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Aviation NOx-induced CH₄ effect: fixed mixing ratio boundary conditions versus flux boundary conditions 2

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Abstract

13 Atmospheric chemistry-climate models are often used to calculate the effect of aviation 14 NOx emissions on atmospheric ozone (O_3) and methane (CH_4) . Due to the long (~10 yr) 15 atmospheric lifetime of methane, model simulations must be run for long time periods, typically for more than 40 simulation years, to reach steady-state if using CH₄ emission fluxes. Because 16 17 of the computational expense of such long runs, studies have traditionally used specified CH₄ 18 mixing ratio lower boundary conditions (BCs) and then applied a simple parameterization based 19 on the change in CH₄ lifetime between the control and NOx-perturbed simulations to estimate 20 the change in CH₄ concentration induced by NOx emissions. In this parameterization a feedback 21 factor (typically a value of 1.4) is used to account for the feedback of CH₄ concentrations on its 22 lifetime. Modeling studies comparing simulations using CH₄ surface fluxes and fixed mixing 23 ratio BCs are used to examine the validity of this parameterization. The latest version of the 24 Community Earth System Model (CESM), with the CAM5 atmospheric model, was used for this 25 study. Aviation NOx emissions for 2006 were obtained from the AEDT (Aviation Environmental 26 Design Tool) global commercial aircraft emissions. Results show a 31.4 ppb change in CH_4 27 concentration when estimated using the parameterization and a 1.4 feedback factor, and a 28.9 28 ppb change when the concentration was directly calculated in the CH₄ flux simulations. The 29 model calculated value for CH₄ feedback on its own lifetime agrees well with the 1.4 feedback 30 factor. Systematic comparisons between the separate runs indicated that the parameterization 31 technique overestimates the CH₄ concentration by 8.6%. Therefore, it is concluded that the 32 estimation technique is good to within ~10% and decreases the computational requirements in 33 our simulations by nearly a factor of 8.

34 **1. Introduction**

35 Methane (CH₄) plays an important role in atmospheric chemistry and as a greenhouse gas that can affect climate. Since pre-industrial times (~1750), atmospheric CH_4 has increased about 36 37 150% and it accounts for 20% of the change in radiative forcing on climate from all long-lived 38 greenhouse gases from 1750 to 2000, excluding water vapor (IPCC, 2013). NOx emissions affect 39 atmospheric concentrations of CH₄ as an indirect result of their effect on concentrations of ozone 40 (O₃) (Wild et al., 2001). Resolving the resulting effects of aviation NOx emissions on ozone and 41 methane remains an important issue towards understanding the effects of aviation emissions on 42 climate. Many studies have shown that aviation NOx emissions at cruise altitudes ($\sim 200 - 300$ 43 hPa in the UTLS) increase the production of ozone in this region (Derwent et al., 1999; Fuglestvedt et al., 1999; Stevenson et al., 2004; Köhler et al., 2008; Hoor et al., 2009; Koffi et 44 45 al., 2010; Hodnebrog et al., 2011; Khodayari et al., 2014; and others). Additionally, these studies show that increased concentrations of O3 will increase the atmospheric concentrations of 46 47 hydroxyl (OH). OH is a major sink for CH₄ in the troposphere and stratosphere, and thus decreases its concentration, while also affecting the feedback of CH₄ on its own lifetime (Prather, 48 49 1994; Wild et al., 2001; IPCC, 2007).

50 The lifetime of methane has been evaluated in many studies. IPCC (2001, 2007) reported a 51 methane lifetime of 9.6 years against reaction with OH as evaluated with contemporary 52 chemistry-transport models (CTMs) (Ehhalt et al., 2001). Due to the near decadal lifetime of 53 methane, in order to directly calculate the changes in its atmospheric concentration and response 54 time, three-dimensional (3-D) models using CH₄ surface fluxes must run for more than 40 55 simulated years to reach steady-state. Simulations of this length are, although computationally feasible (Hsu and Prather, 2010; Prather and Hsu, 2010), often too computationally expensive; 56 57 therefore, past studies have used fixed mixing ratio lower BCs for CH₄ and then applied a 58 parameterization to estimate the change in CH4 concentrations that would have occurred if CH₄ 59 surface fluxes had been used. The parameterization equation (Equation 1), is derived from a one-box model assumption that assumes the change in CH₄ concentration is proportional to the 60 change in CH₄ lifetime obtained from simulations with and without perturbations (e.g., aviation 61 emissions), using fixed mixing ration BCs for CH₄ (Fuglestvedt et al. 1999). The 62 parameterization coefficient is derived from a CTM study (Fuglestvedt et al. 1999). 63

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$$\Delta[CH_4] = [CH_4]_{bg} \times \left(-1.4\left(\frac{\Delta \tau}{\tau_{bg}}\right)\right)$$
(1)

65 $[CH_4]_{bg}$ and τ_{bg} represent the CH₄ concentration and lifetime in the control simulation.

