

PUBLIC ROADS

A JOURNAL OF HIGHWAY RESEARCH



UNITED STATES DEPARTMENT OF AGRICULTURE
BUREAU OF PUBLIC ROADS



VOL. 10, NO. 2



APRIL, 1929



HUTCHINSON RIVER PARKWAY IN THE PARK SYSTEM OF WESTCHESTER COUNTY, NEW YORK

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U. S. DEPARTMENT OF AGRICULTURE

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R. E. ROYALL, Editor

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PARKWAY FEATURES OF INTEREST TO THE HIGHWAY ENGINEER

Reported by E. W. JAMES, Chief, Division of Design, United States Bureau of Public Roads

CONDITIONS responsible for the conception of the superhighway have led also to the use of the parkway to make possible the rapid movement of light-weight vehicular traffic through congested areas. Such developments have usually been in metropolitan and suburban areas; but the inherent possibilities of the parkway are so great that the Bureau of Public Roads considered it desirable to make an examination of some of the more important constructions within convenient distances of Washington with a view to analyzing the features that are of special interest to the engineer.

The parkway can serve a twofold purpose when adequately handled: It may be made to provide at the same time a park, in its proper sense, and an arterial highway. The two objectives, however, conflict to some degree and an even balance must be struck to

Undoubtedly the outstanding parkway developments are in the New York metropolitan district, where Palisade Interstate Park, Bear Mountain Park, the Bronx Parkway, and the Westchester County park system furnish a variety of detail nowhere else available in the Eastern States. The condition of improvement of the Bronx Parkway, New York City, and the Westchester County park system make these two areas of peculiar interest, and they may well be considered together as they are contiguous in location, largely identical in conception and purpose, continuing to a large extent in administration, and identified by similar influences on design and success in execution.

From the first contacts the wisdom of the design and the satisfying quality of the work are apparent and impressive. This feeling is intensified when opportu-



SEPARATION OF HIGHWAY GRADES IN THE BRONX RIVER PARKWAY

secure the most satisfactory results. Vistas are generally short, especially in lateral directions, and landscaping as a park feature must be done accordingly. This requires taking advantage of many small details that might be developed in a bolder manner in ample park areas. The highway itself must be considered constantly in order that the capacity of the parkway as a means of traffic relief may be maintained.

OUTSTANDING PARKWAY FEATURES SUMMARIZED

These observations are the result of inspections of several parks and parkways, where it was possible to see, completed and in operation, parkway features and designs that are entirely satisfactory from both an artistic and technical viewpoint, and also to see others, likewise completed, that demonstrate the disadvantages of certain details.

nity is found to observe, as later it was by the writer in Boston and vicinity, other parkways destined to the same general purpose, planned along the same generous and widespread layout, and detailed in such a manner as to be adequate for service but quite undistinctive as parkways.

The principal incentive to development of the big system of parks and parkways in Westchester and the Bronx, apart from the relatively minor impulse due to the need of renovating the lower reaches of the Bronx River in upper New York City, as the city extended beyond the Harlem River, was the need for additional traffic arteries leading out from the New York metropolitan area into the only contiguous mainland available for suburban development. The intensity of this incentive may be somewhat measured by the alternatives of using bridges or tunnels on the East and Hudson

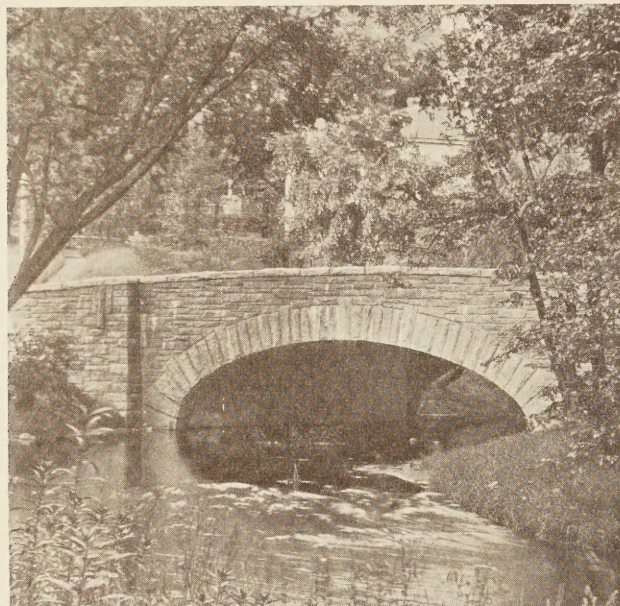
Rivers, or the inherently inadequate ferries across a normally more or less crowded harbor.

The fact that essentially the Bronx and Westchester Parkways were conceived and have so far been executed as relief highways to a great metropolitan area is notable. The cleaning up following the completion of the great Bronx River Valley trunk sewer opened the way to elevating such needed highways into parkways, and the success with which the idea has been carried out is an example for all such work.

The completed part of the system, although but a quarter of the whole proposed system, is large enough and old enough to furnish evidence of sound design.

Certain outstanding features may be conveniently and briefly summarized:

(a) The parkway is developed from the interior outward rather than from the margins inward. This is fundamentally important.



(i) Bridge and structure designs are rustic and unsymmetrical and made to fit the situation.

(j) The flat arch has been developed satisfactorily and attractively, and has been used in the solution of many difficult grade separation problems.

(k) Watercourses are cleaned, cleared, and controlled by judicious dredging and filling and by the use of small, inexpensive weirs.

(l) Tangents are avoided in the pavement layouts.

(m) Deep cuts are avoided and grades follow the surface. Earth necessary for fills is obtained by widening cuts and flattening slopes in cut. To reduce fills curvature is introduced.

PARKWAYS SHOULD BE LOCATED IN INTERIOR OF PARKS

By placing the highway development in the interior of the parkway area and working outward, all possible freedom in details of location is secured, and what is of



BRIDGES OVER THE BRONX RIVER IN THE BRONX RIVER PARKWAY

(b) Intersections at grade with other traffic lines of all kinds are eliminated.

(c) Access or approach roads, ramps, and border roads are brought into the parkway sparingly. The parkway is not intended to be just another local avenue or street.

(d) A single 40-foot pavement is considered and apparently is adequate for all traffic so far developed under the limitations of the parkway regulations.

(e) Two 20-foot pavements segregating traffic, with a parking between, are not adequate. Apparently two 30-foot pavements are needed to equal a single 40-foot pavement in capacity.

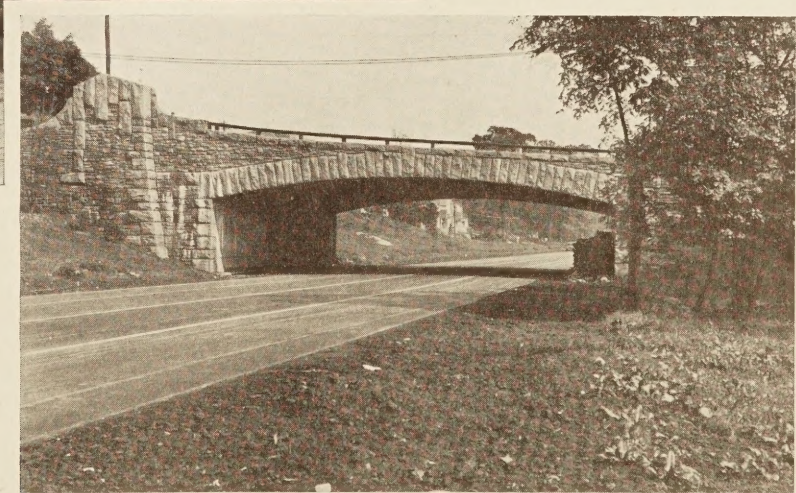
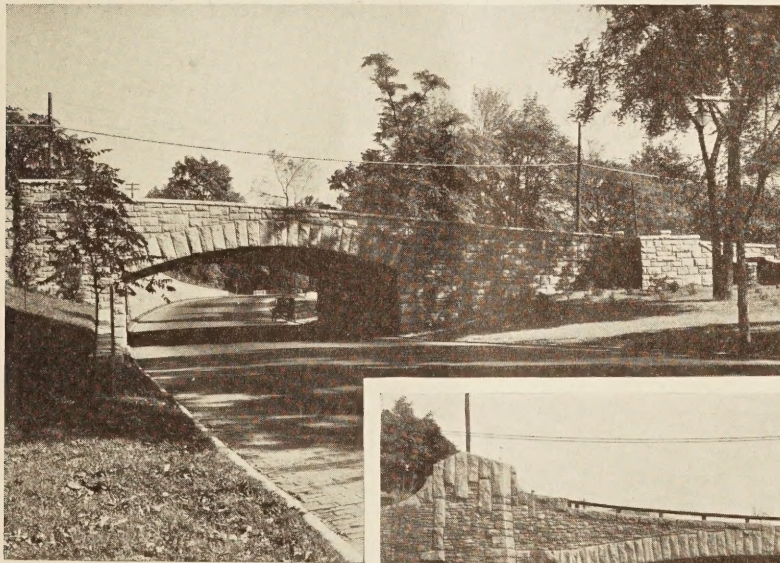
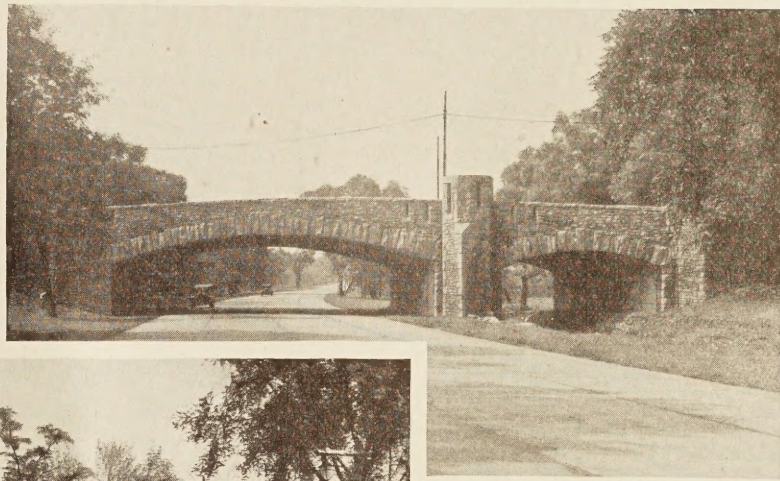
(f) Landscaping, finishing, planting, and opening to the public follow as rapidly as construction conditions permit. Completed sections are built from the rough in two seasons.

