs) Ch.#1	•	Defl		n/in)	_	Obs @
Appl Total (mV)	(in)	(in)	Obs.	Calc.	Base	Gauge
57						
floor 2.240	[0 00	0.060	0.040	1 1 00	1 06
DL 2.328		0.00	0.042		1.89	1.26
60 2.824	•	1.03	0.351	0.294	12.43	10.53
32 92 3.032	•	1.50	0.481	0.429	18.05	14.42
32 124 3.242	•	2.00	0.611	0.563	23.67	18.34
32 156 3.469		2.55	0.753	0.698	29.29	22.59
32 188 3.705	•	3.12	0.900	0.832	34.91	27.00
32 220 3.909		3.64	1.027	0.967	40.53	30.81
16 236 4.011		3.91	1.091	1.034	43.34	32.72
16 252 4.115	1	4.18	1.155	1.101	46.15	34.66
16 268 4.213	•	4.47	1.216	1.168	48.96	36.49
16 284 4.327	•	4.79	1.287	1.236	51.77	38.62
16 300 4.431	1	5.15	1.352	1.303	54.58	40.57
16 316 4.539	•	5.52	1.420	1.370	57.39	42.59
16 332 4.656	,	5.89	1.492	1.437	60.20	44.77
16 348 4.757	•	6.34	1.555	1.505	63.01	46.66
16 364 4.902	0.60	6.94	1.646	1.572	65.82	49.37

^{*} Nominal yield stress

Table A.7. Results of 72 Inch Bending Test: Marion 3 1b/ft - 80 ksi Post; 4 Inch Back to Back Splice in Critical Configuration (Grade 5 Field Bolts).

	~~~~~~~~~~								
   Splice	length (	in)	4 00		BENDING TEST				
	o bolt A			M(AT)	TON 3 11 /	£ 00 1	• .•.		
	o gauge (				MARION 3 lb/ft - 80 ksi *				
Moment	arm (in)		72 50		Back to back; gr 5 bolts Critical orientation				
	()	••••	. / 2 . 3 0		LICICAL O	riencacio	on j		
				l STI	STRAIN   S				
LOAD	1	Tip	Total	•	Gauge	STRE   (ks	i		
(lbs)	Ch.#1	Def1	Def1		n/in)		Obs @		
Appl Total	(mV)	(in)	(in)	Obs.	Calc.	Base	Gauge		
floor	0.015	Ì		İ		! !	i I		
DL	0.049	İ	0.00	0.041	0.041	1.90	1.23		
60 60	0.459	0.78	0.78	0.296	0.293	12.48	8.89		
32 92	0.668	0.41	1.18	0.427	0.428	18.13	12.80		
32 124	0.884	0.43	1.61	0.561	0.562	23.77	16.84		
32 156	1.106	0.43	2.04	0.700	0.697	29.42	20.99		
32 188	1.321	0.42	2.46	0.834	0.832	35.06	25.01		
32 220	1.536	0.43	2.89	0.967	0.966	40.71	29.02		
32 252	1.536	0.43	3.32	0.967	1.101	46.35	29.02		
32 284	1.772	0.50	3.82	1.115	1.236	52.00	33.44		
32 316	1.979	0.47	4.29	1.243	1.370	57.64	37.30 i		
32 348	2.175	0.47	4.76	1.366	1.505	63.28	40.97		
16 364	2.293	0.30	5.06	1.439	1.572	66.11	43.17		
32 396	2.502	0.43	5.49	1.569	1.707	71.75	47.08		
16 412	2.630	0.35	5.84	1.649	1.774	74.57	49.47		
16 428	2.728	0.27	6.11	1.710	1.842	77.40	51.30		
16 444	2.828	0.28	6.39	1.772	1.909	80.22	53.17		
16 460	2.912	0.27	6.66	1.825	1.976	83.04	54.74		
16 476	3.013	0.35	7.01	1.888	2.044	85.86	56.63		
16 492	3.104	0.33	7.33	1.944	2.111 j	88.69	58.33		

^{*} Nominal yield stress

Table A.8. Results of 72 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 4 Inch Nested Splice in Critical Configuration (Grade 5 Field Bolts).

					BENDING TEST				
	Dist to	length (i bolt A o gauge (i arm (in)	(in) in)	1.50 8.88	MARION 3 lb/ft - 80 ksi * Nested; gr 5 bolts Critical orientation				
					STRAIN   STRESS			SS	
L	DAD	1	Tip	Total	At G	auge	(ks	i)	
(:	lbs)	Ch.#1	Defl	Defl	(uin	/in)		Obs @	
App1	Total	(mV)	(in)	(in)	Obs.	Calc.	Base	Gauge	
	floor	2.251				0.044	1 00	.11.	
	DL	8.706		0.00	**	0.041	1.90	** 0 01	
60	60	12.700	0.81	0.81	0.297	0.297	12.61	8.91	
32	92	12.890	0.52	1.33	0.415	0.434	18.35	12.46 16.57	
32	124	13.110	0.45	1.78	0.552 0.690	0.571 0.708	24.09 1 29.83	20.69	
32	156	13.330	0.45		0.814	0.708	35.57	24.42	
32 32	188	13.530   13.730	0.43	2.67 3.13	0.014   0.939	0.844	41.31	28.16	
32	220 252	13.730   13.910	0.40	3.53	1.051	1.118	47.05	31.53	
32	284	14.110	0.41		1.176	1.255	52.80	35.27	
32	316	1 14.110 1 14.370	0.53		1.338	1.391	1 58.54	40.13	
32	348	14.580	0.48	4.96	1.468	1.528	64.28	44.05	
32	380	14.790	0.51	5.47	1.599	1.665	70.02	47.98	
32	412	15.010	0.55	6.02	1.736	1.802	75.76	52.09	
16	428	15.140	0.38		1.817	1.870	78.63	54.52	
16	444	15.270	0.40		1.898	1.939	81.50	56.95	
16	460	15.390	0.54	7.33	j 1.973	2.007	84.37	59.19	
16	476	15.530	0.57	7.90	2.060	2.075	87.24	61.81	

^{*} Nominal yield stress

^{**} Strain gauge malfunction - data omitted

Table A.9. Results of 72 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 4 Inch Face to Face Splice in Critical Configuration (Grade 5 Field Bolts).

					<b>.</b> .				
!	~ ~ ~ .						BENDING	TEST	
		length (i bolt A				MARI	ON 3 1b/i	t - 80 k	si *
•		gauge (					to face;		
•		arm (in)					itical or		
i		` ,			۱-				
					İ	STR	STRE	SS	
LO	AD	Ì	Tip	Total	1	At G	auge	(ks	i)
(1	.bs)	Ch.#1	Defl	Def1		(uin	/in)		Obs @
Appl	Total	(mV)	(in)	(in)		Obs.	Calc.	Base	Gauge
	~ ~ ~ ~ ~				-			*****	
1	floor		[						4 00
	DL	2.244		0.00	!	0.041	0.041	1.90	1.23
60	60	1.831	0.82	0.82	İ	0.298	0.293	12.45	8.95
32	92	1.624	0.40		!	0.427	0.428	18.07	12.82
32	124	1.415	0.42	1.64	ļ	0.558	0.563	23.70	16.73
32	156	1.201	0.45	2.09	ļ	0.691	0.697	29.32	20.73
32	188	0.993	0.43			0.820	0.832	34.95	24.61
32	220	0.783	0.45		1	0.951	0.967	40.57	28.54
32	252 284	0.547   0.325	0.51	3.48 3.97		1.098 1.237	1.101 1.236	46.20   51.82	32.95 37.10
1 32	316	0.323	0.49	3.97 4.47	1	1.373	1.236	57.45	41.19
1 32	348	0.106   -0.134	0.50		1	1.523	1.505	63.07	45.68
1 16	364	-0.134	0.37	5.36	1	1.601	1.573	65.89	48.03
1 16	380	1 -0.345	0.32		1 1	1.654	1.640	68.70	49.62
1 16	396	-0.465	0.25		!	1.729	1.707	71.51	51.87
1 16	412	I -0.582	0.42	6.36	!	1.802	1.775	74.32	54.05
16	428	I -0.702	0.52	6.88	1	1.877	1.842	77.14	56.30
					1			– .	

^{*} Nominal yield stress

Table A.10. Results of 72 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 4 Inch Back to Back Splice in Non-critical Configuration (Grade 5 Field Bolts).

1	Colica	1 cm = th /	:\	/ OC		BENDING	TEST	<u> </u>			
1	-	length (	•		14.77		g. 66.1	!			
1		o bolt A				MARION 3 lb/ft - 80 ksi *					
		o gauge (			Back to back; gr 5 bolts						
1	moment	arm (in)		./3.31	Non-	Non-critical orientation					
 					 	RAIN	l STRE				
1 7.0	OAD	1	Tip	Total	1			,			
	lbs)	Ch.#1	Defl	Defl	At Gauge   (ksi)   (uin/in)   Ob			Obs @			
	Total	(mV)	(in)	(in)	l Obs.		l Base	Gauge			
		()	(±11)	( ±11 )	055.	Galc.	Dase	Gauge			
1	floor	   -0.129	! 								
i	DL	-0.231	İ	0.00	0.041	0.041	1.89	1.23			
j 60	60	-0.646	0.68	0.68	0.300	0.297	12.59	8.99			
32	92	-0.863	0.37	1.05	0.435	0.434	18.30	13.04			
32	124	-1.083	0.37	1.41	0.572	0.570	24.01	17.16			
32	156	1.283	0.36	1.77	0.696	0.707	29.72	20.89			
32	188	-1.485	0.36	2.13	0.822	0.843	35.43	24.67			
32	220	-1.701	0.39	2.52	0.957	0.980	41.13	28.71 i			
32	252	-1.905	0.37	2.89	1.084	1.117	46.84	32.52			
32	284	-2.137	0.42	3.31	1.229	1.253	52.55	36.86			
32	316	-2.346	0.39	3.70	1.359	1.390	58.26	40.76			
32	348	-2.544	0.38	4.08	1.482	1.527	63.97	44.46			
32	380	-2.769	0.44	4.52	1.622	1.663	69.67	48.67			
32	412	-2.993	0.47	4.99	1.762	1.800	75.38	52.86			
16	428	-3.103	0.35	5.33	1.830	1.868	78.24	54.91			
16	444	-3.220	0.28	5.62	1.903	1.936	81.09	57.10 j			
16	460	-3.322	0.27	5.89	1.967	2.005	83.95	59.01 i			
16	476	-3.438	0.36	6.24	2.039	2.073	86.80	61.17			
								•			

^{*} Nominal yield stress

Table A.11. Results of 72 Inch Bending Test: Marion 3 1b/ft - 80 ksi Post; 4 Inch Nested Splice in Non-critical Configuration (Grade 5 Field Bolts).

			***************************************			BENDING	TEST		
	Dist to	length (; o bolt A o gauge (; arm (in)	(in) in)	1.75 7.25	MARION 3 lb/ft - 80 ksi * Nested; gr 5 bolts Non-critical orientation				
(	DAD lbs) Total	   Ch.#1   (mV)	Tip   Defl   (in)	Total Defl (in)	At G	AIN auge /in) Calc.	STRE   (ks     Base		
60   32   48   32   32   32   32   32   32   32   16   16	floor DL 60 92 140 172 204 236 268 300 332 364 396 412 428 444	2.238   2.191   1.770   1.561   1.222   1.005   0.774   0.543   0.329   0.107   -0.121   -0.347   -0.558   -0.651   -0.752   -0.867	0.86 0.44 0.72 0.46 0.50 0.48 0.45 0.47 0.48 0.49 0.47 0.22	0.00 0.86 1.30 2.02 2.47 2.97 3.45 3.90 4.36 4.84 5.32 5.79 6.01 6.26 6.57	1.066 1.199 1.337	0.043 0.307 0.448 0.660 0.801 0.942 1.083 1.224 1.365 1.506 1.647 1.788 1.858 1.929 1.999	1.91 12.68 18.42 27.03 32.77 38.52 44.26 50.00 55.74 61.48 67.23 72.97 75.84 78.71 81.58	1.29 9.13 13.02 19.34 23.38 27.68 31.99 35.97 40.11 44.36 48.57 52.50 54.23 56.11 58.25	
16   16   16   16	460 476 492 508	-0.962   -1.078   -1.209   -1.295	0.29 0.36 0.48 0.26	6.85 7.21 7.69 7.95	2.001   2.073   2.154   2.208	2.070 2.140 2.211 2.281	84.45 87.32 90.19 93.07	60.02   62.19   64.63   66.23	

^{*} Nominal yield stress

Table A.12. Results of 72 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 4 Inch Face to Face Splice in Non-critical Configuration (Grade 5 Field Bolts).

		~~~~									
1	0.1:	1 .1 .		4 00			BENDING	TEST			
1		length (15.5					
] 		o bolt A				MARION 3 lb/ft - 80 ksi * Face to face; gr 5 bolts					
l I		o gauge (arm (in)					critical				
1	Homene	arm (III)	• • • • •	. / 2 . 30	1_	NOII-	cricical	orientat	ion		
i						STRAIN STRESS					
i L	OAD	1	Tip	Total	1		Gauge	ks (ks	,		
i c	lbs)	Ch.#1	Defl	Def1	,				Obs @		
Appl	Total	(MV)	(in)	(in)	i	Obs.	Calc.	Base	Gauge		
					j -		******				
	floor] 2.235			1			ļ	Ì		
	DL	2.442		0.00		0.041	0.041	1.90	1.23		
60		2.849	0.88	0.88	ĺ	0.295	0.293	12.52	8.84		
32		3.041	0.40	1.28		0.414	0.427	18.18	12.43		
32		3.255	0.45	1.73		0.548	0.561	23.85	16.43		
32	156	3.478	0.47	2.20		0.686	0.696	29.51	20.59		
32		3.711	0.49	2.68	1	0.832	0.830	35.17	24.95		
32		3.927	0.46	3.14	1	0.966	0.965	40.83	28.99 i		
32	252	4.139	0.47	3.61	l	1.098	1.099	46.50	32.95		
32	284	4.358	0.48	4.09		1.235	1.233	52.16	37.04		
32	316	4.598	0.55	4.64		1.384	1.368	57.82	41.53		
32	348	4.808	0.51	5.14	ĺ	1.515	1.502	63.49	45.45		
32	380	5.006	0.51	5.65	ĺ	1.639	1.637	69.15	49.16		
32	412	5.204	0.59	6.24		1.762	1.771	74.81	52.86		
16	428	5.310	0.31	6.55	l	1.828	1.838	77.64	54.84		
16	444	5.398	0.35	6.90	ĺ	1.883	1.905	80.47	56.48		
16	460	5.506	0.40	7.30	l	1.950	1.972	83.30	58.50		
16	476	5.603	0.41	7.71		2.010	2.040	86.14	75.26		
									•		

^{*} Nominal yield stress

Table A.13. Results of 72 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 5 Inch Back to Back Splice in Critical Configuration (Grade 5 Field Bolts).

							BENDING	TEST		
1		length (
Į.		o bolt A				MARION 3 lb/ft - 80 ksi *				
		o gauge (; gr 5 bc		
	Moment	arm (in)	• • • • •	. 73 , 38		Cr	itical of	rientatio	n	
					-	cmp	A T'NT			
I T.C	DAD		Tip	Total	1		AIN auge	STRE		
•	lbs)	Ch.#1	Defl	Defl.	1		/in)	(ks	Obs@	
	Total	•	(in)		1	Obs.		 Base	Gauge	
					¦ -			Lance		
İ	floor	1.762			i			! 		
1	DL	2.172	ĺ	0.00	İ	0.039	0.039	1.90	1.17	
60	60	2.585	0.67	0.67	ĺ	0.296	0.287	12.61	8.89	
32	92	2.818	0.40	1.07	1	0.442	0.420	18.32	13.25	
32	124	3.046	0.40	1.46		0.584	0.552	24.04	17.51	
32	156	3.276	0.40	1.86		0.727	0.684	29.75	21.81	
32	188	3.502	0.39	2.25		0.868	0.817	35.46	26.03	
32	220	3.735	0.40	2.65		1.013	0.949	41.17	30.39	
32	252	3.963	0.40	3.05		1.155	1.081	46.89	34.65	
32	284	4.194	0.41	3.46		1.299	1.214	52.60	38.97	
32	316	4.408	0.40	3.86		1.432	1.346	58.31	42.97	
32	348	4.614	0.39	4.25		1.561	1.478	64.03	46.82	
32	380	4.834	0.42	4.67		1.698	1.610	69.74	50.93	
32	412	5.051	0.42	5.09		1.833	1.743	75.45	54.98	
32 32	444	5.278	0.45	5.53		1.974	1.875	81.16	59.23	
1 32	476	5.492	0.44	5.97	l	2.108	2.007	86.88	63.23	
1 32	508	5.705	0.50	6.46		2.240	2.140	92.59	67.21	
1 16	540 556	5.872	0.43	6.89	İ	2.344	2.272	98.30	70.33	
1 10	ا مدد	5.965	0.34	7.23	l	2.402	2.338	101.16	72.07	

^{*} Nominal yield stress

Table A.14. Results of 72 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 5 Inch Nested Splice in Critical Configuration (Grade 5 Field Bolts).

l I s	plice	length (in)	5 00			BENDING	TEST		
		bolt A				МАРТ	ai v			
		gauge (:				MARION 3 lb/ft - 80 ksi * Nested; gr 5 bolts				
		arm (in)				Critical orientation				
					-					
					i	STR	AIN	STRE	SS	
LOA	_		Tip	Total	İ	At G	auge	(ks	i)	
(1b	,	Ch.#1	Defl	Defl	j	(uin	/in)	Ì	Óbs @	
Appl '	Total	(mV)	(in)	(in)		Obs.	Calc.	Base	Gauge	
	loor	0.007			-					
T	DL	2.034 2.413	 1	0.00	!	0 020	0.020			
60	60	2.413	l 0.75	0.00	1	0.039	0.039	1.90	1.17	
32	92	3.025	0.73	1.15	1	0.420	0.287	12.46	8.59	
32	124	3.237	0.40	1.56	1	0.420	0.420 0.552	18.10	12.61	
32	156	3.454	0.41	1.99	!	0.552	0.552	23.73 29.37	16.57 20.63	
32	188	3.664	0.41	2.40	1	0.818	0.816	35.00	24.55	
32	220	3.902	0.47	2.87	1	0.967	0.010	40.64	29.00	
32	252	4.091	0.37	3.24	1	1.084	1.081	46.27	32.53	
32	284	4.302	0.42	3.66	1	1.216	1.213	51.91	36.48	
32	316	4.518	0.43	4.09	ĺ	1.351	1.346	57.54	40.52	
32	348	4.721	0.41	4.50	i	1.477	1.478	63.18	44.31	
32	380	4.904	0.38	4.87	i	1.591	1.610	68.81	47.73	
32	412	5.101	0.41	5.28	i	1.714	1.742	74.45	51.41	
32	444	5.289	0.39	5.67	i	1.831	1.875	80.08	54.93	
32	476	5.504	0.47	6.14	Ī	1.965	2.007	85.72	58.95	
32	508	5.729	0.52	6.65		2.105	2.139	91.35	63.15	
32	540	5.918	0.49	7.14	l	2.223	2.271	96.99	66.68	
32	572	6.165	0.75	7.88	İ	2.377	2.404	102.62	71.30	
16	588	6.303	0.41	8.29		2.463	2.470	105.44	73.88	

^{*} Nominal yield stress

Table A.15. Results of 72 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 5 Inch Face to Face Splice in Critical Configuration (Grade 5 Field Bolts).

Splice length (in) 5.00	•										
Dist to bolt A (in) . 1.88								BENDING	TEST		
Dist to gauge (in)10.50 Face to face; gr 5 bolts Critical orientation STRAIN STRESS LOAD Tip Total At Gauge (ksi) (lbs) Ch.#1 Defl Defl (uin/in) Obs @ Appl Total (mV) (in) (in) Obs. Calc. Base Gauge Ch.#1 Defl Defl (uin/in) Obs. Calc. Base Gauge Ch.#2 Ch.#3 O.870 O.870 O.870 O.870 O.870 O.870 O.870 O.870 O.870 O.870 O.870 O.870 O.870 O.871 O.78 O.78 O.286 O.287 12.54 8.57 O.32 O.92 O.061 O.41 O.41 O.417 O.419 O.418											
Moment arm (in)72.88							MARI	ON 3 1b/	ft - 80 l	csi *	
LOAD		l						Face	to face	; gr 5 bc	1ts
LOAD			Moment	arm (in)	• • • • •	.72.88		Cr	itical o	rientatio	n
LOAD							-				
(1bs)							1	STR	AIN	STRE	SS
Appl Total (mV) (in) (in) Obs. Calc. Base Gauge									-	(ks	:i)
floor 0.870			•	1			1	(uin	/in)	1	0bs @
DL		Appl	Total	(mV)	(in)	(in)		Obs.	Calc.	Base	Gauge
DL 0.667 0.00 0.039 0.039 1.90 1.17 60 60 0.271 0.78 0.78 0.286 0.287 12.54 8.57 32 92 0.061 0.41 1.19 0.417 0.419 18.21 12.50 32 124 -0.144 0.42 1.60 0.544 0.551 23.88 16.33 32 156 -0.335 0.39 2.00 0.663 0.684 29.56 19.90 32 188 -0.535 0.41 2.41 0.788 0.816 35.23 23.64 32 220 -0.745 0.44 2.85 0.919 0.948 40.91 27.56 32 252 -0.946 0.43 3.27 1.044 1.081 46.58 31.32 32 284 -1.170 0.47 3.75 1.184 1.213 52.25 35.51 32 316 -1.358 0.41 4.16 1.301 1.345 57.93 39.02 32 348 -1.571 0.45 4.61 1.433 1.477 63.60 43.00 32 380 -1.786 0.47 5.07 1.567 1.610 69.28 47.02 32 412 -1.977 0.42 5.49 1.686 1.742 74.95 50.59 16 428 -2.076 0.23 5.71 1.748 1.808 77.79 52.44 16 444 -2.171 0.22 5.93 1.807 1.874 80.62 54.22 16 460 -2.266 0.24 6.17 1.866 1.940 83.46 55.99 16 476 -2.391 0.32 6.49 1.944 2.006 86.30 58.33 16 492 -2.520 0.34 6.83 2.025 2.073 89.14 60.74 16 508 -2.623 0.31 7.13 2.089 2.139 91.97 62.67 16 524 -2.750 0.37 7.50 2.168 2.205 94.81 65.04 16 540 -2.838 0.29 7.78 2.223 2.271 97.65 66.68 16 556 -2.943 0.34 8.12 2.288 2.337 100.48 68.65							-				~
60				•	!	0.00					
32 92 0.061 0.41 1.19 0.417 0.419 18.21 12.50 32 124 -0.144 0.42 1.60 0.544 0.551 23.88 16.33 32 156 -0.335 0.39 2.00 0.663 0.684 29.56 19.90 32 188 -0.535 0.41 2.41 0.788 0.816 35.23 23.64 32 220 -0.745 0.44 2.85 0.919 0.948 40.91 27.56 32 252 -0.946 0.43 3.27 1.044 1.081 46.58 31.32 32 284 -1.170 0.47 3.75 1.184 1.213 52.25 35.51 32 316 -1.358 0.41 4.16 1.301 1.345 57.93 39.02 32 348 -1.571 0.45 4.61 1.433 1.477 63.60 43.00 32 380 -1.786 0.47 5.07 1.567 1.610 69.28 47.02 32 412 -1.977 0.42 5.49 1.686 1.742 74.95 50.59 16 428 -2.076 0.23 5.71 1.748 1.808 77.79 52.44 16 444 -2.171 0.22 5.93 1.807 1.874 80.62 54.22 16 460 -2.266 0.24 6.17 1.866 1.940 83.46 55.99 16 476 -2.391 0.32 6.49 1.944 2.006 86.30 58.33 16 492 -2.520 0.34 6.83 2.025 2.073 89.14 60.74 16 508 -2.623 0.31 7.13 2.089 2.139 91.97 62.67 16 524 -2.750 0.37 7.50 2.168 2.205 94.81 65.04 16 540 -2.838 0.29 7.78 2.223 2.271 97.65 66.68 16 556 -2.943 0.34 8.12 2.288 2.337 100.48 68.65]			•			1			•	
32		l .		•	•		1			•	
32	-			,						1	
32	ļ				•						
32 220 -0.745 0.44 2.85 0.919 0.948 40.91 27.56 32 252 -0.946 0.43 3.27 1.044 1.081 46.58 31.32 32 284 -1.170 0.47 3.75 1.184 1.213 52.25 35.51 32 316 -1.358 0.41 4.16 1.301 1.345 57.93 39.02 32 348 -1.571 0.45 4.61 1.433 1.477 63.60 43.00 32 380 -1.786 0.47 5.07 1.567 1.610 69.28 47.02 32 412 -1.977 0.42 5.49 1.686 1.742 74.95 50.59 16 428 -2.076 0.23 5.71 1.748 1.808 77.79 52.44 16 444 -2.171 0.22 5.93 1.807 1.874 80.62 54.22 16 460 -2.266 0.24 6.17 1.866 1.940 83.46 55.99 16 476 -2.391 0.32 6.49 1.944 2.006 86.30 58.33 16 492 -2.520 0.34 6.83 2.025 2.073 89.14 60.74 16 508 -2.623 0.31 7.13 2.089 2.139 91.97 62.67 16 524 -2.750 0.37 7.50 2.168 2.205 94.81 65.04 16 540 -2.838 0.29 7.78 2.223 2.271 97.65 66.68 16 556 -2.943 0.34 8.12 2.288 2.337 100.48 68.65	-			•	•					1	
32 252 -0.946 0.43 3.27 1.044 1.081 46.58 31.32 32 284 -1.170 0.47 3.75 1.184 1.213 52.25 35.51 32 316 -1.358 0.41 4.16 1.301 1.345 57.93 39.02 32 348 -1.571 0.45 4.61 1.433 1.477 63.60 43.00 32 380 -1.786 0.47 5.07 1.567 1.610 69.28 47.02 32 412 -1.977 0.42 5.49 1.686 1.742 74.95 50.59 16 428 -2.076 0.23 5.71 1.748 1.808 77.79 52.44 16 444 -2.171 0.22 5.93 1.807 1.874 80.62 54.22 16 460 -2.266 0.24 6.17 1.866 1.940 83.46 55.99 16 476 -2.391 0.32 6.49 1.944 2.006 86.30 58.33 16 492 -2.520 0.34 6.83 2.025 2.073 89.14 60.74 16 508 -2.623 0.31 7.13 2.089 2.139 91.97 62.67 16 524 -2.750 0.37 7.50 2.168 2.205 94.81 65.04 16 540 -2.838 0.29 7.78 2.223 2.271 97.65 66.68 16 556 -2.943 0.34 8.12 2.288 2.337 100.48 68.65	!				•						
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16 428 -2.076 0.23 5.71 1.748 1.808 77.79 52.44 16 444 -2.171 0.22 5.93 1.807 1.874 80.62 54.22 16 460 -2.266 0.24 6.17 1.866 1.940 83.46 55.99 16 476 -2.391 0.32 6.49 1.944 2.006 86.30 58.33 16 492 -2.520 0.34 6.83 2.025 2.073 89.14 60.74 16 508 -2.623 0.31 7.13 2.089 2.139 91.97 62.67 16 524 -2.750 0.37 7.50 2.168 2.205 94.81 65.04 16 540 -2.838 0.29 7.78 2.223 2.271 97.65 66.68 16 556 -2.943 0.34 8.12 2.288 2.337 100.48 68.65			1								
16 444 -2.171 0.22 5.93 1.807 1.874 80.62 54.22 16 460 -2.266 0.24 6.17 1.866 1.940 83.46 55.99 16 476 -2.391 0.32 6.49 1.944 2.006 86.30 58.33 16 492 -2.520 0.34 6.83 2.025 2.073 89.14 60.74 16 508 -2.623 0.31 7.13 2.089 2.139 91.97 62.67 16 524 -2.750 0.37 7.50 2.168 2.205 94.81 65.04 16 540 -2.838 0.29 7.78 2.223 2.271 97.65 66.68 16 556 -2.943 0.34 8.12 2.288 2.337 100.48 68.65	- [,		,						
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16 508 -2.623 0.31 7.13 2.089 2.139 91.97 62.67 16 524 -2.750 0.37 7.50 2.168 2.205 94.81 65.04 16 540 -2.838 0.29 7.78 2.223 2.271 97.65 66.68 16 556 -2.943 0.34 8.12 2.288 2.337 100.48 68.65	-								,		
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16 540 -2.838 0.29 7.78 2.223 2.271 97.65 66.68 16 556 -2.943 0.34 8.12 2.288 2.337 100.48 68.65	-						l				
16 556 -2.943 0.34 8.12 2.288 2.337 100.48 68.65	-						[
16 570							ļ		,		
1 10 3/2 -3.042 0.40 8.52 2.350 2.403 103.32 70.50	-		,				l				
	1	TO	5/2	-3.042	0.40	8.52		2.350	2.403	103.32	70.50

^{*} Nominal yield stress

Table A.16. Results of 72 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 5 Inch Back to Back Splice in Non-critical Configuration (Grade 5 Field Bolts).

