

| | | | | | |
|--|--|--|--|---|--|
| 1. Report No. FHWA-RD-96-201 | | 2. Government Accession No. | | 3. Recipient's Catalog No. | |
| 4. Title and Subtitle NCHRP REPORT 350 COMPLIANCE TEST OF THE NEW JERSEY SAFETY SHAPED BARRIER | | | | 5. Report Date | |
| 7. Author(s) King K. Mak and Wanda L. Menges | | | | 8. Performing Organization Report No. Project 405491-1 | |
| 9. Performing Organization Name and Address Texas Transportation Institute The Texas A&M University System College Station, Texas 77843-3135 | | | | 10. Work Unit No. 3A5B | |
| | | | | 11. Contract or Grant No. DTFH61-95-C-00135 | |
| 12. Sponsoring Agency Name and Address Office of Safety & Traffic Operations R&D Federal Highway Administration 6300 Georgetown Pike McLean, Virginia 22101-2296 | | | | 13. Type of Report and Period Covered Draft Report September 1995 through May 1996 | |
| | | | | 14. Sponsoring Agency Code | |
| 15. Supplementary Notes Contracting Officer's Technical Representative (COTR) - Charles F. McDevitt - HSR-20 | | | | | |
| 16. Abstract <p>The New Jersey safety shaped barrier is one of the most common barriers currently in use on the Nation's highways. The barrier has successfully met all evaluation criteria set forth in National Cooperative Highway Research Program (NCHRP) Report 230. However, with the adoption of NCHRP Report 350 by the Federal Highway Administration (FHWA) as the official guidelines for crash testing of roadside safety features, it became necessary to reevaluate the New Jersey safety shaped barrier to the new guidelines. Of particular importance is the replacement of one of the design test vehicles specified in NCHRP Report 230, the 2044-kg passenger car, by a 2000-kg pickup truck (2000P) under NCHRP Report 350 guidelines. The crash test reported herein was performed as an effort to evaluate the New Jersey safety shaped barrier according to NCHRP Report 350 guidelines.</p> <p>The crash test performed corresponded to NCHRP Report 350 test designation 3-11 involving a 2000P test vehicle impacting the barrier at a nominal speed and angle of 100 km/h and 25 degrees. The New Jersey safety shaped barrier met all evaluation criteria set forth in NCHRP Report 350 and the test was judged to be satisfactory.</p> | | | | | |
| 17. Key Words Bridge rails, roadside safety, safety shape, barriers | | | | 18. Distribution Statement No restrictions. This document is available to the public through the National Technical Information Service, 5285 Port Royal Road, Springfield, Virginia 22161 | |
| 19. Security Classif. (of this report) Unclassified | | 20. Security Classif. (of this page) Unclassified | | 21. No. of Pages 42 | |
| | | | | 22. Price | |

SI* (MODERN METRIC) CONVERSION FACTORS

APPROXIMATE CONVERSIONS TO SI UNITS

APPROXIMATE CONVERSIONS FROM SI UNITS

| Symbol | When You Know | Multiply By | To Find | Symbol | Symbol | When You Know | Multiply By | To Find | Symbol |
|-------------------------------------|----------------------------|----------------------------|--------------------------------|-------------------|-------------------------------------|--------------------------------|-------------|----------------------------|---------------------|
| LENGTH | | | | | LENGTH | | | | |
| in | inches | 25.4 | millimeters | mm | mm | millimeters | 0.039 | inches | in |
| ft | feet | 0.305 | meters | m | m | meters | 3.28 | feet | ft |
| yd | yards | 0.914 | meters | m | m | meters | 1.09 | yards | yd |
| mi | miles | 1.61 | kilometers | km | km | kilometers | 0.621 | miles | mi |
| AREA | | | | | AREA | | | | |
| in ² | square inches | 645.2 | square millimeters | mm ² | mm ² | square millimeters | 0.0016 | square inches | in ² |
| ft ² | square feet | 0.093 | square meters | m ² | m ² | square meters | 10.764 | square feet | ft ² |
| yd ² | square yards | 0.836 | square meters | m ² | m ² | square meters | 1.195 | square yards | yd ² |
| ac | acres | 0.405 | hectares | ha | ha | hectares | 2.47 | acres | ac |
| mi ² | square miles | 2.59 | square kilometers | km ² | km ² | square kilometers | 0.386 | square miles | mi ² |
| VOLUME | | | | | VOLUME | | | | |
| fl oz | fluid ounces | 29.57 | milliliters | mL | mL | milliliters | 0.034 | fluid ounces | fl oz |
| gal | gallons | 3.785 | liters | L | L | liters | 0.264 | gallons | gal |
| ft ³ | cubic feet | 0.028 | cubic meters | m ³ | m ³ | cubic meters | 35.71 | cubic feet | ft ³ |
| yd ³ | cubic yards | 0.765 | cubic meters | m ³ | m ³ | cubic meters | 1.307 | cubic yards | yd ³ |
| MASS | | | | | MASS | | | | |
| oz | ounces | 28.35 | grams | g | g | grams | 0.035 | ounces | oz |
| lb | pounds | 0.454 | kilograms | kg | kg | kilograms | 2.202 | pounds | lb |
| T | short tons (2000 lb) | 0.907 | megagrams (or "metric ton") | Mg (or "t") | Mg (or "t") | megagrams (or "metric ton") | 1.103 | short tons (2000 lb) | T |
| TEMPERATURE (exact) | | | | | TEMPERATURE (exact) | | | | |
| °F | Fahrenheit temperature | 5(F-32)/9 or (F-32)/1.8 | Celcius temperature | °C | °C | Celcius temperature | 1.8C + 32 | Fahrenheit temperature | °F |
| ILLUMINATION | | | | | ILLUMINATION | | | | |
| fc | foot-candles | 10.76 | lux | lx | lx | lux | 0.0929 | foot-candles | fc |
| fl | foot-Lamberts | 3.426 | candela/m ² | cd/m ² | cd/m ² | candela/m ² | 0.2919 | foot-Lamberts | fl |
| FORCE and PRESSURE or STRESS | | | | | FORCE and PRESSURE or STRESS | | | | |
| lbf | poundforce | 4.45 | newtons | N | N | newtons | 0.225 | poundforce | lbf |
| lbf/in ² | poundforce per square inch | 6.89 | kilopascals | kPa | kPa | kilopascals | 0.145 | poundforce per square inch | lbf/in ² |

* SI is the symbol for the International System of Units. Appropriate rounding should be made to comply with Section 4 of ASTM E380.

(Revised September 1993)

TABLE OF CONTENTS

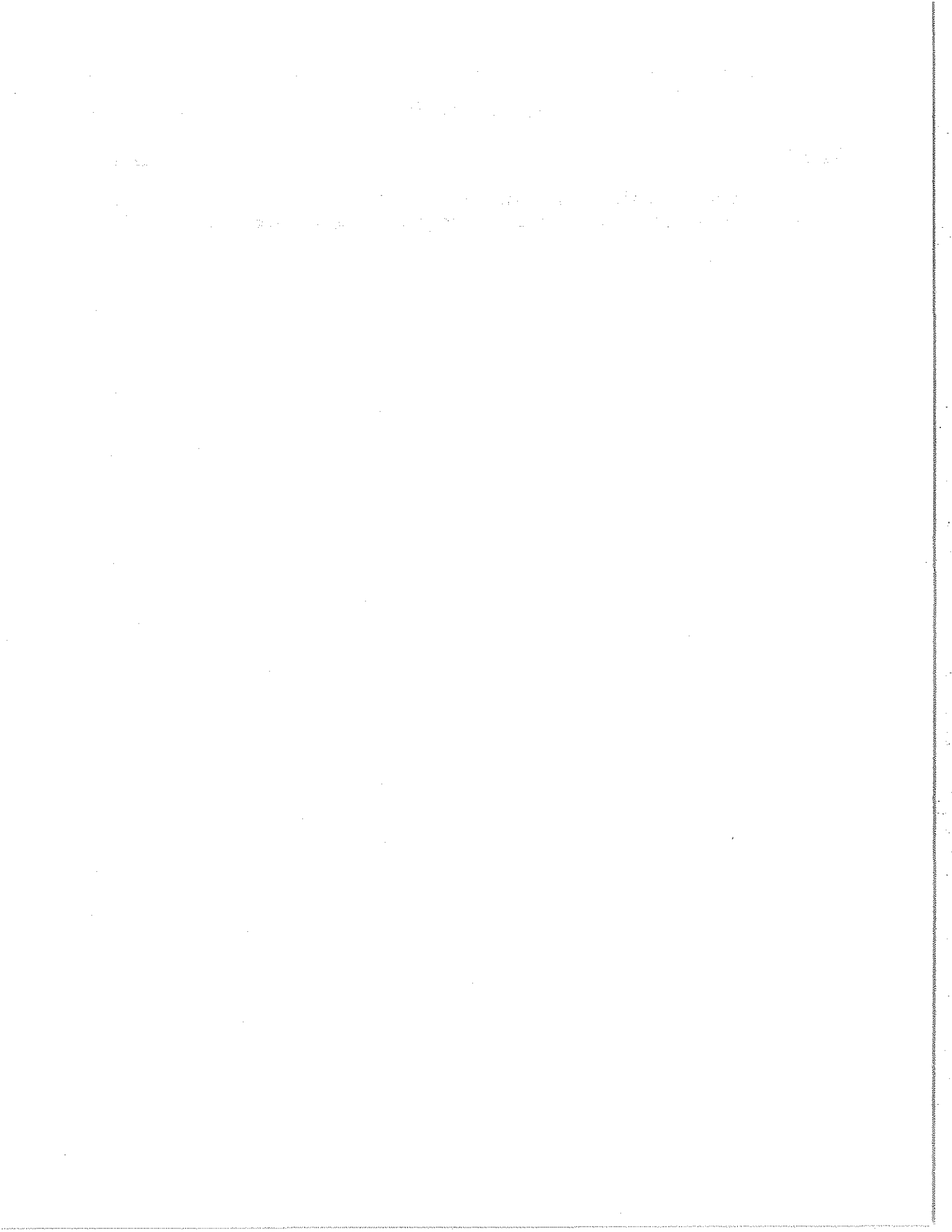
| | <u>Page</u> |
|---|-------------|
| I. INTRODUCTION | 1 |
| II. STUDY APPROACH | 3 |
| 2.1 TEST ARTICLE | 3 |
| 2.2 CRASH TEST CONDITIONS | 3 |
| 2.3 CRASH TEST AND DATA ANALYSIS PROCEDURES | 3 |
| 2.3.1 Electronic Instrumentation and Data Processing | 6 |
| 2.3.2 Anthropomorphic Dummy Instrumentation | 8 |
| 2.3.3 Photographic Instrumentation and Data Processing | 8 |
| 2.3.4 Test Vehicle Propulsion and Guidance | 8 |
| III. CRASH TEST RESULTS | 9 |
| 3.1 TEST DESCRIPTION | 9 |
| 3.2 DAMAGE TO TEST INSTALLATION | 9 |
| 3.3 VEHICLE DAMAGE | 18 |
| 3.4 OCCUPANT RISK VALUES | 18 |
| IV. SUMMARY OF FINDINGS AND CONCLUSIONS | 35 |
| REFERENCES | 37 |

LIST OF FIGURES

| <u>Figure No.</u> | | <u>Page</u> |
|-------------------|--|-------------|
| 1 | Details of the New Jersey safety shaped barrier test installation | 4 |
| 2 | New Jersey safety shaped barrier test installation before test 405491-1 | 5 |
| 3 | Vehicle/installation geometrics for test 405491-1 | 10 |
| 4 | Vehicle before test 405491-1 | 11 |
| 5 | Vehicle properties for test 405491-1 | 12 |
| 6 | Sequential photographs for test 405491-1 (overhead and oblique views) | 13 |
| 7 | Sequential photographs for test 405491-1 (frontal view) | 15 |
| 8 | Sequential photographs for test 405491-1 (onboard view) | 16 |
| 9 | New Jersey safety shaped barrier test installation after test 405491-1 | 17 |
| 10 | Vehicle after test 405491-1 | 19 |
| 11 | Interior of vehicle after test 405491-1 | 20 |
| 12 | Summary of results for test 405491-1 | 21 |
| 13 | Vehicle angular displacements for test 405491-1 | 22 |
| 14 | Vehicle longitudinal accelerometer trace for test 405491-1 (accelerometer located at center-of-gravity) | 23 |
| 15 | Vehicle lateral accelerometer trace for test 405491-1 (accelerometer located at center-of-gravity) | 24 |
| 16 | Vehicle vertical accelerometer trace for test 405491-1 (accelerometer located at center-of-gravity) | 25 |
| 17 | Vehicle longitudinal accelerometer trace for test 405491-1 (accelerometer located over vehicle rear axle) | 26 |
| 18 | Vehicle lateral accelerometer trace for test 405491-1 (accelerometer located over vehicle rear axle) | 27 |
| 19 | Vehicle vertical accelerometer trace for test 405491-1 (accelerometer located over vehicle rear axle) | 28 |
| 20 | Vehicle longitudinal accelerometer trace for test 405491-1 (accelerometer at top of instrument panel) | 29 |
| 21 | Vehicle lateral accelerometer trace for test 405491-1 (accelerometer located on right wheel) | 30 |
| 22 | Vehicle longitudinal accelerometer trace for test 405491-1 (accelerometer on left wheel) | 31 |
| 23 | Vehicle longitudinal accelerometer trace for test 405491-1 (accelerometer at top of engine) | 32 |
| 24 | Vehicle longitudinal accelerometer trace for test 405491-1 (accelerometer at bottom of engine) | 33 |

LIST OF TABLES

| <u>Table No.</u> | | <u>Page</u> |
|------------------|--|-------------|
| 1 | Locations of vehicle accelerometers for test 405491-1 | 7 |
| 2 | Assessment of results of test on New Jersey safety shaped barrier. | 36 |



I. INTRODUCTION

The Federal Highway Administration (FHWA) has recently adopted the new performance evaluation guidelines for roadside safety features set forth in National Cooperative Highway Research Program (NCHRP) Report 350.⁽¹⁾ Most of the existing roadside safety features were tested according to the previous guidelines contained in NCHRP Report 230⁽²⁾ and there are questions as to how the existing roadside safety features would perform under the new guidelines. Specifically, there is concern that existing barrier systems, including the New Jersey safety shaped barrier, may not perform satisfactorily to contain and redirect the 2000P test vehicle, i.e., 2000-kg pickup truck, and the vehicle may vault or go over the barrier or roll over. A series of crash tests were therefore conducted with the 2000P test vehicle on the more commonly used guardrail systems, one of which is the New Jersey safety shaped barrier. All these pickup truck crash tests were conducted under NCHRP Report 350 test level 3 conditions, i.e., impacting the length-of-need section at a nominal speed and angle of 100 km/h and 25 degrees.

