# COMPUTER MODELING AND SIMULATION OF NEW JERSEY SIGNALIZED HIGHWAYS 

(VOLUME I- OPTIMIZATION)

FINAL REPORT

June 2005

Submitted by
Steven I-Jy Chien, PhD.
Principal Investigator, Associate Professor
New Jersey Institute of Technology
Interdisciplinary Program in Transportation
George Fallat, P.E.
Deputy Director
New Jersey Institute of Technology
National Center for Transportation and Industrial Productivity


NJDOT Research Project Manager Karl Brodtman

In cooperation with
New Jersey
Department of Transportation
Division of Research and Technology and
U.S. Department of Transportation Federal Highway Administration

## DISCLAMER STATEMENT

"The contents of this report reflect the views of the author(s) who is (are) responsible for the facts and the accuracy of the data presented herein. The contents do not necessarily reflect the official views or policies of the New Jersey Department of Transportation or the Federal Highway
Administration. This report does not constitute a standard, specification, or regulation. "

| 1. Report No. | R. Recipient's Catalog No. |
| :--- | :--- | :--- |
| FHWA-NJ-2005-008 |  |

Form DOT F 1700.7 (8-69)

## Acknowledgements

We wish to express our sincere thanks to the New Jersey Department of Transportation for their dedication to this project. We especially would like to thank Mike Asson, the project customer and Karl Brodtman, the Project Manager. We would also like to thank the following the following persons from NJDOT who provided excellent technical insight to the project: Scott Oplinger, Dave Martin, Pete Amin, and Wayne Mathis. Finally, we would like to thank several students who assisted us in this project, especially, Jiangtao Luo, Xiabo Liu, Saroj Joshi, and Kitae Kim.

## TABLE OF CONTENTS

Page
SUMMARY ..... 1
INTRODUCTION ..... 4
LITERATURE REVIEW ..... 6
RESEARCH APPROACH ..... 7
FINDINGS ..... 22
CONCLUSIONS ..... 32
REFERENCES ..... 33
APPENDIX A: LITERATURE REVIEW ..... 37
APPENDIX B: STUDY CORRIDOR INTERSECTION FIGURES ..... 55
APPENDIX C: ROUTE 23 TIMING DIRECTIVES ..... 91
APPENDIX D: ROUTE 42/322 TIMING DIRECTIVES ..... 114
APPENDIX E: SYNCHRO MOE RESULTS TABLES ..... 137

## LIST OF FIGURES

Page
Figure 1. Configuration of Research Approach ..... 8
Figure 2. Route 23 Corridor ..... 9
Figure 3. Route 42/322 Corridor ..... 9
Figure 4. Balanced Volume (Scenario 1) ..... 15
Figure 5. Balanced Volume (Scenario 2) ..... 16
Figure 6. Procedure for Generating Signal Timing Directives ..... 21
Figure A-1. Flow-Density Relationship ..... 38
LIST OF TABLES
Table 1. Data Collected for Route 23 ..... 11
Table 2. Data Collected for Route 42/322 ..... 12
Table 3. MOEs Comparison of Route 23 ..... 23
Table 4. MOEs Comparison of Route 42/322 ..... 24
Table 5. Existing vs. Optimal Signal Timing on Route 23 ..... 28
Table 6. Existing vs. Optimal Signal Timing on Route 42/322 ..... 29

## SUMMARY

The New Jersey Department of Transportation has undertaken an initiative to systematically improve traffic operations along the state's signalized highway corridors. Two corridors in this study, NJ Route 23 and NJ Route 42/322 were selected as studied arterials for undertaking a systematic approach to observe current traffic conditions, obtain current traffic volume data and then assimilate this information as well as existing roadway geometric characteristics into a traffic signal optimization software. The results of these efforts would produce new timing directives that could be readily implemented. Expanding such initiatives to New Jersey's signalized arterials has the potential of reducing congestion and improving air quality.

As a follow up to this study, a cost benefit analysis is being conducted to better evaluate the savings (or losses) experienced through comparing selected measures of effectiveness before and after implementing optimized timing plans. The results of the cost benefit analysis could then provide justification for receiving future funding update traffic signal timing plans for New Jersey's signalized corridors.

The studied section of the Route 23 corridor consists of 19 signalized intersections and is a total length of 12 miles. The study section is physically divided with no provisions for direct left turns from the mainline. Therefore, the timing/phasing plans do not include separate phasing to accommodate direct left turns from the mainline. The Route $42 / 322$ study section is approximately 9 -miles long and includes Route 42 from MP 0.0 and ending at MP 6.17 and Route 322 from MP 24.71 to MP 26.87. The study section consists of 17 signalized intersections, many of which, provide signal phasing for direct left turn movements were permitted.

For the two study corridors, several steps were undertaken to develop the final version of traffic signal timing directives containing optimal timing settings. The first step included an extensive data collection effort for which the following information was obtained:

- Existing roadway geometric features, including number and designation of lanes, lane widths and presence of shoulders;
- Distance between intersections;
- Traffic counts, turning movement, and truck percentages; and
- Existing signal timing plans.

The project team also conducted field observations of traffic flow patterns and identified locations where large traffic generators exist.

The next step consisted of "balancing" traffic volumes between adjacent intersections, so that the total traffic volume exiting on the main street was equal to the total traffic on the main street approach. Where there were potentially large uncounted traffic generators (e.g. unsignalized intersections, driveways from large retail facilities) between two intersections, network flows were not balanced. The adjusted flows as well as geometric data were then used as the input for modeling Synchro networks. Existing splits and offsets were entered into the Synchro models, and then the traffic simulation during morning, noon and evening peak periods can be performed and the results were tabulated.

The Synchro software is capable of optimizing green times for all intersection approaches and overall green time progression on a selected section. The software also enables the user to optimize the intersection phasing sequence to maximize traffic signal progression along the corridor. The user can also specify a set phasing scenario or allow Synchro to generate an optimal phasing plan. With direct left turns permitted along the Route 42/322 corridor, there is opportunity to employ innovative phasing alternatives, such as lagging left turn phases and different phasing options for different times of day. However, it was requested that the current phasing be retained and that it remain consistent throughout the day with only optimized splits and offsets. In addition, Timing modifications also considered the limitation of existing traffic signal equipment.

The following periods were examined for optimizing existing traffic signal timing plans at the two studied corridors:

Route 23

- Weekday morning peak hours (From 5:30 A.M. to 9:00 A.M.)
- Weekday noon peak hours (From 11:00 A.M to 1:00 P.M.)
- Weekday evening peak hours (From 3:00 P.M. to 7:30 P.M.)

Route 42/322

- Weekday morning peak hours (From 6:00 A.M. to 10:00 A.M)
- Weekday noon peak hours (From 10:00 A.M. to 3:00 P.M) and Weekend (From 8:00 A.M. to 6:00 P.M.)
- Weekday evening peak hours (From 3:00 P.M. to 7:00 P.M.)
- Weekday off-peak hours (All other time periods)

Since turning movement data was not available for off-peak hours, it was assumed that the current timing in place for off-peak hours would be retained. In addition, the revised timing plans also had to accommodate potential pedestrian crossing volumes, although few, pedestrians were observed during peak periods.

The results of this study include the optimal timing plans and the development of new timing directives for both studied sections on Route 23 and Route 42/322. The directives are produced in a format such that they can be readily understood by field maintenance personnel and can be easily updated in the future. The revised timing directives were also reviewed and approved by NJDOT's Bureau of Traffic Engineering and Safety Programs to ensure that they comply with NJDOT standards and format.

Initial results of our analysis indicate that significant improvements in Level of Service (LOS) could be achieved by simply retiming the traffic signals. For example, on Route $42 / 322$, average vehicle delays were reduced by over half at one intersection during the morning peak hour, resulting in a LOS improvement from C to B. Arterial travel speeds and improved progression, overall, also improved.

A programmatic approach for optimizing signalized state highway corridors, however, would require a consistent funding source for collecting the up-to-date traffic volume data, entering and manipulating this information into a computer model, developing traffic signal timing directives and then implementing these changes in the field.

Therefore, as a follow up to this report, a study will be conducted to quantify the full extent of implementation costs and benefits associated with optimized traffic signal timing plans for each corridor.

## INTRODUCTION

Various costly ITS technologies are considered for deployment along ITS freeways, arterials and streets operated by the New Jersey Department of Transportation (NJDOT). In the area of traffic control, these technologies include an optimal array of signal cycle lengths, splits, and offsets while considering dynamic traffic conditions. In taking advantage of these technologies, however, there is a need for traffic engineers to develop computer models for signalized highways, optimize the array of decision variables, evaluate optimized timing plans, and determine the level of service prior to actual implementation and operation at the study site. Traffic engineers must also monitor and update implemented timing plans in response to time variant traffic conditions.

The development of a method for integrating simulation/optimization models to optimize traffic control for New Jersey highways was primarily motivated by the following factors:

1. NJDOT needs a better method to develop, implement and update traffic signal timing plans for roadway networks of connected and non-connected intersections.
2. Existing traffic simulation models require extensive data collection and substantial efforts to develop and are not responsive to dynamic patterns of traffic flow. Furthermore, development of traffic signal timing plans, the means to implement the results of these models, has not been integrated into the output of the models.
3. The application of simulation/optimization models can advance the state of the art in research and development of advanced traffic control systems, and can enhance the state of the practice in their implementation.

Computerized simulation and optimization models (e.g., SimTraffic and Synchro) can be employed to evaluate the performance of traffic control systems. These models allow experimentation with "what-if" scenarios and evaluation of technologies and systems impacts before they are actually deployed. However, due to the dynamic nature of traffic conditions, the output of these models is not effective in responding
to changing traffic conditions. Furthermore, considerable resources are required to collect traffic data, develop simulation and optimization models, and then implement the solutions recommended by these models. In addition to providing excellent learning opportunities for students, the New Jersey Institute of Technology Traffic Simulation Laboratory (NJIT-TSL) is an ideal candidate for collecting the necessary data, developing models for non-connected and connected intersections on the selected networks and optimizing signal cycle lengths, timings, and offsets.

The NJIT-TSL was engaged in collecting data, evaluating traffic control systems, developing simulation/optimization models and producing the documentation necessary for field implementation

The NJIT-TSL, consisting of experienced/trained research members and a number of personal computers supported by the Interdisciplinary Program in Transportation at NJIT, has achieved the following objectives:

1. Identify and collect necessary data for developing signal optimization and traffic simulation models;
2. Develop Synchro models to optimize signal cycle lengths, splits, and offsets for selected non-connected or connected signalized intersections;
3. Assist NJDOT traffic engineers in implementing the results on the selected roadway sections, until the signalized roadway(s) and sections have been optimized;
4. Prepare traffic signal directives in accordance with NJDOT's format so that NJDOT field personnel can easily implement the model output results.

## LITERATURE REVIEW

The existence of the signal control system greatly affects the traffic movements over space and time and contributes the primary delay and other measures of effectiveness (MOEs) on the traffic stream in a signalized transportation network. NJDOT needs a better method to optimize traffic signal timing plans for roadways with connected and non-connected intersections. Existing traffic simulation models require extensive data collection and substantial efforts to develop, and some of them are not responsive to dynamic patterns of traffic flow. Furthermore, development of traffic signal timing plans, the means to implement the results of these models, has not been integrated into the output of the models. The application of traffic simulation and signal optimization models can advance the state-of-the-art traffic control systems, and can enhance the state-of-the-practice in their implementation. Therefore, it is necessary to research the application of simulation/optimization models and develop an integrated method for optimizing signalized traffic control on New Jersey highways.

The complete literature review of signal optimization and traffic simulation models are discussed and shown in Appendix E.

## RESEARCH APPROACH

This section of the report discusses the research approach, which includes tasks for developing optimal signal timing plan for Route 23 and Route 42/322 corridors. While each corridor is unique in terms of its traffic volume patterns and roadway characteristics, similar research methodologies were applied to build the simulation networks and optimize traffic signal progression. The tasks included in the research approach are listed below, and itemized tasks are illustrated in Figure 1.

- Task 1. Site Identification and Data Needs.
- Task 2. Data Collection.
- Task 3. Network Modeling with Synchro and SimTraffic.
- Task 4. Optimization of Signal Timing Plan with Synchro and SimTraffic.
- Task 5. Generation of Timing Directives.


## Sections of Studied Corridors

The sections of Route 23 (located in the northern portion of the state) and Route $42 / 322$ (in the southern half of the state) were identified by NJDOT as the two studied corridors in this project. Route 23 runs primarily north-south and is a heavy commuter route for motorists accessing Interstate 80 from residential areas in suburban Morris County. Route 42/322 runs primarily east-west and provides access between Interstate 295 and residential areas in Camden, Gloucester and Atlantic Counties. The Route 42/322 corridor is also a major route to Atlantic City and other summer recreational communities along the Jersey shore. Both Route 23 and Route 42/322 are considered major urban signalized arterials and provide atgrade access to cross streets, adjacent commercial development, and surrounding residential areas. Pedestrian activity was observed to be minimal along both corridors, with vehicle usage consisting largely of single occupant passenger cars.

The studied section of Route 23 is approximately 12-mile long with 19 signalized intersections and extends from milepost (MP) 14.98 to MP 27.30. The geographic location of the study site is mapped and shown in Figure 2.

*: Detailed Procedure is illustrated in Figure 6.

Figure 1. Configuration of Research Approach


Figure 2. Route 23 Corridor
The Route $42 / 322$ study corridor includes Route 42 from MP 0.0 to MP 6.17and Route 322 from MP 24.71 to MP 26.87. The Route 42/322 section includes 17 signalized intersections and totals approximately 9 miles. The configuration of the studied site is shown in Figure 3.


