NOISE REPORT

ODOT Solar Highway Project: West Linn Site Clackamas County

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NOISE REPORT Solar Highway Project Clackamas County

1.0 Summary

This report analyzes the potential changes in noise levels resulting from the proposed Solar Highway Project in West Linn, Oregon. The project will place solar arrays and inverters on the north side of I-205 to generate approximately 3,000,000 kilowatt-hours of renewable energy to power the Oregon transportation system. The project will place between 13,000 and 17,000 panels and ten 260 kilowatt (kW) inverters at the site. Solar inverters will be clustered at 3 separate locations with 3 to 4 inverters at each location for a total of 10 inverters.

Changes to the noise environment which is dominated by the traffic noise from I-205, due to either the noise emitted from the solar inverters or as a result of on-site tree removal are analyzed in this report as part of the National Environmental Policy Act (NEPA) process. The conservative analysis determined that during the day the solar inverters will increase noise levels at residential receivers (receiver) by 2 dBA or less and that this change will not be perceptible to human ears¹. However, in spring and summer, during the 1st hour and last two hours of daylight when traffic noise is reduced, solar inverters may increase noise levels at the closest residences by 3 dBA or less. This change is just perceptible to human ears. At night, the inverters will not emit any sound. The effects of tree removal on the project site will not cause clearly noticeable changes in noise levels (5 dBA). The trees slated for removal are not currently dense or tall enough to provide shielding for the residences located along the northern edge of the right-of-way (ROW) from I-205 traffic noise.

Once the project is in place, additional noise monitoring will be conducted to determine if mitigation needs to be considered.

2.0 Background

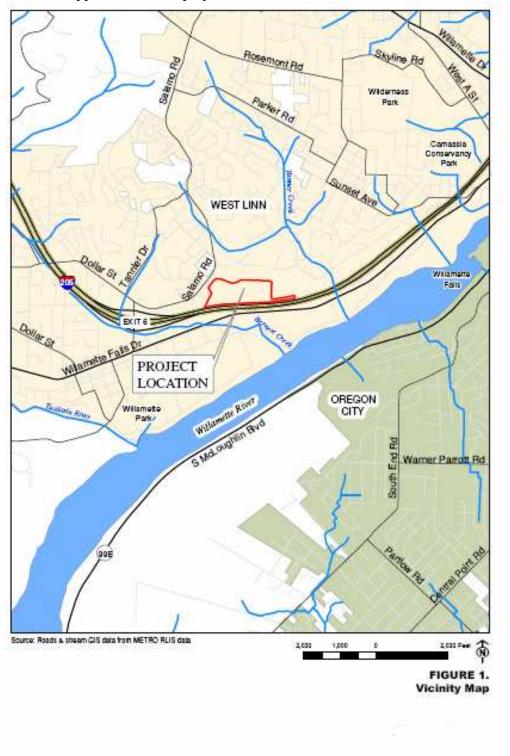
2.1 Project Site and Surroundings

The Solar Highway project will be located within ODOT right-of-way (ROW), on the north side of I-205, in the south portion of the City of West Linn. The site contains 3 geological benches, carved into the bedrock to stabilize the slope and protect the highway. The benches increase in elevation from I-205, as you go north, with the 3rd bench, located at the northern edge of the ROW, being the highest. The first and second benches will be used for placement of the solar inverters and arrays. The areas adjacent to the project include single-family residences to the north and industrial and commercial properties to the south of I-205. Figure 1 shows the Vicinity Map.

¹ The findings of this report are specific to the inverter locations and inverter groupings examined in this report.

2.2 Applicable Regulations

Noise impacts from highway transportation projects are regulated by 23 CFR 772, however, for this project there are no changes to the number of lanes or the vertical or horizontal roadway alignment or traffic volumes, distributions, or speeds; therefore, 23 CFR 772 is not applicable to this project.



The Oregon Revised Statues (ORS Chapter 467) Noise Control and Oregon Administrative Rules (OAR Division 35) Noise Control Regulations were reviewed for applicability. Although the site is unzoned highway ROW and currently not classified as industrial use, the project could be considered a new industrial/commercial noise source and thus subject to state noise regulations (OAR 340-035-0035). The total noise level contributed from this new source is summarized in the results tables and compared to the applicable noise standard (Table 9).

The National Environmental Policy Act (NEPA) requires that the environmental impacts from federally funded projects be evaluated and therefore the change in noise levels for the project with solar inverters will be evaluated. Because the site is unzoned highway right-of-way, the City of West Linn's noise zoning codes are not applicable. The City staff requested that the Noise Report for the West Linn Solar Highway Project include a discussion of potential changes to the noise levels resulting from tree removal. The City also requested that ODOT provide a comparison of ambient noise levels to new noise levels with inverter noise contribution to determine if there would be an increase in noise levels.

2.3 Background on Noise

Sound is composed of pressure waves within the atmosphere. The human ear can detect some of these atmospheric disturbances. A logarithmic scale, the decibel system, has been selected to describe the range of hearing from the weakest pressure wave that can be heard by a person with good hearing in very quiet surroundings to the strongest. The measurement unit is the decibel (dB). The equation for this descriptor is:

decibel = $10 \log \left(\frac{\text{Pressure}}{0.00002 \text{ Newton per square meter}}\right)^2$

Using this scale, the weakest sound which can be heard (0.00002 N/m^2) is 0 dB. The pressure creating pain (about 200 N/m²) is about 140 dB.

The "A-scale" is a frequency weighting system which closely represents the average human hearing response. It has become the most widely accepted frequency system today. A sound level adjusted with this system is called decibels "A-weighted" or dBA. Table 1 shows how the change in dBA is perceived by the human ear.

