

Test Report No. 608331-4-6 Test Report Date: March 2020

MASH TL-3 EVALUATION OF 2019 MASH 2-TUBE BRIDGE RAIL THRIE BEAM TRANSITION

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The results reported herein apply only to the article tested. The full-scale crash tests were performed according to TTI Proving Ground quality procedures and according to the *MASH* guidelines and standards.

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16. Abstract

The purpose of the tests reported herein was to assess the performance of the 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition according to the safety-performance evaluation guidelines included in AASHTO MASH The crash tests were performed in accordance with MASH TL-3, which involves two fullscale crash tests (MASH Tests 3-20 and 3-21). However, MASH states that when there are transitions between two barrier types with different stiffness, one from a more flexible barrier and the other to a more rigid barrier, a full-scale crash test is recommended for both types. Therefore, MASH Test 3-21 was performed at the transition from the thrie beam rail to bridge rail, and at the transition from the W-beam rail to thrie beam rail.

This report provides details of the 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition, detailed documentation of the crash tests and results, and an assessment of the performance of the 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition for MASH TL-3 transition evaluation criteria.

The 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition performed acceptably for MASHTL-3 transitions.

17. Key Words		18. Distribution Statemen1		
Transition, bridge rail, thrie beam, longitudinal		Copyrighted. Not to be copied or reprinted without		
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Chapter 1. INTRODUCTION

1.1 BACKGROUND

In May 1998, Texas A&M Transportation Institute contracted with the Alaska Department of Transportation to perform engineering analyses, design, and full-scale testing on the following:

- 1.) Alaska Multi-State (2-Tube) Bridge Rail (1, 2, 3).
- 2.) Alaska Multi-State Bridge Rail Thrie Beam Transition (4, 5).
- 3.) Alaska Multi-State W-Beam Transition (6, 7).

Under that project (TTI Project No. 404311), TTI researchers performed engineering analyses, developed engineering details, and performed full-scale crash testing on the Alaska Multi-State (2-Tube) Bridge Rail (1-3). The bridge rail successfully met the performance requirements of National Cooperative Highway Research Program (NCHRP) Report 350 Test Level 4 (TL-4) (8). TTI researchers evaluated the strength and performance of a new, taller Alaska Multi-State 2-Tube Bridge Rail, herein after it was re-designated as the 2019 MASH 2-Tube Bridge Rail, with respect to American Association of State Highway and Transportation Officials (AASHTO) Manual for Assessing Safety Hardware (MASH), Second Edition 2016, specifications (9, 10). TTI researchers performed engineering analyses and developed engineering details for this design to meet the performance requirements of MASH TL-4. TTI Proving Ground performed full-scale crash testing on the 2019 MASH 2-Tube Bridge Rail with respect to MASH TL-4, and the bridge rail performed acceptably.

1.2 OBJECTIVE

As part of this current project, TTI researchers performed analyses, designed, and full-scale tested a new Alaska Multi-State Bridge Rail Thrie Beam Transition. This new thrie beam transition design was tested with respect to *MASH* TL-3.

The purpose of the tests reported herein was to assess the performance of the 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition according to the safety-performance evaluation guidelines included in AASHTO MASH. The crash tests were performed in accordance with MASH TL-3, which involves two full-scale crash tests (MASH Tests 3-20 and 3-21). However, MASH states that when there are transitions between two barrier types with different stiffness, one from a more flexible barrier and the other to a more rigid barrier, a full-scale crash test is recommended for both types. Therefore, MASH Test 3-21 was performed at the transition from the thrie beam rail to bridge rail, and at the transition from the W-beam rail to thrie beam rail.

This report provides details of the 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition, detailed documentation of the three crash tests and results, and an assessment of the performance of the 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition for *MASH* TL-3 evaluation criteria.

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Chapter 2. SYSTEM DETAILS

2.1. TEST ARTICLE AND INSTALLATION DETAILS

The 2019 MASH 2-Tube Bridge Rail test installation was comprised of a 154-ft long section of reinforced concrete bridge deck that incorporated two steel rails, a 12½-ft long (nominal) section of two nested thrie beams (RTM08a) attached to the bridge rails with a thrie beam terminal connector (RTE01b) and unique guardrail connector, a standard symmetrical 75-inch long (nominal) thrie-beam-to-W-beam transition rail section (RWT01b), 25 ft of W-beam guardrail (in length of need), and a standard 9 ft-4½ inch long TxDOT DAT terminal (posts 1 and 2) at the end.

The total length of the installation was approximately 207 ft-3½ inches (53 ft-3½ inches transition + 154 ft bridge deck). The top edges of the DAT rail and W-beam were located 31 inches above grade. The top edge of the nested thrie beam was 34¾ inches above grade, and the top of the upper bridge rail was 38 inches above the bridge deck.

Posts 3 through 6 were 72 inches long (embedded 40 inches), posts 7 and 8 were 72 inches long, and posts 9 through 15 were 78 inches long. Posts 1 through 6 were spaced at 75 inches; posts 7 through 10 were at 37½ inches; and posts 10 through 15 were at 18¾ inches. Timber blockouts, 8-inches deep, were installed on posts 2 through 6. Posts 7 and 8 were fitted with 12-inch deep, short (14 inches) steel hollow structural section (HSS) tubing blockouts, and posts 9 through 15 were fitted with 12-inch deep, long (21½ inches) steel HSS blockouts,

The concrete portion of the 2019 MASH 2-Tube Bridge Rail test installation consisted of a reinforced cantilevered deck and curb, with two 2-inch wide joints extending through both the curb and the deck. The curb was 10 inches tall, with a 4-inch thick lift of grout, yielding a 6-inch tall traffic side face. The curb was 18 inches wide at the base, and 17 inches wide at the top, with the traffic side face sloping 1-inch toward the field side. Anchor bolts were cast in the deck and extended through the curb.

Sixteen fabricated steel posts were longitudinally spaced on 10 ft centers, beginning at 24 inches from each end of the concrete curb. Two steel rectangular HSS rail elements spanned the posts and extended past them at each end of the installation. The tops of the rails were located 24 inches and 38 inches above grade.

Figure 2.1 presents overall information on the 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition, and Figure 2.2 provides photographs of the installation. Appendix A provides further details of the 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition.

2.2. DESIGN MODIFICATIONS DURING TESTS

No modification was made to the installation during the testing phase.

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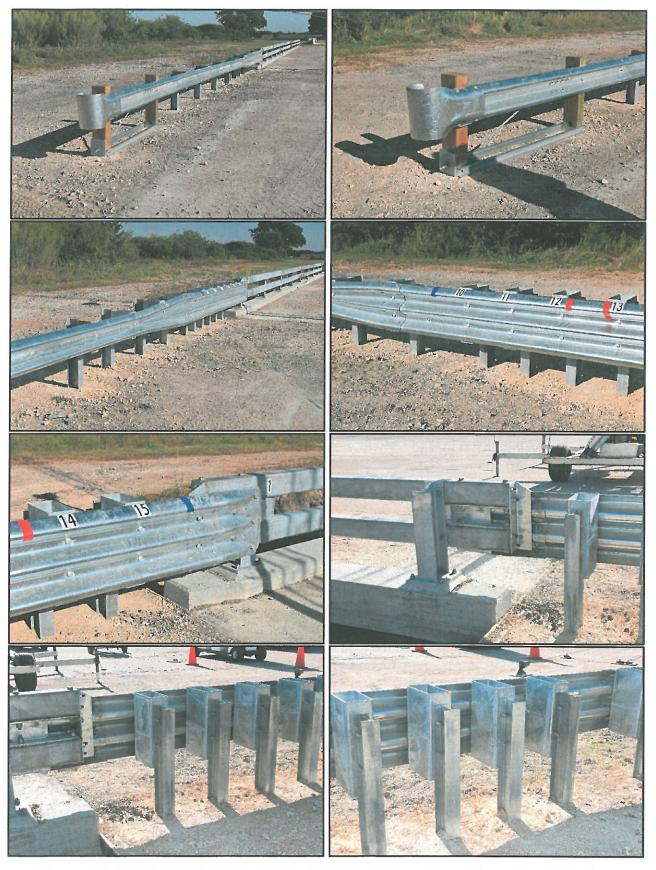


Figure 2.2. 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition prior to Testing.

2.3. MATERIAL SPECIFICATIONS

The specified minimum unconfined compressive strength of the concrete was 4000 psi for the curb, and 5000 psi for the deck. On December 10, 2018 (date of the first test on the 2-Tube Bridge Rail and deck), the average compressive strength of the concrete was 5060 psi (at 42 days) for the curb, and 5670 psi (at 44 days) for the deck.

Appendix B provides material certification documents for the materials used to install/construct the 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition.

2.4. SOIL CONDITIONS

The transition and terminal of the test installation were installed in soil meeting grading B of AASHTO standard specification M147 "Materials for Aggregate and Soil Aggregate Subbase, Base and Surface Courses."

In accordance with Appendix B of MASH, soil strength was measured the day of the crash test. During installation of the 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition for full-scale crash testing, two 6-ft long W6×16 posts were installed in the immediate vicinity of the transition using the same fill materials and installation procedures used in the test installation and the standard dynamic test. Table C.1 in Appendix C presents minimum soil strength properties established through the dynamic testing performed in accordance with MASH Appendix B.

As determined by the tests summarized in Appendix C, Table C.1, the minimum post loads required for deflections at 5 inches, 10 inches, and 15 inches, measured at a height of 25 inches, are 3940 lb, 5500 lb, and 6540 lb, respectively (90 percent of static load for the initial standard installation).

On the day of Test No. 608331-01-4, September 2, 2019, loads on the post at deflections of 5 inches, 10 inches, and 15 inches were 9087 lbf, 9948 lbf, and 10,395 lbf. Table C.2 in Appendix C shows the strength of the backfill material in which the 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition was installed met minimum *MASH* requirements.

On the day of Test No. 608331-01-5, September 5, 2019, load on the post at 5 inches of deflection was 11,359 lbf, which was almost triple the required load. It was determined during the test pull that any additional loading may impart stresses on the W6×16 post that could cause it to yield and bend, or could cause damage to the test pull equipment (e.g. winch, load cell, etc.) Therefore, the test was terminated and the loads at deflections of 10 inches and 15 inches were not measured. Table C.3 in Appendix C shows the strength of the backfill material in which the 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition was installed met minimum *MASH* requirements.

On the day of Test No. 608331-01-6, December 19, 2019, loads on the post at deflections of 5 inches, 10 inches, and 15 inches were 9225 lbf, 8537 lbf, and 7504 lbf. Table C.2 in Appendix C shows the strength of the backfill material in which the 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition was installed met minimum *MASH* requirements.

Chapter 3. TEST REQUIREMENTS AND EVALUATION CRITERIA

3.1. CRASH TEST PERFORMED / MATRIX

Table 3.1 shows the test conditions and evaluation criteria recommended for MASH TL-3 transitions. However, MASH states that when there are transitions between two barrier types with different stiffness, one from a more flexible barrier and the other to a more rigid barrier, a full-scale crash test is recommended for both types. Therefore, MASH Test 3-21 was performed at the transition from the thrie beam rail to bridge rail, and at the transition from the W-beam rail to thrie beam rail.

Table 3.1. Test Conditions and Evaluation Criteria Specified for MASH TL-3 Transitions.

Tost Auticle	Test Designation	Togt Valida	Impact Conditions			
Test Article	Test Designation	t Designation Test Vehicle		Angle	Evaluation Criteria	
Transitions	3-20	1100C	62 mi/h	25°	A, D, F, H, I	
1 ransitions	3-21	2270P	62 mi/h	25°	A, D, F, H, I	

The target critical impact point (CIP) for each test was determined in accordance with the guidance provided in *MASH Section 2.3.2* and *MASH Figure 2-1*. For *MASH* Test 3-20, the target CIP was 5.1 ft upstream of the end of the concrete curb/deck. The target CIP for *MASH* Test 3-21 on the thrie beam to bridge rail transition was 7.0 ft upstream of the concrete curb/deck. The target CIP for *MASH* Test 3-21 on the W-beam to thrie beam transition was 7.3 ft upstream of the centerline of post 7. TTI researchers determined that *MASH* Test 3-20 on the W-beam to thrie beam transition was not necessary and was therefore not performed.

The crash tests and data analysis procedures were in accordance with guidelines presented in *MASH*. Chapter 4 presents brief descriptions of these procedures.

3.2. EVALUATION CRITERIA

The appropriate safety evaluation criteria from Tables 2-2 and 5-1 of *MASH* were used to evaluate the crash tests reported herein. The test conditions and evaluation criteria required for *MASH* TL-3 transitions are listed in Table 3.1, and the substance of the evaluation criteria in Table 3.2. An evaluation of the crash test results is presented in detail under the section Assessment of Test Results.

Table 3.2. Evaluation Criteria Required for MASH TL-3 Transitions.

Evaluation Factors	Evaluation Criteria		
Structural Adequacy	A. Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable.		
	D. Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present undue hazard to other traffic, pedestrians, or personnel in a work zone.		
	Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.2.2 and Appendix E of MASH.		
Occupant Risk	F. The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.		
	H. Occupant impact velocities (OIV) should satisfy the following limits: Preferred value of 30 ft/s, or maximum allowable value of 40 ft/s.		
	I. The occupant ridedown accelerations should satisfy the following: Preferred value of 15.0 g, or maximum allowable value of 20.49 g.		

Chapter 4. TEST CONDITIONS

4.1. TEST FACILITY

The full-scale crash tests reported herein were performed at Texas A&M Transportation Institute (TTI) Proving Ground, an International Standards Organization (ISO)/International Electrotechnical Commission (IEC) 17025-accredited laboratory with American Association for Laboratory Accreditation (A2LA) Mechanical Testing Certificate 2821.01. The full-scale crash tests were performed according to TTI Proving Ground quality procedures, and according to the MASH guidelines and standards.

The test facilities of the TTI Proving Ground are located on the Texas A&M University System RELLIS Campus, which consists of a 2000-acre complex of research and training facilities situated 10 miles northwest of the flagship campus of Texas A&M University. The site, formerly a United States Army Air Corps base, has large expanses of concrete runways and parking aprons well suited for experimental research and testing in the areas of vehicle performance and handling, vehicle-roadway interaction, durability and efficacy of highway pavements, and evaluation of roadside safety hardware and perimeter protective devices. The site selected for construction and testing of the 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition was along the edge of an out-of-service apron. The apron consists of an unreinforced jointed-concrete pavement in 12.5-ft × 15-ft blocks nominally 6 inches deep. The aprons were built in 1942, and the joints have some displacement, but are otherwise flat and level.

4.2 VEHICLE TOW AND GUIDANCE SYSTEM

Each test vehicle was towed into the test installation using a steel cable guidance and reverse tow system. A steel cable for guiding the test vehicle was tensioned along the path, anchored at each end, and threaded through an attachment to the front wheel of the test vehicle. An additional steel cable was connected to the test vehicle, passed around a pulley near the impact point, through a pulley on the tow vehicle, and then anchored to the ground such that the tow vehicle moved away from the test site. A 2:1 speed ratio between the test and tow vehicle existed with this system. Just prior to impact with the installation, the test vehicle was released and ran unrestrained. The vehicle remained freewheeling (i.e., no steering or braking inputs) until it cleared the immediate area of the test site (no sooner than 2 s after impact), after which the brakes were activated, if needed, to bring the test vehicle to a safe and controlled stop.

4.3 DATA ACQUISITION SYSTEMS

4.3.1 Vehicle Instrumentation and Data Processing

Each test vehicle was instrumented with a self-contained, on-board data acquisition system. The signal conditioning and acquisition system is a 16-channel, Tiny Data Acquisition System (TDAS) Pro produced by Diversified Technical Systems, Inc. The accelerometers, which measure the x, y, and z axis of vehicle acceleration, are strain gauge type with linear millivolt output proportional to acceleration. Angular rate sensors, measuring vehicle roll, pitch, and yaw rates, are ultra-small, solid state units designed for crash test service. The TDAS Pro hardware

and software conform to the latest SAE J211, Instrumentation for Impact Test. Each of the 16 channels is capable of providing precision amplification, scaling, and filtering based on transducer specifications and calibrations. During the test, data are recorded from each channel at a rate of 10,000 samples per second with a resolution of one part in 65,536. Once data are recorded, internal batteries back these up inside the unit should the primary battery cable be severed. Initial contact of the pressure switch on the vehicle bumper provides a time zero mark and initiates the recording process. After each test, the data are downloaded from the TDAS Pro unit into a laptop computer at the test site. The Test Risk Assessment Program (TRAP) software then processes the raw data to produce detailed reports of the test results.

Each of the TDAS Pro units is returned to the factory annually for complete recalibration and all instrumentation used in the vehicle conforms to all specifications outlined by SAE J211. All accelerometers are calibrated annually by means of an ENDEVCO® 2901, precision primary vibration standard. This standard and its support instruments are checked annually and receive a National Institute of Standards Technology (NIST) traceable calibration. The rate transducers used in the data acquisition system receive a calibration via a Genisco Rate-of-Turn table. The subsystems of each data channel are also evaluated annually, using instruments with current NIST traceability, and the results are factored into the accuracy of the total data channel, per SAE J211. Calibrations and evaluations are also made any time data are suspect. Acceleration data are measured with an expanded uncertainty of ± 1.7 percent at a confidence factor of 95 percent (k=2).

TRAP uses the data from the TDAS Pro to compute occupant/compartment impact velocities, time of occupant/compartment impact after vehicle impact, and the highest 10-millisecond (ms) average ridedown acceleration. TRAP calculates change in vehicle velocity at the end of a given impulse period. In addition, maximum average accelerations over 50-ms intervals in each of the three directions are computed. For reporting purposes, the data from the vehicle-mounted accelerometers are filtered with an SAE Class 180-Hz low-pass digital filter, and acceleration versus time curves for the longitudinal, lateral, and vertical directions are plotted using TRAP.

TRAP uses the data from the yaw, pitch, and roll rate transducers to compute angular displacement in degrees at 0.0001-s intervals, then plots yaw, pitch, and roll versus time. These displacements are in reference to the vehicle-fixed coordinate system with the initial position and orientation of the vehicle-fixed coordinate systems being initial impact. Rate of rotation data is measured with an expanded uncertainty of ± 0.7 percent at a confidence factor of 95 percent (k=2).

4.3.2 Anthropomorphic Dummy Instrumentation

An Alderson Research Laboratories Hybrid II, 50th percentile male anthropomorphic dummy, restrained with lap and shoulder belts, was placed in the front seat on the impact side of the 1100C vehicle. The dummy was not instrumented.

According to MASH, use of a dummy in the 2270P vehicle is optional. However, it is recommended a dummy be used when testing "any longitudinal barrier with a height greater than or equal to 33 inches." Use of the dummy in the 2270P vehicle is recommended for tall rails to

evaluate the "potential for an occupant to extend out of the vehicle and come into direct contact with the test article." Although this information is reported, it is not part of the impact performance evaluation. Since the rail height of the 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition was 34¾ inches, a dummy was placed in the front seat of the 2270P vehicle on the impact side and restrained with lap and shoulder belts.

A dummy was not used in MASH Test 3-21 test of the W-beam to thrie beam transition as the rail height at impact was 31 inches.

4.3.3 Photographic Instrumentation Data Processing

Photographic coverage of each test included three digital high-speed cameras:

- One overhead with a field of view perpendicular to the ground and directly over the impact point;
- One placed behind the installation at an angle; and
- A third placed to have a field of view parallel to and aligned with the installation at the downstream end.

A flashbulb on the impacting vehicle was activated by a pressure-sensitive tape switch to indicate the instant of contact with the transition. The flashbulb was visible from each camera. The video files from these digital high-speed cameras were analyzed to observe phenomena occurring during the collision and to obtain time-event, displacement, and angular data. A digital camera recorded and documented conditions of each test vehicle and the installation before and after the test.

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Chapter 5. *MASH* TEST 3-20 (CRASH TEST NO. 608331-01-4)

5.1 TEST DESIGNATION AND ACTUAL IMPACT CONDITIONS

MASH Test 3-20 involves an 1100C vehicle weighing 2420 lb ± 55 lb impacting the CIP of the transition at an impact speed of 62 mi/h ± 2.5 mi/h and an angle of 25° ± 1.5 °. The target CIP for MASH Test 3-20 on the 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition was 5.10 ft ± 1 ft upstream of the end of the concrete curb/deck. Figure 5.1 depicts the target CIP.



Figure 5.1. Transition/Test Vehicle Geometrics for Test No. 608331-01-4.