(g) All formal and studied landscaping is avoided. More local trees and shrubs, taken from the adjacent woods and reset, are used than nursery stock.

(h) Local stone is used in structures to a great extent, and unevenness of texture, color, and coursing, rather than evenness and regularity, are sought.

most importance, there is available on both sides of the roadway ample space for landscape development necessary to screen and hide any objectionable or unsightly features adjacent to the parkway. Such screening is essential along a parkway laid out through city suburbs, along railroads, and through small towns that invariably have purlieus that are unattractive. In addition, the interior development of the parkway encourages its separation from the rest of the highway and street net in the vicinity. The relative advantages of the two general methods of interior and marginal development, respectively, are seen by comparing the Bronx and Westchester developments with the metropolitan park system around Boston where the marginal system of designing prevails.

The metropolitan park system is comparable in size, conception, and purpose with the Bronx and Westchester systems. Starting with a sanitary clean-up of the lower reaches of the Fenway, a sluggish marsh estuary, outlet of a small brook from Jamaica Pond, the system has spread to include an area comparable with Westchester County. The marginal scheme of development has been unfortunately used to a large



FLAT ARCH BRIDGES USED FOR SEPARATION OF HIGHWAY GRADES, WESTCHESTER COUNTY, N. Y.

extent, with the disadvantages that are associated with it. As a result, the drives become the frontage streets for miles of private property. A large number of private driveways debouch directly into the park drives; for miles there is only a nominal distinction between the parkway and an ordinary avenue. There are numerous points where it has been impossible to screen from view objectionable property abutting the parkways.

On the other hand, in the Bronx and Westchester systems there is room for screening, and with the exception of a few hundred feet at one point the park driveway never serves as a frontage street to private property. Also, the distance from the right-of-way lines where interior development is used facilitates the separation of intersecting routes.

HIGHWAY INTERSECTIONS AT GRADE OBJECTIONABLE

The original policy of the Westchester County Park Commission with regard to intersecting routes has been greatly strengthened. At first they eliminated only the most dangerous grade intersections. Those remaining became such obstacles to traffic that the commission has removed all such intersections. Their policy now is to leave no grade intersection whatever, but at all principal highway grade separations ramps between the two arteries furnish a connection. This is unquestionably sound and emphasizes the superhighway idea which was the strongest impulse toward the creation of the parkway system.

The disadvantage of unseparated highway intersections was noted definitely at many points in Fairmont Park, Philadelphia. Traffic police, automatic signal control, and objectionable intersections are there numerous. The inadequacy of the design of earlier days is apparent, and one is left with the conviction that there should be not the slightest hesitation to abandon the older ideas for new details that promise to serve better the demands of present traffic.

In the matter of access roads the arterial highway aspect is also fully recognized in the Westchester park system. Access to the parkway is provided at rather long intervals; by no means at every street intersection. In some instances the intervals are a mile or more in length. If abutting development requires it, a separate border road or street is constructed on which development faces, distinct entirely from the parkway and having access to the park drive only at long intervals.

This condition is in marked contrast with the design and development of Roosevelt Boulevard northward from Philadelphia.

This boulevard clearly indicates what should be avoided in parkway design. To the city line the parkway consists of two 20-foot or two 30-foot pavements with a separating parked strip of approximately uniform cross section throughout. At the present time traffic uses the east-side pavement only for a considerable distance because of the bad condition of the west side

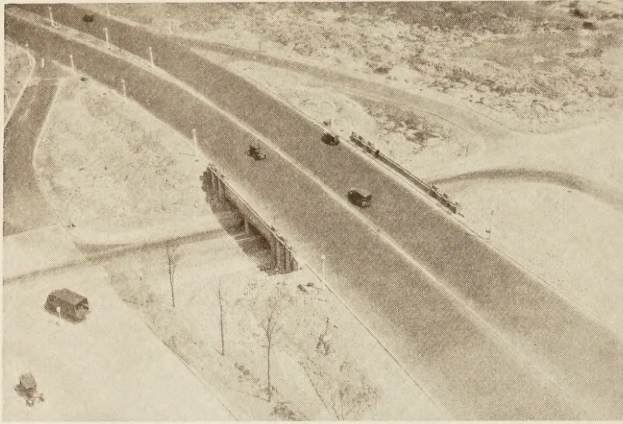


AIRPLANE VIEW OF ROOSEVELT BOULEVARD, PHILADELPHIA, SHOWING FREQUENT STREET INTERSECTIONS AT GRADE



PARKWAYS CONSTRUCTED BY THE PARKS DIVISION OF THE METROPOLITAN DISTRICT COMMISSION OF MASSACHUSETTS.
UPPER—WOBURN PARKWAY NEAR WOBURN. LOWER—MYSTIC VALLEY PARKWAY NEAR MEDFORD

With the exception of a few important railroad grade-crossing eliminations, the entire boulevard is at the same grade as the streets of the subdivisions rapidly opening to the north of Broad Street, and the continued interruption to traffic promised by this design will in a few years ruin the parkway as an arterial route. It will become an elaborate city street and nothing more.



SEPARATION OF HIGHWAY GRADES IN LINCOLN PARK, CHICAGO

Estimates of the probable traffic capacity of a pavement should be modified where the layout affords relative freedom from direct intersections. With few access roads and grades separated at all main intersections, the observations stated under (d) are believed to be sound. With the four to five million people and 600,000 automobiles of New York City as a principal source of traffic, and with a highly developed suburban territory adjacent to much of the system, the Westchester commission finds the 40-foot drive generally adequate. Two 20-foot pavements, however, do not serve the peak traffic; and where the traffic lanes are separated by a parked strip, two 30-foot pavements are found to be the equivalent of a single 40-foot drive. In only a few sections, approaching resorts that are developed or to be developed, where traffic will be excessively concentrated, has the commission used or planned a 60-foot pavement.

DEFINITE PROVISION SHOULD BE MADE FOR PARKING VEHICLES

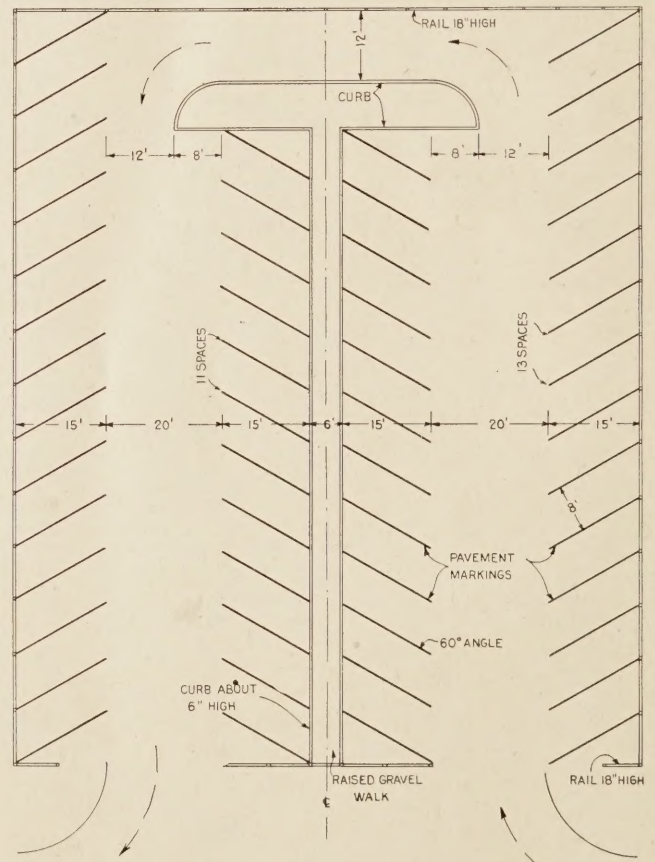
On Saturdays, Sundays, and holidays all parking of vehicles along the parkways, except at areas definitely provided, is absolutely prohibited and the regulation is enforced. Incidentally, luncheon parties are forbidden except at places provided. With these restrictions on vehicle parking during the days of peak traffic, the 40-foot pavement or the two 30-foot pavements adequately serve the traffic throughout most of the system.

Parking grounds for vehicles constitute a difficult problem for the parkway designer, because large areas, barren in appearance, add nothing of beauty to the parkway. Definite provision must be made for parking, however, if it is to be allowed. The design, layout, and construction of parking areas for motor vehicles in Valley Forge State Park, Pa., was observed as one of the distinctive features of this park.

The pathways which were noted between the parked vehicles added relatively little to the required parking area and furnished an element of safety and convenience. This feature would be particularly desirable in an expansion of the design to accommodate several hundred cars.

A sketch is shown of the smaller of the two areas seen, which gives the details and dimensions. Two such areas are located in Valley Forge Park, one to hold about 40 cars and the other about 90. Similarly, at Bear Mountain Park rather skillful use has been made of limited areas for vehicle-parking purposes. No fair judgment could be reached regarding the effect of parking areas on the congestion at the west end of Bear Mountain Bridge. There is a heavy traffic which naturally seeks access to the various roads from the bridge, and also a maneuvering of vehicles to get into and out of the irregular and scattered parking areas. But the need of such areas is obvious, and they should be located and their layouts studied with great care to insure freedom of access and ease of entrance and exit.

The circuitous approaches to the Bear Mountain Bridge, compelled by the topography, are in all cases to be avoided where possible and especially when in juxtaposition with parking areas. Their disadvantage is obvious to one driving over them.



LAYOUT OF AREA FOR VEHICLE PARKING IN VALLEY FORGE STATE PARK, PA.

LANDSCAPING AN IMPORTANT PROBLEM

The Westchester County Park Commission has found its work popularized and results expedited by landscaping and finishing the parkways with its own forces immediately after construction. In the heavy grading the slopes are not left with unsightly angles, but are flattened, so that the parkway forces can, with little additional work, ease them off naturally into the existing topography. Only in a few cases, where heavy fills have been unavoidable, is there any impression of outstanding or sharp construction lines. On the other hand, no effort is made to keep the slopes in a flat plane;

they are rounded, flattened, or worked into warped surfaces to match with the topography, maintaining only the general direction of slope required by drainage.

In the finishing, the local resources are used as much as possible. Trees, shrubs, wild flowers, and rock obtained from adjacent land in or without the parkways are used in appropriate ways. White birch trees, scattered through the woods, are taken up, reset, and grouped. Wild flowers are bedded in groups, and even the common sumach was observed as an especially good material for low screening purposes.