Sound levels decrease as the distance from the sound source increases. The reduction rate varies with the type of source. Theoretically, a point source, like a solar inverter, has a rate described as a 6 dBA reduction per doubling of distance. A line source, such as the highway, has a 3 dBA reduction per doubling of distance. Acoustic barriers such as topography, like the large flat areas divided by steep slopes at this project site, vegetation, buildings, or walls can also reduce noise.²

² http://www.fhwa.dot.gov/environment/noise/design/index.htm

Sound levels within the environment, like traffic, often change randomly. To describe varying sound, a measurement system which averages the sound pressure levels over time is used. The Leq measurement system is the energy-averaged³ decibel level and has been found to correlate well with human's perceptions of noise and its effects. Another noise statistical descriptor is L_{10} which represents the noise level that is exceeded 10% of the time in the noisiest hour of the day. Leq for typical traffic noise conditions is usually about 3 dBA less than L_{10} for the same traffic conditions.⁴

The addition of a point source to an existing noise environment would have a larger change in noise level for quiet (lower) noise hours compared to higher or peak noise hour. This occurs because peak noise hour will shield some of the effect of the additional noise source.

Table 1. Perceived Change in Noise Levels					
Change in Sound Level	Perceived Change to the Human Ear				
+/- 1 dBA	Not Perceptible				
+/- 3 dBA	Threshold of Perception				
+/- 5 dBA	Clearly Noticeable				
+/- 10 dBA	Twice (or Half) as Loud				
+/- 20 dBA	Fourfold (4x) change				

Figure 2 shows a comparison between noise levels and familiar activities.

Figure 2. Noise Levels of Common Outdoor and Indoor Actitives

³ usually hourly averages for highway noise measurements

⁴ http://www.fhwa.dot.gov/environment/probresp.htm

Common Outdoor Activities	Noise Level (dBA)	Common Indoor Activities
Jet Fly-over at 300m (1000 ft)		Rock Band
Gas Lawn Mower at 1 m (3 ft)	(100)	
Diesel Truck at 15 m (50 ft), at 80 km (50 mph) Noisy Urban Area, Daytime	90 80	Food Blender at 1 m (3 ft) Garbage Disposal at 1 m (3 ft)
Gas Lawn Mower, 30 m (100 ft) Commercial Area	70	Vacuum Cleaner at 3 m (10 ft) Normal Speech at 1 m (3 ft)
Heavy Traffic at 90 m (300 ft) Quiet Urban Daytime	60 50	Large Business Office Dishwasher Next Room
Quiet Urban Nighttime Quiet Suburban Nighttime	40	Theater, Large Conference Room (Background)
Quiet Rural Nighttime	30 20	Library Bedroom at Night, Concert Hall (Background) Broadcast/Recording Studio
Lowest Threshold of Human	10	Lowest Threshold of Human
Hearing	0	Hearing

3.0 Methodology

To analyze the change in noise levels resulting from the addition of the noise from the solar inverters, three residences (receivers, RM6, RM8 and R11) closest to each of the 3 inverter pads (I10, IM5 and IM7) were selected. The measured noise levels at the residential locations were then compared to the calculated noise levels with inverter noise contribution. The noise measurements were conducted at an off peak noise hour to represent the average noise level. Inverter noise levels, at 50 feet from the source, were supplied by the manufacturer. The inverter noise level contributed from each inverter pad was calculated based on the number of inverters and the distance between the inverters and the receivers. The combined noise level at the receivers was the logarithmic sum of the measured noise level and the inverter noise contribution from each group of inverters. Figure 3 shows measured and calculated noise levels at the project site.

Additionally, the analysis calculated the daytime noise levels with inverter noise contribution at the peak traffic noise hour and at quiet (lowest) traffic noise hour. Traffic volume counts near the project site were used to approximate the changes in traffic levels from quiet, average and peak noise hours. Figure 4 shows the daylight changes in noise

levels for quiet, average and peak noise hour at the three closest residences to the inverter pads.

Noise levels associated with the new source were compared to applicable standards.

The measured noise data was analyzed to identify site specific noise shielding characteristics based on the topography. The shielding effect of vegetation on noise is qualitatively discussed.

4.0 Noise Levels

4.1 Solar Inverter Noise

Solar inverters convert electricity generated by the solar modules into alternating current. When a 260 kW solar inverter is in operational mode, it emits a buzz which at a distance of 50 feet, sounds as loud as a large business office. Figure 2 gives additional examples of common activities and their associated noise levels. PV Powered (manufacturer of the solar inverters) measured 59 dBA as the noise level for a 260kW inverter at 50 feet.⁵ Solar inverter structures measure approximately 8 feet by 8.5 feet by 2 feet.

The change in the noise level at a receiver will depend on the noise contribution from each inverter that can be heard at each receiver. The noise contribution from each inverter depends on the number of inverters that are grouped together at each inverter pad and the distance between each inverter pad and the receiver. Inverters will be installed in groups of 3 to 4 at each location for a total of 10 inverters. There are 3 possible scenarios that inverters may be arranged. The worst case scenario will be presented in this report and Figure 3; the other scenarios are summarized in Appendix A.

4.1.1 Summing Noise Levels of Multiple Inverters

The following noise calculations assume a measured noise level of 59 dBA at 50 feet for one 260 kW inverter. When adding sound levels together the logarithmic rule given in equation 1 is used.

A dBA+ B dBA+ C dBA+ D dBA= $10*\log 10^{(A/10)} + 10^{(B/10)} + 10^{(C/10)} + 10^{(D/10)})$ equation (1)⁶

Where:

A, B, C and D = different noise sources

This equation shows how 4 different sound levels are added together. Table 2 summarizes the expected noise level at 50 feet from grouped inverters. Three inverters will be located at IM5 and I10. Four inverters will be located at IM7.

⁵ Personal communication to Lynn Averbeck of ODOT from Tucker Ruberti of PVPowered, October 14, 2009.

⁶ http://www.fhwa.dot.gov/environment/noise/design/3.htm

Table 2. Addition of Inverter Noise at 50 feet						
Number of Inverters Combined Noise Level (dBA)						
1	59					
2	$10*\log 10^{(10^{(59/10)})} + 10^{(59/10)}) = 62$					
3	$10*\log 10^{(10^{(59/10)} + 10^{(59/10)} + 10^{(59/10)})} = 64$					
4	$10*\log 10^{(59/10)} + 10^{(59/10)} + 10^{(59/10)} + 10^{(59/10)} + 10^{(59/10)}) = 65$					

4.1.2 Decrease of Noise Level with Increase in Distance

As the distance between the source (inverter pads) and receiver increases, the sound wave dissipates and the noise level at the receiver decreases. Equation 2 calculates the noise level (L_r) at a given distance, if the noise level at a specific distance (50 feet) is known. The equation assumes L_{50} as the noise level at 50 feet which could be either 64 dBA (group of 3 inverters) or 65 dBA (group of 4 inverters).