Figure 3. Route 42/322 Corridor

## Data Identification

Data identification was divided into two sections of studied corridors (Route 23 and Route 42/322) to provide a clear understanding at each site. Each section will be deployed as guided in Figure 1.

## Data Collection

An important aspect of this study is to develop optimal signal timing plans using accurate, up-to-date information. NJDOT, under its on-going traffic counting program, provided existing intersection turning movement and volume counts for the studied Route 23 corridor. For both studied corridors, NJDOT provided intersection plans, signal timing directives, and straight line diagrams. Geometric data included the following information:

- Number of lanes
- Lane width and length
- Intersection location and layout
- Spacing between intersections.

NJDOT provided current turning movement data for the studied Route 23 corridor for weekday morning and evening peak periods. Current traffic data for the Route 42/322 corridor was not readily available. Therefore, NJIT solicited proposals and selected a consultant, Louis Berger and Associates, to obtain up-to-date turning movement and traffic volume counts at signalized locations along the Route 42/322 corridor. The consultant also provided 24-hour Automatic Traffic Recorder (ATR) counts at selected locations. This data provided insight as to the general traffic patterns during both peak and non-peak traffic periods. In addition to traffic volume data, the consultant provided sketches, depicting the number and configuration of lanes, for each signalized intersection. Turning movement data for the corridor was obtained for weekday morning, evening and Noon peak periods. The collected data for intersections for Route 42/322 is summarized in Table 2.

Table 1. List of Data Collected for Route 23 (19 Signalized Intersections)

| No. | MP | Intersection | Count | Plan | Signal | Timing | Note * | Figure** |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 27.32 | Lake Stockholm Rd.(SB) |  |  |  |  | T, 2220 |  |
| 1 | 26.9 | Vernon Stockholm Rd.(Rt.515) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | 5650 | B-1 |
| 2 | 25.83 | Canister Rd. | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | 6810 | B-2 |
| 3 | 24.54 | Reservior Rd. | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | 2060 | B-3 |
| 4 | 24.15 | Doremus | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | 4700 | B-4 |
| 5 | 23.26 | Paradise Rd. | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | 1265 | B-5 |
|  | 23.02 | Allson Ave. (NB) |  |  |  |  | T, 845 |  |
| 6 | 22.86 | Oak Ridge Rd. | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | 1110 | B-6 |
| 7 | 22.65 | Clinton Rd. | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | 2375 | B-7 |
| 8 | 22.2 | Larue Rd. (NB) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | B-8 |
| 9 | 22.2 | Larue Rd. (SB) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | 685 | B-9 |
|  | 22.07 | Green Rd. (Rt.513) (SB) |  |  |  |  | T, 1055 |  |
|  | 21.87 | Union Valley Rd. (Rt.513) (NB) |  |  |  |  | T, 740 |  |
| 10 | 21.73 | Kanhouse (Old Rt. 23) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | 2325 | B-10 |
|  | 21.29 | (Connect Old Rt.23) (NB) |  |  |  |  | T, 4435 |  |
| 11 | 20.45 | Echo Lake Rd. | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | 9345 | B-11 |
|  | 18.68 | Unnamed Rd.(NB) |  |  |  |  | T, 2270 |  |
|  | 18.25 | Germantown Rd.(SB) |  |  |  |  | T, 210 |  |
|  | 18.21 | Germantown Rd.(NB) |  |  |  |  | T, 5225 |  |
|  | 17.22 | High Crest Rd. (NB) |  |  |  |  | T, 3960 |  |
| 12 | 16.47 | Center Court | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | 2320 | B-12 |
| 13 | N/A | Kiel Ave. \&Ramp CC | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | B-13 |
| 14 | 16.03 | Kinnelon Rd. (Rt.618) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | 1585 | B-14 |
| 15 | N/A | Kakeout Connector \& Kinnelon Rd. | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | B-15 |
|  | 15.73 | Hillcrest Ave.(NB) |  |  |  |  | T, 790 |  |
|  | 15.58 | Valley Rd.(NB) |  |  |  |  | T, 790 |  |
|  | 15.43 | Roosevelt Ave.(NB) |  |  |  |  | T, 580 |  |
| 16 | 15.32 | Cascade Way | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | 1635 | B-16 |
| 17 | 15.01 | Boonton Ave. | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | 530 | B-17 |
|  | 14.91 | Bartholdi Ave. |  |  |  |  | 1480 |  |
| 18 | 14.63 | Morse Ave. | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | 1635 | B-18 |
|  | 14.32 | Mathews Ave. |  |  |  |  | T,1160 |  |
|  | 14.1 | Drive Way (NB) |  |  |  |  | T, 530 |  |
| 19 | 14 | Cotluss Rd. | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | B-19 |
| Total |  | Marked | 19 | 19 | 19 | 19 |  |  |

*: Type T intersection, and the distance (ft) between connected two intersections.
For example, Lake Stockholm intersection is a T intersection, and the distance is 2220 (ft) to Vernon Stockholm intersection.
**: Figure of each intersection is provided in Appendix B.

Table 2. List of Data Collected for Route 42/322 (17 Signalized Intersections)

| No. | MP | Intersection | Count | Plan | Signal | Timing | Note * | Figure |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 6.17 | Shopping Center Dr. | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | 1375 | B-20 |
|  | 5.91 | Unnamed Rd. 1 |  |  |  |  | T, 530 |  |
| 2 | 5.81 | Greentree Rd. | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | 160 | B-21 |
|  | 5.78 | Irvin Ave.(NB) |  |  |  |  | T, 580 |  |
| 3 | 5.67 | Whitman Dr. | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | 1595 | B-22 |
|  | N/A | Unnamed Rd.2(NB) |  |  |  |  | T, 360 |  |
| 4 | 5.3 | Gantown Rd. | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | 195 | B-23 |
|  | N/A | Unnamed Rd. 3 (NB) |  |  |  |  | T, 595 |  |
|  | 5.15 | W Garfield Ave.-Garfield Ave. |  |  |  |  | 265 |  |
| 5 | 5.1 | Johnson Rd.(NB) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | T, 475 | B-24 |
|  | 5.01 | Mckinley Ave.(SB) |  |  |  |  | T, 475 |  |
| 6 | 4.92 | Fries Mill Rd.(SB) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | T, 1375 | B-25 |
|  | 4.66 | Unnamed Rd. 4 (SB) |  |  |  |  | T, 1320 |  |
|  | 4.41 | Leddon Ln.(NB) |  |  |  |  | T, 900 |  |
|  | 4.24 | Medison Ave. |  |  |  |  | 270 |  |
|  | N/A | Unnamed Rd. 5 (SB) |  |  |  |  | T, 1420 |  |
| 7 | 3.92 | Watson Dr. | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | 1265 | B-26 |
|  | 3.68 | American Blvd.(SB) |  |  |  |  | T, 550 |  |
|  | N/A | Unnamed Rd. 6 (SB) |  |  |  |  | T, 350 |  |
| 8 | 3.51 | Tuckahoe Rd.-Stagecoach Rd. | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | 790 | B-27 |
|  | 3.36 | Ardmore Ave*** |  |  |  |  | 210 |  |
|  | N/A | Unnamed Rd. 7 (SB) |  |  |  |  | T, 160 |  |
|  | 3.29 | Wayne Ave.(SB) |  |  |  |  | T, 315 |  |
|  | 3.23 | Narbeth Ave.(SB) |  |  |  |  | T, 55 |  |
|  | 3.22 | Unnamed Rd. 8 (NB) |  |  |  |  | T, 315 |  |
|  | 3.16 | Woodlawn Ave. (SB) |  |  |  |  | T, 220 |  |
|  | N/A | Unnamed Rd.9(NB) |  |  |  |  | T, 95 |  |
|  | 3.1 | Evergreen Ave.(SB) |  |  |  |  | T, 160 |  |
|  | 3.07 | Fairmount Dr.(NB) |  |  |  |  | T, 210 |  |
|  | 3.03 | Sycamore Ave. (SB) |  |  |  |  | T, 265 |  |
|  | N/A | Twin Hollow Ct. (NB) |  |  |  |  | T, 50 |  |
|  | 2.97 | Strand Ave.(SB) |  |  |  |  | T, 370 |  |
|  | 2.9 | Highland Ave.(SB) |  |  |  |  | T, 315 |  |
|  | 2.84 | Summit Ave.(SB) |  |  |  |  | T, 370 |  |
|  | 2.77 | Laurel Ave.(SB) |  |  |  |  | T, 790 |  |
| 9 | 2.62 | Berlin Cross Keys Rd. | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | 565 | B-28 |
|  | N/A | Unnamed Rd. 10 (NB) |  |  |  |  | T, 555 |  |
|  | N/A | Unnamed Rd. 11 (NB) |  |  |  |  | T, 675 |  |
|  | 2.28 | Prosser Ave. (NB) |  |  |  |  | T, 265 |  |
|  | 2.23 | Unnamed Rd. 12 (SB) |  |  |  |  | T, 740 |  |
| 10 | 2.09 | Kennedy Dr. (SB) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | T, 475 | B-29 |
|  | 2 | Veronica Ln.(NB) |  |  |  |  | T, 1160 |  |
|  | 1.78 | Wildwood Ave.(NB) |  |  |  |  | T, 330 |  |
|  |  | Unnamed Rd. 13 (NB) |  |  |  |  | T, 410 |  |
|  | 1.64 | Dewey Ave.(NB) |  |  |  |  | T, 265 |  |
|  | 1.59 | Crystal Dr.(NB) |  |  |  |  | T, 475 |  |
|  | 1.5 | Laurel Ave.(NB) |  |  |  |  | T, 950 |  |
|  | 1.32 | Kelal Ave.(NB) |  |  |  |  | T, 160 |  |
|  | 1.29 | Grandview Ave.(SB) |  |  |  |  | T, 210 |  |

Table 2. List of Data Collected for Route 42/322 (Continued)

| No. | MP | Intersection | Count | Plan | Signal | Timing | Note * | Figure** |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1.25 | Harrell Ave (SB) |  |  |  |  | 2T, 160 |  |
|  | N/A | Flemming Ln.(NB) |  |  |  |  | T, 370 |  |
|  | 1.15 | ENT to APT (Brookdale Blvd.) (NB) |  |  |  |  | T, 1955 |  |
| 11 | 0.78 | Lake Ave. | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | 880 | B-30 |
|  | N/A | Unnamed Rd. 14 (SB) |  |  |  |  | T, 440 |  |
|  | 0.53 | Maxine Ave.(SB) |  |  |  |  | T, 420 |  |
|  | 0.45 | Marsha Ave. (SB) |  |  |  |  | T, 160 |  |
|  | 0.42 | Pedrick Ave.-Hoffman Ave.(SB, NB) |  |  |  |  | 2T, 530 |  |
|  | 0.32 | Lindele Ave. (SB) |  |  |  |  | T, 160 |  |
|  | 0.29 | May Ave.(NB) |  |  |  |  | T, 160 |  |
|  | 0.26 | Saybrook Ave.(SB) |  |  |  |  | T, 530 |  |
|  | 0.16 | Pine St.1(NB) |  |  |  |  | T, 160 |  |
|  | 0.13 | Pine St. 2 (SB) |  |  |  |  | T, 265 |  |
|  | 0.08 | Broad St.(NB) |  |  |  |  | T, 160 |  |
|  | 0.05 | Willow Ave.(SB) |  |  |  |  | T, 265 |  |
| 12 | 0 | Sicklerville Rd. | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | 475 | B-31 |
|  | N/A | Gordon Ave.(SB, NB) |  |  |  |  | 2T, 315 |  |
|  | N/A | Unnamed Rd. 15 (SB) |  |  |  |  | T, 740 |  |
| 13 | 24.71 | Poplar St.- New Brooklyn Rd. | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | 740 | B-32 |
|  | 24.85 | Washington Ave.(SB, NB) |  |  |  |  | 2T, 790 |  |
|  | 25 | Jefferson Ave.(SB, NB) |  |  |  |  | 2T, 950 |  |
|  | N/A | Hartman Ave.(NB) |  |  |  |  | T, 160 |  |
|  | 25.18 | Walnut St.(SB, NB) |  |  |  |  | 2T, 560 |  |
|  | N/A | James Rd. |  |  |  |  | T, 1760 |  |
|  | N/A | Unnamed Rd. 16 (SB, NB) |  |  |  |  | 2T, 265 |  |
|  | 25.67 | Mellisa Ln. (NB) |  |  |  |  | T, 265 |  |
| 14 | 25.72 | Main St. (Rt.322) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | 2375 | B-33 |
|  | N/A | Dickens Ct. (SB, NB) |  |  |  |  | 2T, 580 |  |
| 15 | 26.28 | Corkery Ln. | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | 580 | B-34 |
|  | 26.39 | Forest Dr.(SB) |  |  |  |  | T, 1265 |  |
|  | 26.63 | Karen Dr.(SB) |  |  |  |  | T, 580 |  |
|  | 26.74 | Concord Dr.(NB) |  |  |  |  | T, 685 |  |
|  | N/A | Unnamed Rd. 17 (SB) |  |  |  |  | T, 325 |  |
| 16 | 26.87 | Malaga Rd. | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | 375 | B-35 |
|  | N/A | Unnamed Rd. 18 (NB) |  |  |  |  | T, 220 |  |
|  | N/A | Luther Ave. (NB) |  |  |  |  | T, 750 |  |
|  | N/A | Luther (SB) |  |  |  |  | T, 650 |  |
|  | N/A | Luther Ave. (SB,NB) |  |  |  |  | 2T, 1110 |  |
|  | N/A | Unnamed Rd. 19 (SB) |  |  |  |  | T, 1000 |  |
|  | N/A | Unnamed Rd. 20 (NB) |  |  |  |  | T, 325 |  |
|  | 27.69 | Battles Rd.(NB) |  |  |  |  | T, 265 |  |
|  | 27.74 | Theresa Ln.(NB) |  |  |  |  | T, 100 |  |
|  | N/A | Unnamed Rd. 21 (SB) |  |  |  |  | T, 610 |  |
|  | N/A | Unnamed Rd. 22 (NB) |  |  |  |  | T, 1525 |  |
|  | N/A | Unnamed Rd. 23 (SB, NB) |  |  |  |  | 2T, 265 |  |
| 17 | 28.2 | White Hall Rd.-Corkery Ln. | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | 220 | B-36 |
|  |  | Unnamed Rd. 24 (NB) |  |  |  |  |  |  |
| Total |  | Marked | 17 | 17 | 17 | 17 |  |  |

*: Type T intersection, and the distance (ft) between connected two intersections.
**: Figure of intersection is provided in Appendix B.
***: Included in Synchro files.
These data were subsequently configured, entered into Synchro and ultimately used to develop revised traffic timing directives.