Local stone has been used for structures in preference to a better quality but more uniformly colored stone from other places. The variegations of the local stone are much preferred to the flat tones of even colored granite from the New England quarries within reach. Both stones have been tried and the commission now uses granite of uniform color only for copes, quoins, and other occasional trim, in which it contrasts pleasantly with the uneven and more roughly dressed local stone.

Besides using a material natural to the landscape setting, the structural designs are made to fit each location. Bridge copes are not always symmetrical; where the situation requires it one side is raised higher by steps to meet the topography. Flat surfaces are broken with pilasters and counterforts; exposed abutment faces under flat arches are paneled in different colors. Flat, stepped, battlemented, and random cope is freely used, often in the same structure, and the effect is pleasing. The flat arch, used originally to provide clearance at the sides, has been developed satisfactorily, and is unquestionably less tunnellike than circular arches.

(Continued on p. 32)



A FOOTBRIDGE AND SPILLWAY ON TIBBITS BROOK, WEST-CHESTER COUNTY, N. Y.



REINFORCED CONCRETE BRIDGE, BRONX RIVER PARKWAY, NEW YORK

A MACHINE FOR MOLDING LABORATORY SPECIMENS OF BITUMINOUS PAVING MIXTURES

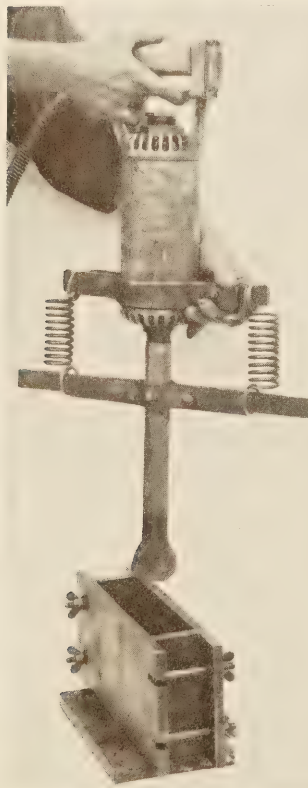
Reported by J. T. PAULS, Senior Highway Engineer, Division of Tests, Bureau of Public Roads

THE STABILITY of a pavement and the resistance of its surface to raveling are important factors under present-day traffic. Present methods of designing asphalt paving mixtures are not certain of producing these qualities. If the aggregate always conformed closely in size and grading to the so-called "standard" a mixture could be designed on the basis of past experience with a reasonable assurance that it would have sufficient stability and cohesion. Unfortunately, the grading, size, and character of aggregate available on different jobs are variable and the designs adopted are often lacking in stability or resistance to raveling.

It should be an important function of a bituminous laboratory to determine in advance of construction the best possible combination of the available aggregates, filler, and asphalt. The work being done in various laboratories in developing apparatus and tests for determining the stability of asphalt paving mixtures is an important step in this direction.

EARLY METHODS FOUND UNSATISFACTORY

In any laboratory test for stability the method of preparing the specimens is as important as the test itself. It should be such that uniform specimens of predetermined density can be prepared through a wide range of practical values. There should be no difference in the results secured by different operators.

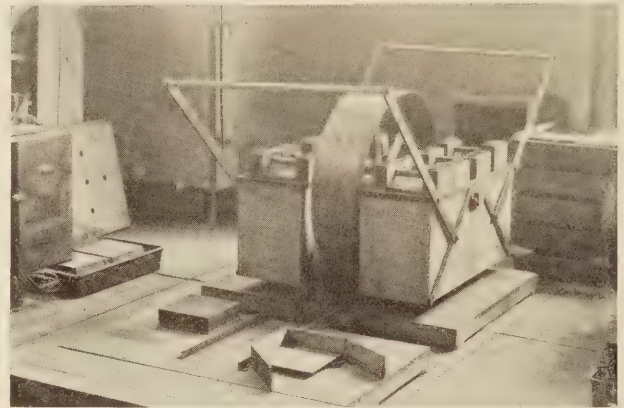


AN ELECTRIC HAMMER ARRANGED FOR MOLDING SPECIMENS 1 3/4" WIDE

In recent years the bureau has been making field and laboratory studies of the stability of bituminous mixtures. In the earlier laboratory work various methods of molding specimens were used, the earliest being a weighted roller. This machine was unsatisfactory because of the lack of uniformity in the molded specimen and difficulty of duplication.

Until recently the electric hammer has been used as illustrated for compacting specimens.¹ Although used for some time, this method was not satisfactory, because of the difficulty in duplicating specimens and in com-

pressing to a desired density and void content with reasonable accuracy. Molding by direct compression was unsatisfactory for the same reasons. It proved



AN EARLY MOLDING MACHINE OF THE ROLLER TYPE WHICH PROVED UNSATISFACTORY BECAUSE OF LACK OF UNIFORMITY IN THE SPECIMENS

very difficult to compact large specimens to the density found in road surfaces. Crushing of the stone particles often occurred in compacting the coarse-aggregate mixes to the higher densities.

NEW MOLDING MACHINE DESCRIBED

The illustrations and Figure 1 show a molding machine developed by the bureau during the last year. It was designed primarily for molding specimens for test in the roller stability machine,² but the specimens are suitable for other types of stability tests. The machine has decided advantages over apparatus formerly used for this purpose. Specimens of different mixtures can be molded under the same pressure and to the same density obtained in actual paving. Another equally important advantage is that specimens of desired density and void content can be prepared. This makes it possible to determine the sufficiency of rolling on any asphalt paving project by comparing the density obtained in the construction with the maximum density obtainable on molded specimens using the same materials and proportions. The operation of the machine is entirely mechanical, thereby eliminating the personal equation of the operator.

The machine is designed to duplicate the compressing and kneading action of the roller actually used in construction. For this reason a heavy unit load, exceeding that used in construction, is not required and crushing of the aggregate does not occur.

The machine is very simple in design. It consists essentially of a loading arm with a rocker arm attached, a collapsible steel box for holding the specimen, and a driving mechanism by which the box is moved backward and forward. The loading arm is an I-beam 8 feet long, pivoted at one end and loaded with lead weights at the other. The load is transmitted to the specimen by means of a rocker suspended 18 inches from the fixed end of the beam. The rocker is a built-up section faced with a segmental circular shoe 4 inches wide and 8 inches in length, having a radius of 18 inches.

¹A detailed description and the method of operation is given in PUBLIC ROADS, vol. 6, No. 4, June, 1925.

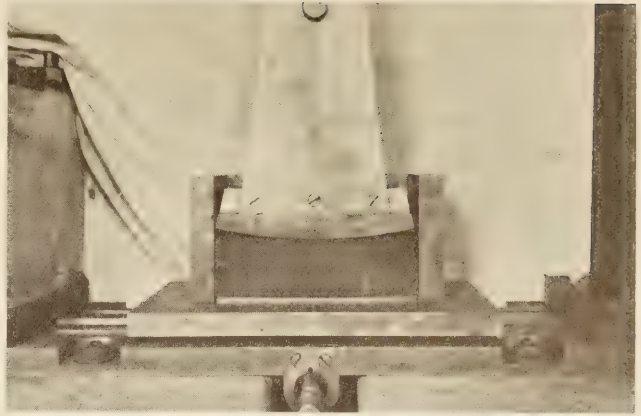
²This machine, which is described in PUBLIC ROADS, vol. 7, No. 10, December, 1926, was recently rebuilt to eliminate certain objectionable features found in the design illustrated.

The collapsible box, in which the specimen is formed, is of 1-inch machined steel plates and rests on a heavy steel plate, which is supported on ball-bearing races. To the bottom of this plate is attached a rack and pinion, which provides for the backward and forward movement of the box containing the specimen. Operation is by means of a hand wheel.

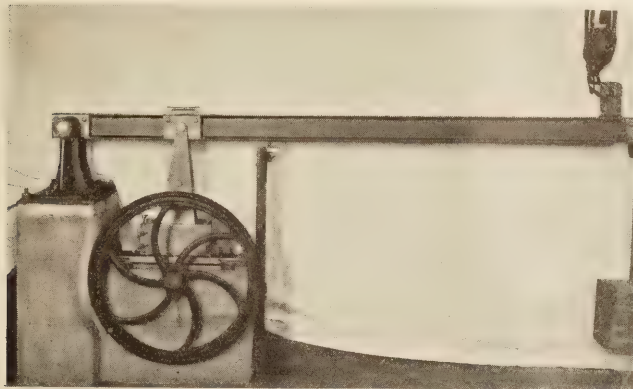
The vertical stop arrangement shown in contact with the arm is a rigidly fixed channel with an adjustable slow-motion screw at the top. This device not only regulates the thickness and density of the specimen but also insures parallelism of the top and bottom faces.

NEW MACHINE IS SIMPLE IN OPERATION

In molding a specimen, the necessary quantity of the mix (method of determination explained later) is heated