66 Δ [*CH*₄] and $\Delta \tau$ are the changes in CH₄ concentration and lifetime due to the aviation NOx 67 emissions, and 1.4 represents the CH₄ feedback on its own lifetime.

68 The feedback of CH₄ on its own lifetime lengthens the duration of a CH₄ perturbation (CH₄ 69 response time) to 12 years (Prather, 1994; IPCC, 1995). This can be illustrated as follows: the 70 initial perturbation in nitrogen oxides (NOx) ($\Delta E_{NO_{x}}$) affects the amount of ozone, which

71 produces an effect on OH ($\Delta[OH]_0$) that then affects CH₄ ($\Delta[CH_4]_0$) (e. g. Prather et al., 1999;

Wuebbles and Hayhoe, 2000; and Stevenson et al., 2004). The change in CH₄ then leads to further effects on OH and CH₄ ($\Delta[OH]_1, \Delta[CH_4]_1, \Delta[OH]_2, \Delta[CH_4]_2, etc$) until eventually the system reaches steady-state (the feedback effect). The entire process can be illustrated as the
following sequence of feedbacks (Fuglestvedt et al., 1999):

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$$\Delta E_{NO_x} \to \Delta[OH]_0 \to \Delta[CH_4]_0 \to \Delta[OH]_1 \to \Delta[CH_4]_1 \to \Delta[OH]_2 \to etc.$$

The feedback effect due to the initial sequence of feedbacks can then be calculated fromEquation 2.

$$R_1 = \frac{\Delta [CH_4]_1 / \Delta [CH_4]_0}{\Delta \tau_1 / \Delta \tau_0}$$
(2)

80 Here, R_1 corresponds to the initial feedback effect. $\Delta [CH_4]_0$ and $\Delta \tau_0$ are the initial changes

81 in CH₄ concentration and lifetime and $\Delta [CH_4]_1$ and $\Delta \tau_1$ are the changes in CH₄ concentration

and lifetime after the first sequence of feedbacks. The initial feedback (R₁) can be calculated by performing two simulations, first a NOx-perturbed simulation with fixed CH₄ mixing ratio BCs and then a similar NOx-perturbed simulation, but with a small increase in CH₄ mixing ratio at the boundary layer (i.e., $\Delta [CH_4]_1 / \Delta [CH_4]_0 = 0.20$ when there is a 20% increase in CH₄ mixing

⁸⁶ ratio at the boundary layer). The corresponding CH₄ lifetime is calculated in each simulation.

Assuming that the feedback strength does not vary significantly with the strength of the initial perturbation, the feedback factor due to the whole sequence can be derived from Equation 3 (Fuglestvedt et al., 1999; Karlsdottir and Isaksen, 2000; IPCC, 2013):

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$$f = \frac{1}{1-s} = \frac{1}{1-\frac{1}{R_1}}; \text{ where } s = \frac{1}{R_1}$$
 (3)

91 IPCC (2001) calculated a feedback factor with a range of 1.33 – 1.45 (with an average value
92 of 1.4). This feedback factor of 1.4 has been widely accepted and used (e.g., IPCC, 2001;
93 Holmes et al., 2011).

94 In this study we used the latest version of the atmospheric component of the Community 95 Earth System Model (CESM), CAM5, to evaluate the parameterization commonly used to 96 correct for assuming fixed CH₄ mixing ratio BCs and also to evaluate the validity of the 1.4 97 feedback factor for the case of aviation perturbations. Estimates of the methane feedback on its 98 own lifetime have been evaluated for aviation perturbations previously, e.g., feedback factors of 99 1.3 and 1.52 were calculated in Köhler et al. (2008) and Holmes et al. (2011), respectively, and 100 in this study we re-evaluate this feedback factor using CAM5. However, there has been no 101 previous evaluation of the validity of the aforementioned parameterization (Equation 1) for the 102 case of aviation perturbations.