This report contains the results of a crash test conducted on the New Jersey safety shaped barrier with a 2000-kg pickup truck under NCHRP Report 350 test level 3 conditions. The purpose of the test was to determine if the barrier would perform satisfactorily with the 2000P test vehicle under the new NCHRP Report 350 requirements.

1. The first part of the document discusses the importance of maintaining accurate records of all transactions and activities. It emphasizes that proper record-keeping is essential for ensuring transparency and accountability in financial reporting. This section also highlights the role of internal controls in preventing errors and fraud, and the need for regular audits to verify the accuracy of the data.

2. The second part of the document focuses on the importance of communication and collaboration between different departments and stakeholders. It stresses that effective communication is key to ensuring that everyone is on the same page and that information is shared in a timely and accurate manner. This section also discusses the importance of documenting all communications and decisions, and the need for clear lines of responsibility and authority.

3. The third part of the document discusses the importance of staying up-to-date on industry trends and regulations. It emphasizes that organizations must be proactive in monitoring changes in the market and regulatory environment, and must be prepared to adapt their strategies and processes accordingly. This section also highlights the importance of ongoing training and development for employees, and the need for a culture of continuous learning and improvement.

4. The fourth part of the document discusses the importance of maintaining a strong relationship with customers and clients. It emphasizes that excellent customer service is a key differentiator for many organizations, and that it is essential for building trust and loyalty. This section also discusses the importance of understanding customer needs and preferences, and the need for personalized and proactive service.

5. The fifth part of the document discusses the importance of maintaining a strong relationship with suppliers and vendors. It emphasizes that reliable and high-quality suppliers are essential for ensuring the smooth operation of an organization's supply chain. This section also discusses the importance of negotiating favorable terms and conditions, and the need for clear communication and collaboration with suppliers.

II. STUDY APPROACH

2.1 TEST ARTICLE

The New Jersey safety shaped barrier used for this crash test was actually a bridge rail constructed under a previous study. Since the New Jersey safety shaped barrier is a rigid barrier, the fact that the test installation was a bridge rail and not a roadside barrier has no effect on the results of the crash test. The total length of the test installation was 30.5 m. A cross section of the test installation is shown in figure 1 and photographs of the test installation are shown in figure 2.

The total height of the New Jersey safety shaped barrier is 813 mm. The thickness of the barrier is 381 mm at its base and 152 mm at the top. Again, since the barrier is a rigid barrier, the thickness of the barrier has no effect on the results of the crash test as long as the structural capacity of the barrier is sufficient to handle the impact force imparted by the test vehicle. For this particular test installation, the barrier has eight 13-mm diameter longitudinal bars and 16-mm diameter stirrups spaced at 203 mm center to center. The specified concrete strength was 24 804 kPa at 28 days, and specified yield strength for the steel rebars was 413 400 kPa. The barrier was attached to a cantilevered bridge deck with an overhang of 991 mm.

2.2 CRASH TEST CONDITIONS

The crash test conducted on the New Jersey safety shaped barrier was NCHRP Report 350 test designation 3-11 which involved a 2000P test vehicle impacting the length-of-need section of the barrier at a nominal speed and angle of 100 km/h and 25 degrees. The impact point was selected to be near the one-third point of the test installation. The typical purpose of this length-of-need redirection test is to evaluate the structural adequacy of the barrier in containing and redirecting the 2000P test vehicle. However, for the New Jersey safety shaped barrier, there was no question that the barrier has the required structural capacity to contain and redirect a 2000P test vehicle. The concern was more with the stability and post-impact trajectory of the test vehicle since the 2000P test vehicle has been shown to have the propensity for rolling over in similar tests with other barrier systems.

2.3 CRASH TEST AND DATA ANALYSIS PROCEDURES

The crash test and data analysis procedures were in accordance with guidelines presented in NCHRP Report 350. Brief descriptions of these procedures are presented as follows.

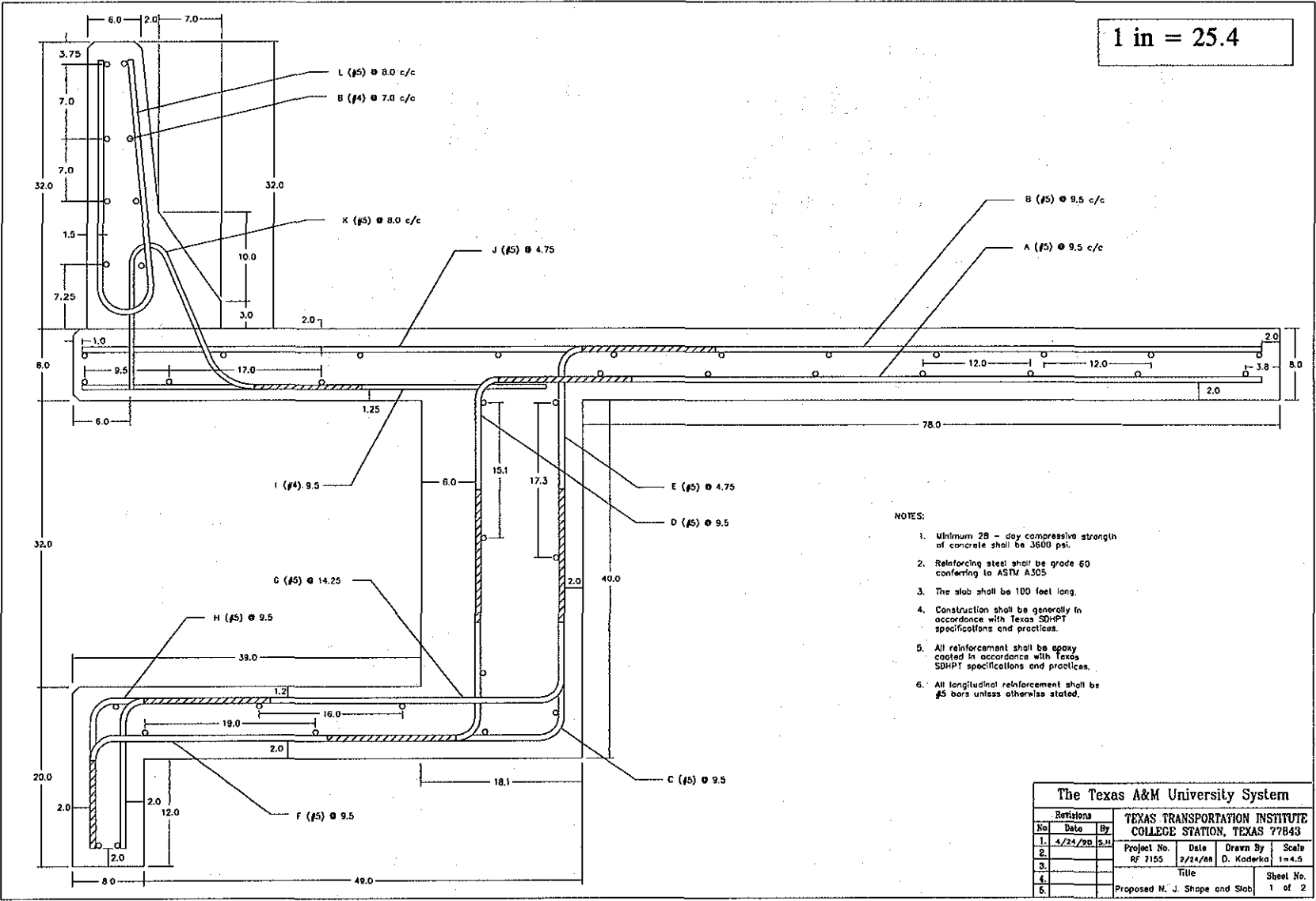


Figure 1. Details of the New Jersey safety shaped barrier test installation.

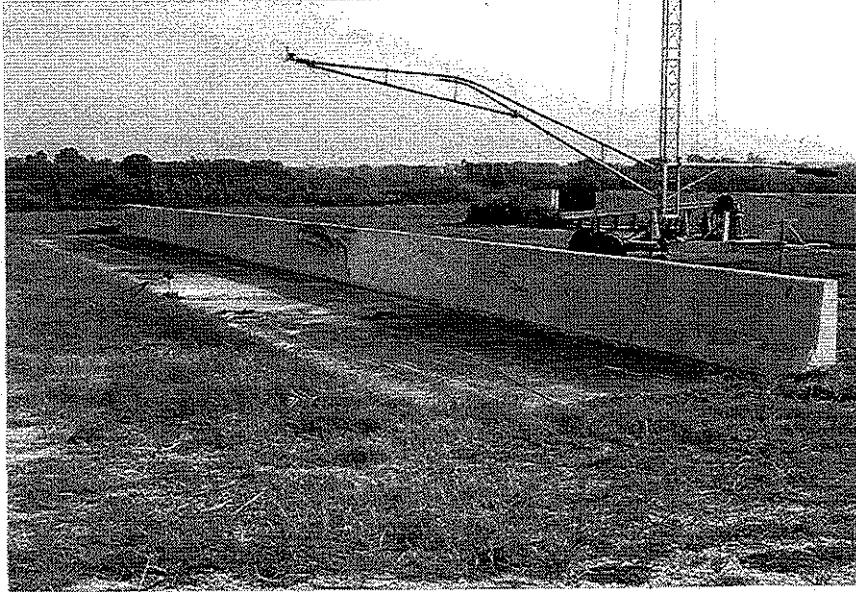


Figure 2. New Jersey safety shaped barrier test installation before test 405491-1.

2.3.1 Electronic Instrumentation and Data Processing

The test vehicle was instrumented with three solid-state angular rate transducers to measure roll, pitch and yaw rates; a triaxial accelerometer at the vehicle center-of-gravity to measure longitudinal, lateral, and vertical acceleration levels; and a triaxial accelerometer mounted in the bed of the vehicle over the rear axle to measure longitudinal, lateral, and vertical acceleration levels. The accelerometers were strain gauge type with a linear millivolt output proportional to acceleration.

The electronic signals from the triaxial accelerometers and the rate transducers were transmitted to a base station by means of constant bandwidth FM/FM telemetry link for recording on magnetic tape and for display on a real-time strip chart. Calibration signals were recorded before and after the test, and an accurate time reference signal was simultaneously recorded with the data. Pressure sensitive switches on the bumper of the impacting vehicle were actuated just prior to impact by wooden dowels to indicate the elapsed time over a known distance to provide a measurement of impact velocity. The initial contact also produced an "event" mark on the data record to establish the exact instant of contact with the barrier.

The multiplex of data channels, transmitted on one radio frequency, were received at the data acquisition station, and demultiplexed into separate tracks of Inter-Range Instrumentation Group (I.R.I.G.) tape recorders. After the test, the data were played back from the tape machines, filtered with an SAE J211 filter, and digitized using a microcomputer, for analysis and evaluation of impact performance.

In addition, the test vehicle was instrumented with five uniaxial accelerometers mounted in the following locations: (1) center top surface of instrument panel; (2) inside end of right front wheel spindle; (3) inside end of left front wheel spindle; (4) top of engine block; and (5) bottom of engine block. The exact locations of each accelerometer was measured and are reported in table 1. These accelerometers were ENDEVCO Model 7264A low mass piezoresistive accelerometers with a ± 2000 g range.

The data from these uniaxial accelerometers were captured using a Prosig P4000 data acquisition system. The P4000 is a modular, distributed data acquisition system based on independent data collection elements called POD's. Each POD has 4 high-speed analog, 3 digital and T-zero inputs. The POD's sample synchronously at up to 12.5 kHz per channel with 12-bit resolution. Non-volatile memory holds up to 13 s at 10 kHz data capture. Analog inputs have integral bridge conditioning, 8-pole fixed-frequency, low-pass Butterworth 48 dB/octave anti-aliasing filter. Each channel has a fully programmable amplifier and input offset adjustment. Data capture is started by a trigger pulse from a bumper switch or a predefined g level. Twenty-five percent of the captured data is prior to the trigger signal.

The digitized data were then processed using two computer programs: DIGITIZE and PLOTANGLE. Brief descriptions of the functions of these two computer programs are provided as follows.

Table 1. Locations of vehicle accelerometers for test 405491-1.

| Location | X (Distance from front bumper) | Y (Distance from centerline) | Z (Distance from ground) | Axis |
|--|--------------------------------------|------------------------------------|--------------------------------|----------|
| Center top surface of instrument panel | -1575 | 0 | -1295 | +X |
| Inside end of right front wheel spindle | -889 | 635 | -356 | -Y* |
| Inside end of left front wheel spindle | -889 | -635 | -356 | +X |
| Top of engine block | -838 | 25 | -939 | +X |
| Bottom of engine block | -1156 | 0 | -381 | +X |
| Vehicle c.g. | -2375 | 0 | -737 | +X,+Y,+Z |
| Vehicle rear axle | -4242 | 0 | -889 | +X,+Y,+Z |

* Data corrected in graphical output to show +Y.

The DIGITIZE program uses digitized data from vehicle-mounted linear accelerometers to compute occupant/compartiment impact velocities, time of occupant/compartiment impact after vehicle impact, and the highest 10-ms average ridedown acceleration. The DIGITIZE program also calculates a vehicle impact velocity and the change in vehicle velocity at the end of a given impulse period. In addition, maximum average accelerations over 50-ms intervals in each of the three directions are computed. For reporting purposes, the data from the vehicle-mounted triaxial accelerometers were then filtered with a 60 Hz digital filter and acceleration versus time curves for the longitudinal, lateral, and vertical directions were plotted using a commercially available software package (QUATTRO PRO). The data from the five uniaxial accelerometers were filtered with a Class 180 filter and acceleration versus time curves were plotted using QUATTRO PRO.

The PLOTANGLE program used the digitized data from the yaw, pitch, and roll rate transducers to compute angular displacement in degrees at 0.00067-s intervals and then instructs a plotter to draw a reproducible plot: yaw, pitch, and roll versus time. These displacements are in reference to the vehicle-fixed coordinate system with the initial position and orientation of the vehicle-fixed coordinate system being that which existed at initial impact.

2.3.2 Anthropomorphic Dummy Instrumentation

An Alderson Research Laboratories Hybrid II, 50th percentile male anthropomorphic dummy, restrained with standard equipment lap and shoulder belts, was placed in the driver's position of the vehicle. The dummy was un-instrumented; however, an onboard high-speed camera recorded the motions of the dummy during the test period.