Manual traffic counts were broken into 15-minute groups and included individual turning movement volumes and vehicle classifications. Some limited speed information was also collected. NJDOT provided signal timing data in the form of the existing timing directives in Microsoft Excel format. These directives include information such as cycle lengths, signal phases, splits, and offsets. The collected data for Route 23 are summarized in Table 1. Collected data for Route 42/322 are shown in Table 2.

In addition to traffic volume and roadway geometric data, the project team has conducted several site visits to verify the intersection layouts, roadway geometry, posted speed limits, and traffic operational conditions. Locations at which turning movement data were not collected and are significant trip generators (e.g., shopping centers, driveways, or street intersections), were noted for the determination of "break points". Break points are locations at which the total exiting traffic flow from the downstream location does not equal to the total entering flow from its upstream intersection.

## Network Modeling

The collected data were applied for establishing Synchro networks. Based on the data collected, traffic simulation models were developed by importing the developed Synchro networks into SimTraffic for morning, evening and noon peak periods for both study corridors.

While the time and durations of peak periods are consistent for both study corridors, peak traffic volumes at intersections do not occur at the same time interval. Therefore, it was necessary to adjust the volumes and balance the flows. The total volume leaving an intersection was thus equal to the total volume entering its downstream intersection. For any non-signalized intersection, the peak hour volumes should be determined based on land usage, such as residential, retail, or office spaces, etc.

For signalized intersections, the difference between volumes at two adjacent signalized intersections was adjusted based on one of two scenarios.

In the first scenario, at least one non-signalized intersection is between two signalized intersections. Volume differences between the two signalized intersections were then assigned to the unsignalized intersections based on the percentages of turning movements. For example, in Figure 4, Route 23 Southbound (SB) traffic volume (3832 vph) entering Morse intersection was increased from 3832 to 4130 vph to be balanced with the maximum peak volume at the adjacent upstream signalized intersection. The increased volume ( 298 vph ) has been added into traffic volume exiting Morse intersection hence the exiting traffic volume will be increased from 4082 to 4380 for the next downstream signalized intersection.

In the second scenario, there is no access point between two signalized intersections. The volume difference was based on fixing the critical signal intersection whose volume remains unchanged, while the volume at the other intersection can be adjusted.


Figure 4. Balanced Volume (Scenario 1)
In Figure 5, Route 23 Northbound (NB) volume (406 vph) at Paradise intersection was increased to 507 vph to be balanced with the identified maximum peak volume
in network. Since NB traffic volume (405 vph) exiting Paradise intersection and NB traffic volume (479 vph) entering Doremus intersection were not consistent, the volume in the link between Paradise and Doremus intersection was changed to 487 vph to be balanced with the volume ( 507 vph ) entering Paradise intersection. SB volumes were also balanced in the same manner.

The purpose of the two volume balancing scenarios was intended to consider the worse case (e.g., maximum peak volume) during each peak period at the studied location. When optimizing splits, Synchro attempts to provide enough green time to serve the $90^{\text {th }}$ percentile lane group flow. If there is not enough cycle time to meet this objective, Synchro will attempts to serve the $70^{\text {th }}$ percentile traffic and then the $50^{\text {th }}$ percentile traffic. Any extra time is given to the main street phases.


Figure 5. Balanced Volume (Scenario 2)
The next step of network modeling is inputting data into Synchro. In addition to adjusting volumes and peak hour factors, existing signal timing plan information including cycle lengths, phases, splits, yellow times, all red times, offsets, vehicle extensions, controller type, etc. were entered into Synchro for morning, noon, and evening peak periods. In order to compare the output of developed Synchro models with field conditions, the SimTraffic Models were converted from the Synchro
models. Both the Synchro and SimTraffic files were reviewed and approved by NJDOT. Some adjustments were made to better reflect actual field conditions. For example, the model conditions did not reflect actual field conditions at the intersection of Route 23 and Oak Ridge Road. During a PM field visit, it was found that the queues at different jug handles would develop on the right hand shoulder in the two lane section of Route 23. In order to correct for this situation, the model was modified by adding a $3^{\text {rd }}$ lane to the northbound section of the road with NJDOT's approval.

## Model Calibration and Validation

Synchro and SimTraffic contain many parameters that describe traffic control operation, traffic flow characteristics, and driver behavior. Although these models provide default values for each variable, great attention should be paid to calibration so that the model accurately represents local conditions. Calibration is an iterative process in which the engineer adjusts the simulation model parameters until the results produced by the simulator match field measurements. The calibrated parameters in Synchro and SimTraffic are listed below:

- Lost Time
- Lane Utilization Factor
- Right (Left) Turn Factor
- Right (Left) Pedestrian Factor
- Heavy Vehicle Factor
- Headway Factor
- Right (Left) Turning Speed

Synchro and SimTraffic generally yielded un-calibrated results that most closely reflected observed field conditions. Particularly, SimTraffic provides queue calculations in terms of feet rather than number of vehicles. This was felt to provide more accurate queue estimates and required less computation time for the user. Nonetheless, Synchro and SimTraffic networks required fine tuning. The adjustment made in Synchro was the lost time factors as 2 seconds, 4 seconds, and 3 seconds for AM, NOON, and PM period, respectively in order to consider difference of driver's behavior in each time period. Right turn speed factor was also adjusted slightly to
achieve better results. It was felt that the default right turning speed ( 15 mph ) was too slow for the most congested segments, resulting in many vehicles blocking traffic while waiting to make right turn.

## Signal Optimization

The research team used Synchro to optimize signal timing plans for both studied sections on Route 23 and Route 42/322. The following optimization stages were considered to be performed:

1. Optimize offsets (low impact)
2. Optimize offsets and cycle lengths (low-medium impact)
3. Optimize Signal Phase, offsets and cycle lengths (medium-high impact)
4. Suggest possible geometric changes and optimize Signal Phase, offsets and cycle lengths (high impact)

Fourth stage optimization was not considered for this research project.

The different tools of Synchro were used in the following steps to perform the optimization:

- Network Partitioning
- Signal Phase and Cycle Length Optimization
- Offset Optimization

Network partitioning allows a studied street network to be coordinated by different zones and cycle lengths, while timing plans within each zone are allowed to be tailored to fit local conditions. The process of network partitioning begins by dividing the full network into smaller networks or zones. Each intersection is then assigned to a specific zone. Partitioning a network into multiple zones is recommended under the following conditions:

- Large distances geographically separate the studied network into several subnetworks;
- The studied network contains different traffic characteristics within various locations or zones. For example, the signals at CBD may use two phase
signals with short cycle lengths, while the ones in suburban areas may applying eight phase signals with long cycle lengths; and
- It is possible to use shorter cycle lengths in some areas and longer cycle lengths in the more congested areas
Two reasons to use one zone optimization instead of multi-zone optimization:
- Controller hardware is not able to support multiple zones, and
- All intersections are close to each other (e.g., less than 500 ft )

According to the criteria listed above Route 23 was partitioned into three zones:

- Cotluss Road to Center Court Road (2.4 Miles, 8 Intersections)
- Echo Lake Road to Larue Road (1.7 Miles, 4 Intersections)
- Clinton Road to Lake Stockholm Road (4.2 Miles 7 Intersections)

Through the procedures performed in Signal Phase and Cycle Length Optimization, two different cycle lengths for the peak periods of the network were produced. Since the last two zones ( from Echo Lake Road to La Rue Road \& from Clinton Road to Lake Stockholm Road) were given the same optimal cycle lengths, they were combined to form one zone and leave the entire network divided into two zones as currently found on the roadway. With this assumption the offsets could be set to the same master controllers as in the existing timing directives. Once the optimization of the offsets was completed the new timing directives were created.

The Route 42/322 network was partitioned into five different zones by the roads listed as follows:

- Shopping Center Dr. to Fries Mill Rd (1.3 Miles, 6 Intersections)
- Watson Dr. to Tuckahoe Rd (0.4 Miles, 2 Intersections)
- Cross Keys Rd to Kennedy Dr. (0.53 Miles, 2 Intersections)
- Lake Ave to Poplar St. (1.1 Miles, 3 Intersections)
- Main St. to White Hall Rd. (2.5 Miles, 4 Intersections)

The optimum cycle lengths for individual intersections were around 110 seconds, and ranged from 90 seconds to 120 seconds. It was necessary that all of the intersections would function as a coordinated single network. A cycle length of 110
seconds was selected for all of the intersections, with the offsets determined from a single master controller location. A 90-second cycle length was selected for off-peak periods but still with the offsets measured from a single master controller location.

In developing off peak timing plans for Route 42/322, it was decided to compare the volumes obtained from ATR counts with turning movement volumes for the midday period. The midday period was selected as it represents non-commuter conditions, as would be typical during off peak periods. Average and median values were calculated for non-peak hour periods. It was found that the median value was approximately 30 percent of the noon peak hour values. Therefore, the midday peak hour turning movement volumes were adjusted accordingly to reflect average off peak hour conditions. Splits and offset were then calculated for off peak periods using a 90 second cycle length. These outputs were then incorporated into the revised timing directives for Route 42/322.

## Timing Directives

Once the splits and offsets were optimized for the studied corridors, timing directives were prepared in accordance with NJDOT format. Initially, it was believed that the information recommended by Synchro could be directly integrated into an NJDOT format electronic spreadsheet. Due to the complexity of the timing plans, phasing options and other unique elements associated with standard timing directive, converting Synchro output into the timing directives was very labor intensive and not practical to be done. Therefore, the new timing directives for each signalized intersection needs to be developed manually. However, with the revised timing directives now in Excel format, revisions to cycle length, splits and offsets can be easily made. Changes that would result in adding or eliminating signal phases would require entire revamping of the directives.

The recommended timing directives by Synchro were reviewed by NJDOT. The procedure for developing the timing directives is summarized in Figure 6. The final directives for both study corridors Rt 23 and Rt 42/322 are provided in Appendix C and D .


Figure 6. Procedure for Generating Signal Timing Directives

## FINDINGS

Implementing optimized traffic signal timing plans based on the most updated traffic data is a relatively inexpensive way to improve performance at individual intersections as well as corridor-wide. As a follow-up to this research project, the NJIT team is undertaking a cost benefit analysis to quantify costs and benefits associated with the implementation of optimal timing directives

## MOEs

While reductions in delay were not significant at some intersections, the accumulated delay incurred by the volume over the studied time period is considerable. Consider an average delay reduction is merely 5 seconds per each cycle during AM and PM peak hours, the volume of 1000 vph would result in a savings of nearly 24,000 vehicle-hours per year.

Note that the MOEs were not improved or debased at some locations to achieve a greater overall improvement. Thus, the signal timing optimization presented in this study can be further extended into several areas. One aspect is to extend the improvement at these locations, for example, by changing geometric conditions.

The MOEs for the Route 23 corridor are based on optimal signal timings and are summarized in Tables 3-a, 3-b, and 3-c for the peak periods of AM, NOON, and PM, respectively. MOEs for Route 42/322 are summarized in Tables 4-a, 4-b, 4-c, and 4d for the peak periods of AM, NOON, PM, and OFF PEAK, respectively.

The complete MOE tables obtained from Synchro for Route 23 and Route 42/322 are summarized in Appendix E.