The 2007 Kia Rio* used in the test weighed 2446 lb, and the actual impact speed and angle were 60.9 mi/h and 26.5°, respectively. The actual impact point was 6.06 ft upstream of the end of the concrete curb/deck. Minimum target impact severity (IS) was 51 kip-ft, and actual IS was 61 kip-ft.

5.2 WEATHER CONDITIONS

The test was performed on the morning of September 2, 2019. Weather conditions at the time of testing were as follows: wind speed: 4 mi/h; wind direction: 105° (vehicle was traveling at magnetic heading of 335°); temperature: 93°F; relative humidity: 53 percent.

5.3 TEST VEHICLE

Figures 5.1 and 5.2 show the 2007 Kia Rio used for the crash test. The vehicle's test inertia weight was 2446 lb, and its gross static weight was 2611 lb. The height to the lower edge of the vehicle bumper was 7.75 inches, and height to the upper edge of the bumper was 21.5 inches. Table D.1 in Appendix D1 gives additional dimensions and information on the

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^{*} The 2007 model vehicle used is older than the 6-year age noted in MASH, and was selected based upon availability. An older model vehicle is permitted by AASHTO as long as it is otherwise MASH compliant. Other than the vehicle's year model, this 2007 model vehicle met the MASH requirements.

vehicle. The vehicle was directed into the installation using a cable reverse tow and guidance system, and was released to be freewheeling and unrestrained just prior to impact.



Figure 5.2. Test Vehicle before Test No. 608331-01-4.

5.4 TEST DESCRIPTION

The test vehicle was traveling at an impact speed of 60.9 mi/h when it contacted the 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition 6.06 ft upstream of the end of the concrete curb/deck at an impact angle of 26.5°. Table 5.1 lists events that occurred during Test No. 608331-01-4. Figures D.1 and D.2 in Appendix D2 present sequential photographs during the test.

TIME (s)	EVENTS
0.000	Vehicle contacts transition
0.023	Vehicle begins to redirect
0.091	Vehicle makes a slight increase in clockwise yaw rate
0.234	Vehicle traveling parallel with transition
0.355	Left rear corner and bumper of vehicle contacts transition
0.447	Vehicle loses contact with transition while traveling at 39.5 mi/h,
	trajectory of 7.1°, and heading of 14.0°

Table 5.1. Events during Test No. 608331-01-4.

For longitudinal barriers, it is desirable that the vehicle redirects and exits the barrier within the exit box criteria (not less than 32.8 ft downstream from loss of contact for cars and pickups). The test vehicle exited within the exit box criteria defined in *MASH*. After loss of contact with the transition, the vehicle came to rest 145 ft downstream of the impact point and 137 ft toward the traffic lanes.

5.5 DAMAGE TO TEST INSTALLATION

Figure 5.3 shows the damage to the 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition. Posts 12 through 15 were leaning back at 89°, and the soil was disturbed around each

of those posts. There was no visible soil disturbance at posts 1 and 2. The bottom edge of the thrie beam rail was deformed in the impact area, and the concrete deck cracked at post 16 (the first post on the bridge deck). Working width* was 26.1 inches, and height of working width was 34.75 inches. Maximum dynamic deflection during the test was 3.5 inches, and maximum permanent deformation was 1.25 inches.

5.6 DAMAGE TO TEST VEHICLE

Figure 5.4 shows the damage sustained by the vehicle. The front bumper, hood, grill, radiator and support, left front strut and tower, left lower control arm, left front tire and rim, left front fender, left front door and glass, left front floor pan, and left rear quarter panel were damaged. No fuel tank damage was observed. The windshield sustained stress cracks from displacement of the left A-pillar, and the roof was slightly deformed. A small hole in the windshield was caused by the impact of the hood. Maximum exterior crush to the vehicle was 14.0 inches in the side plane at the left front corner at bumper height. Maximum occupant compartment deformation was 3.5 inches in the left kick panel area. Figure 5.5 shows the interior of the vehicle. Tables D.3 and D.4 in Appendix D1 provide exterior crush and occupant compartment measurements.

5.7 OCCUPANT RISK FACTORS

Data from the accelerometers were digitized for evaluation of occupant risk, and the results are shown in Table 5.2. Figure D.3 in Appendix D3 shows the vehicle angular displacements, and Figures D.4 through D.6 in Appendix D4 show acceleration versus time traces. Figure 5.6 summarizes pertinent information from the test.

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^{*} Per MASH, "The working width is the maximum dynamic lateral position of any major part of the system or vehicle. These measurements are all relative to the pre-impact traffic face of the test article." In other words, working width is the total barrier width plus the maximum dynamic intrusion of any portion of the barrier or test vehicle past the field side edge of the barrier.



Figure 5.3. Transition after Test No. 608331-01-4.



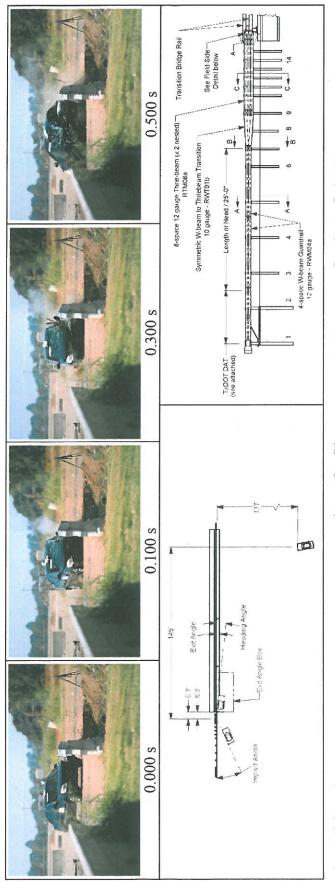
Figure 5.4. Test Vehicle after Test No. 608331-01-4.



Figure 5.5. Interior of Test Vehicle after Test No. 608331-01-4.

Table 5.2. Occupant Risk Factors for Test No. 608331-01-4.

Occupant Risk Factor	Value	Time
Occupant Impact Velocity (OIV)		
Longitudinal	22.6 ft/s	at 0.0824 s on left side of interior
Lateral	30.5 ft/s	at 0.0824 \$ 611 left side of interior
Occupant Ridedown Accelerations		State of the second
Longitudinal	14.5 g	0.0975 - 0.1075 s
Lateral	9.2 g	0.0940 - 0.1040 s
Theoretical Head Impact Velocity (THIV)	41.0 km/h 11.4 m/s	at 0.0805 s on left side of interior
Acceleration Severity Index (ASI)	2.17	0.0496 - 0.0996 s
Maximum 50-ms Moving Average		
Longitudinal	−12.0 g	0.0292 - 0.0792 s
Lateral	16.8 g	0.0303 - 0.0803 s
Vertical	-3.6 g	0.0850 - 0.1350 s
Maximum Roll, Pitch, and Yaw Angles		
Roll	12°	1.9987 s
Pitch	3°	2.0000 s
Yaw	63°	1.5386 s



9. \$_	-	.0° Test Article Deflections Dynamic. Permanent Working Width. Height of Working Width	km/h	
Impact Conditions T1) Speed	Impact Severity	Trajectory/Heading Ar Occupant Risk Values Longitudinal OIV Lateral OIV Longitudinal Ridedown	Σ	Longitudinal
Texas A&M Transportation Institute (TTI) MASH Test 3-20 608331-01-4 2019-09-02	Transition 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition	207 ft 3½ inches (incl 154 ft of deck) Thrie beam guardrail terminal to 38-inch tall 2-tube bridge rail, 34% inch tall thrie beam guardrail section, symmetrical W-beam to thrie beam terminal, 25 ft of W-beam guardrail		1100C 2007 Kia Rio 2470 lb 2446 lb 165 lb 2611 lb
General Information Test Agency	Test Article Type Name	Installation Length	Soil Type and Condition Test Vehicle	Type/Designation Make and Model Curb Test Inertial Dummy Gross Static

Figure 5.6. Summary of Results for MASH Test 3-20 on 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition.

Chapter 6. MASH TEST 3-21 AT TRANSITION FROM THRIE BEAM TO BRIDGE RAIL (CRASH TEST NO. 608331-01-5)

6.1 TEST DESIGNATION AND ACTUAL IMPACT CONDITIONS

MASH Test 3-21 involves a 2270P vehicle weighing 5000 lb ± 110 lb impacting the CIP of the transition at an impact speed of 62 mi/h ± 2.5 mi/h and an angle of 25° ± 1.5 °. The target CIP for MASH Test 3-21 on the 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition was 7.00 ft ± 1 ft upstream of the end of the concrete curb/deck. Figure 6.1 depicts the target CIP.





Figure 6.1. 2019 Transition/Test Vehicle Geometrics for Test No. 608331-01-5.

The 2013 RAM 1500 pickup truck used in the test weighed 5050 lb, and the actual impact speed and angle were 61.9 mi/h and 25.3°, respectively. The actual impact point was 6.52 ft upstream of the end of the concrete curb/deck. Minimum target IS was 106 kip-ft, and actual IS was 118 kip-ft.

6.2 WEATHER CONDITIONS

The test was performed on the morning of September 5, 2019. Weather conditions at the time of testing were as follows: wind speed: 2 mi/h; wind direction: 244° (vehicle was traveling at magnetic heading of 335°); temperature: 91°F; relative humidity: 57 percent.

6.3 TEST VEHICLE

Figures 6.1 and 6.2 show the 2013 RAM 1500 pickup truck used for the crash test. The vehicle's test inertia weight was 5050 lb, and its gross static weight was 5215 lb. The height to the lower edge of the vehicle bumper was 11.75 inches, and height to the upper edge of the bumper was 27.0 inches. The height to the vehicle's center of gravity was 28.25 inches. Tables E.1 and E.2 in Appendix E1 give additional dimensions and information on the vehicle. The vehicle was directed into the installation using a cable reverse tow and guidance system, and was released to be freewheeling and unrestrained just prior to impact.



Figure 6.2. Test Vehicle before Test No. 608331-01-5.

6.4 TEST DESCRIPTION

The test vehicle was traveling at an impact speed of 61.9 mi/h when it contacted the 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition 6.52 ft upstream of the end of the concrete curb/deck at an impact angle of 25.3°. Table 6.1 lists events that occurred during Test No. 608331-01-5. Figures E.1 and E.2 in Appendix E2 present sequential photographs during the test.

TIME (s)	EVENTS
0.000	Vehicle contacts transition
0.035	Vehicle begins to redirect
0.149	Right front tire leaves the pavement
0.210	Vehicle traveling parallel with transition
0.207	Left rear bumper and corner of vehicle contacts transition
0.377 Vehicle loses contact with transition while traveling at 47.9 mi/h trajectory of 6.9°, and heading of 6.5°	

Table 6.1. Events during Test No. 608331-01-5.

For longitudinal barriers, it is desirable that the vehicle redirects and exits the barrier within the exit box criteria (not less than 32.8 ft downstream from loss of contact for cars and pickups). The test vehicle exited within the exit box criteria defined in *MASH*. Brakes on the vehicle were applied at 3.0 s after impact, and the vehicle subsequently came to rest 174 ft downstream of the impact point.

6.5 DAMAGE TO TEST INSTALLATION

Figure 6.3 shows the damage to the 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition. There was no visible indication of movement at posts 1 through 10. The soil was disturbed around post 10, and posts 10, 11, and 12 were leaning 89° toward the field side. There was a 0.5-inch gap in the soil on the traffic side of post 12. Posts 13-15 were leaning slightly toward field side, posts 13 and 15 had an 0.5-inch gap between the posts and soil on the traffic

and field sides, and post 14 on the field side only. Working width* was 26.9 inches, and height of working width was 34.75 inches. Maximum dynamic deflection during the test was 6.1 inches, and maximum permanent deformation was 3.75 inches.

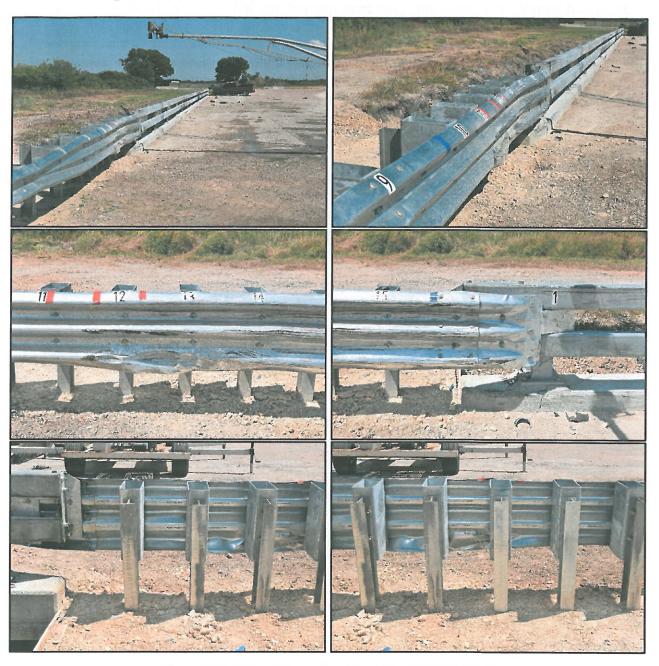


Figure 6.3. Transition after Test No. 608331-01-5.

^{*} Per MASH, "The working width is the maximum dynamic lateral position of any major part of the system or vehicle. These measurements are all relative to the pre-impact traffic face of the test article." In other words, working width is the total barrier width plus the maximum dynamic intrusion of any portion of the barrier or test vehicle past the field side edge of the barrier.

6.6 DAMAGE TO TEST VEHICLE

Figure 6.4 shows the damage sustained by the vehicle. The front bumper, hood, grill, radiator and support, left front fender, left front tire and rim, left upper and lower A-arms, left front door and window glass, left front floor pan, left rear door, left rear cab corner, left rear exterior bed, left rear rim, and rear bumper were damaged. No fuel tank damage was observed. Maximum exterior crush to the vehicle was 15.0 inches in the side plane at the left front at bumper height. Maximum occupant compartment deformation was 4.0 inches in the left side kick panel. Figure 5.5 shows the interior of the vehicle. Tables E.3 and E.4 in Appendix E1 provide exterior crush and occupant compartment measurements.



Figure 6.4. Test Vehicle after Test No. 608331-01-5.



Figure 6.5. Interior of Test Vehicle after Test No. 608331-01-5.

6.7 OCCUPANT RISK FACTORS

Data from the accelerometers were digitized for evaluation of occupant risk, and the results are shown in Table 6.2. Figure E.3 in Appendix E3 shows the vehicle angular displacements, and Figures E.4 through E.6 in Appendix E4 show acceleration versus time traces. Figure 6.6 summarizes pertinent information from the test.

Table 6.2. Occupant Risk Factors for Test No. 608331-01-5.

Occupant Risk Factor	Value	Time	
OIV			
Longitudinal	20.3 ft/s	at 0.1075 s on left side of interior	
Lateral	23.6 ft/s		
Occupant Ridedown Accelerations		100000000000000000000000000000000000000	
Longitudinal	7.4 g	0.1313 - 0.1413 s	
Lateral	13.0 g	0.2459 - 0.2559 s	
THIV	9.3 m/s	at 0.1042 s on left side of interior	
ASI	1.51	0.0598 - 0.1098 s	
Maximum 50-ms Moving Average			
Longitudinal	-8.7 g	0.0477 - 0.0977 s	
Lateral	10.9 g	0.0386 - 0.0886 s	
Vertical	-4.7 g	0.0572 - 0.1072 s	
Maximum Roll, Pitch, and Yaw Angles			
Roll	8°	1.1616 s	
Pitch	11°	1.9957 s	
Yaw	43°	0.8706 s	

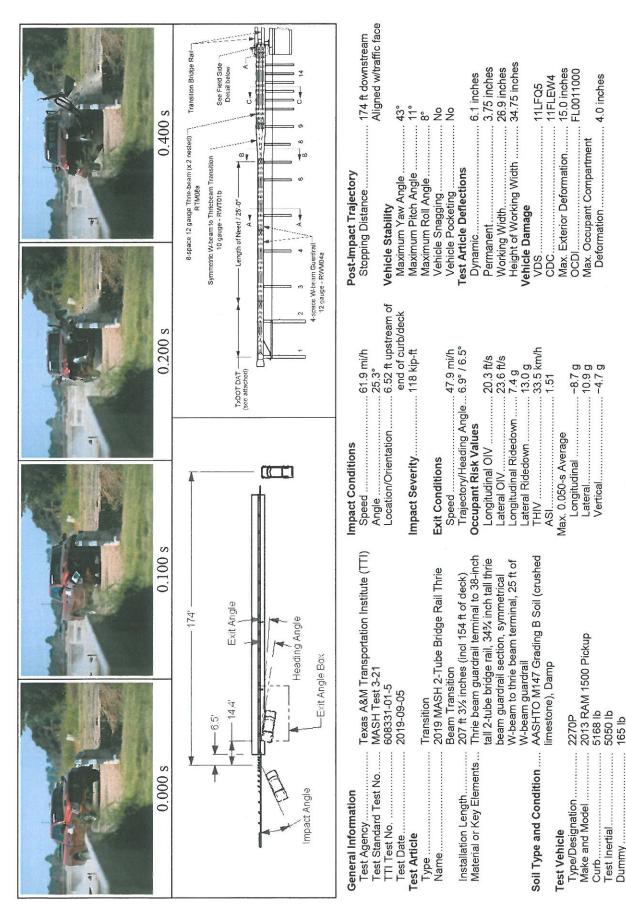


Figure 6.6. Summary of Results for MASH Test 3-21 on 2019 MASH 2-Tube Transition from Thrie Beam to Bridge Rail. Gross Static ..

5215 lb

Chapter 7. MASH TEST 3-21 AT TRANSITION FROM W-BEAM TO THRIE BEAM (CRASH TEST NO. 608331-01-6)

7.1 TEST DESIGNATION AND ACTUAL IMPACT CONDITIONS

MASH Test 3-21 involves a 2270P vehicle weighing 5000 lb ± 110 lb impacting the CIP of the transition at an impact speed of 62 mi/h ± 2.5 mi/h and an angle of 25° ± 1.5 °. The target CIP for MASH Test 3-21 on the 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition was 7.3 ft ± 1 ft upstream of the centerline of post 7. Figure 7.1 depicts the target CIP.





Figure 7.1. Transition/Test Vehicle Geometrics for Test No. 608331-01-6.

The 2013 RAM 1500 used in the test weighed 5038 lb, and the actual impact speed and angle were 62.6 mi/h and 24.9°. The actual impact point was 7.5 ft upstream of the centerline of post 7. Minimum target IS was 106 kip-ft, and actual IS was 117 kip-ft.

7.2 WEATHER CONDITIONS

The test was performed on the morning of December 19, 2019. Weather conditions at the time of testing were as follows: wind speed: 1 mi/h; wind direction: 140° (vehicle was traveling at magnetic heading of 335°); temperature: 45°F; relative humidity: 66 percent.

7.3 TEST VEHICLE

Figure 7.2 shows the 2013 RAM 1500 pickup truck used for the crash test. The vehicle's test inertia weight was 5038 lb, and its gross static weight was 5038 lb. The height to the lower edge of the vehicle bumper was 11.75 inches, and height to the upper edge of the bumper was 27.0 inches. The height to the vehicle's center of gravity was 29.0 inches. Tables F.1 and F.2 in Appendix F1 give additional dimensions and information on the vehicle. The vehicle was directed into the installation using a cable reverse tow and guidance system, and was released to be freewheeling and unrestrained just prior to impact.



Figure 7.2. Test Vehicle before Test No. 608331-01-6.

7.4 TEST DESCRIPTION

Table 7.1 lists events that occurred during Test No. 608331-01-6. Figures F.1 and F.2 in Appendix F2 present sequential photographs during the test.

TIME (s)	EVENTS
0.000	Vehicle contacts transition
0.017	Post 5 and 6 begin to deflect toward protected side
0.028	Vehicle begins to redirect
0.028	Post 7 begins to deflect toward protected side
0.053	Post 4 begins to rotate counter-clockwise
0.125	Right front tire lifts off pavement
0.203	Right rear tire lifts off pavement
0.284	Vehicle is traveling parallel with transition
0.609	Vehicle loses contact with transition while traveling at 31.8 mi/h,
	trajectory of 23.3°, and heading of 24.7°
0.776	Right front tire makes contact with pavement
0.885	Left rear tire makes contact with pavement

Table 7.1. Events during Test No. 608331-01-6.

For longitudinal barriers, it is desirable that the vehicle redirects and exits the barrier within the exit box criteria (not less than 32.8 ft downstream from loss of contact for cars and pickups). The test vehicle exited within the exit box criteria defined in *MASH*. Brakes on the vehicle were applied at 3.5 s after impact. After loss of contact with the barrier, the vehicle came to rest 133 ft downstream of the impact and 2 ft toward traffic lanes.