2.3.3 Photographic Instrumentation and Data Processing

Photographic coverage of the test included four high-speed cameras: one overhead with a field of view perpendicular to the ground and directly over the impact point; and one placed behind the rail at an angle; a third placed to have a field of view parallel to and aligned with the installation at the downstream end; and a fourth placed onboard the vehicle to record the motions of the dummy placed in the driver seat during the test sequence. A flash bulb activated by pressure sensitive tapeswitches was positioned on the impacting vehicle to indicate the instant of contact with the barrier and was visible from each camera. The films from these high-speed cameras were analyzed on a computer-linked Motion Analyzer to observe phenomena occurring during the collision and to obtain time-event, displacement and angular data. A 16-mm movie cine, a Betacam and a VHS-format video cameras and recorders, and still cameras were used for to record and document conditions of the test vehicle and installation after the test.

2.3.4 Test Vehicle Propulsion and Guidance

The test vehicle was towed into the test installation using a steel cable guidance and reverse tow system. A steel cable for guiding the test vehicle was tensioned along the path, anchored at each end, and threaded through an attachment to the front wheel of the test vehicle. An additional steel cable was connected to the test vehicle, passed around a pulley near the impact point, through a pulley on the tow vehicle, and then anchored to the ground such that the tow vehicle moved away from the test site. A 2 to 1 speed ratio between the test and tow vehicle existed with this system. Just prior to impact with the installation, the test vehicle was released to be free-wheeling and unrestrained. The vehicle remained free-wheeling, i.e., no steering or braking inputs, until the vehicle cleared the immediate area of the test site, at which time brakes on the vehicle were activated to bring it to a safe and controlled stop.

III. CRASH TEST RESULTS

A 1991 Chevrolet 2500 pickup truck, shown in figures 3 and 4, was used for this crash test on the New Jersey safety shaped barrier (test no. 405491-1). Test inertia weight of the vehicle was 2000 kg, and its gross static weight was 2077 kg. The height to the lower edge of the vehicle bumper was 435 mm and it was 655 mm to the upper edge of the bumper. Additional dimensions and information on the vehicle are given in figure 5. The vehicle was directed into the installation using the cable reverse tow and guidance system, and was released to be free-wheeling and unrestrained just prior to impact.

3.1 TEST DESCRIPTION

The vehicle impacted the barrier 3.1 m downstream of the upstream end of the test installation at a speed of 101.2 km/h and at an angle of 25.6 degrees. At 0.019 s after initial impact, the right front tire aired out, and at 0.208 s, the right front tire reached the top of the barrier. The vehicle became parallel with the installation at 0.224 s traveling at the speed of 80.8 km/h. The vehicle became totally airborne at 0.243 s, and shortly thereafter, the front of the vehicle started to nose down. At 0.375 s, the vehicle lost contact with the safety shape, traveling at a speed of 80.6 km/h with an exit angle of 1.3 degrees. The left front wheel contacted the ground at 0.532 s, and the right front tire made contact with the ground at 0.828 s. Maximum roll angle of 34 degrees occurred at 1.079 s. At 1.181 s, the left rear wheel of the vehicle contacted the ground, and the vehicle began to yaw clockwise. Brakes were applied after the vehicle exited the test area, and the vehicle subsequently came to rest facing back toward the installation 56.4 m downstream from point of impact. Photographs of the test sequence are shown in figures 6 through 8.

3.2 DAMAGE TO TEST INSTALLATION

There was only cosmetic damage to the New Jersey safety shaped barrier, as shown in figure 9. Tire marks reached the top of the barrier starting at 0.5 m after impact and continued along the top edge of the barrier on the traffic side until loss of contact. However, the tire marks did not extend across the top of the barrier. Total length of contact of the vehicle with the barrier was 6.8 m.

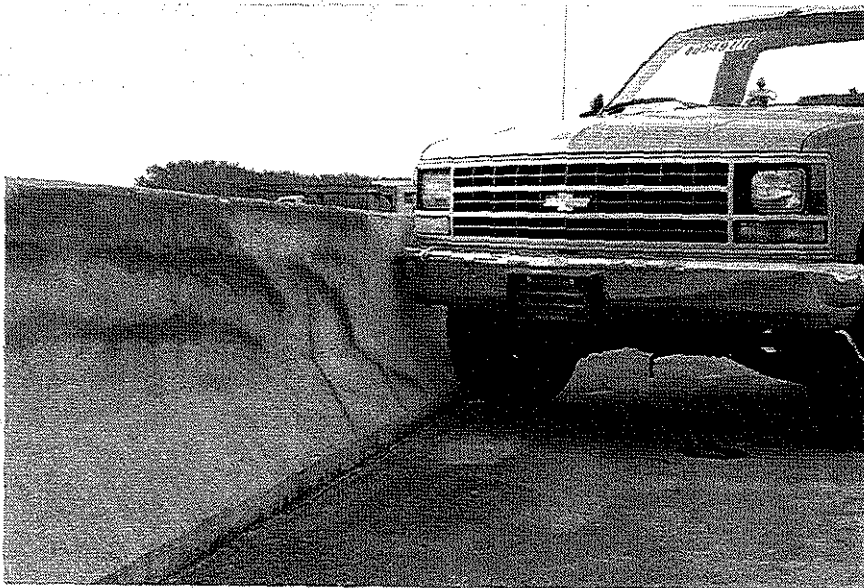
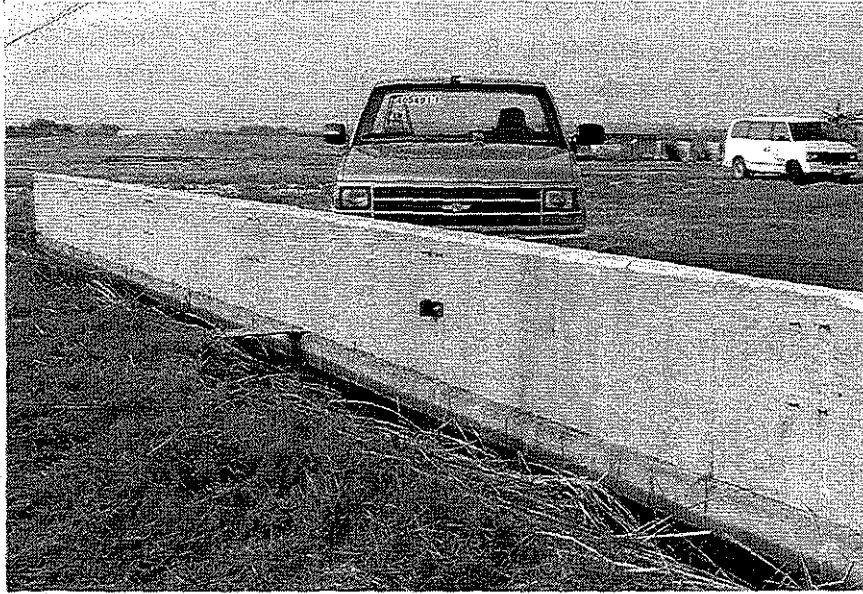


Figure 3. Vehicle/installation geometrics for test 405491-1.

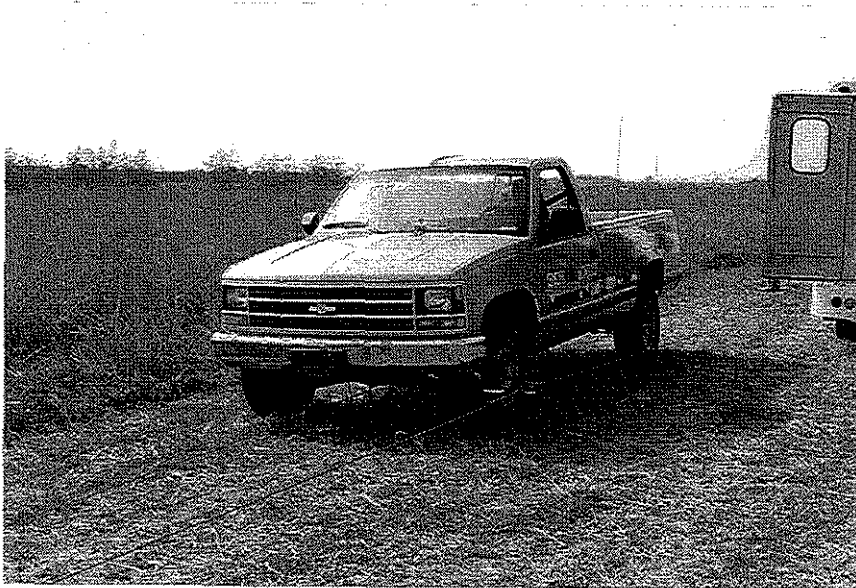


Figure 4. Vehicle before test 405491-1.

DATE: 09/06/95 TEST NO.: 405491-1 VIN NO.: 1GCGC24K3MF130540
 YEAR: 1991 MAKE: Chevrolet MODEL: 2500 Pickup
 TIRE INFLATION PRESSURE: _____ ODOMETER: 099387 TIRE SIZE: 245/75R16

MASS DISTRIBUTION (kg) LF 542 RF 549 LR 455 RR 454

DESCRIBE ANY DAMAGE TO VEHICLE PRIOR TO TEST:

● Denotes accelerometer location.
 NOTES: _____

ENGINE TYPE: 8 cyl
 ENGINE CID: 5.7 L
 TRANSMISSION TYPE:
 AUTO
 MANUAL
 OPTIONAL EQUIPMENT:

DUMMY DATA:
 TYPE: _____
 MASS: _____
 SEAT POSITION: _____

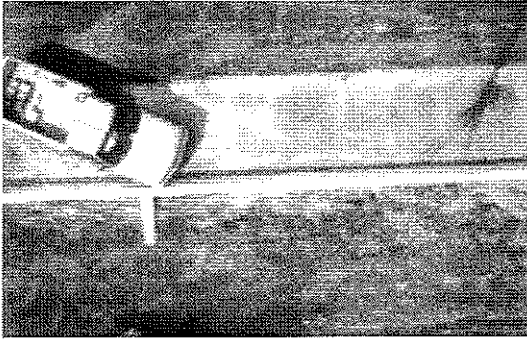
GEOMETRY - (mm)

| | | | | | | | | | |
|---|-------------|---|---------------|---|-------------|---|-------------|---|-------------|
| A | <u>1890</u> | E | <u>1330</u> | J | <u>1085</u> | N | <u>1585</u> | R | <u>737</u> |
| B | <u>760</u> | F | <u>5590</u> | K | <u>655</u> | O | <u>1625</u> | S | <u>889</u> |
| C | <u>3345</u> | G | <u>1520.3</u> | L | <u>85</u> | P | <u>765</u> | T | <u>1505</u> |
| D | <u>1835</u> | H | _____ | M | <u>435</u> | Q | <u>445</u> | U | <u>3345</u> |

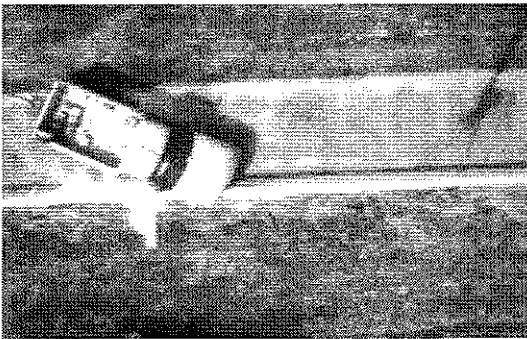
MASS - (kg)

| MASS - (kg) | CURB | TEST INERTIAL | GROSS STATIC |
|----------------|-------------|---------------|--------------|
| M ₁ | <u>1159</u> | <u>1091</u> | <u>1139</u> |
| M ₂ | <u>902</u> | <u>909</u> | <u>938</u> |
| M _T | <u>2061</u> | <u>2000</u> | <u>2077</u> |

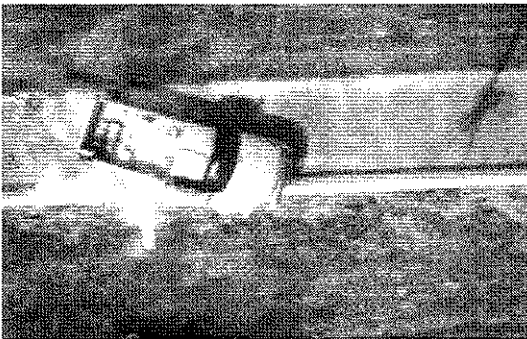
Figure 5. Vehicle properties for test 405491-1.



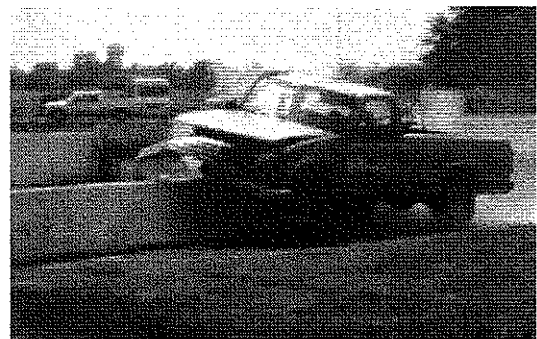
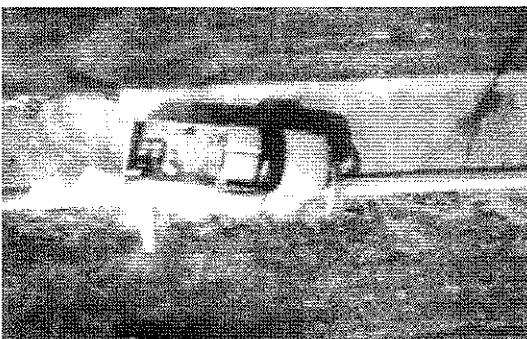
0.000 s



0.054 s

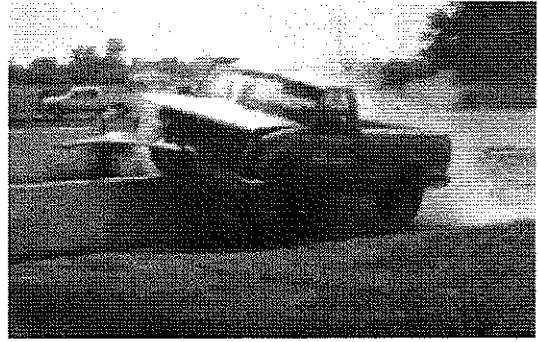
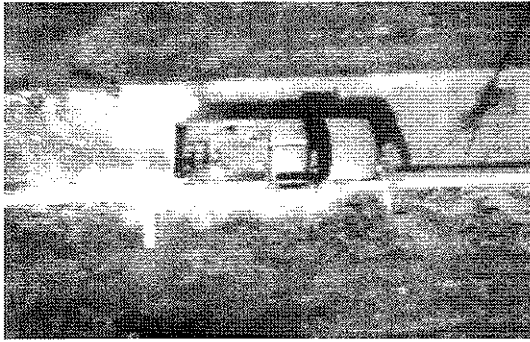


0.107 s

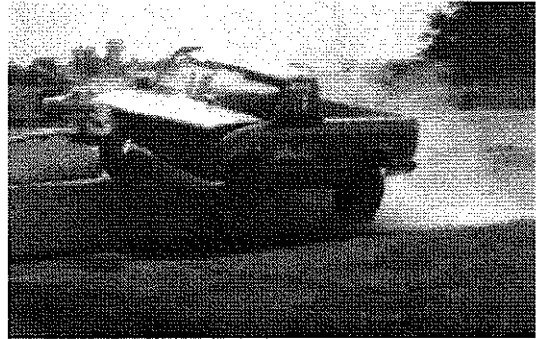
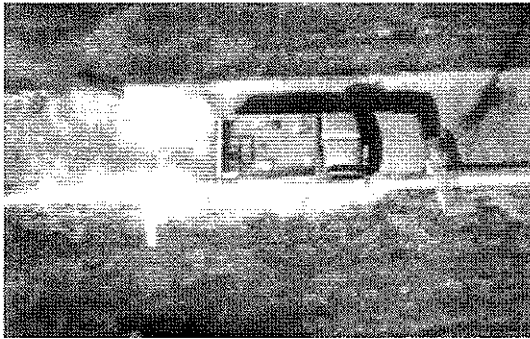


0.161 s

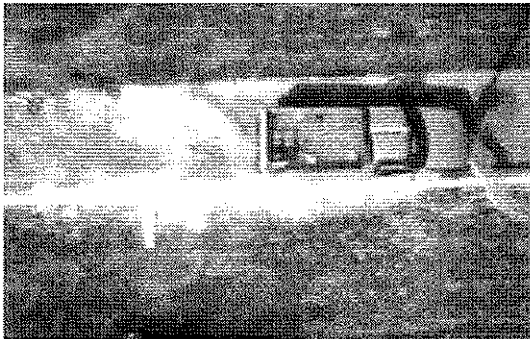
Figure 6. Sequential photographs for test 405491-1 (overhead and oblique views).