Table 3-a. MOEs comparison of Route 23 (AM)

|  | EXISTING |  |  | OPTIMIZED |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Signal Delay (veh-hr) | Average <br> Speed <br> (mph) | Fuel Use (gallons | Signal Delay (veh-hr) | Average <br> Speed <br> (mph) | Fuel Use (gallons ) |
| Vernon Stockholm(Rt.515) | 15 | 7 | 35 | 15 | 8 | 35 |
| Canister Rd. | 40 | 4 | 70 | 35 | 4 | 57 |
| Reservior Rd. | 3 | 30 | 16 | 2 | 33 | 12 |
| Doremus Rd. | 3 | 30 | 22 | 2 | 34 | 12 |
| Paradise Rd. | 6 | 69 | 50 | 4 | 76 | 37 |
| OaK Ridge Rd. | 127 | 13 | 185 | 114 | 13 | 176 |
| Clinton Rd. | 36 | 18 | 77 | 20 | 34 | 54 |
| LaRue Rd. (NB) | 6 | 7 | 12 | 6 | 7 | 12 |
| LaRue Rd. (SB) | 83 | 11 | 164 | 56 | 15 | 137 |
| Kanouse (Old Route23) | 54 | 49 | 109 | 66 | 51 | 120 |
| Echo Lake Rd. | 86 | 6 | 123 | 74 | 9 | 130 |
| Center Court | 3 | 33 | 25 | 2 | 35 | 23 |
| Kinnelon Rd. (Rt. 618) | 18 | 17 | 68 | 5 | 11 | 11 |
| Kiel Ave. \& Ramp CC | 4 | 11 | 10 | 4 | 12 | 9 |
| Kakeout \& Kinnelon Rd. | 6 | 9 | 15 | 17 | 18 | 65 |
| Casecade Way | 31 | 29 | 123 | 10 | 54 | 59 |
| Boonton Ave. | 176 | 5 | 272 | 52 | 13 | 143 |
| Morse Ave. | 86 | 5 | 120 | 101 | 4 | 148 |
| Cotluss Rd. | 25 | 9 | 53 | 63 | 4 | 115 |
| Total | 808 | Avg. 19 | 1,549 | 648 | Avg. 23 | 1,355 |

Table 3-b. MOEs comparison of Route 23 (NOON)

|  | EXISTING |  |  | OPTIMIZED |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Signal Delay (veh-hr) | Average <br> Speed <br> (mph) | Fuel Use (gallons ) | Signal Delay (veh-hr) | Average <br> Speed <br> (mph) | Fuel Use (gallons ) |
| Vernon Stockholm(Rt.515) | 3 | 20 | 13 | 4 | 19 | 14 |
| Canister Rd. | 3 | 23 | 17 | 3 | 25 | 13 |
| Reservior Rd. | 2 | 27 | 10 | 2 | 32 | 8 |
| Doremus Rd. | 1 | 35 | 10 | 1 | 42 | 7 |
| Paradise Rd. | 3 | 79 | 28 | 2 | 88 | 27 |
| OaK Ridge Rd. | 18 | 29 | 48 | 11 | 37 | 38 |
| Clinton Rd. | 6 | 37 | 21 | 4 | 44 | 17 |
| LaRue Rd. (NB) | 2 | 16 | 7 | 3 | 15 | 7 |
| LaRue Rd. (SB) | 1 | 44 | 18 | 2 | 40 | 20 |
| Kanouse (Old Route23) | 5 | 44 | 30 | 2 | 53 | 22 |
| Echo Lake Rd. | 4 | 48 | 15 | 4 | 47 | 17 |
| Center Court | 1 | 39 | 9 | 1 | 39 | 9 |
| Kinnelon Rd. (Rt. 618) | 13 | 14 | 41 | 12 | 15 | 38 |
| Kiel Ave. \& Ramp CC | 3 | 14 | 10 | 3 | 16 | 9 |
| Kakeout \& Kinnelon Rd. | 2 | 21 | 8 | 2 | 21 | 7 |
| Casecade Way | 5 | 63 | 37 | 3 | 75 | 24 |
| Boonton Ave. | 8 | 28 | 41 | 10 | 25 | 55 |
| Morse Ave. | 7 | 33 | 48 | 6 | 36 | 41 |
| Cotluss Rd. | 19 | 9 | 66 | 14 | 11 | 48 |


| Total | 106 | Avg. 33 | 477 | 89 | Avg. 36 | 421 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |

Table 3-c. MOEs comparison of Route 23 (PM)

|  | EXISTING |  |  | OPTIMIZED |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Signal Delay (veh-hr) | Average Speed (mph) | Fuel Use (gallons ) | Signal Delay (veh-hr) | Average Speed (mph) | Fuel Use (gallons ) |
| Vernon Stockholm (Rt.515) | 4 | 20 | 17 | 4 | 22 | 13 |
| Cotluss Rd. | 48 | 6 | 117 | 2 | 33 | 15 |
| Morse Ave. | 12 | 35 | 76 | 4 | 24 | 16 |
| Boonton Ave. | 34 | 16 | 98 | 2 | 32 | 20 |
| Casecade Way | 34 | 35 | 125 | 3 | 84 | 42 |
| Kiel Ave. \& Ramp CC | 41 | 8 | 117 | 24 | 42 | 77 |
| Kinnelon | 11 | 7 | 22 | 62 | 15 | 109 |
| Kakeout \& Kinnelon Rd. | 3 | 18 | 13 | 17 | 10 | 44 |
| Center Court | 5 | 25 | 23 | 1 | 44 | 15 |
| Echo Lake Rd. | 55 | 24 | 105 | 14 | 49 | 87 |
| LaRue Rd. (NB) | 2 | 40 | 18 | 32 | 29 | 78 |
| LaRue Rd. (SB) | 19 | 9 | 45 | 4 | 30 | 20 |
| Clinton Rd. | 74 | 14 | 135 | 32 | 10 | 109 |
| OaK Ridge \& Rt. 23 | 48 | 19 | 107 | 10 | 8 | 22 |
| Paradise Rd.(N) \& Rt. 23 | 5 | 80 | 49 | 3 | 20 | 9 |
| Doremus Rd.\& Rt. 23 | 10 | 15 | 45 | 18 | 53 | 84 |
| Reservior Rd.\& Rt. 23 | 19 | 9 | 58 | 65 | 10 | 144 |
| Canister Rd. \& Rt. 23 | 3 | 32 | 16 | 8 | 39 | 64 |
| Kanouse (Old Route23) | 20 | 42 | 100 | 30 | 9 | 91 |
| Total | 447 | Avg. 24 | 1286 | 335 | Avg. 30 | 1,059 |

Table 4-a. MOEs comparison of Route 42/322 (AM)

| Intersection | EXISTING |  |  | OPTIMIZED |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Signal Delay (veh-hr) | Average Speed (mph) | Fuel Use (gallons ) | Signal Delay (veh-hr) | Average Speed (mph) | Fuel Use (gallons ) |
| Shopping Center Dr. | 7 | 18 | 29 | 6 | 20 | 27 |
| Greentree Rd. | 61 | 4 | 93 | 24 | 9 | 60 |
| Whitman Dr. | 9 | 16 | 28 | 6 | 19 | 23 |
| Gantown Rd. | 40 | 4 | 74 | 12 | 12 | 35 |
| Johnson Rd.(NB) | 10 | 15 | 32 | 9 | 17 | 36 |
| Fries Mill Rd.(SB) | 15 | 11 | 29 | 7 | 20 | 21 |
| Watson Dr. | 14 | 20 | 46 | 9 | 24 | 38 |
| Tuckahoe Rd.-Stagecoach Rd. | 15 | 10 | 35 | 11 | 12 | 32 |
| Berlin Cross Keys Rd. | 15 | 15 | 41 | 14 | 16 | 38 |
| Kennedy Dr. (SB) | 2 | 31 | 11 | 2 | 32 | 9 |
| Lake Ave. | 3 | 35 | 21 | 3 | 34 | 20 |
| Sicklerville Rd. | 38 | 2 | 52 | 16 | 4 | 28 |
| Poplar St.- New Brooklyn Rd. | 10 | 15 | 29 | 7 | 19 | 24 |
| Main St. (Rt.322) | 2 | 21 | 9 | 1 | 25 | 5 |
| Corkery Ln. | 5 | 20 | 19 | 6 | 17 | 20 |
| Malaga Rd. | 3 | 17 | 11 | 4 | 14 | 9 |
| White Hall Rd.-Corkery Ln. | 2 | 14 | 8 | 3 | 11 | 8 |


| Total | 251 | Avg. 16 | 567 | 140 | Avg. 18 | 433 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |

Table 4-b. MOEs comparison of Route 42/322 (NOON)


Table 4-c. MOEs comparison of Route 42/322 (PM)

|  | EXISTING |  |  | OPTIMIZED |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Signal Delay (veh-hr) | Average Speed (mph) | Fuel Use (gallons | Signal Delay (veh-hr) | Average Speed (mph) | Fuel Use (gallons |
| Intersection |  |  | (gal) |  |  | ) |
| Shopping Center Dr. | 25 | 9 | 63 | 19 | 11 | 61 |
| Greentree Rd. | 72 | 5 | 105 | 55 | 6 | 88 |
| Whitman Dr. | 19 | 12 | 49 | 15 | 14 | 45 |
| Gantown Rd. | 82 | 3 | 115 | 43 | 6 | 83 |
| Johnson Rd.(NB) | 22 | 12 | 61 | 14 | 16 | 51 |
| Fries Mill Rd.(SB) | 15 | 16 | 42 | 9 | 21 | 30 |
| Watson Dr. | 23 | 18 | 68 | 13 | 24 | 56 |
| Tuckahoe Rd.-Stagecoach Rd. | 24 | 9 | 50 | 14 | 13 | 35 |
| Berlin Cross Keys Rd. | 35 | 12 | 76 | 28 | 14 | 70 |
| Kennedy Dr. (SB) | 7 | 21 | 30 | 8 | 21 | 28 |
| Lake Ave. | 5 | 29 | 31 | 6 | 28 | 31 |
| Sicklerville Rd. | 47 | 2 | 64 | 23 | 3 | 43 |
| Poplar St.- New Brooklyn Rd. | 12 | 18 | 41 | 11 | 19 | 38 |
| Main St. (Rt.322) | 4 | 15 | 27 | 2 | 24 | 9 |
| Corkery Ln. | 4 | 23 | 20 | 6 | 19 | 22 |
| Malaga Rd. | 3 | 18 | 14 | 5 | 15 | 12 |
| White Hall Rd.-Corkery Ln. | 3 | 14 | 11 | 3 | 13 | 11 |


| Total | 402 | Avg. 14 | 867 | 274 | Avg. 16 | 713 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |

Table 4-d. MOEs comparison of. Route 42/322 (OFF PEAK)

|  | EXISTING |  |  | OPTIMIZED |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Signal Delay (veh-hr) | Average Speed (mph) | Fuel Use (gallons | Signal Delay (veh-hr) | Average Speed (mph) | Fuel Use (gallons |
| Intersection |  |  | ) |  |  | ) |
| Shopping Center Dr. | 11 | 14 | 39 | 2 | 23 | 8 |
| Greentree Rd. | 55 | 5 | 80 | 3 | 18 | 12 |
| Whitman Dr. | 13 | 14 | 40 | 2 | 20 | 9 |
| Gantown Rd. | 33 | 6 | 68 | 4 | 12 | 14 |
| Johnson Rd.(NB) | 46 | 6 | 94 | 3 | 21 | 13 |
| Fries Mill Rd.(SB) | 13 | 19 | 41 | 3 | 25 | 11 |
| Watson Dr. | 13 | 26 | 61 | 2 | 32 | 14 |
| Tuckahoe Rd.-Stagecoach Rd. | 24 | 10 | 53 | 4 | 16 | 13 |
| Berlin Cross Keys Rd. | 19 | 15 | 54 | 4 | 19 | 15 |
| Kennedy Dr. (SB) | 3 | 29 | 20 | 1 | 34 | 5 |
| Lake Ave. | 4 | 34 | 31 | 1 | 38 | 8 |
| Sicklerville Rd. | 18 | 3 | 33 | 3 | 5 | 7 |
| Poplar St.- New Brooklyn Rd. | 12 | 15 | 35 | 2 | 21 | 8 |
| Main St. (Rt.322) | 2 | 22 | 9 | 0 | 24 | 2 |
| Corkery Ln. | 3 | 24 | 15 | 1 | 24 | 4 |
| Malaga Rd. | 2 | 22 | 7 | 1 | 21 | 2 |
| White Hall Rd.-Corkery Ln. | 1 | 19 | 5 | 0 | 18 | 2 |
| Total | 272 | Avg. 17 | 685 | 36 | Avg. 22 | 147 |

## Signal Optimization

Further investigation is needed on network partition and a procedure that allows a network with multiple zones and cycle lengths. When a large signalized network exists, breaking it into smaller networks becomes necessary. Thus, a guideline for partitioning a large scale network to manage queue if any on boundary of adjacent subnetworks should be developed.

The related optimal signal timing information such as controller types, cycle lengths, and offsets is summarized in Tables 5-a, 5-b, and 5-c for the peak periods of AM, NOON, and PM, respectively. Tables $5-a, 5-b$, and $5-\mathrm{c}$ show that there are two cycle lengths in AM (e.g., 160 sec and 150 sec ) and PM (e.g., 140 sec and 150 sec ) periods and one cycle length in NOON (e.g., 90 sec ) period. As discussed above, Route 23 was partitioned into three zones. These zones denominated were as zone $B$, zone $F$, and zone $G$ in Synchro.

- Zone B ( from Cotluss Road to Center Court Road)
- Zone F (from Echo Lake Road to Larue Road)
- Zone G (from Clinton Road to Lake Stockholm Road).

However, zone $F$ and zone $G$ were given the same cycle lengths. Thus, intersection of Route 23 and Echo Lake Road were selected as a reference point for zone F and Zone G, and intersection at Boonton Avenue was identified as a reference point for zone B .

Optimal signal timing plan of Route 42/322 was produced in four time periods (e.g., AM, NOON, PM, and OFFPEAK) with NJDOT's approval. Once splits and offsets were optimized, intersection of Route 42 and Shopping Center Drive was selected as a reference point of optimal signal timing plan. The related optimal signal timing information such as controller types, cycle lengths, and offsets is summarized in Tables 6-a, 6-b, 6-c, and 6-d for the peak period of AM, NOON, PM, and OFF PEAK, respectively.

## Timing Directives

Another important result is the establishment of a process whereby traffic volume data can be updated and timing directives can be easily modified. While this process was initially thought to be well suited for automatic data transfer, this was shown not to be the case. Due to the complexity of the timing directives and the current desire to maintain the directives in a MS Word format, it was necessary to manually enter the green, red, yellow and all red times. However, now that the timing plans have been developed, they would be relatively easy to update in the future.