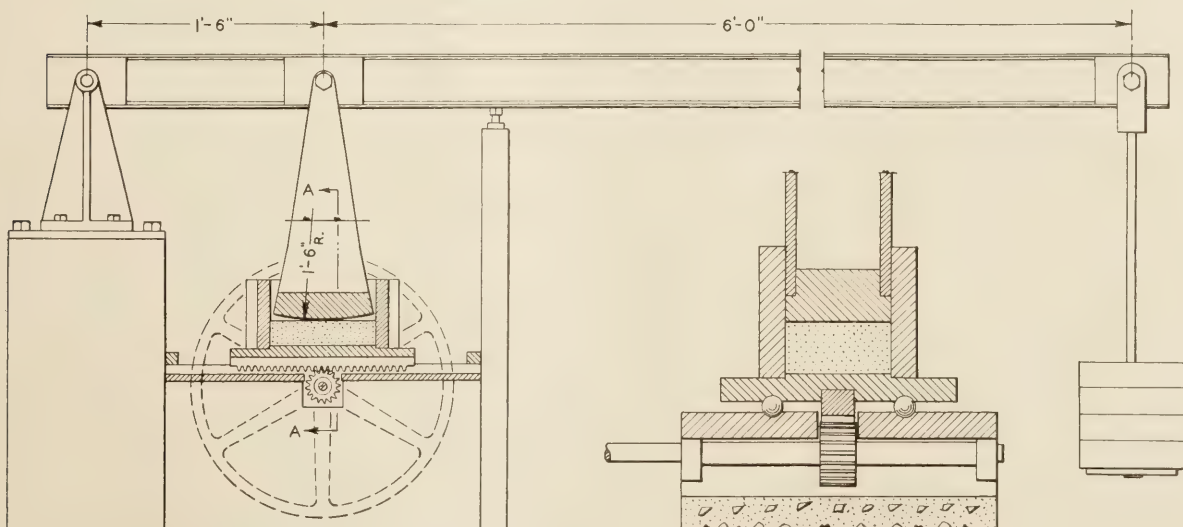
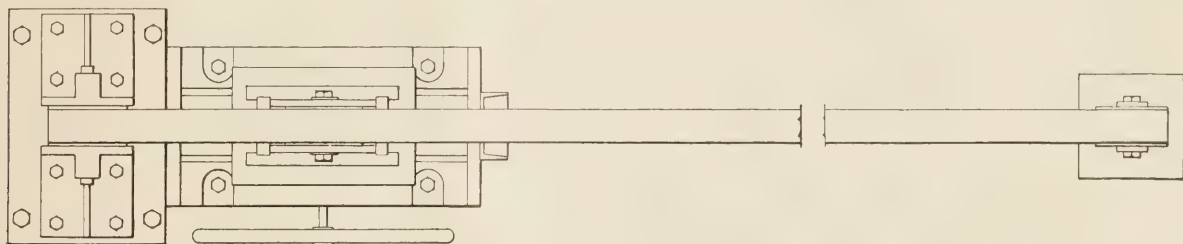


SIDE OF MOLDING BOX REMOVED TO SHOW MOLDED SPECIMEN



GENERAL VIEW OF NEW MACHINE

to the proper temperature and placed loosely and evenly in the mold. A steel plate is placed on top of the uncompact material to prevent its being squeezed upward at the ends during the initial compression. The rocker arm is lowered on the plate and the loading weights are applied at the end of the beam. The specimen is then rolled backward and forward for a period of about one minute. The plate is then removed and the rocker is again lowered. The process of rolling is continued until the stop, which has been set to give a specimen of the desired thickness, takes the load over the full length of travel, indicating that the desired compression has been obtained throughout and that the specimen is of uniform thickness. The time required to mold a specimen averages about five minutes



SECTION A-A

FIGURE 1.—DETAILED DRAWING OF NEW MACHINE FOR MOLDING ASPHALT MIXTURES

but varies somewhat, depending upon the nature and character of the mix and the compression desired. Any desired load may be used with a corresponding time of operation. In the work done up to this time, a load of 375 pounds per inch width of specimen has been used. This conforms closely to actual construction conditions and, so far, has proved satisfactory.

In preparing the mix to be molded the specific gravities of the materials are determined in the usual manner. From these values the maximum theoretical density of the mix in grams per cubic centimeter is calculated from the following equations in which all percentages are by weight.

In molding specimens of mixtures other than sheet asphalt equally satisfactory results are obtained. Table 2 gives the results secured in molding a bituminous concrete mix composed of three-fourths to

For sheet asphalt:

$$(1) \quad D_t = \frac{100}{\frac{\text{Percentage sand}}{\text{Sp. gr. sand}} + \frac{\text{Percentage filler}}{\text{Sp. gr. filler}} + \frac{\text{Percentage A. C.}}{\text{Sp. gr. A. C.}}}$$

For bituminous concrete:

$$(2) \quad D_t = \frac{100}{\frac{\text{Percentage stone}}{\text{Sp. gr. stone}} + \frac{\text{Percentage sand}}{\text{Sp. gr. sand}} + \frac{\text{Percentage filler}}{\text{Sp. gr. filler}} + \frac{\text{Percentage A. C.}}{\text{Sp. gr. A. C.}}}$$

Having determined the maximum theoretical density of the mix, the next step is to calculate the grams of mix necessary to make a molded specimen of a given height and void content. This is done as follows:

$$\text{Weight of mix in grams required} = A \times D_t \times C,$$

where A = the percentage of solid material in the specimen—i. e., 100 per cent minus percentage of voids—

D_t = the maximum theoretical density of the mix in grams per cubic centimeter,

C = volume of the molded specimen in cubic centimeters.

SPECIMENS PRODUCED OF SATISFACTORY UNIFORMITY AND OF DESIRED VOID CONTENT

Table 1 gives the actual void content obtained in molding specimens of a sheet asphalt, compared with the respective void contents desired. The results agree closely over the wide range of voids selected.

TABLE 1.—Comparison between desired percentage of voids and actual voids obtained

Sample No.	Desired voids	Actual voids obtained	Sample No.	Desired voids	Actual voids obtained
1	3.0	3.03	7a	7.0	7.18
2a	3.5	3.51	7b	7.0	7.18
2b	3.5	3.42	8a	8.0	7.98
3a	4.0	4.17	8b	8.0	8.13
3b	4.0	4.08	9a	9.0	9.05
3c	4.0	4.00	9b	9.0	9.02
4a	4.5	4.55	10a	10.0	10.14
4b	4.5	4.37	10b	10.0	9.98
5a	5.0	5.10	11a	11.0	10.90
5b	5.0	4.95	11b	11.0	10.65
6a	6.0	6.13	12a	12.0	12.26
6b	6.0	6.13	12b	12.0	12.32

one-eighth inch stone, sand, filler, and asphalt. These results are characteristic of those obtained on coarse aggregate mixtures. The actual voids within the specimens (excluding surface voids) are slightly lower than those planned except on specimen No. 1. This is probably due to the slight honeycombing of the surface of the specimen at the ends and sides.

In weighing the material for each of these specimens no allowance was made for the decreased amount of material required because of the surface condition. Since the machine formed specimens of the correct dimensions the material which should have filled the surface voids caused greater density in other portions of the specimen. Closer check results could no doubt be obtained by reducing the quantity of mix for each specimen to allow approximately for the surface voids.

TABLE 2.—Comparison of desired percentage of voids and actual voids obtained for specimens of asphaltic concrete. The mix contained 40 per cent stone between the three-fourths and one-eighth inch size

Sample No.	Desired voids	Actual voids obtained	Sample No.	Desired voids	Actual voids obtained
1	3	3.29	4a	6	5.62
2a	4	3.78	4b	6	5.58
2b	4	3.82	5a	7	6.24
2c	4	3.91	5b	7	6.54
3a	5	4.79	6a	8	7.90
3b	5	4.61	6b	8	7.16
3c	5	4.61			

There is a fairly wide difference between the maximum theoretical density and the maximum practical density under field conditions, particularly for the coarse-aggregate type mixes. Aggregate which is either soft and fragile or which is placed in an improperly designed mixture will crush under the roller before the maximum theoretical density is obtained. It is sometimes desirable to know the maximum practical density of a mix of this type and it is believed that the molding machine can be used to make this determination. As shown in Table 2, the voids obtained in specimen No. 1 exceeded the amount planned, indicating that a void content of 3 per cent is impractical for the particular materials and proportions used. As it was easily possible to reduce the voids to all percentages from 4 up it appears that the minimum practical void content for this mixture is between 3 and 4 per cent.

A comparison of the results obtained in molding specimens 2 by 4 by 8 inches in size by each of the three methods described is given in Table 3. The mix in each case was identical, consisting of 10 per cent

asphalt, 12 per cent dust, and 78 per cent sand by weight.

TABLE 3.—Comparative densities and voids obtained in molding specimens by different methods, using the same mix and same size specimens throughout

[Maximum theoretical density of the mix 2.308]

DIRECT COMPRESSION BY TESTING MACHINE

Pounds	Density	Voids
16,000	1.835	20.49
32,000	1.901	17.63
48,000	1.966	14.82
64,000	2.007	13.04
80,000	2.045	11.39
96,000	2.073	10.18
¹ 100,000	2.076	10.05

ELECTRIC HAMMER

Density	Voids
2.182	5.46
2.169	6.02
2.165	6.20
2.147	6.97

NEW MACHINE, USING LOAD OF APPROXIMATELY 375 POUNDS PER INCH OF WIDTH

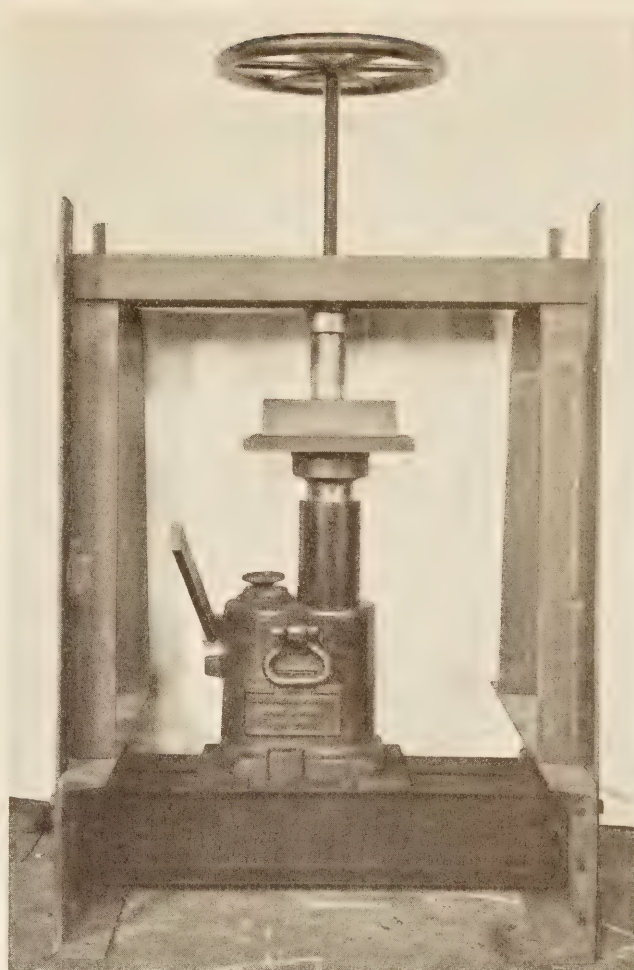
Density	Voids
2.218	3.90
2.217	3.94
2.216	3.99

¹ Limit of machine.