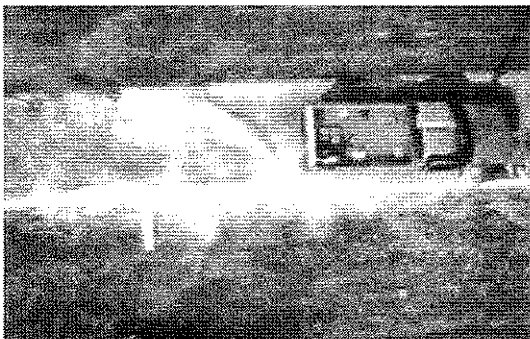
0.214 s



0.268 s



0.322 s

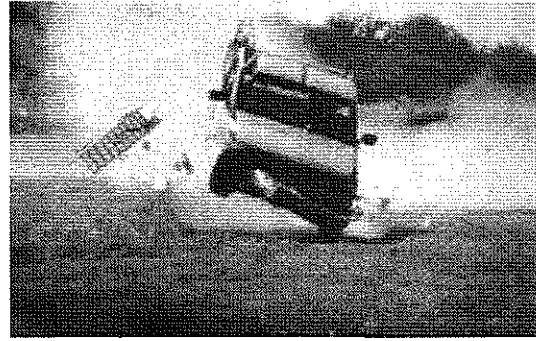


0.375 s

Figure 6. Sequential photographs for test 405491-1 (overhead and oblique views) (continued).



0.000 s



0.588 s



0.147 s



0.735 s



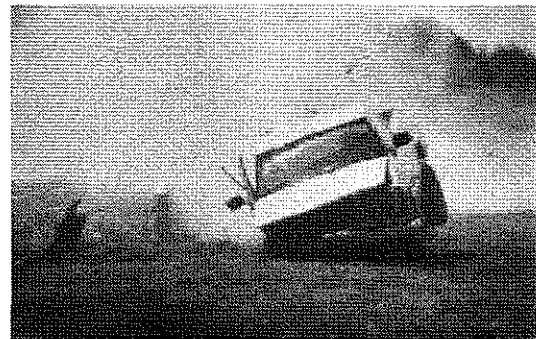
0.294 s



0.882 s

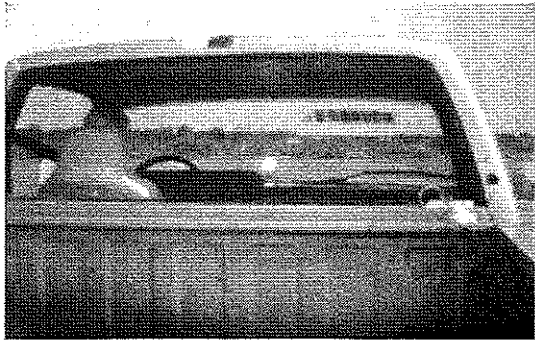


0.441 s

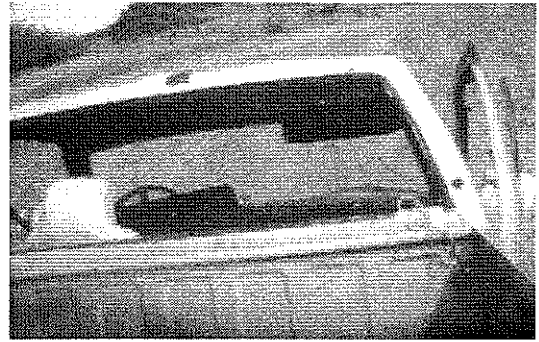


1.029 s

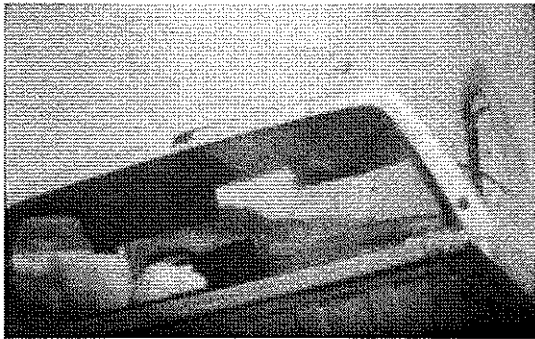
Figure 7. Sequential photographs for test 405491-1
(frontal view).



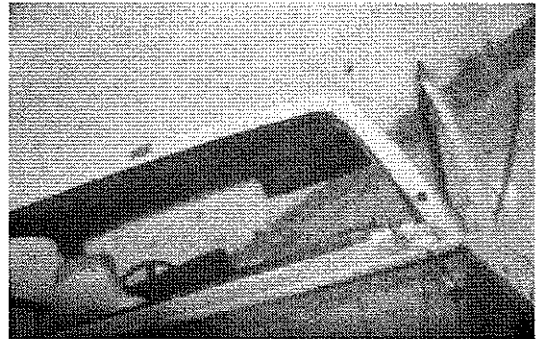
0.000 s



0.880 s



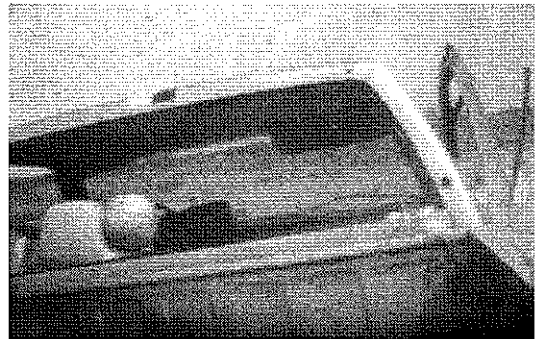
0.220 s



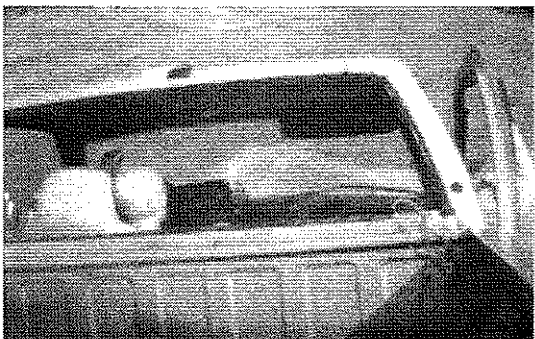
1.110 s



0.440 s



1.320 s



0.660 s



1.540 s

Figure 8. Sequential photographs for test 405491-1
(on-board view).

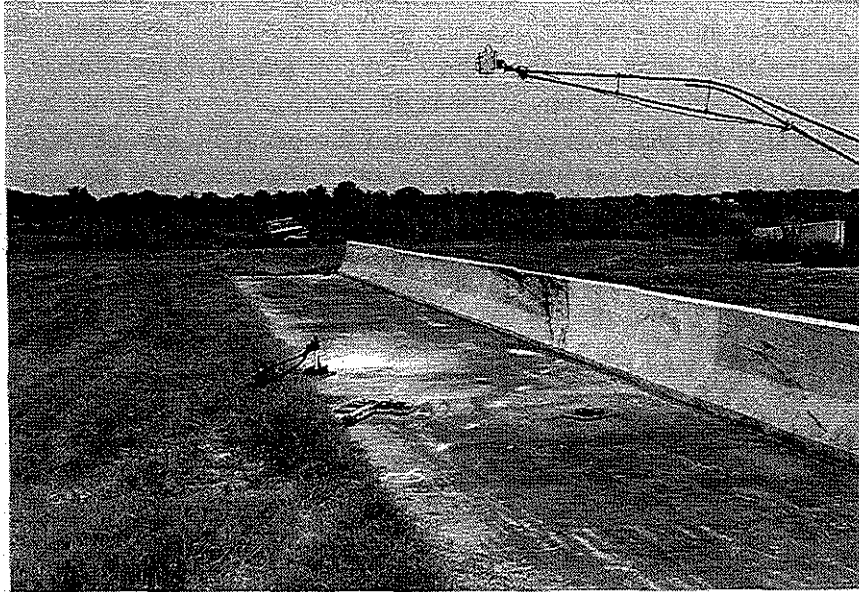


Figure 9. New Jersey safety shaped barrier test installation after test 405491-1.

3.3 VEHICLE DAMAGE

The front and right side of the vehicle were damaged during impact as shown in figure 10. The right side stabilizer bar, tie rods, and A-arms were damaged, and the right front frame was bent. Also damaged were the bumper, grill, radiator and fan, the right and left front quarter panels, the right door, and the right front and rear tires and rims. Maximum exterior crush to the vehicle was 560 mm at the right front corner at bumper height. During the collision the right side firewall was pushed toward the occupant compartment and deformed the floorpan and instrument panel, and caused stress cracks in the windshield. Maximum deformation into the occupant compartment was 84 mm at the center front firewall area. Buckling of the floorpan and damage to the instrument panel is shown in figure 11.

3.4 OCCUPANT RISK VALUES

Data from the accelerometers located at the vehicle center-of-gravity were digitized for evaluation of occupant risk and were computed as follows. In the longitudinal direction, the occupant impact velocity was 5.9 m/s at 0.161 s, the highest 0.010-s occupant ridedown acceleration was -4.5 g from 0.175 to 0.185 s, and the maximum 0.050-s average acceleration was -9.1 g between 0.010 and 0.060 s. In the lateral direction, the occupant impact velocity was 4.0 m/s at 0.143 s, the highest 0.010-s occupant ridedown acceleration was -19.6 g from 0.204 to 0.214 s, and the maximum 0.050-s average acceleration was -8.1 g between 0.176 and 0.226 s. These data and other pertinent information from the test are summarized in figure 12. Vehicle angular displacements are displayed in figure 13. Vehicular accelerations versus time traces are presented in figure 14 through 19. Five uniaxial accelerometers were mounted in various places on the vehicle and traces from these accelerometers are shown in figures 20 through 24.

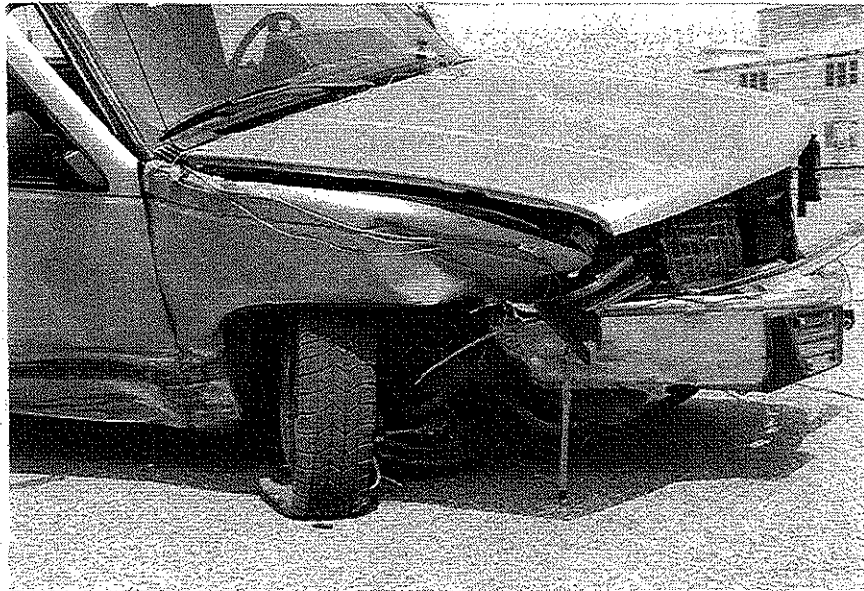
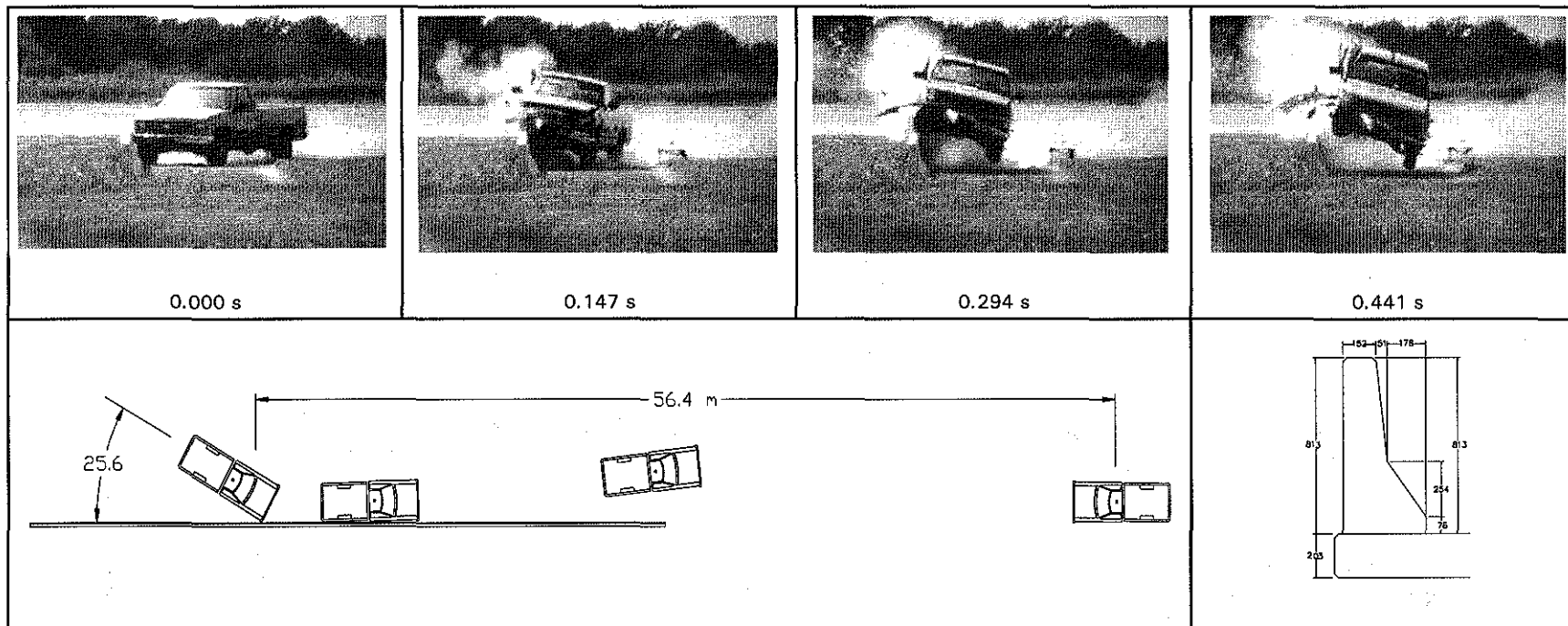


Figure 10. Vehicle after test 405491-1.