Table 3 shows the distance (d_r) between each inverter pad and each receiver that was used to calculate the noise contribution (L_r) from the inverter location at each receiver when 4 inverters are placed at IM7 and 3 inverters are placed at I10 and IM5. Tables for noise contributions of other scenarios are presented in Appendix A, Tables A-1 and A-2. All three scenarios predicted identical changes in noise levels. Table 3 also gives the noise contribution from each inverter pad at the receiver.

 $L_r = L_{50} + 20 * log 10 (d_{50}/d_r) dBA$

equation $(2)^2$

Where:

 L_r = sound level at receiver at given distance (dr) dBA L_{50} = sound level at distance 50 feet dBA d_{50} = distance of 50 feet d_r = distance between inverter pad and nearest receiver (feet)

Table 3. Inverter Noise Levels at Various Distances with Four Inverters at IM7							
Location of Source (number of inverters)	Noise Level at 50 Feet	Receiver Location	Distance from Source to Receiver	Noise Level from Inverters at Receiver			
	dBA		(feet)	Leq/dBA			
I10 (3)	64		800	40			
IM5 (3)	64	RM6	360	47			
IM7 (4)	65		2040	33			
l10 (3)	64		1280	36			
IM5 (3)	64	RM8	1800	33			
IM7 (4)	65		216	52			
l10 (3)	64		224	51			
IM5 (3)	64	R11	544	43			
IM7 (4)	65		1336	36			

Note: Locations of inverter pads can be see on Figure 3.

4.2 Measured Noise Levels

Noise levels were measured with a Bruel & Kjaer sound level meters model Type 2221 at various locations at the project site on September 24, 2009. Monitoring locations included the proposed locations for the inverter pads, residences at the western and northern border of the project site, and other selected locations within the project area for collection of project noise data. Other project noise data collected included sound levels measurements for I-205 (M1); the midway elevation of the project site (M2); a location in the solar array (M4); and an additional residential location (RM9). Noise measurements were taken in pairs to ensure the same source of traffic noise and to document any topographical shielding at the site. These measurements were conducted on September 24th, 2009 between 10:00 am and 2:00 pm in an off-peak traffic noise hour to represent the average traffic noise levels. One measurement was also conducted on July 16th between 11:15 am to 11:30 am at M12. Figure 3 shows measured noise levels in dBA.

The noise level taken at M12 was used to represent noise levels at R11 because they both have similar vertical and horizontal distance from I-205 which is the major source of noise. FWHA guidance for noise measurements was followed for these measurements and the noise monitoring sheets are provided in Appendix A. Noise monitoring photographs are included in Appendix B. Table 4 summarizes the measured noise data.

Measurement Location	Description	Noise Level (Leq/dBA)	Time of Measurement	
M1	At I-205 gate to ROW	75	1:08-1:23 pm	
M2	East Side, first bench	60	1:08-1:23 pm	
M4	Center site, first bench	60	12:24-12:39 pm	
IM5	West side, first bench	53	10:33-10:48 am	
RM6	Green Street & Salamo Rd, SE corner	64	10:33-10:48 am	
IM7	East Side 2, first bench	50	11:41-11:56 am	
RM8	East side, second bench	56	11:41-11:56 am	
RM9	Center, second bench	52	12:24-12:39 pm	
M12*	Empty lot at corner of Salamo Rd & Barrington Drive	58	11:15- 11:30 am	

*Measurements for M12 were conducted on July 16, 2009

All noise measurements taken at the project site varied between 50 and 60 dBA except M1 and M6. Noise levels at sites M1 (75 dBA) and M6 (64 dBA) were the loudest and were adjacent to I-205 and Salamo Road, respectively.

4.3 Calculated Existing Noise Levels Before Inverter Installation

4.3.1 Calculated Peak Hour Noise Levels

Peak hour noise levels were calculated by comparing traffic volumes between 10 a.m. and 2 p.m. to peak traffic volumes based on traffic counts of I-205 taken near the project site in June 2009⁷. The data show that traffic volumes between 10 a.m and 2 p.m. are approximately 75% of peak p.m. volumes. Peak noise hour traffic volumes would have to double the hourly traffic volumes observed during noise measurements in order to produce a 3 dBA increase in noise levels. To calculate peak noise hour sound levels conservatively, 3 dBA was added to the measured noise levels.

4.3.2 Calculated Quiet Hour Noise Levels

Daylight, quiet noise hour levels were calculated by comparing traffic volumes between 10 a. m. to 2 p.m. to traffic volumes during the quiet daylight hours. Traffic counts on I-205 near the project site taken in June, 2009 show that traffic volumes between 5 a.m. and 6 a.m., 7 p.m. and 8 p.m. and between 8 p.m. and 9 p.m. were 48%, 67% and 56% of traffic volumes taken between 10 a.m. to 2 p.m., respectively. These hours represent daylight hours in summer when I-205 noise levels would be lowest. Based on the June 2009 traffic volumes, quiet noise hour levels are best approximated by subtracting 3 dBA from noise level measurements which represents a halving of traffic volumes.

⁷ The traffic data were supplied by Gretchen Harvey, ODOT Traffic System Monitoring Unit

4.4 Calculated Noise Levels with Inverters

4.4.1 Calculated Noise Levels for Average Noise Hour with Inverter Noise

To estimate the average noise hour, the noise levels at residential receivers when the inverters are operating were calculated by logarithmically summing (Equation 1) the noise level measured at the receivers and the contribution from each of the three grouped inverter pads given in Table 3. The measured noise levels, each inverter pad noise contribution, the total of all inverters noise and the resulting calculated noise level at the receiver for the scenario with 4 solar inverters at IM7 (worst case) are summarized in Table 5. Figure 3 shows the calculated noise levels at 3 residences (RM6, RM8 and R11) with inverter noise. The calculated noise levels are in blue. Noise levels increase by 0 - 2 dBA when inverters are operating. Results for the other two scenarios are presented in Appendix A, Tables A-3 and A-4.