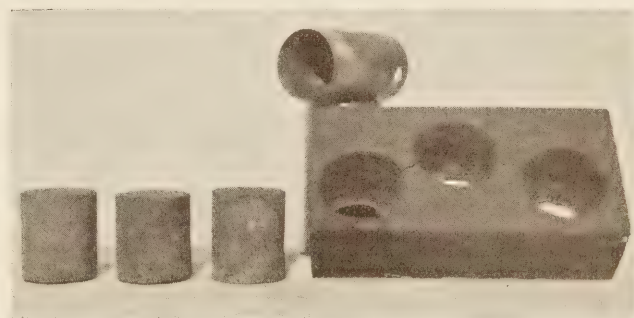
In molding under direct compression, using a universal testing machine, the total load varied from 16,000 to 100,000 pounds, equivalent to a unit load of 500 to 3,125 pounds per square inch. The voids obtained by this method ranged from 20.49 per cent for the light load to 10.05 per cent for the heaviest. These values greatly exceed those which are obtained in actual construction. With smaller specimens sufficiently low voids can be obtained by this method but where coarse aggregate is used, crushing often occurs particularly when using soft materials.

The results obtained with the electric hammer on a similar mix and for the same size of specimens show a variation in voids ranging from 5.46 to 6.97 per cent, which is about the minimum possible with this method and indicates the degree of uniformity obtainable by a single operator. In contrast to these results are those obtained with the new molding machine which check very closely.

Tests made on cores taken from newly laid sheet asphalt pavements in general showed higher voids in the top than in the bottom portion, while in the older pavements the reverse was found to be true. In the few cases studied, the specimens of sheet asphalt molded with the new molding machine had slightly higher density at the bottom than at the top (except at the corners), thus conforming with field experience. Table 4 shows the density at the lower corners to be materially lower than for the rest of the specimen. However, since the low density is confined to such a small portion of the specimen, which are tested in the same position in which they are molded, it will probably not greatly affect their value for test purposes.



PUNCHING CORES FROM SPECIMEN MOLDED IN NEW MACHINE



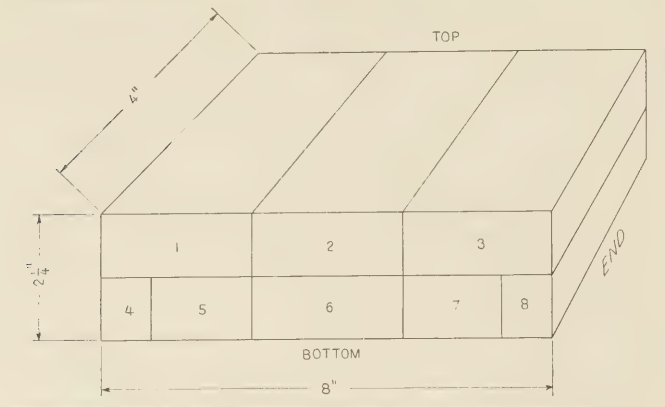
CORES PUNCHED FROM MOLDED SPECIMEN TO BE TESTED IN THE HUBBARD-FIELD MACHINE

MACHINE USEFUL FOR VARIOUS TESTS

The molding machine was developed primarily for preparing specimens of various types of paving mixtures for testing in the roller stability machine, but its use is not limited to that purpose. It has proved valuable in connection with the Hubbard-Field stability test on fine-grain mixtures. Three cores suitable for this test may be obtained from each of the molded specimens. The advantages of obtaining cores in this manner are that they are uniform in character and the density and voids can be controlled so that their effect and that of other factors may be readily studied. Illustrations show how cores for use in this test are taken from the molded specimens.

TABLE 4.—Showing variation in density of specimens molded with the new machine, using a mixture having a maximum possible density of 2.338

(Continued from p. 27)



Specimen	Density of specimen ¹	Density of the portions							
		Top				Bottom			
		1	2	3	4	5	6	7	8
1.....	2.187	2.192	2.192	2.193	2.052	2.198	2.194	2.190	2.013
2.....	2.189	2.194	2.187	2.199	2.055	2.191	2.198	2.179	2.031
3.....	2.173	2.188	2.193	2.189			2.194		
4.....	2.193	2.186	2.187	2.195	2.019	2.178	2.207	2.180	2.015
5.....	2.200	2.241	2.221	2.212		2.218	2.240		2.192

¹ No attempt was made to obtain maximum density.

In the design of types of surfacing, using bituminous materials applied cold, it is often desirable to make a preliminary study of the effect of such factors as character and quantities of bituminous material, grading, and size of aggregates, rate of hardening of the mix, etc. This can very often be done to advantage by molding specimens in the laboratory and observing their behavior.

It is not expected that this particular machine, as now designed, will prove adaptable to all the different types of stability test now used by different laboratories. However, it is believed that the principle of this machine is highly satisfactory and that with slight modifications its use can be widely extended and should prove a valuable adjunct to any bituminous laboratory.

INTERNATIONAL ASSOCIATION OF ROAD CONGRESSES ANNOUNCES ESSAY CONTEST

The following announcement is reprinted from the Bulletin of the Permanent International Association of Road Congresses:

The last triennial prize was awarded at the fourth congress, held at Seville, May, 1923. In accordance with the decisions taken, the 6th of September, 1926, and the 30th of June, 1928, by the Permanent International Commission, the next prize will be awarded during the sixth congress, which will be held in Washington in October, 1930.

This prize consists in the sum of 4,500 francs (approximately \$175).

The conditions for entering this competition are as follows:

(a) The jury will award the prize to the author of the most remarkable study or essay submitted for encouraging construction progress, maintenance, and exploitation of the road and for facilitating traffic.

(b) It is obligatory that the authors be members of the Permanent Association of Road Congresses for at least six months and their inscription can not be subsequent to March 1, 1920.

With all this departure from established engineering lines, always, of course, for the purpose of obtaining beautiful effects, the merely novel finds no satisfactory place. In two instances masonry bridges have been built with the outlines of suspension bridges, and these designs have resulted in nothing but deserved failure, admitted frankly by the commission's engineers as unfortunate mistakes.

The presence of a brook or small stream in a parkway is assuredly an asset from the point of beauty. By a very simple treatment of dredging, filling, and introducing small weirs, all shallows and marshy areas are at once eliminated, a clear demarcation set between water and dry land, and the stream lines are varied by broadening and contracting the channel.

A distinctive and very pleasing feature of Forest Park, Springfield, Mass., is the development of basins and the use of aquatic plants as well as land plants for pleasing effects. Even the common cat-tail, as well as delicate Egyptian and Phœnician lotus, is there used effectively.

The final points, (*l*) and (*m*), relating to tangents, curvature, and grading are important in their application to parkway construction. The constant rather sharp curvature in some places in Westchester is undesirable as observed, and the introduction of curvature is carried to extremes, certainly at some points. It has been done, doubtless, in the interests of landscaping. On the other hand, it requires no expert qualities to determine that long, unbroken tangents are ugly and undesirable except on an intended speedway. They are to be avoided rather than sought, and where used should be relieved by some vistas that convert them into attractions.

The widening of cuts excessively to get earth, instead of deepening them and of reducing fills by curvature, has the general effect of leaving the land largely unmarred and enables the landscape forces to disguise and conceal construction lines. Reducing the gradient of side slopes to angles below that of repose largely prevents slipping, washing, and weathering, and planting and growth of vegetation are facilitated.

The members of the Permanent International Commission are disqualified from entering this competition.

(c) The essays must be in the hands of the general secretary of the association in Paris, 1, Avenue d'Iena, before April 1, 1930.

If the essays are written in any language other than German, English, or French, the original must be accompanied by a good translation in any of the aforesaid languages.

(d) The essays, handwritten or typewritten, must bear a date, must not be signed, but bear a mark without the author's name. The surname, proper name, attributes, and domicile must be placed in a sealed envelope, with the aforesaid mark plainly written on it, and the whole sent to the general secretary in a registered envelope.

(e) The essay winning the prize will be published by and at the expense of the association under the terms fixed in the first article of the regulations.

In case this essay has already been published, the author shall give the associations, gratuitously, the necessary authorization.

The amount of the prize will be paid to the winner only after this publication, and 25 copies in each of the languages admitted by the association for its publications shall be placed at the disposal of the author.

With regard to the nonwinning manuscripts, the association reserves the right to publish them, partially or in extenso, under the conditions fixed in the first article of the regulations.

(f) The result of the competition shall be proclaimed at the meeting held by the Permanent International Commission at the opening of the Sixth International Congress of the Road (1930).

SOME ASPECTS OF FLOW OF WATER AROUND BENDS AND BRIDGE PIERS¹

By D. L. YARNELL, Senior Drainage Engineer, Bureau of Public Roads, U. S. Department of Agriculture

HYDRAULIC RESEARCHES on the flow of water around bends have been conducted for the last three years at the hydraulic laboratory of the University of Iowa by the university in cooperation with the Bureau of Public Roads. The investigation was undertaken to determine the laws governing the changes in pressure and velocity in different parts of a flowing stream as the moving water undergoes the transition from motion along a straight line to motion around a bend, and again as it undergoes the opposite transition back to a straight-line motion. This condition of transitional flow exists whenever water flows in a crooked channel or whenever moving water meets a bridge pier or any other form of obstruction.

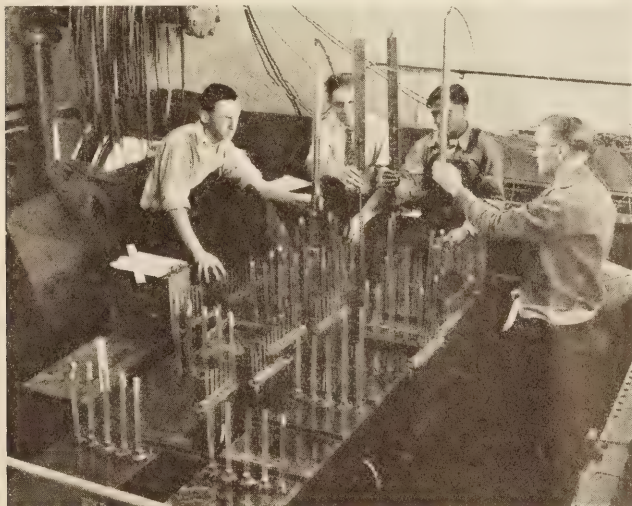


FIGURE 1.—DETERMINING VELOCITY DISTRIBUTION WITH PITOT TUBES

The apparatus for the tests consisted of a tank 5 by 5 feet in horizontal cross section and 8 feet deep, an approach channel 26 feet long leading from the tank to the bend, a 180° bend with a 5-inch inner radius, and a discharge channel 30 feet long. The bend and the two channels were 10 inches square.