Figure 11. Interior of vehicle after test 405491-1.

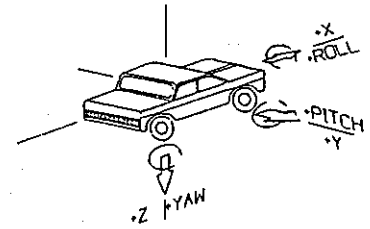
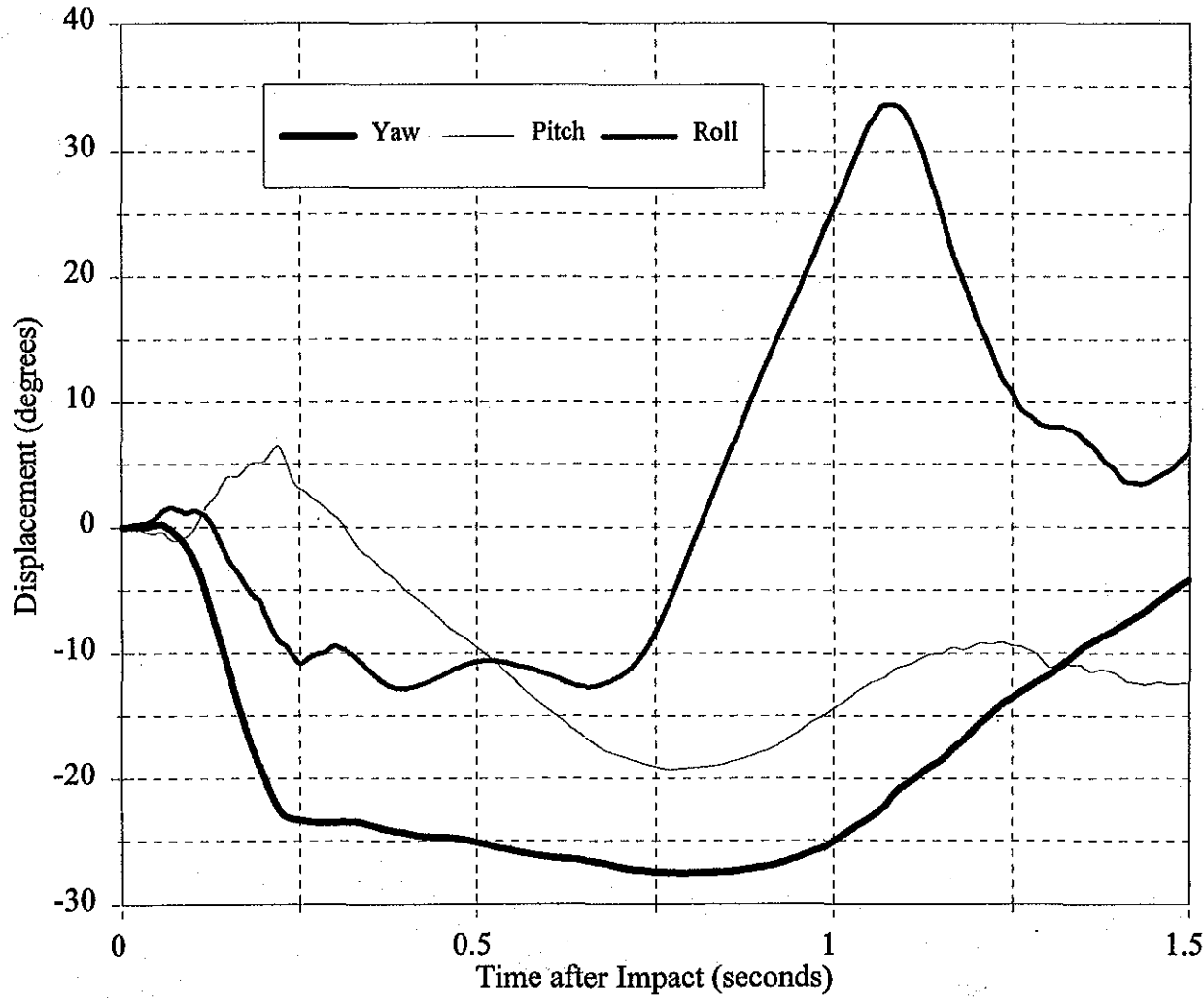


| | | | | | |
|----------------------------|--------------------------------|------------------------------|-------|-------------------------------------|-----------|
| General Information | | Impact Conditions | | Test Article Deflections (m) | |
| Test Agency | Texas Transportation Institute | Speed (km/h) | 101.2 | Dynamic | None |
| Test No. | 405491-1 | Angle (deg) | 25.6 | Permanent | None |
| Date | 09/06/95 | Exit Conditions | | Vehicle Damage | |
| Test Article | | Speed (km/h) | 80.6 | Exterior | |
| Type | Bridge Rail | Angle (deg) | 1.3 | VDS | 01RFQ5 |
| Name or Manufacturer | New Jersey Safety Shape | Occupant Risk Values | | CDC | 01FREW4 |
| Installation Length (m) | 30.5 | Impact Velocity (m/s) | | Interior | |
| Size and/or dimension | 813 mm Concrete New | x-direction | 5.9 | OCDI | AS0000000 |
| and material of key | Jersey Safety Shape | y-direction | 4.0 | Maximum Exterior | |
| elements | | THIV (optional) | | Vehicle Crush (mm) | 560 |
| Soil Type and Condition | Bridge deck, dry | Ridedown Accelerations (g's) | | Max. Occ. Compart. | |
| Test Vehicle | | x-direction | -4.5 | Deformation (mm) | 84 |
| Type | Production | y-direction | -19.6 | Post-Impact Behavior | |
| Designation | 2000P | PHD (optional) | | Max. Roll Angle (deg) | 34 |
| Model | 1991 Chevrolet 2500 Pickup | ASI (optional) | | Max. Pitch Angle (deg) | -21 |
| Mass (kg) Curb | 2061 | Max. 0.050-sec Average (g's) | | Max. Yaw Angle (deg) | -28 |
| Test Inertial | 2000 | x-direction | -9.1 | | |
| Dummy | 77 | y-direction | -8.1 | | |
| Gross Static | 2077 | z-direction | -10.7 | | |

Figure 12. Summary of results for test 405491-1.

Crash Test 405491-1

Vehicle Mounted Rate Transducers



Axes are vehicle fixed.
Sequence for determining
orientation is:

1. Yaw
2. Pitch
3. Roll

Figure 13. Vehicle angular displacements for test 405491-1.

Crash Test 405491-1

Accelerometer at center-of-gravity

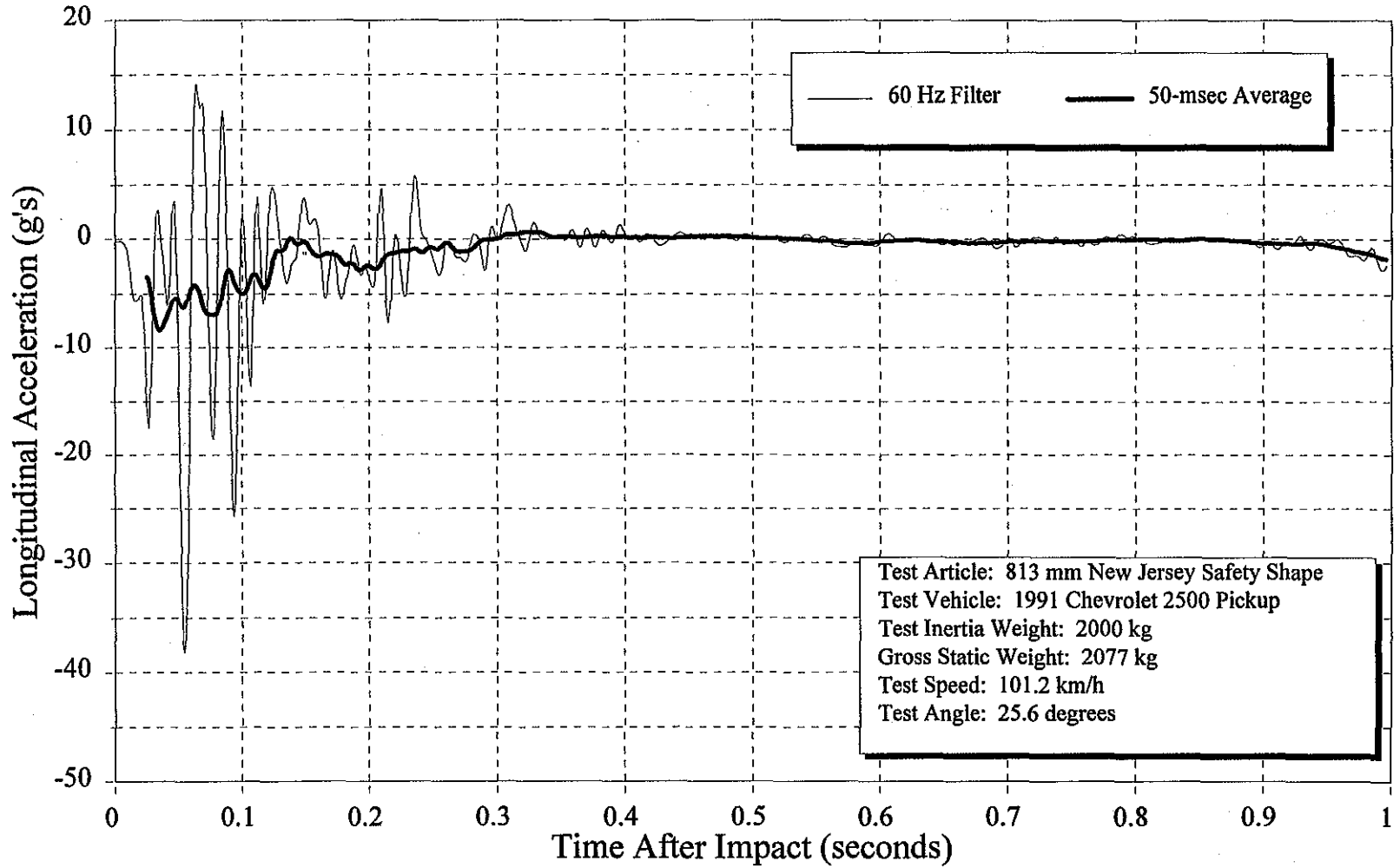


Figure 14. Vehicle longitudinal accelerometer trace for test 405491-1.
(accelerometer located at center-of-gravity)