Levels and Calculated Inverter Noise Levels at Residential Receivers (Leq/dBA) New Inverter Noise Total Inverter Contribution Average Traffic Ho Contribution Existing Noise from: Contribution									
Level	l10	IM5	IM7	Contribution	Noise Level*	Noise Level			
64 (RM6)	40	47	33	48	64	0			
56 (RM8)	36	33	52	52	58	2			
58 (R11) 51 43 36 52 59 1									
*Added logarithmically with equation 2									
Assumes four inverters at location IM7; 3 inverters at I10; and 3 inverters at IM5.									

4.4.2 Calculated Noise Levels for Peak Hour Noise Levels

To estimate sound levels for the peak noise hour, noise levels for the peak noise hour were calculated by adding 3 dBA to measured noise levels (See Table 6 column 1). The peak traffic hour noise levels with the inverter noise contribution are shown in Table 6. Using this conservative method, change in noise levels from measured to calculated at peak noise hour increase by 0-1 dBA which are similar or less than the changes in noise levels shown in Table 5 (last column).

Table 6. Estimated Noise Levels at Peak Traffic Noise Hour: Measured Noise Levels and Calculated Inverter Noise Levels at Residential Receivers (Leq/dBA)								
New Inverter Noise New Contribution from Combined Noise Peak Traffic Hour								
Existing Noise Level								
64 + 3 = 67 (RM6)	40	47	33	67	0			
56 + 3 = 59 (RM8)	36	33	52	60	1			
58 + 3 =61 (R11)	58 + 3 =61 (R11) 51 43 36 62 1							
*Added logarithmically with equation 2 Assumes four inverters at location IM7; 3 inverters at I10; and 3 inverters at IM5.								

4.4.3 Calculated Noise Levels for Quiet Noise Hour with Inverter Noise

Noise levels for the quiet traffic noise hour during daylight were calculated by subtracting 3 dBA from measured noise levels (See Table 7 column 1) which represents traffic volumes being half the volume of average traffic hour. The quiet hour noise levels with the inverter noise contribution are shown in Table 7. Using this method, change in noise levels from measured to calculated during quiet noise hour increase by 0-3 dBA which is slightly more than increase for average daylight noise hour and which is just perceivable to human ears. These calculations are conservatively assuming that all 10 inverters would operate during those daylight quiet noise hours.

Table 7. Estimated Noise Levels at Quiet Traffic Noise Hour: Measured Noise Levels and Calculated Inverter Noise Levels at Residential Receivers (Leq/dBA)								
New Inverter Noise Contribution from New Combined Change in Noise								
Existing Noise Level								
64 - 3 = 61 (RM6)	40	47	33	61	0			
56 - 3 = 53 (RM8)	36	33	52	56	3			
58 - 3 =55 (R11)	51	43	36	57	2			
*Added logarithmically with equation 2 Assumes four inverters at location IM7; 3 inverters at I10; and 3 inverters at IM5.								

4.5 Discussion of Calculated Noise Levels for Specific Hours, Specific Seasons

Since solar inverters only operate in daylight hours, the change in noise level varies from season to season based on the number of daylight hours and quiet, average and peak traffic noise hour. Generally, noise levels could increase by up to 3 dBA⁸ during the first and last two hours of sunlight during in May, June and July and during the last hour of sunlight in March, April and August. On a worst case summer day, a 3 dBA increase in noise level would occur for a maximum of 13% of time. All other daylight hours will experience a change of 2 dBA or less which is not perceptible to human ears. Table 8 compares the change in noise levels by season and time of day.

⁸ Assumes that traffic volumes are half of volumes during peak traffic hour.

	Table 0. Seas	onal Changes in Noise Level	Relative to noul of Day	
Season	Change in Noise Level (dBA)	Traffic Noise Period	Number of Hours That Experience Change	% of Day by Season
Winter	0	Night time	13	54%
(December,	1	peak noise hour am and pm	5	21%
January and February)	2	all other daylight hours	6	25%
	0	Night time	10	42%
Spring (March	1	peak noise hour am and pm	5	21%
April)	2	average daylight noise hour	8	33%
	3	quiet daylight noise hour	1 hour (7pm to 8pm)	4%
a (11	0	Night time	8	33%
Summer (May, June and July &	1	peak noise hour am and pm	5	21%
August)	2	average daylight noise hour	8	33%
, tagaot)	3	quiet daylight noise hour	3 (5 to 6am & 7 pm to 9 pm)	13%
Fall (September,	0	Night time	12	50%
October and	1	peak noise hour am and pm	5	21%
November)	2	all other daylight hours	7	29%

Table 8. Seasonal Changes in Noise Level Relative to Hour of Day

Notes: For all seasons, peak am daylight traffic noise hour is assumed to be 7 am to 9 am and peak pm daylight traffic noise hour to be 3pm to 6pm; for nighttime hours, the solar inverters are not operating

Spatially, the increase in noise level depends on the distance of receivers from inverter pads. Figure 4 compares the calculated change in noise at the three closest residential receivers for various daylight hours. Houses in the vicinity of RM8 will experience an increase of 3 dBA in noise levels during quiet daylight noise hours. At RM8 for non-quiet hours and for all hours of other locations, residences will experience changes of 2 dBA or less which are not perceptible to human ears.

Comparison of Calculated Noise Levels to New Source Standards

Table 9 shows, the ambient statistical noise level for L_{10} of all inverters operating at the same time compared to the DEQ New Industrial and Commercial Noise Source Standards. The highest noise level by location in the 5th column of Table 5, A3 and A4 were converted from Leq to L_{10} by adding 3 dBA. Noise levels during 7 a. m. to 10 p.m. will be within the noise standard. During daylight hours between 5 a.m. to 7 a.m. when all inverters are operating, L_{10} noise levels could be as high as 56 dBA which is slightly higher than the L_{10} standard of 55 dBA. This approach is conservative; the analysis assumes no muffling of inverter noise. Noise monitoring will be conducted at the project site after the project is completed to determine if noise levels are at acceptable levels. If necessary, noise mitigation will be examined at the project site.