The bend and 8 feet of each of the approach and discharge tangents next to the bend were made of transparent material so that studies might be made of the direction of flow of various particles of water in moving around the bend. A small steel frame, 10 inches square, was built and lined with transparent pyralin, or celluloid. Some 300 piezometric connections were made in the apparatus so as to study the changes in pressure as the water flows around the bend. A comparison of velocities at various points was essential to the investigation, and special Pitot tubes, made and calibrated in the laboratory, were used in the tests.

A view of the bend showing the men taking velocity measurement, and also showing part of the 300 piezometer connections, is given in Figure 1.

Tests were made with the channel flowing full under some pressure and also partly full. The experiments included studies with uniform velocity distribution, and also with nonuniform-velocity distribution in the channel approaching the bend.

A complete experiment for one quantity of flow required the measurement of pressures at 300 different points, the recording of velocities at 700 different points in the two tangents and the bend, as well as studies on the direction of flow. Approximately 45 man-hours were required to collect the necessary data for one experiment.

TESTS SHOW SPIRAL MOTION OF WATER AT BENDS

This paper discusses only one phase of the investigation—the direction of flow of the various particles of water in moving around a bend.

Let us consider the case when there is uniform velocity distribution in the channel approaching the bend.

When such a condition occurs the water in the bottom part of the bend will rotate counterclockwise, while the water in the top part of the bend will rotate clockwise, as shown in Figure 2. Assuming such a condition of flow exists, if several yarns attached to a pin are placed in the channel next to the outside wall the yarns should diverge, whereas if placed next to the inside wall they should converge. That such a condition prevails is illustrated in Figure 3, which is composed of 11 separate pictures taken of yarns attached to pins and placed at various distances from the outside wall of the channel.

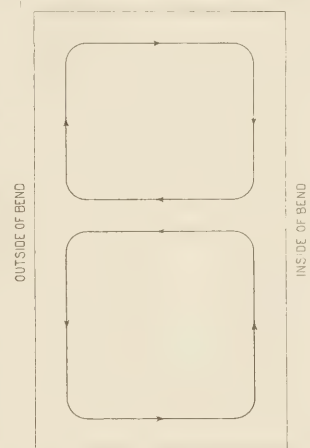


FIGURE 2.—NORMAL CONDITION OF SPIRAL FLOW DETECTED IN CLOSED CHANNEL BEND. DOUBLE SPIRAL IN CHANNEL

Where the friction along the bottom of the channel is greater than along the top the greatest velocity would be along the top and the lowest velocity along the bottom of the channel. With this velocity distribution in the channel approaching the bend, the water takes a single spiral or helical motion in addition to its forward motion in flowing around the bend. This spiral motion is counterclockwise as shown in Figure 4. Thus the yarns next to the outside wall will deflect downward, whereas those next to the inside wall will tip upward. This is illustrated in Figures 5 and 6.

The spiral motion shown in Figures 5 and 6 exists at the bends of rivers and is the cause of the erosion along the outer bank. The downward motion of the water rolls the particles of soil to the bottom of the channel, from whence they are carried diagonally toward the inner bank. The highest velocity of water is not along

¹ Paper presented before the Federation of Engineering Societies of Minnesota on Feb. 22.

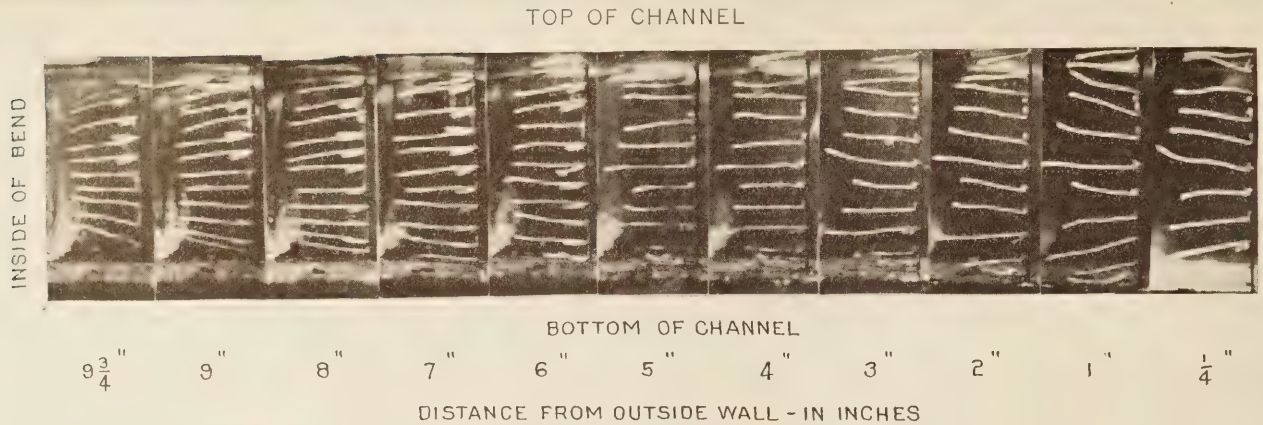


FIGURE 3.—DETERMINING SPIRAL FLOW BY MEANS OF YARNS IN 180° CLOSED CHANNEL BEND WITH 5-INCH INNER RADIUS. CHANNEL 10 INCHES SQUARE. VIEW IS COMPOSED OF 11 SEPARATE PICTURES TAKEN OF YARNS ATTACHED TO WIRES AND PLACED AT VARIOUS DISTANCES FROM OUTSIDE WALL



FIGURE 4.—NORMAL CONDITION OF SPIRAL FLOW IN BEND OF RIVER OR IN CLOSED CHANNEL BEND IN WHICH THE FRICTION IS GREATEST AT THE BOTTOM OF THE CHANNEL APPROACHING THE BEND

the outer bank, as commonly supposed, but is along the inner bank.

A practical demonstration of this spiral motion of water in flowing around a bend can easily be made. Take a glass of water and put in it two teaspoons of sugar. Then stir the water and notice how the sugar collects near the center at the bottom of the tumbler. This phenomenon is due to the unbalanced centrifugal force and spiral motion set up in the water. When the liquid is set in rotation by stirring, centrifugal force produces a greater hydrostatic pressure near the walls of the tumbler. But the liquid very close to the bottom surface of the tumbler, because of friction, can not rotate so fast,

and thus the centrifugal force is not so great and hence does not counteract the radial hydrostatic pressure. The liquid in contact with the bottom of the tumbler is thus forced inward and carries the sugar with it.

It is believed that the erosion at bridge pier noses is due to a similar action. This spiral motion is greatest during flood stages. It is difficult to measure accurately the actual depth of the eroded section around pier noses, since the flood waters during their subsidence tend to silt up the pockets which were scoured out by the rising waters.

Tests were also made with various other conditions of velocity distribution in the approach channel to the bend and studies made of the spiral motion of the water in the bend. These researches are to be reported later.

There are several possible applications of this knowledge of the spiral motion of water in bends. It will be useful in the design of bridge substructures and stream-control structures. In pipe bends the spiral motion represents a loss of head, and where it is possible to straighten out the direction of flow of the filaments of water there should be an increase in efficiency. Quarter turn draft tubes are now designed with guide vanes in the bend, so as to make the water flow in a straight

direction as well as to reduce eddy losses. In a large generating plant in Chicago a 90,000 kilowatt steam turbine has sharp 90° bends equipped with blade turns designed especially to reduce the spiral motion and consequent eddy losses.

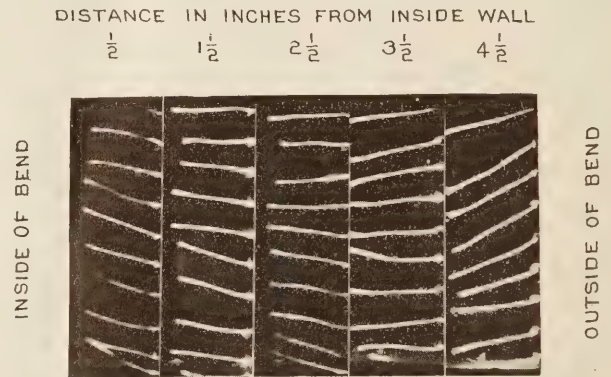


FIGURE 5.—DETERMINING SPIRAL FLOW BY MEANS OF YARNS IN 180° CLOSED CHANNEL BEND WITH 5-INCH INNER RADIUS. FRICTION IS GREATER AT THE BOTTOM THAN AT THE TOP. CHANNEL 5 INCHES WIDE BY 10 INCHES DEEP. VIEW IS COMPOSED OF FIVE SEPARATE PICTURES TAKEN OF YARNS ATTACHED TO WIRES AND PLACED AT VARIOUS DISTANCES FROM INSIDE WALL

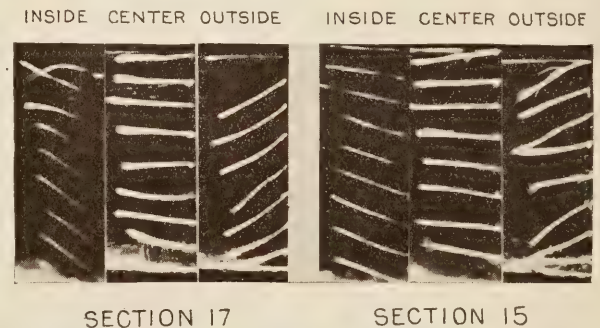


FIGURE 6.—DETERMINING SPIRAL FLOW BY MEANS OF YARNS IN 180° CLOSED CHANNEL BEND WITH 5-INCH INNER RADIUS. FRICTION IS GREATER AT THE BOTTOM THAN AT THE TOP. CHANNEL 5 INCHES WIDE BY 10 INCHES DEEP. SECTION 15 IS 45° AND SECTION 17, 135° FROM BEGINNING OF BEND. THE VIEW FOR EACH SECTION IS COMPOSED OF THREE SEPARATE PICTURES TAKEN OF YARNS ATTACHED TO WIRES NEAR OUTSIDE, MIDDLE, AND INSIDE OF CHANNEL

MOTOR-VEHICLE REGISTRATIONS, 1928¹

[Compiled from reports of State authorities]