Crash Test 405491-1

Accelerometer at center-of-gravity

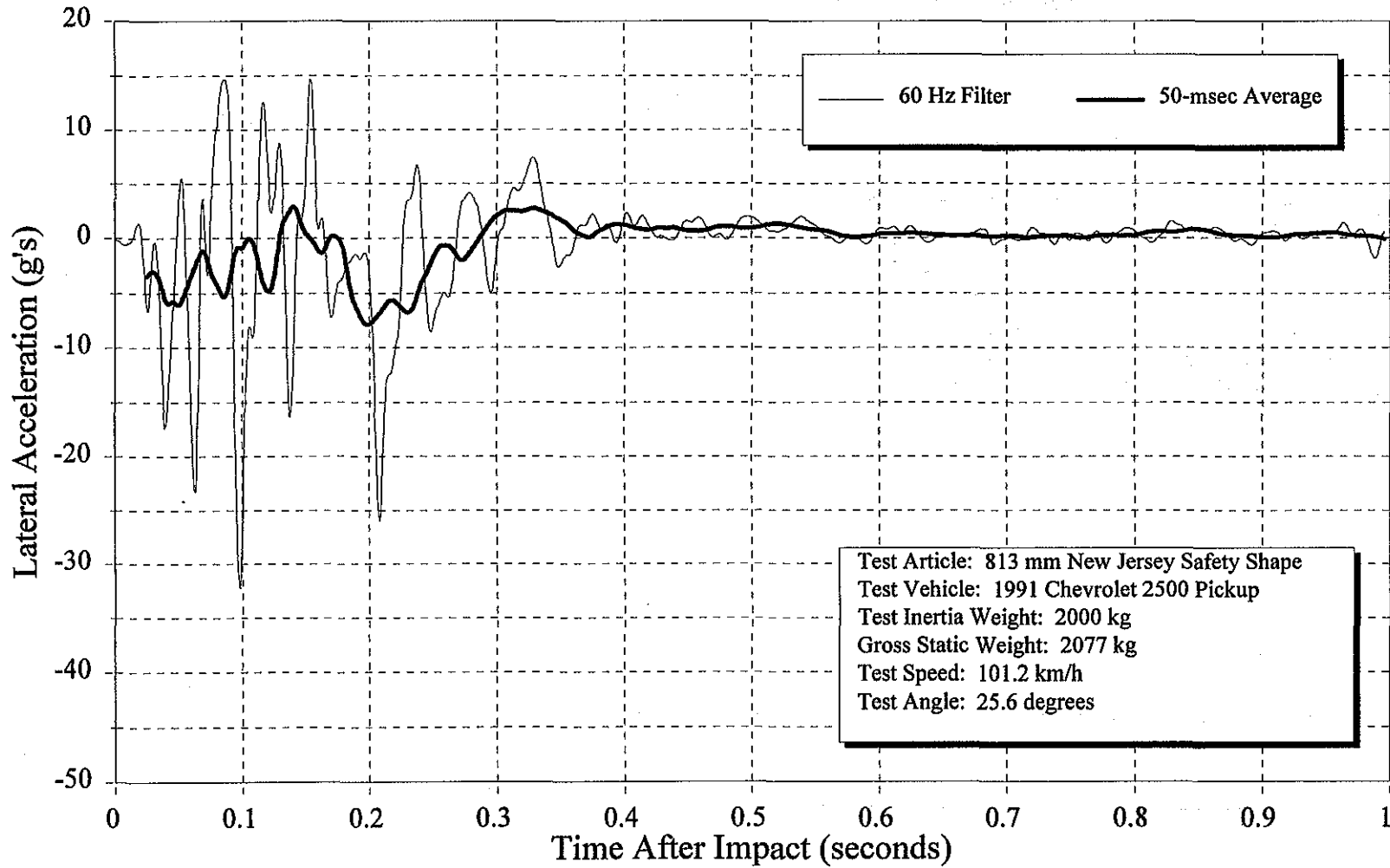
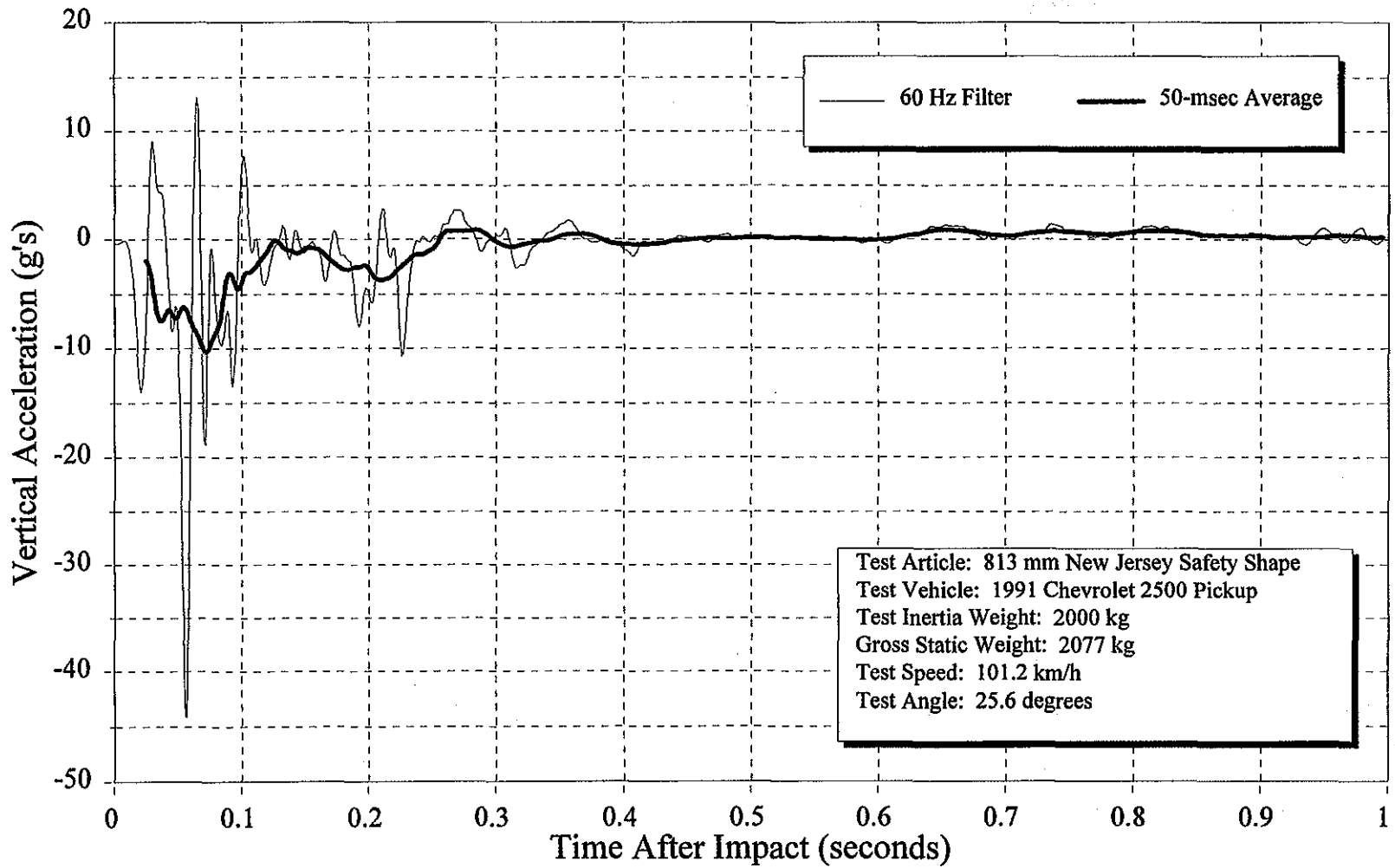


Figure 15. Vehicle lateral accelerometer trace for test 405491-1.
(accelerometer located at center-of-gravity)

Crash Test 405491-1

Accelerometer at center-of-gravity



25

Figure 16. Vehicle vertical accelerometer trace for test 405491-1.
(accelerometer located at center-of-gravity)

Crash Test 405491-1

Accelerometer over vehicle rear axle

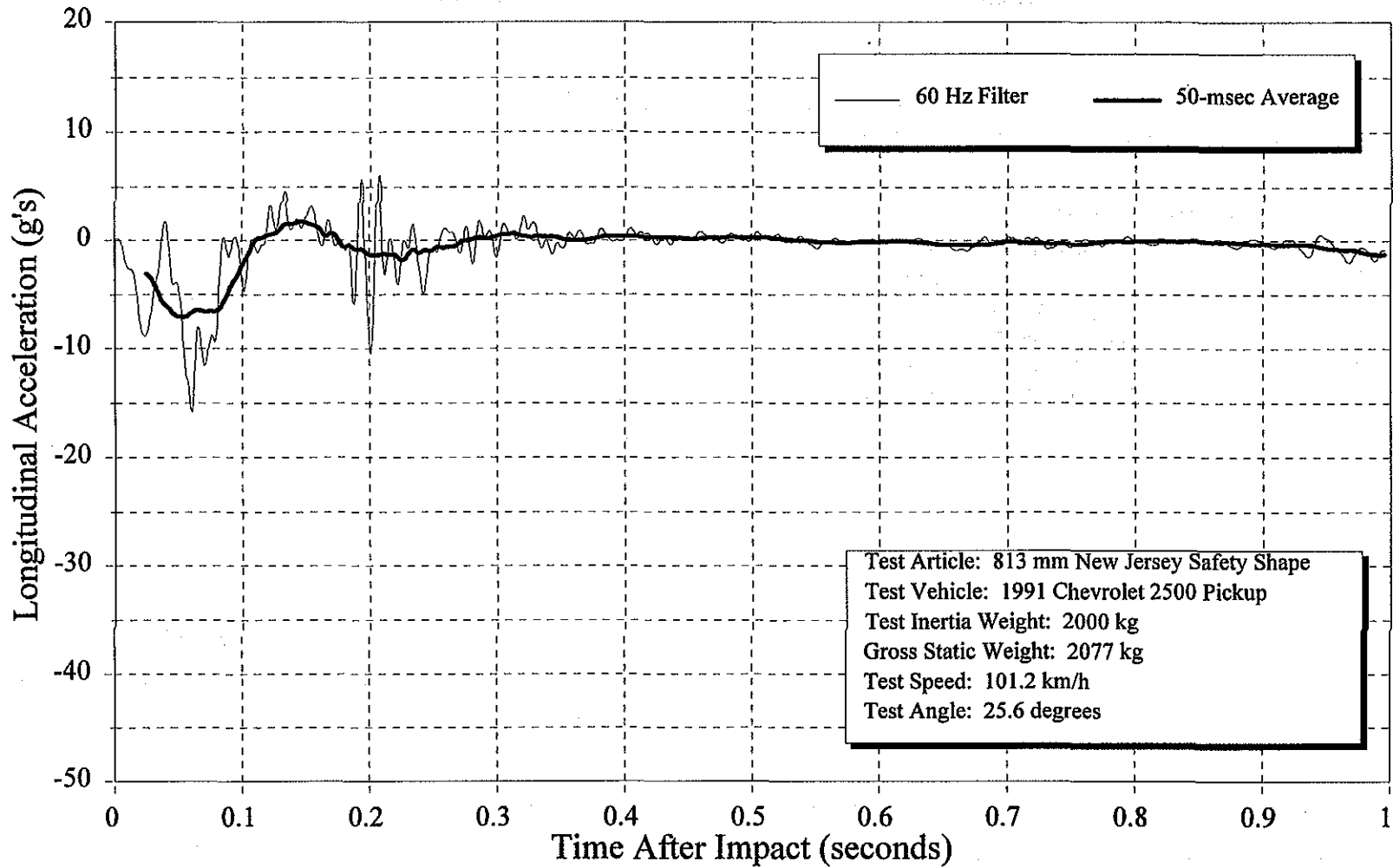


Figure 17. Vehicle longitudinal accelerometer trace for test 405491-1.
(accelerometer located over vehicle rear axle)

Crash Test 405491-1

Accelerometer over vehicle rear axle

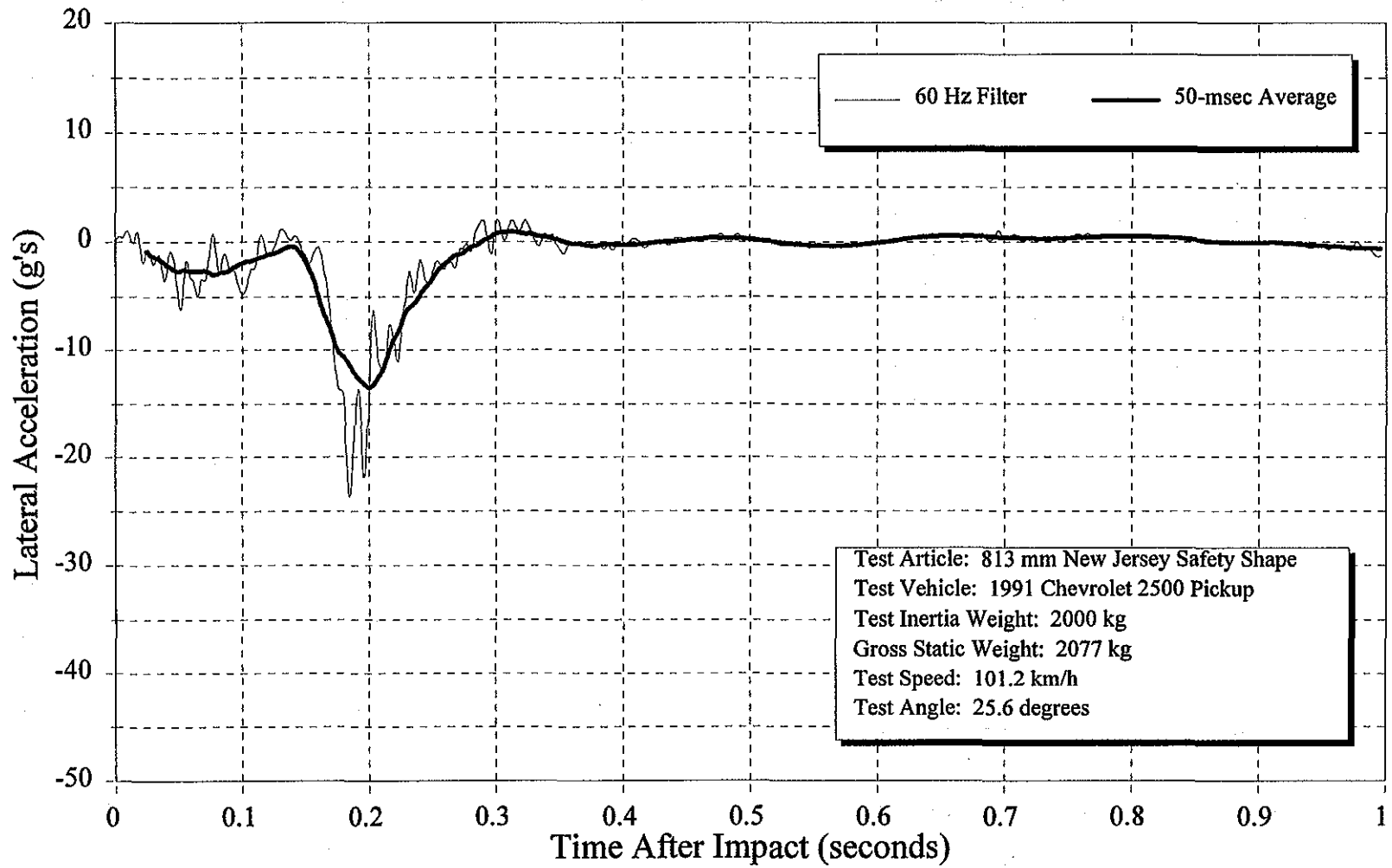


Figure 18. Vehicle lateral accelerometer trace for test 405491-1.
(accelerometer located over vehicle rear axle)