103 The remainder of this paper is organized as follows: section 2 describes the data and model 104 used in the study, section 3 describes the model configuration, section 4 describes the model 105 simulations done to test the accuracy of Equation 1, section 5 will discuss the results, and section 106 6 provides a concluding argument.

107 **2. Model Description and Configuration**

CAM5 is the atmospheric component for the Community Earth System Model (CESM) (http://www.cesm.ucar.edu/). The previous version of the Community Atmosphere Model (CAM) and CAM5 have been documented and discussed in other studies (e.g. Neale et al., 2011, Gent et al., 2011, Lamarque et al., 2012). CAM5 was successfully coupled to the full chemical mechanism and released in CESM 1_2_0 and versions thereafter. We used the development version of CAM5 (Community Atmosphere Model version 5, cesm1_1_alpha17b_modal) in this study since the coupling of aerosols and chemistry in CAM5 has not been released at the time model runs were completed.

116 CAM5 includes tropospheric and stratospheric chemistry with 133 species and 330 117 photochemical reactions as described in Lamarque et al. (2012). A major improvement in 118 CAM5 over CAM4 is a new modal aerosol module (MAM) (Liu et al., 2012) with two different 119 versions available: a version with seven lognormal modes (MAM7), and a version with three 120 lognormal modes—Aitken, accumulation, and coarse (MAM3) (Liu et al., 2012). For this study, 121 CAM5 was configured with MAM3. MAM simulates the size distribution of aerosols for both 122 internal and external mixing, the chemical and optical properties of aerosols, as well as various 123 other complicated aerosol processes (Liu et al., 2012). Further details on CAM5 can be found on 124 the NCAR website (http://www.cesm.ucar.edu/models/cesm1.0/cam/).

125 CAM5 was run with a horizontal resolution of 2° latitude x 2.5° longitude with 30 vertical 126 levels from the surface up to ~2 hPa. To reduce the year-to-year climate variability in the model 127 simulation and to be able to detect the aviation NOx-induced signal, specified dynamics ("off-128 line" mode) simulations were performed. The model was driven with the 2005 meteorology from 129 a coupled CAM5 simulation. The aviation NOx emissions are from the AEDT aviation emissions 130 scenarios for the year 2006 (Roof et al., 2007; Wilkerson et al., 2010; Olsen et al., 2012). The NOx emissions used as the input to the model had a horizontal resolution of 1° latitude x 1° 131 132 longitude, vertical resolution of 150 m, and hourly temporal resolution. The total NO_X emissions 133 amounted to 2.7 Tg (NO₂)/yr. The NOx emissions were then regridded to the model resolution. 134 Background emissions of non-aviation short-lived species (e.g., NOx, volatile organic 135 compounds (VOCs)) and longer-lived species (e.g., CO₂, chlorofluorocarbons (CFCs), and nitrous oxide (N₂O)), which were specified as mixing ratio lower BCs, are from the IPCC 136 137 RCP4.5 scenario (van Vuuren et al., 2011). Biogenic emissions were from the Model of 138 Emissions of Gases and Aerosols from Nature (MEGAN) (Guenther et al., 2006).

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141 **3. Experimental Design**

142 We evaluated the CH₄ feedback factor and the parameterization commonly used to calculate the change in CH₄ concentration based on the changes in its lifetime by performing three sets of 143 144 simulations: Set 1- a control (1c) and an aviation NOx-perturbed (1p) run with fixed mixing ratio 145 BCs for zonal mean CH₄ that had a monthly temporal resolution and were interpolated to the 146 model resolution, Set 2- an aviation NOx-perturbed (2p) run with a 20% increase in CH_4 mixing 147 ratio at the boundary layer, and Set 3- a control (3c) and a NOx-perturbed (3p) run with CH₄ 148 surface fluxes. The changes induced by aviation NOx were then obtained by taking the 149 difference between the control and the NOx-perturbed simulation in each set of simulation.

The purpose of Set 1 was to calculate the changes in CH_4 lifetime with fixed CH_4 mixing ratio at the boundary layer. After running these simulations for 7 years, the steady-state condition was reached. Data from the 7th year was used to calculate the steady state change in CH_4 lifetime due to its reaction with tropospheric OH. The parameterization described in Equation 1 (Fuglestvedt et al., 1999) was then used to calculate the steady state change in CH_4 concentration using the changes in its lifetime and the 1.4 feedback factor.