7.5 DAMAGE TO TEST INSTALLATION

Figures 7.3 through 7.5 show the damage to the transition. The metal rail element released from posts 1-5 and 7-10. Post 1 was pulled downstream 0.75 inch and post 2 was split.

Post 5 was leaning toward field side 88°, and there was a gap between the soil and post of 0.5 inch on the field side and 1.0 inch on the traffic side. Post 6 was leaning toward field side 76°, and there was a gap between the soil and post of 1.5 inches on the field side and 6.0 inches on the traffic side. Posts 7 through 9 were pushed toward field side and downstream. Post 10 was leaning toward field side 80°, and the gap between the soil and post was 3.0 inches on the field side and 0.75 inch on the traffic side. Post 11 was leaning toward field side 84°, and the gap between the soil and post was 3.0 inches on the field side. Post 12 was leaning toward field side 87°, and the gap between the post and soil was 0.13 inches on the traffic side and 1.5 inches on the field side. Post 13 was leaning toward field side 88°, and the post was pushed toward field side 0.75 inch. Post 14 was pushed toward field side 0.5 inch, and the soil around post 15 was disturbed only. Working width* was 44.7 inches, and height of working width was 61.8 inches. Maximum dynamic deflection during the test was 33.6 inches, and maximum permanent deformation was 28.0 inches.



Figure 7.3. Transition after Test No. 608331-01-6.

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^{*} Per MASH, "The working width is the maximum dynamic lateral position of any major part of the system or vehicle. These measurements are all relative to the pre-impact traffic face of the test article." In other words, working width is the total barrier width plus the maximum dynamic intrusion of any portion of the barrier or test vehicle past the field side edge of the barrier.



Figure 7.4. Posts 1 through 5 after Test No. 608331-01-6.



Figure 7.5. Posts 6 through 15 after Test No. 608331-01-6.

7.6 DAMAGE TO TEST VEHICLE

Figure 7.6 shows the damage sustained by the vehicle. The front bumper, radiator and support, hood, grill, left front fender, left frame rail, left upper and lower control arms, left front tire and rim, left front door, left rear exterior bed, left rear rim, and rear bumper were damaged. No fuel tank damage was observed. The windshield showed stress cracks radiating upward and inward from the lower left A-post. Maximum exterior crush to the vehicle was 20.0 inches in the side plane at the left front corner at bumper height. No occupant compartment deformation or intrusion was observed. Figure 7.7 shows the interior of the vehicle. Tables F.3 and F.4 in Appendix F1 provide exterior crush and occupant compartment measurements.

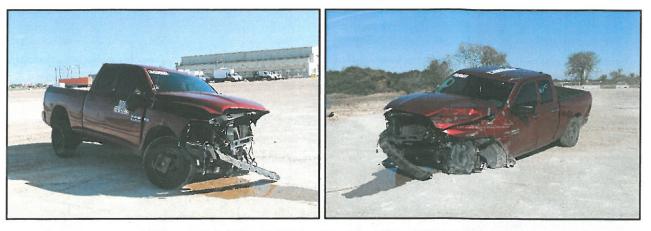


Figure 7.6. Test Vehicle after Test No. 608331-01-6.

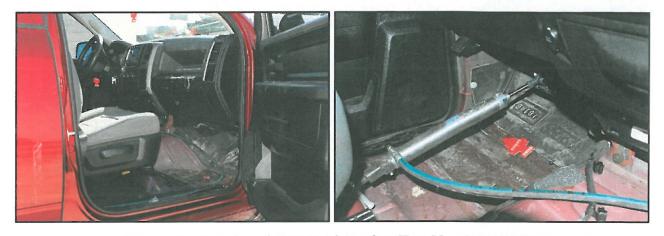


Figure 7.7. Interior of Test Vehicle after Test No. 608331-01-6.

7.7 OCCUPANT RISK FACTORS

Data from the accelerometers were digitized for evaluation of occupant risk, and the results are shown in Table 7.2. Figure F.3 in Appendix F3 shows the vehicle angular displacements, and Figures F.4 through F.6 in Appendix F4 show acceleration versus time traces. Figure 7.8 summarizes pertinent information from the test.

Table 7.2. Occupant Risk Factors for Test No. 608331-01-6.

Occupant Risk Factor	Value	Time
OIV		14
Longitudinal	24.9 ft/s	-+0142016:1-6:-:
Lateral	16.4 ft/s	at 0.1439 s on left side of interior
Occupant Ridedown Accelerations		
Longitudinal	10.7 g	0.1467 - 0.1567 s
Lateral	9.8 g	0.2125 - 0.2225 s
THIV	8.6 m/s	at 0.1373 s on left side of interior
ASI	1.02	0.2115 - 0.2615 s
Maximum 50-ms Moving Average		
Longitudinal	−9.1 g	0.1163 - 0.1663 s
Lateral	7.7 g	0.1863 - 0.2363 s
Vertical	-4.6 g	0.7919 - 0.8419 s
Maximum Roll, Pitch, and Yaw Angles		
Roll	15°	0.7865 s
Pitch	14°	0.8046 s
Yaw	53°	0.8341 s

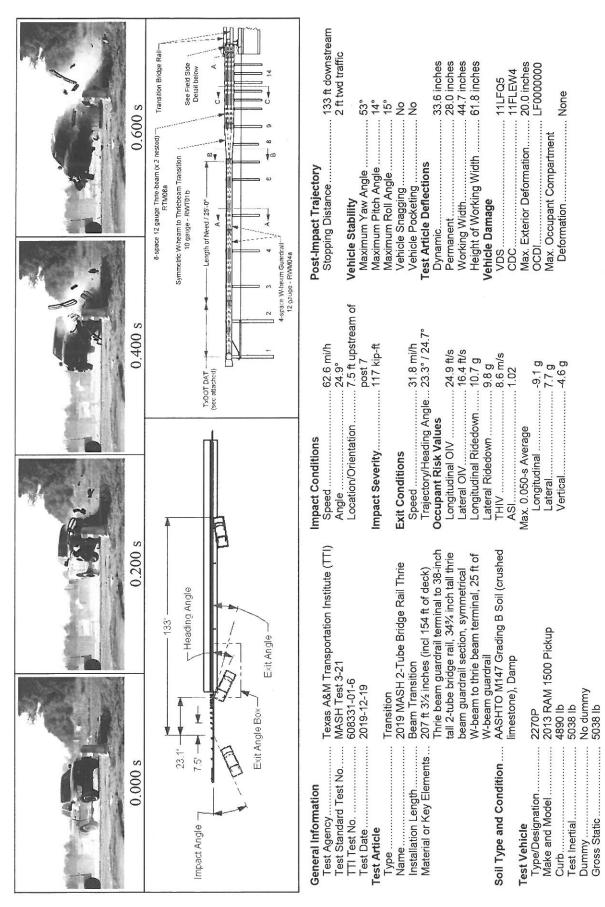


Figure 7.8. Summary of Results for MASH Test 3-21 2019 MASH 2-Tube Transition from W-Beam to Thrie Beam.

Chapter 8. SUMMARY AND CONCLUSIONS

8.1 ASSESSMENT OF TEST RESULTS

The crash tests reported herein were performed in accordance with *MASH* TL-3 transitions. An assessment of each test based on the applicable safety evaluation criteria for *MASH* TL-3 transitions is provided in Tables 8.1 through 8.3.

8.2 CONCLUSIONS

Table 8.4 shows the 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition performed acceptably as reported herein for a *MASH* TL-3 transition.

Table 8.1. Performance Evaluation Summary for MASH Test 3-20 on 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition.

Te	Test Agency: Texas A&M Transportation Institute	Test No.: 608331-01-4	Test Date: 2019-09-02
	MASH Test 3-20 Evaluation Criteria	Test Results	Assessment
St	Structural Adequacy		
A.	Test article should contain and redirect the vehicle or	The 2019 MASH 2-Tube Bridge Rail Thrie	
	bring the vehicle to a controlled stop; the vehicle	Beam Transition contained and redirected the	
	should not penetrate, underride, or override the	1100C vehicle. The vehicle did not penetrate,	Pass
	installation although controlled lateral deflection of	underride, or override the installation. Maximum	
	the test article is acceptable.	dynamic deflection was 3.5 inches.	
Ŏ	Occupant Risk		
D.	Detached elements, fragments, or other debris from	No detached elements, fragments, or other debris	
	the test article should not penetrate or show potential	were present to penetrate or show potential for	
	for penetrating the occupant compartment, or present	penetrating the occupant compartment, or present	
	an undue hazard to other traffic, pedestrians, or	hazard to others in the area.	Dog
	personnel in a work zone.		Газз
	Deformations of, or intrusions into, the occupant	Maximum occupant compartment deformation	
	compartment should not exceed limits set forth in	was 3.5 inches in the left kick panel area.	
	Section 5.2.2 and Appendix E of MASH.		
F.	The vehicle should remain upright during and after	The 1100C vehicle remained upright during and	
	collision. The maximum roll and pitch angles are not	after the collision event. Maximum roll and pitch	Pass
	to exceed 75 degrees.	angles were 12° and 3°, respectively.	
H.	Occupant impact velocities (OIV) should satisfy the	Longitudinal OIV was 22.6 ft/s, and lateral OIV	
	following limits: Preferred value of 30 ft/s, or	was 30.5 ft/s.	Pass
2767	maximum allowable value of 40 ft/s.		
I.	The occupant ridedown accelerations should satisfy	Longitudinal occupant ridedown acceleration	
	the following limits: Preferred value of 15.0 g, or	was 14.5 g, and lateral occupant ridedown	Pass
= =	maximum allowable value of 20.49 g.	acceleration was 9.2 g.	

Table 8.2. Performance Evaluation Summary for MASH Test 3-21 on 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition from Thrie Beam to Bridge Rail.

			·	
<u> </u>	rest /	Test Agency: Texas A&M Transportation Institute	Test No.: 608331-01-5	Test Date: 2019-09-05
		MASH Test 3-21 Evaluation Criteria	Test Results	Assessment
S	truc	Structural Adequacy		
4	A	Test article should contain and redirect the vehicle or	The 2019 MASH 2-Tube Bridge Rail Thrie	
	7	bring the vehicle to a controlled stop; the vehicle	Beam Transition contained and redirected the	
	-7	should not penetrate, underride, or override the	2270P vehicle. The vehicle did not penetrate,	Pass
	7	installation although controlled lateral deflection of	underride, or override the installation. Maximum	
	7	the test article is acceptable.	dynamic deflection was 6.1 inches.	
	noo(Occupant Risk		
T	D. 1	Detached elements, fragments, or other debris from	No detached elements, fragments, or other debris	
	1	the test article should not penetrate or show potential	were present to penetrate or show potential for	
-	-	for penetrating the occupant compartment, or present	penetrating the occupant compartment, or present	
	2	an undue hazard to other traffic, pedestrians, or	hazard to others in the area.	ć
	T	personnel in a work zone.		Fass
	7	Deformations of, or intrusions into, the occupant	Maximum occupant compartment deformation	
)	compartment should not exceed limits set forth in	was 4.0 inches in the left front kick panel.	
	- 4	Section 5.2.2 and Appendix E of MASH.		æ
F.		The vehicle should remain upright during and after	The 2270P vehicle remained upright during and	
	7	collision. The maximum roll and pitch angles are not	after the collision event. Maximum roll and pitch	Pass
	~	to exceed 75 degrees.	angles were 8° and 11°, respectively.	
F	Н. (Occupant impact velocities (OIV) should satisfy the	Longitudinal OIV was 20.3 ft/s, and lateral OIV	
	(following limits: Preferred value of 30 ft/s, or	was 23.6 ft/s.	Pass
	1	maximum allowable value of 40 ft/s.		
I.		The occupant ridedown accelerations should satisfy	Longitudinal occupant ridedown acceleration	
	1	the following limits: Preferred value of 15.0 g, or	was 7.4 g, and lateral occupant ridedown	Pass
	1.	maximum allowable value of 20.49 g.	acceleration was 13.0 g.	

Table 8.3. Performance Evaluation Summary for MASH Test 3-21 on 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition from W-Beam to Thrie Beam.

Te	Test Agency: Texas A&M Transportation Institute	Test No.: 608331-01-6	Test Date: 2019-12-19
	MASH Test 3-21 Evaluation Criteria	Test Results	Assessment
S	Structural Adequacy		,
Ä.	Test article should contain and redirect the vehicle or	The 2019 MASH 2-Tube Bridge Rail Thrie	
=	bring the vehicle to a controlled stop; the vehicle	Beam Transition contained and redirected the	
	should not penetrate, underride, or override the	2270P vehicle. The vehicle did not penetrate,	Pass
=	installation although controlled lateral deflection of	underride, or override the installation. Maximum	
	the test article is acceptable.	dynamic deflection was 33.6 inches.	
Ó	Occupant Risk		
D.	Detached elements, fragments, or other debris from	No detached elements, fragments, or other debris	
	the test article should not penetrate or show potential	were present to penetrate or show potential for	
200	for penetrating the occupant compartment, or present	penetrating the occupant compartment, or present	
	an undue hazard to other traffic, pedestrians, or	hazard to others in the area.	Doog
	personnel in a work zone.		I 455
_	Deformations of, or intrusions into, the occupant	No occupant compartment deformation or	
	compartment should not exceed limits set forth in	intrusion was observed.	
	Section 5.2.2 and Appendix E of MASH.		
F.	The vehicle should remain upright during and after	The 2270P vehicle remained upright during and	
	collision. The maximum roll and pitch angles are not	after the collision event. Maximum roll and pitch	Pass
	to exceed 75 degrees.	angles were 15° and 14°, respectively.	
H.	Occupant impact velocities (OIV) should satisfy the	Longitudinal OIV was 24.9 ft/s, and lateral OIV	
-	following limits: Preferred value of 30 ft/s, or	was 16.4 ft/s.	Pass
	maximum allowable value of 40 ft/s.		
T.	The occupant ridedown accelerations should satisfy	Longitudinal occupant ridedown acceleration	
	the following limits: Preferred value of 15.0 g, or	was 10.7 g, and lateral occupant ridedown	Pass
	maximum allowable value of 20.49 g.	acceleration was 9.8 g.	

Table 8.4. Assessment Summary for MASH TL-3 Testing on 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition.

Evaluation Factors	Evaluation Criteria	Test No. 608331-01-4	Test No. 608331-01-5	Test No. 608331-01-6
Structural Adequacy	A	S	S	S
	D	S	S	S
Occupant	F	S	S	S
Risk	Н	S	S	S
	I	S	S	S
MASH	Γest No.	MASH Test 3-20	MASH Test 3-21 at Transition to Bridge Rail	MASH Test 3-21 at Transition to Thrie Beam
Pass	/Fail	Pass	Pass	Pass

Key: S = Satisfactory

U = Unsatisfactory

NA = Not applicable

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REFERENCES

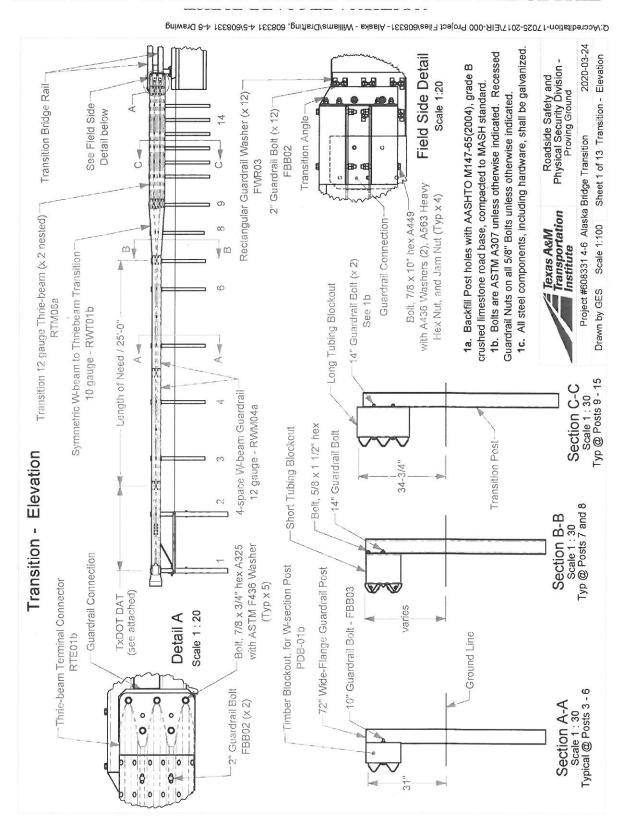
- C. E. Buth, W. F. Williams, W. L. Menges, and S. K. Schoeneman. NCHRP Report 350
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 Transportation Institute, College Station, TX, December 1998.
- 2. C. E. Buth, W. F. Williams, W. L. Menges, and S. K. Schoeneman. *NCHRP Report 350 Test 4-11 of the Alaska Multi-State Bridge Rail*, Test Report No.; 404311-2, Texas A&M Transportation Institute, College Station, TX, December 1998.
- 3. C. E. Buth, W. F. Williams, W. L. Menges, and S. K. Schoeneman. *NCHRP Report 350 Test 4-12 of the Alaska Multi-State Bridge Rail*, Test Report No.; 404311-3, Texas A&M Transportation Institute, College Station, TX, February 1998.
- 4. C. E. Buth, W. F. Williams, W. L. Menges, and S. K. Schoeneman. *NCHRP Report 350 Test 4-21 of the Alaska Multi-State Bridge Rail Thrie Beam Transition*, Test Report No.; 404311-5, Texas A&M Transportation Institute, College Station, TX, July 1999.
- 5. C. E. Buth, W. F. Williams, W. L. Menges, and S. K. Schoeneman. *NCHRP Report 350 Test 4-22 of the Alaska Multi-State Bridge Rail Thrie Beam Transition*, Test Report No.; 404311-6, Texas A&M Transportation Institute, College Station, TX, July 1999.
- 6. C. E. Buth, W. F. Williams, W. L. Menges, and S. K. Schoeneman. *NCHRP Report 350 Test 3-21 of the Alaska Multi-State Bridge Rail W-Beam Transition*, Test Report No.; 404311-7, Texas A&M Transportation Institute, College Station, TX, July 2000.
- 7. C. E. Buth, W. F. Williams, W. L. Menges, and S. K. Schoeneman. *NCHRP Report 350 Test 3-20 of the Alaska Multi-State Bridge Rail W-Beam Transition*, Test Report No.; 404311-8, Texas A&M Transportation Institute, College Station, TX, August 2000.
- 8. H. E. Ross, D. L. Sicking, R. A. Zimmer, and J. D. Michie, *Recommended Procedures for the Safety Performance Evaluation of Highway Features*, National Cooperative Highway Research Program Report 350, Transportation Research Board, National Research Council, Washington, D.C., 1993.
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- 10. AASHTO. Manual for Assessing Roadside Safety Hardware, Second Edition. 2016, American Association of State Highway and Transportation Officials: Washington, D.C.
- 11. AASHTO/FHWA Joint Implementation Agreement for Manual for Assessing Safety Hardware (MASH).

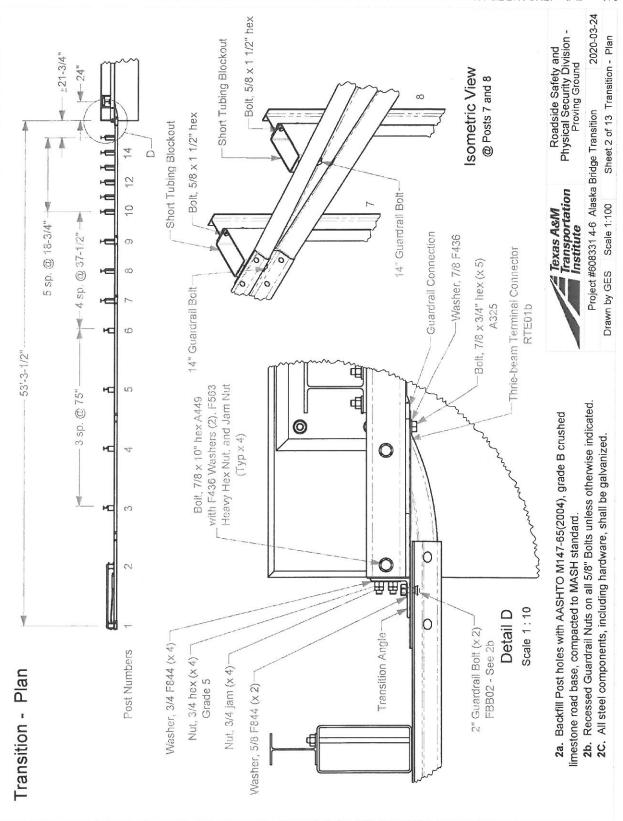
 https://safety.fhwa.dot.gov/roadway_dept/countermeasures/reduce_crash_severity/docs/memo_joint_implementation_agmt.pdf, January 7, 2016, last access January 2019.