					DENDING			
Dist to	length (i bolt A (gauge (i arm (in)	(in) ln)	1.75 10.25	BENDING TEST MARION 3 lb/ft - 80 ksi * Back to back; gr 5 bolts Non-critical orientation				
LOAD (1bs) Appl Total	Ch.#1 (mV)	Tip Defl (in)	At G uin	AIN auge /in) Calc.	STRE (ks			
floor 60 60 32 92 32 124 32 156 32 188 32 220 32 252 32 284 32 316 32 348 32 348 32 442 32 476 32 508 32 540 16 556 16 572 16 588	1.897 1.704 1.300 1.079 0.863 0.652 0.418 0.202 -0.017 -0.236 -0.455 -0.677 -0.902 -1.118 -1.347 -1.539 -1.738 -1.738 -1.957 -2.038 -2.162 -2.263	0.73 0.41 0.41 0.41 0.46 0.44 0.44 0.44 0.46 0.44 0.46 0.44 0.45 0.45 0.35	0.00 0.73 1.14 1.55 1.96 2.42 2.85 3.72 4.15 4.59 5.05 5.48 5.96 6.36 6.80 7.32 7.56 7.90 8.28	0.048 0.300 0.437 0.572 0.703 0.849 0.984 1.120 1.257 1.393 1.531 1.672 1.806 1.949 2.069 2.193 2.329 2.379 2.457 2.520	0.048 0.357 0.522 0.687 0.851 1.016 1.181 1.346 1.511 1.675 1.840 2.005 2.170 2.335 2.499 2.664 2.829 2.911 2.994 3.076	1.90 12.66 18.41 24.15 29.89 35.63 41.38 47.12 52.86 58.60 64.34 70.09 75.83 81.57 87.31 93.05 98.80 101.67 104.54 107.41	1.44 8.99 13.12 17.16 21.10 25.48 29.51 33.61 37.70 41.79 45.94 50.15 54.19 58.47 62.06 65.78 69.87 71.38 73.70 75.59	

^{*} Nominal yield stress

Table A.17. Results of 72 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 5 Inch Nested Splice in Non-critical Configuration (Grade 5 Field Bolts).

Splice length (in) 5.00						* 9 9 3 6 8 8 8 8 8		
LOAD	Dist t Dist t	o bolt A o gauge ((in) in)		RION 3 1b/ Nested; g	ft - 80 k r 5 bolts	; į	
LOAD					l S'	TRAIN	I STRE	ess i
(1bs)	LOAD	1	Tip	Total	•	,		
Appl Total (mV) (in) (in) Obs. Calc. Base Gauge	(1bs)	Ch.#1			•			
floor 2.218	Appl Total	(mV)	(in)	(in)	•	, ,	l Base	
DL								
60	floor	2.218	İ		i		Ì	i
60	•	2.042	1	0.00	0.03	9 0.039	1.90	1.17
32 92 1.424 0.41 1.18 0.424 0.418 18.10 12.72 32 124 1.207 0.42 1.60 0.559 0.550 23.74 16.78 32 156 0.986 0.42 2.02 0.697 0.682 29.37 20.91 32 188 0.763 0.43 2.45 0.836 0.814 35.01 25.08 32 220 0.553 0.40 2.85 0.967 0.946 40.65 29.00 32 252 0.360 0.37 3.22 1.087 1.078 46.28 32.61 32 284 0.152 0.40 3.63 1.217 1.210 51.92 36.50 32 316 -0.057 0.41 4.04 1.347 1.341 57.55 40.40 32 348 -0.279 0.43 4.46 1.485 1.473 63.19 44.55 32 380 -0.478 0.41 4.87 1.609 1.605 68.82 48.27 32 412 -0.673 0.39 5.26 1.731 1.737 74.46 51.92 32 444 -0.864 0.38 5.64 1.850 1.869 80.09 55.49 32 476 -1.059 0.40 6.04 1.971 2.001 85.73 59.13 32 508 -1.254 0.41 6.45 2.093 2.133 91.36 62.78 32 540 -1.434 0.39 6.84 2.205 2.265 97.00 66.14 32 572 -1.652 0.48 7.32 2.341 2.396 102.63 70.22 16 588 -1.743 0.21 7.53 2.397 2.462 105.45 71.92 16 604 -1.871 0.36 7.89 2.477 2.528 108.27 74.31 16 620 -1.934 0.19 8.08 2.516 2.594 111.08 75.49 28 648 -2.036 0.31 8.39 2.580 2.710 116.01 77.39 16 664 -2.122 0.31 8.70 2.633 2.776 118.83 79.00	•	1.640	0.77	0.77	0.28	9 0.286	•	
32	•	•	0.41	1.18	0.42	4 0.418	•	,
32	1		1		0.55	9 0.550	23.74	
32	•	•	,		0.69	7 0.682	29.37	
32 252 0.360 0.37 3.22 1.087 1.078 46.28 32.61 32 284 0.152 0.40 3.63 1.217 1.210 51.92 36.50 32 316 -0.057 0.41 4.04 1.347 1.341 57.55 40.40 32 348 -0.279 0.43 4.46 1.485 1.473 63.19 44.55 32 380 -0.478 0.41 4.87 1.609 1.605 68.82 48.27 32 412 -0.673 0.39 5.26 1.731 1.737 74.46 51.92 32 444 -0.864 0.38 5.64 1.850 1.869 80.09 55.49 32 476 -1.059 0.40 6.04 1.971 2.001 85.73 59.13 32 508 -1.254 0.41 6.45 2.093 2.133 91.36 62.78 32 540 -1.434 0.39 6.84 2.205 2.265 97.00 66.14 32 572 -1.652 0.48 7.32 2.341 2.396 102.63 70.22 16 588 -1.743 0.21 7.53 2.397 2.462 105.45 71.92 16 604 -1.871 0.36 7.89 2.477 2.528 108.27 74.31 16 620 -1.934 0.19 8.08 2.516 2.594 111.08 75.49 28 648 -2.036 0.31 8.39 2.580 2.710 116.01 77.39 16 664 -2.122 0.31 8.70 2.633 2.776 118.83 79.00	•	•	•		0.83	6 0.814	35.01	
32 252 0.360 0.37 3.22 1.087 1.078 46.28 32.61 32 284 0.152 0.40 3.63 1.217 1.210 51.92 36.50 32 316 -0.057 0.41 4.04 1.347 1.341 57.55 40.40 32 348 -0.279 0.43 4.46 1.485 1.473 63.19 44.55 32 380 -0.478 0.41 4.87 1.609 1.605 68.82 48.27 32 412 -0.673 0.39 5.26 1.731 1.737 74.46 51.92 32 444 -0.864 0.38 5.64 1.850 1.869 80.09 55.49 32 476 -1.059 0.40 6.04 1.971 2.001 85.73 59.13 32 508 -1.254 0.41 6.45 2.093 2.133 91.36 62.78 32 540 -1.434 0.39 6.84 2.205 2.265 97.00 66.14 32 572 -1.652 0.48 7.32 2.341 2.396 102.63 70.22 16 588 -1.743 0.21 7.53 2.397 2.462 105.45 71.92 16 604 -1.871 0.36 7.89 2.477 2.528 108.27 74.31 16 620 -1.934 0.19 8.08 2.516 2.594 111.08 75.49 28 648 -2.036 0.31 8.39 2.580 2.710 116.01 77.39 16 664 -2.122 0.31 8.70 2.633 2.776 118.83 79.00	•	•	•		0.96	7 0.946	40.65	29.00 j
32 316 -0.057 0.41 4.04 1.347 1.341 57.55 40.40 32 348 -0.279 0.43 4.46 1.485 1.473 63.19 44.55 32 380 -0.478 0.41 4.87 1.609 1.605 68.82 48.27 32 412 -0.673 0.39 5.26 1.731 1.737 74.46 51.92 32 444 -0.864 0.38 5.64 1.850 1.869 80.09 55.49 32 476 -1.059 0.40 6.04 1.971 2.001 85.73 59.13 32 508 -1.254 0.41 6.45 2.093 2.133 91.36 62.78 32 540 -1.434 0.39 6.84 2.205 2.265 97.00 66.14 32 572 -1.652 0.48 7.32 2.341 2.396 102.63 70.22 16 588 -1.743 0.21 7.53 2.397 2.462 105.45 71.92 16 604 -1.871 0.36 7.89 2.477 2.528 108.27 74.31 16 620 -1.934 0.19 8.08 2.516 2.594 111.08 75.49 28 648 -2.036 0.31 8.39 2.580 2.710 116.01 77.39 16 664 -2.122 0.31 8.70 2.633 2.776 118.83 79.00	•	•	•		1.08	7 1.078	46.28	
32 348 -0.279 0.43 4.46 1.485 1.473 63.19 44.55 32 380 -0.478 0.41 4.87 1.609 1.605 68.82 48.27 32 412 -0.673 0.39 5.26 1.731 1.737 74.46 51.92 32 444 -0.864 0.38 5.64 1.850 1.869 80.09 55.49 32 476 -1.059 0.40 6.04 1.971 2.001 85.73 59.13 32 508 -1.254 0.41 6.45 2.093 2.133 91.36 62.78 32 540 -1.434 0.39 6.84 2.205 2.265 97.00 66.14 32 572 -1.652 0.48 7.32 2.341 2.396 102.63 70.22 16 588 -1.743 0.21 7.53 2.397 2.462 105.45 71.92 16 604 -1.871 0.36 7.89 2.477 2.528 108.27 74.31 16 620 -1.934 0.19 8.08 2.516 2.594 111.08 75.49 28 648 -2.036 0.31 8.39 2.580 2.710 116.01 77.39 16 664 -2.122 0.31 8.70 2.633 2.776 118.83 79.00	•	1	1	3.63	1.21	7 1.210	51.92	36.50
32 380 -0.478 0.41 4.87 1.609 1.605 68.82 48.27 32 412 -0.673 0.39 5.26 1.731 1.737 74.46 51.92 32 444 -0.864 0.38 5.64 1.850 1.869 80.09 55.49 32 476 -1.059 0.40 6.04 1.971 2.001 85.73 59.13 32 508 -1.254 0.41 6.45 2.093 2.133 91.36 62.78 32 540 -1.434 0.39 6.84 2.205 2.265 97.00 66.14 32 572 -1.652 0.48 7.32 2.341 2.396 102.63 70.22 16 588 -1.743 0.21 7.53 2.397 2.462 105.45 71.92 16 604 -1.871 0.36 7.89 2.477 2.528 108.27 74.31 16 620 -1.934 0.19 8.08 2.516 2.594 111.08 75.49 28 648 -2.036 0.31 8.39 2.580 2.710 116.01 77.39 16 664 -2.122 0.31 8.70 2.633 2.776 118.83 79.00		•	•		1.34	7 1.341	57.55	40.40 i
32	•	•			1.48	5 1.473	63.19	44.55
32 444 -0.864 0.38 5.64 1.850 1.869 80.09 55.49 32 476 -1.059 0.40 6.04 1.971 2.001 85.73 59.13 32 508 -1.254 0.41 6.45 2.093 2.133 91.36 62.78 32 540 -1.434 0.39 6.84 2.205 2.265 97.00 66.14 32 572 -1.652 0.48 7.32 2.341 2.396 102.63 70.22 16 588 -1.743 0.21 7.53 2.397 2.462 105.45 71.92 16 604 -1.871 0.36 7.89 2.477 2.528 108.27 74.31 16 620 -1.934 0.19 8.08 2.516 2.594 111.08 75.49 28 648 -2.036 0.31 8.39 2.580 2.710 116.01 77.39 16 664 -2.122 0.31 8.70 2.633 2.776 118.83 79.00		•	•		1.60	1.605	68.82	48.27
32 476 -1.059 0.40 6.04 1.971 2.001 85.73 59.13 32 508 -1.254 0.41 6.45 2.093 2.133 91.36 62.78 32 540 -1.434 0.39 6.84 2.205 2.265 97.00 66.14 32 572 -1.652 0.48 7.32 2.341 2.396 102.63 70.22 16 588 -1.743 0.21 7.53 2.397 2.462 105.45 71.92 16 604 -1.871 0.36 7.89 2.477 2.528 108.27 74.31 16 620 -1.934 0.19 8.08 2.516 2.594 111.08 75.49 28 648 -2.036 0.31 8.39 2.580 2.710 116.01 77.39 16 664 -2.122 0.31 8.70 2.633 2.776 118.83 79.00	•	•			1.73	L 1.737	74.46	51.92 j
32 508 -1.254 0.41 6.45 2.093 2.133 91.36 62.78 32 540 -1.434 0.39 6.84 2.205 2.265 97.00 66.14 32 572 -1.652 0.48 7.32 2.341 2.396 102.63 70.22 16 588 -1.743 0.21 7.53 2.397 2.462 105.45 71.92 16 604 -1.871 0.36 7.89 2.477 2.528 108.27 74.31 16 620 -1.934 0.19 8.08 2.516 2.594 111.08 75.49 28 648 -2.036 0.31 8.39 2.580 2.710 116.01 77.39 16 664 -2.122 0.31 8.70 2.633 2.776 118.83 79.00		•	1		1.850	1.869	80.09	55.49 j
32 540 -1.434 0.39 6.84 2.205 2.265 97.00 66.14 32 572 -1.652 0.48 7.32 2.341 2.396 102.63 70.22 16 588 -1.743 0.21 7.53 2.397 2.462 105.45 71.92 16 604 -1.871 0.36 7.89 2.477 2.528 108.27 74.31 16 620 -1.934 0.19 8.08 2.516 2.594 111.08 75.49 28 648 -2.036 0.31 8.39 2.580 2.710 116.01 77.39 16 664 -2.122 0.31 8.70 2.633 2.776 118.83 79.00	•	•	•		1.97	L 2.001	85.73	59.13
32	•	,	•		2.093	3 2.133	91.36	62.78 j
16 588 -1.743 0.21 7.53 2.397 2.462 105.45 71.92 16 604 -1.871 0.36 7.89 2.477 2.528 108.27 74.31 16 620 -1.934 0.19 8.08 2.516 2.594 111.08 75.49 28 648 -2.036 0.31 8.39 2.580 2.710 116.01 77.39 16 664 -2.122 0.31 8.70 2.633 2.776 118.83 79.00	•	•	•		2.20	2.265	97.00	66.14
16 604 -1.871 0.36 7.89 2.477 2.528 108.27 74.31 16 620 -1.934 0.19 8.08 2.516 2.594 111.08 75.49 28 648 -2.036 0.31 8.39 2.580 2.710 116.01 77.39 16 664 -2.122 0.31 8.70 2.633 2.776 118.83 79.00					2.343	2.396	102.63	70.22 j
16 620 -1.934 0.19 8.08 2.516 2.594 111.08 75.49 28 648 -2.036 0.31 8.39 2.580 2.710 116.01 77.39 16 664 -2.122 0.31 8.70 2.633 2.776 118.83 79.00	•	•	1				105.45	71.92
28 648 -2.036 0.31 8.39 2.580 2.710 116.01 77.39 16 664 -2.122 0.31 8.70 2.633 2.776 118.83 79.00		•	•				108.27	74.31 j
16 664 -2.122 0.31 8.70 2.633 2.776 118.83 79.00	•		•				111.08	75.49 i
16 600 10.00 2.000 2.770 110.00	•				•		116.01	77.39
1 16 600 1 0 006 1 0 00 0 00 0 0 0 0 0 0							118.83	79.00 j
1 10 000 -2.286 0.30 9.00 2.736 2.842 121.65 82.07	16 680	-2.286	0.30	9.00	2.736	2.842	121.65	82.07

^{*} Nominal yield stress

Table A.18. Results of 72 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 5 Inch Face to Face Splice in Non-critical Configuration (Grade 5 Field Bolts).

	Colina	1	:\	BENDING TEST				
	Dist to	length (: bolt A	(in)	MARION 3 lb/ft - 80 ksi *				
		o gauge (:				e to face		
1	Moment	arm (in)		.72.38	Non	-critical	orientat	ion
					ST	RAIN	l STRE	355
į LO	DAD	1	Tip	Total		Gauge	(ks	
j (1	lbs)	Ch.#1	Def1	Defl	•	n/in)	1	Obs @
Appl	Total	(mV)	(in)	(in)		Calc.	Base	Gauge
	floor	 0.792						
i I	DL	1.011	i I	0.00	I I 0.040	0.040	1.89	1.20
60	60	1.467	I I 0.84	0.84	l 0.324		12.46	9.72
32	92	1.665	0.38	1.22	0.324		18.09	13.42
32		1.801	0.41	1.63	0.532		1 23.73	15.42
j 32	156	2.095	0.41	2.03	0.715		29.36	21.46
j 32	188	2.325	0.44	2.47	0.859		35.00	25.76
j 32	220	2.527	0.39	2.86	0.985		40.63	29.54
32	252	2.702	0.35	3.21	1.094		46.27	32.81
32	284	2.895	0.39	3.60	1.214		51.90	36.41
32	316	3.144	0.50	4.10	1.369		57.54	41.07
32	348	3.338	0.38	4.48	1.490		63.17	44.70
32	380 J	3.544	0.41	4.89	1.618	1.615	68.81	48.55
32	412	3.764	0.44	5.33	1.755	1.748	74.44	52.66
32	444	3.984	0.47	5.79	1.892	1.881	80.08	56.77
16	460	4.112	0.28	6.07	1.972	1.947	82.90	59.16 i
16	476	4.210	0.23	6.29	2.033	2.013	85.71	60.99 j
16	492	4.330	0.31	6.60	2.108	2.080 j	88.53	63.24 j
16	508	4.451	0.33	6.93	2.183	2.146	91.35	65.50
16	524	4.569	0.35	7.28	2.257	2.212	94.17	67.70
16	540	4.692	0.38	7.66	2.333	2.279	96.98	70.00
16	556	4.815	0.37	8.03	2.410	2.345	99.80	72.30
16	572	4.943	0.40	8.42	2.490	2.411	102.62	74.70
16	588	5.092	0.50	8.92	2.583	2.478	105.44	77.48

^{*} Nominal yield stress

17 " BENDING TESTS

FIELD BOLT SUMMARY TABLES

Franklin 3 & 4 lb/ft Posts - 60 ksi Nominal Yield Stress
Marion 3 & 4 lb/ft Posts - 80 ksi Nominal Yield Stress

Back to Back, Nested and Face to Face Splices
Critical and Non-critical Configurations

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Table B.1. Results of 17 Inch Bending Test: Franklin 3 lb/ft - 60 ksi Post; 3 Inch Back to Back Splice in Critical Configuration (Grade 5 Field Bolts).

	Dist to	length (; bolt A gauge (; arm (in)	(in) in)	BENDING TEST FRANKLIN 3 lb/ft - 60 ksi * Back to back; gr 5 bolts Critical orientation				
			 Read (in)		At G	AIN auge /in) Calc.	STR (ks	ESS i) Obs @ Gauge
0 200 200 200 200 200 200 100 100 43	floor	0.838 0.849 1.076 1.131 1.532 1.764 1.982 2.217 2.326 2.420	-1.22 -1.31 -1.40 -1.49 -1.58 -1.69 -1.80 -1.87 -1.97	0.00 0.09 0.18 0.27 0.37 0.47 0.58 0.65 0.75	-0.052 -0.059 -0.200 -0.234 -0.484 -0.629 -0.764 -0.911 -0.979 -1.037 -1.115	-0.052 -0.052 -0.189 -0.327 -0.464 -0.602 -0.739 -0.877 -0.945 -1.014 -1.083	1.94 1.94 10.09 18.25 26.41 34.57 42.73 50.89 54.97 59.05 63.13 64.88	

^{*} Nominal yield stress

Table B.2. Results of 17 Inch Bending Test: Franklin 3 lb/ft - 60 ksi Post; 3 Inch Nested Splice in Critical Configuration (Grade 5 Field Bolts).

1				BENDING TEST						
	-	length (bolt A	-		FRANK	LIN 3 1b	/ft - 60	ksi *		
İ	Dist to	gauge (in)	8.31	Nested; gr 5 bolts					
	Moment	arm (in)		16.75	Cr	Critical orientation				
1				İ						
						AIN		ESS.		
)AD		,	Total		auge	(ks	-		
	.bs)	Ch.#1	Read		(uin	/in)	1	Obs @		
Appl	Total	(mV)	(in)	(in)	Obs.	Calc.	Base	Gauge		
	***			***						
l	floor	0.644								
	DL	0.589			0.052	0.052	1.94	1.55		
0	0	0.606	-0.69	0.00	0.041	0.052	1.94	1.23		
200	200	0.396	1-0.79	0.10	0.172	0.191	10.25	5.74		
200	400	0.153	-0.90	0.21	0.323	0.331	18.56	9.93		
200	600	-0.083	-1.01	0.32	0.470	0.471	26.87	14.12		
200	800	-0.335	-1.13	0.44	0.627	0.610	35.19	18.30		
200	1000	-0.588	-1.26	0.57	0.785	0.750	43.50	22.49		
200	1200	-0.849	•	0.72	0.948	0.889	51.81	26.68		
200	1400		-1.65	0.96	1.130	1.029	60.12	30.87		
100	1500	-1.261	-1.83	1.14	1.204	1.099	64.28	32.96		
346	1846		-2.49	1.80			78.66			

^{*} Nominal yield stress

⁻ Stub cracked and allowed increased load and deflection proir to bolt failure - bolt fails at 1846 lbs

Table B.3. Results of 17 Inch Bending Test: Franklin 3 lb/ft - 60 ksi Post; 3 Inch Face to Face Splice in Critical Configuration (Grade 5 Field Bolts).