Table 5-a. Existing vs. Optimal Signal Timing of Route 23 (AM)

|  | Existing |  |  | Optimized |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
|  | Controller <br> Type | Cycle <br> Length <br> $(\mathrm{sec})$ | Offset <br> $(\mathrm{sec})$ | Controller <br> Type | Cycle <br> Length <br> $(\mathrm{sec})$ | Offset <br> $(\mathrm{sec})$ |
| Intersection | AC | 160 | 108 | AC | 160 | 81 |
| Vernon Stockholm Rd.(Rt.515) | AC | 160 | 42 | AC | 160 | 122 |
| Canister Rd. | AC | 160 | 126 | AC | 160 | 24 |
| Reservior Rd. | AC | 160 | 2 | AC | 160 | 75 |
| Doremus | AC | 160 | 85 | AC | 160 | 138 |
| Paradise Rd. | AC | 160 | 117 | AC | 160 | 135 |
| Oak Ridge Rd. | AC | 160 | 151 | AC | 160 | 110 |
| Clinton Rd. | AC | 160 | 43 | AC | 160 | 129 |
| Larue Rd. (NB) | AC | 160 | 43 | AC | 160 | 129 |
| Larue Rd. (SB) | AC | 160 | 80 | AC | 160 | 73 |
| Kanhouse (Old Rt. 23) | AC | 160 | 0 | AC | 160 | 0 |
| Echo Lake Rd. | AC | 150 | 49 | AC | 150 | 92 |
| Center Court | AC | 150 | 58 | AC | 150 | 112 |
| Kiel Ave. \&Ramp CC | AC | 150 | 58 | AC | 150 | 93 |
| Kinnelon Rd. (Rt.618) | AC | 150 | 54 | AC | 150 | 70 |
| Kakeout \& Kinnelon Rd. | AC | 150 | 118 | AC | 150 | 3 |
| Cascade Way | AC | 150 | 0 | AC | 150 | 0 |
| Boonton Ave. | AC | 150 | 30 | AC | 150 | 36 |
| Morse Ave. | AC | 150 | 57 | AC | 150 | 85 |
| Cotluss Rd. |  |  |  |  |  |  |
| *.Actated-Coordinate |  |  |  |  |  |  |

*:Actuated-Coordinate
Table 5-b. Existing vs. Optimal Signal Timing of Route 23 (NOON)

|  | Existing |  |  | Optimized |  |  |
| :--- | :---: | ---: | ---: | ---: | ---: | ---: |
|  | Controller <br> Type | Cycle <br> Length <br> $(\mathrm{sec})$ | Offset <br> (sec) | Controller <br> Type | Cycle <br> Length <br> $(\mathrm{sec})$ | Offset <br> $(\mathrm{sec})$ |
| Intersection | AC | 90 | 45 | AC | 90 | 39 |
| Vernon Stockholm Rd.(Rt.515) | AC | 90 | 0 | AC | 90 | 80 |
| Canister Rd. | AC | 90 | 0 | AC | 90 | 80 |
| Reservior Rd. | AC | 90 | 45 | AC | 90 | 58 |
| Doremus | AC | 90 | 0 | AC | 90 | 85 |
| Paradise Rd. | AC | 90 | 87 | AC | 90 | 52 |
| Oak Ridge Rd. | AC | 90 | 35 | AC | 90 | 32 |
| Clinton Rd. | AC | 90 | 59 | AC | 90 | 8 |
| Larue Rd. (NB) | AC | 90 | 49 | AC | 90 | 8 |
| Larue Rd. (SB) | AC | 90 | 0 | AC | 90 | 44 |
| Kanhouse (Old Rt. 23) | AC | 90 | 0 | AC | 90 | 0 |
| Echo Lake Rd. | AC | 90 | 76 | AC | 90 | 83 |
| Center Court | AC | 90 | 45 | AC | 90 | 16 |
| Kiel Ave. \&Ramp CC | AC | 90 | 45 | AC | 90 | 52 |
| Kinnelon Rd. (Rt.618) | AC | 90 | 41 | AC | 90 | 46 |
| Kakeout \& Kinnelon Rd. | AC | 90 | 81 | AC | 90 | 11 |
| Cascade Way | AC | 90 | 0 | AC | 90 | 0 |
| Boonton Ave. | AC | 90 | 56 | AC | 90 | 54 |
| Morse Ave. | AC | 90 | 16 | AC | 90 | 88 |
| Cotluss Rd. |  |  |  |  |  |  |

Table 5-c. Existing vs. Optimal Signal Timing of Route 23 (PM)

|  | Existing |  |  | Optimized |  |  |
| :--- | :---: | :---: | ---: | ---: | ---: | ---: |
|  | Controller <br> Type | Cycle <br> Length <br> $(\mathrm{sec})$ | Offset <br> (sec) | Controller <br> Type | Cycle <br> Length <br> $(\mathrm{sec})$ | Offset <br> $(\mathrm{sec})$ |
| Intersection | AC | 140 | 3 | AC | 140 | 82 |
| Vernon Stockholm Rd.(Rt.515) | AC | 140 | 67 | AC | 140 | 15 |
| Canister Rd. | AC | 140 | 114 | AC | 140 | 65 |
| Reservior Rd. | AC | 140 | 71 | AC | 140 | 60 |
| Doremus | AC | 140 | 133 | AC | 140 | 119 |
| Paradise Rd. | AC | 140 | 78 | AC | 140 | 87 |
| Oak Ridge Rd. | AC | 140 | 33 | AC | 140 | 92 |
| Clinton Rd. | AC | 140 | 36 | AC | 140 | 97 |
| Larue Rd. (NB) | AC | 140 | 36 | AC | 140 | 97 |
| Larue Rd. (SB) | AC | 140 | 107 | AC | 140 | 85 |
| Kanhouse (Old Rt. 23) | AC | 140 | 0 | AC | 140 | 0 |
| Echo Lake Rd. | AC | 150 | 120 | AC | 150 | 123 |
| Center Court | AC | 150 | 77 | AC | 150 | 73 |
| Kiel Ave. \&Ramp CC | AC | 150 | 77 | AC | 150 | 88 |
| Kinnelon Rd. (Rt.618) | AC | 150 | 73 | AC | 150 | 77 |
| Kakeout \& Kinnelon Rd. | AC | 150 | 30 | AC | 150 | 31 |
| Cascade Way | AC | 150 | 0 | AC | 150 | 0 |
| Boonton Ave. | AC | 150 | 125 | AC | 150 | 133 |
| Morse Ave. | AC | 150 | 85 | AC | 150 | 80 |
| Cotluss Rd. |  |  |  |  |  |  |

Table 6-a Existing vs. Optimal Signal Timing of Route 42/322 (AM)

|  | Existing |  |  | Optimized |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Controller Type | Cycle <br> Length (sec) | Offset (sec) | Controller Type | Cycle Length (sec) | Offset (sec) |
| Shopping Center Dr. | AC* | 120 | 0 | AC | 110 | 0 |
| Greentree Rd. | AC | 120 | 70 | AC | 110 | 55 |
| Whitman Dr. | AC | 120 | 63 | AC | 110 | 78 |
| Gantown Rd. | AC | 120 | 0 | AC | 110 | 92 |
| Johnson Rd.(NB) | AC | 120 | 3 | AC | 110 | 78 |
| Fries Mill Rd.(SB) | AC | 120 | 12 | AC | 110 | 34 |
| Watson Dr. | AC | 88 | 48 | AC | 110 | 82 |
| Tuckahoe Rd.-Stagecoach Rd. | AC | 125 | 71 | AC | 110 | 31 |
| Berlin Cross Keys Rd. | AC | 120 | 114 | AC | 110 | 76 |
| Kennedy Dr. (SB) | Semi-A* | 90 | N/A | AC | 110 | 10 |
| Lake Ave. | Semi-A | 92 | N/A | AC | 110 | 0 |
| Sicklerville Rd. | Semi-A | 120 | 0 | AC | 110 | 4 |
| Poplar St.- New Brooklyn Rd. | Semi-A | 120 | 62 | AC | 110 | 104 |
| Main St. (Rt.322) | Semi-A | 107 | N/A | AC | 110 | 10 |
| Corkery Ln. | Semi-A | 88 | N/A | AC | 110 | 16 |
| Malaga Rd. | Semi-A | 84 | N/A | AC | 110 | 57 |
| White Hall Rd.-Corkery Ln. | Semi-A | 88 | N/A | AC | 110 | 0 |
| *:Actuated-Coordinate <br> **:Semi-Actuated |  |  |  |  |  |  |

Table 6-b Existing vs. Optimal Signal Timing of Route 42/322 (NOON)

|  | Existing |  |  | Optimized |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Controller Type | Cycle <br> Length (sec) | Offset (sec) | Controller Type | Cycle <br> Length (sec) | Offset (sec) |
| Shopping Center Dr. | AC | 120 | 0 | AC | 110 | 0 |
| Greentree Rd. | AC | 120 | 71 | AC | 110 | 105 |
| Whitman Dr. | AC | 120 | 74 | AC | 110 | 19 |
| Gantown Rd. | AC | 120 | 0 | AC | 110 | 32 |
| Johnson Rd.(NB) | AC | 120 | 3 | AC | 110 | 18 |
| Fries Mill Rd.(SB) | AC | 120 | 21 | AC | 110 | 93 |
| Watson Dr. | AC | 88 | 48 | AC | 110 | 33 |
| Tuckahoe Rd.-Stagecoach Rd. | AC | 125 | N/A | AC | 110 | 88 |
| Berlin Cross Keys Rd. | AC | 120 | 114 | AC | 110 | 104 |
| Kennedy Dr. (SB) | Semi-A | 90 | N/A | AC | 110 | 0 |
| Lake Ave. | Semi-A | 92 | N/A | AC | 110 | 0 |
| Sicklerville Rd. | Semi-A | 120 | 0 | AC | 110 | 7 |
| Poplar St.- New Brooklyn Rd. | Semi-A | 120 | 62 | AC | 110 | 100 |
| Main St. (Rt.322) | Semi-A | 85 | N/A | AC | 110 | 98 |
| Corkery Ln. | Semi-A | 88 | N/A | AC | 110 | 2 |
| Malaga Rd. | Semi-A | 84 | N/A | AC | 110 | 48 |
| White Hall Rd.-Corkery Ln. | Semi-A | 88 | N/A | AC | 110 | 0 |

Table 6-c Existing vs. Optimal Signal Timing of Route 42/322 (PM)

|  | Existing |  |  | Optimized |  |  |
| :--- | :---: | :---: | ---: | ---: | ---: | ---: |
|  | Controller <br> Type | Cycle <br> Length <br> $(\mathrm{sec})$ | Offset <br> $(\mathrm{sec})$ | Controller <br> Type | Cycle <br> Length <br> $(\mathrm{sec})$ | Offset <br> $(\mathrm{sec})$ |
| Intersection | AC | 120 | 75 | AC | 110 | 0 |
| Shopping Center Dr. | AC | 120 | 73 | AC | 110 | 33 |
| Greentree Rd. | AC | 120 | 84 | AC | 110 | 44 |
| Whitman Dr. | AC | 120 | 0 | AC | 110 | 75 |
| Gantown Rd. | AC | 120 | 3 | AC | 110 | 65 |
| Johnson Rd.(NB) | AC | 120 | 31 | AC | 110 | 28 |
| Fries Mill Rd.(SB) | AC | 88 | N/A | AC | 110 | 90 |
| Watson Dr. | AC | 125 | N/A | AC | 110 | 13 |
| Tuckahoe Rd.-Stagecoach Rd. | AC | 120 | 114 | AC | 110 | 16 |
| Berlin Cross Keys Rd. | Semi-A | 90 | N/A | AC | 110 | 34 |
| Kennedy Dr. (SB) | Semi-A | 92 | N/A | AC | 110 | 0 |
| Lake Ave. | Semi-A | 120 | 0 | AC | 110 | 20 |
| Sicklerville Rd. | Semi-A | 120 | 62 | AC | 110 | 12 |
| Poplar St.- New Brooklyn Rd. | Semi-A | 40 | N/A | AC | 110 | 70 |
| Main St. (Rt.322) | Semi-A | 88 | N/A | AC | 110 | 80 |
| Corkery Ln. | Semi-A | 84 | N/A | AC | 110 | 6 |
| Malaga Rd. | Semi-A | 88 | N/A | AC | 110 | 0 |
| White Hall Rd.-Corkery Ln. |  |  |  |  |  |  |

Table 6-d Existing vs. Optimal Signal Timing of Route 42/322 (OFF PEAK)

|  | Existing |  |  | Optimized |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Controller Type | Cycle Length (sec) | Offset (sec) | Controller Type | Cycle <br> Length (sec) | Offset (sec) |
| Shopping Center Dr. | AC | 120 | 0 | AC | 90 | 0 |
| Greentree Rd. | AC | 120 | 71 | AC | 90 | 24 |
| Whitman Dr. | AC | 120 | 74 | AC | 90 | 34 |
| Gantown Rd. | AC | 120 | 0 | AC | 90 | 58 |
| Johnson Rd.(NB) | AC | 120 | 3 | AC | 90 | 38 |
| Fries Mill Rd.(SB) | AC | 120 | 21 | AC | 90 | 85 |
| Watson Dr. | AC | 88 | 48 | AC | 90 | 46 |
| Tuckahoe Rd.-Stagecoach Rd. | AC | 125 | N/A | AC | 90 | 88 |
| Berlin Cross Keys Rd. | AC | 120 | 114 | AC | 90 | 64 |
| Kennedy Dr. (SB) | Semi-A | 90 | N/A | AC | 90 | 32 |
| Lake Ave. | Semi-A | 92 | N/A | AC | 90 | 0 |
| Sicklerville Rd. | Semi-A | 120 | 0 | AC | 90 | 52 |
| Poplar St.- New Brooklyn Rd. | Semi-A | 120 | 62 | AC | 90 | 24 |
| Main St. (Rt.322) | Semi-A | 85 | N/A | AC | 90 | 57 |
| Corkery Ln. | Semi-A | 88 | N/A | AC | 90 | 61 |
| Malaga Rd. | Semi-A | 84 | N/A | $\mathrm{AC}^{*}$ | 90 | 5 |
| White Hall Rd.-Corkery Ln. | Semi-A | 88 | N/A | AC* | 90 | 0 |

## CONCLUSIONS

While New Jersey has not seen significant increases in overall population, vehicles miles traveled (VMT) continues to increase and activity patterns are constantly changing. These tendencies significantly impact travel patterns. A programmatic updating of existing traffic signal timing plans provides an effective means to be responsive to these changes. And while the benefits of implementing these changes may not be as profound as adding new roadway capacity, new construction and associated property taking in a state which has earned the distinction of being the most densely populated in the nation, is often controversial and costly. Therefore, an important component to New Jersey's transportation success is extracting as much as possible from its existing infrastructure, which is also consistent with national transportation and environmental policies. Updating existing traffic signal timing plans based on current traffic volume conditions is a highly effective means for reducing driver delay, congestion and improving air quality.