State	Registered motor vehicles individually and commercially owned ²				Other registered vehicles		Tax-exempt official motor cars and motor cycles		Number of licenses or permits		Registered motor cars and trucks, 1927	Year's change in motor-vehicle registrations		
	Total registered cars and trucks	Passenger automobiles, taxis, and busses	Motor trucks and road tractors	Trailers ³	Motor cycles	United States cars	State and local cars	Motor cycles (official)	Dealers	Operators and chauffeurs		Number increase or decrease (-)	Per cent	
Alabama.....	269,519	235,026	34,493	1,952	611	167	666	---	586	1,097	243,539	25,980	10.7	
Arizona.....	94,372	88,326	8,326	800	281	176	985	---	1,039	12,342	81,047	13,325	16.4	
Arkansas.....	33,631	33,631	342	2,054	342	39	851	27	508	4,085	206,568	8,363	4.0	
California.....	1,791,800	1,582,477	217,413	37,073	9,440	1,217	13,526	149	3,547	7,977	1,693,195	106,695	6.3	
Colorado.....	284,807	291,006	48,701	294	2,407	283	1,923	108	3,751	337,623	28,271	16,375	6.1	
Connecticut.....	569,752	491,195	48,105	301	345	41	1,923	108	610	56,923	47,124	28,271	10.0	
Delaware.....	352,961	296,691	56,272	1,000	1,127	71	3,652	233	2,047	2,853	394,734	41,068	8.7	
Florida.....	318,856	277,881	40,975	816	1,075	933	1,231	18	1,155	2,301	300,635	18,221	6.1	
Georgia.....	108,194	106,060	11,124	1,194	5,820	103	3,995	---	458	3,995	101,336	6,818	6.7	
Illinois.....	823,806	706,713	117,093	3,712	3,820	979	4,531	18	4,548	94,169	1,438,985	65,374	4.5	
Indiana.....	733,466	672,147	61,019	7,884	3,728	3,44	4,531	---	2,716	39,021	813,637	10,169	1.2	
Iowa.....	533,799	471,937	61,902	2,830	1,728	3,144	3,200	60	2,479	16,563	704,203	29,263	4.2	
Kansas.....	304,231	223,445	80,848	339	1,169	192	2,463	60	2,676	501,401	31,898	31,898	6.4	
Louisiana.....	172,638	139,400	33,178	(⁴)	412	190	1,910	66	1,138	9,146	285,621	18,610	6.5	
Maine.....	285,311	273,221	10,090	4,000	625	209	1,326	75	480	16,029	255,000	9,293	3.6	
Maryland.....	726,285	637,153	89,132	3,898	1,919	1,069	1,300	---	5,853	76,669	163,623	9,015	5.5	
Massachusetts.....	1,249,221	1,084,615	164,606	3,874	3,856	37	1,563	---	2,370	870,160	694,107	8,448	4.6	
Michigan.....	673,573	583,789	89,784	3,894	2,083	252	1,153	---	2,192	311,413	1,154,773	94,448	8.2	
Minnesota.....	246,242	214,754	31,488	2,919	1,821	74	1,472	3	2,579	29,222	218,043	28,199	12.9	
Mississippi.....	712,965	636,717	76,248	2,004	1,821	228	1,242	---	512	210	112,735	13,300	11.8	
Missouri.....	126,035	104,251	21,804	2,975	1,020	226	1,288	---	3,344	---	373,912	17,443	4.7	
Montana.....	391,355	338,173	53,182	2,975	1,020	226	1,288	---	115	---	27,776	1,600	6.2	
Nebraska.....	27,376	21,753	5,643	543	1,330	22	442	---	---	---	96,009	6,635	6.9	
Nevada.....	102,644	88,394	14,050	343	1,330	22	6,303	846	3,176	1,186,736	712,396	46,034	6.5	
New Hampshire.....	738,430	624,748	113,682	1,996	6,383	768	6,303	---	201	---	56,291	6,446	10.9	
New Jersey.....	63,737	63,737	128,682	340	2,438	156	1,453	---	4,832	2,494,156	146,024	146,024	7.5	
New Mexico.....	2,083,942	1,700,549	323,393	7,148	14,394	1,666	14,153	1,208	1,108	---	1,437,618	33,877	7.9	
New York.....	464,376	418,864	45,512	1,944	1,334	423	6,200	---	---	---	160,701	12,824	8.1	
North Carolina.....	173,525	151,778	21,747	14,006	9,472	2,362	10,097	---	3,987	4,419	1,570,734	18,965	5.0	
North Dakota.....	1,649,699	1,450,994	198,705	14,006	1,124	330	1,244	34	1,384	49,250	503,126	26,717	1.4	
Ohio.....	329,843	463,530	64,293	---	2,012	11	943	---	4,300	1,933,450	1,554,915	37,546	1.4	
Oklahoma.....	248,118	227,404	20,714	1,238	1,071	1,883	683	95	4,300	1,933,450	1,554,915	37,546	1.4	
Oregon.....	1,642,207	1,420,957	221,250	4,283	13,807	1,883	2,694	---	1,063	---	193,635	17,170	5.6	
Pennsylvania.....	125,698	106,155	19,543	61	332	96	683	---	658	---	169,552	21,822	6.5	
Rhode Island.....	194,805	194,267	20,307	1,637	1,071	85	2,694	---	1,063	---	294,567	21,822	12.9	
South Carolina.....	191,374	171,067	20,307	(⁴)	1,039	132	3,289	---	3,881	---	111,407	102,890	9.4	
South Dakota.....	322,137	294,305	27,832	11,955	3,430	2,503	3,289	---	---	---	93,974	4,567	4.9	
Tennessee.....	1,214,297	1,060,028	154,269	14,521	3,430	173	4,521	---	---	---	79,527	6,704	8.4	
Texas.....	98,541	84,220	14,321	218	524	28	3,062	143	3,576	89,606	337,007	22,498	6.8	
Utah.....	86,231	78,685	7,546	640	2,128	11	3,081	---	3,576	7,746	337,007	22,498	6.8	
Vermont.....	306,345	306,911	53,684	2,279	2,128	1,117	3,081	143	4,783	499,140	384,583	18,292	4.8	
Virginia.....	402,875	344,977	57,898	617	1,355	33	2,044	124	4,108	73,468	245,819	5,737	2.3	
Washington.....	231,536	213,787	35,669	601	1,246	92	1,246	120	329	---	698,289	43,846	6.3	
West Virginia.....	742,135	646,737	95,398	412	2,128	206	2,246	---	---	---	57,655	4,381	8.4	
Wisconsin.....	56,336	48,700	7,636	---	---	---	---	---	---	---	57,655	4,381	8.4	
Wyoming.....	125,536	112,505	14,031	---	1,092	537	2,188	200	1,835	34,025	111,680	14,876	13.3	
District of Columbia.....	---	---	---	---	---	---	---	---	---	---	---	---	---	---
Total.....	24,493,124	21,379,125	3,113,999	148,169	117,946	33,179	103,618	3,710	86,734	8,941,861	23,133,241	1,359,883	5.9	

¹ This table lists only the number of registrations, licenses, and permits. For financial statement see table on next page.
² The first 3 columns show regularly registered motor cars and trucks which may require license fees, eliminating registrations, nonresident registrations, etc. Busses are included with passenger cars except as noted.
³ Some States include trailers with trucks; others do not register trailers.
⁴ Estimated.

⁵ Reported with tractors, but here separated as per semiannual report.
⁶ Busses registered with trucks.
⁷ Trailers registered as trucks.
⁸ As reported by Bureau of Budget in 1925 and includes 7,859 "cars at large," not allocated to any State.
⁹ Decrease compared to previous years due to eliminated dealers' plates formerly reported by some States.

MOTOR VEHICLE REGISTRATION FEES, LICENSES, PERMITS, FINES, ETC., 1928¹
 [Compiled from reports of State authorities]