		~ ~ ~ ~ ~ ~							
-		Splice	longth (:\	3 00		BENDING	TEST	!
		Dist to	length () bolt A gauge () arm (in)	(in) in)	1.75 8.25	Face	KLIN 3 lb, to face itical or	gr 5 bo	1ts
						STR	RAIN	STR	ESS
ĺ	LC	AD		Tip	Total	At G	auge	(ks	
ĺ	(1	bs)	Ch.#1	Defl	Def1		n/in)	,	Obs @
ĺ	App1	Total	(mV)	(in)	(in)	Obs.	•	Base	Gauge
-								~~~~~~	
- 1		floor	1.191						į
1		DL	1.259		1	0.052	0.052	1.94	1.55
ı	0	0	1.277	-1.33	0.00	0.040	0.052	1.94	1.21
ı	200	200		-1.43	0.10	0.161	0.188	10.25	4.82
إ	200	400		-1.52	0.20	0.293	0.325	18.56	8.80
	200	600	0.671	-1.63	0.30	0.418	0.461	26.87	12.54
I	200	800		-1.79	0.46	0.555	0.598	35.19	16.64
ļ	200	1000		-1.97	0.64	0.697	0.734	43.50	20.90
	200	1200		-2.20	0.88	0.837	0.871	51.81	25.10
	100	1300	-0.118	-2.46	1.13	0.910	0.939	55.97	27.29
١	67	1367	-0.194	-2.98	1.66	0.957	0.985	58.75	28.71

^{*} Nominal yield stress

⁻ Stub cracked and allowed increased load and deflection - bolt did not fail - stroke limit reached at -2.98 in

Table B.4. Results of 17 Inch Bending Test: Franklin 3 lb/ft - 60 ksi Post; 3 Inch Back to Back Splice in Non-critical Configuration (Grade 5 Field Bolts).

!	C-14-	1		2 00	BENDING TEST					
		length (*****			_		
ļ		bolt A			FRANKLIN 3 lb/ft - 60 ksi *					
]		gauge (
1	Moment	arm (in)	• • • • • •	16./5	. Non-	critical	orientat	ion		
! !					cmn	ATN				
: 	DAD		~ ~ ~ 	Total	•	AIN		I		
	lbs)	 Ch.#1	 Read	Defl	•	auge	l (KS			
Appl			•		•	/in)	[D	~ [
lwhhr	TOCAT	ј (шу)	(in)	(in)	Obs.	Calc.	l base	Gauge		
· 	floor	-1.134				*****				
! 	DL	-1.320	1		0.052	0.052	1 1 1 0/4	1 55 1		
0	0	-1.327	0.75	0.00	0.056	0.052	•			
200	200	-1.588	0.66	0.09	0.030	0.032	•	,		
200	400	-1.832	0.56	0.18	0.371	0.333				
200	600	-2.105	0.47	0.28	0.541	0.474				
200	800	-2.376	0.37	0.38	0.710	0.614				
200	1.000	-2.654	0.27	0.48	0.883	0.755	•			
200	1200	-2.948	0.17	0.57	1.066	0.895				
200	1400	-3.260	0.06	0.69	1.260	1.036				
100	1500	-3.438	-0.02	0.76	1.371	1.106				
100	1600	-3.613	-0.12	0.86	1.480	1.177		,		
100	1700	-3.803	-0.24	0.99	1.599	1.247	72.59			
75	1775 j	-3.895	-0.36	1.10	1.656	1.300				
75	1850 j	-4.135	-0.49	1.23	1.806	1.352	78.83	54.17		
50	1900	-4.267	-0.60	1.34	1.888	1.388	80.91	56.64		
50	1950	-4.414	-0.79	1.53	1.979	1.423	82.98	59.38 i		
56	2006		İ				85.31			
	•		-	•	,		•	1		

^{*} Nominal yield stress

Table B.5. Results of 17 Inch Bending Test: Franklin 3 lb/ft - 60 ksi Post; 3 Inch Nested Splice in Non-critical Configuration (Grade 5 Field Bolts).

						~~~~~~		
1						BENDING	TEST	
! .	~	length (						_
!		bolt A					/ft - 60	
ļ		gauge (:					c 5 bolts	
] · !	moment	arm (in)	• • • • • •	10.30	NON-	critical	orientat	lon
 					STR	AIN	I STR	ESS
LC	AD	1	I	Total	At G		ks (ks	
j (1	.bs)	Ch.#1	Read	Defl		/in)	į ,	Obs @
Appl	Total	(mV)	(in)	(in)	Obs.	Calc.	Base	Gauge
					*****			
ļ	floor	1.092						
!	DL	1.240	1 10	0.00	-0.052	-0.052	1.94	-1.55
0	0	1.203	1.42	0.00	-0.029	-0.052	1.94	-0.86
200	200	1.436	1.32	0.10	-0.174	-0.188	10.06	-5.21
200	400	1.661	1.23	0.19	-0.314	-0.325	18.19	-9.42
200	600	1.870	1.13	0.29	-0.444	-0.461	26.32	-13.33
200	800	2.102	1.03	0.40	-0.589	-0.598	34.45	-17.66
200	1000	2.326	0.92	0.50	-0.728	-0.734	42.58	-21.85
200	1200	2.568	0.81	0.62	-0.879	-0.871	50.71	-26.37
100	1300	2.688	0.74	0.68	-0.954	-0.939	54.77	-28.62
100	1400	2.816	0.66	0.76	-1.034	-1.007	58.84	-31.01
100	1500	2.937	0.58	0.85	-1.109	-1.076	62.90	-33.27
100	1600	3.095	0.43	1.00	-1.207	-1.144	66.97	-36.22
100	1700	3.250	0.28	1.14	-1.304	-1.212	71.03	-39.12
100	1800	3.410	0.11	1.31	-1.404	-1.280	75.10	-42.11
100	1900	3.615	-0.13	1.55	-1.531	-1.348	79.16	-45.94
100	2000	3.831	1-0.40	1.82	-1.666	-1.417	83.23	-49.98
53	2053						85.38	

^{*} Nominal yield stress

Table B.6. Results of 17 Inch Bending Test: Franklin 3 lb/ft - 60 ksi Post; 3 Inch Face to Face Splice in Non-critical Configuration (Grade 5 Field Bolts).

-									
1							BENDING	TEST	
			length (						i
-			bolt A			FRANK	LIN 3 1b,	/ft - 60	0 ksi *
-			gauge (i				to face		
i		moment	arm (in)	• • • • •	16.69	Non-	critical	orient	ation
1						כייים בייים	AIN		 TRESS
	T.(	DAD		Tip	Total	,	auge		ksi)
i		lbs)	Ch.#1	Defl	Defl	•	/in)	i (1	Obs @
j		Total	,	(in)	(in)	•	Calc.	Base	Gauge
İ					*****	****			
1		floor	1.216						
		DL	1.386			-0.052	-0.052	1.94	-1.55
İ	0	0	1.391	2.28	0.00	-0.055	-0.052	1.94	-1.64
ļ	200	200	1.573	2.20	0.08	-0.168	-0.194	10.22	-5.05
!	200	400	1.786	2.10	0.18	-0.301	-0.335	18.50	-9.03
!	200	600	2.010	2.00	0.29	-0.440	-0.477	26.78	-13.21
ļ	200	800	2.231	1.89	0.39	-0.578	-0.618	35.07	
	200	1000	2.458	1.78	0.51	-0.720	-0.760	43.35	
i	200	1200   1400	2.727	1.64	0.64	-0.887	-0.902	51.63	
1	100	1500	2.983   3.196	1.46	0.82	-1.047	-1.043		-31.40
1	50	1550	3.252	1.24 1.15	1.04 1.13	-1.179	-1.114	64.06	
1	50	1600	3.357	1.06	1.23	-1.214 -1.280	-1.149	66.13	
1	50	1650	3.457	0.92	1.36	-1.342	-1.185   -1.220	70.27	-38.39
i	50	1700	3.598	0.59	1.69	-1.430	-1.256		-40.26   -42.90
			J. J. J	5.55	V./	- 1.430	~I.2J0	12.34	-44.90

^{*} Nominal yield stress

⁻ End of post (79 in) displaces 18 in laterally

Table B.7. Results of 17 Inch Bending Test: Franklin 4 lb/ft - 60 ksi Post; 4 Inch Back to Back Splice in Critical Configuration (Grade 5 Field Bolts).

	Dist to	length ( bolt A gauge ( arm (in)	(in) in)	1.50 9.19	Back	BENDING LIN 4 lb, to back	/ft - 60 ; gr 5 bo	lts
(1	AD   bs)   Total	Ch.#1 (mV)	•	Total Defl (in)	STRAIN   STRESS At Gauge   (ksi) (uin/in)   Obs Obs. Calc.   Base Gaug			
0 200 200 200 200 200 200 200 200 100 51	floor   DL   0   200   400   800   1000   1200   1400   1700   1751	0.254 0.418 0.594	-1.09  -1.18  -1.26  -1.33  -1.41  -1.49  -1.56  -1.65  -1.76	0.00 0.09 0.17 0.24 0.32 0.40 0.47 0.56 0.67 0.79	-0.048 -0.047 -0.147 -0.253 -0.355 -0.465 -0.576 -0.688 -0.803 -0.917 -0.977	-0.147 -0.246 -0.345	1.86 1.86 8.11 14.36 20.61 26.86 33.11 39.36 45.61 51.86 54.98 56.58	-1.42 -4.41 -7.59 -10.65 -13.94 -17.29 -20.64 -24.09

^{*} Nominal yield stress

Table B.8. Results of 17 Inch Bending Test: Franklin 4 lb/ft - 60 ksi Post; 4 Inch Nested Splice in Critical Configuration (Grade 5 Field Bolts).

1		Splice	length (	in)	4.00		BENDING	TEST	. <b>-</b> 4 * * * * * * * * * * * * * * * * * *
1		Dist to	bolt A	(in)	1.63			/ft - 60	
ĺ			gauge ( arm (in)					r 5 bolts	
l I		nomenc	arm (III)	• • • • • •	10.03	Gr ı	itical o	rientatio	on
-						grp	AIN	i cm	ESS
i	L	DAD		Į	Total	•	auge	31K	,
ĺ	(	lbs)	Ch.#1	Read	Defl		/in)	, (23 	Obs @
A	pp1	Total	(mV)	(in)	(in)		Calc.	Base	Gauge
- !		floor	0.145						ľ
Ţ	_	DL	0.065	1		0.049	0.049	1.86	1.48
! ,	0	0	0.061	-0.90	0.00	0.052	0.049	1.86	1.55
4 -	200	200	-0.082	1-0.96	0.06	0.141	0.136	7.80	4.22 j
	200 200	400	-0.232	-1.02	0.12	0.234	0.224	13.74	7.03
	200	600   800	-0.372	-1.09	0.19	0.321	0.312	19.68	9.64
	200	1000	-0.514 -0.673	-1.16	0.26	0.410	0.400	25.61	12.30
_	200	1200	-0.819	-1.22  -1.28	0.32	0.509	0.488	31.55	15.27
	200	1400	-0.981	1-1.25	0.39	0.600	0.576	37.49	18.00
	200	1600	-1.130	-1.33  -1.43	0.46	0.701 0.794	0.664	43.43	21.03
, -	100	1700 i	-1.315	-1.43  -1.47	0.58	0.794	0.751	49.37	23.81
	.00	1800	-1.294	•	0.63	0.896	0.795   0.839	52.34	27.27
j 1	.00	1900		-1.57	0.67	0.850	0.883	55.31 58.28	26.88
j 1	.00	2000	-1.455	-1.63	0.74	0.996	0.883	61.25	28.50   29.89
						0.770	0.72/	01.20	47.07

^{*} Nominal yield stress

Table B.9. Results of 17 Inch Bending Test: Franklin 4 lb/ft - 60 ksi Post; 4 Inch Nested Splice in Critical Configuration; Assembled Backwards (Grade 5 Field Bolts).

1		0-11	1	! \	, 00		BENDING	TEST	!
I			length (: bolt A			FRANK	LIN 4 1b/	/ft - 60	ksi *
i			gauge (				ested; gr		
i			arm (in)				itical (b		
i			` '			****			
i						STR	AIN	STR	ESS
j	LC	AD		Tip	Total	At G	auge	(ks	i)
j	(1	.bs)	Ch.#1	Defl	Def1	(uin	/in)		Obs @
Ì	App1	Total	(mV)	(in)	(in)	Obs.	Calc.	Base	Gauge
ļ									
		floor	0.088	1					
1		DL	0.128	1		-0.048	-0.048	1.86	-1.44
1	0	0	0.119	-0.27	0.00	-0.042	-0.048	1.86	-1.27
	200	200	0.260	1-0.34	0.07	-0.130	-0.136	7.77	-3.91
	200	400	0.413	1-0.40	0.13	-0.226	-0.224	13.69	-6.77
	200	600		-0.47		-0.316	-0.312	19.60	-9.48
.	200	800	0.711	-0.51	0.24	-0.411	-0.399	25.51	-12.34
I	200	1000	0.876	-0.60	0.33	-0.514	-0.487	31.43	-15.42
1	200	1200	1.022	-0.67	0.40	-0.605	-0.575	37.34	-18.15
	200	1400	1.191	1-0.74	0.47	-0.710	-0.663	43.26	-21.31
-	200	1600	1.341	1-0.82	0.55	-0.804	-0.750	49.17	-24.11
-	200	1800	1.493	-0.90	0.63	-0.898	-0.838	55.09	-26.95
j	200	2000	1.654	-1.00	0.73	-0.999	-0.926	61.00	-29.96
ĺ	8.0	2080	1.704	-1.11	0.84	-1.030	-0.961	63.37	-30.90
į	17	2097		l				63.87	

^{*} Nominal yield stress

Table B.10. Results of 17 Inch Bending Test: Franklin 4 lb/ft - 60 ksi Post; 4 Inch Face to Face Splice in Critical Configuration (Grade 5 Field Bolts).

	Dist to	length ( o bolt A o gauge ( arm (in)	(in) in)	. 1.50 . 9.13	Face	to face	TEST  /ft - 60 ; gr 5 borientation	olts
i	LOAD (1bs) l Total	   Ch.#1   (mV)	Tip   Defl   (in)	Total Defl (in)	At G	AIN auge /in) Calc.	STR   (ks   Base	ESS i)   Obs @   Gauge
200   200   200   200   200   200   200   200   100	0 400 0 600 0 800 0 1000 0 1200 0 1400 0 1600 0 1800 0 2000 0 2100	-0.100 -0.158 -0.169 -0.322 -0.470 -0.604 -0.760 -0.906 -1.064 -1.215 -1.487 -1.560 -1.702 -1.786	-1.34  -1.42  -1.56  -1.56  -1.63  -1.70  -1.78  -1.85  -1.94  -2.03  -2.12	0.00 0.08 0.15 0.22 0.29 0.36 0.44 0.51 0.60 0.69 0.78 0.85	0.048 0.055 0.150 0.242 0.326 0.423 0.514 0.612 0.707 0.876 0.921 1.010 1.062	0.048 0.048 0.136 0.224 0.312 0.399 0.487 0.575 0.663 0.750 0.838 0.926 0.970	1.86 1.86 7.75 13.64 19.54 25.43 31.32 37.21 43.11 49.00 54.89 60.79 63.73 65.21	1.44   1.64   4.50   7.27   9.78   12.69   15.42   18.37   21.20   26.28   27.64   30.30   31.87   0.00

^{*} Nominal yield stress

Table B.11. Results of 17 Inch Bending Test: Franklin 4 1b/ft - 60 ksi Post; 4 Inch Back to Back Splice in Non-critical Configuration (Grade 5 Field Bolts).

			~ ~ ~ ~ ~ ~ ~		******				
						BENDING	TEST		
	-	length (	-						
-	Dist to	bolt A	(in)	1.75	FRANKLIN 4 lb/ft - 60 ksi *				
		gauge (:			Back	to back	; gr 5 bo	lts	
	Moment	arm (in)		16.75	Non-	critical	orientat	ion	
~ ~ ~ ~ ~					•	RAIN	STR	ESS	
	AD		•	Total	•	Sauge	(ks	i)	
•	(lbs)   Ch.#1   Read			Defl	(uir	ı/in)		0bs @	
Appl Total (mV) (in) (in)				(in)	Obs.	Calc.	Base	Gauge	
	floor	-0.170							
_	DL	-0.287	0.00	2 22	0.048	0.048	1.86	1.44	
0	0	-0.297	0.89	0.00	0.054	0.048	1.86	1.63	
200	200	-0.438	0.83	0.06	0.142	0.136	7.84	4.26	
200	400	-0.599	0.77	0.12	0.242	0.224	13.82	7.27	
200	600	-0.736	0.70	0.19	0.328	0.311	19.80	9.83	
200	800	-0.889	0.64	0.25	0.423	0.399	25.79	12.69	
200	1000	-1.033	0.57	0.32	0.513	0.487	31.77	15.38	
200	1200	-1.190	0.50	0.39	0.611	0.575	37.75	18.32	
200	1400	-1.351	0.44	0.45	0.711	0.662	43.73	21.33	
100	1500	-1.431	0.40	0.49	0.761	0.706	46.72	22.82	
100 100	1600   1700	-1.511   -1.584	0.37	0.52	0.811	0.750	49.71	24.32	
100	1800		0.33	0.56	0.856	0.794	52.71	25.68	
100	1900	-1.0/2	0.29	0.60	0.911 0.956	0.838 0.882	55.70 58.69	27.33 28.69	
100	2000		0.26	0.63	1.012	0.882	61.68	30.37	
100	2100		0.22	0.87	1.012	0.923	64.67	31.89	
100	2200		0.13	0.76	1.115	1.013	67.66	33.46	
100	2300	-2.000	0.13	0.76	1.174	1.013	70.65	35.23	
100	2400	-2.190	-0.01	0.90	1.234	1.101	73.64	37.01	
100	2500	-2.293	-0.11	1.00	1.298	1.145	76.63	38.93	
100	2600		1-0.24	1.12	1.348	1.143	79.63	40.43	
80	2680	~~ 	- U . 24 	An a Andra	1 1.J40	1.109	82.02	40.43	
00	2000		I		I		1 02.02		

^{*} Nominal yield stress

Table B.12. Results of 17 Inch Bending Test: Franklin 4 lb/ft - 60 ksi Post; 4 Inch Nested Splice in Non-critical Configuration (Grade 5 Field Bolts).

-										
١						BENDING TEST				
i		Splice	length (	in)	4.00			10 mm cp 100		
i			bolt A			FRANK	IIN 4 1b	/ft - 60	kei *	
i			gauge (:					r 5 bolts		
i			arm (in)					orientat		
i			( / /		20.00		CITCICAL	Orrencac		
i						מידים ו	AIN	ן פידיס	ESS	
i	LC	AD	1	t	Total		auge	(ks		
i		.bs)	Ch.#1	Read	Defl	•	/in)	1 (23	Obs @	
	•	Total		(in)	(in)	Obs.	Calc.	   Base	Gauge	
1	bb~		. ()	(	( 111)	00s.	calc.	l pase	Gauge	
1		floor	-0.175					1		
i		DL	-0.022	ŀ		   -0.048	-0.048	1 1 1.86	-1.44	
i	0	0	-0.022	1.55	0.00	-0.048	-0.048	1.86	-1.44	
1	200	200	0.125	1.46	0.09	-0.140	-0.137	7.89	-4.19	
1	200	400	0.279	1.40	0.16	-0.236	-0.137	13.91	-7.07	
1	200	600	0.438	1.32	0.23	-0.335	-0.314	19.94	,	
1	200	800	0.430	1.25	0.23	-0.333		I .	-10.04	
!	200	1000	0.758	1.18	0.31	-0.534	-0.402	25.97	-13.29	
1	200	1200	0.738	1.11	0.36	-0.534	-0.491	32.00	-16.02	
1	200	1400	1.079	1.04	0.44		-0.579	38.03	-19.03	
1	200	1600	1.244	0.97	0.51	-0.734	-0.668	44.06	-22.02	
1	100	1700	1.323			-0.837	-0.757	50.09	-25.10	
1	100	1800	1.459	0.93	0.62	-0.886	-0.801	53.10	-26.58	
1	100	1900	1.596	0.89	4	-0.971	-0.845	56.11	-29.12	
1	100	2000	1.576	0.85	0.71	-1.056	-0.889	59.13	-31.68	
1	100	2100			0.75	-1.044	-0.934	62.14	-31.31	
	100	2200	1.711	0.75	0.80	-1.128	-0.978	65.16	-33.83	
!	100	2300	1.847	0.66	0.89	-1.212	-1.022	68.17	-36.37	
!	100	2400	1.930	0.60	0.96	-1.264	-1.067	71.19	-37.93	
i	100	2500	1.962	0.52	1.04	-1.284	-1.111	74.20	-38.52	
1	100	,	2.083	0.42	1.14	-1.360	-1.155	77.21	-40.79	
1		2600	2.164	0.29	1.26	-1.410	-1.199	80.23	-42.30	
- [	100	2700	2.286	0.17	1.38	-1.486	-1.244	83.24	-44.58	
1	74	2774	l		ļ		ļ	85.47	I	

^{*} Nominal yield stress

Table B.13. Results of 17 Inch Bending Test: Franklin 4 lb/ft - 60 ksi Post; 4 Inch Nested Splice in Non-critical Configuration; Assembled Backwards (Grade 5 Field Bolts).

*****									
D:	ist to	length ( bolt A gauge ( arm (in)	(in)	1.63 9.06	BENDING TEST  FRANKLIN 4 1b/ft - 60 ksi Nested; gr 5 bolts Non-critical (backwards)				
LOAI (1bs		   Ch.#1   (mV)	   Read   (in)	Total Defl (in)	At (	RAIN Gauge n/in) Calc.	STR   (ks     Base	ESS i) Obs @ Gauge	
0	Loor DL 0 200 400 600 800 L000 L200 L400 L200 L200 L200 L200 L2	-0.980 -1.133 -1.296 -1.451 -1.618 -1.784 -1.862 -1.942 -2.029 -2.107 -2.198 -2.298 -2.382	0.46   0.39   0.34   0.28   0.21   0.05   0.02  -0.04  -0.11  -0.19  -0.23  -0.27  -0.33  -0.39  -0.46  -0.54  -0.64	0.00 0.07 0.13 0.18 0.25 0.31 0.37 0.44 0.50 0.57 0.65 0.69 0.73 0.79 0.85 0.92 1.00 1.10	0.049   0.032   0.138   0.234   0.316   0.419   0.511   0.606   0.708   0.804   0.908   1.012   1.060   1.110   1.164   1.213   1.270   1.332   1.384   1.435	0.049 0.049 0.139 0.229 0.319 0.409 0.499 0.589 0.679 0.769 0.860 0.950 0.955 1.040 1.085 1.130 1.175 1.220 1.265 1.310	1.86   1.86   7.80   13.74   19.68   25.61   31.55   37.49   43.43   49.37   55.31   61.25   64.22   67.19   70.16   73.13   76.10   79.07   82.04   85.01   87.18	1.48 0.97 4.16 6.86 9.57 12.27 14.97 17.68 20.38 23.08 25.79 28.49 29.84 31.20 32.55 33.90 35.25 36.60 37.95 39.31	

^{*} Nominal yield stress

Table B.14. Results of 17 Inch Bending Test: Franklin 4 lb/ft - 60 ksi Post; 4 Inch Face to Face Splice in Non-critical Configuration (Grade 5 Field Bolts).

			length ( o bolt A			E'D A NIL	BENDING		1		
i			o gauge (				FRANKLIN 4 lb/ft - 60 ksi * Face to face; gr 5 bolts				
1			arm (in)								
i		2101110110	carm (III)	• • • • •	. 10. 30	NOII.	critical	orientat	lon		
						STE	RAIN	I STR	RESS		
ĺ	L	DAD	i	Tip	Total	•	auge	(ks			
ı	(:	lbs)	Ch.#1	Defl	Def1	*	ı/in)	(	Obs @		
1 4	Appl	Total	(mV)	(in)	(in)	•	Calc.	Base	Gauge		
-	****	******									
1		floor	-0.105	ĺ		İ		, 			
		DL	0.064			-0.048	-0.048	1.86	-1.44		
1	0	0	0.074	2.36	0.00	-0.054	-0.048	1.86	-1.63		
1	200	200	0.202	2.31	0.05	-0.134	-0.136	7.75	-4.02		
	200	400	0.351	2.25	0.11	-0.227	-0.224	13.64	-6.80		
Į	200	600	0.512	2.19	0.17	-0.327	-0.312	19.54	-9.81		
	200	800	0.653	2.13	0.23	-0.415	-0.399	25.43	-12.45		
1	200	1000	0.812	2.07	0.29	-0.514	-0.487	31.32	-15.42		
	200	1200	0.972	2.01	0.36	-0.614	-0.575	37.21	-18.41		
	200	1400	1.132	1.95	0.42	-0.713	-0.663	43.11	-21.40		
1	200	1600	1.288	1.88	0.49	-0.811	-0.750 j	49.00	-24.32		
1	200	1800	1.451	1.81	0.55	-0.912	-0.838	54.89	-27.36		
	200	2000	1.621	1.72	0.64	-1.018	-0.926	60.79	-30.54 j		
ļ	100	2100	1.702	1.67	0.69	-1.069	-0.970	63.73	-32.06 j		
!	100	2200	1.793	1.61	0.75	-1.125	-1.014	66.68	-33.76		
	100	2300	1.889	1.54	0.83	-1.185	-1.057	69.63	-35.55		
	100	2400	1.982	1.44	0.92	-1.243	-1.101	72.57	-37.29		
-	100	2500	2.086	1.34	1.03	-1.308	-1.145	75.52	-39.23		
	100	2600	2.187	1.24	1.13	-1.371	-1.189	78.46	-41.12		
ı	100	2700	2.312	1.11	1.25	-1.449	-1.233	81.41	-43.46		

^{*} Nominal yield stress

⁻ Bolt did not break-lateral translation of 18"

Table B.15. Results of 17 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 4 Inch Back to Back Splice in Critical Configuration (Grade 5 Field Bolts).

								~ ~ ~ ~ ~ ~ ~ ~ ~
1						BENDING	TEST	1
j I	Dist to	length (in) bolt A (in) gauge (in) arm (in)	(in) in)	1.38 9.00	Back	on 3 lb/i to back;	gr 5 bo	lts
					STE	AIN	I STR	ESS
i LO	AD		]	Total		auge	(ks	
(1	.bs)	Ch.#1	Read	Def1	(uir	n/in)		Obs @
Appl	Total	(mV)	(in)	(in)	Obs.	Calc.	Base	Gauge
       0   200	floor   DL   0 200	1.016 1.130 1.134 1.332	      -1.09  -1.16	0.00	0.041 0.043 0.167		1.90 1.90 1.90	1.23   1.30   5.01
j 200	400	1.527	-1.22	0.14	0.288	0.263		8.65
200	600	1.718	-1.29	0.20	0.407	0.374	27.27	12.22
200	800	1.909	•	0.28	0.526	0.485		15.79
200	1000		-1.43	0.35	0.642	0.596		19.25
200	1200		-1.54	0.45	0.769	0.707	52.64	23.08
200	1400   1600		-1.63  -1.73	0.54 0.64	0.883	0.818	61.10	26.50
100   100	1700   1800	2.892 2.892	-1.79		1.015	0.929   0.985	69.56   73.79   78.01	30.44   34.16

^{*} Nominal yield stress

Table B.16. Results of 17 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 4 Inch Nested Splice in Critical Configuration (Grade 5 Field Bolts).

Dist to	length () bolt A gauge () arm (in)	(in) in)	1.96 9.25	N	ested; gi	TEST  ft - 80 k  5 bolts  cientatio	
LOAD (lbs)	   Ch.#1		 Total	STR At G	AIN auge /in)		ESS
floor   DL   0 0   200 200   200 400   200 800   200 1200   200 1200   200 1400   200 1800   200 2000   100 2100   50 2150   49 2199	0.944 0.880 0.865 0.705 0.538 0.391 0.223 0.058 -0.120 -0.297 -0.470 -0.650 -0.831 -0.928 -0.967	-0.31  -0.39  -0.46  -0.53  -0.61  -0.68  -0.76  -0.84  -0.93  -1.02  -1.15  -1.23	0.00 0.08 0.15 0.22 0.29 0.37 0.45 0.53 0.61 0.71 0.84 0.92 1.05	0.040 0.049 0.149 0.253 0.345 0.449 0.552 0.663 0.773 0.881 0.993 1.106 1.166	0.040 0.040 0.142 0.245 0.347 0.449 0.551 0.653 0.756 0.858 0.960 1.062 1.113 1.139	1.90 1.90 10.15 18.40 26.66 34.91 43.16 51.42 59.67 67.92 76.18 84.43 88.56 90.62	1.20 1.48 4.27 7.34 10.41 13.47 16.54 19.60 22.67 25.73 28.80 31.87 33.40 34.16

^{*} Nominal yield stress

Table B.17. Results of 17 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 4 Inch Face to Face Splice in Critical Configuration (Grade 5 Field Bolts).

					90 00 00 and and and any up my my	BENDING	TECT	
 	Dist to	length ( bolt A gauge ( arm (in)	(in) in)	1.88 9.38	Face	on 3 lb/i to face;	ft - 80 k gr 5 bo	lts
(1	AD   bs)   Total	Ch.#1 (mV)	Tip   Defl   (in)	Total   Defl   (in)	At G	AIN auge /in) Calc.	STR (ks	ESS i) Obs @ Gauge
0   200   200   200   200   200   200   200   200   200	floor   DL   0   200   400   800   1000   1200   1400   1600   1750	0.894 0.725 0.572 0.409 0.231 0.053 -0.128 -0.302 -0.442	    -1.52  -1.60  -1.68  -1.76  -1.84  -1.93  -2.02  -2.10  -2.31  -2.31	0.00 0.08 0.16 0.24 0.32 0.41 0.50 0.58 0.69 0.79	0.040 0.084 0.148 0.253 0.348 0.450 0.561 0.672 0.785 0.893 0.980 1.089	0.040 0.040 0.140 0.239 0.338 0.438 0.537 0.637 0.736 0.835 0.910 1.012	1.90 1.90 10.11 18.33 26.54 34.75 42.97 51.18 59.40 67.61 73.77 82.23	1.20 2.51 4.43 7.59 10.45 13.50 16.83 20.15 23.54 26.79 29.41 32.66

^{*} Nominal yield stress

Table B.18. Results of 17 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 4 Inch Back to Back Splice in Non-critical Configuration (Grade 5 Field Bolts).

•						~~~			
1							BENDING	TEST	]
1		Splice	length (	in)	4.00				1
-		Dist to	o bolt A	(in)	1.19	Mari	on 3 1b/	ft - 80 k	si* i
-		Dist to	o gauge (	in)	9.13	Back	to back	; gr 5 bo	lts
ļ		Moment	arm (in)	• • • • •	16.19	Non-	critical	orientat	ion
ļ									
İ						STR	AIN	STR	ESS
		DAD			Total	•	auge	(ks	1)
1	(lbs)					(uin	/in)	1	Obs @
1	Appr	Total	(mV)	(in)	(in)	Obs.	Calc.	Base	Gauge
- [	E & C E &	£7	********				****		
		floor	1.002	1		1		1	ĺ
ļ		DL	0.928			0.040	0.040	1.90	1.20
-	0	0	1.006	0.96	0.00	-0.009	0.040	1.90	-0.26
	200	200	0.833	0.90	0.07	0.099	0.134	9.78	2.98
l	200	400	0.672	0.84	0.13	0.200	0.228	17.65	5.99
1	200	600	0.419	0.77	0.19	0.357	0.321	25.53	10.71
ļ	200	800	0.334	0.71	0.26	0.410	0.415	33.41	12.30
ļ	200	1000	0.162	0.65	0.32	0.517	0.508	41.29	15.52
-	200 200	1200	-0.005	0.58	0.38	0.621	0.602	49.17	18.64
ļ		1400	-0.181	0.50	0.46	0.731	0.695	57.05	21.93
ļ	200 200	1600	-0.372	0.43	0.54	0.850	0.789	64.92	25.50
-	200	1800   2000	-0.548	0.35	0.62	0.960	0.883	72.80	28.79
1	100	2100	-0.727	0.23	0.73	1.071	0.976	80.68	32.13
1	100	2200	-0.815	0.17	0.79	1.126	1.023	84.62	33.78
1	100	2300 [	-0.909	0.09	0.88	1.185	1.070	88.56	35.54
1	90	2390	-0.990 -1.076	0.02	0.94	1.235	1.117	92.50	37.05
1	80	2470		-0.07	1.03	1.289	1.159	96.04	38.66
I I	130	2600	-1.145 -1.240	-0.16	1.12	1.332	1.196	99.20	39.95
	83	2683	-1.240	-0.31	1.27	1.391	1.257	104.32	41.72
1		2005		l	I			107.59	1

^{*} Nominal yield stress

Table B.19. Results of 17 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 4 Inch Nested Splice in Non-critical Configuration (Grade 5 Field Bolts).

Dist to	length (; bolt A gauge (; arm (in)	(in) in)	1.50 8.94	BENDING TEST  Marion 3 lb/ft - 80 ksi * Nested; gr 5 bolts Non-critical orientation				
LOAD (lbs)	Ch.#1 (mV)	•	Total Defl (in)	At C	AIN Gauge Jin) Calc.	STR   (ks     Base	ESS   i)   Obs @   Gauge	
floor DL 0 0 200 200 200 400 200 600 200 800 200 1000 200 1200 200 1400 200 1600 230 1830 220 2050 140 2190 160 2350 125 2475 115 2590 102 2692	1.161 1.226 1.216 1.419 1.592 1.808 1.980 2.180 2.372 2.567 2.761 3.017 3.246 3.388 3.555 3.702 3.856	1.40   1.32   1.24   1.15   1.07   0.98   0.88   0.79   0.67   0.52   0.38   0.27   0.13   -0.03	0.00 0.09 0.17 0.26 0.33 0.43 0.52 0.61 0.73 0.89 1.02 1.14 1.28 1.44 1.70	0.041 0.035 0.161 0.269 0.404 0.511 0.635 0.755 0.877 0.997 1.157 1.300 1.388 1.492 1.584 1.680	0.041 0.041 0.154 0.268 0.381 0.494 0.608 0.721 0.835 0.948 1.079 1.204 1.283 1.374 1.445 1.510	1.90 1.90 10.41 18.93 27.45 35.96 44.48 52.99 61.51 70.02 79.82 89.19 95.15 101.96 107.28 112.18 116.52	1.23   1.04   4.84   8.07   12.11   15.32   19.06   22.65   26.30   29.92   34.71   38.99   41.64   44.76   47.51   50.39	

^{*} Nominal yield stress

Table B.20. Results of 17 Inch Bending Test: Marion 3 1b/ft - 80 ksi Post; 4 Inch Face to Face Splice in Non-critical Configuration (Grade 5 Field Bolts).

Dist to	length (	(in) in)	1.38 8.75	Face	BENDING on 3 lb/	ft - 80 k ; gr 5 bo	lts
Moment	arm (in)	Tip   Defl   (in)	Total Defl (in)	STR At G	critical AIN Gauge (/in) Calc.		ESS
floor   DL   0 0   200 200   200 400   200 600   200 800   200 1000   200 1200   200 1400   200 1600   200 1800   200 2000   200 2000   200 2200   100 2300   100 2400	1.159 1.197 1.199 1.385 1.563 1.771 1.954 2.152 2.352 2.462 2.727 2.963 3.159 3.372 3.461 3.565	2.57   2.48   2.40   2.31   2.23   2.13   2.05   1.87   1.76   1.62   1.45   1.34	0.00 0.08 0.17 0.25 0.34 0.43 0.52 0.61 0.70 0.81 0.94 1.12 1.22 1.37	0.041 0.042 0.158 0.269 0.399 0.513 0.636 0.761 0.829 0.994 1.141 1.263 1.396 1.452	0.041 0.041 0.158 0.275 0.392 0.508 0.625 0.742 0.859 0.976 1.093 1.210 1.327 1.385 1.444	1.90 1.90 10.36 18.81 27.27 35.73 44.19 52.64 61.10 69.56 78.01 86.47 94.93 99.16	1.23   1.27   4.74   8.07   11.96   15.38   19.08   22.82   24.87   29.83   34.24   37.90   41.88   43.55   45.49

^{*} Nominal yield stress

Table B.21. Results of 17 Inch Bending Test: Marion 4 lb/ft - 80 ksi Post; 4 Inch Back to Back Splice in Critical Configuration (Grade 5 Field Bolts).

		C-li	1	d \	, 00		BENDING	TEST	
		Dist to	length ( bolt A gauge ( arm (in)	(in) in)	1.56 13.19	Back	to back	ft - 80 k ; gr 5 bo ientation	lts
	 			~~~~		STR	AIN	l STR	ESS
	LC	AD			Total	I At G	auge	(ks	i)