Crash Test 405491-1

Accelerometer over vehicle rear axle

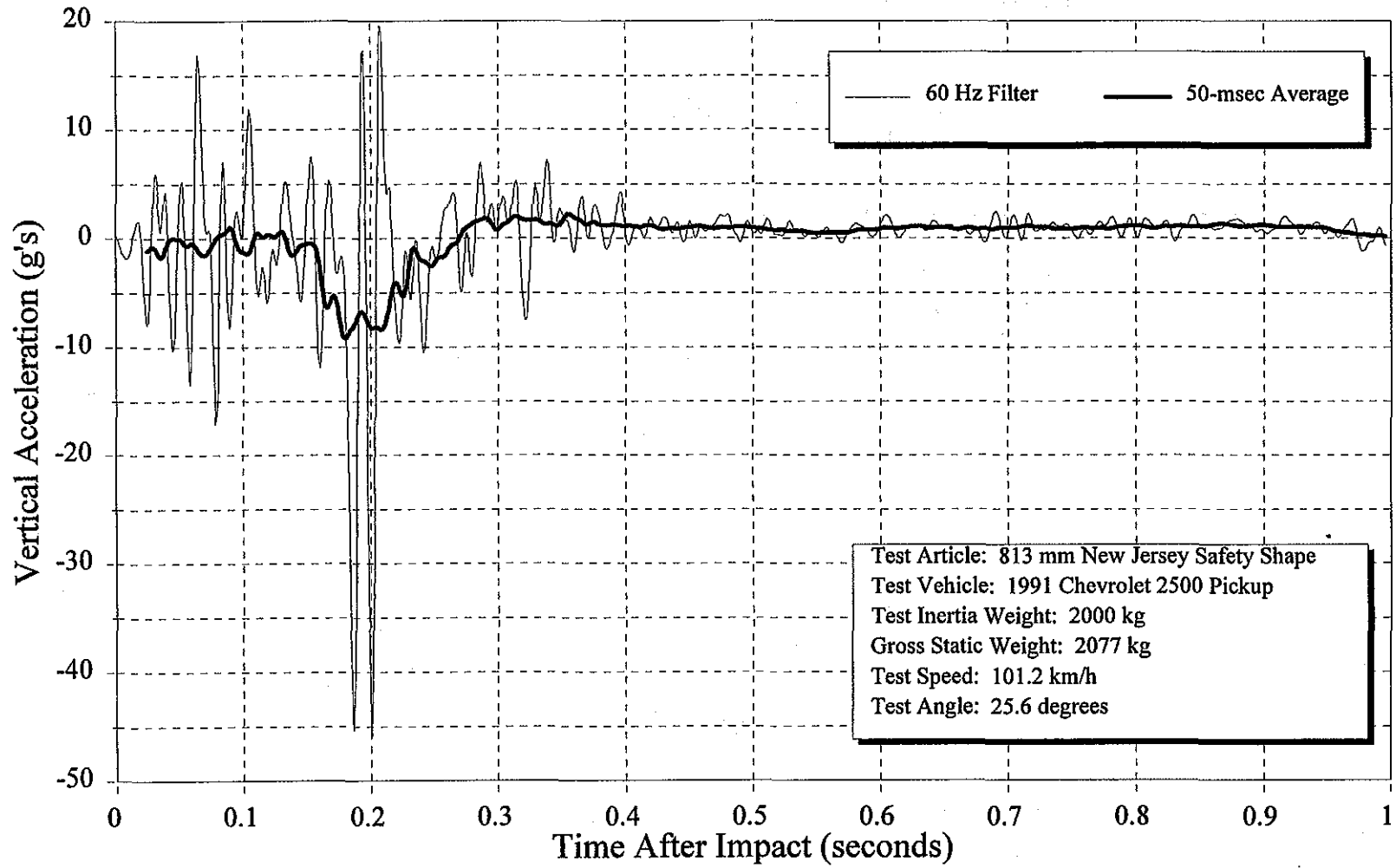


Figure 19. Vehicle vertical accelerometer trace for test 405491-1.
(accelerometer located over vehicle rear axle)

Crash Test 405491-1

Accelerometer at top of instr. panel

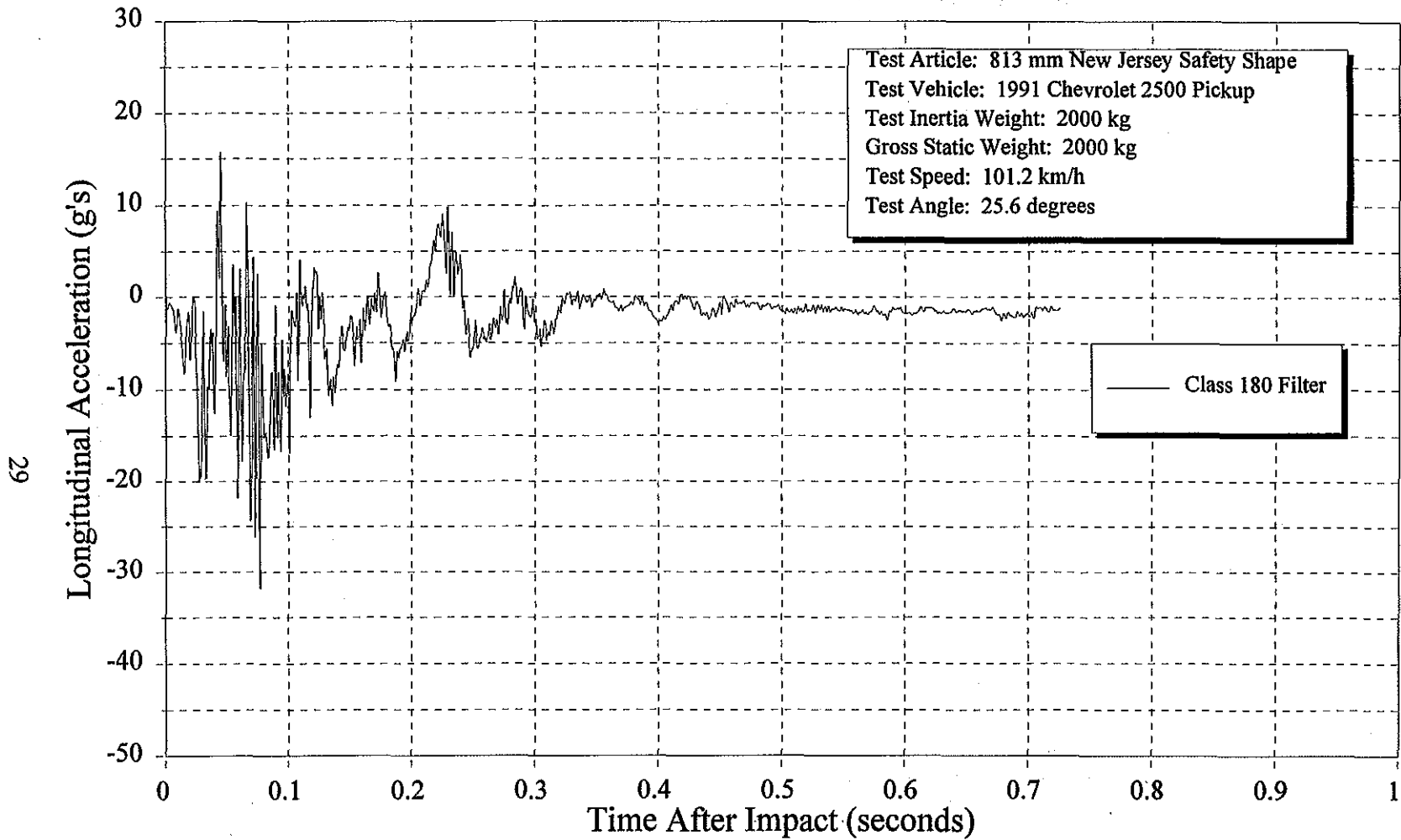
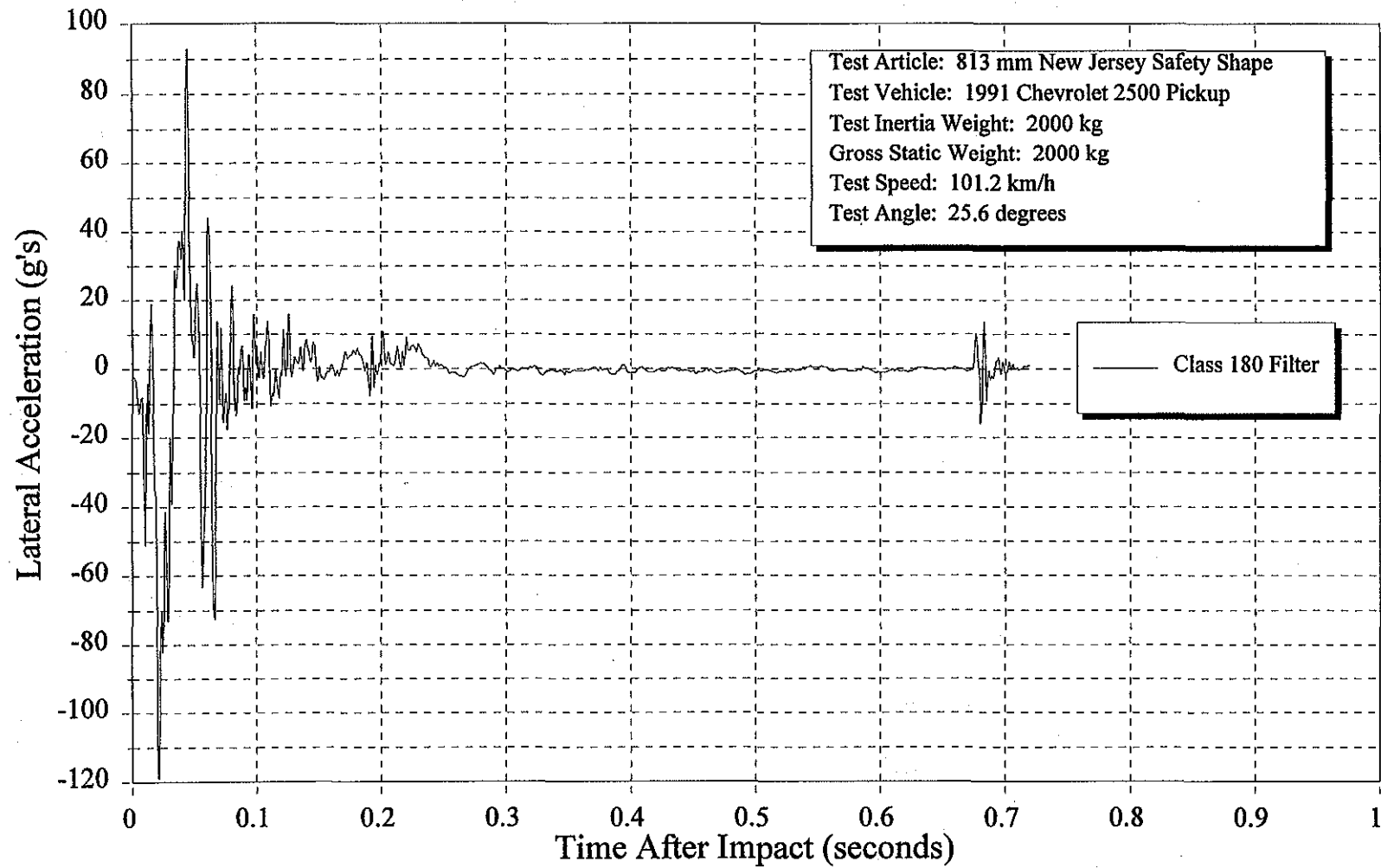


Figure 20. Vehicle longitudinal accelerometer trace for test 405491-1.
(accelerometer at top of instrument panel)

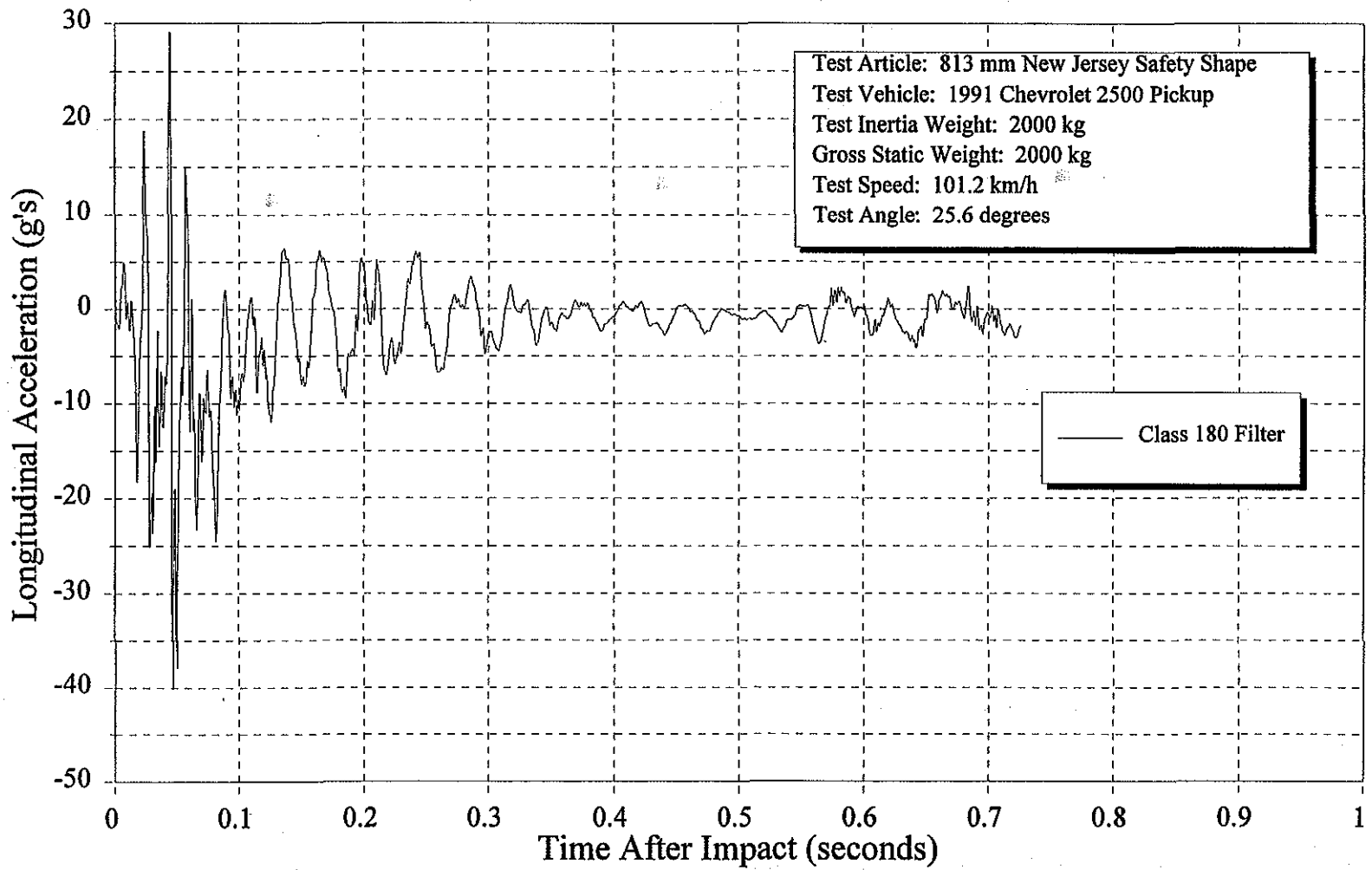
Crash Test 405491-1
Accelerometer on right wheel



30

Figure 21. Vehicle lateral accelerometer trace for test 405491-1.
(accelerometer on right wheel)