TR No. 608331-4-6 39 2020-03-26

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APPENDIX A. DETAILS OF THE 2019 MASH 2-TUBE BRIDGE RAIL

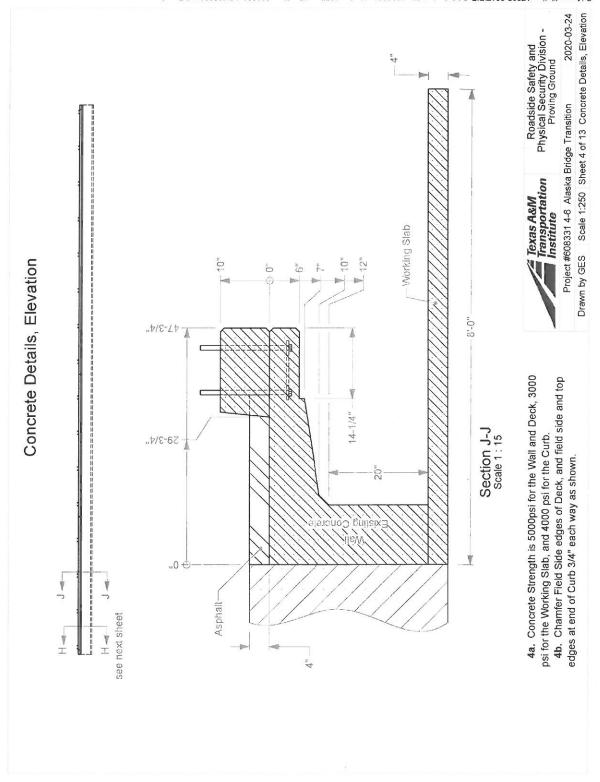


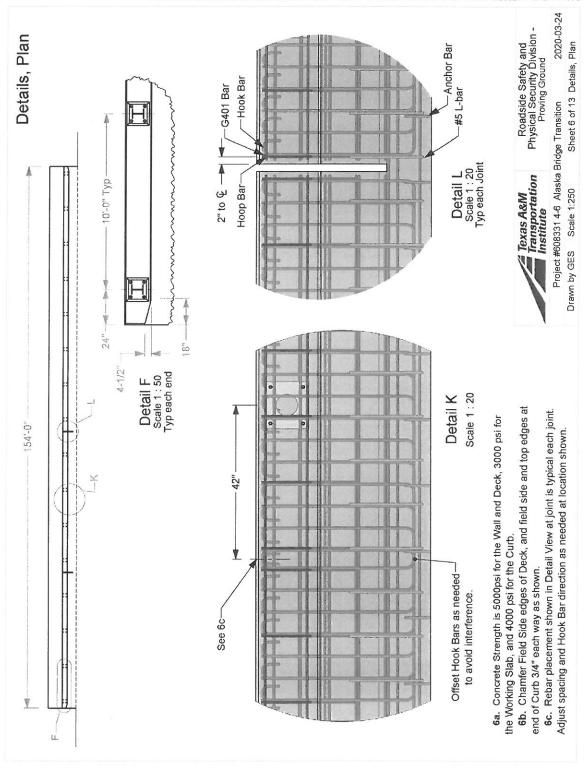


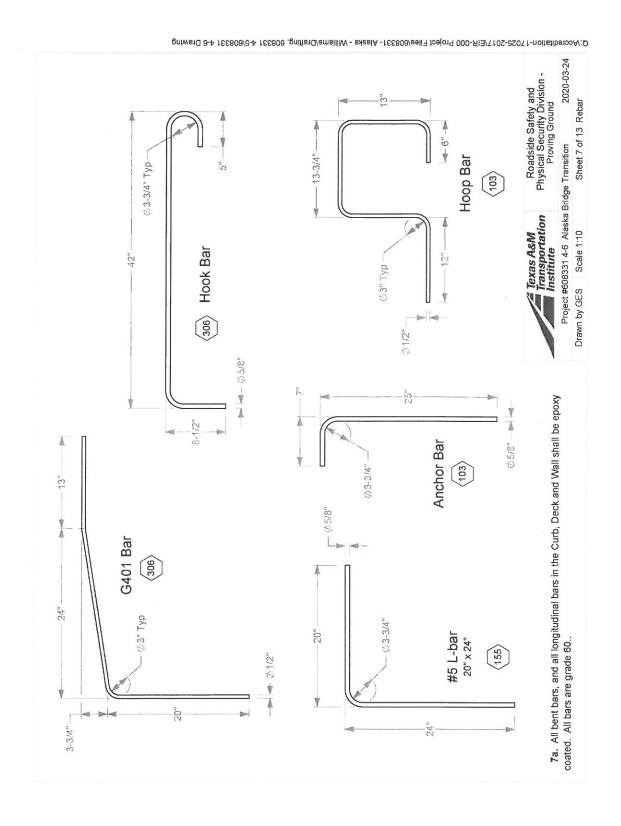
24"

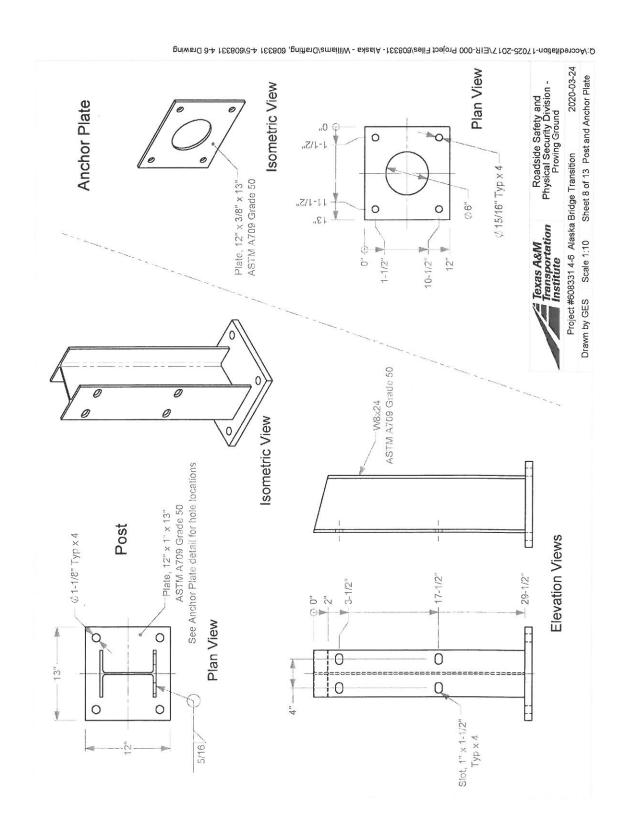
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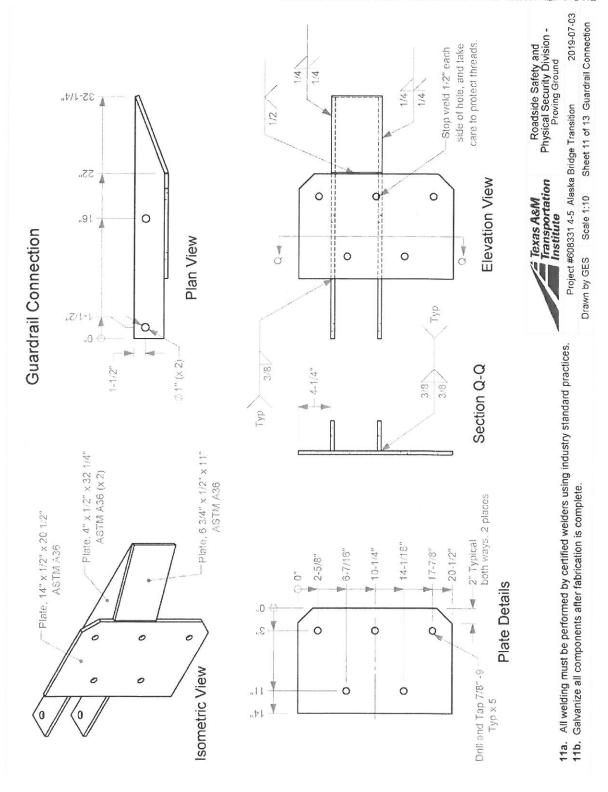
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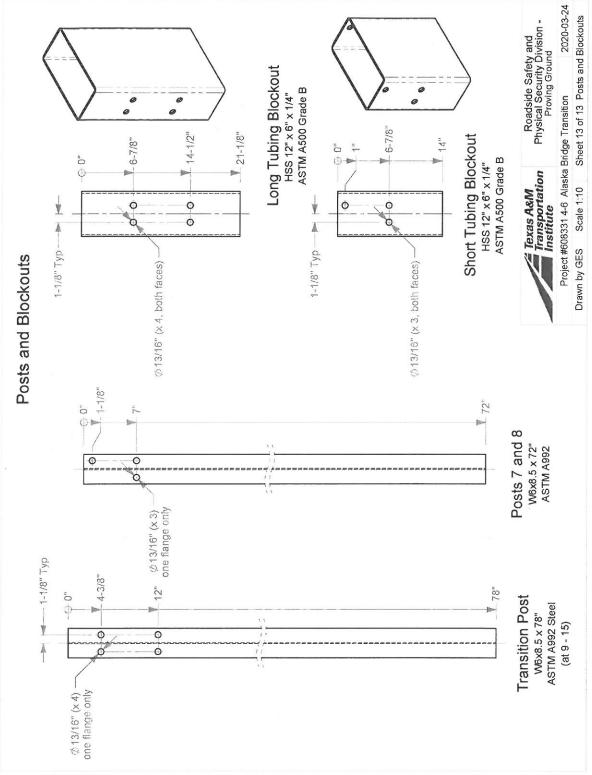


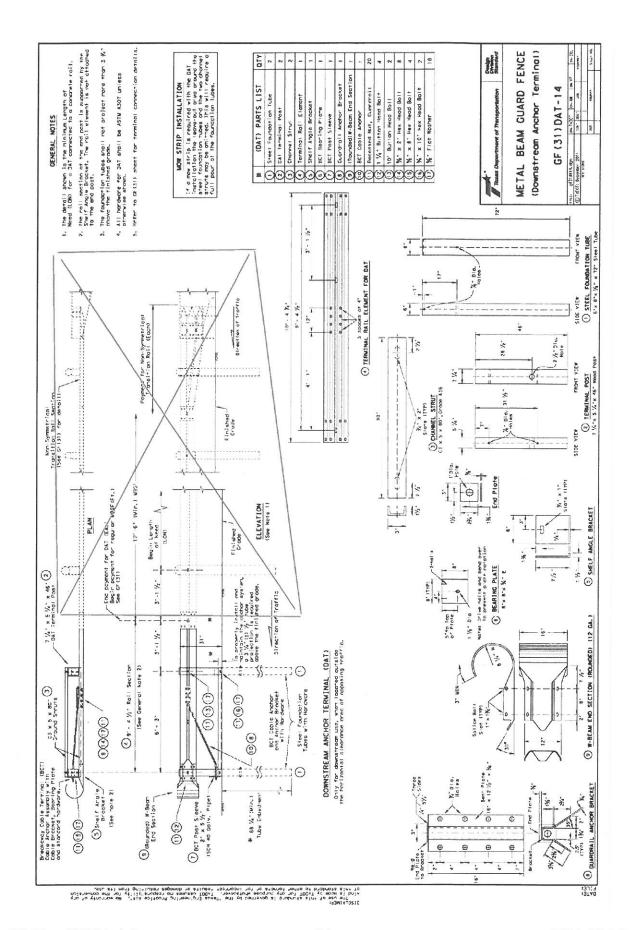


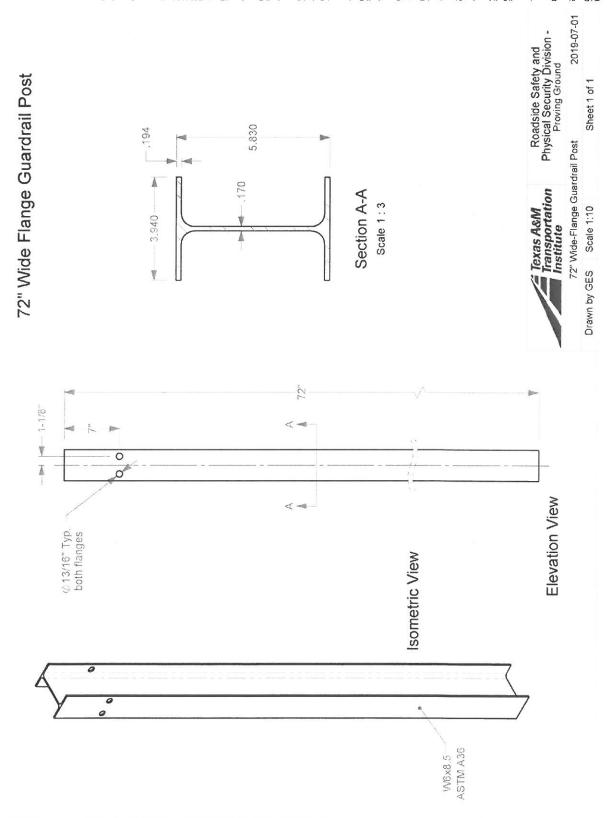


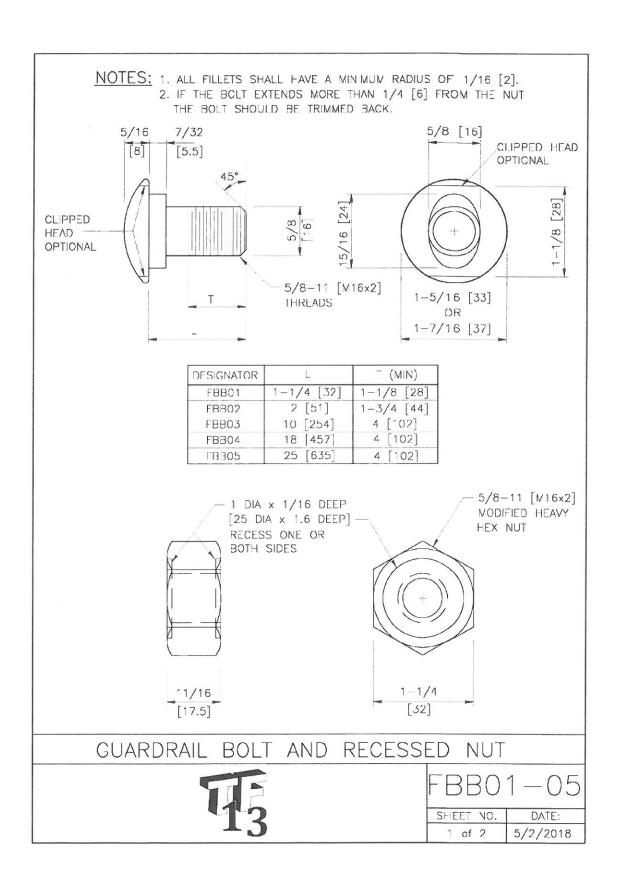












SPECIFICATIONS

The geometry and material specifications for this oval shoulder button-headed bolt and hex nut are found in AASHTO M 180. The bolt shall have 5/8-11 [M16x2] threads as defined in ANSI B1.1 [ANSI B1.13M] for Class 2A [6g] tolerances. Bolt material shall conform to ASTM A307 Grade A [ASTM F 568M Class 4.6], with a tensile strength of 60 ksi [400 MPa] and yield strength of 36 ksi [240 MPa]. Material for corrosion-resistant bolts shall conform to ASTM A325 Type 3 [ASTM F 568M Class 8.8.3], with tensile strength of 120 ksi [830 MPa] and yield strength of 92 ksi [660 MPa]. This bolt material has corrosion resistance comparable to ASTM A588 steels. Metric zinc-coated bolt heads shall be marked as specified in ASTM F 568 Section 9 with the symbol "4.6."

Nuts shall have ANSI B1.1 Class 2B [ANSI B1.13M Class 6h] 5/8-11 [M16x2] threads. The geometry of the nuts, with the exception of the recess shown in the drawing, shall conform to ANSI B18.2.2 [ANSI B18.2.4.1M Style 1] for zinc-coated hex nuts (shown in drawing) and ANSI B18.2.2 [ANSI B18.2.4.6M] for heavy hex corrosion-resistant nuts (not shown in drawing). Material for zinc-coated nuts shall conform to the requirements of AASHTO M 291 (ASTM A 563) Grade A [AASHTO M 291M (ASTM A 563M) Class 5], and material for corrosion-resistant nuts shall conform to the requirements of AASHTO M 291 (ASTM A 563) Grade C3 [AASHTO M 291M (ASTM A 563M) Class 8S3].

When zinc-coated bolts and nuts are required, the coating shall conform to either AASHTO M 232 (ASTM A 153/A 153M) for Class C or AASHTO M 298 (ASTM B 695) for Class 50. Zinc-coated nuts shall be tapped over-size as specified in AASHTO M 291 (ASTM A 563) [AASHTO M 291M (ASTM A 563M)], except that a diametrical allowance of 0.020 inch [0.510 mm] shall be used instead of 0.016 inches [0.420 mm].

	Stress Area of	Min. Bolt
Designator	Threaded Bolt Shank	Tensile Strength
10 - 2	$(in^2 [mm^2])$	(kips [kN])
FBB01-05	0.226 [157.0]	13.6 [62.8]

Dimensional tolerances not shown or implied are intended to be those consistent with the proper functioning of the part, including its appearance and accepted manufacturing practices.

INTENDED USE

These bolts and nuts are used in numerous guardrail and median barrier designs.

GUARDRAIL BOLT AND RECESSED NUT

FBB0	B01-05	
SHEET NO.	DATE	
2 of 2	5/2/2018	



Thrie-beam End Shoe 10 gauge (0.1345" before galvanizing)

R2"

2-3/8"

6-3/16"

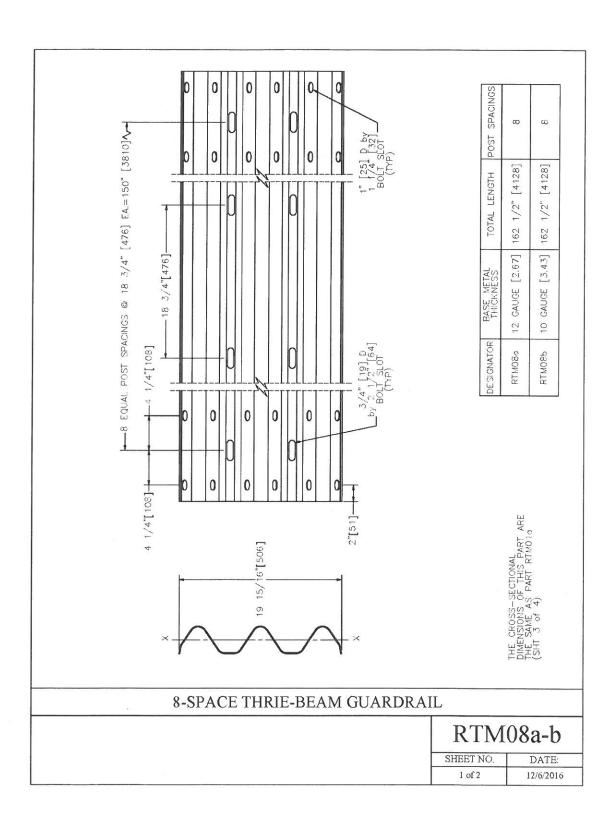
13-13/16"

10"

.08

20"

17-5/8"



SPECIFICATIONS

Corrugated sheet thrie beam guardrail shall conform to the current requirements of AASHTO M180. The section shall be manufactured from sheets with a nominal width of 29½" [750]. RTM08a shall conform to AASHTO M180 Class A and RTM08b shall conform to Class B. Thrie beams may be either Type I or II (zinc-coated) or Type IV (corrosion resistant steel). Corrosion resistant steel should conform to ASTM A606 for Type IV material and shall not be zinc-coated, painted or otherwise treated. Inertial properties are calculated for the whole cross-section without a reduction for the splice bolt holes or slots.

Designator	Area in. ² [10 ³ mm ²]	I _x in. ⁴ [10 ⁶ mm ⁴]	I _y in. ⁴ [10 ⁶ mm ⁴]	S_x in. ³ [10 ³ mm ³]	Sy in. ⁴ [10 ³ mm ³]
RTM08a	3.16 [2.0]	3.8 [1.6]		2.22 [36.4]	
RTM08b	4.03 [2.6]	4.8 [2.0]		2.87 [47.0]	

Dimensional tolerances not shown or implied are intended to be those consistent with the proper functioning of the part, including its appearance and accepted manufacturing practices.