	(1	.bs)	Ch.#1	Read	Def1	•	/in)	1	Obs @
	App1	Total	•	(in)	(in)	•	Calc.	Base	Gauge
		floor	1.259]					
		DL	1.302			0.034	0.034	1.91	1.02
	0	0		-1.01	0.00	0.036	0.034	1.91	1.08
	200	200	1.418	-1.06	0.05	0.106	0.066	7.99	3.19
	200	400	1.547	-1.10	0.09	0.187	0.097	14.06	5.60
	200	600		-1.14	0.13	0.256	0.129	20.14	7.67
ļ	200	800		-1.18	0.18	0.328	0.160	26.22	9.84
-	200	1000	1.898	1	0.22	0.405	0.192	32.29	12.16
-	200	1200		-1.27	0.26	0.480	0.224	38.37	14.40
1	200	1400		-1.32	0.31	0.559	0.255	44.45	16.78
-	200	1600		-1.37	0.36	0.638	0.287	50.53	19.13
	200	1800		-1.44	0.43	0.710	0.319	56.60	21.30
	200	2000	2.515	-1.57	0.56	0.790	0.279	62.68	23.69
	21	2021		l				63.32	

^{*} Nominal yield stress

Table B.22. Results of 17 Inch Bending Test: Marion 4 lb/ft - 80 ksi Post; 4 Inch Back to Back Splice in Critical Configuration (Grade 9 Field Bolts).

1						BENDING	TEST		
		length (
		bolt A			MARION 4 lb/ft - 80 ksi *				
		gauge (gr 9 bo		
1	moment	arm (in)	• • • • • •	16.56	. Cri	tical or	ientation	L	
1						e o o o o o o o o o o o		700	
1 TC)AD			Total	1	AIN		ESS	
	(1bs) Ch.#1			Defl	•	auge	(ks	-	
Appl		•	Read (in)	(in)	l (uin l Obs.	/in) Calc.	l Base	Obs @	
			(111)	(TII)	VUS.	ualc.	l base	Gauge	
	floor	1.259	1		1				
İ	DL	1.287	İ		0.034	0.034	1.91	1.02	
j 0	0	1.297	-1.01	0.00	0.040	0.034	1.91	1.21	
200	200	1.422	j-1.06	0.05	0.118	0.066	7.99	3.54	
200	400	1.536	-1.10	0.10	0.189	0.097	14.06	5.67	
200	600	1.650	-1.15	0.14	0.260	0.129	20.14	7.81	
200	800		-1.19	0.18	0.335	0.160	26.22	10.05	
200	1000	1.898	-1.23	0.23	0.415	0.192	32.29	12.44	
200	1200	2.009	-1.28	0.27	0.484	0.224	38.37	14.52	
200	1400	2.126	-1.32	0.31	0.557	0.255	44.45	16.70	
200	1600	2.261	1-1.37	0.36	0.641	0.287	50.53	19.23	
200	1800	2.387	-1.41	0.41	0.719	0.319	56.60	21.58	
200	2000	2.507	-1.46	0.45	0.794	0.350	62.68	23.82	
1 200	2200 2400	2.635	-1.52	0.51	0.874	0.382	68.76	26.22	
1 200	2600 I	2.765	-1.58	0.58	0.955	0.414	74.83	28.65	
1 100	2700	2.890 2.939	-1.68 -1.75	0.67	1.033	0.445	80.91	30.98	
1 30	2730	2.939	[-1./3	0.74	1.063	0.461	83.95	31.90	
1 30	2/30		l	l		ļ	84.86	İ	

^{*} Nominal yield stress

Table B.23. Results of 17 Inch Bending Test: Marion 4 lb/ft - 80 ksi Post; 4 Inch Nested Splice in Critical Configuration (Grade 9 Field Bolts).

Dist to	length () bolt A gauge () arm (in)	(in) in)	1.63 9.31	N	ested; g	TEST ft - 80 k r 9 bolts ientation	į
LOAD (lbs)	 Ch.#1 (mV)	 Read (in)	Total Defl (in)	At G	AIN auge /in) Calc.	STR (ks Base	ESS i) Obs @ Gauge
floor DL 0	-0.343 -0.388 -0.392 -0.517 -0.632 -0.751 -0.876 -1.004 -1.128 -1.260 -1.396 -1.503 -1.636 -1.764 -1.888 -2.020	 -0.10 -0.14 -0.18 -0.23 -0.27 -0.32 -0.37 -0.42 -0.47 -0.52 -0.57 -0.63 -0.70	0.00 0.04 0.09 0.13 0.18 0.23 0.27 0.32 0.37 0.42 0.47 0.53 0.60 0.67	0.038 0.040 0.118 0.190 0.264 0.342 0.422 0.499 0.581 0.666 0.733 0.816 0.895 0.973 1.055	0.038 0.038 0.107 0.175 0.244 0.313 0.382 0.450 0.519 0.588 0.657 0.725 0.794 0.863 0.932	1.91 1.91 8.01 14.11 20.22 26.32 32.42 38.53 44.63 50.73 56.83 62.94 69.04 75.14 81.24 86.98	1.14 1.21 3.55 5.70 7.93 10.26 12.65 14.97 17.44 19.98 21.98 24.47 26.86 29.18 31.64

^{*} Nominal yield stress

Table B.24. Results of 17 Inch Bending Test: Marion 4 lb/ft - 80 ksi Post; 4 Inch Face to Face Splice in Critical Configuration (Grade 8 Field Bolts).

					~~~~~		~		
 	Splice	length (in)	4 00		BENDING	TEST		
	Dist to	bolt A gauge (arm (in)	(in) . in)	. 1.56 . 9.13	MARION 4 lb/ft - 80 ksi * Face to face; gr 8 bolts Critical orientation				
(1	AD bs)	Ch.#1	Tip Defl (in)	Total Defl (in)	At G	AIN auge /in) Calc.	STR (ks Base	ESS i) Obs @ Gauge	
 0 200 200 200 200 200 200 200 200 200 40 44	floor DL 0 200 400 600 1200 1400 1600 1800 2200 2240 2284 2284	0.744 0.612 0.489 0.367 0.241 0.109	-1.36 -1.42 -1.48 -1.53 -1.59 -1.65 -1.70 -1.76 -1.82 -1.89 -1.89 -1.95	0.00 0.07 0.12 0.17 0.23 0.29 0.35 0.40 0.46 0.53 0.60 0.69 0.78	0.038 0.049 0.126 0.201 0.274 0.350 0.432 0.508 0.584 0.663 0.745 0.827 0.905 0.921	0.038 0.038 0.108 0.178 0.247 0.317 0.387 0.457 0.527 0.596 0.666 0.736 0.806 0.820	1.91 1.91 7.99 14.06 20.14 26.22 32.29 38.37 44.45 50.53 56.60 62.68 68.76 69.97 71.31	1.14 1.46 3.79 6.04 8.22 10.49 12.95 15.25 17.53 19.89 22.36 24.82 27.16 27.63	

^{*} Nominal yield stress

Table B.25. Results of 17 Inch Bending Test: Marion 4 lb/ft - 80 ksi Post; 4 Inch Back to Back Splice in Non-critical Configuration (Grade 5 Field Bolts).

 	•	length (•		MΛD	BENDING		ai v
1		gauge (:				to back		
		arm (in)	-			critical	_	
İ								
						RAIN		ESS
,)AD	634	 Read	Total	•	Gauge	(ks	•
	(lbs) Ch.#1 Appl Total (mV)					n/in)	_	Obs @
AbbT	Total	(mV)	(in)	(in)	Ubs.	Calc.	Base	Gauge
 	floor	1.272						
1	DL	1.139	! !		0.034	0.034	l 1.91	1.02
. 0	0	1.145	! 1.19	0.00	0.030	0.034	1.91	0.91
200	200	1.027	1.14	0.05	0.104	0.066	8.01	3.11
200	400	0.905	1.10	0.09	0.180	0.098	14.11	5.39
200	600	0.770	1.06	0.13	0.264	0.131	20.22	7.92
200	800	0.649	1.01	0.17	0.339	0.163	26.32	10.18
200	1000	0.521	0.97	0.22	0.419	0.195	32.42	12.57
200	1200	0.385	0.93	0.26	0.504	0.228	38.53	15.11
200	1400	0.269	0.88	0.31	0.576	0.260	44.63	17.28
200	1600	0.140	0.83	0.35	0.656	0.292	50.73	19.69
200	1800	0.012	0.79	0.40	0.736	0.325	56.83	22.09
200	2000	-0.126	0.74	0.45	0.822	0.357	62.94	24.67
200	2200	-0.254	0.68	0.50	0.902	0.389		27.06
200	2400	-0.380	0.62	0.56	0.980	0.421	75.14	29.41
200	2600	-0.510 -0.579	0.55	0.64 0.71	1.061	0.454	81.24	31.84 33.13
	2700 2759	-0.5/9	U.48	0.71	1.104	0.470	84.30	33.13
59	2759	ł	1				86.10	

^{*} Nominal yield stress

Table B.26. Results of 17 Inch Bending Test: Marion 4 lb/ft - 80 ksi Post; 4 Inch Back to Back Splice in Non-critical Configuration (Grade 9 Field Bolts).

1	Splice	length (:	in)	4.00		BENDING	TEST	
	Dist to	bolt A	(in)	1.63	MAR]	ON 4 1b/	ft - 80 k	si *
1	Dist to	gauge (:	in)	13.19		•	; gr 9 bo	
	Moment	arm (in)		16.63			orientat	
1							****	
****					STF	RAIN	STR	ESS.
•	AD		1	Total	At 0	Sauge	(ks	i)
•	(lbs) Ch.#1		Read	${\tt Defl}$	(uir	ı/in)	1	Obs @
Appl	Total	(mV)	(in)	(în)	Obs.	Calc.	Base	Gauge
					*******			~ ~ ~ ~ ~ ~ ~
!	floor	1.272						
!	DL	1.131			0.034	0.034	1.91	1.02
0	0	1.116	1.18	0.00	0.043	0.034	1.91	1.30
200	200	0.985	1.13	0.05	0.125	0.066	8.01	3.75
200	400	0.862	1.09	0.09	0.202	0.098	14.11	6.05
200	600	0.754	1.05	0.13	0.269	0.131	20.22	8.07
200	800	0.630	1.00	0.17	0.346	0.163	26.32	10.39
200	1000	0.500	0.96	0.22	0.427	0.195	32.42	12.81
200	1200	0.386	0.91	0.26	0.498	0.228	38.53	14.95
200	1400	0.246	0.87	0.31	0.585	0.260	44.63	17.56
200	1600	0.118	0.82	0.35	0.665	0.292	50.73	19.96
200	1800	-0.009	0.77	0.40	0.744	0.325	56.83	22.33
200	2000 2200	-0.141	0.73	0.45	0.827	0.357	62.94	24.80
1 200	2400 2400	-0.261	0.68	0.50	0.901	0.389	69.04	27.04
	2400 j 2600 j	-0.401	0.62	0.56	0.989	0.421	75.14	29.66
200	2800 I	-0.527	0.56	0.62	1.067	0.454	81.24	32.01
200	3000	-0.657	0.50	0.68	1.148	0.486	87.35	34.44
200	3200	-0.795	0.42	0.76	1.234	0.518	93.45	37.02
200	3400	-0.934 -1.063	0.33	0.85	1.321	0.551	99.55	39.62
1 100	3500 I	-1.138		0.96	1.401	0.583	105.66	42.03
71	3500 3571	-T.T38	0.15	1.03	1.462	0.599	108.71	43.85
1 /1	22/T		İ				110.87	

^{*} Nominal yield stress

Table B.27. Results of 17 Inch Bending Test: Marion 4 lb/ft - 80 ksi Post; 4 Inch Nested Splice in Non-critical Configuration (Grade 5 Field Bolts).

Dist to	length (; b bolt A (; c gauge (; arm (in)	(in) in)	1.38 9.00	N	BENDING ON 4 lb/fested; gr	ft - 80 k	İ
LOAD (lbs)	 Ch.#1 (mV)	 Read (in)		At G	AIN auge /in) Calc.	STR (ks	ESS i) Obs @ Gauge
floor DL 0 0 200 200 200 400 200 600 200 800 200 1000 200 1200 200 1400 200 1600 200 1800 200 2000 200 2200 200 2400 200 2600 200 2800 117 2917	-0.339 -0.264 -0.268 -0.145 -0.033 0.089 0.248 0.338 0.473 0.603 0.722 0.853 0.982 1.102 1.355 1.355 1.480	1.51 1.45 1.40 1.35 1.30 1.25 1.20 1.15 1.10 0.99 0.94 0.88 0.82 0.74	0.00 0.06 0.11 0.16 0.21 0.26 0.31 0.36 0.41 0.46 0.51 0.57 0.63 0.69	0.038 0.036 0.112 0.182 0.258 0.357 0.413 0.497 0.578 0.652 0.734 0.814 0.889 1.047 1.047	0.038 0.038 0.108 0.177 0.246 0.316 0.385 0.454 0.523 0.593 0.662 0.731 0.801 0.870 0.939 1.008	1.91 1.91 7.92 13.93 19.94 25.95 31.96 37.97 43.99 50.00 56.01 62.02 68.03 74.04 80.05 86.06 89.58	1.14 1.07 3.36 5.46 7.74 10.71 12.39 14.92 17.35 19.57 22.02 24.43 26.67 31.40 31.40

^{*} Nominal yield stress

Table B.28. Results of 17 Inch Bending Test: Marion 4 lb/ft - 80 ksi Post; 4 Inch Nested Splice in Non-critical Configuration (Grade 9 Field Bolts).

Dist to	length (: bolt A gauge (: arm (in)	(in) in)	1.38 9.00	BENDING TEST MARION 4 lb/ft - 80 ksi * Nested; gr 9 bolts Non-critical orientation				
LOAD (lbs) Appl Total	Ch.#1	 Read (in)	Total Defl (in)	At (RAIN Gauge n/in) Calc.	STR (ks Base	ESS i) Obs @ Gauge	
floor DL 0 0 200 200 200 1200 200 1200 200 1400 200 1600 200 1800 200 2200 200 2400 200 2400 200 2600 200 3200 150 3350 150 3500 100 3700 79 3779	-0.339 -0.268 -0.275 -0.148 -0.003 0.090 0.208 0.334 0.462 0.586 0.711 0.870 0.996 1.119 1.243 1.349 1.476 1.598 1.731 1.840 1.942 1.988 2.056	1.46 1.41 1.36 1.31 1.26 1.21 1.16 1.11 1.06 1.01 0.95 0.90 0.84 0.72 0.66 0.59 0.53 0.46 0.34	0.00 0.06 0.10 0.15 0.20 0.25 0.30 0.35 0.40 0.46 0.51 0.56 0.62 0.68 0.74 0.80 0.87 0.93 1.01	0.038 0.034 0.113 0.203 0.261 0.335 0.413 0.493 0.570 0.648 0.747 0.826 0.902 0.979 1.045 1.125 1.201 1.283 1.351 1.444 1.486	0.038 0.038 0.108 0.177 0.246 0.316 0.385 0.454 0.523 0.593 0.662 0.731 0.801 0.870 0.939 1.008 1.078 1.147 1.199 1.251 1.286 1.320	1.91 1.91 7.92 13.93 19.94 25.95 31.96 37.97 43.99 50.00 56.01 62.02 68.03 74.04 80.05 86.06 92.07 98.08 102.59 107.10 110.11 113.11 115.49	1.14 1.01 3.38 6.09 7.83 10.04 12.39 14.79 17.10 19.44 22.41 24.77 27.07 29.38 31.36 33.74 32.33 34.41 35.97 37.53 38.57 39.61	

^{*} Nominal yield stress

Table B.29. Results of 17 Inch Bending Test: Marion 4 lb/ft - 80 ksi Post; 4 Inch Face to Face Splice in Non-critical Configuration (Grade 8 Field Bolts).

			*********	BENDING	TEST		
Dist	ce length (to bolt A to gauge (nt arm (in)	(in)	. 1.63 . 9.25	MARION 4 lb/ft - 80 ksi * Face to face; gr 8 bolts Non-critical orientation			
LOAD (lbs)	 Ch.#1 al (mV)	Tip Defl (in)	At G	AIN auge /in) Calc.	STR (ks Base	ESS i) Obs @ Gauge	
floo 0 200 20 200 40 200 60 200 80 200 120 200 120 200 140 200 160 200 200 200 220 200 240 200 260 200 280 200 300 100 310 75 317 26 320	L 1.258 0 1.211 0 1.015 0 1.117 0 1.220 0 1.278 0 1.389 0 1.511 0 1.635 0 1.758 0 1.877 0 2.012 0 2.136 0 2.264 0 2.402 0 2.532 0 2.532 0 2.727 5 2.767	2.85 2.80 2.75 2.70 2.64 2.59 2.54 2.48 2.43 2.37 2.31 2.25 2.19 2.12 2.04 1.95 1.84	0.00 0.05 0.10 0.15 0.21 0.26 0.31 0.37 0.42 0.48 0.54 0.60 0.66 0.73 0.81 0.90 0.94	0.038 0.009 -0.113 -0.050 0.014 0.050 0.120 0.196 0.273 0.350 0.424 0.508 0.585 0.665 0.751 0.832 0.913 0.978	0.038 0.038 0.107 0.177 0.246 0.315 0.385 0.454 0.523 0.592 0.662 0.731 0.800 0.870 0.939 1.008 1.078 1.112 1.138	1.91 1.91 8.01 14.11 20.22 26.32 32.42 38.53 44.63 50.73 56.83 62.94 69.04 75.14 81.24 87.35 93.45 96.50 98.79 99.58	1.14 0.26 -3.40 -1.50 0.43 1.51 3.59 5.87 8.19 10.49 12.71 15.23 17.55 19.94 22.52 24.95 27.38 28.60 29.35

^{*} Nominal yield stress

⁻ Bolt did not break - post tip translated 18 in laterally

APPENDIX C

FINAL 71 BENDING TESTS

FIELD BOLT SUMMARY TABLES

Franklin 3 & 4 lb/ft Posts - 60 ksi Nominal Yield Stress
Marion 3 & 4 lb/ft Posts - 80 ksi Nominal Yield Stress

Back to Back and Nested Splices
Critical Configuration

APPENDIX C

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APPENDIX C

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Table C.1. Results of 71 Inch Bending Test: Franklin 3 lb/ft - 60 ksi Post; 3 Inch Back to Back Splice in Critical Configuration (Grade 5 Field Bolts).

 Spli	ice lens	gth (in)		3 00	BENDING TEST				
		t A (in)		FRAN	KLIN 3 1	o/ft - 60	ksi *		
Dist	to str	ain gauge	e (in)	7.56	Back	to back	gr 5 bo	lts	
Mome	ent arm	(in)		71.38	Cr	itical or	rientatio	n	
İ					omn				
1 TO	DAD	. 	Tip	Total		AIN auge	l (ks	ESS	
	lbs)	Ch.#1	Defl	Defl		/auge i/in)	(KS	Obs@	
Appl	•		(in)	(in)		Calc.	Base	Gauge	
								~ ~ ~ ~ ~ ~	
	floor	0.317						į	
	tight	0.333							
	DL	0.456	0.00	0.00	-0.053	-0.053	1.93	-1.59	
1 32	60 92	0.986	0.94	0.94	-0.383	-0.368	12.50	-11.50	
1 32	124	1.286 1.559	0.51	1.45 1.96	-0.570 -0.740	-0.536 -0.704	18.14 23.78	-17.10 -22.21	
1 32	156	1.843	0.51	2.50	-0.740		29.42	-22.21	
32	188	2.119	0.54	3.04	1 -1.089	-1.040	35.06	-32.67	
32	220	2.389	0.55	3.59	-1.257	-1.208	40.70	-37.72	
32	252	2.638	0.52	4.11	-1.412	-1.376	46.34	-42.37	
32	284	2.883	0.54	4.65	-1.565	-1.544	51.98	-46.95	
32	316	3.141	0.60	5.24	-1.726	-1.712	57.62	-51.78	
32	348	3.369	0.62	5.86	-1.868	-1.880	63.26	-56.04	
32	380 396	3.589 3.608	0.71	6.57 6.98	-2.005	-2.048	68.90	-60.15	
1 16	412	3.711	0.42	7.44	-2.017 -2.081	-2.132 -2.216	71.72 74.53	-60.50 -62.43	
1 16	428	3.796	0.59	8.03	-2.134	-2.300	77.35	-64.02	
•		•					,		

^{*} Nominal yield stress

Table C.2. Results of 71 Inch Bending Test: Franklin 3 1b/ft - 60 ksi Post; 3 Inch Nested Splice in Critical Configuration (Grade 5 Field Bolts).

	Dist	to bol	gth (in) Lt A (in)		1.63		BENDING KLIN 3 11	o/ft - 60	
			cain gauge (in)				lested; gr itical or		
 - 	LC)AD		 Tip	Total		AIN	STR (ks	ESS
Ì	(]	.bs)	Ch.#1	Defl	Defl		/in)	,	Obs @
ļΑ	ppl	Total	(mV)	(in)	(in)		Calc.	Base	Gauge
-	60	floor tight DL	0.249 0.415 0.380 -0.158	 0.00 1.35	0.00	0.052	0.052	1.93 12.53	1.55 11.61
	32	92	-0.445	0.60	1.95	0.566	0.536	18.18	16.97
ı	32	124	-0.710	0.53	2.48	0.731	0.704	23.84	21.93
	32	156	-1.004	0.62	3.10	0.731	0.704	29.49	27.42
1	32	188	-1.265	0.58	3.67	1.077	1.041	35.14	32.30
i	32	220	-1.539	0.62	4.29	1.247	1.209	40.80	37.42
i	32	252	-1.809	0.63	4.91	1.416	1.377	46.45	42.47
i	32	284	-2.094	0.71	5.62	1.593	1.545	52.11	47.79
İ	32	316	-2.399	0.92	6.54	1.783	1.713	57.76	53.50
İ	16	332	-2.540	0.48	7.01	1.871	1.798	60.59	56.13
İ	16	348	-2.699	0.58	7.59	1.970	1.882	63.41	59.10
1	16	364	-2.829	0.55	8.13	2.051	1.966	66.24	61.53
	16	380	-2.963	0.81	8.94	2.135	2.050	69.07	64.04

^{*} Nominal yield stress

Table C.3. Results of 71 Inch Bending Test: Franklin 4 lb/ft - 60 ksi Post; 4 Inch Back to Back Splice in Critical Configuration (Grade 5 Field Bolts).

						-	
				BENDING	TEST		
			ር D A N	'ሆ፣ TN /. 1'	h/f+ 60	lead of	
						•	
	(***
				STR	AIN	l STR	ESS
DAD		Tip	Total	At G	auge	(ks	i)
lbs)	Ch.#1	Defl	Defl	(uin	/in)	İ	Obs @
Total	(mV)	(in)	(in)	Obs.	Calc.	Base	Gauge

		<u> </u>		0 000		ļ	
-	l .		0.00			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 00
		, .					
		•		1		1	-7.63
				,		•	-11.21
				l e		,	-14.93
				I.		•	-18.62 -22.07
						•	-25.93
,		•				•	-29.63
	1						-33.20
		•		•			-37.16
,							-40.45
380	1.291	0.42					-44.19
412	1.500	0.51		-1.603		•	-48.09
428		0.28	5.67	, .	-1.622	56.04	
	t to bold to strent arm OAD Lbs) Total Floor tight 00 124 156 188 220 252 284 316 348 380 412	t to bolt A (in) t to strain gauge ent arm (in) DAD Lbs) Ch.#1 Total (mV) floor -1.412 tight -1.410 DL -1.015 60 -0.665 92 -0.473 124 -0.274 156 -0.077 188 0.108 220 0.314 252 0.512 284 0.703 316 0.915 348 1.091 380 1.291 412 1.500	t to bolt A (in) t to strain gauge (in) ent arm (in) DAD Tip Lbs) Ch.#1 Defl Total (mV) (in)	Lbs) Ch.#1 Def1 Def1 Total (mV) (in) (in) floor -1.412 tight -1.410 DL -1.015 0.00 0.00 60 -0.665 0.71 0.71 92 -0.473 0.41 1.12 124 -0.274 0.41 1.53 156 -0.077 0.41 1.93 188 0.108 0.40 2.33 220 0.314 0.43 2.76 252 0.512 0.42 3.18 284 0.703 0.42 3.60 316 0.915 0.45 4.05 348 1.091 0.42 4.47 380 1.291 0.42 4.89 412 1.500 0.51 5.39	to bolt A (in) 1.44 FRAN to strain gauge (in) 9.25 Back ent arm (in)	ice length (in) 4.00 t to bolt A (in) 1.44 t to strain gauge (in) 9.25 ent arm (in)	Eto bolt A (in) 1.44 Eto strain gauge (in) 9.25 Ent arm (in) 71.50 Critical orientation CAD

^{*} Nominal yield stress

Table C.4. Results of 71 Inch Bending Test: Franklin 4 lb/ft - 60 ksi Post; 4 Inch Nested Splice in Critical Configuration (Grade 5 Field Bolts).

) ksi *
5
on
RESS
si)
Obs @
Gauge
1
1.10
7.66
11.20
14.65
18.19
21.78
25.53
28.92
32.47
36.37 40.19
43.85
48.13
52.92
55.40
E

^{*} Nominal yield stress

Table C.5. Results of 71 Inch Bending Test: Marion 3 1b/ft - 80 ksi Post; 3 Inch Back to Back Splice in Critical Configuration (Grade 5 Field Bolts).

	BENDING TEST											
		gth (in)						Ì				
		lt A (in)					ft - 80 k					
		rain gauge			Back	to back	; gr 5 bo	lts				
Mome	ent arm	(in)	· · · · · · ·	72.38	Cr	itical o	rientatio	on [
.												
						AIN		ESS				
,	DAD	633	Tip	Total		auge	(ks	•				
	bs)	Ch.#1	Defl	Def1		/in)		Obs @				
Abbr	Total	(mV)	(in)	(in)	Obs.	Calc.	Base	Gauge				
	£1	 **										
!	floor	**					ļ	l				
1	tight DL		0.00	0 00	0.040	0.010	!					
1 60	60 I	8.242 7.848	0.00	0.00	0.042	0.042	1.90	1.26				
32	92	7.661	0.74	0.74	0.287	0.298	12.46	8.62				
1 32	124	7.471	0.39	1.11	0.404	0.435	18.10	12.12				
32	156	7.266	0.39	1.50 1.91	0.522 0.650	0.572	23.73	15.67				
32	188	7.268	0.41	2.34	0.630	0.709 0.845	29.37	19.50				
32	220	6.878	0.45	2.79	0.773	0.843	35.00	23.20				
1 32	252	6.653	0.40	3.34	1.032		40.64	26.75				
32	284	6.446	0.50	3.84	1.161	1.119 1.256	46.27	30.96				
32	316	6.252	0.50	4.34	1.282	1.393	51.91	34.83				
32	348	6.052	0.67	5.01	1.406	1.529	57.54 63.18	38.45				
16	364	5.980	0.66	5.66	1.451	1.529	1 66.00	42.19				
		J. 200	0.00	3.00	4.471	T.730	1 00.00	43.54				

^{*} Nominal yield stress

^{**} Strain gauge malfunction - data omitted

Table C.6. Results of 71 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 3 Inch Back to Back Splice in Critical Configuration (Grade 9 Field Bolts).

Splice leng Dist to bol Dist to str Moment arm	t A (in) ain gauge	 e (in)	BENDING TEST MARION 3 lb/ft - 80 ksi * Back to back; gr 9 bolts Critical orientation				
LOAD (lbs) Appl Total	Total Defl (in)	At (AIN Gauge n/in) Calc.	STR (ks Base	ESS i) Obs @ Gauge		
floor tight DL 60 60 32 92 32 124 32 156 32 188 32 220 32 252 32 284 32 316 32 348 32 348 32 348 32 348 32 442 16 460 16 476 16 492	2.253 2.233 2.372 2.801 3.017 3.250 3.474 3.697 3.917 4.125 4.125 4.318 4.709 4.935 5.140 5.348 5.496 5.617 5.739	0.00 0.82 0.41 0.47 0.51 0.50 0.52 0.56 0.76 0.70 0.79 0.62 0.46	1.69 2.16 2.67 3.17 3.69 4.20 4.75 5.35 6.10 6.80 7.59 8.21 8.67	0.042 0.309 0.443 0.589 0.728 0.867 1.004 1.134 1.254 1.154 1.498 1.639 1.766 1.896 1.988 2.063	0.695 0.830 0.964	1.90 12.32 17.88 23.43 28.99 34.55 40.11 45.66 51.22 56.78 62.34 67.89 73.45 79.01 81.79 84.57 87.35	1.25 9.27 13.30 17.66 21.85 26.01 30.13 34.01 37.62 34.63 44.93 49.16 52.99 56.87 59.64 61.90 64.18

^{*} Nominal yield stress

Table C.7. Results of 71 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 3 Inch Nested Splice in Critical Configuration (Grade 5 Field Bolts).

** ** ** **								
 Sp1	ice len	gth (in)		. 3.00		BENDING	TEST	
Dis	t to bo	lt A (in) rain gaug				ft - 80 k	si *	
Mom	ent arm	(in)	• • • • • • • • • • • • • • • • • • • •	7.75 72.06		ested; gr	rientatio	n
	~~=~		*****	*****	STR	RAIN	i STR	 ESS
L	OAD	1	Tip	Total	At C	auge	(ks	
(lbs)	Ch.#1	Defl	Def1	-	ı/in)	1	Obs @
Appl	Total	(WV)	(in)	(in)	•	Calc.	Base	Gauge
	CT							
ļ	floor	4.797	!					1
ļ	tight	4.112	1 0 00	0.00				1
1 60	DL	** **	0.00	0.00	**	0.042	1.90	**
1 32	60 92	1	0.90	0.90	**	0.298	12.42	**
1 32	124	4.952	0.50	1.39	0.434	0.434	18.03	13.02
1 32	,	5.188	0.51	1.90	0.581	0.571	23.64	17.43
1 32	156 188	5.415	0.50	2.40	0.722	0.707	29.25	21.67
1 32		5.634	0.49	2.89	0.859	0.843	34.86	25.77
1 32	220	5.866	0.54	3.43	1.003	0.980	40.47	30.10
1 48	252	6.078	0.52	3.95	1.136	1.116	46.08	34.07
1 16	300	6.415	0.93	4.88	1.346	1.321	54.50	40.37
1 16	316	6.525	0.33	5.21	1.414	1.389	57.30	42.42
1 16	332	6.647	0.48	5.69	1.490	1.457	60.11	44.70
1	348	6.756	0.50	6.19	1.558	1.525	62.91	46.74
16	364	6.878	0.59	6.78	1.634	1.593	65.72	49.02

^{*} Nominal yield stress

^{**} Strain gauge malfunction - data omitted

Table C.8. Results of 71 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 3 Inch Nested Splice in Critical Configuration (Grade 9 Field Bolts).

 Spli	ao lone	gth (in)		2 00	me ton man met man nya nya nya nya	BENDING	TEST		
Dist	to bol	th (in) tain gauge (in)	 e (in)	1.44 10.06	MARION 3 lb/ft - 80 ksi * Nested; gr 9 bolts Critical orientation				
	AD bs) Total	Ch.#1 (mV)	Tip Defl (in)	Total Defl (in)	At (RAIN Gauge n/in) Calc.	STR (ks Base	ESS i) Obs @ Gauge	
60 32 32 32 32 32 32 32 32	floor tight 00 92 124 156 188 220 252 284 316 348 380 412	1.800 1.811 1.726 1.339 1.135 0.922 0.717 0.492 0.285 0.081 -0.107 -0.306 -0.516 -0.709 -0.837	0.00 0.92 0.51 0.52 0.52 0.57 0.53 0.53 0.53 0.59 0.80 0.80	0.00 0.92 1.43 1.95 2.47 3.03 3.56 4.09 4.61 5.20 6.00 6.80 7.39	0.039 0.280 0.408 0.540 0.668 0.808 0.937 1.064 1.181 1.305 1.436 1.557	0.039 0.283 0.414 0.544 0.674 0.804 0.934 1.064 1.195 1.325 1.455 1.585	1.90 12.33 17.89 23.45 29.01 34.58 40.14 45.70 51.26 56.83 62.39 67.95 73.51	1.18 8.41 12.23 16.21 20.04 24.25 28.12 31.93 35.44 39.16 43.09 46.70 49.09	
32 16 16 16	444 460 476 492	-1.006 -1.129 -1.200 -1.368	0.92 0.60 0.48 1.13	8.31 8.91 9.38 10.51	1.742 1.818 1.862 1.967	1.845 1.910 1.976 2.041	79.07 81.86 84.64 87.42	52.25 54.55 55.87 59.01	

^{*} Nominal yield stress

Table C.9. Results of 71 Inch Bending Test: Marion 4 lb/ft - 80 ksi Post; 4 Inch Back to Back Splice in Critical Configuration (Grade 5 Field Bolts).

	olioo lon	~+h (im)		4 00		BENDING	TEST	
		gth (in) lt A (in)			MAR]	ON 4 1b/	ft - 80 k	si *
-		rain gauge				to back		
		(in)				itical o		
İ		, ,						
					STE	RAIN	STR	ESS
	LOAD		Tip	Total	At (Gauge	(ks	i)
1	(lbs)	Ch.#1	Defl	\mathtt{Defl}	(uir	ı/in)		0bs @
App	ol Total	(mV)	(in)	(in)	0bs.	Calc.	Base	Gauge
			~ ~ ~ ~					
	floor							!
1	tight	-0.426		0.00	!			!
1 ,	DL	-0.319	0.00	0.00	0.038	0.038	1.91	1.14
,	50 60 32 92	-0.022	0.53	0.53	0.223	0.214	9.75	6.69
•		0.156	0.32	0.85	0.334		13.94	10.02
		0.299	0.25	1.10	0.423	0.402	18.12	12.69
	32 156 32 188	0.459 0.635	0.29	1.38	0.523	0.495	22.30	15.68
	32 220	0.633	0.31		0.632	0.589	26.49	18.97
	32 252	0.793	0.29	1.98	0.731	0.683	30.67	21.93
,	32 284	1.125	0.31	2.29 2.58	0.838	0.776	34.85	25.14
1	32 316	1.295	0.30	2.38	0.938 1 1.044	0.870 0.964	39.04	28.13
,	32 348	1.468	0.31	3.22	1.151		43.22	31.31
, -	32 380	1.633	0.34		1.254	$1.057 \\ 1.151$	47.40 51.59	34.54 37.63
•	32 412	1.801	0.34		1.359	1.245	55.77	37.63 40.77
	.6 428	1.001	0.34	4.22	1 1.339	1.292	1 57.79	40.//
' "		1	0.54	-r . 4 . 4 .	I	4.676	37.73	1

^{*} Nominal yield stress

Table C.10. Results of 71 Inch Bending Test: Marion 4 lb/ft - 80 ksi Post; 4 Inch Back to Back Splice in Critical Configuration (Grade 9 Field Bolts).

 Splice leng	th (in)	BENDING	TEST	**************************************			
Dist to bol	t A (in)		1.44	MARION 4 lb/ft - 80 ksi * Back to back; gr 9 bolts			
Moment arm					itical o		
	~~~~			   STR	AIN	l STR	 ESS
Appl. Total		Tip	Total	At G	auge	(ks	
load Load	Ch.#1	Defl	Defl	•	ı/in)	i `	Obs @
(lbs) (lbs)	(mV)	(in)	(in)	Obs.	Calc.	Base	Gauge
floor	-0.430	 	***************************************		***		
tight	-0.426	İ					i
DL	-0.337	0.00	0.00	0.038	0.038	1.91	1.15
60 60	-0.028	0.56	0.56	0.231	0.214	9.75	6.93
32 92	0.132	0.29	0.85	0.331	0.308	13.94	9.92
32 124	0.296	0.30	1.15	0.433	0.402	18.12	12.99
32 156	0.458	0.30	1.45	0.534	0.495	22.30	16.01
32 188	0.628	0.32	1.77	0.640	0.589	26.49	19.19
32 220	0.797	0.31	2.08	0.745	0.683	30.67	22.35
32 252	0.960	0.31	2.38	0.847	0.776	34.85	25.40
32 284		0.30	2.68	0.946	0.870	39.04	28.39
32 316	1.279	0.30	2.98	1.045	0.964	43.22	31.36
32 348	1.444	0.32	3.29	1.148	1.057	47.40	34.44
32 380	1.604	0.31	3.60	1.248	1.151	51.59	37.43
32 412	1.767	0.33	3.93	1.349	1.245	55.77	40.48
32 444	1.926	0.34	4.27	1.448	1.339	59.95	43.45
32 476	2.071	0.33	4.59	1.539	1.432	64.14	46.16
32 508	2.244	0.40	4.99	1.647	1.526	68.32	49.40
32 540	2.398	0.38	5.37	1.743	1.620	72.50	52.28
32 572	2.568	0.49	5.85	1.848	1.713	76.69	55.45
16 588	2.635	0.24	6.09	1.890	1.760	78.78	56.71