The primary result of the optimal signal timing is that both studied corridors achieved their significant overall improvements (e.g., signal delay, average speed, fuel consumption, accident rate, vehicle emission rate, etc.). However, these improvements were not obtained in every intersection. For example, while signal delay at Boonton Avenue intersection in Route 23 was decreased by 142 veh-hr for AM period, it was increased nearly 4 veh-hr for AM period at Cotluss Road intersection in Route 23. Although entire network signal delay was drastically improved, some intersections were sacrificed to achieve better results. Thus, it is required to develop a new method enhancing the debased intersections.

Moreover, it was found that a systematic network partitioning process should be developed. Development of such procedure of network partitioning that can control queue management on the one network partition and the adjacent subnetworks would adopt multiple systems and cycle lengths into any types of network condition.

Finally, the project team suggests that traffic signal timing and coordination plans should be routinely updated to ensure system optimization.

## REFERENCES

1. Abu-Lebdeh, G., and Benekohal, R. "Development of a Traffic Control and Queue Management Procedure for Oversaturated Arterials". Transportation Research Board Annual Meeting Paper \#970707, 1997.
2. Algers, S., Bernauer, E., Boero, M., Breheret, L., di Taranto, C., Dougherty, M., Fox, K., and J. Gabard "Smartest Project Deliverable D3". University of Leeds, 1998.
3. Allsop, R.E. "Estimating a traffic capacity of a signalized road junction." Transportation Research, Vol. 6, pp. 245-255, 1972.
4. Benekohal,R. F., Elzohairy, Y.M., and Saak, J.E. "A Comparison of Delay from HCS, Synchro, PASSER II, PASSER IV and CORSIM for an Urban Arterial". The $81^{\text {st }}$ Annual Meeting, TRB, 2002.
5. Bloomberg, L., and Dale, J., 2000. "A Comparison of the VISSIM and CORSIM Traffic Simulation Models On A Congested Network". The 79 Annual Meeting, TRB, 2000.
6. Bullock, D., Morales, J.M. and Sanderson Jr., B. "Impact of Signal Preemption on the operation of the Virginia Route 7 Corridor." ITS America Annual Meeting, 1999.h
7. Cheu, R. L., X. Jin, K. C. Ng, Y. L. Ng, and D. Srinivasan. "Calibration of FRESIM for Singapore Expressway Using Genetic Algorithm". Journal of Transportation Engineering, Vol. 124, No. 6, pp. 526-535, November/December 1998
8. Chu, L.Y., Liu, H.X., Recker, W., Zhang, H.M. "Development of A Simulation Laboratory for Evaluating Ramp Metering Algorithms." The $81^{\text {st }}$ Annual Meeting, TRB, 2002.
9. Daganzo, C. F. "The Cell Transmission Model: A Dynamic Representation of Highway Traffic Consistent with the Hydrodynamic Theory". Transportation Research, 28B(4), 269-287, 1994.
10. Daganzo, C. F. "The Cell Transmission Model, Part II: Network Traffic". Transportation Research 29B(2), 79-93, 1995.
11. Federal Highway Administration. CORSIM User Manual Version 4.2. U.S. Department of Transportation, Federal Highway Administration, McLean, Virginia, 1998.
12. Fellendorf, M. "Public Transport Priority within SCATS - A Simulation Case Study in Dublin". Institute of Transportation Engineers, $67^{\text {th }}$ Annual Meeting, Boston, August 1997.
13. Gartner, N.H. "OPAC: A Demand-Responsive Strategy for Traffic Signal Control". Transportation Research Record 906. TRB, pp. 75-81, 1983.
14. Gazis, D.C. "Optimum Control of Over-saturated Intersections". Operations Research 12, 815-831, 1964.
15. Girianna, M., and Benekohal, R. F. " Dynamic Signal Coordination for Networks with Oversaturated Intersections". The 81 ${ }^{\text {st }}$ Annual Meeting, TRB, 2002.
16. Goldberg, D.E. "Genetic Algorithm in Search, Optimization and Machine Learning". Addison Wesley Longman, Inc., 1989.
17. Hansen, B.G., Martin, P.T., and Perrin H.J., 2000. "SCOOT Real-time Adaptive Control in a CORSIM Simulation Environment". The 79 ${ }^{\text {th }}$ Annual Meeting, TRB, 2000.
18. Hoyer, R., and Fellendorf, M. "Parametrization of Microscopic Traffic Flow Models
19. "Through Image Processing". $8^{\text {th }}$ IFAC Symposium on Transportation Systems, Chania, Greece, June 1997.
20. Husch, D., and J. Albeck. "Synchro 4.0 User Guide". Trafficware, Albany, California, 1999.
21. Husch, D., and Albeck, J. "SimTraffic User Guide." Trafficware Corporation, Albany, California, 2000.
22. ITT Systems and Sciences Corporation. CORSIM User's Manual, Version 1.04. Federal Highway Administration, March 1998.
23. ITT Systems and Sciences Corporation. TRAFVU User's Guide, Version 1.01. Federal Highway Administration, March 1998.
24. Jayakrishnan, R., Oh, J.S., and Sahraoui, A.E.K. "Calibration and Path Dynamics Issues in Microscopic Simulation For Advanced Traffic Management and Information Systems". The 81 ${ }^{\text {st }}$ Annual Meeting, TRB, 2002.
25. Kovvali, V. G., and Messer, C. J. " Senstivity Analysis of Genetic Algorithm Parameters in Traffic Signal". The $81{ }^{\text {st }}$ Annual Meeting, TRB, 2002.
26. Kovvali, V. G., Messer, C. J., and Chaudhary, N. A. "Progression Bandwidth Optimization Using Genetic Algorithms". The 81 ${ }^{\text {st }}$ Annual Meeting, TRB, 2002.
27. Lee, D. H., Yang, X., and Chandrasekar, P. "Parameter Calibration for PARAMICS Using Genetic Algorithm". The 80 ${ }^{\text {th }}$ Annual Meeting, TRB, 2001.
28. Lee, S., and Messer C. J. "Assessment of Three Traffic Simulation Models for Diamond Interchange Analysis". The 81 ${ }^{\text {st }}$ Annual Meeting, TRB, 2002.
29. Lighthill, M. J., and Whitham, J. B. "On Kinematic Waves. I. Flow Movement in Long Rivers. II. A Theory of Traffic Flow on Long Crowded Roads". Proceedings of the Royal Society (London), A229, 281-345, 1955.
30. Lo, H. "Signal Control for Over-Saturated Traffic Conditions". Presented at World Congress on Transport Research, Antwerp, Belgium. July 12-17, 1998.
31. Lo, H. "A Novel Traffic Signal Control Formulation". Transportation Research, 33A, pp. 433-448, 1999a.
32. Lo, H. "A Cell-Based Traffic Control Formulation: Strategies and Benefits of Dynamic Timing Plans". Transportation Science, 1999b.
33. Lo H. K., Chang, E., and Chan, Y.C., 2000. "Performance of A New Cell-based Dynamic Traffic Control Approach". The 79 ${ }^{\text {th }}$ Annual Meeting, TRB, 2000.
34. Luo, Y., Cheng, G. L. "Exploring the Robust Signal Optimization Method for Pretimed Control at Isolated Intersections". The 81 ${ }^{\text {st }}$ Annual Meeting, TRB, 2002.
35. Messer, C.J., H.E. Haenel, and E.A. Koeppe. "A Report on the User's Manual for Progression Analysis and Signal System Evaluation Routine - PASSER II". TTI Research Report 165-14, College Station, Texas, 1974.
36. Michalopoulos, P., and G. Stephanopoulos. "Over-saturated Signal Systems with Queue Length Constraints/I. Single Intersection/II. Systems of Intersections". Transportation Research, 11, pp. 413-28, 1977.
37. Park, B., Messer, C. J., and Urbanik II, T. "Enhanced Genetic Algorithm for Signal Timing Optimization of Oversaturated Intersections". The $79^{\text {th }}$ Annual Meeting, TRB, 2000.
38. Robertson, D. I. "TRANSYT: A Traffic Networks Study Tool". Road Research Laboratory Report 253. Crowthorne, Berkshire, Great Britain, 1969.
39. Sadek, A.W., and Mark, C. "Evaluating the Effectiveness of the New Features in TRANSYT-7F, Version 9.2". The $81^{\text {st }}$ Annual Meeting, TRB, 2002.
40. Stephanopoulos, G., P. Michalopoulos, and G. Stephanopoulos. "Modelling and Analysis of Traffic Queue Dynamics at Signalized Intersections". Transportation Research, 13A, pp. 295-307, 1979.
41. TRB. "Highway Capacity Manual - Special Report 209, 3rd Ed." Transportation Research Board, National Research Council, Washington D.C., 1997.
42. Trafficware. "Survey of Traffic Software Use" Trafficware Corporation, Albany, CA, hittp://www.trafficware.com/survey2000.htm . July 2001.
43. Trueblood, M. "Should I Use CORSIM or SimTraffic?" Trafficware Corporation, Albany, CA, 'http://www.trafficware.com/downloads/crsmvst.pdif.
44. Washburn, S., and Larson, N. "Signalized Intersection Delay Estimation: Case Study: TRAMSYT-7F, Synchro, and HCS". The 80 ${ }^{\text {th }}$ Annual Meeting, TRB, 2001.
45. Webster, F.V., and Cobbe, B.M. "Traffic Signals, Road Research Technical Paper No. 56", Road Research Laboratory, HMSO, London, 1966.
46. Wey, W.M., and Jayakrishnan, R. "A Network Traffic Signal Optimization Formulation with Embedded Platoon Dispersion Simulation". Transportation Research Board, Annual Meeting Paper \#971337, 1997.
47. Wood, K. "Urban Traffic Control, Systems Review". Transport Research Laboratory, Project Report 41, 1993.
48. Xie, C., and Parkany, E. "Signalized Intersection Simulation in CORSIM and SIMTRAFFIC". The 81 ${ }^{\text {st }}$ Annual Meeting, TRB, 2002.
49. Yagar, S. "Capacity of a signalized road junction: Critique and extensions." Transportation Research, Vol. 8, pp. 137-147, 1974
50. Zahavi, V., and Ryan, J.M. "Stability of Travel over Time." Transportation Research Report 750, TRB, National Research Council, Washington, D.C., 1980, pp. 70-75

## APPENDIX A: LITERATURE REVIEW

## Signal Optimization Models

Over the past decades mathematical programming values has been carried out by various methods for optimizing signalized intersections. The theoretical concept as well as formulation was first discussed by Webster and Cobbe (1966). The basic assumption was that the traffic volume of the intersection did not exceed its capacity. Based upon this assumption, each approach of the intersection was given a predetermined 'desired degree of saturation' to limit the level of saturation. The objective was to minimize the total intersection delay during the entire period of operation subject to some typical constraints (e.g., cycle length, splits, and mean arrival rate of vehicles). However, this model did not respond to flow variation. Thus, the signal control would be far from real optimal control (Luo, et al., 2002). Following Webster's concept, Allsop (1972) used a Linear Programming method to maximize the total departure of an intersection. Yagar (1974) extended Webster and Cobbe's theory by considering stochastic vehicle arrivals at an intersection and reformulated Allsop's model by considering changeable saturation flows in different calculation stages. Yagar's model became one of the operational techniques to calculate cycle lengths and green times in the 1994 Highway Capacity Manual (HCM). However, it was not a real-time calculation model in lack of efficient dynamic queue formulation. Many models and simulators have been developed and already applied to the practice, among which, OPAC (1983), TRANSYT-7F (1991), PASSER (1991), and SCOOT (1996), are the major representatives. Shepherd (1992) and Wood (1993) summarized these models from the view of both theory and practice and concluded that most of them served well for under saturated or slightly congested condition and may be inaccurate while dealing with oversaturated situation (Liu, 2001).

For oversaturated traffic condition where queues persist and cannot be fully discharged, two models were firstly developed by Gazis (1964) and Michalopoulos and Stephanopoulos (1979). However, both models considered effects of traffic signal under a constant flow condition. In reality, traffic flow at a signalized intersection follows a step function. The exit flow is at saturation (zero) when the time of interest is in a green (red) phase. Secondly, both models considered a signal
control system as a queuing network. More recently, a number of enhanced models were developed (Abu-Lebdeh, et al., 1997; and Wey, et al., 1997) to deal with oversaturated traffic condition.