Table 9. Comparison of New Source Contribution Noise Levels to Industrial New SourceStandard							
			Day Standard	Below	Night Standard	Below	
			7 a.m. to 10	Standard?	10 p.m. to 7	Standard?	
			p.m.	(dBA	a.m.	(dBA	
Location	Leq/dBA	L10/dBA	L10/dBA	Difference)	L10/dBA	Difference)	
D MO							
RM6	49	52	60	yes (-8)	55	yes (-3)	
RM6 RM8	49 52	52 55	60 60	yes (-8) yes (-5)	55 55	yes (-3) no (0)	

5.0 Additional Site Characteristics

5.1 Topography

The project site has 3 distinct geological benches that block the line of sight between receiver at the edge of highway ROW and the dominant noise source (I-205). When topography blocks the line of sight between a source and a receiver, it shields some of the source noise from the receiver. Table 10 arranges the noise measurement data in order of increasing distance from I-205. At IM5 and IM7 the noise levels are lower than expected at the indicated distances from I-205, likely because of the shielding effect of the complex terrain between source and receiver.

Table 10. Change in Noise Levels with Increasing Horizontal Distance from I-205						
ID	Distance from Roadway (feet)	Noise Level (dBA)				
M1	88	75				
M2	400	60				
M4	400	60				
IM5	448	53				
IM7	520	50				
RM8	736	56				
RM9	904	52				
Note: Bold values are lower noise levels RM6 was not included in the table as Salamo Road was major noise source.						

5.2 Noise Level Shielding from Trees

A common misconception is that vegetation has sound reducing qualities. The project site contains a number of trees on the first and second benches. The majority of trees that will be removed for the project are located on the second bench. Most of the residences along the northern edge of the project site are 50 to 150 feet higher in elevation than the vegetation being removed; therefore only sparsely spaced treetops are currently visible at these residences. Sparsely spaced treetops do not provide any clearly noticeable noise shielding (5 dBA). Additionally, some of the trees that will be removed are deciduous and provide no noise shielding in winter time.

In order to provide a clearly noticeable decrease in noise levels (5 dBA), vegetation needs to be at least 100 foot wide with a minimum height of 20 feet above the shielded property. The vegetation has to be dense enough that the noise source cannot be seen. There are many trees in the existing project area; however the trees that will be removed are not densely spaced, nor tall enough, and do not completely shield the line of sight for residences 50 to 150 feet higher in elevation than the I-205 roadway, the biggest source of noise for the project site and the surrounding areas. The trees at the project site do not provide a clearly noticeable reduction in traffic noise levels for nearby residences. Therefore the removal of trees in the project area will not create a clearly noticeable increase in the sound levels at bordering residences. The trees on the 3rd bench and at the edges of ODOT ROW will be left in place.

6.0 Conclusions

The West Linn Solar Highway Project will increase noise levels for receivers outside of ODOT right-of-way by up to 2 dBA when the solar inverters operate. This change will not be perceptible to the human ear. However, in spring and summer, during the 1st hour and last two hours of daylight, solar inverters may increase noise levels at residences adjacent to RM8 by up to 3 dBA; this change is just perceptible to human ears. Since inverters will not operate after dark, nighttime noise levels will not change. The removal of trees at the project site will not create clearly noticeable increases in I-205 noise levels at the closest residents because the trees being removed are not currently thick or tall enough to provide significant noise shielding. There will be minimal tree removal and there will be replanting of trees in other locations at the site. Additional noise shielding at residences will be provided by the site topography in instances where the line of sight between the roadway and the residences is blocked.

Noise monitoring will be conducted after the project is built to confirm that noise levels are at acceptable levels as calculated in this report. If necessary, noise mitigation will be examined and addressed at the project site.

7.0 References

National Environmental Policy Act (http://ceq.hss.doe.gov/Nepa/regs/nepa/nepaeqia.htm)

Appendix A

Noise Level Calculations for Other Scenarios

Table A1a. Inverter Noise Levels at Various Distances with Four Inverters at I10							
Location of Source (number of inverters)	Noise Level at 50 Feet	Receiver Location	Distance from Source to Receiver	Noise Level from Inverters at Receiver			
	dBA		(feet)	dBA			
l10 (4)	65		800	41			
IM5 (3)	64	RM6	360	47			
IM7 (3)	64		2040	32			
l10 (4)	65		1280	37			
IM5 (3)	64	RM8	1800	33			
IM7 (3)	64		216	51			
l10 (4)	65		224	52			
IM5 (3)	64	R11	544	43			
IM7 (3)	64		1336	36			

Table A1b. New Noise Levels with Inverters at Sensitive Receivers (Leq/dBA)

Existing Noise Level	New Inverter Contribution from			Total Inverter	New Combined Noise Level	Change in Noise Level
	l10	IM5	IM7	Contribution*		
64 (RM6)	41	47	32	48	64	0
56 (RM8)	37	33	51	51	57	1
58 (R11)	52	43	36	53	59	1
*Added logarithmically w	ith equation 2					

Assumes four inverters at location I10; 3 inverters at IM5, 3 inverters at IM7

Table A2a. Inverter Noise Levels at Various Distances with Four Inverters at IM5								
Location of Source (number of inverters)	Noise Level at 50 Feet	Receiver Location	Distance from Source to Receiver	Noise Level from Inverters at Receiver				
	dBA		(feet)	Leq/dBA				
l10 (3)	64		800	40				
IM5 (4)	65	RM6	360	48				
IM7 (3)	64		2040	32				
l10 (3)	64		1280	36				
IM5 (4)	65	RM8	1800	34				
IM7 (3)	64		216	51				
110 (3)	64		224	51				
IM5 (4)	65	R11	544	44				
IM7 (3)	64		1336	35				

Table A2b. New Noise Lev	vel with Inverters at New Inverter Contribution from		rter	Sensitive Receiver (Lee Total Inverter	q/dBA) New Combined Noise Level	Change in Noise Level			
Existing Noise Level	I10	IM5	IM7	Contribution*					
64 (RM6)	40	48	32	49	64	0			
56 (RM8)	36	34	51	51	57	1			
58 (R11)	51	44	35	52	59	1			
*Added logarithmically with equation 2 Four inverters at location IM5, 3 inverters at I10, 3 inverters at IM7									

Appendix B

Noise Monitoring Sheets

OREGON DEPARTMENT OF TRANSPORTATION HIGHWAY DIVISION – GEO-ENVIRONMENTAL SECTION

NOISE MEASUREMENT RECORD (USING AN INTEGRATING SOUND LEVEL METER)