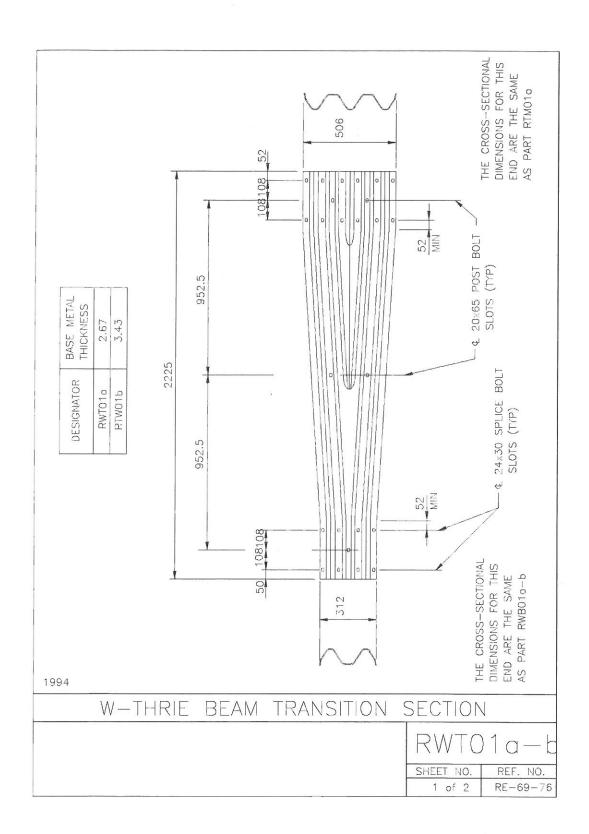
INTENDED USE

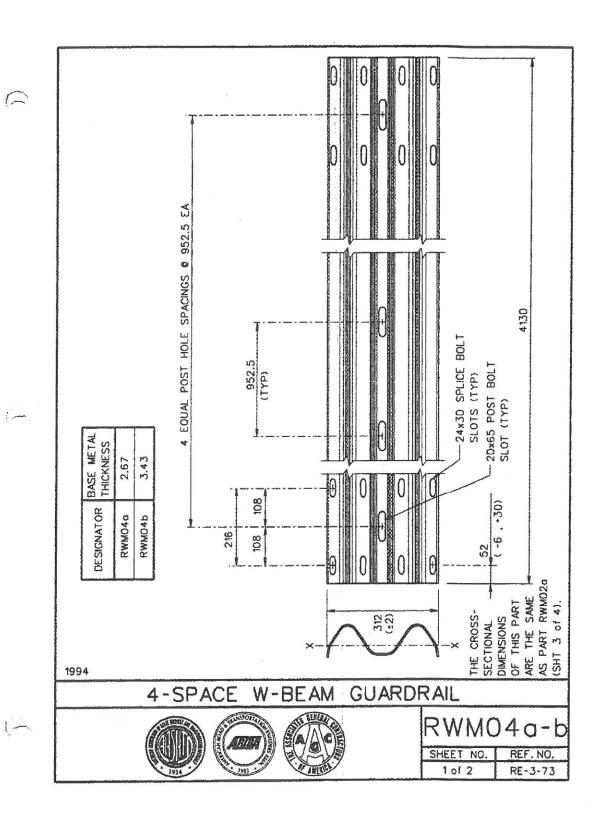
The 8-space thrie beam guardrail is used in the W-beam to thrie beam transition with standard posts (STG03a-b).

8-SPACE THRIE-BEAM GUARDRAIL

RTM08a-b

SHEET NO.	DATE:
2 of 2	12/6/2016





SPECIFICATIONS

Corrugated sheet steel beams shall conform to the current requirements of AASHTO M180. The section shall be manufactured from sheets with a nominal width of 483 mm. Guardrail RWM04a shall conform to AASHTO M180 Class A and RWM04b shall conform to Class B. Corrosion protection may be either Type II (zinc-coated) or Type IV (corrosion resistant steel). Corrosion resistant steel should conform to ASTM A606 for Type IV material and shall not be zinc-coated, painted or otherwise treated. Inertial properties are calculated for the whole cross-section without a reduction for the splice bolt holes.

Designator	Area (10 ³ mm ²)	1 _x (10 ⁶ mm ⁴)	I _y (10 ⁶ mm ⁴)	(10^3 mm^3)	S _y (10 ³ mm ³)	
RWM04a-b	1.3	1.0		23		

Dimensional tolerances not shown or implied are intended to be those consistent with the proper functioning of the part, including its appearance and accepted manufacturing practices.

INTENDED USE

This corrugated sheet steel beam is used as a rail element in transition systems STB02 and STB03 or when a reduced post spacing is desired in the SGR02, SGR04a-b, SGM02, and SGM04a-b.

4-SPACE W-BEAM GUARDRAIL

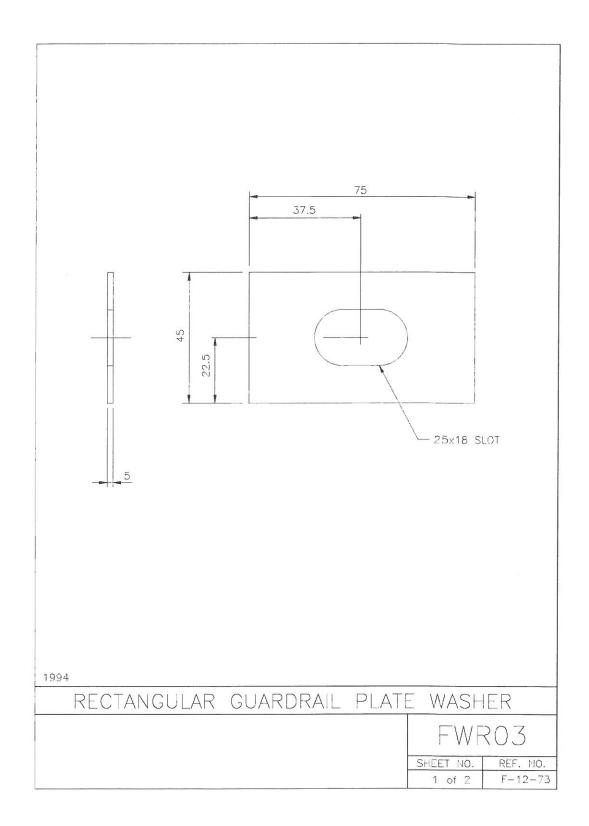
RWM04a-b

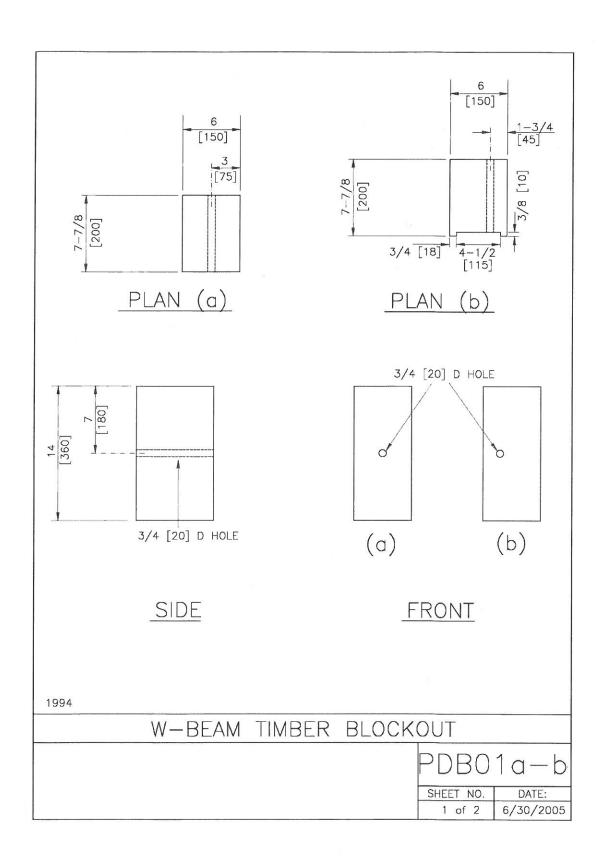
SHEET NO.	DATE
2 of 2	84-01-95











SPECTI	FICA	TION	JC

Blockouts shall be made of timber with a stress grade of at least 1160 psi [8 MPa]. Grading shall be in accordance with the rules of the West Coast Lumber Inspection Bureau, Southern Pine Inspection Bureau, or other appropriate timber association. Timber for blockouts shall be either rough-sawn (unplaned) or S4S (surfaced four sides) with nominal dimensions indicated. The variation in size of blockouts in the direction parallel to the axis of the bolt holes shall not be more than $\pm \frac{1}{4}$ inch [6 mm]. Only one type of surface finish shall be used for posts and blockouts in any one continuous length of guardrail.

All timber shall receive a preservation treatment in accordance with AASHTO M 133 after all end cuts are made and holes are drilled.

Dimensional tolerances not shown or implied are intended to be those consistent with the proper functioning of the part, including its appearance and accepted manufacturing practices.

INTENDED USE

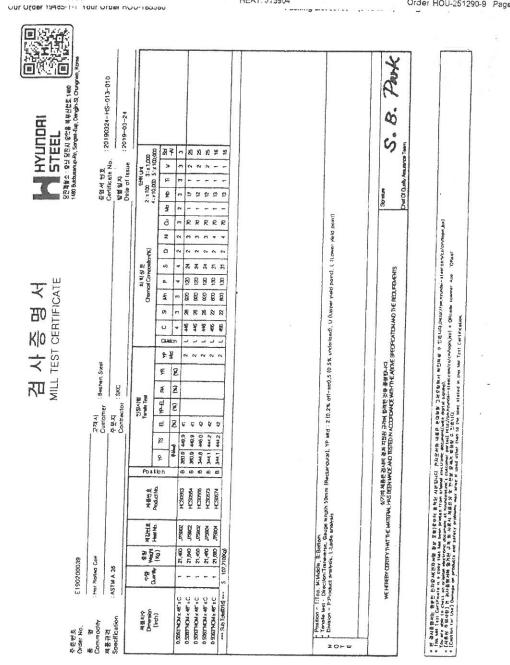
Blockout PDB01a is used with wood post PDE01 or PDE02 in the SGR04b strong-post W-beam guardrail and the SGM04b median barrier. Blockout PDB01b is routed to be used with steel post PWE01 or PWE02 in the SGR04c guardrail and the SGM04a median barrier.

W-BEAM TIMBER BLOCKOUT						
PDB0	1a-b					
SHEET NO.	DATE					
2 of 2	7/06/2005					

APPENDIX B. SUPPORTING CERTIFICATION DOCUMENTS

ATE A36 TEMPER LEVELED 2 X 48,0000" X 96,0000"			PO/REL HEAT	10U-35377 <i>i</i> : J75964		BL HOU-775673-8 5/21/2019 Order HOU-251290-9 Page:1				
5%		0000			CEF	RTIFIC	ATE OF	NALYSIS		
STEE	PROCES	SING				Number eference	38789-5 52133	6/18/201		
TRIPLE-S STEI 6000 JENSEN I HOUSTON, TX						Issued BESHERT JOINT VE STEEL WA TRIPLE-S: 15255 JAC HOUSTON	From STEEL PAOCESSING NUME OF MENOUSE CO 4. STEEL HOLDINGS INC INTO PORT BOLL CVI TX 77015	and the second		
Sold To: Ship To:		L SUPPLY CO., 6000 L. 6000 JENSEN DRIV	VE, HOUSTON, "	TX 77026	26					
Customer 100200/0 Your Order Our Order 19485-1-1 Packing Li			Ref HOU-18558 38789-1 (6/	ference 66 (6/12/2019) 18/2019)						
0.5000" x 42" x 96			Product	Informátion Heat J75904	Tag 235660 23666 23666 23666)	Pcs 15 15 15 10	LBS 9,805 9,805 9,805 6,536 35,951		
Conform To	ML1248 ASTM-A36312750		Chemical	Composition		C.E.: 0.1	935	D.I.: 0		
0.0466 Cu	0.80 Al	0.022 V	0.013	0.0031	0.02		VI D4	Mo 0:01		
0.07	0.016	0.001	0.001	0.013	0.014	-				
				0.013	0,014	1				
	D - H (T)	TENSILE	Physic - H (T)	ol Tests		1	YIELD - M	T)		
55 TENSI	.7 KSI LE - M (T)	63.2 K ELONGATIO	Physic - H (T) - SI N - M (T)		н (n)		YIELD - M (56.7 KSI	m		
55 TENSI 62	.7 KSI	63.2 K	Physic - H (T) - SI N - M (T)	ELONGATION	н (n)			n.		
55 TENSI 62 Product of Coli	.7 KSI LE - M (T) .6 K\$I	63.2 K ELONGATIO	Physic - H (T) - SI N - M (T)	ELONGATION	н (n)	1		<u>.</u>		
55 TENSI 62 Product of Coli	.7 KSI LE - M (T) .6 K\$I	63.2 K ELONGATIO	Physic - H (T) - SI N - M (T)	ELONGATION	н (n)			n		
55 TENSI 62 Product of Coli	.7 KSI LE - M (T) .6 K\$I	63.2 K ELONGATIO	Physic - H (T) - SI N - M (T)	ELONGATION	н (n)					
55 TENSI	7 KSI LE - M (T) 6 KSI . Korea	63.2 K ELONGATIO 34.5 S	Physic - H (T) SI N - M (T) %	ELONGATION S4.5	н (n)					
55 TENSI 62 Product of Coli	7 KSI LE - M (T) 6 KSI . Korea	63.2 K ELONGATIO	Physic - H (T) SI N - M (T) %	ELONGATION S4.5	н (n)			n		
55 TENSI 62 Product of Coli	7 KSI LE - M (T) 6 KSI . Korea	63.2 K ELONGATIO 34.5 S	Physic - H (T) SI N - M (T) %	ELONGATION S4.5	н (n)			n		
55 TENSI 62 Product of Coli	7 KSI LE - M (T) 6 KSI . Korea	63.2 K ELONGATIO 34.5 S	Physic - H (T) SI N - M (T) %	ELONGATION S4.5	н (n)			n		
55 TENSI 62 Product of Coli	7 KSI LE - M (T) 6 KSI . Korea	63.2 K ELONGATIO 34.5 S	Physic - H (T) SI N - M (T) %	ELONGATION S4.5	н (n)			T)		
55 TENSI 62 Product of Coli	7 KSI LE - M (T) 6 KSI . Korea	63.2 K ELONGATIO 34.5 S	Physic - H (T) SI N - M (T) %	ELONGATION S4.5	н (n)					

6/18/2019 09:33 AM () () 1



RECTANGULAR TUBING A500 GR B 12 X 6 X .250 X 20"

PO/PEL HOU-35377/ HEAT: A8U3188

BL HOU-775673-9 6/21/2019 Order HOU-251290-10 Page:1

Southland Tube a Nucor Company 3526 Richard Arrington Jr Blvd N Birmingham, AL 35234 800-543-9024 Fax: 205-261-1553

https://www.nucortubular.com https://www.ntpportal.com Certificate Number: BHM 950476

Sold By: SOUTHLAND TUBE INCORPORATED 3525 Richard Arrington Jr Blvd N Birmingham, AL 35234 Tel: 800-543-9024 Fax: 205-251-1553 Sold To: 2039 - TRIPLE "S" STEEL SUPPLY P.O. BOX 21119

Purchase Order No: HOU-183284 Sales Order No: BHM 494279 - 4 Bill of Lading No: BHM 3197 - 3 Invoice No:

Shipped: 1/4/2019

Ship To: 8 - IRVINGTON WAREHOUSE 8411 IRVINGTON HOUSTON, TX 77022

CERTIFICATE of ANALYSIS and TESTS

Customer Part No:

HOUSTON, TX 77226

TUBING A500 GRADE B(C) 12" X 8" X 1/4" X 40"

Certificate No: BHM 950476

Test Date: 1/3/2019

Total Pieces Total Weight

Bundle Tag	Mill	Heat	P	_		27,040
415341 719919	6N	A8U3188	Specs YLD=65284/TEN=80606/ELG=29.5/RWB=84.4	Y/T Ratio 0.8099	Pieces	Weight
731578	78N	10 10030	YLD=56200/TEN=75300/ELG=31/RWB=83.37 YLD=61000/TEN=76800/ELG=32.5/RWB=84.89		6 6	7.015 7.015
				0.7943	6	7.015

Mill #: 78N Heat #: 1815097 Carbon Eq: 0.3766 Heat Src Origin: MELTED AND MANUFACTURED IN THE USA

	Mn	Р	S	Si	Ai	1						
	0.2200 0.8400	0.0050	0.0010	0.0300	0.0000	000	Cr	Mo	V	Ni	Sn	N T
	0.2200 0.8400 Ti Ca			0.0300	0.0280	0.0900	0.0300	0.0100	0.0030	0.0300	0.0050	0.0000
							The second				0,0000	0.0030
п	0.0010 0.0020											

LEED Information (based on the most recent LEED information from the producing mill)

Method	Location		ond usi)	
EAF		Recycled Content	Post Consumer	
	Berkeley, SC	40.0%		Post Industrial
		40.076	29.8%	10 2%

Mill #: 78 Heat #: 1815098 Carbon Eq: 0.3621 Heat Src Origin; MELTED AND MANUFACTURED IN THE USA

0.0100	P I S I Si T	Al C.	1 0-	·				
0.2100 0.8200 0.0	050 0.0030 0.0300 0	0.0200 0.0300	Cr	Mo	/ V	Ni	Sn	N
7	1 0.0300 0	0.0260 0.0700	0.0300	0.0100	0.0040	0.0300	0.0000	0.0000
1) Ca						0.0500	0.0050	0.0060
0.0010 0.0030								

LEED Information (based on the most recent LEED information from the producing mill)

Method	Location	T D I I I I I I I I I I I I I I I I I I	cing mai)	
EAF	Berkeley, SC	Recycled Content	Post Consumer	Post Industrial
	1=+	40.0%	29.8%	10 000

Mill #: 6N Heat #: A8U3188 Carbon Eq: 0.3995 Heat Src Origin: MELTED AND MANUFACTURED IN THE USA

C	MN	P	S	Si	Cu	7 0-			101 AC 10.	KED III II	HE USA	
0.2200	0.9000	0.0090	0.0060	0.0400	0.1500	0.0000	0.0500	Cr	Мо	Al	N	V
CD	Ti	В	Ca	Co		1 11000	0.0000	0.0600	0.0160	0.0240	0.0060	0.0050
0.0030	0.0020	0.0002	0.0014	0.3995								

LEED Information (based on the most recent LEED information from the producing mill)

Method	Location	The production are production	cing mill)	
EAF	Tuscaloosa, AL	Recycled Content 56.6%	Post Consumer 31.6%	Post Industrial 25.0%

Southland Tube

a Nucor Company

3525 Richard Arrington Jr Blvd N Birmingham, AL 35234 800-543-9024 Fax: 205-251-1553

https://www.nucortubular.com https://www.ntpportal.com Certificate Number: BHM 950476

Certification:

I certify that the above results are a true and correct copy of records prepared and maintained by Southland Tube Incorporated. Swom this day, 1/3/2019.

WE PROUDLY MANUFACTURE ALL OUR PRODUCTS IN THE USA NUCOR TUBULAR PRODUCTS ARE MANUFACTURED, TESTED, AND INSPECTED IN ACCORDANCE WITH ASTM STANDARDS. MATERIAL IDENTIFIED AS A500 GRADE B(C) MEETS BOTH ASTM A500 GRADE B AND A500 GRADE C SPECIFICATIONS.