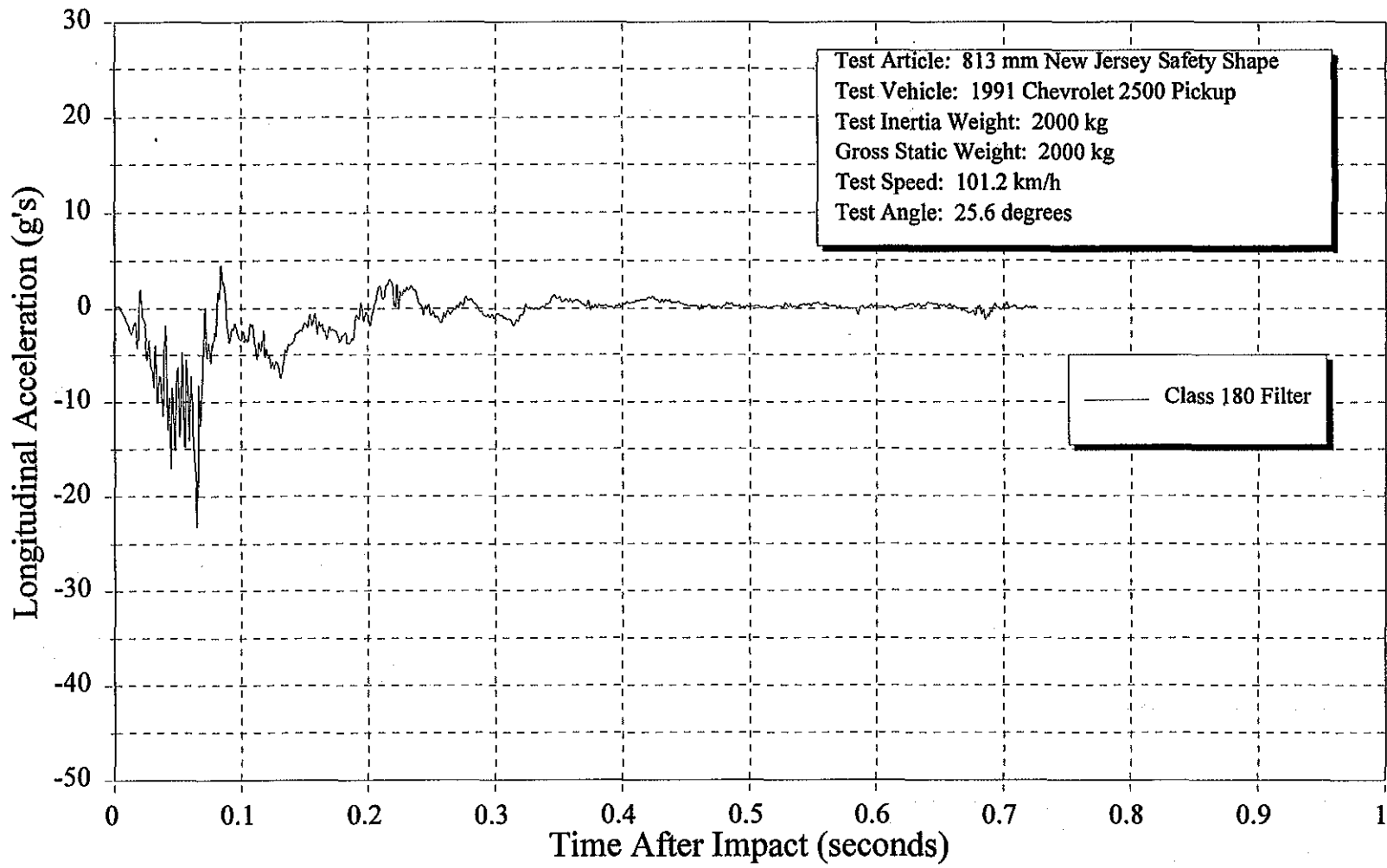
Crash Test 405491-1
Accelerometer on left wheel



31

Figure 22. Vehicle longitudinal accelerometer trace for test 405491-1.
(accelerometer on left wheel)

Crash Test 405491-1
Accelerometer at top of engine



32

Figure 23. Vehicle longitudinal accelerometer trace for test 405491-1.
(accelerometer at top of engine)

Crash Test 405491-1
Accelerometer at bottom of engine

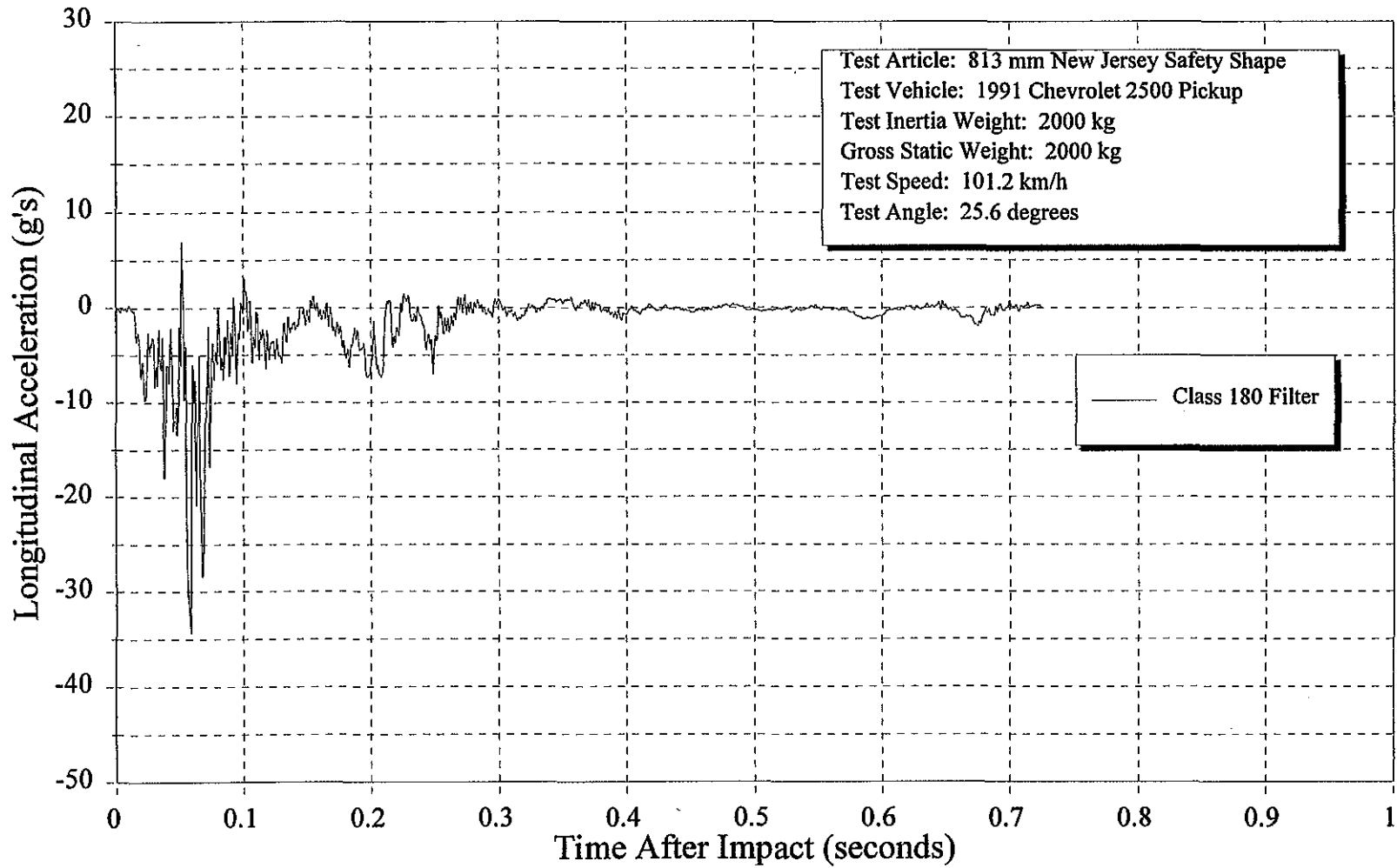
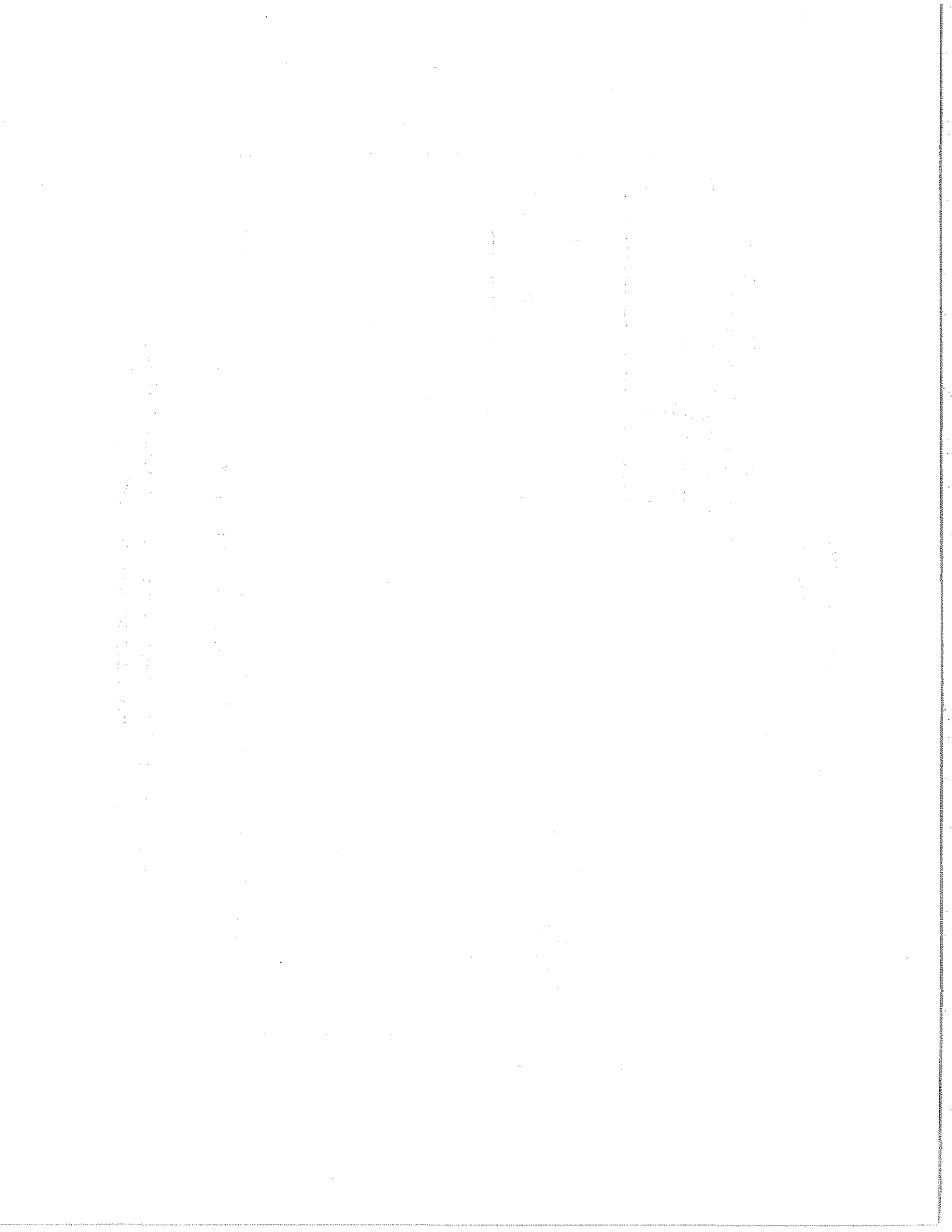


Figure 24. Vehicle longitudinal accelerometer trace for test 405491-1.
(accelerometer at bottom of engine)



IV. SUMMARY OF FINDINGS AND CONCLUSIONS

The New Jersey safety shaped barrier was judged to have met all evaluation criteria set forth in NCHRP Report 350. The barrier successfully contained and redirected the impacting vehicle without the vehicle penetrating or overriding the barrier. Tire marks from the vehicle reached the top of the front edge of the barrier, but did not extend across the top of the barrier. There were no detached elements or debris from the barrier that show potential for penetrating the occupant compartment or to present undue hazard to other traffic or people in the area. Maximum deformation of the occupant compartment was 84 mm at the center front firewall area, but the deformation was judged not to cause serious injuries. The vehicle remained upright and relatively stable during and after the collision period. Maximum roll of the vehicle was 34 degrees away from the barrier, i.e., toward the traffic side. The exit trajectory of the vehicle did not intrude into adjacent traffic lanes with an exit angle of 1.3 degrees. The occupant risk factors were well within the limits set forth by NCHRP 350.

In summary, the New Jersey safety shaped barrier is judged to have met all evaluation criteria set forth in NCHRP Report 350 for test designation 3-11.

Table 2. Assessment of results of test on New Jersey safety shaped barrier.

| Test Agency: Texas Transportation Institute | | Test No.: 405491-1 | Test Date: 09/06/95 |
|--|--|--------------------|---------------------|
| Evaluation Criteria | Test Results | Assessment | |
| Structural Adequacy | | | |
| A. Test article should contain and redirect the vehicle; the vehicle should not penetrate, underide, or override the installation although controlled lateral deflection of the test article is acceptable. | The New Jersey safety shaped barrier contained and redirected the vehicle. The vehicle did not penetrate or override the installation. | Pass | |
| Occupant Risk | | | |
| D. Detached elements, fragments or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone. Deformations of, or intrusions into, the occupant compartment that could cause serious injuries should not be permitted. | There were no detached elements or debris from the barrier to show potential for penetrating the occupant compartment or present undue hazard to others in the area. Maximum deformation into the occupant compartment was 84 mm the center front firewall area, which was judged not to cause serious injury. | Pass | |
| F. The vehicle should remain upright during and after collision although moderate roll, pitching and yawing are acceptable. | The vehicle remained upright and relatively stable throughout the collision and upon exiting the safety shape. Maximum roll attained by the vehicle was 34 degrees. | Pass | |
| Vehicle Trajectory | | | |
| K. After collision it is preferable that the vehicle's trajectory not intrude into adjacent traffic lanes. | The vehicle did not intrude into adjacent traffic lanes. | Pass | |
| L. The occupant impact velocity in the longitudinal direction should not exceed 12 m/s and the occupant ridedown acceleration in the longitudinal direction should not exceed 20 G's. | Longitudinal occupant impact velocity = 5.9 m/s Longitudinal occupant ridedown acceleration = -4.5 g | Pass | |
| M. The exit angle from the test article preferably should be less than 60 percent of test impact angle, measured at time of vehicle loss of contact with test device. | The exit angle at loss of contact with the New Jersey safety shaped barrier was 1.3 degrees which was less than 60 percent of the impact angle. | Pass | |

REFERENCES

1. H. E. Ross, Jr., D. L. Sicking, R. A. Zimmer, and J. D. Michie, "Recommended Procedures for the Safety Performance Evaluation of Highway Features," NCHRP Report 350, Transportation Research Board, Washington, DC, 1993.
2. J. D. Michie, "Recommended Procedures for the Safety Performance Evaluation of Highway Appurtenances," NCHRP Report 230, Transportation Research Board, Washington, DC, 1980.

1911

1. The first part of the report deals with the general situation of the country and the progress of the work during the year.

2. The second part of the report deals with the results of the work during the year and the progress of the work during the year.