^{*} Nominal yield stress

Table C.11. Results of 71 Inch Bending Test: Marion 4 lb/ft - 80 ksi Post; 4 Inch Nested Splice in Critical Configuration (Grade 5 Field Bolts).

   Splice leng   Dist to bol   Dist to str	lt A (in)		1.75		BENDING ON 4 1b/i sted; gr	Et - 80 k	si *
Moment arm				Cr	itical or	cientatio	n i
LOAD   Tip Total     (lbs)   Ch.#1   Defl Defl     Appl Total   (mV)   (in) (in)				At G	AIN auge /in) Calc.	STR (ks	ESS   i)   Obs @   Gauge
floor tight DL 60 60 32 92 32 124 32 156 32 188 32 220 32 252 32 284 32 316 32 348 32 380 32 412 32 444 32 476	0.356 0.384 0.305 -0.015 -0.164 -0.326 -0.488 -0.653 -0.818 -0.973 -1.128 -1.283 -1.283 -1.375 -1.596 -1.745 -1.903 -2.054	0.00   0.61   0.29   0.32   0.33   0.33   0.31   0.31   0.41   0.23   0.32   0.32	0.00 0.61 0.90 1.21 1.54 1.87 2.19 2.50 2.81 3.12 3.53 3.76 4.07 4.39 4.77	0.038   0.237   0.330   0.431   0.532   0.635   0.738   0.834   0.931   1.027   1.085   1.222   1.315   1.414   1.508	0.038 0.214 0.308 0.402 0.496 0.590 0.684 0.778 0.871 0.965 1.059 1.153 1.247 1.341 1.435	1.91 9.81 14.02 18.23 22.45 26.66 30.87 35.08 39.30 43.51 47.72 51.94 56.15 60.36 64.57	1.14   7.12   9.91   12.94   15.96   19.05   22.13   25.03   27.93   30.82   32.54   36.67   39.46   42.41   45.24

^{*} Nominal yield stress

Table C.12. Results of 71 Inch Bending Test: Marion 4 lb/ft - 80 ksi Post; 4 Inch Nested Splice in Critical Configuration (Grade 9 Field Bolts).

			9 00 00 40 KA KA KA KA KA KA	BENDING	TEST		
Splice lengt   Dist to bold   Dist to strate   Moment arm	t A (in) ain gauge	 e (in)	1.75 9.25	MARION 4 lb/ft - 80 ksi * Nested; gr 9 bolts Critical orientation			j
*****		~ ~ ~ ~ ~ ~		STR	AIN	STR	ESS
Appl. Total		Tip	Total	At G	auge	(ks	i)
load Load	Ch.#1	Defl	Defl	(uin	/in)		Obs @
(lbs) (lbs)	(mV)	(in)	(in)	Obs.	Calc.	Base	Gauge
floor	0.356	 					
tight	0.384					! 	, 
j DL j	0.304	0.00	0.00	0.038	0.038	1.91	1.14
60 60	-0.013	0.62	0.62	0.236	0.214	9.81	7.07
32 92	-0.165	0.30	0.91	0.330	0.308	14.02	9.91
32 124	-0.330		1.24	0.433	0.402	18.23	12.99
32   156	-0.491	0.32	1.56	0.533	0.496	22.45	16.00
32 188	-0.652	0.32	1.88	0.634	0.590	26.66	19.01
32 220	-0.815	0.33	2.21	0.735	0.684	30.87	22.06
32 252	-0.968	0.32	2.52	0.831	0.778	35.08	24.92
32 284	-1.126	0.32	2.84	0.929	0.871		27.87
32 316	-1.287		3.18	1.029	0.965	43.51	30.88
32 348	-1.444		3.49	1.127	1.059	47.72	33.81
32 380	-1.587	0.30	3.79	1.216	1.153	51.94	36.49
32 412	-1.743	0.32	4.11	1.313	1.247	56.15	39.40
32 444	-1.891	0.32	4.43	1.406	1.341		42.17
32 476	-2.04		4.76	1.495	1.435	64.57	44.86
32 508	-2.19		5.11	1.593	1.529	68.79	47.80
32 540   32 572	-2.34	0.35	5.46	1.687	1.623	73.00	50.60
32 5/2	-2.48 -2.63	0.36	5.81	1.770	1.716	77.21	53.09
1 16 620	-2.63 -2.71	0.32	6.34 6.57	1.866 1.917	1.810	81 [.] .43	55.98
10 020	-2./I	0.23	0.5/	1.91/	1.857	03.33	57.50

^{*} Nominal yield stress

### APPENDIX D

### TORSION TESTS

#### FIELD AND CALIBRATED BOLT SUMMARY TABLES

Franklin 3 & 4 lb/ft Posts - 60 ksi Nominal Yield Stress
Marion 3 & 4 lb/ft Posts - 80 ksi Nominal Yield Stress

Back to Back and Nested Splices & Post W/O Splice

# APPENDIX D

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Table D.1. Results of Torsion Test: Franklin 3 lb/ft - 60 ksi Post; Post W/O Splice.

TO	TORSION TEST							
60								
post	length:	123 in						
Load		Theta     (deg)						
0   50   100   150   200   250   300   450   550   600   650   700   750   800   950   1000   750   500   250   000   250   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000   000	0.00   0.21   0.41   0.62   0.83   1.03   1.24   1.44   1.65   2.06   2.27   2.48   2.68   2.89   3.09   3.30   3.51   3.71   3.92   4.13   3.09   2.06   1.03   0.00	0.0   15.0   30.0   45.0   60.5   75.0   91.0   123.0   136.0   147.5   166.5   183.5   224.0   246.5   267.0   295.5   315.5   338.0   362.0   315.0   252.0   179.5   92.0						

* Nominal yield stress

Table D.2. Results of Torsion Test: Franklin 3 lb/ft - 60 ksi Post; 3 Inch Back to Back Splice (Calibrated and Grade 5 Field Bolts).

ļ	TORSION TEST										
ļ	<u> </u>										
	FI			- 60 ksi							
				r 5 bolts							
1			e length			BOLT	LOADS				
1		post.	length:	123 IN		= = = = = = = = = = = = = = = = = = =	ח של במו				
Tot	al	Applied	1			Bolt A	POTC R				
		Moment	   Theta	Ch.#1	Ch.#2	l Obs.	l Obs.				
		(k-in)	(deg)	(mV)			(kips)				
						~~~~~	(Krbs)				
loos	e			0.421	0.065	0.00	0.00				
tigh	t	İ		-1.740	-2.327	3.71	3.67				
	0	0.00	0.0	-1.710	-2.274	3.66	3.59				
5		0.21	16.5	-1.724	-2.249	3.68	3.55				
10		0.41	33.0	-1.748	-2.216	3.72	3.50				
15		0.62	50.5	-1.780	-2.181	3.78	3.45				
20		0.83	66.0	-1.818	-2.162	3.84	3.42				
25		1.03	81.5	-1.860	-2.159	3.92	3.41				
30		1.24	96.5	-1.192	-2.154	2.77	3.41				
35	, ,	1.44	111.5	-1.964	-2.149	4.09	3.40				
40		1.65	126.5	-2.024	-2.145	4.20	3.39				
45¢		1.86	139.0	-2.071	-2.165	4.28	3.42				
550	,	2.06 2.27	152.0 170.0	-2.121	-2.189	4.36	3.46				
600		2.48	190.0	-2.175 -2.199	-2.268 -2.409	4.46	3.58				
650		2.68	215.5	-2.199	-2.409	4.50 4.51	3.80				
700	•	2.89	240.5	-2.169	-2.813	4.45	4.10 4.42				
750	,	3.09	266.5	-2.092	-3.061	4.43	4.42				
800		3.30	295.0	-2.008	-3.371	4.17	4.80 5.27				
850	o i	3.51	331.0	-1.904	**	3.99	**				
900	o i	3.71	371.5	-1.832	! !	3.87					
500	o j	2.06	284.0	-1.697		3.64	 				
250	o i	1.03	221.5	-1.599	i	3.47					
1	C	0.00	125.0 j	-1.417		3.15	j				
. سیمسا		*****					. .				

^{*} Nominal yield stress

^{**} Bolt #7 not working properly - data omitted

Table D.3. Results of Torsion Test: Franklin 3 lb/ft - 60 ksi Post; 3 Inch Nested Splice (Calibrated and Grade 5 Field Bolts).

TORSION TEST										
[[.]	FRANKLIN 3 lb/ft - 60 ksi *									
	neste	ed; gr 5	bolts							
	splice	e length:	: 3 in		BOLT	LOADS				
	post 1	Length: 1	123 in			*****				
					Bolt A	Bolt B				
•	Applied	•			1					
•	Moment	Theta	Ch.#1	Ch.#2	Obs.	0bs.				
(lbs)	(k-in)	(deg)	(mV)	(mV)	(kips)	(kips)				
11		-	**	0 /2/	 **	0.00				
loose		[XX	0.434	1 777	0.00				
tight 0	l l 0.00	l l 0.0		-1.336	i.	3.04				
50	0.00	14.0	 	-1.282 -1.283	1	2.95 2.95				
100	0.21	29.5	 	-1.277	1	2.94				
150	0.41	43.5	 	-1.277	1	2.94				
200	0.83	58.4	! !	-1.290	1	2.94				
250	1.03	74.0	 	-1.294	l l	2.97				
300	1.24	89.5	1 [-1.312	1	3.00				
350	1.44	105.0	[]	-1.351] 	3.06				
400	1.65	122.5		-1.391	1	3.13				
450	1.86	137.5		-1.414		3.17				
500	2.06	149.0		-1.454		3.24				
550	2.27	169.0	<u>'</u>	-1.504	İ	3.33				
600	2.48	j 191.5	Ì	-1.566	İ	3.43				
650	2.68	214.5	ĺ	-1.628	į	3.54				
700	2.89	236.0	İ	-1.713	ĺ	3.69				
750	3.09	259.5	İ	-1.785	j	3.81				
800	3.30	285.0	ļ	-1.860		3.94				
850	3.51	309.5	1	-1.918		4.04				
900	3.71	337.0		-1.985		4.15				
950	3.92	369.0		-2.012		4.20				
500	2.06	277.0		-1.301	1	2.98				
250	1.03	213.0		-0.971	1	2.41				
0	0.00	114.0		-0.668		1.89				

^{*} Nominal yield stress

^{**} Bolt #7 not working properly - data omitted

Table D.4. Results of Torsion Test: Franklin 4 lb/ft - 60 ksi Post; Post W/O Splice.

T	TORSION TEST							
T773 A NT	 FRANKLIN 4 lb/ft *							
-	60 (ksi)	b/ft *						
	O SPLICE							
•	length:	123 in						
	Applied							
	Moment	Theta						
(TDS)	(k-in)	(deg)						

1		i 1						
ioi	0.00	0.0						
100	0.41	13.5						
200	0.83	26.5						
300	1.24	40.0						
400	1.65	53.5						
500	2.06	68.0						
600	2.48	83.0						
700	2.89	98.0						
800 900	3.30	114.0						
1 1000 1	3.71 4.13	130.5						
1 1100	4.54	142.0 161.0						
1 1200	4.95	185.0						
1300	5.36	212.5						
1400	5.78	246.5						
1500	6.19	286.0						
1600	6.60	325.0						
1700	7.01 j	360.0						
1000	4.13	298.0 j						
500	2.06	240.0						
1 0 1	0.00	158.0						

^{*} Nominal yield stress

Table D.5. Results of Torsion Test: Franklin 4 lb/ft - 60 ksi Post; 4 Inch Back to Back Splice (Calibrated and Grade 5 Field Bolts).

TORSION TEST								
3	FRANKITN	4 1h/ft	- 60 ksi	*				
		•	5 bolts					
		length:			BOLT	LOADS		
		length: 1						
					Bolt A	Bolt B		
Total	Applied							
Load	Moment	Theta	Ch.#1	Ch.#2	Obs.	Obs.		
(lbs)	(k-in)	(deg)	(mV)	(mV)	(kips)	(kips)		
loose			-0.136	0.115	0.00	0.00		
tight			-2.633	-2.719	3.56	4.35		
0	0.00	0.0	-2.569	-2.679	3.47	4.29		
100	0.41	13.5	-2.561	-2.669	3.46	4.27		
200	0.83	26.0	-2.556	-2.661	3.45	4.26		
300	1.24	37.5	-2.574	-2.656	3.48	4.25		
400	1.65	52.0	-2.639	-2.682	3.57	4.29		
500	2.06	66.0	-2.746	-2.719	3.72	4.35		
600	2.48	81.0	-2.890	-2.806	3.93	4.48		
700	2.89	97.0	-3.077	-2.944	4.19	4.70		
800	3.30	116.0	-3.227	-3.102	4.41	4.94		
900	3.71	131.5	-3.436	-3.237	4.71	5.15		
1000	4.13	146.5	-3.577	-3.349	4.91	5.32		
1100	4.54	168.5	-3.782	-3.483	5.20	5.52		
1200	4.95	201.5	-4.014	-3.764	5.53	5.95		
1300	5.36	241.5	-4.125	-3.913	5.69	6.18		
1400	5.78	270.0	-4.175	-4.104	5.76	6.48		
1500	6.19	298.0	-4.220	-4.261	5.83	6.72		
1600	6.60	335.0	-4.280	-4.397	5.91	6.93 5.13		
1000	4.13	275.5	-3.512	-3.224	1 4.82	•		
500 0	2.06	209.5 104.0	-2.712 -2.200	-2.155 -1.450	3.67 2.94	3.48		
U	0.00	1 104.0	1 -2.200	-T.470	4.74	1 2.40		

^{*} Nominal yield stress

Table D.6. Results of Torsion Test: Franklin 4 lb/ft - 60 ksi Post; 4 Inch Nested Splice (Calibrated and Grade 5 Field Bolts).

1	TORSION TEST									
						i				
	FRANKLIN	4 lb/ft	- 60 ksi	*		1				
		ed; gr 5								
		e length:			BOLT	LOADS				
	post	length: 1	l23 in							
				*******	Bolt A	Bolt B				
•	Applied	•	İ		1					
•	Moment	Theta	Ch.#1	Ch.#2	Obs.	Obs.				
(1bs)	(k-in)	(deg)	(mV)	(mV)	(kips)	(kips)				
loose]		-0.410	0.262	0.00	0.00				
tight			-3.126	-0.251	3.87	0.79				
0	0.00	0.0	-3.042	-0.257	3.75	0.80				
100	0.41	13.0	-3.044	-0.220	3.76	0.74				
200	0.83	26.5	-3.048	-0.249	3.76	0.78				
300	1.24	40.5	-3.051	-0.249	3.77	0.78				
400	1.65	54.0	-3.059	-0.291	3.78	0.85				
500	2.06	68.5	-3.073	-0.362	3.80	0.96				
600	2.48	83.0	-3.089	-0.441	3.82	1.08				
700	2.89	98.0	-3.114	-0.550	3.86	1.25				
800	3.30	116.5	-3.149	-0.690	3.91	1.46				
900	3.71	132.5	-3.181	-0.820	3.95	1.66				
1000	4.13	144.0	-3.203	-0.925	3.98	1.82				
1100	4.54	164.5	-3.249	-1.087	4.05	2.07				
1200	4.95	192.0	-3.313	-1.286	4.14	2.38				
1300	5.36	223.5	-3.370	-1.507	4.22	2.72				
1400	5.78	258.0	-3.425	-1.765	4.30	3.11				
1400	5.78	286.5	-4.954	**	6.48	**				
1000	4.13	242.5	-3.962	**	5.07	**				
500	2.06	175.0	-2.611	**	3.14	**				
0	0.00	86.0	-0.685	**	0.39	**				

^{*} Nominal yield stress

^{**} bolt #8 breaks at 3.11 kips; probably due to fatigue since Pu = 12 kips

Table D.7. Results of Torsion Test: Marion 3 lb/ft - 80 ksi Post; Post W/O Splice.

	TORSION TEST							
	MARION 3 lb/ft 80 (ksi) * NO SPLICE post length: 123 in							
Load	Total Applied Load Moment (1bs) (k-in)							
0 50 100 150 200 250 300 350 400 450 500 650 700 750 800 950 900 950 1000 1050 1100 1200 500	0.41	100.0 114.0 128.5 138.0 148.0 161.0 177.0 189.0 204.5 219.5 234.5 251.0 269.0 288.5 306.0 331.0 380.0 222.0						

^{*} Nominal yield stress

Table D.8. Results of Torsion Test: Marion 3 1b/ft - 80 ksi Post; 3 Inch Back to Back Splice (Calibrated and Grade 5 Field Bolts).

-		TO	RSION TE	5T	***********	୩୯୬ ପ୍ରଥନ୍ତ୍ର	<i>ଉ</i> ପ୍ତର୍ଶ କଥା କଥା କଥା କଥା କଥା କଥା କଥା କଥା କଥା କଥା								
ļ															
1	MARION 3 lb/ft - 80 ksi *														
	back to back; gr 5 bolts splice length: 3 in BOLT LOADS														
			BOLT	LOADS											
1	post length: 123 in														
1	Total	Applied	~ ~ ~ ~ ~ ~ ~ . 1	,		Bolt A	ROTE R								
1		Appiled Moment	 Theta	 Ch.#1	Ch.#2	 0h =	1 05								
1		(k-in)	(deg)	(mV)	(mV)	Obs.	Obs.								
1	(100)	(~	(deg)	(MV)	(mv)	(kips)	(kips)								
1	loose	i İ	! !	-0.308	0.097	0.00	0.00								
i	tight		! 	-2.034	-1.669	2.46	0.00 2.71								
i	0	0.00	0.0	-2.101	-1.624	2.56	2.64								
İ	100	0.41	16.5	-2.097	-1.655	2.55	2.69								
ĺ	200	0.83	44.0	-2.102	-1.685	2.56	2.74								
1	300	1.24	71.5	-2.119	-1.704	2.58	2.76								
1	400	1.65	100.0	-2.144	-1.721	2.62	2.79								
	500	2.06	129.0	-2.144	-1.729	2.62	2.80								
1	600	2.48	159.0	-2.140	-1.720	2.61	2.79								
ĺ	700	2.89	203.0	-2.144	-1.707	2.62	2.77								
1	800	3.30	241.0	-2.124	-1.931	2.59	3.11								
	900	3.71	271.0	-2.124	-2.190	2.59	3.51								
	1000	4.13	305.0	-2.124	-2.449	2.59	3.91								
1	1100	4.54	345.0	-2.115	-2.674	2.58	4.25								
1	1200	4.95	383.0	-2.117	-2.813	2.58	4.47								
1	1000	4.13	356.5	-1.947	-2.373	2.34	3.79								
	500	2.06	256.0	-1.621	-1.115	1.87	1.86								
	0	0.00	78.0	-1.533	-0.270	1.75	0.56								

^{*} Nominal yield stress

Table D.9. Results of Torsion Test: Marion 3 lb/ft - 80 ksi Post; 3 Inch Nested Splice (Calibrated and Grade 5 Field Bolts).

	TOI	RSION TES	ST	ല ചാ ത ത ത ത ത ബ	***************									
	MARION 3 1b/ft - 80 ksi *													
nested; gr 5 bolts														
splice length: 3 in BOLT LOAD														
İ	post	length: 1	123 in			*****								
					Bolt A	Bolt B								
Total	Applied				İ	ĺ								
	Moment	Theta	Ch.#1	Ch.#2	Obs.	Obs.								
(1bs)	(k-in)	(deg)	(mV)	(Vm)	(kips)	(kips)								
loose			0.448	**	**	0.00								
tight			-1.571			3.47								
0	0.00	0.00	-1.455		!	3.27								
100	0.41	28.50	-1.471			3.29								
200	0.83	57.50	-1.523			3.38								
300	1.24	86.50	-1.598			3.51								
400	1.65	105.50	-1.671		1	3.64								
500	2.06	138.00	-1.736			3.75								
600	2.48	165.50	-1.806		1	3.87								
700	2.89	195.50	-1.894			4.02								
800	3.30	226.00	-2.062		1	4.31								
900	3.71	260.50	-2.293		1	4.70								
1000	4.13	296.50	-2.584			5.20								
1100	4.54	340.00	-2.937		1	5.81								
1200	4.95	384.00	-3.308			6.45								
750	3.09	304.50	-2.455			4.98								
500		260.00	-2.111			4.39								
250	•	179.00	-1.559			3.44								
0	0.00	94.00	-1.223		1	2.87								

^{*} Nominal yield stress

^{**} Bolt #7 not working properly - data omitted

Table D.10. Results of Torsion Test: Marion 4 1b/ft - 80 ksi Post; Post W/O Splice.

T	TORSION TEST												
	MARION 4 lb/ft 80 (ksi) * NO SPLICE post length: 123 in												
Load	Total Applied Load Moment 1 (lbs) (k-in)												
0	4.54 4.95 5.36	148.5											

^{*} Nominal yield stress

Table D.11. Results of Torsion Test: Marion 4 lb/ft - 80 ksi Post; 4
Inch Back to Back Splice (Calibrated and Grade 5 Field Bolts).

	TO	RSION TES	 ST											
	MARION 4 lb/ft - 80 ksi *													
	back to back; gr 5 bolts													
1	splice length: 4 in BOLT LOADS													
1	post length: 123 in													
				******	Bolt A	IBOIT B								
Total	Applied	I	ı		1	I I								
	Moment	Theta	Ch.#1	Ch.#2	Obs.	Obs.								
•	(k-in)	(deg)	(mV)		(kips)	(kips)								
loose			-0.219	0.456	0.00	i 0.00 i								
tight			-2.128	-1.674	2.72	3.27								
1 0	0.00	0.0	-2.216	-1.595	2.85	3.15								
100	0.41	10.5	-2.213	-1.602	2.84	3.16								
200	0.83	20.0	-2.215	-1.607	2.85	3.17								
300	1.24	31.0	-2.216	-1.609	2.85	3.17								
400	1.65	41.5	-2.220	-1.612	2.85	3.17								
500	2.06	51.0	-2.240	-1.613	2.88	3.18								
600	2.48	62.0	-2.228	-1.612	2.87	3.17								
700	2.89	71.5	-2.229	-1.608	2.87	3.17								
800	3.30	82.5	-2.224	-1.602	2.86	3.16								
900 900	3.71	93.5	-2.248	-1.593	2.89	3.15								
1000	3.71 4.13	109.0 122.0	-2.246	-1.560	2.89	3.09								
1 1100	4.13 4.54	134.5	-2.301	-1.561 -1.547	2.97 3.03	3.10								
1 1200	4.34 4.95	144.0	-2.344	-1.547	3.03 3.11	3.07 3.05								
1300	5.36	158.0	-2.497	-1.546	3.25	3.03 3.07								
1400	5.78	178.5	-2.653	-1.715	3.47	3.33								
1500	6.19	202.0	-2.773	-1.867	3.64	3.57								
1600	6.60	229.0	-2.857	-2.094	3.76	3.91								
1700	7.01	257.5	-2.863	-2.328	3.77	4.27								
1800	7.43	281.0	-2.862	-2.537	3.77	4.59								
1900	7.84	305.5	-2.837	-2.748	3.73	4.92								
2000	8.25	332.5	-2.818	-2.971	3.71	5.26 j								
1000	4.13	243.5	-1.879	-1.127	2.37	2.43								
500	2.06	179.0	-1.413	-0.274	1.70	1.12								
0	0.00	90.0	-1.376	0.020	1.65	0.67								

^{*} Nominal yield stress

Table D.12. Results of Torsion Test: Marion 4 lb/ft - 80 ksi Post; 4
Inch Nested Splice (Calibrated and Grade 5 Field Bolts).