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157 The purpose of Set 2 was to calculate the CH_4 feedback on its lifetime. By using the CH_4 158 lifetime obtained in this run (2p) and the CH_4 lifetime obtained in the NOx-perturbed run from 159 Set 1 (1p) with Equations 3 and 4, the CH_4 feedback factor was calculated.

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161 The purpose of Set 3 was to directly calculate the changes in CH₄ concentration caused by 162 aviation NOx emissions. A control run and a NOx-perturbed run with CH₄ surface fluxes were 163 done to calculate the actual changes in CH₄ response time and concentration. The CH₄ fluxes 164 used in Set 3 were obtained using the global annual mean steady-state loss of CH₄ from the 165 control run of Set 1 (1c) since at steady-state, production is equal to loss. This resulted in a 166 global annual mean CH₄ flux of 453 Tg that is well within the IPCC (2007) reported range (428-167 507 Tg) and close to the most recent reported range of 554±56 Tg/yr (Prather, 2012; IPCC, 2013). Next, the CH₄ fluxes from IPCC RCP 4.5, that had a horizontal resolution of 2.8° latitude 168 x 2.8° longitude and monthly temporal resolution, were scaled to match the global annual mean 169

170 CH_4 flux calculated from Set 1 (453 Tg). This was done to produce a regional and temporal 171 distribution of CH_4 input flux that matched the background atmosphere of Set 1, for Set 3. The 172 two simulations were then run until steady-state conditions were achieved. By comparing the 173 result from Set 1 to the direct changes in CH_4 concentration calculated from Set 3, using CH4 174 fluxes, the accuracy of Equation 1 was evaluated.

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- 176 177

4. Results and Discussion

178 Based on our three sets of simulations the accuracy of the parameterization used in Equation 179 1 has been evaluated and the feedback factor used to describe CH₄ feedback on its lifetime has 180 been calculated. Set 1 resulted in a global annual mean background CH₄ concentration of 1713.0 181 ppb in both the control and the NOx-perturbed simulations, since both simulations were run with 182 the same CH₄ mixing ratio BCs. The calculated CH₄ lifetime for the control run and the NOx-183 perturbed simulations using the global burden and the global loss of CH₄ were 10.74 and 10.58 184 years, respectively. The global losses do not include losses to soils, the stratosphere, or Cl-atom 185 losses. The reduction in CH₄ lifetime is about 1.3% (1.60%/[TgN/yr]), which falls within the -186 1.4 ± 0.40 (%/[TgN/yr]) to -1.6 ± 0.37 (%/[TgN/yr]) range reported by Hodnebrog et al. (2011) 187 using an ensemble of six different atmospheric chemistry models with different emissions. A 188 global mean aviation NOx-induced CH₄ change of 31.4 ppb was calculated by using the CH₄ 189 lifetimes and the global annual mean background CH₄ concentration in Equation 1.

Based on Set 2, the CH_4 feedback on its lifetime was calculated. The CAM5 calculated feedback factor was 1.39, very close to the average feedback factor of 1.4 adopted in most studies.

Based on Set 3, the change in CH₄ concentration was calculated directly. As discussed earlier, the runs in this set used CH₄ fluxes to produce the actual change in CH₄ concentration. Both the NOx-perturbed run and the control run were run until reached steady-state.

196 Since the surface CH_4 fluxes used in Set 3 were calculated based on the steady-state loss 197 of CH_4 in the control simulation of Set 1, the background CH_4 concentration calculated in the 198 control simulation of Set 3 should be very similar to the background CH_4 concentration in the 199 control simulation of Set 1. A comparison of the background concentration in the two sets 200 indicates that the CH_4 concentration in the background atmospheres between the two sets were 201 essentially the same (\pm 0.10% difference at a global annual level and \pm 0.35% difference (with a 202 max difference of 3%) at a monthly grid box level).

The aviation NOx-induced global mean changes in CH_4 concentration calculated from the Set 3 simulations was 28.9 ppb which is about 8.6% lower than the change calculated from simulations in Set 1.