CURRENT STANDARDS: A252-10 A500/A500M-18 A513/A513M-15 ASTM A53/A53M-12 | ASME SA-53/SA-53M-13 A847/A847M-14 A1085/A1085M-15

Barney Hatten

Supervisor of Technical Services & Quality Standards

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0.004	ala ure co
0.034 MPS 538 536	We certify that these data a se with EN 10204 3.1.
0.11 0.16 V.R.P 7.8867 77759	in the permanent records of company anulactured in the USA. CMTR compil
G/L 200.0 200.0	ing grades: 36: A709-50 fiffed chemical and physical test records as contained. This material, including the billets, was melted and manaway and the billets, was melted and manaway and the billets. The statement of the property of the
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APPENDIX C. SOIL PROPERTIES

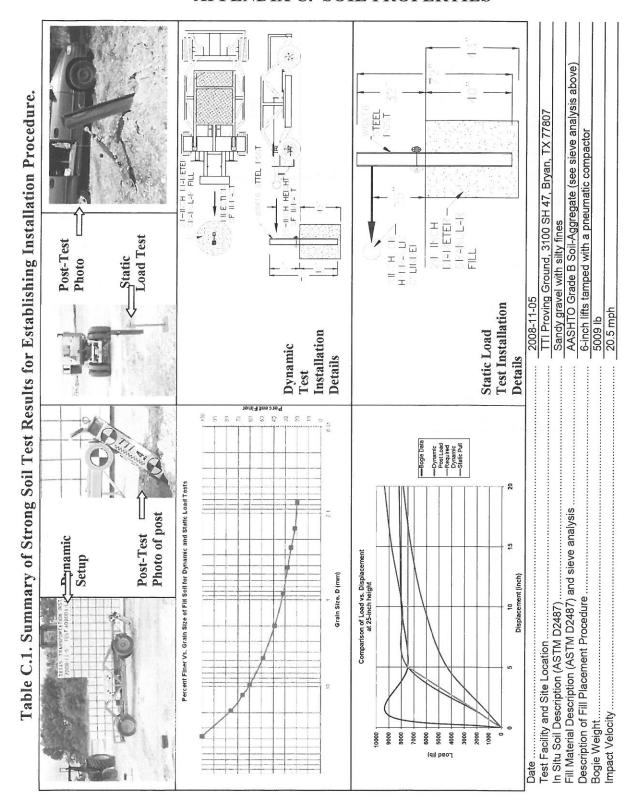
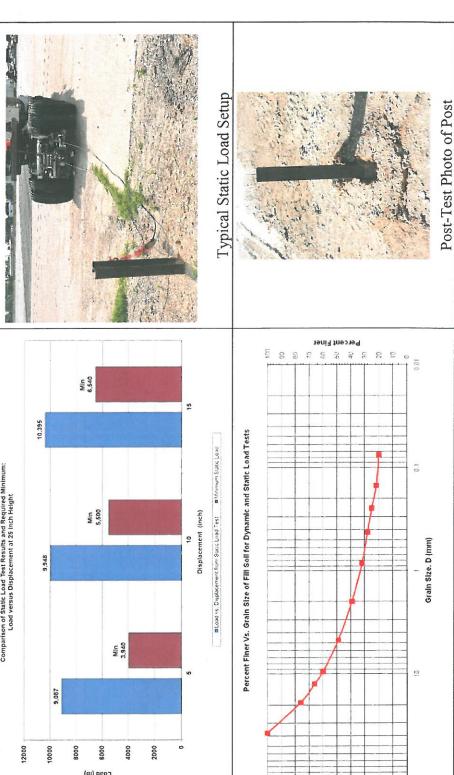
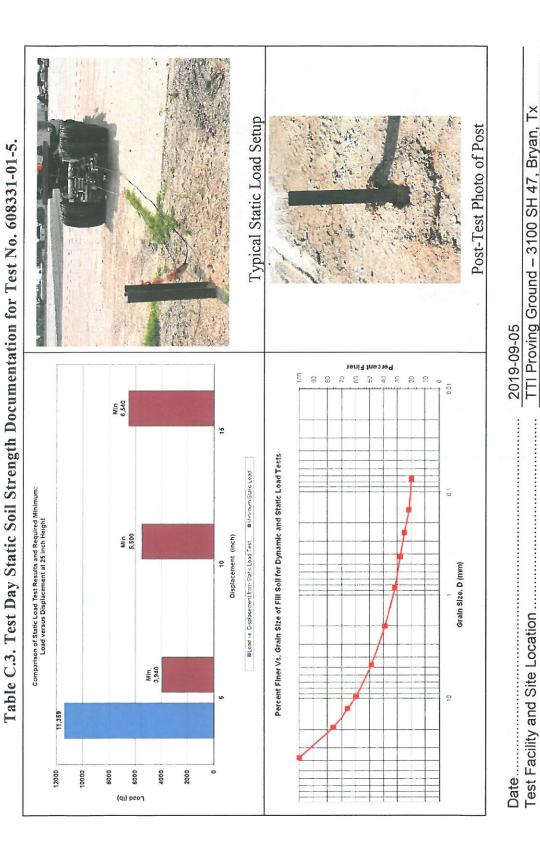


Table C.2. Test Day Static Soil Strength Documentation for Test No. 608331-01-4. Min 6,540 10,395 Comparison of Static Load Test Results and Required Minimum: Load versus Displacement at 25 inch Height Min. 5,500 9,087 12000 (qı) peoq



Date	2019-09-02
Test Facility and Site Location	TTI Proving Ground - 3100 SH 47, Bryan, Tx
In Situ Soil Description (ASTM D2487)	Sandy gravel with silty fines
Fill Material Description (ASTM D2487) and sieve analysis	AASHTO Grade B Soil-Aggregate (see sieve analysis)
Description of Fill Placement Procedure	6-inch lifts tamped with a pneumatic compactor



AASHTO Grade B Soil-Aggregate (see sieve analysis) 6-inch lifts tamped with a pneumatic compactor

Description of Fill Placement Procedure.....

Fill Material Description (ASTM D2487) and sieve analysis

In Situ Soil Description (ASTM D2487)

Sandy gravel with silty fines

Typical Static Load Setup Post-Test Photo of Post Table C.4. Test Day Static Soil Strength Documentation for Test No. 608331-01-6. 5 8 8 5 5 3 3 6 8 5 6,540 Min. 7,504 Percent Finer Vs. Grain Size of Fill Soll for Dynamic and Static Load Tests Bload vs. Displacement from State Lead Test BM evenum State Lead Comparison of Static Load Test Results and Required Minimum Load versus Displacement at 25 inch Height 5,500 Min Displacement (inch) Grain Size. D (mm) 3,940 Min. 9,225 7000 3000 2000 1000 9009 (qı) peoŋ

2019-12-19	TTI Proving Ground - 3100 SH 47, Bryan, Tx	Sandy gravel with silty fines	vsis AASHTO Grade B Soil-Aggregate (see sieve analysis)	6-inch lifts tamped with a pneumatic compactor
Date	Test Facility and Site Location	In Situ Soil Description (ASTM D2487)	Fill Material Description (ASTM D2487) and sieve analysis	Description of Fill Placement Procedure

APPENDIX D. MASH TEST 3-20 (CRASH TEST NO. 608331-01-4)

D1 VEHICLE PROPERTIES AND INFORMATION

Table D.1. Vehicle Properties for Test No. 608331-01-4.

Date:	2019-09-02	_ Test No.:	608331-4	VIN No.: K	KNADE123376251020
Year:	2007	_ Make:	Kia	Model: F	Rio
Tire Infl	ation Pressure: 32	PSI	Odometer: <u>137463</u>	Ti	ire Size: <u>185/65R14</u>
Describ	e any damage to th	e vehicle pric	r to test: None	en a collina — como	
• Deno	tes accelerometer	ocation.			
NOTES	None		- \	0	N T
Engine Engine	CID: 1.6 L				
V	ission Type: Auto or FWD RWD II Equipment:	Manual 4WD	P	3	
None					B
Dummy Type: Mass: Seat P	Data: 50th Perce 165 lb Cosition: IMPACT S		F - F - F - F - F - F - F - F - F - F -	W E X	D K
Geome	try: inches		—	C	
A 66.3	8 F <u>33</u>	.00	K <u>12.25</u>	P 4.12	U <u>14.75</u>
B <u>51.50</u>	<u> </u>		L <u>25.25</u>	Q 22.50	V <u>20.50</u>
C 165.	75 H <u>35</u>	.04	M <u>57.75</u>	R <u>15.50</u>	W <u>35.00</u>
D 34.00	<u> </u>	75	N <u>57.70</u>	S <u>8.25</u>	X <u>72.50</u>
E <u>98.75</u>			O <u>27.00</u>	T 66.20	
	el Center Ht Front ANGE LIMIT: A = 65 ±3 inches	C = 169 ±8 inches, E	Wheel Center Ht I E = 98 ±5 inches; F = 35 ±4 inches; H _inches; (M+Ny2 = 56 ±2 inches; W+	= 39 ±4 inches; O (Bo	W-H 0.00 ottom of Hood Lip) = 24 ±4 inches
GVWR	Ratings:	Mass: Ib	Curb	Test Iner	
Front	1718	Mfront	1602	1578	1663
Back	1874	M_{rear}	868	868	948
Total	3638	M _{Total}	2470	2446	2611
			Allowable TIM = 2420) lb ±55 lb Allowable	GSM = 2585 lb ± 55 lb
Mass D	istribution: LF:	766	RF: <u>812</u>	LR: <u>452</u>	RR: <u>416</u>

Table D.2. Exterior Crush Measurements for Test No. 608331-01-4.

VIN No.: KNADE123376251020

Year:	2007 M	ake:	K	(ia	N	Model:			F	Rio	
	VEH	ASUR		NT SE	IEET ¹						
Complete When Applicable End Damage Side Damage											
	End Damage						Side I	Damage		29-11	
	Undeformed end				Во	wing: l	31	X1		_	
	Corner shi	ft: A1					32				
		A2									
	End shift at frame (Cl	DC)				g const					
	(check one)				X	1+X	2 =				
	< 4 i	nches			in an artist of	2	_ =		_		
	≥ 4 i	nches									
Note: Mea	asure C ₁ to C ₆ from Drive	to Passeng	ger Side in 1	Front or I	Rear Ir	npacts	– Rear	to Fron	nt in Sid	de Imp	acts.
		Direct I									
Specific Impact Number	Plane* of C-Measurements	Width** (CDC)	Max**** Crush	Field L***	C ₁	C ₂	C ₃	C ₄	C ₅	C ₆	±D
1	Front plane at bumper ht	15	8	20	8	6	2	-	-	-	-22
2	Side plane at bumper ht	15	14	48	1	3	5	8	10	15	64
	Measurements recorded		-								

√ inches or

2019-09-02

Date:

Test No.:

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc. Record the value for each C-measurement and maximum crush.

Note: Use as many lines/columns as necessary to describe each damage profile.

¹Table taken from National Accident Sampling System (NASS).

^{*}Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

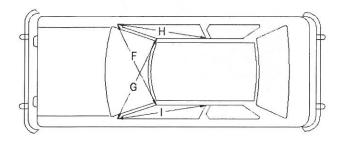
^{**}Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

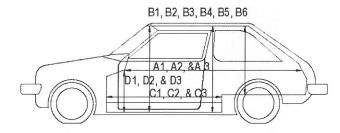
^{***}Measure and document on the vehicle diagram the location of the maximum crush.

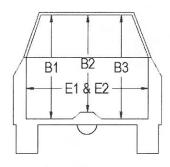
Table D.3. Occupant Compartment Measurements for Test No. 608331-01-4.

 Date:
 2019-09-02
 Test No.:
 608331-4
 VIN No.:
 KNADE123376251020

 Year:
 2007
 Make:
 Kia
 Model:
 Rio







*Lateral area across the cab from driver's side kick panel to passenger's side kick panel.

OCCUPANT COMPARTMENT DEFORMATION MEASUREMENT

	Before	After (inches)	Differ.
A1	67.50	67.50	0.00
A2	67.25	67.25	0.00
A3	67.75	67.75	0.00
B1	40.50	40.50	0.00
B2	39.00	39.00	0.00
В3	40.50	40.50	0.00
B4	36.25	36.25	0.00
B5	36.00	36.00	0.00
B6	36.25	36.25	0.00
C1	26.00	23.00	-3.00
C2	0.00	0.00	0.00
СЗ	26.00	26.00	0.00
D1	9.50	11.50	2.00
D2	0.00	0.00	0.00
D3	9.50	9.50	0.00
E1	51.50	53.00	1.50
E2	51.00	55.50	4.50
F	51.00	51.00	0.00
G	51.00	51.00	0.00
Н	37.50	37.50	0.00
1	37.50	37.50	0.00
J*	51.00	47.50	-3.50

D2 SEQUENTIAL PHOTOGRAPHS

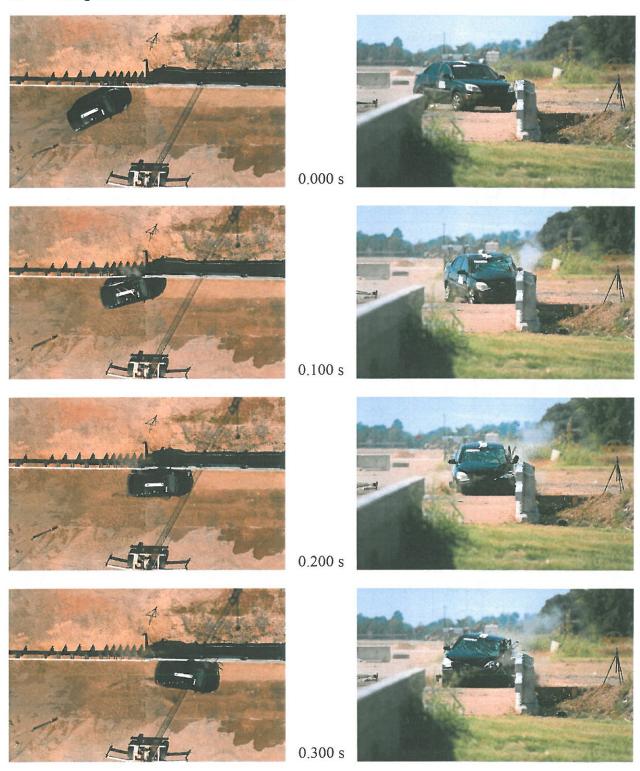


Figure D.1. Sequential Photographs for Test No. 608331-01-4 (Overhead and Frontal Views).

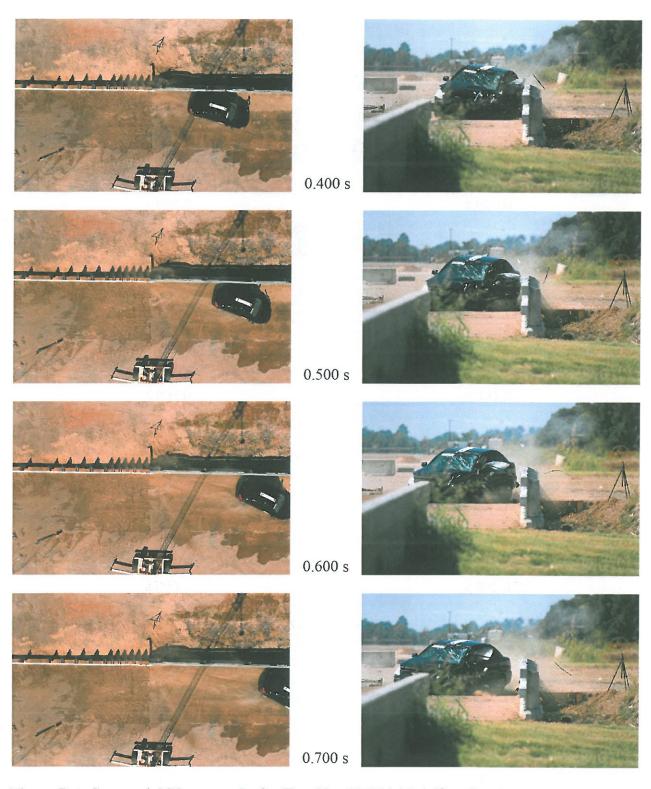


Figure D.1. Sequential Photographs for Test No. 608331-01-4 (Overhead and Frontal Views) (Continued).

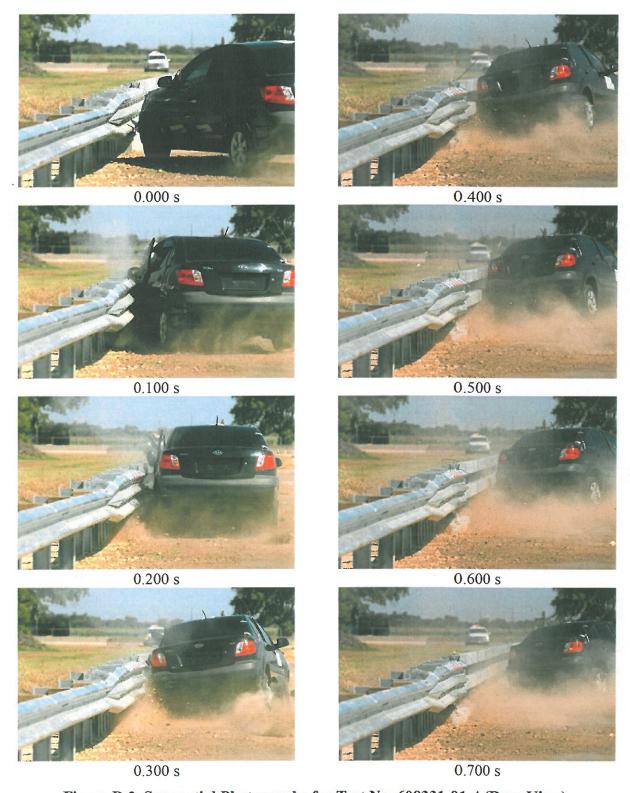


Figure D.2. Sequential Photographs for Test No. 608331-01-4 (Rear View).

Test Number: 608331-01-4
Test Standard Test Number: MASH Test 3-20
Test Article: 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition
Test Vehicle: 2007 Kia Rio
Inertial Mass: 2446 lb
Gross Mass: 2611 lb
Impact Speed: 60.9
Impact Angle: 26.5°

Yaw

Pitch

Roll

Axes are vehicle-fixed. Sequence for determining

orientation:

Yaw. Pitch. Roll.

← 01 m

Figure D.3. Vehicle Angular Displacements for Test No. 608331-01-4.

00

20

40

30

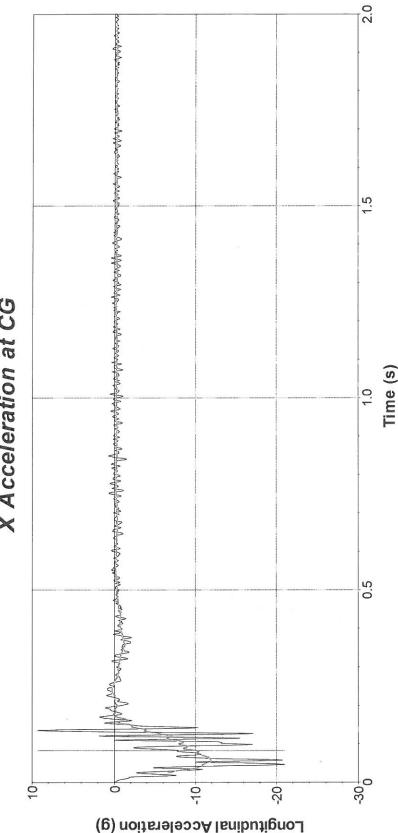
Angles (degrees)

20

9

70

-10

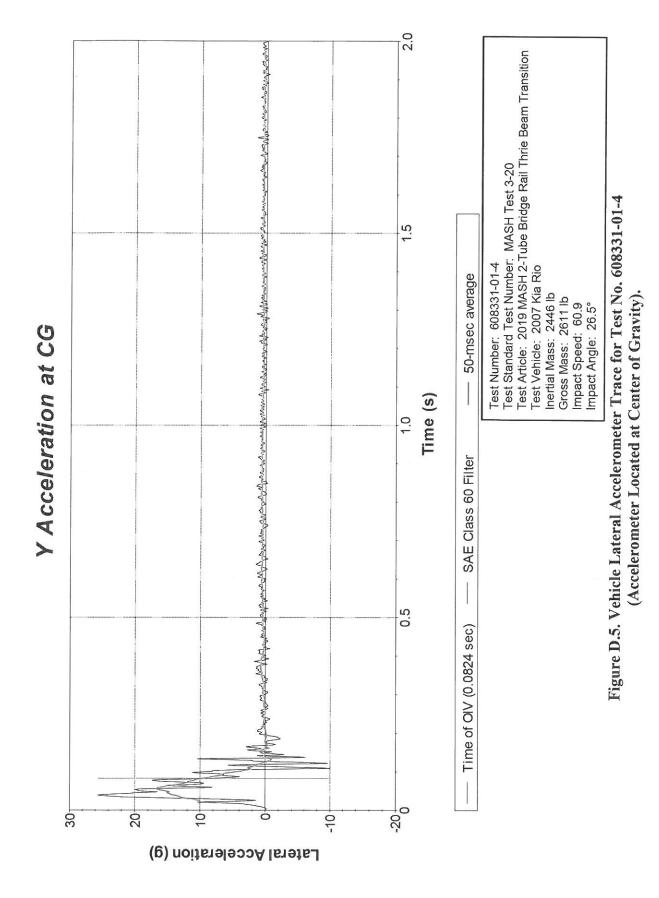


Test Standard Test Number: MASH Test 3-20 Test Article: 2019 MASH 2-Tube Bridge Rail Thrie Beam Transition Test Number: 608331-01-4 Test Vehicle: 2007 Kia Rio Inertial Mass: 2446 lb 50-msec average Gross Mass: 2611 lb Impact Speed: 60.9 Impact Angle: 26.5°

SAE Class 60 Filter

Time of OIV (0.0824 sec)

Figure D.4. Vehicle Longitudinal Accelerometer Trace for Test No. 608331-01-4 (Accelerometer Located at Center of Gravity).