Stephanopoulos et al. (1979) pointed out the problem of modeling congested traffic without the Fundamental Diagram (Figure 7). The study approach taken was macroscopic in nature (i.e. cars are treated as a continuum rather than individually) and is based on the theory of shock waves developed by Lighthill and Whitham (1955)


Figure A-1. Flow-density relationship
Frequent stop-and-go movements in congested situation generate traffic dynamics in the form of shockwaves. Density along the queue length was constantly in a state of transition, which rendered the assumptions of compact queue and constant average density questionable. In short, without the Fundamental Diagram, it is difficult for a model to describe queue dynamics accurately, which is needed to generate good timing plans for over-saturated traffic condition (Lo, et al., 2000).

Recently, Lo (1998, 1999a, 1999b) developed a cell-based dynamic signal control formulation designated as Dynamic Intersection Signal Control Optimization (DISCO). DISCO, a heuristic solution approach, considers the entire range of the Fundamental Diagram by encapsulating the Cell-Transmission Model (CTM) (Daganzo, 1994 and 1995). CTM provided a convergent approximation to the Lighthill and Whitham, and Richards (LWR) model and covered the entire Fundamental Diagram. The features and validation of CTM were discussed by Lin and Ahanotu (1995).

Basically, CTM can replicate kinematic waves, queue formation and dissipation in an explicit manner. This capability makes it a suitable platform for modeling dynamic traffic. While Lo (1998, 1999a, 1999b) applied DISCO to a range of demand scenarios to demonstrate its ability, the results were promising. For light to moderate traffic condition, DISCO produced timing plans consistent with the plan recommended by other models. Moreover for gridlock conditions, DISCO was able to produce a timing plan better than that using conventional queue management practices.

In highway networks, traffic interruptions occur at signalized intersections, while road users experience frequent stops and delay. Furthermore, for an arterial with more than two signalized intersections, vehicle arrivals are moving with platoons and traveling to downstream intersections. If appropriate signal coordination is designed on such an arterial, the platoon of vehicles can pass through downstream intersections with minimum number of stoppings, thus decreasing intersection delays experienced by the road users (Kovvali, et al., 2002). The majority of existing signal coordination algorithms did not consider the dynamic queue length at each intersection approach. Therefore, the application to oversaturated conditions may lead to sub-optimal results. Over saturation occurs when a signalized intersection cannot process all arrived vehicles at the end of a green period, thus a queue is developed and may be carried over to the next cycle. If corrective steps are not taken, the growing queue will block the upstream intersections and reduce the network capacity (Girianna, et al., 2002).

Considering a network with corrected multiple signalized arterials, coordination can be accomplished by changing offsets and splits. The coordination among the arterials is usually bounded by critical intersections of two arterials. The optimization of network wide arterial coordination is a combinatorial combination problem. A micro Genetic Algorithm ( $\mu \mathrm{GA}$ ) was developed (Goldberg, 1989) to solve the problem. GA regarded as an emerging optimization tool due to its simplicity, minimal problem restrictions and capability in solving large combinatorial combination problems, parallelism and productivity of global solutions. GAs simulate the genetic state or chromosome of an individual population by selecting the most influential individual through genetic operators, such as natural selection, mutation, and crossover, while
the chromosome can represent the set of green times in signal coordination problems.

Currently, the most widely used signal coordination programs include PASSER, TRANSYT-7F, SCOOT, OPAC, and Synchro etc. They are discussed next.

## PASSER

PASSER (Progression Analysis and Signal System Evaluation Routine) is the most widely used bandwidth optimization software for arterial streets. PASSER II was developed by the Texas Transportation Institute in the early 1980s. It is a macroscopic simulation model designed to optimize signal timing parameters and progression on arterials. PASSER II calculates splits using Webster's methodology. The program then adjusts the splits through minimizing delay for all intersections. While calculating splits, PASSER II applies a half-integer concept based on Brook's bandwidth algorithm for maximizing progression bandwidth along an arterial (Messer, et al., 1974). Thus, the interference to progression bands was minimized. The maximum progression efficiency in PASSER II along an arterial was obtained by optimizing cycle length, offsets and phasing sequences. (Kovvali, et al., 2002). As an enhanced version of PASSER II, PASSER II-90 can model multiple phase plans, one-way streets, variable cycle lengths and maximize arterial progression.

PASSER III is designed for under saturated conditions. It can optimize signal timings by minimizing delay at each intersection. Since the delay module in PASSER III applies vertical stacking of queues, the optimization could be inaccurate for short links even during under saturated conditions. PASSER III applies vertical stacking of queues and hence is not capable of modeling queue spillback conditions in its current form (Kovvali, et al., 2002).

In the early 1990s PASSER IV-96 was released. Based on the MAXBAND program, the DOS based PASSER IV-96 is used to optimize a network wide signalized traffic control through maximizing bandwidth. The bandwidth is maximized so that a car can potentially pass through a series of signalized intersections with minimal number of stoppings. It is able to optimize arterial signal timings as well as closed-loop networks in central business districts (CBD). Unlike PASSER II-90, PASSER IV-96
can handle multiple connected arterials with one-way and two-way traffic operations (Benekohal, et al., 2002).

## TRANSYT-7F

TRANSYT-7F is a macroscopic simulation program with optimization feature originally developed by Robertson (1969). Since then, the program has been continuously enhanced. The first U.S. version of TRANSYT-7F was developed in 1981 by the Florida Transportation Center at the University of, and the most recent TRANSYT-7F is version 9.

TRANSYT-7F is a powerful tool, for signal optimization, within which the simulation module is a deterministic model that simulates macroscopic traffic flow in a stepwise fashion (Wallace, et al., 1998). Before version 7, the simulation was performed in individual links whereby the model would complete all the time steps for one link, before proceeding to the next link. This approach, however, could not simulate spillback effects, and was thus refined in version 8 (Sadek, et al., 2002).

For signal optimization, TRANSYT-7F traditionally used a special application of the hill climbing search method with different step sizes, which is an iterative, gradient search algorithm that typically requires extensive computation. The process of searching the optimal solution will continue until no further improvement in the value of the objective function.

Various objective functions were applied before version 7, such as minimizing delay, minimizing the combination of delay and number of stops (the Disutility Index - DI), maximizing progression opportunities (PROS), and optimizing the combination of DI and PROS (Sadek, et al., 2002). Version 8 was developed to model oversaturated traffic conditions, where a step-wise simulation rather than link-wise simulation was applied. Four new additional functions were introduced to version8:

- Minimizing the product of queuing ratio (QR) and the DI.
- Maximizing the ratio of throughput (Thru) over DI (i.e. Thru/DI).
- Maximizing throughput, and then minimizing the DI without reducing the throughput.
- Maximizing throughput, with a penalty imposed if the volume/capacity (v/c) ratio exceeds a user-defined threshold was intruded in release.

By enhancing version 8, three major new features were introduced version 9, including: (1) a routine for thorough cycle length optimization (CYCOPT); (2) a method for modeling traffic-actuated controllers (T7FACT); and (3) a Genetic Algorithm (GA) routine to augment the traditional hill-climbing algorithm in determining optimal signal offsets. Although the use of the CYCOPT and T7FACT modules appears to yield superior timing plans to those developed using the older version of TRANSYT-7F, the GA routine is not very effective in improving the quality of the timing plans. (Sadek, et al., 2002).

## SCOOT

SCOOT (Split, Cycle, and Offset Optimization Technique) is a third generation adaptive traffic signal control system introduced to the UK in early 1980's (Hunt, et al., 1981). The goal of adaptive signal control systems is to improve flow conditions on urban networks by optimizing signal coordination, considering real-time traffic conditions. SCOOT is one of few adaptive control systems widely applied around the world (Hansen, et al., 2000).

SCOOT optimizes traffic signal timings (e.g., cycle length, offsets, and splits) that minimize Performance Index (PI), the measure of joint impacts of average queue length and number of stops. If a critical intersection is identified, it will influence the signal optimization for intersections of each section within the studied network. Embedded within SCOOT are models for handling queue accumulation, queue dissipation and platoon dispersion that receive real-time information (e.g., flow and occupancy information) for SCOOT's optimization processes. SCOOT has been regarded as an "on-line TRANSYT" because a similar method to optimize off-line signal timings is employed. Unlike fixed signal timing plans that age rapidly and require costly data collection for updating, the optimal signal timings from SCOOT continuously respond to changing demands and thus do not require updating. SCOOT employs information from vehicle detectors to predict total delay and stops based on current signal timings over short rolling horizons. In this manner, frequent small alterations can adapt to the short-term fluctuations in traffic demand (Hansen, et al., 2000).

## OPAC

The Optimized Policies for Adaptive Control (OPAC) strategy is a real-time signal timing optimization algorithm that has been developed by Parsons Brinkerhoff Farradyne Inc. and the University of Massachusetts at Lowell since 1980's (Gartner, 1982 and 1983). OPAC is a distributed control strategy featuring a dynamic optimization algorithm that calculates signal timings to minimize a performance function considering total intersection delay and stops without requiring a rigid, fixed cycle time. The algorithm uses a combination of measured and modeled demand to determine phase durations at signalized intersections subject to minimum and maximum green times. If it is running in a coordinated mode, the optimal cycle length and offsets can be updated based on real-time data. In the early 90's, a real-time traffic-adaptive signal control system (RT-TRACS) was developed by Federal Highway Administration (FHWA), which served as a platform for the implementation of a variety of traffic signal control algorithms. In a latest study, the OPAC strategy was developed on RT-TRACS that provided capabilities for both individual and coordinated control at signalized intersections. Reduced delays and number of stops maintained the progressions along a tested arterial were demonstrated after comparing that with a fixed time system (Kovvali, et al., 2002).

## Synchro

Synchro was developed in the mid-1990s by Trafficware Inc., which performs simulation and optimization, based on a deterministic and macroscopic modeling approach. Synchro relies more on analytical relationships for estimating these effects (Washburn, et al., 2001). It adopts a window-based, menu-driven approach for data input and output processes (Husch, et al., 1999). Due to its simplicity of manipulation and flexibility of applications, it has gained popularity in signal optimization. Synchro has the following significant features:

- Ability to simultaneously optimize lead-lag phase ordering in addition to cycle length, phase lengths, and coordination offsets. Synchro can search for the best cycle length (within a user-specified range), determine appropriate phase lengths and offsets for the selected cycle length, and evaluate different
lead/lag phase orderings. Separate optimization of multiple divided zones within the overall network can be managed. Synchro allows different cycle lengths within one coordinated network.
- Percentile Delay estimation method which provides an alternative to model the effects of actuation and coordination in a more realistic manner. Synchro offers users a choice between two types of signal delay calculations: 1) the 1997 HCM formulation or called Webster ${ }^{\text {TM }}$ s delay, and 2) percentile delay.

Synchro integrates the area under the arrival-departure curve to calculate uniform delay, using a 0.1 -second time slice resolution. This method, again, explicitly accounts for the effects of coordination. The component of delay is calculated according to the 1997 HCM formulation. For the Percentile Delay, the main distinction is in how the traffic volume was modeled. The HCM method utilizes a constant traffic volume for the entire hour, or peak 15 minutes, while the Percentile method uses five different traffic volume loadings $10^{\text {th }}, 30^{\text {th }}, 50^{\text {th }}, 70^{\text {th }}$ and $90^{\text {th }}-$ percentile based on a Poisson distribution. These loadings are used for a 15 -minute analysis period (they are adjusted by the PHF) to calculate weighted delay measurement. Essentially, this technique is intended to more realistically model traffic demand variability experienced from cycle to cycle as well as calculate green times for actuated signals. This, in combination with the ability of actuated signals to efficiently respond to variable traffic loadings, usually results in more accurate modeling of actuated signals. Nearly- and over-saturated conditions can also result in significant differences between the Percentile and HCM delay estimation methods.

- Easy data input and comprehensive output options. Synchro allows the user to click and drag to create links (nodes are created implicitly). It also allows the use of a "background" Drawing Exchange Format (DXF) file as a template for tracing the studied street network. This graphical input method is very intuitive and user-friendly. Once the studied network has been created graphically, the remaining data are input in a format that basically mirrors the HCM worksheets, with an additional worksheet for actuated operations. A key feature of Synchro is that most of its calculations and analysis results are
updated immediately following changes to user-adjustable values. In addition, Synchro networks can be easily converted to be used by other models (e.g., CORSIM, and TRANSYT) for extensive and comprehensive analysis. Synchro can produce various MOEs. The user can read basic operational analysis information directly from the input screens as parameter values are entered or changed. The user can also place a query for one or more reports of any operational statistics by lane group, approach, intersection, arterial, or network. Synchro can also create interactive time-space diagrams with immediate results.

Other beneficial features in Synchro include:

- Capability of modeling right-turns on red, u-turns, and five-legged intersections.
- Multiple intersections can be controlled by a single controller, simplifying the process for modeling situations like diamond interchanges.
- Optimization objective function is to minimize delay.
- Modeling of Actuated Control.

The modeling of pre-timed signal operation is fairly straight forward since phase durations are fixed at the same length for every cycle, while Synchro can model complicated actuated signal operations.

Synchro also employs its own green time calculator for actuated conditions. It estimates green times for each of the five different percentile volume loadings according to the Poisson distribution. Synchro uses formulas, which are based on the inputs from the actuated controller settings input page, to predict phase gapping and skipping probabilities for each of the five volume scenarios, and adjusts the average green times accordingly. The delay is calculated for each volume scenario and then averaged across all five volume loadings to determine the overall signal delay under actuated conditions. The Synchro documentation states that its actuated estimated green times will be consistent to those determined by the method in HCM, Chapter 9 and Appendix II. Synchro can handle dual-ring controllers, which allows it to accommodate overlapping phases.