20 60		ସ୍ତ୍ର ପ୍ରଥ ପ୍ରଥ ପ୍ରଥ											
1		TO	RSION TE	ST .									
i		20.					1						
i	MARION 4 lb/ft - 80 ksi *												
i	nested; gr 5 bolts												
j		splice	BOLT	LOADS									
ĺ		post											
-				Bolt A	Bolt B								
	Total	Applied		1		į	i i						
1		Moment	Theta	Ch.#1	Ch.#2	Obs.	Obs.						
	(lbs)	(k-in)	(deg)	(mV)	(mV)	(kips)	(kips)						
-					-								
•	loose	!		-0.228	0.572	0.00	0.00						
İ£	ight	!		-1.873	-1.049	2.35	2.49						
	0	0.00	0.0	-1.780	-0.929	2.21	2.30						
ļ	100	0.41	12.0	-1.750	-0.918	2.17	2.29						
	200	0.83	25.0	-1.697	-0.951	2.10	2.34						
1	300	1.24	36.5	-1.682	-0.956	2.07	2.35						
-	400	1.65	48.5	-1.665	-0.973	2.05	2.37						
-	500	2.06	61.5	-1.633	-1.007	2.00	2.42						
-	600	2.48	73.5	-1.606	-1.048	1.97	2.49						
!	700	2.89	86.5	-1.614	-1.103	1.98	2.57						
!	800	3.30	99.5	-1.555	-1.158	1.89	2.66						
ļ	900	3.71	113.0	-1.539	-1.232	1.87	2.77						
-	1000	4.13	126.0	-1.546	-1.326	1.88	2.91						
-	1100	4.54	136.0	-1.538	-1.396	1.87	3.02						
	1200	4.95	145.5	-1.543	-1.477	1.88	3.15						
	1300	5.36	160.5	-1.552	-1.599	1.89	3.33						
	1500	5.78 6.19	177.0	-1.559	-1.749	1.90	3.56						
•	1600	6.60	195.0	-1.571	-1.955	1.92	3.88						
•	1700	7.01	216.5	-1.571	-2.210	1.92	4.27						
•	1800	7.43	238.5 263.0	-1.585	-2.471	1.94	4.67						
•	1900	7.84	288.0	-1.594	-2.753	1.95	5.10						
•	2000	8.25	319.5	-1.601 -1.603	-3.029	1.96	5.53						
•	1000	4.13	220.0	-1.387	-3.338	1.96	6.00						
¦	500	2.06	158.0	-1.236	-1.974	1.65 1.44	3.91						
1	0 1	0.00	83.0	-1.072	-0.442	1.20	2.50 1.56						
!		0.00	05.0 [-1.0/2	~V.444	1.20	ן טניד						

^{*} Nominal yield stress

APPENDIX E

75" COMBINED BENDING AND TORSION TESTS (NEGLECTING AND INCLUDING WARPING STRESSES)

FIELD BOLT SUMMARY TABLES

Franklin 3 & 4 lb/ft Posts - 60 ksi Nominal Yield Stress
Marion 3 & 4 lb/ft Posts - 80 ksi Nominal Yield Stress

Back to Back and Nested Splices
Critical Configuration

APPENDIX E

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Table E.1. Results of 75 Inch Combined Bending and Torsion Test (Neglecting Warping Stresses): Franklin 3 lb/ft - 60 ksi Post; 3 Inch Back to Back Splice in Critical Configuration (Grade 5 Field Bolts).

Splice len Dist to bo Dist to st Moment arm Eccentric	olt A (in) crain gaug n (in)	e (in) .	1.50 7.88 75.38	,	BENDING TORSION TEST (Warping Neglected) FRANKLIN 3 lb/ft - 60 ksi * Back to back; gr 5 bolts Critical orientation						
LOAD (lbs) Appl Tot	LOAD Tip Tip (lbs) Ch.#1 Defl Rot				At G	AIN auge /in) Calc.	 Bending Mc/I	(ks			
0 26 26 24 50 24 74 24 98 24 122 24 146 24 170 24 194 24 218 24 242 24 266 24 290 8 298 8 306	1.003 1.238 1.457 1.671 1.878 2.080 2.276 2.472 2.646 2.813 2.976 3.095 3.146 3.249 3.124	0.00 0.60 1.18 1.83 2.47 3.12 3.76 4.43 5.13 5.84 6.70 7.65 8.81 9.81	0.0 7.5 13.0 17.5 22.0 25.0 28.0 30.0 32.5 34.5 36.0 38.0 39.0 40.0 40.5	6.30 6.25 6.14 6.01 5.84 5.71 5.56 5.46 5.31 5.19 5.10 4.96 4.90 4.83 4.79	0.052 0.198 0.335 0.468 0.597 0.723 0.845 0.967 1.076 1.180 1.281 1.355 1.355 1.374	0.052 0.195 0.327 0.460 0.592 0.724 0.856 0.989 1.121 1.253 1.384 1.516 1.647 1.691 1.735	1.94 6.74 11.17 15.61 20.04 24.47 28.90 33.32 37.74 42.17 46.58 50.99 55.40 56.86	0.00 2.80 5.34 7.83 10.24 12.61 14.91 17.17 19.36 21.51 23.62 25.68 27.70 28.37 29.03	0.00 0.00 0.00 0.00 0.00 0.01 0.01 0.01	1.94 7.75 13.32 18.86 24.35 29.80 35.21 40.59 45.92 51.22 56.48 61.71 66.90 68.63 70.35	

^{*} Nominal yield stress

Table E.2. Results of 75 Inch Combined Bending and Torsion Test (Neglecting Warping Stresses): Franklin 3 lb/ft - 60 ksi Post; 3 Inch Nested Splice in Critical Configuration (Grade 5 Field Bolts).

Dist Dist Momen	to bol to str nt arm	th (in) t A (in) tain gauge (in)	(in) .	1.50 8.25 75.50		BENDING TORSION TEST (Warping Neglected) FRANKLIN 3 lb/ft - 60 ksi * Nested; gr 5 bolts Critical orientation					
							AIN			TRESSES	1
1 -	OAD	ot- u1	Tip	Tip	Tor	•	auge	 P	(ks	•	Combined
	bs)	Ch.#1	Defl	Rot	Arm	l (uin l Obs.	/in) Calc.		Torsion	P/A	(Mohr)
Appl	Tot	(mV)	(in)	(deg)	(in)	l obs.	carc.	Mc/I	Th/J	E/15	(HOLL)
	DL	0.411	0.00	0.0	6.30	0.052	0.051	1.94	0.00	0.00	1.94
26	26	0.177	0.61	7.0	6.25	0.198	0.194	6.75	2.80	0.00	7.76
24	50	-0.042	1.17	13.5	6.13	0.334	0.326	11.19	5.34	0.00	13.33
24	74	-0.261	1.71	18.5	5.97	0.471	0.458	15.63	7.81	0.00	18.86
24	98	-0.480	2.27	23.5	5.78	0.607	0.589	20.07	10.20	0.00	24.34
24	122	-0.701	2.85	27.0	5.61	0.745	0.721	24.51	12.52	0.01	29.78
24	146	-0.920	3.41	30.5	5.43	0.881	0.853	28.94	14.77	0.01	35.15
24	170	-1.137	3.98	34.0	5.22	1.017	0.985	33.38	16.93	0.01	40.47
24	194	-1.353	4.56	36.5	5.06	1.151	1.116	37.81	19.03	0.01	45.74
24	218	-1.569	5.22	38.0	4.96	1.286	1.248	42.24	21.08	0.02	50.98
24	242	-1.785	5.90	40.0	4.83	1.420	1.379	46.67	23.08	0.02	56.17
24	266	-1.999	6.70	42.5	4.64	1.554	1.511	51.09	25.00	0.03	61.31
24	290	-2.226	7.76	43.0	4.61	1.695	1.642	55.51	26.91	0.03	66.44
8	298	-2.323	•	44.0	4.53	1.755	1.685	56.98	27.53	0.04	68.14
8	306	-2.401	8.68	44.5	4.49	1.804	1.729	•	28.15	0.04	69.84
8	314	-2.493	9.16	45.0	4.45	1.861	1.773	59.92	28.77	0.04	71.53

^{*} Nominal yield stress

Table E.3. Results of 75 Inch Combined Bending and Torsion Test (Neglecting Warping Stresses): Franklin 4 lb/ft - 60 ksi Post; 4 Inch Back to Back Splice in Critical Configuration (Grade 5 Field Bolts).

Dist Dist Mome	to bol to str nt arm	gth (in) It A (in) Sain gauge (in) Ty (in) .	······································	1.50 9.25 75.63			FRA Ba	(Warping NKLIN 4 1 ck to bac	ORSION TE Neglecte lb/ft - 6 ck; gr 5 orientat	d) 0 ksi * bolts	
1 7	OAD 1		Tip	Tip	Tor		AIN auge			TRESSES	!
•	bs)	Ch.#1	Defl	Rot	Arm	•	-	i Bending	(ks Torsion	•	 Combined
App1	Tot	(mV)	(in)	(deg)	(in)	Obs.	•	Mc/I	Th/J	P/A	(Mohr)
1 55	DL	-0.888	0.00	0.0	6.30	0.049	0.049	1.45	0.00	0.00	1.45
55	55	-0.521	•	7.5	6.25	0.278	0.272	9.07	4.38	0.00	10.84
32	87	-0.320	1.51	11.5	6.17	0.403	0.402	13.50	6.90	0.00	16.41
32	119	-0.113	2.04	15.0	6.09	0.532	0.532	17.93	9.39	0.00	21.95
32	151	0.113	2.62	18.5	5.97	0.673	0.661	22.36	11.82	0.00	27.46
32	183	0.320	3.19	21.0	5.88		0.791	26.79	14.22	0.01	32.94
32	215	0.534	3.74	23.5	5.78	0.935	0.920	31.22	16.58	0.01	38.39
32	247	0.753	4.37	26.0	5.66	1.071	1.050	35.64	18.89	0.01	43.80
32	279	0.972	4.92	27.5	5.59	1.208	1.179	40.06	21.17	0.02	49.19
32	311	1.205	5.53	29.5	5.48	1.353	1.308	44.48	23.41	0.02	54.55
32	343	1.441	6.14	31.5	5.37	1.500	1.438	48.90	25.61	0.02	59.87
32	375	1.738	7.11	33.5	5.25	1.685	1.567	53.31	27.75	0.03	65.16 j

^{*} Nominal yield stress

Table E.4. Results of 75 Inch Combined Bending and Torsion Test (Neglecting Warping Stresses): Franklin 4 lb/ft - 60 ksi Post; 4 Inch Nested Splice in Critical Configuration (Grade 5 Field Bolts).

Dist Dist Mome	to bol to str nt arm	gth (in) lt A (in) rain gauge (in) ty (in) .	e (in) .	1.50 7.06 75.56			BENDING TORSION TEST (Warping Neglected) FRANKLIN 4 lb/ft - 60 ksi * Nested; gr 5 bolts Critical orientation						
				- <i>-</i>		STR	AIN	1	BASE S	TRESSES			
	LOAD Tip Tip Tor						auge	1	(ks	•			
	bs)	Ch.#1	Defl	Rot	Arm				Torsion		Combined		
Appl	Tot	(mV)	(in)	(deg)	(in)	Obs.	Calc.	Mc/I	Th/J	P/A	(Mohr)		
	DL	0 367	0.00		6 20	0.053	0.052	1 1 /1			1 , 1		
1 55	55	0.367	0.00	0.0	6.30	0.053	0.053	1.41	0.00	0.00	1.41		
32	87	-0.058 -0.300	0.81 1.72	7.5	6.25	0.318	0.283	9.02	4.38	0.00	10.80		
1 32	119	•	•	15.5	6.07	0.469	0.416	13.45	6.86	0.00	16.33		
1 32	151	-0.306	2.19	18.0	5.99	0.472	0.550	17.88	9.31	0.00	21.84		
1 32	183	-0.530	2.66	22.0	5.84	0.612	0.684	22.30	11.69	0.00	27.31		
1 32		-0.761	3.12	24.5	5.73	0.756	0.818	26.73	14.03	0.01	32.75		
•	215	-1.002	3.61	27.5	5.59	0.906	0.951	31.15	16.31	0.01	38.14		
32	247	-1.222	4.06	29.0	5.51	1.043	1.085	35.57	18.56	0.01	43.50		
32	279	-1.467	4.53	32.0	5.34	1.196	1.218	40.00	20.74	0.01	48.82		
32	311	-1.683	5.03	33.5	5.25	1.330	1.352	44.41	22.88	0.02	54.11		
32	343	-1.927	5.57	35.5	5.13	1.482	1.485	48.83	24.98	0.02	59.36		
32	375	-2.157	6.21	38.0	4.96	1.626	1.619	53.24	27.00	0.03	64.56		
32	407	-2.426	6.95	40.0	4.83		1.752	57.65	28.97	0.03	69.73		
32	439	-2.706	7.32	41.5	4.72	1.968	1.885	62.06	30.90	0.04	74.85		
16	455	**	7.32	41.5	4.72	**	**	64.27	31.86	0.04	77.42		

^{*} Nominal yield stress

^{**} Data not taken

Table E.5. Results of 75 Inch Combined Bending and Torsion Test (Neglecting Warping Stresses): Marion 3 lb/ft - 80 ksi Post; 3 Inch Back to Back Splice in Critical Configuration (Grade 9 Field Bolts).

Dist Dist Mome	to bo to stant ent arm	gth (in) It A (in) rain gaug (in) ty (in) .	e (in) .	1.50 10.00 75.50			BENDING TORSION TEST (Warping Neglected) MARION 3 lb/ft - 80 ksi * Back to back; gr 9 bolts Critical orientation						
I	.OAD		Tip	Tip	Tor	,	AIN auge		BASE S	TRESSES			
(1	.bs)	Ch.#1	Defl	Rot	Arm			Bending	Torsion	Axial	Combined		
Appl	Tot	(mV)	(in)	(deg)	(in)	Obs.	Calc.	Mc/I	Th/J	P/A	(Mohr)		
	DL	1.378	0.00	0.0	6 20		0.000						
55	55	1.709	1 1.00	14.0	6.30 6.11	0.039 0.245	0.039	1.92	0.00	0.00	1.92		
32	87	1.902	1.61	19.5	5.94	0.245	0.278 0.417	12.02	4.70	0.00	13.64		
32	119	2.100	2.22	24.5	5.73	0.489	0.417	17.90	7.36	0.00	20.54		
32	151	2.299	2.85	29.0	5.51	0.489	0.556	23.78 1 29.65	9.92 12.39	0.00 0.01	27.38		
32	183	2.495	3.46	32.0	5.34	0.735	0.833	1 35.52	14.78	0.01	34.15		
1 32	215	2.704	4.12	34.5	5.19	0.865	0.033	41.39	17.10	0.01	40.87 47.55		
32	247	2.914	4.81	37.0	5.03	0.996	1.111	47.26	19.35	0.01	54.19		
32	279	3.117	5.54	39.0	4.90	1.122	1.249	53.12	21.54	0.02	60.78		
16	295	3,237	5.94	40.0	4.83	1.197	1.318	56.05	22.62	0.02	64.06		
16	311	3.342	6.36	40.5	4.79	1.263	1.388	58.98	23.69	0.03	67.34		
16	327	3.447	6.77	41.5	4.72	1.328	1.457	61.91	24.74	0.03	70.61		
16	343	3.566	7.26	42.5	4.64	1.402	1.526	64.83	25.78	0.04	73.87		
16	359	3.680	7.72	43.0	4.61	1.473	1.595	67.76	26.81	0.04	77.12		
16	375	3.791	8.26	44.0	4.53	1.542	1.664	70.68	27.83	0.04	80.36		
16	391	3.928	8.85	44.5	4.49	1.628	1.733	73.60	28.83	0.05	83.59		

^{*} Nominal yield stress

Table E.6. Results of 75 Inch Combined Bending and Torsion Test (Neglecting Warping Stresses): Marion 3 lb/ft - 80 ksi Post; 3 Inch Nested Splice in Critical Configuration (Grade 9 Field Bolts).

Dist Dist Momer	to bol to str nt arm	gth (in) t A (in) rain gauge (in)	(in) .	1.50 10.13 73.50			MAI	(Warping RION 3 lb Nested;	ORSION TE Neglecte o/ft - 80 gr 9 bol orientat	d) ksi * ts	
Eccer		-y (±11)				STR	AIN		BASE S	TRESSES	۱
į Lo	DAD		Tip	Tip	Tor	At G		İ	(ks		1
j (11	os) į	Ch.#1	Defl	Rot	Arm	(uin	/in)	Bending	Torsion	Axial	Combined
Appl	ppl Tot (mV) (in) (deg)				(in)	Obs.	Calc.	Mc/I	Th/J	P/A	(Mohr)
						0.000	0.030	 1.92	0.00	0.00	1.92
-0	DL	0.994	0.00	0.0	6.30	0.039 0.280	0.039 0.249	1 10.86	4.29	0.00	12.35
50	50	0.607	0.87	13.0	6.14 5.99	0.280	0.249	15.15	6.30	0.00	17.43
24	74	0.423	1.28	18.0 22.0	5.84	0.595	0.350	19.45	8.26	0.00	22.48
24	98	0.237	2.08	26.0	5.66	0.625	0.451	23.74	10.16	0.00	27.49
24	122	-0.133	2.52	29.0	5.51	0.023	0.552	28.03	12.01	0.01	32.47
24	146 170	-0.133 -0.317	2.32	32.0	5.34	0.741	0.753	32.31	13.80	0.01	37.41
1 24	194	-0.500	3.35	35.0	5.16	0.830	0.755	36.60	15.53	0.01	42.31
1 24	218	-0.685	3.82	36.5	5.06	1.085	0.954	1 40.89	17.23	0.01	47.19
1 24	242	-0.858	1 4.24	39.0	4.90	1.193	1.055	45.17	18.87	0.02	52.03
25	267	-1.061	4.75	41.0	4.75		1.160	49.63	20.54	0.02	57.04
1 25	292	1 -1.253	5.30	43.0	4.61	1.439	1.264	54.09	22.15	0.02	62.02
25	317	1 -1.449	5.88	44.0	4.53	1.561	1.369	58.55	23.73	0.03	66,98
1 24	341	-1.628	6.49	46.0	4.38	1.673	1.470	62.82	25,20	0.03	71.71
24	365	-1.815	7.20	47.0	4.30	1.789	1.570	67.10	26.64	0.04	76.42
1 24	389	-2.001	8.21	49.0	4.13	1.905	1.670	71.36	28.03	0.05	81.09
1 24	413	-2.049	9.23	50.0	4.05	1.935	1.770	75.62	29.38	0.06	85.75
24	437	-2.228	10.29	51.0	3,96	2.046	1.870	79.87	30.71	0.07	90.38
16	453	-2.400	10.81	51.5	3.92	2.154	1.936	82.70	31.59	0.07	93.45

^{*} Nominal yield stress

Table E.7. Results of 75 Inch Combined Bending and Torsion Test (Neglecting Warping Stresses): Marion 4 lb/ft - 80 ksi Post; 4 Inch Back to Back Splice in Critical Configuration (Grade 9 Field Bolts).

Splice len Dist to bo Dist to st Moment arm Eccentrici	lt A (in) rain gaug (in)	e (in) .	1.50 9.13 75.63		BENDING TORSION TEST (Warping Neglected) MARION 4 lb/ft - 80 ksi * Back to back; gr 9 bolts Critical orientation STRAIN BASE STRESSES						
Appl. Total load Load (lbs) (lbs)	Ch.#1	Tip Defl (in)	Tip Rot (deg)	Tor Arm (in)	At 0	auge	 Bending Mc/I	(ks		Combined (Mohr)	
DL 55 55 32 87 32 119 32 151 32 183 32 215 32 247 32 279 32 343 32 343 32 345 32 407 32 439 32 471 32 503 32 535	-0.245 0.060 0.222 0.394 0.558 0.738 0.909 1.092 1.262 1.445 1.611 1.782 1.966 2.125 2.344 2.514 2.723	0.00 0.67 1.03 1.42 1.79 2.22 2.60 3.01 3.36 4.23 4.64 5.07 5.48 6.02 6.51 7.24	0.0 7.5 10.5 13.0 16.5 19.5 21.5 24.0 25.5 27.5 29.0 30.5 32.5 33.5 34.5 35.5	6.30 6.25 6.19 6.14 6.04 5.94 5.86 5.76 5.69 5.59 5.51 5.31 5.25 5.19 5.13 5.03	0.038 0.228 0.329 0.436 0.538 0.650 0.757 0.871 0.977 1.091 1.194 1.301 1.416 1.515 1.651 1.757 1.887	0.038 0.210 0.310 0.410 0.510 0.610 0.709 0.809 0.909 1.009 1.109 1.208 1.308 1.408 1.507 1.607	1.45 9.08 13.52 17.96 22.40 26.84 31.28 35.71 40.15 44.58 49.02 53.45 57.88 62.31 66.73 71.16 75.58	0.00 3.10 4.88 6.65 8.40 10.11 11.80 13.46 15.10 16.71 18.30 19.87 21.40 22.91 24.41 25.89 27.34	0.00 0.00 0.00 0.00 0.00 0.01 0.01 0.01	1.45 10.04 15.10 20.16 25.20 30.22 35.23 40.22 45.20 50.16 55.11 60.04 64.95 69.85 74.74 79.61	

^{*} Nominal yield stress

Table E.8. Results of 75 Inch Combined Bending and Torsion Test (Neglecting Warping Stresses): Marion 4 lb/ft - 80 ksi Post; 4 Inch Nested Splice in Critical Configuration (Grade 9 Field Bolts).

Dist Dist Momen	to bol to str nt arm	gth (in) It A (in) Sain gaug (in) Ty (in)	e (in) .	1.50 9.19 75.63			MA	(Warping RION 4 11 Nested;	ORSION TE Neglecte O/ft - 80 gr 9 bol orientat	d) ksi * ts	
14	то+-1			m		•	AIN	!	BASE S		
	Total		Tip	Tip	Tor	•	auge	I	(ks	•	!
load	(lbs)	Ch.#1	Defl	Rot	Arm	, ,			Torsion		
(IDS)	(10S)	(mV)	(in)	(deg)	(in)	Obs.	Calc.	Mc/I	Th/J	P/A	(Mohr)
1	DL	-0.488	0.00	0.0	6.30	0.038	0.038	1 1.40	0.00	0.00	1.40
j 55	55	-0.821	0.64	7.0	6.25	0.245	0.210	8.76	3:32	0.00	9.88
32	87	-1.003	1.02	11.0	6.18	0.359	0.310	13.04	5.23	0.00	14.88
32	119	-1.184	1.39	14.0	6.11	0.472	0.409	17.33	7.12	0.00	19.88
32	151	-1.355	1.77	17.5	6.01	0.578	0.509	21.61	8.98	0.00	24.85 i
32	183	-1.530	2.12	20.5	5.90	0.687	0.609	25.89	10.80	0.00	29.81
32	215	-1.706	2.48	23.5	5.78	0.797	0.709	30.17	12.59	0.01	34.74
32	247	-1.880	2.85	26.0	5.66	0.905	0.809	34.45	14.34	0.01	39.64
32	279	-2.044	3.24	28.5	5.54	1.007	0.908	38.73	16.05	0.01	44.52
32	311	-2.214	3.60	30.5	5.43	1.113	1.008	43.01	17.72	0.01	49.38
32	343	-2.379	4.00	32.5	5.31	1.216	1.108	47.28	19.37	0.01	54.22
32	375	-2.533	4.40	33.5	5.25	1.312	1.207	51.56	20.99	0.02	59.04
32	407	-2.713	4.83	36.0	5.10	1.424	1.307	55.83	22.56	0.02	63.83
32	439	-2.874	5.23	37.5	5.00	1.525	1.406	60.11	24.11	0.02	68.61
32	471	-3.043	5.65	39.0	4.90		1.506	64.38	25.62	0.03	73.36
32	503	-3.226	6.09	40.5	4.79		1.606	68.65	27.10	0.03	78.09
32	535	-3.396	6.09	42.0	4.68	1.850	1.705	72.92	28.55	0.04	82.80
24	559	-3.552	6.09	42.0	4.68	8 1.947 1.780 76.12 29.63 0.04 86.33					86.33

^{*} Nominal yield stress

Table E.9. Results of 75 Inch Combined Bending and Torsion Test (Including Warping Stresses): Franklin 3 lb/ft - 60 ksi Post; 3 Inch Back to Back Splice in Critical Configuration (Grade 5 Field Bolts).

Splice len Dist to bo Dist to st Moment arm Eccentrici	lt A (in) rain gaug (in)	e (in)	1.50 7.88 75.38			FRA Ba	ENDING TO (Includin NKLIN 3) ck to bac Critical	ng Warpir lb/ft - 6 ck; gr 5	ng) 50 ksi * bolts	
LOAD (1bs) Appl Tot	Ch.#1 (mV)	Tip Defl (in)	Tip Rot (deg)	Tor Arm (in)	At G	AIN auge /in) Calc.	 Bending Mc/I	(ks		Combined (Mohr)
0 26 26 24 50 24 74 24 98 24 122 24 146 24 170 24 194 24 218 24 242 24 266 24 290 8 306 8 314	1.003 1.238 1.457 1.671 1.878 2.080 2.276 2.472 2.646 2.813 2.976 3.095 3.146 3.249 3.124 3.036	0.00 0.60 1.18 1.83 2.47 3.12 3.76 4.43 5.13 5.84 6.70 7.65 8.81 9.81 10.55	0.0 7.5 13.0 17.5 22.0 25.0 28.0 30.0 32.5 34.5 36.0 39.0 40.0 40.5 41.5	6.30 6.25 6.14 6.01 5.84 5.71 5.56 5.46 5.31 5.19 5.10 4.96 4.90 4.83 4.79 4.72	0.052 0.198 0.335 0.468 0.597 0.723 0.845 0.967 1.076 1.180 1.281 1.355 1.387 1.451 1.374	0.052 0.246 0.424 0.601 0.777 0.952 1.126 1.299 1.471 1.642 1.812 1.980 2.149 2.204 2.260 2.316	1.94 8.26 14.07 19.85 25.59 31.31 36.98 42.64 48.25 53.84 59.40 64.92 70.43 72.26 74.08 75.90	0.00 1.49 2.85 4.17 5.46 6.72 7.94 9.15 10.32 11.46 12.59 13.68 14.76 15.12 15.47	0.00 0.00 0.00 0.00 0.01 0.01 0.01 0.02 0.02	1.94 8.52 14.62 20.69 26.71 32.69 38.63 44.53 50.38 56.20 61.98 67.72 73.43 75.33 77.22 79.11

^{*} Nominal yield stress

Table E.10. Results of 75 Inch Combined Bending and Torsion Test (Including Warping Stresses): Franklin 3 lb/ft - 60 ksi Post; 3 Inch Nested Splice in Critical Configuration (Grade 5 Field Bolts).

Dist Dist Mome	to bol to str nt arm	th (in) t A (in) tain gauge (in)	(in) .	1.50 8.25 75.50			FRAI	(Includin NKLIN 3 1 Nested; g	ORSION TE ng Warpin lb/ft - 6 gr 5 bolt orientat	g) 0 ksi * s	 - -
		·y (***/ ·				STRAIN BASE STRESSES					į
L	OAD		Tip	Tip	Tor	At G	auge	1	(ks	,	I
(1	(lbs) Ch.#l Defl Rot				Arm	(uin		Bending	Torsion		
Appl					(in)	Obs.	Calc.	Mc/I	Th/J	P/A	(Mohr)
	DL	0.411	0.00	0.0	6.30	0.052	0.051	1.94	0.00	0.00	1.94
26	26	0.177	0.61	7.0	6.25	0.198	0.245	8.27	1.49	0.00	8.53
1 24	50	-0.042	1.17	13.5	6.13	0.334	0.422	14.08	2.84	0.00	14.64
1 24	74	-0.261	1.71	18.5	5.97	0.471	0.599	19.87	4.16	0.00	20.70
1 24	98	-0.480	2.27	23.5	5.78	0.607	0.774	25.60	5.44	0.00	26.71
24	122	-0.701	2.85	27.0	5.61	0.745	0.948	31.30	6.67	0.01	32.67
24	146	-0.920	3.41	30.5	5.43	0.881	1.120	36.96	7.87	0.01	38.57
24	170	-1.137	3.98	34.0	5.22	1.017	1.291	42.56	9.02	0.01	44.41
24	194	-1.353	4.56	36.5	5.06	1.151	1.460	48.13	10.14	0.01	50.19
24	218	-1.569	5.22	38.0	4.96	1.286	1.629	53.68	11.23	0.02	55.95
24	242	-1.785	5.90	40.0	4.83	1.420	1.797	59.19	12.30	0.02	61.66
24	266	-1.999	6.70	42.5	4.64	1.554	1.963	•	13.32	0.03	67.32
24						1.695	2.128	70.11	14.34	0.03	72.96
8	298	-2.323	8.30	44.0	4.53		2.183	71.92	14.67	0.04	74.83
8	306	-2.401	8.68	44.5	4.49	1.804	2.238	73.73	15.00	0.04	76.70
8	314	-2.493	9.16	45.0	4.45	1.861	2.293	75.53	15.33	0.04	78.56

^{*} Nominal yield stress

Table E.11. Results of 75 Inch Combined Bending and Torsion Test (Including Warping Stresses): Franklin 4 lb/ft - 60 ksi Post; 4 Inch Back to Back Splice in Critical Configuration (Grade 5 Field Bolts).

Dist	to bole to strain	gth (in) It A (in) Cain gauge (in) Ty (in) .	e (in) .	1.50 9.25 75.63			FRAI Ba	(Includia NKLIN 4 1 ck to bac	DRSION TE ng Warpin lb/ft - 6 ek; gr 5 orientat	ig) 0 ksi * bolts		
	040					•	AIN	BASE STRESSES				
	OAD (σ ₁ μ1	Tip	Tip	Tor		auge		(ks	•	1	
	.bs)	Ch.#1	Defl	Rot	Arm	•			Torsion		Combined	
Appl	Tot	(mV)	(in)	(deg)	(in)	Obs.	Calc.	Mc/I	Th/J	P/A	(Mohr)	
1	DL	-0.888	0.00	0.0	6.30	0.049	0.049	 1.45	0.00	0.00	1 /5	
i 55	55	-0.521	0.99	7.5	6.25		0.309	10.18	3.61	0.00	1.45 11.33	
32	87	-0.320	1.51	11.5	6.17		0.460	15.25	5.69	0.00	17.14	
32	119	-0.113	2.04	15.0	6.09		0.400	20.31	7.73	0.00	22.92	
32	151	0.113	2.62	18.5	5.97	0.673	0.761	25.36	9.74	0.00	28.67	
32	183	0.320	3.19	21.0	5.88	0.802	0.911	1 30.39	11.72	0.00	34.39	
32	215	0.534	3.74	23.5	5.78	0.935	1.060	35.42	13.66	0.01	40.08	
32	247	0.753	4.37	26.0	5.66	1.071	1.209	1 40.43	15.57	0.01	45.74	
32	279	0.972	4.92	27.5	5.59	1.208	1.358	1 45.43	17.45	0.01	51.37	
32			5.48	1.353	1.506	50.41	19.29	0.02	56.97			
32	343	1.441	6.14	31.5	5.37	1.500	1.654	55.39	21.10	0.02	62.53	
32	375	1.738	7.11	33.5	5.25	1.685	1.801	60.34	22.86	0.02	68.05	

^{*} Nominal yield stress

Table E.12. Results of 75 Inch Combined Bending and Torsion Test (Including Warping Stresses): Franklin 4 lb/ft - 60 ksi Post; 4 Inch Nested Splice in Critical Configuration (Grade 5 Field Bolts).