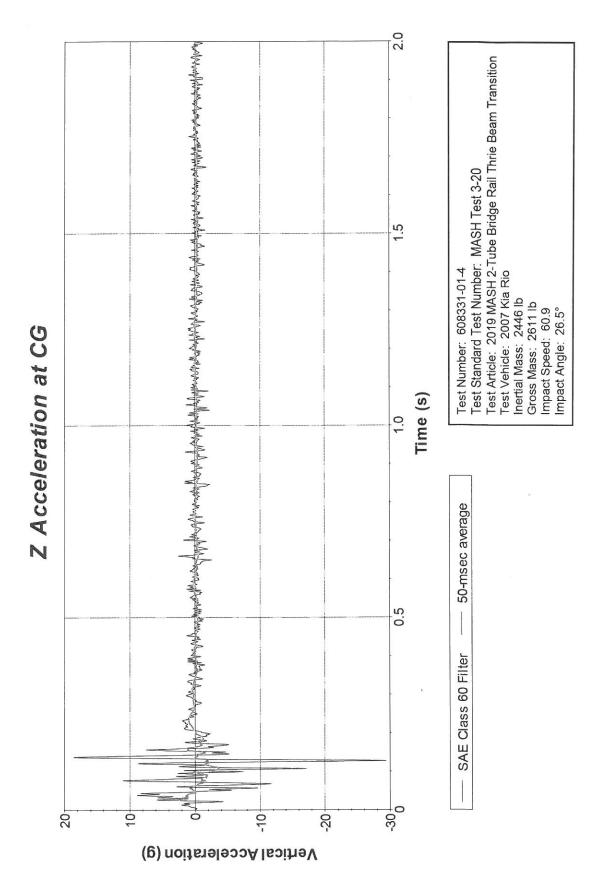


Figure D.6. Vehicle Vertical Accelerometer Trace for Test No. 608331-01-4 (Accelerometer Located at Center of Gravity).

APPENDIX E. MASH TEST 3-21 (CRASH TEST NO. 608331-01-5)

E1 VEHICLE PROPERTIES AND INFORMATION

Table E.1. Vehicle Properties for Test No. 608331-01-5.

Date:	2019-09-	05	Test No.:	608	331-5	VIN No.:	1C6RR6F	HTODS	501020
Year:	2013		Make:	R	AM	Model:		1500	
Tire Siz	e: _265/70	D R 17			Tire I	nflation Pre	ssure:	35	psi
Tread T	ype: Highw	ay				Odo	meter: 15240:	2	50
Note an	y damage to	the vel	nicle prior to te	est: No	ne				
Deno	tes acceleror	neter la	ocation.			X			
NOTES	None			1		7//		<u>)</u> r	1
Engine Engine		liter		A M	CK SEI			ą	N T
	ission Type: Auto or FWD	 RWD	Manual	1	R		—TEST INE	ERTIAL C. M.	1
Optiona None	l Equipment:			1				<u></u>	B
Dummy Type: Mass: Seat P	osition: IMF	16 PACT S		J I	F	U – H – M	V LS E	D -	TK I
Α	78.50	F	40.00	K _	20.00	Р	3.00	U	26.75
в	74.00	G	28.25	L _	30.00	Q _	30.50	٧.	30.25
C	227.50	Η_	60.84	Μ	68.50	R	18.00	W	60.80
D	44.00	1 _	11.75	Ν	68.00	s _	13.00	X	79.00
E	140.50	J _	27.00	0 _	46.00	Τ _	77.00		-000
He	eel Center ight Front	1	4.75 Clea	Wheel We	t)	6.00	Bottom Frame Height - Front		12.50
He	el Center eight Rear		No. Vers San	Wheel We	r)	9.25	Bottom Frame Height - Rear		22.50
	Ratings:	C=237 ±13	Mass: Ib		74		ches; 0=43 ±4 inches; (
Front	3700		M _{front}	<u>Cı</u>	2962	Test I	2863	Gros	ss Static 2948
Back	3900	-	Mrear		2206	XI	2187		2267
Fotal _	6700	_	M _{Total}		5168		5050		5215
Mass Di	istribution:	und			(Allowable R	Range for TIM and	GSM = 5000 lb ±110 lb)		- California - Cal
lb		LF:	1475	RF: _	1388	LR:	1070 R	R:	1117

Table E.2. Measurements of Vehicle Vertical CG for Test No. 608331-01-5.

Date: 2019-09	9-05 Test No .:	60833	1-5	VIN:	1C6RR6H	TODS5010)20
Year:2013	Make:	RAM	1	Model:	1	500	
Body Style: Qu	ad Cab			Mileage:	152402		
Engine: 4.7 liter	- V-8		Tran	smission:	Automatic		
Fuel Level: Em	pty B	allast: 100				(44	l0 lb max)
Tire Pressure: I	Front: <u>35</u>	psi Rea	ır: <u>35</u>	psi S	ize: 265/70 R	17	
Measured Vehi	cle Weights:	(lb)					
LF:_	1475	RF:	1388		Front Axle:	2863	
LR:_	1070	RR:	1117		Rear Axle:	2187	
Left:_	2545	Right:	2505		Total:	5050	
					5000 ±	110 lb allowed	d
	el Base:140.5		Track: F:				inches
1.	48 ±12 inches allowed			Irack = (F+R)/2 = 67 ±1.5 inche	s allowed	
Center of Gravi	ty, SAE J874 St	uspension M	ethod				
X:_	60.85 inches	Rear of F	ront Axle	(63 ±4 inches	allowed)		
Y:_	-0.27 inches	Left -	Right +	of Vehicle	Centerline		
Z:_	28.25 inches	Above Gr	ound	(minumum 28	3.0 inches allowed)		
Hood Heigh	t:46.00	inches	Front	Bumper H	eight:	27.00	inches
Tree a Tree g.	43 ±4 inches allow	200				21.00	
Front Overhang	j:40.00	inches	Rear	Bumper H	eight:	30.00	inches
	39 ±3 inches allow	/ed					
Overall Length	n:227.50	inches					
	237 ±13 inches all	owed					

Table E.3. Exterior Crush Measurements for Test No. 608331-01-5.

Date:	2019-09-05	_ Test No.: _	608331-5	VIN No.: _	1C6RR6HTODS501020
Year:	2013	Make:	RAM	Model:	1500

VEHICLE CRUSH MEASUREMENT SHEET¹

Complete WI	hen Applicable
End Damage	Side Damage
Undeformed end width	Bowing: B1 X1
Corner shift: A1	B2 X2
A2	
End shift at frame (CDC)	Bowing constant
(check one)	X1+X2
< 4 inches	=
≥ 4 inches	

Note: Measure C₁ to C₆ from Driver to Passenger Side in Front or Rear Impacts – Rear to Front in Side Impacts.

C:6-		Direct I	Damage								
Specific Impact Number	Plane* of C-Measurements	Width** (CDC)	Max**** Crush	Field L**	C ₁	C ₂	C ₃	C ₄	C ₅	C ₆	±D
1	Front plane at bumper ht	22	14	28	14	9.5	5	. 3	1	0	-12
2	Side plane at bumper ht	22	15	62	15	11	-	-	8	8	+75
	Measurements recorded										
	inches or mm										
m 11 . 1	C 27. 14 11	. G 1'	2	T A G(G)							

¹Table taken from National Accident Sampling System (NASS).

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc. Record the value for each C-measurement and maximum crush.

Note: Use as many lines/columns as necessary to describe each damage profile.

^{*}Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

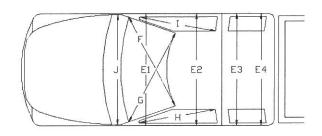
^{**}Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

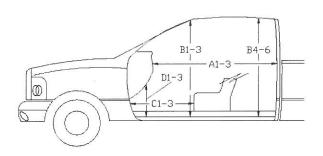
^{***}Measure and document on the vehicle diagram the location of the maximum crush.

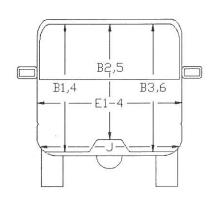
Table E.4. Occupant Compartment Measurements for Test No. 608331-01-5.

 Date:
 2019-09-05
 Test No.:
 608331-5
 VIN No.:
 1C6RR6HTODS501020

 Year:
 2013
 Make:
 RAM
 Model:
 1500







*Lateral area across the cab from driver's side kickpanel to passenger's side kickpanel.

OCCUPANT COMPARTMENT DEFORMATION MEASUREMENT

DLI		WILAGOIN	LIVILLIA I
	Before	After	Differ.
		(inches)	
A1	65.00	65.00	0.00
A2	63.00	63.00	0.00
АЗ	65.50	65.50	0.00
B1	45.00	45.00	0.00
B2	38.00	38.00	0.00
В3	45.00	45.00	0.00
B4	39.50	39.50	0.00
B5	43.00	43.00	0.00
B6	39.50	39.50	0.00
C1	26.00	25.00	-1.00
C2	0.00	0.00	0.00
C3	26.00	26.00	0.00
D1	11.00	10.00	-1.00
D2	0.00	0.00	0.00
D3	11.50	11.50	0.00
E1	58.50	60.50	2.00
E2	63.50	67.50	4.00
E3	63.50	63.50	0.00
E4	63.50	63.50	0.00
F	59.00	59.00	0.00
G	59.00	59.00	0.00
Н	37.50	37.50	0.00
1 .	37.50	37.50	0.00
J*	25.00	21.00	-4.00

E2 SEQUENTIAL PHOTOGRAPHS

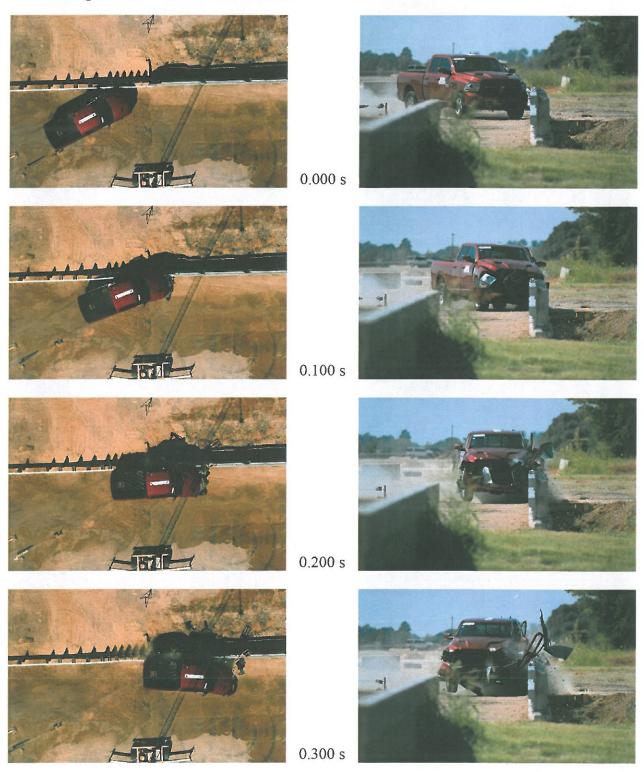


Figure E.1. Sequential Photographs for Test No. 608331-01-5 (Overhead and Frontal Views).

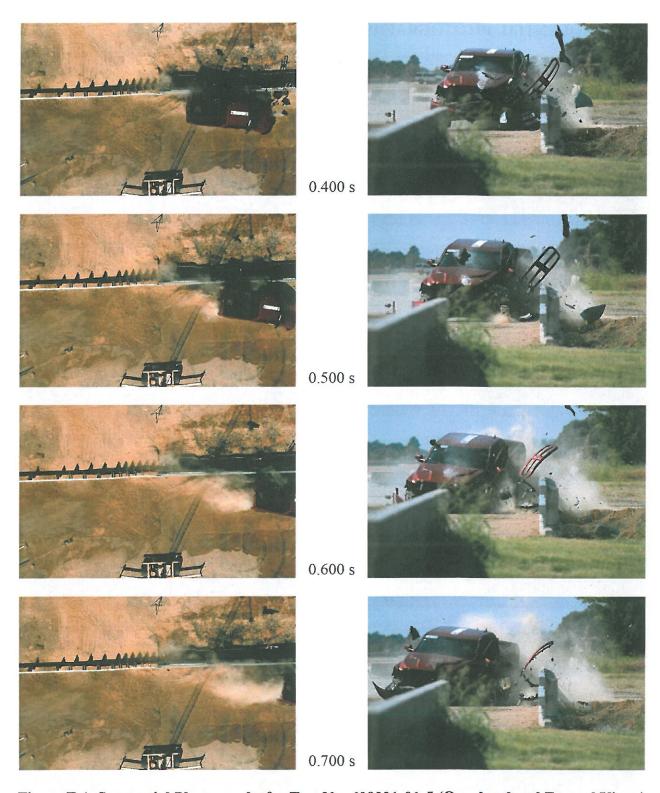


Figure E.1. Sequential Photographs for Test No. 608331-01-5 (Overhead and Frontal Views) (Continued).

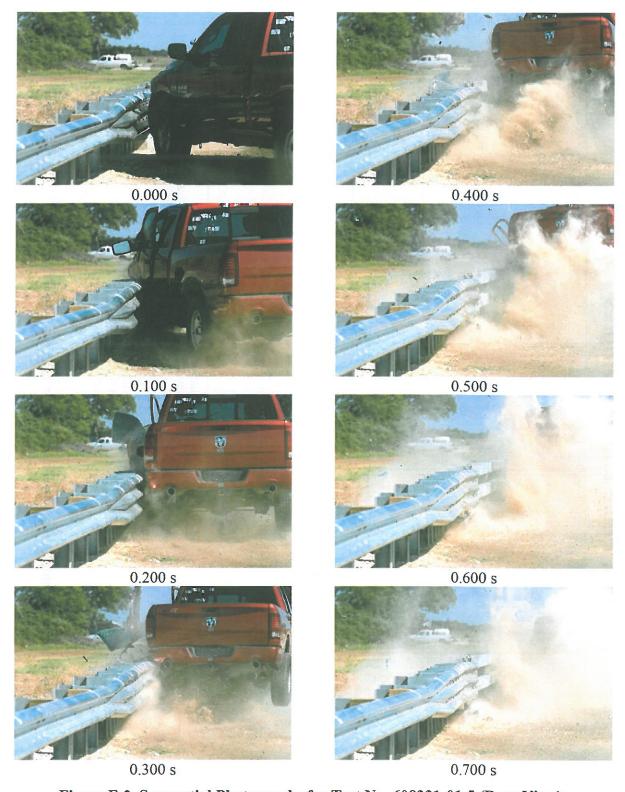


Figure E.2. Sequential Photographs for Test No. 608331-01-5 (Rear View).

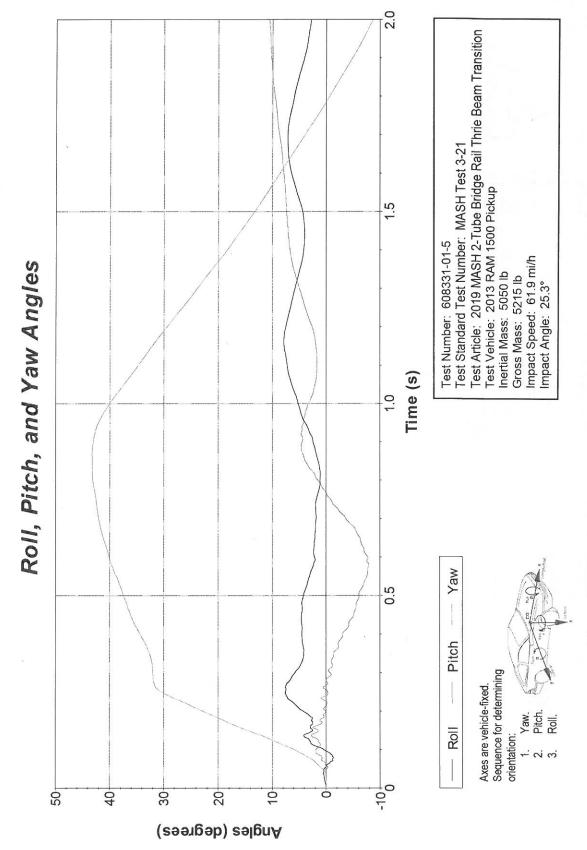


Figure E.3. Vehicle Angular Displacements for Test No. 608331-01-5.

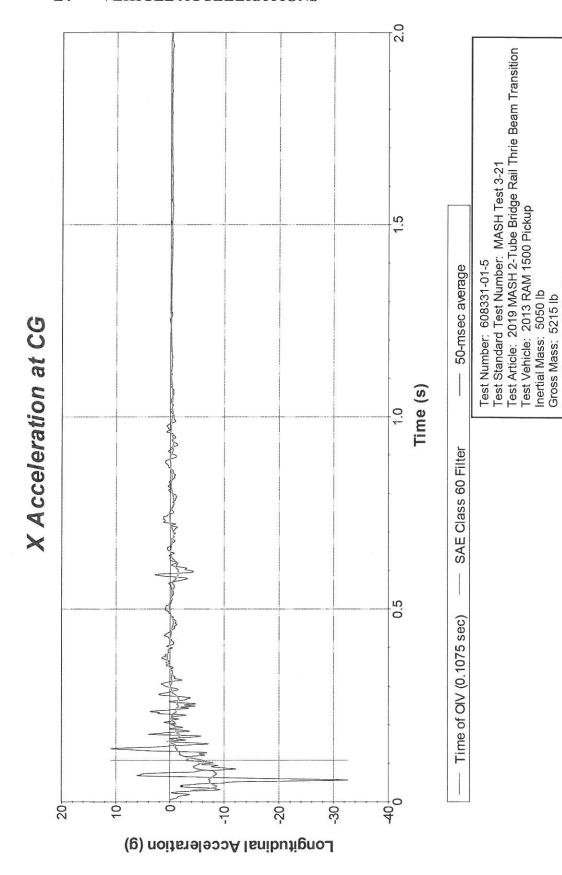
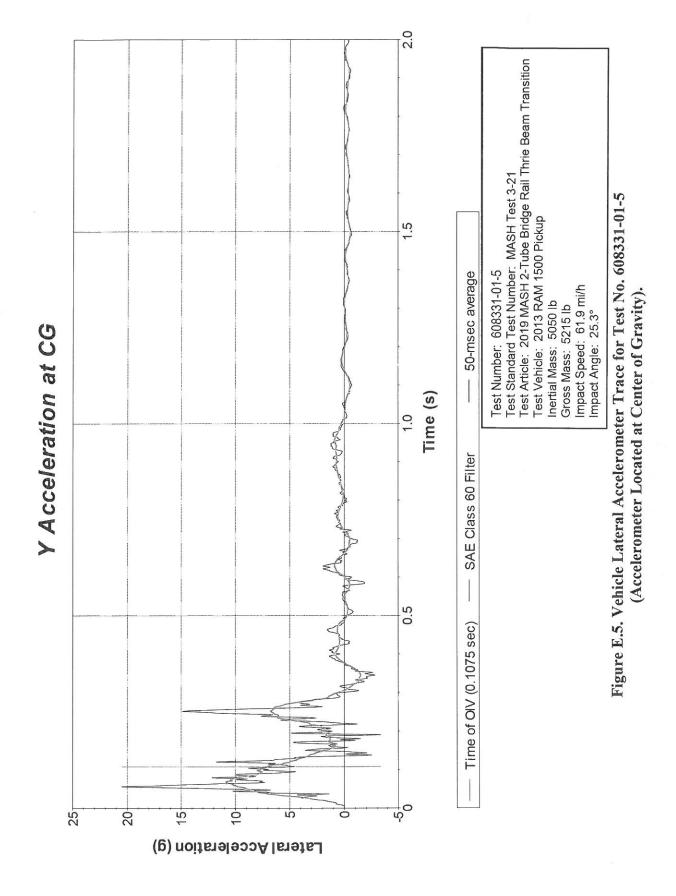


Figure E.4. Vehicle Longitudinal Accelerometer Trace for Test No. 608331-01-5 (Accelerometer Located at Center of Gravity).