206 Four approaches (lifetime approaches) were used to calculate the atmospheric concentration 207 of CH₄ and its lifetime as all these approaches were used alternatively in previous studies (e.g., 208 Dentener et al., 2003; Stevenson et al., 2004; Stevenson et al., 2006). The most representative 209 lifetime approach was the global annual mean, which was calculated by using the global annual 210 mean burden and the global annual mean loss of CH₄. The other three lifetime approaches 211 differed by: (1) using the tropospheric CH_4 burden and loss, with the tropopause marked by the 212 pressure level of the tropopause, (2) using the tropospheric CH₄ burden and loss, with the 213 tropopause marked by the altitude where the ozone concentration dropped below 150 ppb, and 214 (3) using the global CH_4 burden and tropospheric CH_4 loss with the tropopause marked by the 215 altitude where the ozone concentration dropped below 150 ppb. Using these four different 216 approaches, a range for the values of interest is presented in the third column of table 1. Table 1 217 shows the results from the three sets of simulations using the aforementioned approaches. 218 Columns 2 and 3 show the values of the quantities of interest using the global mean lifetime 219 approach and the range of values obtained using other defined lifetime approaches (approaches 220 1-4).

The most representative and thereby accurate lifetime method was the global mean approach (global burden and loss of CH₄). The feedback factor using this lifetime approach was 1.39, very close to the IPCC reported value of 1.40 (0.4% lower). For the other lifetime approaches, the feedback factor ranges from 1.35 to 1.43 (differs from the IPCC adopted value of 1.4 by -3.7% to 2.2%). The CH₄ concentration change calculated from the Set 1 simulations using Equation 1 is about 8.6% higher than the actual CH_4 concentration change calculated from the simulations in Set 3. For the other lifetime approaches, the change in CH_4 concentration calculated from the Set 1 simulations using Equation 1 is about 12.1% to 20.0% higher than the actual change in CH_4 concentration calculated from the Set 3 simulations. Thus, the parameterization used in Equation 1 is good to within ~10% when using the global mean CH_4 lifetime and decreases the computational requirements by nearly a factor of 8.

5. Conclusion

233 We evaluated the accuracy of the parameterization widely used in estimating the changes in 234 CH₄ concentration based on the changes in its lifetime and calculated the feedback factor that 235 describes CH₄ feedback on its own lifetime. Results show a 1.3% decrease in CH₄ lifetime due 236 to total aviation NOx emissions from the year 2006 in the simulations with fixed CH₄ mixing 237 ratio as the boundary condition. The CAM5 calculated global mean CH_4 feedback factor of 1.39 238 compared well with the IPCC adopted feedback factor of 1.4. It was concluded that for the 239 simulations with fixed CH₄ at the lower boundary condition, the parameterizing technique using 240 the global mean lifetime approach overestimates the change in CH₄ by 8.6% compared to the 241 change calculated directly from the model using CH₄ surface emissions. The overestimation is 242 12.1% to 20.0% if using other lifetime approaches. Thus, for these simulations, the parameterization technique is good to within ~10% when using the global mean lifetime 243 244 approach and decreases the computational requirements by nearly a factor of 8.

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Table 1. Results from comparisons of the three sets of simulations, a control and a NOxperturbed simulation with fixed mixing ratio boundary conditions for CH_4 , a NOx-perturbed simulation with a 20% increase in CH_4 mixing ratio at the boundary layer, and a control and a NOx-perturbed simulation with CH_4 fluxes.

	Global annual	Range using	
	mean method	other methods	
	(Approach 1)	(Approach 2-4)	
CH ₄ lifetime (yr), control simulation, fixed CH ₄	10 74	9.70 to 11.4	
mixing ratio boundary condition (Set 1)	10.74		
CH ₄ lifetime (yr), NOx-perturbed simulation,	10.58	9.52 to 11.21	
fixed CH_4 mixing ratio boundary condition (Set 1)	10.50		
Aviation-induced ΔCH_4 (ppb) using Eq. 1	31.4	32.5 to 35.3	
Aviation-induced ΔCH_4 (ppb) using CH_4 fluxes	28.9	28.9 to 29.4	
(Set 3)	20.7		
CAM5 calculated feedback factor (Set 2)	1.39	1.35 to 1.43	
Percent difference in feedback factor	-0.4%	-3.5% to 2.2%	
Percent difference in CH ₄ concentration using CH ₄			
surface fluxes compared to using fixed mixing	8.6%	12.1% to 20.0%	
ratio BCs			

Parameterization used to calculate the change in CH4 concentration was evaluated.

Our CAM5 simulations show that the parameterization technique is good within 10%.

Methane feedback on its own lifetime was calculated.

Our model dependent feedback factor is well within the range reported by IPCC (2001).

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