	Dist Dist Momen	to bol to str nt arm	gth (in) It A (in) rain gauge (in) ty (in) .	e (in) .	1.50 7.06 75.56			FRA	ENDING TO (Includin NKLIN 4 I Nested; g ritical o	ng Warpin lb/ft - 6 gr 5 bolt	ng) 60 ksi * :s	
-	L	DAD		Tip	Tip	Tor	At G	AIN auge	!	(ks	•	; !
 A	(1bs) Ch.#1 Defl Rot Appl Tot (mV) (in) (deg) (/in) Calc.	Bending Mc/I			Combined (Mohr)
		DL	0.367	0.00	0.0	6.30	0.053	0.053	1.41	0.00	0.00	1,41
	55	55	-0.058	0.81	7.5	6.25	0.318	0.320	10.14	3.61	0.00	11.29
ı	32	87 إ	-0.300	1.72	15.5	6.07	0.469	0.474	15.20	5.65	0.00	17.07 j
ı	32	119	-0.306	2.19	18.0	5.99	0.472	0.629	20.25	7.67	0.00	22.83
İ	32	151	-0.530	2.66	22.0	5.84	0.612	0.783	25.28	9.63	0.00	28.54
l	32	183	-0.761	3.12	24.5	5.73	0.756	0.936	30.30	11.56	0.01	34.22
i	32	215	-1.002	3.61	27.5	5.59	0.906	1.089	35.31	13.44	0.01	39.85
1	32	247	-1.222	4.06	29.0	5.51	1.043	1.242	40.30	15.29	0.01	45.46
	32	279	-1.467		32.0	5.34	1.196	1.394	45.28	17.09	0.01	51.02
-	32	311	-1.683	5.03	33.5	5.25	1.330	1.545	50.25	18.85	0.02	56.55
	32	343	-1.927	5.57	35.5	5.13	1.482		55.20	20.58	0.02	62.04
1	32 375 -2.157 6.21 38.0 4.						1.626	1.847	60.13	22.25	0.03	67.49
1					4.83	1.793		65.04	23.87	0.03	72.89	
ļ	32	439	-2.706	7.32	41.5	4.72		2.146	69.94	25.46	0.04	78.26
	16	455	**	7.32	41.5	4.72	**	**	72.39	26.25	0.04	80.94

^{*} Nominal yield stress

^{**} Data not taken

Table E.13. Results of 75 Inch Combined Bending and Torsion Test (Including Warping Stresses): Marion 3 lb/ft - 80 ksi Post; 3 Inch Back to Back Splice in Critical Configuration (Grade 9 Field Bolts).

Dist Dist Mome	to bol to sti nt arm	gth (in) It A (in) Cain gauge (in)	e (in) .	1.50 10.00 75.50			MA Ba	(Includir RION 3 11 ck to bac	ORSION TE ng Warpin o/ft - 80 ck; gr 9 orientat	g) ksi * bolts	
	OAD I		Tip	Tip	Tor	,	AIN auge		BASE S	TRESSES	į
(1		Ch.#1	Defl	Rot	Arm	,	U	 Bending	Torsion	•	Combined
Appl	Tot	(mV)	(in)	(deg)	(in)	Obs.		Mc/I	Th/J	P/A	(Mohr)
											(110111)
i	DL	1.378	0.00	0.0	6.30	0.039	0.039	1.92	0.00	0.00	1.92
j 55	55	1.709	1.00	14.0	6.11	0.245	0.383	15.17	3.09	0.00	15.78
32	87	1.902	1.61	19.5	5.94	0.365	0.581	22.82	4.83	0.00	23.81
32	119	2.100	2.22	24.5	5.73	0.489	0.777	30.42	6.52	0.00	31.76
32	151	2.299	2.85	29.0	5.51	0.613	0.971	37.94	8.14	0.01	39.62
32	183	2.495	3.46	32.0	5.34	0.735	1.163	45.41	9.71	0.01	47.41
32	215	2.704	4.12	34.5	5.19	0.865	1.354	52.84	11.24	0.01	55.14
32	247	2.914	4.81	37.0	5.03	0.996	1.542	60.21	12.72	0.02	62.80
32	279	3.117	5.54	39.0	4.90	1.122	1.730	67.54	14.16	0.02	70.41
16	295	3.237	5.94	40.0	4.83	1.197	1.823	71.19	14.86	0.03	74.19
16	311	3.342	6.36	40.5	4.79	1.263	1.916	74.84	15.57	0.03	77.97
1.6	327	3.447	6.77	41.5	4.72	1.328	2.009	78.47	16.26	0.03	81.74
16	343	3.566	7.26	42.5	4.64	1.402	2.101	82.09	16.95	0.04	85.49
16	359	3.680	7.72	43.0	4.61		2.193	85.70	17.62	0.04	89.22
16	375	3.791	8.26	44.0	4.53	1.542	2.285	89.30	18.29	0.04	92.95
16	391	3.928	8.85	44.5	4.49	1.628	2.376	92.90	18.95	0.05	96.66

^{*} Nominal yield stress

Table E.14. Results of 75 Inch Combined Bending and Torsion Test (Including Warping Stresses): Marion 3 lb/ft - 80 ksi Post; 3 Inch Nested Splice in Critical Configuration (Grade 9 Field Bolts).

Dist Dist Mome	to bol to str nt arm	gth (in) It A (in) cain gauge (in) ty (in) .	e (in) .	1.50 10.13 73.50		BENDING TORSION TEST (Including Warping) MARION 3 lb/ft - 80 ksi * Nested; gr 9 bolts Critical orientation						
!					•••••	•				TRESSES	į	
	OAD		Tip	Tip	Tor	•	auge		(ks	•	ļ	
	bs)	Ch.#1	Defl	Rot	Arm (in)	•	/in)	Bending			Combined	
Appl	opl Tot (mV) (in) (deg)					Obs.	Calc.	Mc/I	Th/J	P/A	(Mohr)	
	DL	0.994	0.00	0.0	6.30	0.039	0.039	1.92	0.00	0.00	1.92	
50	50	0.607	0.87	13.0	6.14	0.280	0.345	13.73	2.82	0.00	14.29	
24	74	0.423	1.28	18.0	5.99	0.395	0.491	19.37	4.14	0.00	20.22	
24	98	0.237	1.66	22.0	5.84	0.511	0.635	24.97	5.43	0.00	26.10	
24	122	0.053	2.08	26.0	5.66	0.625	0.778	30.54	6.68	0.00	31.94	
24	146	-0.133	2.52	29.0	5.51	0.741	0.920	36.06	7.89	0.01	37.72	
24	170	-0.317	2.95	32.0	5.34	0.856	1.061	41.55	9.07	0.01	43.45	
24	194	-0.500	3.35	35.0	5.16	0.970	1.200	47.00	10.21	0.01	49.13	
24	218	-0.685	3.82	36.5	5.06	1.085	1.339	52.42	11.32	0.01	54.77	
24	242	-0.858	4.24	39.0	4.90	1.193	1.476	57.80	12.40	0.02	60.37	
25	267	-1.061	4.75	41.0	4.75	1.319	1.618	63.38	13.50	0.02	66.15	
25	292	-1.253	5.30	43.0	4.61	1.439	1.758	68.92	14.55	0.02	71.89 j	
25	317	-1.449	5.88	44.0	4.53	1.561	1.898	74.43	15.60	0.03	77.60	
24	341	-1.628	6.49	46.0	4.38	1.673	2.032	79.69	16.56	0.03	83.03 j	
24	365	-1.815	7.20	47.0	4.30	1.789	2.164	84.93	17.51	0.04	88.43	
24	389	-2.001	8.21	49.0	4.13		2.295	90.12	18.42	0.05	93.79	
24	413	-2.049	9.23	50.0	4.05	1.935	2.426	95.29	19.31	0.06	99.11	
1 24	437	-2.228	10.29	51.0	3.96	2.046		100.44	20.19	0.07	104.41	
16	453	-2.400	10.81	51.5	3.92	2.154	2.641	103.86	20.76	0.07	107.92	

^{*} Nominal yield stress

Table E.15. Results of 75 Inch Combined Bending and Torsion Test (Including Warping Stresses): Marion 4 lb/ft - 80 ksi Post; 4 Inch Back to Back Splice in Critical Configuration (Grade 9 Field Bolts).

Dist Dist Momen	to bol to str nt arm	gth (in) t A (in) cain gauge (in)	e (in) .	1.50 9.13 75.63			MA Ba	ENDING TO (Includir RION 4 lt ck to bac Critical	ng Warpin o/ft - 80 ck; gr 9	ng)) ksi * bolts	
	Total		Tip	Tip	Tor	•	STRAIN BASE STRESSE At Gauge (ksi)			TRESSES	į
load	,	Ch.#1	Defl	Rot	Arm	•	_	 Bending	•	•	Combined!
•	(lbs)		(in)	(deg)	(in)	Obs.	Calc.	Mc/I	Th/J	P/A	(Mohr)
			(±11)			005. 	Uaic.	1		1/4	(MOHE)
i	DL	-0.245	0.00	0.0	6.30	0.038	0.038	1.45	0.00	0.00	1.45
55	55 i	0.060	0.67	7.5	6.25	0.228	0.256	10.46	3.61	0.00	11.58
32	87 j	0.222	1.03	10.5	6.19	0.329	0.382	15.69	5.69	0.00	17.54
32	119	0.394	1.42	13.0	6.14	0.436	0.508	20.92	7.76	0.00	23.48
32	151	0.558	1.79	16.5	6.04	0.538	0.634	26.13	9.79	0.00	29.39
32	183	0.738	2.22	19.5	5.94	0.650	0.759	31.33	11.79	0.00	35.27
32	215	0.909	2.60	21.5	5.86	0.757	0.884	36.52	13.76	0.01	41.13
32	247	1.092	3.01	24.0	5.76	0.871	1.009	41.69	15.69	0.01	46.95
32	279	1.262	3.36	25.5	5.69	0.977	1.133	46.86	17.61	0.01	52.74
32	311	1.445	3.79	27.5	5.59	1.091	1.256	52.01	19.48	0.01	58.51
32	343	1.611	4.23	29.0	5.51		1.380	57.15	21.34	0.02	64.25
32	375	1.782	4.64	30.5	5.43	1.301	1.503	62.28	23.16	0.02	69.96
32	407	1.966	5.07	32.5	5.31	1.416	1.625	67.39	24.95	0.02	75.64
32	439	2.125	5.48	33.5	5.25	1.515	1.747	72.49	26.72	0.03	81.30
32	471	2.344	6.02	34.5	5.19	1.651	1.869	77.58	28.46	0.03	86.93
32	503 535	2.514	6.51	35.5	5.13	1.757	1.990	82.66	30.19	0.04	92.54
1 32	ا ددد	2.723	7.24	37.0	5.03	1.887	2.111	87.73	31.88	0.04	98.13

^{*} Nominal yield stress

Table E.16. Results of 75 Inch Combined Bending and Torsion Test (Including Warping Stresses): Marion 4 lb/ft - 80 ksi Post; 4 Inch Nested Splice in Critical Configuration (Grade 9 Field Bolts).

Dist Dist Momen	to bol to str nt arm	gth (in) It A (in) Tain gauge (in) Ty (in)	 e (in) .	1.50 9.19 75.63	!		MA	(Includir RION 4 11 Nested;	DRSION TE ng Warpin p/ft - 80 gr 9 bol orientat	g) ksi * ts	
	Appl. Total Tip Tip Load Load Ch.#1 Defl Rot					At G		 Bending Mc/I	BASE S (ks Torsion Th/J	i)	Combined (Mohr)
55 32 32 32 32 32 32 32 32	DL 55 87 119 151 183 215 247 279 311 343 375 407 439 471	-0.488 -0.821 -1.003 -1.184 -1.355 -1.530 -1.706 -1.880 -2.044 -2.214 -2.379 -2.533 -2.713 -2.874 -3.043	0.00 0.64 1.02 1.39 1.77 2.12 2.48 3.24 3.60 4.00 4.40 4.83 5.23 5.65	0.0 7.0 11.0 14.0 17.5 20.5 23.5 26.0 28.5 30.5 32.5 33.5 36.0 37.5 39.0	6.30 6.25 6.18 6.11 6.01 5.90 5.78 5.66 5.54 5.43 5.31 5.25 5.10 5.00 4.90		0.038 0.256 0.382 0.508 0.633 0.758 0.883 1.007 1.130 1.253 1.375 1.497 1.619 1.740 1.860	1.40 10.41 15:64 20.86 26.07 31.27 36.44 41.61 46.75 51.88 57.00 62.11 67.19 72.26	0.00 3.61 5.69 7.75 9.77 11.75 13.70 15.60 17.46 19.29 21.08 22.84 24.56 26.24 27.88	0.00 0.00 0.00 0.00 0.00 0.00 0.01 0.01	1.40 11.54 17.49 23.43 29.33 35.20 41.02 46.81 52.57 58.28 63.96 69.62 75.23 80.80 86.35
32 32 24	503 535 559	-3.226 -3.396 -3.552	6.09 6.09 6.09	40.5 42.0 42.0	4.79 4.68 4.68	1.744 1.850 1.947	1.980 2.100 2.189	82.36 87.38 91.15	29.49 31.07 32.25	0.03 0.04 0.04	91.86 97.33 101.44

^{*} Nominal yield stress

APPENDIX F

PRELIMINARY 72 " BENDING TESTS

CALIBRATED BOLT SUMMARY TABLES

Marion 3 lb/ft Posts - 80 ksi Nominal Yield Stress

Back to Back, Nested and Face to Face Splices
Critical and Non-critical Configurations

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Table F.1. Results of 72 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 3 Inch Back to Back Splice in Critical Configuration (Calibrated Bolts).

Dist	e length (in to bolt A (i: to strain gar t arm (in) .	n) uge (in) .	. 1.25 . 8.00			MAJ	RION 3 I Back t	DING TE	ST - 80 splice	ksi *
LOAD (1bs) Appl Tot	 Ch.#1 Ch.: (mV) (mV		Tip Defl (in)	Total Defl (in)	(ki	LOADS ps) Bolt B	At C	AAIN Gauge n/in) Calc.	STR (ks Base	ESS i) Obs @ Gauge
60 60 32 92 32 124 32 156 32 188 32 220 32 252 32 284 32 316 32 348 32 380 16 492 16 428 16 444 16 460 16 476	-0.791 -0.5 -2.575 -3.4 -2.602 -3.1 -2.605 -3.0 -2.603 -3.0 -2.598 -3.0 -2.592 -3.0 -2.586 -3.0 -2.563 -3.0 -2.542 -3.2 -2.542 -3.4 -2.454 -3.6 -2.396 -3.7 -2.337 -4.0 -2.277 -4.1 -2.277 -4.1 -2.277 -4.1 -2.277 -4.1 -2.274 -4.2 -2.116 -4.64	28 7.321 37 7.048 71 7.499 43 7.732 19 7.969 16 8.220 29 8.464 92 8.690 65 8.934 22 9.181 21 9.426 99 9.646 90 9.877 90 9.89 96 10.210 92 10.330 67 10.440 44 10.550	0.00 0.72 0.39 0.40 0.43 0.42 0.46 0.51 0.48 0.53 0.27 0.29 0.30 0.29 0.31	0.00 0.72 1.11 1.50 1.94 2.35 2.75 3.19 3.65 4.15 4.63 5.16 5.42 5.68 5.97 6.55 6.86 7.17	2.69 2.73 2.74 2.73 2.72 2.71 2.67 2.64 2.58 2.51 2.42 2.33 2.29 2.24 2.15 2.10 2.04 2.00	4.48 4.02 3.91 3.87 3.83 3.85 3.95 4.22 4.47 4.78 5.06 5.38 5.58 5.58 6.11 6.23 6.38	0.042 0.042 0.323 0.468 0.616 0.772 1.065 1.217 1.371 1.524 1.661 1.805 1.874 1.944 2.012 2.027 2.155 2.224 2.299	0.042 0.297 0.433 0.570 0.706 0.842 0.978 1.115 1.251 1.387 1.523 1.660 1.728 1.796 1.864 1.932 2.000 2.068 2.137	1.90 12.45 18.07 23.70 29.32 34.95 40.57 46.20 51.82 57.45 63.07 68.70 71.51 74.32 77.14 79.95 82.76 85.57 88.39	1.26 9.69 14.04 18.47 23.17 27.73 31.95 36.51 41.13 45.71 49.82 54.14 56.23 58.31 60.36 62.66 66.72 68.96 68.96

Effective splice length (critical bolt) 5.0 in

Effective splice length (both bolts) N/A

Table F.2. Results of 72 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 3 Inch Nested Splice in Critical Configuration (Calibrated Bolts).

Dist	to bolt to strai	A (in) in gauge	:	. 1.06 . 7.75				ION 3 LB Nest	ING TEST	r - 80 k ce	si *
								l STR	AIN	STR	ESS
LOAD	1			Tip	Total	BOLT L (kip	s)		auge	(ks	i)
(1bs)	Ch.#1	Ch.#2	Ch.#3	Defl	Defl	Bolt	Bolt	(uin	/in)	,	Obs @
Appl Tot	(mV)	(mV)	(Vm)	(in)	(in)	A	В	Obs.	Calc.	Base	Gauge
floor	0 765	0 531	4.797								
*	1-3.959		•	(·		4.82	5.50	i i			
, ,	1-3.683			0.00	0.00	4.40	5.32	0.042	0.042	1.90	1.26
	-3.432			0.88	0.88	4.02	5.44	0.327	0.298	12.42	9.82
32 92	-3.338	-4.060	10.190	0.44	1.32	3.88	5.55	0.468	0.434	18.03	14.04
32 124	-3.242	-4.123	10.400	0.57	1.89	3.74	5.64	0.599	0.571	23.64	17.97
32 156	-3.150	-4.203	10.640	0.52	2.41	3,60	5.77	0.749	0.707	29.25	22.46
32 188	-3.081	-4.285	10.860	0.50	2.91	3.49	5.90	0.886	0.843	34.86	26.57
•	•		10.100	0.58	3.48	3.41	6.04	0.412	0.980	40.47	12.36
•	1-2.987			0.58	4.06	3.35	6.19	1.178	1.116	46.08	35.35
•	-2.969			0.54	4.60	3.33	6.26	1.303	1.252	51.69	39.09
•	-2.962			0.68	5.28	3.31	6.39	1.446	1.389	•	43.39
•	1-2.965			0.43	5.71	3.32	6.46	1.527	1.457		45.82
•	1-2.970			0.40	6.11		6.48	1.602	1.525	62.91	48.06
16 364	-2.976	-4./00	12.120	0.36	6.46	3.34	6.55	1.671	1.593	65.72	50.12

Effective splice length (critical bolt) 3.8 in Effective splice length (both bolts) 3.8 in

^{*} Nominal yield stress

Table F.3. Results of 72 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 3 Inch Face to Face Splice in Critical Configuration (Calibrated Bolts).

Dist t	e length (in) . co bolt A (in) co strain gauge c arm (in)	(in) .	. 1.63 . 8.25			MAI	RION 3 L Face t	DING TES B/FT POS o face s l orient	ST - 80 splice	
LOAD		Total	- BOLT LOADS STRAIN STR (kips) At Gauge (ks							
(lbs) Appl Tot							(uin Obs.	/in) Calc.	 Base	Obs @ Gauge
floor tight DL 60 60 92 32 92 32 124 32 156 32 188 32 220 16 236 16 252 16 268 16 300 16 316	1.081 0.708 0.388 -0.349 0.454 -0.366 0.622 -0.649 0.699 -0.813 0.771 -1.088 0.834 -1.227 0.879 -1.483 0.931 -1.819 0.949 -1.980 0.969 -2.128 0.983 -2.285 1.001 -2.454 1.022 -2.651 1.036 -2.794 1.056 -2.948	2.259 2.230 2.156 1.739 1.528 1.303 1.094 0.890 0.648 0.534 0.433 0.327 0.211 0.76 -0.026	0.00 1.02 0.52 0.57 0.55 0.43 0.69 0.32 0.31 0.36 0.55	0.00 1.02 1.54 2.11 2.65 3.09 3.77 4.09 4.40 4.71 5.07 5.07 5.96 6.36	1.30 1.18 0.86 0.72 0.58 0.46 0.38 0.28 0.25 0.21 0.11 0.08	2.09 2.13 2.69 3.01 3.56 3.83 4.34 5.01 5.33 5.62 5.93 6.27 6.66 6.94 7.24	0.041 0.041 0.301 0.432 0.572 0.703 0.830 0.981 1.052 1.115 1.181 1.253 1.337 1.466	0.041 0.297 0.434 0.570 0.707 0.844 0.980 1.048 1.117 1.185 1.253 1.321 1.390 1.458	1.90 12.50 18.16 23.81 29.47 35.12 40.78 43.60 46.43 49.26 52.09 54.91 57.74	1.23 9.02 12.97 17.17 21.08 24.89 29.42 31.55 33.44 35.42 37.59 40.11 42.01 43.98

Effective splice length (critical bolt) 3.1 in

Effective splice length (both bolts) N/A

^{*} Nominal yield stress

Table F.4. Results of 72 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 3 Inch Back to Back Splice in Non-critical Configuration (Calibrated Bolts).

				3 00				BEN	DING TES	ST	
Dist Dist	to bolt	A (in)	ge (in)	. 1.38 . 7.88				RION 3 L Back t on-criti	o back s	splice	
LOAD (lbs)	 Ch.#1 (mV)	Ch.#2 (mV)	Ch.#3 (mV)	Tip Defl (in)	Total Defl (in)	(ki	LOADS ps) Bolt B		AIN auge /in) Calc.	(ks	ESS i) Obs @ Gauge
tight DL 60 60 32 92 32 124 32 156 32 188 32 220 32 252 32 252 32 284 32 316 32 348 32 380 32 412	-0.874 -3.068 -3.069 -3.087 -3.116 -3.164 -3.229 -3.325 -3.514 -3.717 -4.162 -4.385 -4.611 -4.805 -4.861	-2.926 -2.847 -2.884 -2.891 -2.910 -2.928 -2.942 -2.947 -2.956 -2.956 -2.954 -2.928 -2.900 -2.867		0.54	0.00 0.75 1.14 1.53 1.94 2.36 2.79 3.24 3.72 4.23 4.73 5.27 5.85 6.44	3.31 3.34 3.38 3.46 3.55 3.70 3.98 4.29 4.61 4.61 5.30 5.64 5.93 6.02	3.66 3.53 3.59 3.60 3.63 3.66 3.71 3.71 3.70 3.66 3.62 3.57 3.52	0.042 0.243 0.324 0.439 0.550 0.662 0.783 1.024 1.1255 1.274 1.403 1.532 1.615	0.042 0.298 0.435 0.572 0.709 0.845 0.982 1.119 1.256 1.393 1.529 1.666 1.803 1.940	1.90 12.46 18.10 23.73 29.37 35.00 40.64 46.27 51.91 63.18 68.81 74.45 80.08	1.26 7.30 9.73 13.17 16.49 19.86 23.48 26.83 30.72 34.64 38.23 42.10 45.97 48.44

Effective splice length (critical bolt) 5.0 in Effective splice length (both bolts) N/A

^{*} Nominal yeild stress

Table F.5. Results of 72 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 3 Inch Nested Splice in Non-critical Configuration (Calibrated Bolts).

Splice length (in) Dist to bolt A (in) Dist to strain gauge (in) Moment arm (in)	. 1.33 . 8.00		BENDING TE: RION 3 LB/FT PO: Nested spl: on-critical ori	ST - 80 ksi * ice
LOAD	Tip Total Defl Defl (in) (in)	BOLT LOADS (kips) Bolt Bolt A B	STRAIN At Gauge (uin/in) Obs. Calc.	STRESS (ksi) Obs@ Base Gauge
floor -0.766 -0.673 8.314 tight -3.414 -3.374 7.561 DL -3.353 -3.186 8.184 60 60 -3.509 -3.019 7.792 32 92 -3.600 -2.934 7.594 32 124 -3.712 -2.864 7.384 32 156 -3.828 -2.808 7.160 32 188 -3.965 -2.768 6.898 32 220 -4.063 -2.756 6.681 32 252 -4.193 -2.761 6.459 32 284 -4.279 -2.787 6.234 32 316 -4.400 -2.817 6.015 32 348 -4.486 -2.858 5.283 16 364 -4.500 -2.883 5.720 16 380 -4.524 -2.907 5.621 16 396 -4.539 -2.933 5.516	0.00 0.00 0.90 0.90 0.51 1.41 0.53 1.94 0.56 2.50 0.62 3.11 0.54 3.65 0.60 4.24 0.67 4.91 0.63 5.53 0.63 6.16 0.35 6.51 0.37 6.88 0.37 7.24 0.36 7.60	3.98 4.24 3.89 3.95 4.12 3.69 4.26 3.55 4.43 3.44 4.60 3.35 4.81 3.29 4.96 3.27 5.16 3.28 5.29 3.32 5.47 3.37 5.60 3.43 5.62 3.47 5.65 3.51 5.68 3.55 5.68 3.59	0.042 0.042 0.286 0.298 0.410 0.434 0.540 0.570 0.680 0.707 0.843 0.843 0.978 0.980 1.117 1.116 1.257 1.252 1.393 1.389 1.849 1.525 1.577 1.594 1.639 1.662 1.704 1.730 1.754 1.798	1.90 1.26 12.46 8.59 18.09 12.29 23.72 16.21 29.35 20.40 34.98 25.30 40.61 29.35 46.25 33.50 51.88 37.71 57.51 41.80 63.14 55.48 65.96 47.32 68.77 49.17 71.59 51.13 74.40 52.61

Effective splice length (critical bolt) 4.9 in Effective splice length (both bolts) 4.6 in

^{*} Nominal yield stress

Table F.6. Results of 72 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 3 Inch Face to Face Splice in Non-critical Configuration (Calibrated Bolts).

Dist	e length to bolt a to strain	A (in) n gauge	(in)	1.31 7.75	,			RION 3 L Face t	DING TES B/FT POS o face s cal orie	ST - 80 splice	į
LOAD (lbs)	 Ch.#1 (mV)	Ch.#2 (mV)	Ch.#3 (mV)	Tip Defl (in)	(ki	LOADS ps) Bolt B	s) At Gauge (ksi) Bolt (uin/in) O				
floor tight DL 60 60 32 92 32 124 48 172 32 204 32 236 32 268 16 284 16 300 16 316	1.077 0.768 0.775 0.342 0.100 -0.155 -0.502 -0.782 -1.073 -1.344 -1.513 -1.672 -1.809	0.707 -0.433 -0.277 0.026 0.141 0.242 0.391 0.445 0.503 0.562 0.589 0.613 0.634	2.240 2.226 2.319 2.801 3.020 3.233 3.479 3.682 3.891 4.088 4.211 4.324 4.425	0.00 1.10 0.53 0.53 0.80 0.43 0.67 0.60 0.34 0.34	0.00 1.10 1.63 2.16 2.96 3.39 4.06 4.65 4.99 5.33 5.63	0.58 0.57 1.38 1.83 2.31 2.96 3.49 4.03 4.54 4.86 5.16	2.26 1.95 1.35 1.12 0.92 0.63 0.52 0.40 0.29 0.23 0.19	0.041 0.341 0.478 0.610 0.764 0.890 1.020 1.143 1.220 1.290 1.353	0.041 0.297 0.434 0.570 0.775 0.912 1.049 1.185 1.254 1.322 1.390	1.90 12.44 18.06 23.68 32.11 37.73 43.35 48.97 51.78 54.59	1.23 10.24 14.33 18.31 22.91 26.71 30.61 34.30 36.59 38.71 40.59

Effective splice length (critical bolt) 4.0 in

Effective splice length (both bolts) N/A

Table F.7. Results of 72 Inch Bending Test: Marion 3 1b/ft - 80 ksi Post; 4 Inch Back to Back Splice in Critical Configuration (Calibrated Bolts).