Impact Speed: 61.9 mi/h Impact Angle: 25.3°



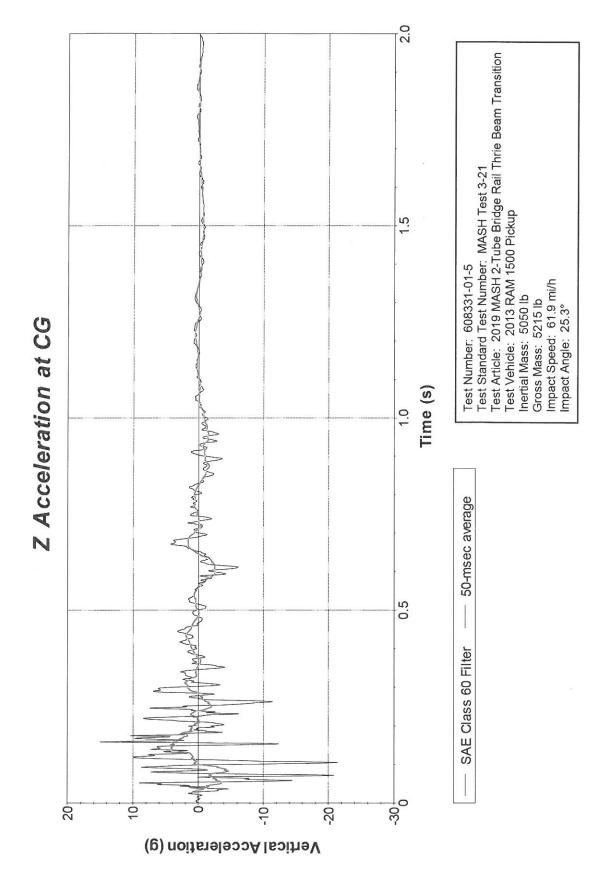


Figure E.6. Vehicle Vertical Accelerometer Trace for Test No. 608331-01-5 (Accelerometer Located at Center of Gravity).

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2020-03-26

APPENDIX F. MASH TEST 3-21 (CRASH TEST NO. 608331-01-6)

F1 VEHICLE PROPERTIES AND INFORMATION

Table F.1. Vehicle Properties for Test No. 608331-01-6.

Date: 2019-12-19	Test No.:	60833	1-6	VIN No.:	1C6RR6F	-T8DS7	24487
Year: 2013	Make:	RAN		_ Model:		1500	
Tire Size: 265/70 R 17			Tire I	nflation Pre	ssure:	35 p	si
Tread Type: Highway				Odo	meter: 14414	5	
Note any damage to the ve	hicle prior to to	est: None					
Denotes accelerometer le	ocation.			X			
NOTES: None		†		77) i	A
NOTES. None		Ţ					
Engine Type: V-8 Engine CID: 4.7 liter		A M -				n	WHEEL TRACK
Transmission Type: Auto or FWD RWD	Manual 4WD	F	R		TEST INE	PRTIAL C M	A
Optional Equipment: None						5) B
Dummy Data: Type: Mass: Seat Position:	y used 0 lb	Ĭ J-Ţ 1-₹	F	U—H—M	G E	D - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 -	FR I
Geometry: inches			-	FRONT	-c	REAR	
A78.50 F _	40.00	Κ	20.00	P _	3.00	U _	26.75
B G _	29.00	L	30.00	Q _	30.50	٧ _	30.25
C <u>227.50</u> H	61.52	Μ	68.50	- R _	18.00	w_{-}	61.50
D 44.00 I	11.75	Ν	68.00	s _	13.00	Х _	79.00
E 140.50 J	27.00	O Wheel Well	46.00	T _	77.00 Bottom Frame	_	40.50
M/heel Center		arance (Front) . Wheel Well		6.00	Height - Front Bottom Frame		12.50
Height Rear RANGE LIMIT: A=78 ±2 inches; C=237 ±1		arance (Rear) _	oc: C = > 29 in	9.25	Height - Rear		22.50
GVWR Ratings:	Mass: Ib	Curb			nertial		Static
Front 3700	M _{front}		877	1031	2832	0108	2832
Back 3900	Mrear		013	***************************************	2206		2206
Total 6700	M _{Total}		390		5038		5038
Mass Distribution:	1393	RF: 1	(Allowable l		GSM = 5000 lb ±110 lb)	'R: ´	1049

Table F.2. Measurements of Vehicle Vertical CG for Test No. 608331-01-6.

Date: 2019-12-	<u> 19 </u>	60833	1-6	VIN:	1C6RR6F	T8DS7244	87
Year:2013	Make: _	RAN	1	Model:	1	1500	
Body Style: Qua	d Cab			Mileage:	144145		
Engine: 4.7 liter	V-8		Tran	smission:	Automatic		
Fuel Level: Emp	oty Bal	last: _180				(44	10 lb max)
Tire Pressure: F	ront: <u>35</u> ps	i Rea	r: <u>35</u>	psi S	Size: 265/70 R	17	
Measured Vehic	ele Weights: (l	b)					
LF:	1393	RF:	1439	_	Front Axle	2832	
LR:	1157	RR:	1049		Rear Axle	2206	
Left:	2550	Right:	2488		Total		
	140.50		-	CO EO		:110 lb allowed	
	B ±12 inches allowed	inches			Inches R: 1.5 inche		Inches
Center of Gravit	y, SAE J874 Sus	pension M	ethod				
X:	61.52 inches	Rear of F	ront Axle	(63 ±4 inches	allowed)		
Y:	-0.42 inches	Left -	Right +	of Vehicle	e Centerline		
Z:	29.00 inches	Above Gro	ound	(minumum 28	3.0 inches allowed)		
Hood Height:	46.00	inches	Front	Bumper H	eight:	27.00	inches
	43 ±4 inches allowed						
Front Overhang:	40.00		Rear	Bumper H	eight:	30.00	inches
	39 ±3 inches allowed						
Overall Length:	227.50						
	237 ±13 inches allow	ed					

Table F.3. Exterior Crush Measurements for Test No. 608331-01-6.

608331-6

VIN No.:

Year:	2013 Make:	RAM	Model:	1500
			EMENT SHEET	i .
	Co	mplete When Appl	icable	
	End Damage		Side I	Damage
	Undeformed end width		Bowing: B1	X1
	Corner shift: A1		B2	X2
	A2			
	End shift at frame (CDC)		Bowing constant	*
	(check one)		X1+X2	
	< 4 inches	<i>i</i> .	2	
	≥ 4 inches			

Note: Measure C₁ to C₆ from Driver to Passenger Side in Front or Rear Impacts – Rear to Front in Side Impacts.

a :e		Direct I	Damage								
Specific Impact Number	Plane* of C-Measurements	Width** (CDC)	Max**** Crush	Field L**	C ₁	C ₂	C ₃	C4	C ₅	C ₆	±D
1	Front plane at bmpr ht	18	16	-	16	-	1	-	1	-	155
2	Side plane at bmpr ht	18	20	54	2	4	9	12	18	20	+70
	Measurements recorded										
	inches or mm										
m 11 . 1		1.	<u> </u>	T A C(C)	L						

¹Table taken from National Accident Sampling System (NASS).

2019-12-19

Test No.:

Date:

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc. Record the value for each C-measurement and maximum crush.

Note: Use as many lines/columns as necessary to describe each damage profile.

1C6RR6FT8DS724487

^{*}Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

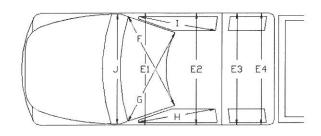
^{**}Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

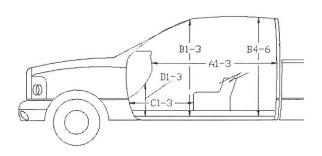
^{***}Measure and document on the vehicle diagram the location of the maximum crush.

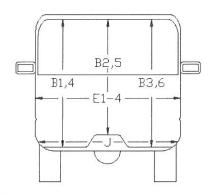
Table F.4. Occupant Compartment Measurements for Test No. 608331-01-6.

 Date:
 2019-12-19
 Test No.:
 608331-6
 VIN No.:
 1C6RR6FT8DS724487

 Year:
 2013
 Make:
 RAM
 Model:
 1500







*Lateral area across the cab from driver's side kickpanel to passenger's side kickpanel.

OCCUPANT COMPARTMENT DEFORMATION MEASUREMENT

Before	After (inches)	Differ.
65.00	65.00	0.00
63.00	63.00	0.00
65.50	65.50	0.00
45.00	45.00	0.00
38.00	38.00	0.00
45.00	45.00	0.00
39.50	39.50	0.00
43.00	43.00	0.00
39.50	39.50	0.00
26.00	26.00	0.00
0.00	0.00	0.00
26.00	26.00	0.00
11.00	11.00	0.00
0.00	0.00	0.00
11.50	11.50	0.00
58.50	58.50	0.00
63.50	63.50	0.00
63.50	63.50	0.00
63.50	63.50	0.00
59.00	59.00	0.00
59.00	59.00	0.00
37.50	37.50	0.00
37.50	37.50	0.00
25.00	25.00	0.00
	65.00 63.00 65.50 45.00 38.00 45.00 39.50 43.00 39.50 26.00 0.00 11.00 0.00 11.50 58.50 63.50 63.50 63.50 59.00 59.00 37.50	(inches) 65.00 65.00 65.00 65.00 65.50 65.50 45.00 45.00 38.00 45.00 39.50 43.00 39.50 26.00 26.00 0.00 26.00 11.00 11.00 0.00 11.50 11.50 58.50 63.50 63.50 63.50 63.50 63.50 59.00 59.00 37.50 37.50 37.50

F2 SEQUENTIAL PHOTOGRAPHS

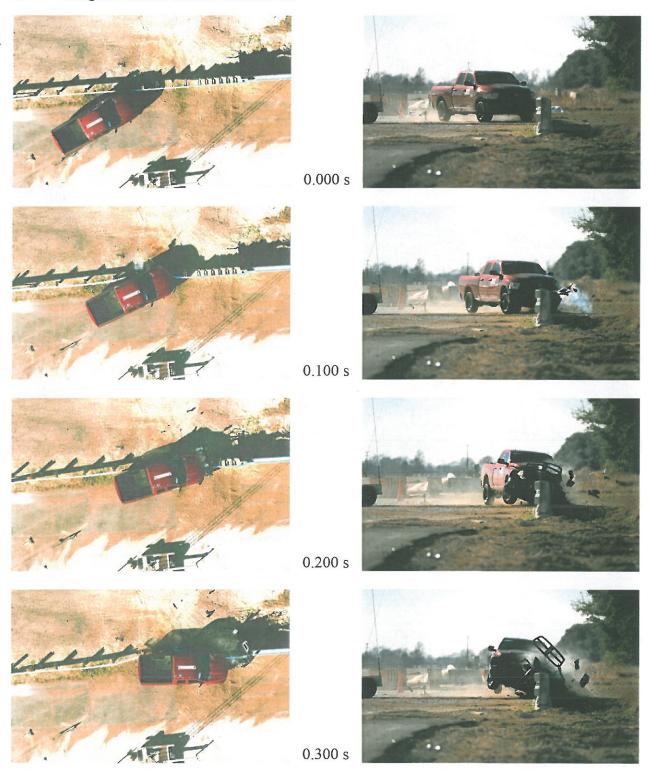


Figure F.1. Sequential Photographs for Test No. 608331-01-6 (Overhead and Frontal Views).

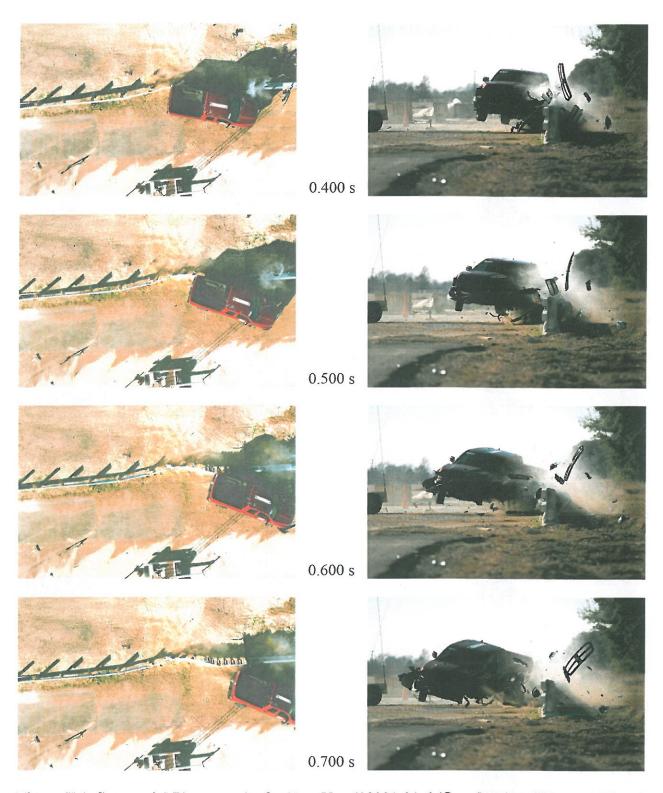


Figure F.1. Sequential Photographs for Test No. 608331-01-6 (Overhead and Frontal Views) (Continued).



Figure F.2. Sequential Photographs for Test No. 608331-01-6 (Rear View).

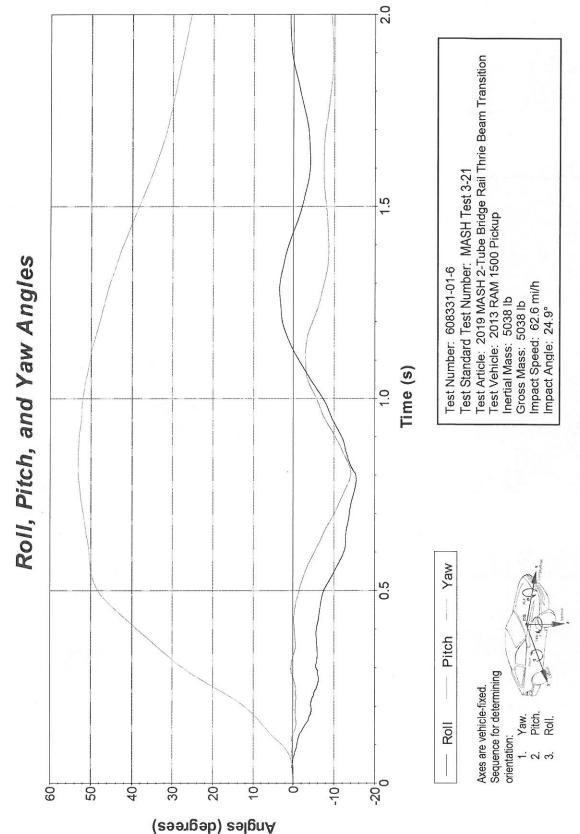
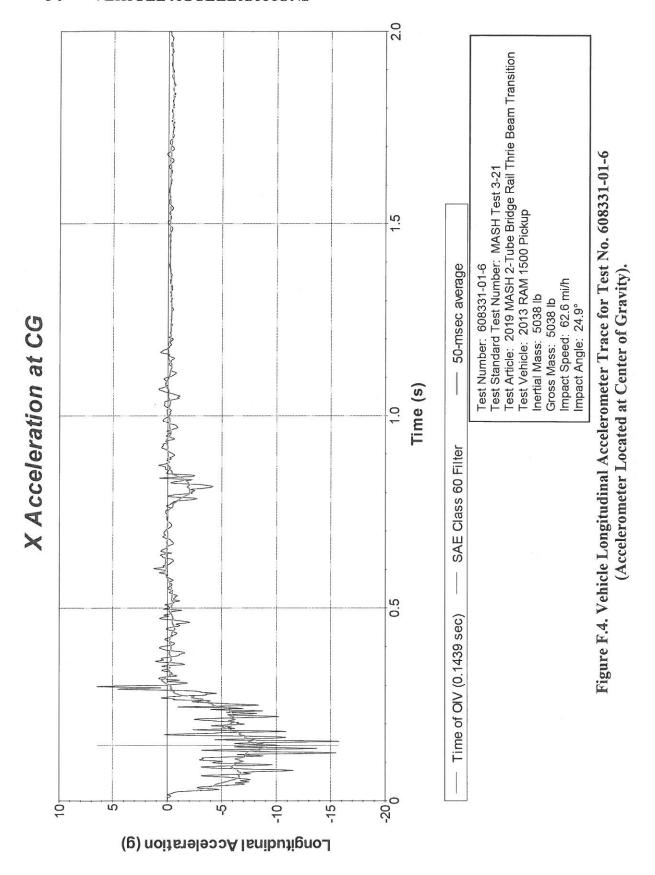
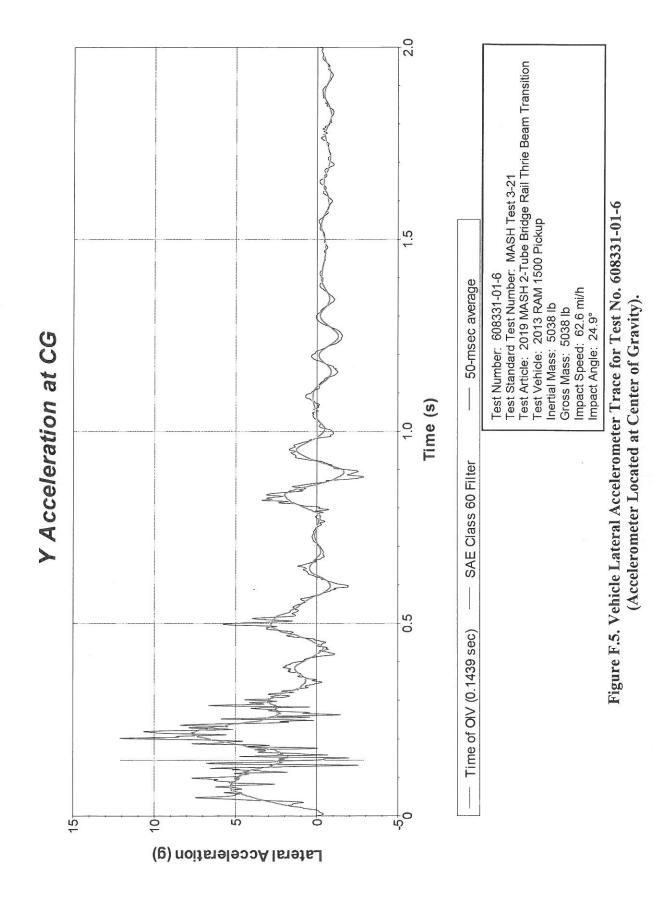


Figure F.3. Vehicle Angular Displacements for Test No. 608331-01-6.





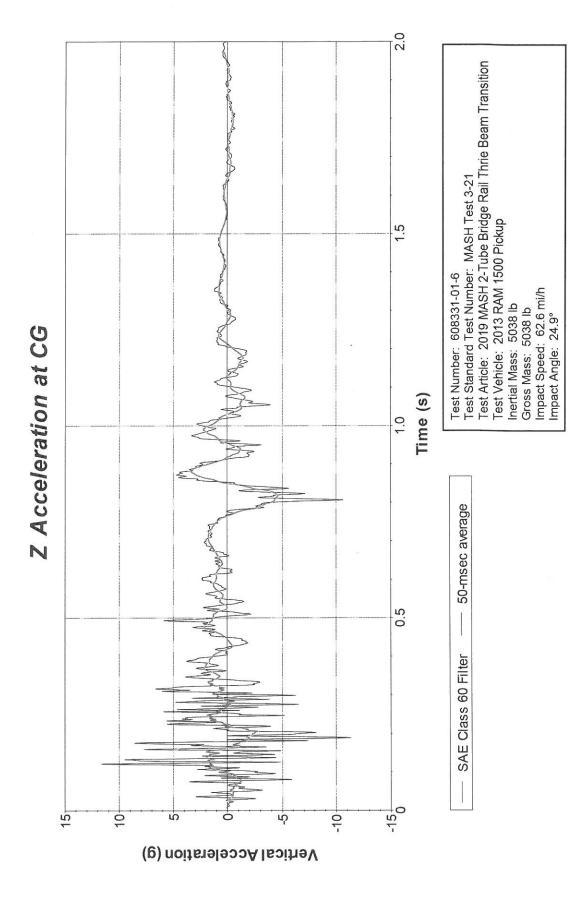


Figure F.6. Vehicle Vertical Accelerometer Trace for Test No. 608331-01-6 (Accelerometer Located at Center of Gravity).

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		2. 2.	
		a.	
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