State ²	Registration receipts ²				Miscellaneous receipts ²			Disposition of gross receipts				State ²
	Motor car receipts				Dealers' license	Chauffeur and operator permits	Other miscellaneous	For highway purposes			For other purposes	
	Total from motor cars	Passenger cars and busses	Trucks and tractors	Trailers				Motor-cycles	State highways	Local roads		
Alabama ²	\$3,474,065	\$300,982	\$132,864	\$3,078	\$3,617	\$12,698	\$111,600	\$151,721	\$1,075,501	\$677,443	\$1,569,400	Alabama ²
Arizona	3,565,806	3,420	30,818	3,597	5,194	21,366	18,923	75,720	365,806	567,901	2,309,462	Arizona
Arkansas	3,786,004	5,174,678	2,682,850	269,318	3,420	330,471	83,938	1,426,942	3,910,311	3,910,311		Arkansas
California	9,292,301	1,331,484	327,417	6,963	28,350	15,870	82,296	166,313	8,911,935	811,935	4,845,137	California
Colorado	1,790,183	4,222,116	1,405,000	2,462	83,274	1,041,649	69,497	7,373,389	7,373,389			Colorado
Connecticut	7,373,580	4,745,256	4,005,210	4,641	6,855	1,094,279	24,622	521,868	3,201,150	1,165,449		Connecticut
Delaware	4,935,995	3,611,324	1,262,287	1,483	26,684	3,367	24,925	143,088	3,898,679	1,400,400		Delaware
Florida	4,873,611	3,491,311	655,034	9,357	27,682	4,367	3,367		166,649			Florida
Georgia	4,041,767	3,308,491	269,900	4,817	27,306	3,491	13,800		9,337,237			Georgia
Illinois	1,626,940	11,777,192	3,401,578	4,645	88,066	331,210	438,350	249,233	3,302,548			Illinois
Indiana	5,751,781	4,121,143	1,227,253	38,878	54,600	33,125	434,820	203,982	10,068,490			Indiana
Iowa	10,138,702	9,092,308	1,041,394	4,068	81,188	33,125	434,820	203,982	3,213,511	1,894,091	6,149,016	Iowa
Kansas	5,394,448	3,605,292	976,751	3,477	32,877	22,485	82,376	195,198	4,041,685	4,488,375	752,583	Kansas
Kentucky	4,795,958	4,582,013	1,083,267	4,303,267					4,383,634			Kentucky
Louisiana	4,383,634	4,303,267	1,083,267	4,303,267					4,383,634			Louisiana
Maine	2,763,598	2,147,118	504,269	4,720	44,750	80,149	185,282	(⁶)	220,513	1,038,802		Maine
Maryland	3,024,621	2,380,885	2,033,384	18,063	34,701	136,137	393,321	303,462	2,124,234			Maryland
Massachusetts	13,919,618	7,854,107	3,273,036	24,127	63,585	1,740,320	928,569	1,352,012	11,643,077	924,529		Massachusetts
Michigan	20,056,848	18,367,667	4,424,654	248,639	69,771	257,156	1,072,718	729,063	12,245,725	6,000,000		Michigan
Minnesota	10,101,785	10,010,861	1,650,733	15,181	38,472		20,306	140,707	6,507,230	2,479,281		Minnesota
Mississippi ²	2,814,150								194,162			Mississippi ²
Missouri ²	8,765,600								5,283,109	3,112,500		Missouri ²
Montana ²	1,298,828	3,166,236	592,276	5,549	49,349		163,889	75,919	370,000	1,189,797	12,33,313	Montana ²
Nebraska	3,240,757								1,149,797	2,682,860		Nebraska
Nevada ²	2,070,957	1,673,914	78,549	11,485	49,349		163,889	75,919	1,149,797	127,836		Nevada ²
New Jersey	13,567,029	9,693,564	3,768,674	71,778	29,305	276,223	84,132	11,485	1,906,428	4,536,976	13,739	New Jersey
New Mexico	34,897,701	6,164,800	78,374	4,066	79,210	2,797,372	673,839	849,699	7,882,354		14,300,000	New Mexico
New York	34,806,706	530,407	68,374	4,066	10,700	13,679	13,679	70,406	371,633	185,712		New York
North Carolina ²	1,778,145	31,094,438	8,783,039	130,341	63,651	2,819,842	3,766	1,785,572	23,999,877	5,196,770		North Carolina ²
North Dakota	1,778,145	1,431,339	328,697	1,285	13,380		474	300,000	3,975,334	737,572		North Dakota
Ohio	11,840,225	11,265,981	4,861,113	134,019	79,340	11,392	328,309	386,503	17,000,000	5,483,924		Ohio
Oklahoma ²	6,238,240	6,404,466	4,861,113	134,019	79,340	11,392	328,309	386,503	17,000,000	5,483,924		Oklahoma ²
Oregon	9,969,217	5,741,931	978,538	10,904	28,213	59,880	149,755	300,000	1,665,855	1,667,305	3,336,061	Oregon
Pennsylvania	20,760,327	14,382,318	6,378,069	46,694	86,000	2,395,656	3,791,046	1,783,898	20,509,755	3,755,166		Pennsylvania
Rhode Island	1,852,157	1,388,895	443,262	1,419	14,730	289,752	131,925	211,995	2,031,516	30,398	18,949,210	Rhode Island
South Carolina	2,440,539	2,281,572	339,971	24,765	29,850	289,752	102,907	19,25,398	2,415,141			South Carolina
South Dakota	2,901,905	2,872,391	391,670	1,073	26,540		1,901	59,901	1,450,002	1,392,002		South Dakota
Tennessee ²	4,066,478	14,117,670	2,842,960	162,482	60,025	30,203	474,107	109,014	3,957,464	7,188,965		Tennessee ²
Texas	17,701,251	16,900,630	2,842,960	162,482	60,025	30,203	474,107	109,014	10,011,767	1,888,965		Texas
Utah ²	2,090,960	1,783,737	286,112	3,589	28,847	230,842	43,945	130,000	2,090,960	257,970		Utah ²
Vermont	5,372,046	1,497,625	286,112	5,913	67,276	35,654	287,152	(⁷)	2,090,960			Vermont
Virginia	7,028,291	3,108,534	826,306	5,113	67,276	35,654	287,152	260,000	5,312,046			Virginia
Washington	4,142,595	6,308,067	4,959,338	3,985	83,903	50,120	7,943	289,913	4,261,591	2,038,965		Washington
West Virginia	10,774,707	3,806,697	820,448	6,011	48,084	119,432	198,086	239,913	1,262,682	2,640,000		West Virginia
Wisconsin	3,727,570	10,408,621	2,965,549	16,261	6,381	2,067,067	1,388	639,497	5,645,210	4,490,000		Wisconsin
Wyoming	473,981	569,904	131,064	614	1,283		233,525	132,627	572,570			Wyoming
District of Columbia	473,981	113,525	21,929	1,092	1,835	102,075	233,525		572,570			District of Columbia
Detailed totals ²	288,883,694	1,704,324	14,725,475	12,127,095								Detailed totals ²
Grand totals	322,630,025				15,133,999	208,880,272	60,399,109	31,825,911	6,390,734			Grand totals

¹ Financial data only on this table. For number of registrations, etc., see other table.
² Several States do not report complete details and receipts are not included in detailed totals.
³ Includes \$346,740 on State bonds and \$1,968,722 on county bonds.
⁴ Revolving fund reserve.
⁵ Undistributed.
⁶ In State general fund.
⁷ Balance for refunds.
⁸ Appropriation \$45,000 from State general fund.
⁹ For Baltimore city streets.
¹⁰ For Baltimore city streets.
¹¹ On county bond obligations assumed by State.
¹² Auto-theft fund.
¹³ Included in miscellaneous.
¹⁴ For State highway office building.
¹⁵ For New York City general fund.
¹⁶ Includes \$130,000 for State bridge fund.
¹⁷ On State bonds, allotted from State highway fund.
¹⁸ Highway motor patrol.
¹⁹ Only expenses of law enforcement reported: Other expenses from highway fund.
²⁰ Appropriated from State general fund.
²¹ State highway patrol.
²² For traffic control and streets, if so appropriated by Congress.

ROAD PUBLICATIONS OF BUREAU OF PUBLIC ROADS

Applicants are urgently requested to ask only for those publications in which they are particularly interested. The Department can not undertake to supply complete sets nor to send free more than one copy of any publication to any one person. The editions of some of the publications are necessarily limited, and when the Department's free supply is exhausted and no funds are available for procuring additional copies, applicants are referred to the Superintendent of Documents, Government Printing Office, this city, who has them for sale at a nominal price, under the law of January 12, 1895. Those publications in this list, the Department supply of which is exhausted, can only be secured by purchase from the Superintendent of Documents, who is not authorized to furnish publications free.

ANNUAL REPORTS

Report of the Chief of the Bureau of Public Roads, 1924.
Report of the Chief of the Bureau of Public Roads, 1925.
Report of the Chief of the Bureau of Public Roads, 1927.
Report of the Chief of the Bureau of Public Roads, 1928.

DEPARTMENT BULLETINS

- No. *136D. Highway Bonds. 20c.
220D. Road Models.
257D. Progress Report of Experiments in Dust Prevention and Road Preservation, 1914.
*314D. Methods for the Examination of Bituminous Road Materials. 10c.
*347D. Methods for the Determination of the Physical Properties of Road-Building Rock. 10c.
*370D. The Results of Physical Tests of Road-Building Rock. 15c.
386D. Public Road Mileage and Revenues in the Middle Atlantic States, 1914.
387D. Public Road Mileage and Revenues in the Southern States, 1914.
388D. Public Road Mileage and Revenues in the New England States, 1914.
390D. Public Road Mileage and Revenues in the United States, 1914. A Summary.
407D. Progress Reports of Experiments in Dust Prevention and Road Preservation, 1915.
463D. Earth, Sand-clay, and Gravel Roads.
*532D. The Expansion and Contraction of Concrete and Concrete Roads. 10c.
*537D. The Results of Physical Tests of Road-Building Rock in 1916, Including all Compression Tests. 5c.
*583D. Reports on Experimental Convict Road Camp, Fulton County, Ga. 25c.
*660D. Highway Cost Keeping. 10c.
*670D. The Results of Physical Tests of Road-Building Rock in 1916 and 1917. 5c.
*691D. Typical Specifications for Bituminous Road Materials. 10c.
*724D. Drainage Methods and Foundations for County Roads. 20c.
1216D. Tentative Standard Methods of Sampling and Testing Highway Materials, adopted by the American Association of State Highway Officials and approved by the Secretary of Agriculture for use in connection with Federal-aid road construction.
1259D. Standard Specifications for Steel Highway Bridges, adopted by the American Association of State Highway Officials and approved by the Secretary of Agriculture for use in connection with Federal-aid road work.

DEPARTMENT BULLETINS—Continued

- No. 1279D. Rural Highway Mileage, Income, and Expenditures, 1921 and 1922.
1486D. Highway Bridge Location.

DEPARTMENT CIRCULARS

- No. 94C. T. N. T. as a Blasting Explosive.
331C. Standard Specifications for Corrugated Metal Pipe Culverts.

TECHNICAL BULLETIN

- No. 55. Highway Bridge Surveys.

MISCELLANEOUS CIRCULARS

- No. 62M. Standards Governing Plans, Specifications, Contract Forms, and Estimates for Federal Aid Highway Projects.
93M. Direct Production Costs of Broken Stone.
*109M. Federal Legislation and Regulations Relating to the Improvement of Federal-aid Roads and National-Forest Roads and Trails. 10c.

FARMERS' BULLETIN

- No. *338F. Macadam Roads. 5c.

SEPARATE REPRINTS FROM THE YEARBOOK

- No. 914Y. Highways and Highway Transportation.
937Y. Miscellaneous Agricultural Statistics.

TRANSPORTATION SURVEY REPORTS

- Report of a Survey of Transportation on the State Highway System of Connecticut.
Report of a Survey of Transportation on the State Highway System of Ohio.
Report of a Survey of Transportation on the State Highways of Vermont.
Report of a Survey of Transportation on the State Highways of New Hampshire.
Report of a Plan of Highway Improvement in the Regional Area of Cleveland, Ohio.
Report of a Survey of Transportation on the State Highways of Pennsylvania.

REPRINTS FROM THE JOURNAL OF AGRICULTURAL RESEARCH

- Vol. 5, No. 17, D- 2. Effect of Controllable Variables upon the Penetration Test for Asphalts and Asphalt Cements.
Vol. 5, No. 19, D- 3. Relation Between Properties of Hardness and Toughness of Road-Building Rock.
Vol. 5, No. 24, D- 6. A New Penetration Needle for Use in Testing Bituminous Materials.
Vol. 6, No. 6, D- 8. Tests of Three Large-Sized Reinforced-Concrete Slabs Under Concentrated Loading.
Vol. 11, No. 10, D-15. Tests of a Large-Sized Reinforced-Concrete Slab Subjected to Eccentric Concentrated Loads.

* Department supply exhausted