Splice length (in) Dist to bolt A (in) Dist to strain gauge (in Moment arm (in)	. 1.56) 9.06	BENDING TEST MARION 3 lb/ft post - 80ksi Back to back splice Critical orientation						
LOAD (1bs) Ch.#1 Ch.#2 Ch.#3 Appl Tot (mV) (mV)	Tip Total Defl Defl (in) (in)	BOLT LOADS (kips) Bolt Bolt A B	STRAIN At Gauge (uin/in) Obs Calc	STRESS (ksi) Obs @ Base Gauge				
floor -0.651 -0.707 0.031 tight -4.857 -3.784 0.007 DL -4.867 -3.712 0.079 60 60 -4.895 -3.671 0.502 32 92 -4.901 -3.656 0.702 32 124 -4.906 -3.651 0.910 32 156 -4.907 -3.653 1.134 32 188 -4.902 -3.659 1.343 32 220 -4.898 -3.679 1.550 32 252 -4.875 -3.721 1.781 32 284 -4.866 -3.811 1.997 32 316 -4.847 -4.068 2.209 32 348 -4.816 -4.314 2.400 32 380 -4.783 -4.601 2.621 32 412 -4.741 -4.927 2.874 16 428 -4.699 -5.067 2.985 16 444 -4.678 -5.195 3.079 16 460 -4.657 -5.339 3.191 16 476 -4.614 -5.465 3.290	0.00 0.00 0.79 0.79 0.40 1.19 0.42 1.61 0.46 2.07 0.42 2.49 0.42 2.90 0.47 3.37 0.44 3.81 0.46 4.27 0.43 4.70 0.59 5.29 0.59 5.87 0.26 6.13 0.23 6.36 0.25 6.61 0.24 6.86	6.35 4.84 6.36 4.72 6.40 4.66 6.41 4.63 6.42 4.63 6.42 4.63 6.41 4.64 6.41 4.67 6.37 4.74 6.36 4.88 6.33 5.28 6.28 5.67 6.23 6.12 6.13 6.11 6.63 6.13 6.11 6.85 6.13 6.08 7.05 6.04 7.28 6	0.057 0.041 0.321 0.293 0.446 0.428 0.575 0.562 0.715 0.697 0.845 0.832 0.974 0.966 1.118 1.101 1.252 1.236 1.385 1.370 1.504 1.505 1.641 1.640 1.799 1.774 1.868 1.842 1.927 1.909 1.996 1.976 2.058 2.044	1.90 1.72 12.49 9.63 18.14 13.37 23.79 17.26 29.44 21.44 35.09 25.35 40.74 29.22 46.39 33.54 52.04 37.57 57.69 41.54 63.34 45.11 68.99 49.24 74.64 53.97 77.46 56.04 80.29 57.80 83.11 59.89 85.94 61.74				

Effective splice length (critical bolt) 4.3 in

Effective splice length (both bolts) $\ensuremath{\mathtt{N}/A}$

^{*} Nominal yield stress

Table F.8. Results of 72 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 4 Inch Nested Splice in Critical Configuration (Calibrated Bolts).

Dis Dis	lice length (in st to bolt A (in st to strain ga	in) auge (in	. 1.38) 8.88		BENDING TEST MARION 3 lb/ft post - 80 Nested splice Critical orientation						
LOAD (lbs) Appl Tot	(lbs) Ch.#1 Ch.#2 Ch.#3 Defl Defl ppl Tot (mV) (mV) (in) (in)						BOLT LOADS STRAIN STR (kips) At Gauge (k Bolt Bolt (uin/in) A B Obs Calc Base				
tight DL 60 60 32 92 32 124 32 156 32 188 32 220 32 252 32 284 32 316 32 348 32 380	-0.894 -0.596 -2.480 -3.359 -2.368 -3.231 -2.140 -3.288 -2.015 -3.321 -1.887 -3.373 -1.787 -3.427 -1.694 -3.486 -1.628 -3.567 -1.574 -3.641 -1.547 -3.731 -1.525 -3.819 -1.515 -3.928 -1.513 -4.043 -1.521 -4.153 -1.535 -4.256	2.251 2.258 2.945 3.370 3.581 3.824 4.043 4.280 4.516 4.772 4.995 5.224 5.453 5.696 5.928 6.168	0.69 0.43 0.50 0.47 0.51 0.52 0.59 0.51 0.55 0.54 0.59 0.58	0.69 1.12 1.62 2.08 2.59 3.11 3.70 4.20 4.75 5.29 5.88 6.46 7.08	5.09 4.92 4.58 4.39 4.20 4.04 3.81 3.72 3.68 3.65 3.63 3.63	6.21 6.01 6.10 6.15 6.24 6.32 6.41 6.54 6.66 6.80 6.94 7.11 7.29 7.46 7.62		0.041 0.297 0.434 0.571 0.708 0.844 0.981 1.118 1.255 1.391 1.528 1.665 1.802 1.870	1.90 12.46 18.10 23.73 29.37 35.00 40.64 46.27 51.91 57.54 63.18 68.81 74.45	1.23 9.17 13.12 17.66 21.75 26.18 30.59 35.38 39.55 43.83 48.11 52.65 56.99 61.47	

Effective splice length (critical bolt) 3.8 in

Effective splice length (both bolts) N/A

Table F.9. Results of 72 Inch Bending Test: Marion 3 lb/ft - 80 ksi
Post; 4 Inch Face to Face Splice in Critical
Configuration (Calibrated Bolts).

Dis Dis	lice length (st to bolt A st to strain and the strain and the strain and the strain)	(in) gauge (in	. 1.25) 8.75			МА	ARION 3 Face	to face	ost - 80k	tsi *
					BOLT LOADS STRAIN				STRE	SS
LOAD		Total	(ki	• •	•	auge	(ks	•		
(lbs)	Ch.#1 Ch.#2		•	Defl		Bolt B	, ,	/in) Calc	7	Obs @
Appl Tot	(mV) (mV)	(mV)	(in)	(in)	A		l obs	Carc	Base	Gauge
tight DL 60 60 32 92 32 124 32 156	1.087 0.702 -0.211 -0.368 -0.097 -0.224 0.122 -0.423 0.220 -0.542 0.311 -0.684 0.414 -0.846 0.515 -1.022 0.612 -1.210 0.693 -1.423 0.762 -1.660 0.762 -1.890 0.905 -2.179 0.930 -2.303	3 2.418 4 2.375 3 1.950 2 1.735 4 1.522 5 1.297 2 1.089 0 0.871 7 0.655 0 0.431 0 0.217 9 -0.039	0.87 0.48 0.48 0.51 0.49 0.50 0.50 0.52	0.87 1.35 1.83 2.34 2.82 3.31 3.81 4.33 4.33 5.49	2.43 2.22 1.81 1.63 1.46 1.26 1.07 0.89 0.74 0.61 0.61 0.34 0.29	1.91 1.62 2.02 2.25 2.54 2.86 3.21 3.58 4.01 4.47 4.93 5.50 5.74	1.386	0.041 0.293 0.428 0.563 0.697 0.832 0.967 1.101 1.236 1.305 1.505	1.90 12.45 18.07 23.70 29.32 34.95 40.57 46.20 51.82 53.07 65.89	1.23 9.17 13.19 17.17 21.38 25.27 29.34 33.38 37.57 41.57 46.35 48.39
16 380 16 396	0.968 -2.420 1.004 -2.556	-0.262	0.32	6.08	0.29	5.98	1.684	1.640	68.70 71.51	50.52 52.91

Effective splice length (critical bolt) 4.2 in

Effective splice length (both bolts) N/A

Table F.10. Results of 72 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 4 Inch Back to Back Splice in Non-critical Configuration (Calibrated Bolts).

 	lice ler	arth (ir	n)	4 00	****			BE	NDING TE	EST	******	
Dis Dis	st to bo	olt A (i rain ga	in) auge (in)	1.31		MARION 3 lb/ft post - 80ksi * Back to back splice						
Mon	ment arm	i (in) .		.72.31	i			Non-cri	tical or	rientatio	n	
						BOLT	LOADS	STR	AIN	STRE	SS	
LOAD				Tip	Total	(ki	ps)	At G	auge	(ks	i)	
(lbs)	Ch.#1	Ch.#2	Ch.#3	Defl	Defl	Bolt	Bolt	(uin	/in)	l	Obs @	
Appl Tot	(mV)	(mV)	(mV)	(in)	(in)	A	В	Obs	Calc	Base	Gauge	
floor	 -1.330	-0.712	0.041							* * * * * * * * * * * * * * * * * * *		
	-6.482		0.011	i		7.77	4.84			i i		
	-6.430		-0.053	0.00	0.00	7.69	4.90	0.043	0.043	1.55	1.29	
60 60	-6.407	-3.850	-0.481	0.71	0.71	7.66	4.93	0.310	0.303	12.10	9.29	
32 92	-6.380	-3.853	-0.685	0.35	1.05	7.62	4.94	0.437	0.442	17.73	13.10	
32 124	-6.360	-3.868	-0.902	0.37	1.42	7.59	4.96	0.572	0.581	23.36	17.16	
32 156	-6.337	-3.881	-1.119	0.38	1.80	7.55	4.98	0.707	0.719	28.99	21.21	
32 188	-6.318	-3.894	-1.327	0.40	2.20	7.53	5.00	0.837	0.858	34.62	25.10	
32 220	-6.291	-3.909	-1.574	0.40	2.59	7.48	5.02	0.991	0.997	40.25	29.72	
32 252	-6.273	-3.930	-1.804	0.41	3.01	7.46	5.06	1.134	1.136	45.88	34.02	
32 284	-6.254	-3.946	-2.004	0.36	3.37	7.43	5.08	1.259	1.275	51.51	37.76	
32 316	-6.228	-3.966	-2.256	0.46	3.82	7.39	5.11	1.416	1.413	57.14	42.47	
32 348	-6.206	-3.985	-2.485	0.41	4.23	7.36	5.14	1.558	1.552	62.77	46.75	
32 380	-6.180	-3.996	-2.708	0.41	4.64	7.32	5.16	1.697	1.691	68.40	50.92	
32 412	-6.156	-4.014	-2.935	0.42	5.06	7.28	5.19	1.839	1.830	74.03	55.16	
16 428	-6.157	-4.018	-3.053	0.22	5.28	7.28	5.19	1.912	1.899	76.85	57.36	
16 444	-6.155	-4.022	-3.152	0.19	5.46	7.28	5.20	1.974	1.968	79.66	59.21	
16 460	-6.161	-4.026	-3.623	0.21	5.67	7.29	5.21	2.267	2.038	82.48	68.02	
16 476	-6.223	-4.028	-3.377	0.20	5.88	7.38	5.21	2.114	2.107	85.29	63.42	
16 492	-6.318	-4.026	-3.476	0.20	6.08	7.53	5.21	2.176	2.176	88.11	65.27	
16 508	-6.427	-4.021	-3.596	0.23	6.31	7.69	5.20	2.250	2.246	90.92	67.51	

Effective splice length (critical bolt) 4.4 in

Effective splice length (both bolts) N/A

Table F.11. Results of 72 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 4 Inch Nested Splice in Non-critical Configuration (Calibrated Bolts).

Splice length (in Dist to bolt A (: Dist to strain games Moment arm (in)	in) 1.7 auge (in) 9.2	5 5	BENDING TEST MARION 3 lb/ft post - 80ksi * Nested splice Non-critical orientation						
LOAD (1bs) Ch.#1 Ch.#2 Appl Tot (mV) (mV)	BOLT LOADS STRAIN STRE (kips) At Gauge (ks Bolt Bolt (uin/in) A B Obs Calc Base								
floor -1.347 -0.410 tight -5.958 -4.630 DL -5.826 -4.424 60 60 -5.981 -4.284 32 92 -6.064 -4.223 32 124 -6.154 -4.160 32 156 -6.244 -4.108 32 188 -6.283 -4.063 32 220 -5.761 -4.028 32 252 -5.743 -3.997 32 284 -5.771 -3.978 32 316 -5.816 -3.966 32 348 -5.802 -3.957 32 380 -5.841 -3.956 32 412 -5.767 -3.960 32 444 -5.731 -3.969	-0.252 0.5 -0.474 0.4 -0.685 0.5	4 0.84 2 1.26 8 1.74 9 2.23 6 2.68 1 3.19 0 3.68 3 4.11 0 4.61 0 5.10 8 5.58 0 6.08	6.96 6.76 6.99 7.12 7.25 7.39 7.45 6.66 6.63 6.67 6.74 6.72 6.72 6.66	6.63 6.31 6.09 5.89 5.81 5.74 5.64 5.59 5.57 5.57	0.040 0.307 0.434 0.576 0.719 0.850 0.995 1.152 1.277 1.423 1.562 1.700 1.832 1.970	0.040 0.297 0.434 0.570 0.707 0.844 0.981 1.117 1.254 1.391 1.528 1.665 1.938	1.89 12.45 18.08 23.71 29.34 34.97 40.60 46.23 51.86 57.49 63.12 68.75 74.38	1.20 9.22 13.03 17.29 21.56 25.50 29.84 34.56 38.32 42.70 46.86 51.01 54.96 59.11	

Effective splice length (critical bolt) **

Effective splice length (both bolts) **

^{*} Nominal yield stress

^{**} Bolt gauge slipped at 35 ksi - data omitted

Table F.12. Results of 72 Inch Bending Test: Marion 3 1b/ft - 80 ksi Post; 4 Inch Face to Face Splice in Non-critical Configuration (Calibrated Bolts).

		*****			*****			BE	NDING TE	EST		
Dis	st to bo	olt A (i rain ga) n) uge (in)	9.00		MARION 3 lb/ft post - 80ksi * Face to face splice Non-critical orientation						
LOAD							LOADS ps) Bolt B		AIN (auge //in) Calc	STRE (ks Base		
DL 60 60 32 92 32 124 32 156 32 284 32 316 16 332 16 348 16 364 16 380 16 396 16 412	-0.351 -0.292 -0.526 -0.643 -0.766 -0.915 -1.089 -1.479 -1.691 -1.923 -2.033 -2.134 -2.240 -2.337 -2.441	-1.424 -1.224 -1.131 -1.044 -0.950 -0.851 -0.755 -0.653 -0.541 -0.358 -0.275 -0.218 -0.163 -0.100 -0.039	2.235 2.226 2.308 2.738 2.938 3.133 3.345 3.577 3.815 4.038 4.275 4.520 4.646 4.760 4.877 4.985 5.099 5.245 5.360	0.89 0.42 0.45 0.50 0.51 0.50 0.54 0.57 0.31 0.29 0.28 0.26 0.36 0.36	0.89 1.31 1.73 2.18 2.68 3.19 3.69 4.23 4.79 5.10 5.39 5.67 5.93 6.57 6.89	2.70 2.59 3.03 3.25 3.48 3.76 4.08 4.47 4.81 5.21 5.65 5.85 6.04 6.24 6.62 6.62 7.08	4.19 4.00 3.61 3.42 3.25 3.06 2.87 2.68 2.47 2.25 2.03 1.89 1.73 1.50 1.38 1.26 1.14	0.041 0.309 0.434 0.555 0.687 0.832 0.980 1.119 1.267 1.419 1.569 1.642 1.780 1.780 1.780 1.943	0.041 0.293 0.427 0.561 0.696 0.830 0.964 1.099 1.233 1.368 1.435 1.502 1.569 1.636 1.704 1.771	51.91 57.54 60.36 63.17 65.99	1.23 9.27 13.01 16.65 20.61 24.95 29.40 33.57 38.00 42.58 44.93 47.06 49.25 51.27 53.40 56.13 58.28	

Effective splice length (critical bolt) 4.1 in

Effective splice length (both bolts) N/A

Table F.13. Results of 72 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 5 Inch Back to Back Splice in Critical Configuration (Calibrated Bolts).

Dis Dis	ice length (in) t to bolt A (in t to strain gau ent arm (in)	ı) uge (in)	1.38 10.25	BENDING TEST MARION 3 LB/FT POST - 80 ksi * Back to back splice Critical orientation						
LOAD (lbs)	 Ch.#1 Ch.#2 (mV) (mV)	Ch.#3 (mV)	Tip Defl (in)	Total Defl (in)	BOLT (ki Bolt A		STR At G (uin Obs.	auge	STRE (ksi Base	
tight DL 60 60 32 92 32 124 32 156 32 188 32 220 32 252 32 284 32 316 32 348 32 348 32 349 32 412 32 444 32 476 32 508 32 540	-0.741 -0.628 -2.413 -2.146 -2.399 -2.156 -2.343 -2.141 -2.344 -2.127 -2.334 -2.119 -2.323 -2.115 -2.311 -2.119 -2.295 -2.140 -2.277 -2.250 -2.253 -2.357 -2.231 -2.460 -2.207 -2.575 -2.182 -2.716 -2.146 -2.861 -2.121 -3.016 -2.088 -3.183 -2.058 -3.323 -2.015 -3.449 -1.979 -3.599 -1.961 -3.670	1.762 1.764 1.838 2.258 2.492 2.709 3.145 3.383 3.625 3.851 4.083 4.309 4.533 4.794 5.039 5.323 5.557 5.839 6.113 6.240	0.00 0.80 0.39 0.35 0.41 0.43 0.40 0.41 0.42 0.42 0.41 0.56 0.52 0.58		2.56 2.54 2.46 2.46 2.43 2.41 2.39 2.36 2.32 2.25 2.25 2.16 2.12 2.07 2.03 1.96	2.39 2.40 2.38 2.36 2.34 2.34 2.38 2.55 2.72 2.88 3.06 3.28 3.51 3.75 4.01 4.23 4.43 4.67	0.039 0.301 0.446 0.582 0.722 0.853 1.002 1.152 1.293 1.438 1.579 1.718 1.881 2.033 2.210 2.356 2.532	0.039 0.290 0.424 0.558 0.692 0.826 0.960 1.093 1.227 1.361 1.495 1.629 1.763 1.897 2.031 2.164 2.298 2.432	1.90 12.46 18.10 23.74 29.37 35.01 40.64 46.28 51.91 57.55 63.18 68.82 74.45 80.09 85.73 97.00 102.63	1.17 9.02 13.39 17.45 21.66 25.60 30.05 34.57 38.80 43.13 47.36 51.54 56.42 61.00 66.31 70.68 75.96 81.08

Effective splice length (critical bolt) ** in

Effective splice length (both bolts) ** in

^{*} Nominal yield stress

^{**} Bolt gauge nearing end of life - data omitted

Table F.14. Results of 72 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 5 Inch Nested Splice in Critical Configuration (Calibrated Bolts).

								BEN	DING TES	ST		
Dist	ice lengt t to bolt t to stra	t A (in)	1.38		MARION 3 LB/FT POST - 80 ksi * Nested splice						
•	ent arm	_	-						al orie			
! 						BOLT	LOADS	STR	AIN	STRE	SS	
LOAD				Tip	Total	(ki	ps)	At G	auge	(ksi	.)	
(lbs)	Ch.#1	Ch.#2	Ch.#3	Defl	Defl	Bolt	Bolt	(uin	/in)	1	0bs @	
App Tot	(mV)	(Vm)	(Va)	(in)	(in)	A	В	Obs.	Calc.	Base	Gauge	
floor	-0.784 ·	-0.548	2.034									
tight	-2.985 -	-2.982	2.007			3.32	3.82			1		
DL	-2.786	-2.895	2.092	0.00	0.00	3.02	3.69	0.039	0.039	1.90	1.17	
60 60	1-2.627 -	-2.935	2.496	0.75	0.75	2.78	3.75	0.291	0.287	12.46	8.72	
T .	-2.542 -		2.709	0.41	1.16		3.77	0.423	0.420	18.10	12.70	
	-2.461 -		2.917	0.41	1.57		3.80	0.553	0.552	,	16.59	
I.	-2.391 -		3.126	0.42	1.99	2.42	3.82	0.683	0.684	29.37	20.50	
1	-2.333 -		3.317	0.38	2.37	•	3.87	0.802	0.817	35.01	24.07	
	1-2.272 ·		3.547	0.47	2.84		3.95	0.946	0.949	•	28.37	
	-2.242		3.761	0.44	3.28	2.20	4.04	1.079	1.081	46.28	32.37	
•	-2.212		4.009	0.51	3.78	2.15	4.16	1.233	1.213	51.91	37.00	
,	-2.192		4.209	0.42		2.12	4.24		1.346		40.74	
1	-2.173		4.468	0.52	4.73	•	4.42		1.478	63.18 68.82	45.58	
	-2.167 -2.155		4.706 4.954	0.53	5.25 5.77	2.09 1 2.07	4.57 4.73	1.668	1.610 1.743	74.45	50.03 54.67	
	-2.133 · -2.149 ·		5.217	0.52	6.34	•	4.73	1.022	1.743	1 80.09	59.58	
1	-2.149 -2.152		5.461	0.57	6.88	1 2.06	5.05	2.138	2.007	85.73	64.14	
1	-2.153		5.713	0.57	7.45	1 2.07	5.24	2.295	2.139		68.85	
	-2.161		5.938	0.54	7.98		5.38	1 2.435	2.272	97.00	73.06	
•	-2.172		6.229	0.69	8.67		5.58	2.617	2.404	102.63	78.50	

Effective splice length (critical bolt) ** in

Effective splice length (both bolts) ** in

^{*} Nominal yield stress

^{**} Bolt gauge nearing end of life - data omitted

Table F.15. Results of 72 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 5 Inch Face to Face Splice in Critical Configuration (Calibrated Bolts).

Splice length (in) Dist to bolt A (in) Dist to strain gauge (in) Moment arm (in)	. 1.88 10.50	BENDING TEST MARION 3 LB/FT POST - 80 ksi * Face to face splice Critical orientation						
(lbs) Ch.#1 Ch.#2 Ch.#3	Tip Total Defl Defl (in) (in)	Bolt Bolt	STRAIN At Gauge (uin/in) Obs. Calc.	STRESS (ksi) Obs @ Base Gauge				
floor 1.105	0.43	1.88 2.97 1.68 3.12 1.50 3.29 1.32 3.46 1.17 3.66 1.04 3.85 0.92 4.08 0.80 4.31 0.70 4.59 0.59 4.91 0.52 5.22 0.43 5.55 0.40 5.70	0.040 0.040 0.291 0.288 0.426 0.420 0.561 0.553 0.692 0.685 0.826 0.817 0.947 0.949 1.079 1.082 1.209 1.214 1.341 1.346 1.467 1.479 1.585 1.611 1.733 1.743 1.763 1.809 1.827 1.875 1.896 1.942	1.90 1.20 12.54 8.73 18.21 12.79 23.89 16.83 29.56 20.77 35.23 24.79 40.91 28.40 46.58 32.38 52.26 36.27 57.93 40.23 63.61 44.02 69.28 47.56 74.96 52.00 77.79 52.90 80.63 54.81 83.47 56.88				

Effective splice length (critical bolt) 5.1 in

Effective splice length (both bolts) N/A

^{*} Nominal yield stress

Table F.16. Results of 72 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 5 Inch Back to Back Splice in Non-critical Configuration (Calibrated Bolts).

								BEN	DING TES	T	
Dist	ice lengt t to bolt t to stra ent arm (A (in in gau) ge (in)	1.75 10.25	MARION 3 LB/FT POST - 80 ksi * Back to back splice Non-critical orientation						
					BOLT	LOADS	STR	AIN	STRE	SS	
LOAD			1	Tip	Total	(ki	,	At G		(ksi	-
(lbs)		Ch.#2	Ch.#3	Defl	Defl	Bolt	,	(uin		_	0bs @
App Tot	(Vm)	(mV)	(mV)	(in)	(in)	A	В	Obs.	Calc.	Base	Gauge
floor tight DL 60 60 32 92 32 124 32 156 32 188 32 220 32 252 32 252 32 316 32 348	-0.789	2.551 2.504 2.492 2.484 2.475 2.470 2.465 2.465 2.462 2.453 2.446	-0.375	0.41 0.41 0.40 0.41 0.44 0.43 0.43	0.00 0.70 1.08 1.49 1.89 2.69 3.13 3.56 3.99 4.41	2.49 2.36 2.31 2.28 2.25 2.23 2.22 2.21 2.20 2.20 2.21 2.24	2.99 2.99 2.98 2.96 2.95 2.95 2.93 2.93 2.91 2.90 2.88	0.039 0.296 0.429 0.570 0.709 0.842 0.979 1.127 1.271 1.417	0.039 0.292 0.426 0.561 0.696 0.830 0.965 1.100 1.234 1.369 1.504	1.90 12.52 18.18 23.85 29.51 35.18 40.84 46.50 52.17 57.83 63.50	1.17 8.87 12.87 17.11 21.26 25.26 29.38 33.82 38.12 42.52 46.61
	-2.449 -			0.40	4.81	2.38	2.87	1.683	1.638	69.16	50.48
	-2.596 -			0.49	5.29	2.60	2.84	1.833	1.773	74.83	54.98
,	12.749 -			0.44	5.73	2.83	2.80	1.967	1.908 2.042	80.49 86.15	59.00 62.85
32 476	-2.873 - -3.012 -			0.44	6.17 6.64	3.02	2.76 2.72	2.093	2.042		66.93
	(-3.131 -			0.53	7.17	3.41	2.72	1 2.380	2.312	97.48	71.41
•	-3.282 -			0.69	7.86	3.63	2.58	2.567	2.446	103.15	77.00

Effective splice length (critical bolt) ** in

Effective splice length (both bolts) ** in

^{*} Nominal yield stress

^{**} Bolt gauge nearing end of life - data omitted

Table F.17. Results of 72 Inch Bending Test: Marion 3 lb/ft - 80 ksi Post; 5 Inch Nested Splice in Non-critical Configuration (Calibrated Bolts).

Dis Dis	ice length (in) t to bolt A (in t to strain gau ent arm (in)	n) ige (in)	1.38		BENDING TEST MARION 3 LB/FT POST - 80 ksi * Nested splice Non-critical orientation						
LOAD (1bs) App Tot	 Ch.#1 Ch.#2 (mV) (mV)	Ch.#3 (mV)	Tip Defl (in)	Total Defl (in)	(ki	LOADS ps) Bolt B	At G	AIN auge /in) Calc.	STRE (ksi Base		
tight DL 60 60 32 92 32 124 32 156 32 188 32 220 32 252 32 284 32 316 32 348 32 380 32 412 32 444 32 476 32 508 32 540 32 572 16 588	-0.804 -0.597 -1.735 -1.805 -1.715 -1.668 -1.856 -1.523 -1.920 -1.461 -1.973 -1.405 -2.040 -1.360 -2.096 -1.323 -2.187 -1.303 -2.274 -1.286 -2.356 -1.274 -2.458 -1.265 -2.530 -1.260 -2.635 -1.258 -2.747 -1.262 -2.858 -1.268 -2.747 -1.262 -2.858 -1.268 -2.979 -1.280 -3.309 -1.318 -3.319 -1.344 -3.369 -1.364 -3.432 -1.383	-0.582 -0.794 -1.014 -1.228 -1.420 -1.627 -1.755	0.42 0.47 0.50 0.51 0.49	0.00 0.76 1.17 1.55 1.96 2.39 2.82 3.26 3.67 4.13 4.49 4.93 5.34 5.31 6.31 7.83 8.16 8.48	1.40 1.37 1.59 1.68 1.76 1.86 1.95 2.09 2.22 2.34 2.50 2.60 2.76 2.93 3.10 3.28 3.45 3.62 3.79 3.87 3.96	1.90 1.68 1.46 1.36 1.27 1.20 1.14 1.11 1.08 1.06 1.05 1.04 1.04 1.05 1.07 1.10 1.13 1.17 1.17 1.21 1.21	0.680 0.817 0.956 1.097 1.227 1.370 1.483 1.615 1.741 1.873 2.010 2.143 2.263 2.392 2.471	0.039 0.290 0.424 0.558 0.692 0.826 0.960 1.094 1.228 1.362 1.496 1.630 1.764 1.898 2.032 2.166 2.300 2.434 2.568	1.90 12.46 18.10 23.74 29.37 35.01 40.64 46.28 51.91 57.55 63.18 68.82 74.45 80.09 85.73 91.36 97.00 102.63 105.45 108.27	1.17 8.74 12.61 16.33 20.39 24.50 28.68 32.91 36.81 41.10 44.50 44.50 64.29 67.88 71.75 74.14 76.40	

Effective splice length (critical bolt) ** in

Effective splice length (both bolts) ** in

^{*} Nominal yield stress

^{**} Bolt gauge nearing end of life - data omitted

Table F.18. Results of 72 Inch Bending Test: Marion 3 1b/ft - 80 ksi Post; 5 Inch Face to Face Splice in Non-critical Configuration (Calibrated Bolts).

								BEN	DING TES	T		
Dist	to bol	t A (in ain gau) ge (in)	1.38 9.81		MARION 3 LB/FT POST - 80 ksi * Face to face splice Non-critical orientation						
Moment arm (in)72.38 							LOADS ps) Bolt	STR At G (uin	AIN auge	STRESS (ksi) Obs @ Base Gauge		
floor tight DL 60 60 32 92 32 124 32 156 32 288 32 252 32 284 32 316 32 348 32 380 32 412 16 428 16 444 16 460 16 476	1.084 0.522 0.657 0.318 0.136 -0.041 -0.385 -0.574 -0.767 -0.949 -1.139 -1.327 -1.511 -1.736 -1.825 -1.950 -2.026 -2.118	0.765 0.136 0.467 0.604 0.641 0.668 0.694 0.713 0.754 0.759 0.761 0.763 0.760 0.761 0.761 0.761 0.761	0.791 0.745 0.816 1.244 1.463 1.681 1.898 2.107 2.345 2.582 2.816 3.045 3.264 3.472 3.730 3.836 3.980 4.072 4.194 4.324	0.00 0.88 0.45 0.44 0.44 0.43 0.48 0.47 0.49 0.48 0.47 0.46 0.58 0.25 0.34 0.31	0.00 0.88 1.33 1.76 2.20 2.63 3.11 3.58 4.07 4.55 5.02 5.48 6.06 6.31 6.65 7.15 7.46	1.05 0.80 1.44 1.78 2.11 2.44 2.76 3.47 3.81 4.17 4.52 4.87 5.29 5.69 5.69 5.69	1.25 0.59 0.32 0.25 0.19 0.14 0.10 0.06 0.02 0.01 0.01 0.01 0.01 0.01	0.040 0.307 0.443 0.579 0.714 0.844 0.993 1.140 1.286 1.429 1.565 1.695 1.856 1.922 2.011 2.069 2.126	0.040 0.288 0.421 0.554 0.687 0.819 0.952 1.085 1.217 1.350 1.483 1.615 1.748 1.814 1.881 1.947 2.013 2.080	1.90 12.46 18.10 23.74 29.37 35.01 40.64 46.28 51.91 57.55 63.18 68.82 74.45 77.27 80.09 82.91 85.73	1.20 9.20 13.29 17.37 21.41 25.33 29.78 34.21 38.58 42.86 46.96 50.84 55.67 57.65 60.34 62.06 64.34 66.77	

Effective splice length (critical bolt) 5.4 in Effective splice length (both bolts) 5.4 in

^{*} Nominal yield stress