PROJECT NAME: Solar Project HIGHWAY NAME AND NUMBER: 205 COUNTY:	MEASUREMENT NO: <u>M</u> DATE <u>Sept 24, 2009</u> . ENGINEER <u>NL</u> WIND: <u>Smooth</u>
START TIME: 1:08 STOP TIME: 1:23 CALIBRATI	ION TONE 94 dB HZ
LENGTH OF MEASUREMENT: 15	LEQ RANGE: 43-705 MICROPHONE HEIGHT: Sfeet
	SEL:
LEQ @ 5 MIN 74.7 OPTIONAL LEQ@ 25 MIN LEQ@ 45 MIN	LEQ:
LEQ @ 10 MIN 74.8 LEQ@ 30 MIN LEQ@ 50 MIN	SEL - LEQ: =
LEQ @ 15 MIN LEQ@ 35 MIN LEQ@ 55 MIN	
LEQ @ 20 MIN LEQ@ 40 MIN LEQ@ 60 MIN	TIME FROM TABLE:
TRAFFIC: ROADWAY: ROADWAY:	ROADWAY:
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NB	205.

(SHOW DISTANCES TO IMPORTANT FEATURES ie centerline, buildings, driveways etc) SEE BACK OF THIS PAGE FOR ANY ADDITIONAL COMMENTS

OREGON DEPARTMENT OF TRANSPORTATION HIGHWAY DIVISION – GEO./HYDRO SECTION NOISE MEASUREMENT RECORD (USING AN INTEGRATING SOUND LEVEL METER)

	PROJECT NAME: HIGHWAY NAME AN COUNTY:	Solar they west DNUMBER:	LINA	DA' ENO	ASUREMENT N FE GINEER ND:		
	START TIME: 1.08	30 p STOP TIME:	1:23:30	CALIBRAT	ION TONE $\underline{93,8}$	<u>d</u> BB	(Z
	LENGTH OF MEASUR	REMENT: <u>15</u>			E: <u>45-105</u> ONE HEIGHT: _	· · · ·	
	LEQ@ 5 MIN 59.4		LEQ@ 45 MIN			•	
• •	LEQ @ 10 MIN <u>59.7</u> LEQ @ 15 MIN <u>66.0</u> LEQ @ 20 MIN	LEQ@ 35 MIN	LEQ@ 55 MIN			- -	
	TRAFFIC: AUTOS; MED. TRUCKS: HEAVY TRUCKS: SPEED: STREET ADDRESS:	ROADWAY:		HR. EQUIV.	ROADWAY: COUNTED = =	HR. EQUIV.	
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	(SHOW DISTANCE	S TO IMPORTANT FEATURES		NTE +0 1-20 vays etc)	25		
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OREGON DEPARTMENT OF TRANSPORTATION HIGHWAY DIVISION – GEO-ENVIRONMENTAL SECTION

NOISE MEASUREMENT RECORD (USING AN INTEGRATING SOUND LEVEL METER)

COUNTY: START TIME: <u>jl 3</u>	AND NUMBER: 205 4 STOP TIME: 1237	 CALIBRATIO	MEASUREMENT NO: <u>M4</u> DATE <u>1-24-09</u> . ENGINEER <u>NC</u> WIND: <u>Smph</u> ON TONE <u>94</u> dB <u>HZ</u> Before 93.7 atter 93.7 LEQ RANGE: <u>Sel</u> .	
LENGTH OF MEAS	UREMENT: Smin		LEQ RANGE:	
			SEL:	
LEQ@ 5 MIN 59.7	OPTIONAL LEQ@ 25 MIN LEQ@	45 MIN	LEQ: 59.5	
LEQ @ 10 MIN 59-4	LEQ@ 30 MINLEQ@		SEL - LEQ: =	
LEQ @ 15 MIN 59.5	_LEQ@ 35 MINLEQ@	55 MIN		
the A Be	_LEQ@ 40 MINLEQ@	60 MIN	TIME FROM TABLE:	
TRAFFIC: AUTOS: MED. TRUCKS: HEAVY TRUCKS: SPEED:	ROADWAY:			
-	•	26	24	
	DRTANT FEATURES ie centerline, buildin R ANY ADDITIONAL COMMENTS	Cemest Prof. ngs, driveways etc)	T Green. Franker Gravel men bench top O tree M	

OREGON DEPARTMENT OF TRANSPORTATION HIGHWAY DIVISION – GEO./HYDRO SECTION NOISE MEASUREMENT RECORD (USING AN INTEGRATING SOUND LEVEL METER)

PROJECT NAME: HIGHWAY NAME AN COUNTY:Mult	SOLAR HUY L	1958 LINN 15		ENGINEER	
START TIME: <u>(0:33</u>	50 A STOP TIM	E: 10:48:50	<u> </u>	LIBRATION TON	TE <u>H. J</u> dB HZ
LENGTH OF MEASUR	Rement: 15		M	CQ RANGE: <u>45</u> ICROPHONE HEIO	
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OREGON DEPARTMENT OF TRANSPORTATION HIGHWAY DIVISION - GEO-ENVIRONMENTAL SECTION

NOISE MEASUREMENT RECORD (USING AN INTEGRATING SOUND LEVEL METER)

COUNTY: START TIME: <u>f0</u> : LENGTH OF MEAS			CALIBRAT	TION TON LEQ R MICRO	: <u>< 5 мр</u> ! NE <u>94</u> dB ANGE: <u>45 –</u> ОРНОПЕ НЕІС	<u>0</u> HZ 105 dB	9374B
LEQ @ 5 MIN	OPTIONAL _ LEQ@ 25 MIN	LEQ@		LEQ:_			
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OREGON DEPARTMENT OF TRANSPORTATION HIGHWAY DIVISION – GEO-ENVIRONMENTAL SECTION

NOISE MEASUREMENT RECORD (USING AN INTEGRATING SOUND LEVEL METER)

PROJECT NAME: <u>S</u> HIGHWAY NAME AN COUNTY: <u>START TIME: 1644</u> LENGTH OF MEASU	MEASUREMENT NO: M7 DATE 9-24-09 ENGINEER NL WIND: < <u>Smpn</u> TION TONE 94 dB HZ 93.7 before 93.7 ffu LEQ RANGE: <u>45-105</u> MICROPHONE HEIGHT: <u>Sfeet</u> SEL:				
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OREGON DEPARTMENT OF TRANSPORTATION HIGHWAY DIVISION – GEO./HYDRO SECTION NOISE MEASUREMENT RECORD (USING AN INTEGRATING SOUND LEVEL METER)

~		CMM			
	PROJECT NAME: <u>Solar Itwy</u> HIGHWAY NAME AND NUMBER: COUNTY:	MEASUREMENT NO: <u>HA</u> HB DATE 9/24 ENGINEER <u>DEVINE</u> WIND: <u>CELM L5</u> MPH			
	START TIME: 11:42:08 STOP TIME: 57:08	CALIBRATION TONE dB HZ			
	LENGTH OF MEASUREMENT: 15	LEQ RANGE: <u>55,9</u> JBA MICROPHONE HEIGHT: <u>SEL:</u>			
17	OPTIONAL LEQ @ 5 MIN LEQ@ 25 MIN	LEQ:			
	LEQ @ 10 MIN LEQ@ 30 MIN LEQ@ 50 MIN	SEL - LEQ: =			
	LEQ @ 15 MIN LEQ@ 35 MIN LEQ@ 55 MIN LEQ @ 20 MIN LEQ@ 40 MIN LEQ@ 60 MIN				
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OREGON DEPARTMENT OF TRANSPORTATION HIGHWAY DIVISION – GEO./HYDRO SECTION NOISE MEASUREMENT RECORD (USING AN INTEGRATING SOUND LEVEL METER)

	PROJECT NAME: <u>Solar Hwy</u> HIGHWAY NAME AND NUMBER: <u>COUNTY:</u>				MEASUREMENT NO: <u>49</u> DATE <u>92409</u> ENGINEER WIND:			
	START TIME: 12:24	₹.08 STOP TIME:	12:39:0	2B	CALIBRAT	TION TONE	dB	_HZ
	LENGTH OF MEASUREMENT: 15'				LEQ RANGE: MICROPHONE HEIGHT: SEL:			
							а ж	
29	LEQ @ 5.MIN 52.4	OPTIONAL LEQ@ 25 MIN	LEQ@ 45 M	/IN	LEQ: 5	۷.		
34	LEQ @ 10 MIN 51.6	LEQ@ 30 MIN			SEL - LEQ: = _			
	LEQ @ 15 MIN 52.1						3	, *
	LEQ @ 20 MIN	LEQ@ 40 MIN	LEQ@ 60 N	MIN	TIME FROM T	ABLE:	-	
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Appendix B

Noise Monitoring Photographs



Looking south towards I-205 southbound lanes



Looking north towards property



Noise reading of 75 dBA



Looking southeast towards I-205 southbound lanes



Looking northeast towards property



Looking northwest towards paved area within property



Looking west along property edge

Noise Monitoring towards M1

Looking south from noise monitor



Looking north of monitor





Looking south from monitor



Looking north towards monitor



Noise reading of 60 dBA

Noise Monitor M2



Looking south towards monitor



Looking west towards monitor



Looking north towards monitor



Looking east towards the monitor



Looking southeast towards monitor



Looking southwest towards monitor



Noise reading of 59.5 dBA

Noise Monitor M4



Looking east towards monitor



Looking west towards monitor



Noise reading of 53.7 dBA



Looking north towards monitor



Looking south towards monitor

Noise Monitor IM5





Looking west towards monitor



Looking northwest towards monitor



Looking southeast toward monitor



Looking north towards monitor



Noise reading of 64.3 dBA



Looking north from monitor



Looking east towards monitor



Looking northeast from monitor



Looking south from monitor



Looking south from monitor



Noise reading of 50.2 dBA

Noise Monitor IM7



Looking west from monitor



Looking east from monitor



Noise reading of 55.9 dBA



Looking southwest from monitor



Looking north from monitor

Noise Monitor RM8



Looking west towards noise monitor



Looking southeast towards monitor



Noise reading of 52.1 dBA



Looking southwest towards monitor



Looking east towards monitor

Noise Monitor RM9



Looking northwest from monitor



Looking north from monitor



Looking east from monitor



Looking southeast towards monitor

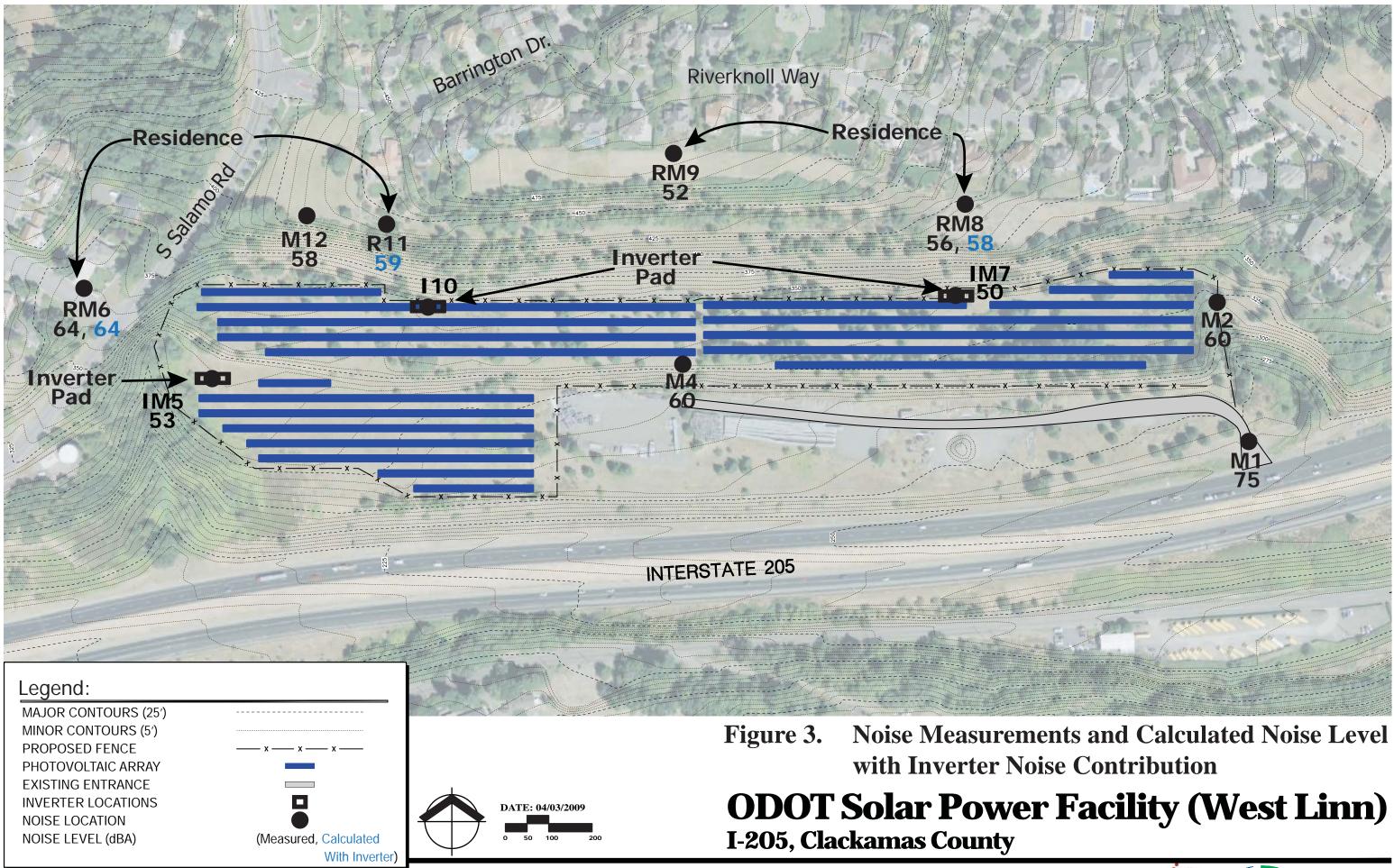


Looking south from monitor

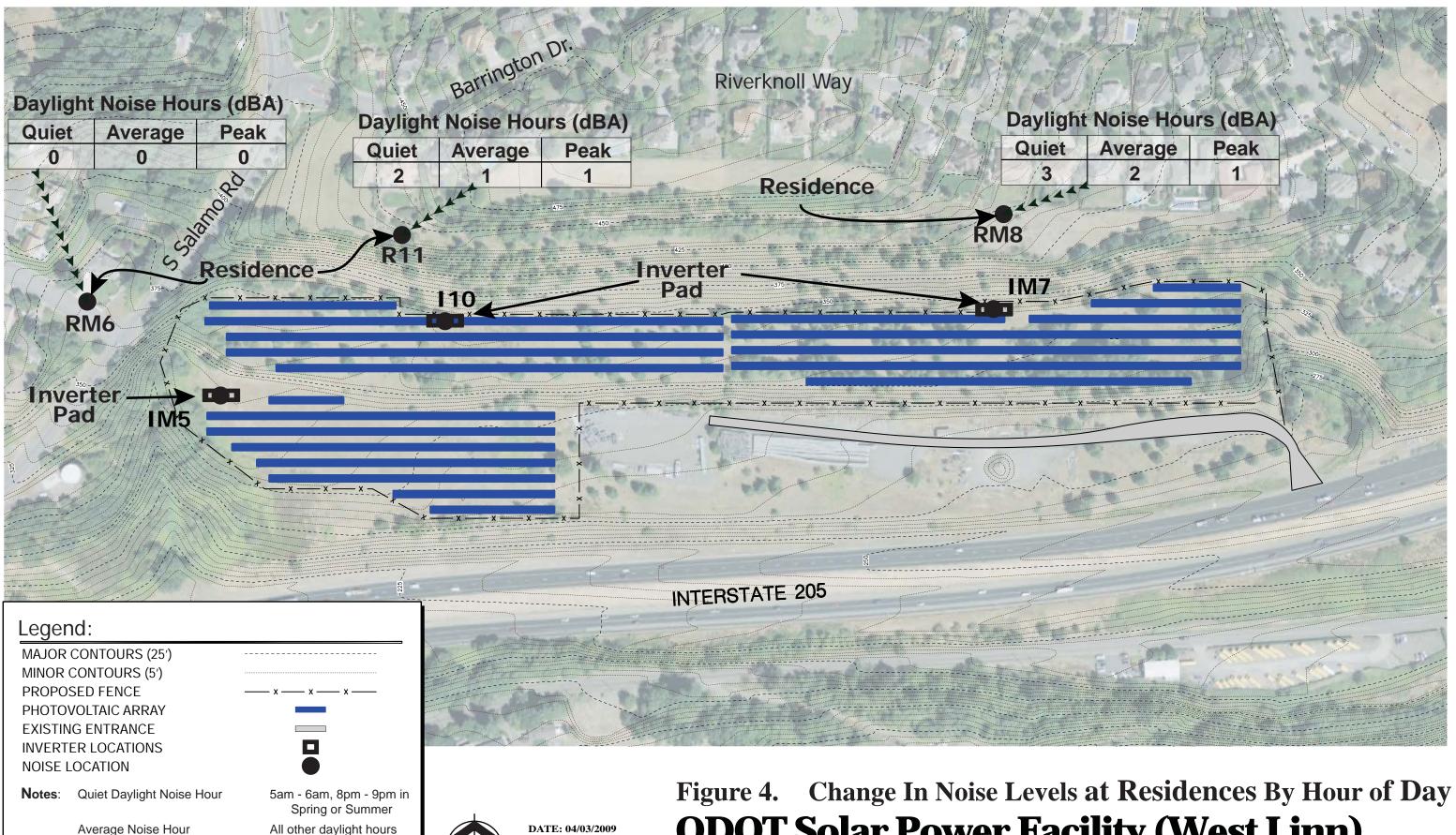


Looking northeast from monitor

Noise Monitor R11

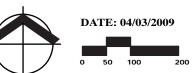






Peak Noise Hours

All other daylight hours 7am -9am and 3pm - 6pm all Seasons



ODOT Solar Power Facility (West Linn) I-205, Clackamas County