For conducting this project, the selected computer software should have the following features:

- The ability to optimize signal timings and simulate operations over a network with signalized intersections;
- The flexibility in terms of data inputs; and
- Provision of results on MOEs required for feasibility studies.

Currently among the widely used signal timing optimization models (e.g., Synchro, TRANSYT, SCOOT, and OPAC etc.), Synchro is a widely used signal timing optimization software. According to significant features discussed above, Synchro 5.0 was selected as a tool for optimizing signal timings for this project.

## Simulation Models

Computer modeling and simulating signalized highway networks have been widely and increasingly applied in traffic analysis and evaluation. The main reasons are classified into two folds. One fold is that the performance of signalized highway operations and traffic impact of tentative modifications can be tested and evaluated before field implementation. The other fold is that some critical MOEs such as signal delay, which are difficult to measure in the field can be obtained through simulation. The widely used simulation packages reviewed here include CORSIM, SimTraffic, PARAMICS, and VISSIM.

## CORSIM

CORSIM (CORridor SIMulation) is a microscopic traffic simulation model developed by FHWA and embedded in TSIS (Traffic Software Integrated System), which integrates two microscopic simulation models: the arterial network model NETSIM and the freeway model FRESIM. It is a discrete time, stochastic, "state-of-thepractice" model used to simulate traffic operations. Visual simulation is realized by an animation processor called TRAFVU (TRAFfic simulation Visualization Utility) also embedded in TSIS. CORSIM is well recognized for its sophisticated algorithms in car-following and lane-changing models and is able to analyze a wide range of traffic, geometric, and control conditions. CORSIM can produce a rich set of MOEs,
including delay, travel time, speed, number of stops, queue time, stop time, queue length, fuel consumption, and vehicle emission etc.

The most important MOEs when modeling and evaluating a signalized intersection are control delay and traffic throughput which are affected by driver and vehicle related factors such as car-following factor, acceleration and deceleration rates, reaction time, and turning speed etc. These traffic characteristics are required to be specified in CORSIM, and needed to calibrate. So that the real-world traffic operations of the studied network can be appropriately replicated.

CORSIM has the capability to simulate pre-timed, semi-actuated and actuated signal operations (including pedestrian-activated signal operation) as well as coordinated control strategies. However, CORSIM does not have built-in analytical and empirical optimization capability. A number of signal studies conducted by using CORSIM are shown below.

Bullock et al. (1999) applied CORSIM to evaluate the effectiveness of emergency vehicle signal preemption. The studied location consisted of three intersections on Leesburg Pike (Route 7, Virginia) near the location of a hospital. This geometric condition was coded into the CORSIM to determine the possible effects on providing emergency vehicle preemption on the three intersections. Results showed that the impact on other traffic is statistically significant, however, it is minimal with a 2.4\% increase in average travel time when the priority is requested

Park et al. (2000) employed CORSIM to simulate three different genetic algorithm (GA) based optimization strategies, which are throughput maximization, delay minimization, and modified delay minimization with a penalty function. Simulation results revealed that the delay minimization strategy produced less queue time for all spacing examined. However, none of the strategies provided dominant performance in terms of system throughput. It should be noting that the minimum queue time did not correspond to maximum throughput.

INTEGRATION (Model integrates a number of unique capabilities),CORSIM and WATSim (Wide Area Traffic Simulation) were applied to three heavily loaded traffic
networks in Honolulu for which detailed, simultaneous, and contemporaneous flow condition are known. The models produced satisfactory and comparable results on most of the tested network links. This study revealed that the main limitation of these models is the large number of parameters that need to be modified to replicate real traffic conditions (Wang and Prevedouros, 1998).

## SimTraffic

Like Synchro, SimTraffic is the key simulation model developed by Trafficware. While Synchro is applied to conduct signal optimization and coordination, SimTraffic performs a microscopic simulation and realizes animation.

Similar to CORSIM, SimTraffic needs the input value of parameters (e.g., carfollowing factor, acceleration and deceleration rates, reaction time, and turning speed etc.) While modeling the traffic operation of the studied network, geometric conditions, such as link length, curb lines and curves, stop lines, left-turn or right-turn pockets, exclusive left turn lanes, median width etc. are required input to build $p$ the network. The following studies are conducted by using SimTraffic.

Park et al. (2004) applied SimTraffic to determine time-of-day (TOD) breakpoints manually using one or two days' worth of traffic data. Signal control can be categorized as pre-timed, actuated and adaptive. Among these, both pre-timed and coordinated actuated controllers deploy multiple signal timing plans to account for traffic demand changes during a day, while adaptive control changes timing plan in real time according to traffic conditions.

Drummond et al. (2002) developed a method for using simulation models to evaluate the safety impacts of increased traffic signal density in suburban corridors. Using 10 years of data from two major arterials in Virginia, actual crash rates were compared to operational performance measures simulated by the Synchro/SimTraffic model. As expected, crash rates were positively correlated with stops per vehicle and delay per vehicle and negatively correlated with mainline speed.

## PARAMICS

PARAMICS is a suite of software tools for microscopic, time-stepping traffic simulation (Lee, et al., 2001). The name PARAMICS is an acronym derived from Parallel Microscopic Simulation. As a suite of ITS-capable, user-programmable, highperformance microscopic traffic simulation package, PARAMICS offers very plausible detailed modeling for many components of an 'ideal' simulator. Individual vehicles are modeled in fine detail for the duration of their entire trips, providing accurate traffic flow, transit time and congestion information, as well as enabling the modeling of the interface between drivers and ITS facilities. In addition, PARAMICS provides users with an Application Programming Interface (API) through which users can customize and extend many features of the underlying simulation model.

Complementary modules could be any ITS application, such as signal optimization, adaptive ramp metering, incident management and so on. In this way, new control strategy can be easily tested and evaluated by the simulator before their implementation in the real world (Chu, et al., 2002). PARAMICS excels in modeling congested networks and ITS infrastructures (Algers, et al., 1998).

## VISSIM

VISSIM (Hoyer, et al., 1997; Fellendorf, 1997) is a microscopic, time driven and behavior based simulation model developed to analyze full range of classified roadways and public transportation operations. VISSIM can model operations for various transportation models (buses, light rail, heavy rail, trucks, pedestrians, and bicycle) in an integrated roadway networks.

VISSIM consists of two primary components: (1) simulator and (2) signal state generator denoted as SSG. The simulator generates traffic onto the user graphically specified network. The user can import an aerial photo or schematic drawing of the studied area. Then, the network attributes (e.g., lane widths, speed zones, priority rules, etc.). Unlike other simulations, VISSIM models do not have traditional node structure, which provides the user with the flexibility to control traffic operations and vehicle paths within an intersection or interchange (Bloomberg, et al., 2000).

The SSG in VISSIM is separated from the simulator. It is where the signal control logic resides. The user has the ability to define the signal control system and thus emulate any type of control logic found in a signal controller manufacturer's firmware. The SSG permits the user to analyze the impact of signal operations including, but not be limited to: fixed time, actuated, adaptive, transit signal priority, and ramp metering. The SSG reads detector information from the simulator every time step and the SSG decides the status of the signal display during the subsequent time step can be decided (Bloomberg, et al., 2000).

As to assess and choose simulation software for this project, the reliability of the MOEs from simulation output; the reality of the network with signalized intersections; and the feasibility and simplicity of data exchange between the signal optimization model (e.g., Synchro) for comprehensive analysis are critical issues to be considered. Thus, the suitable simulation software for this project should be either CORSIM or SimTraffic. Because the traffic modeling process in SimTraffic is similar to CORSIM, both simulation models seem to produce very similar outcomes (Trafficware, 2001). As one of high quality, high credibility, matured simulation software (Trafficware, 2001), SimTraffic has the fast and efficient coding with Synchro, and it is deemed the solution simulation model to evaluate the optimal timing recommended by Synchro.

## Model Calibration

Simulation models should be properly calibrated and then used to perform other analyses, such as evaluating the impact of signal timing changes discussed in this study. In order to calibrate the SimTraffic model and mimic the real-world traffic conditions, the calibrated parameters primarily include those related to driver behavior, vehicle performance and roadway throughput capability (e.g., free flow speed, headway factors, turning speed, saturated flow rate and pedestrian walking speed).

In general, there are two different approaches to calibrate microscopic traffic simulation models. The first approach is to establish the input-output relation and improve accuracy by changing the basic modules. The basic requirement is that the researchers have a good understanding of the details of the particular simulator
modules. The second approach is referred to as parameter calibration, defined as the re-establishment the input-output relation to obtain the desired system accuracy by changing those parameters that govern the input-output relationship in the systems being modeled (Lee, et al., 2001). Parameter calibration in a simulation model may be regarded as an optimization problem in which a set of values for operating parameters that satisfy an objective function are to be searched (Cheu, el at., 1998).

It is difficult to assess the impact when varying several parameters at a time due to the interdependent influence to the simulation results. Thus, simulation results with respect to each varying parameter should be investigated, while other parameter values should be fixed. In order to identify key parameters influencing the simulation results, sensitivity analysis for various parameters should be conducted, while the impacts of changing those parameters should be observed.

The calibration procedure is composed by the following comparisons: Graphical Comparison, Aggregate Comparison, and Statistical Comparison.

## Graphical Comparison

The graphical comparison is a subjective validation approach, which is especially useful for testing the results generated by the simulation model preliminarily. It makes the comparison easy and visible.

## Aggregate Comparison

Aggregate means and standard deviations give general indication of system performances in real world and in simulation. However, they do not present accurate trend or indicate how variables perform over time, what patterns are created, and how much individual measurements deviate. Aggregate comparisons, along with the graphical comparisons of scattered plots, reveal the similarities and discrepancies by changing analyzed variables.

## Statistic Comparison

The statistic analysis is crucial for validating the proposed model based on sample data collected from the real world and simulation. It can be used for assessing the
model accuracy, testing various hypotheses and determining degree of correlation. The following equations are indices used for statistic comparison.

Mean Absolute Percent Error (MAPE) measures the percentage error between simulation results and field data, which can be given by Eq. 1:
MAPE $=\frac{1}{n} \sum_{i=1}^{n} \frac{\left|S_{i}-O_{i}\right|}{O_{i}} * 100 \%$
where $n, S_{i}$ and $O_{i}$ are sample size, observation $i$ of simulation output and observation $i$ of field measurement respectively.

Root Mean Square Error (RMSE) denotes the error between simulation results and field data, which can be given by Eq. 2:
$\mathrm{RMSE}=\sqrt{\frac{1}{n} \sum_{i=1}^{n}\left(S_{i}-O_{i}\right)^{2}}$
where $n, S_{i}$ and $O_{i}$ were defined in Eq. 1.

Mean Absolute Relative Error (MARE) and Variance of Absolute Percentage Error (VAPE), predict accuracy between simulation results and field data, as formulated in Eqs. 3 and 4, respectively.
MARE $=\frac{1}{n} \sum_{i=1}^{n} \frac{\left|O_{i}-S_{i}\right|}{O_{i}}$
where $n, S_{i}$ and $O_{i}$ were defined in Eq. 1
$\operatorname{VAPE}=\operatorname{Var}\left(\frac{\left|S_{i}-O_{i}\right|}{S_{i}}\right)$
where $n, S_{i}$ and $O_{i}$ were defined in Eq. 1

In addition to previous simulation prediction error indices, root relative square error (RRSE) and maximum relative error (MRE) are computed. These indices are defined as:

RRSE $=\sqrt{\frac{\sum_{i=1}^{n}\left(S_{i}-O_{i}\right)}{\sum_{i=1}^{n}\left(O_{i}-\bar{O}\right)^{2}}}$, and $\bar{O}=\frac{1}{n} \sum_{i=1}^{n} O_{i}$
where $n, S_{i}$ and $O_{i}$ were defined in Eq. 1,

MRE $=\max _{i} \frac{\left|O_{i}-S_{i}\right|}{O_{i}}$
where $S_{i}$ and $O_{i}$ were defined in Eq. 1,

MAPE (Eq. 1) and RMSE (Eq. 2) indices were adopted for statistic comparison in this study.

## Model Validation

Once parameters of the simulation model were well calibrated, the results must be validated by comparing MOEs observed in the field against simulated MOEs (Cohoe, 2002). The validation process establishes the credibility of the model by demonstrating its ability to replicate actual network and traffic patterns (Jayakrishnan, et al., 2002), and that should only be performed after the model has been properly calibrated. Validation is largely dependent on two major issues: the context (i.e., model performance could drastically change with the context), and the extent of the calibration effort at the conceptual and operational levels. The context may be for studying safety, environmental effects, and capacity improvement or congestion mitigation. Context variable data is necessary for both calibration and validation. It is important noting that the validation must not rely on a single field data. The preliminary test of MOEs can be conducted through graphic comparison between the values of field observations and simulation results. The statistic analysis can be conducted by calculating MAPE and RMSE for the field and simulated MOEs.

Various optimization packages (PASSER II, TRANSYT-7F, and SYNCHRO, etc.) have been applied to optimize traffic signal timing plans. In order to demonstrate the performance of one is better than others, comparative analyses should be conducted. These packages would generate different optimal timing plans fixed cycle length and splits, etc. because the objective functions applied in these programs were different. Thus, the outputs from these optimization programs are recommended to be fairly evaluated through a series of simulation runs.

## SUMMARY

According to the review of literature and current practice, traffic modeling software can be classified into two catalogs according to their functions on traffic analyses. They are signal timing optimization models (e.g., Synchro, TRANSYT, PASSER, SOAP, TSPP Draft, etc.) and simulation models (e.g., CORSIM, SimTraffic, PARAMICS, VISSIM, INTEGRATION, CINEMA, CORFLO, etc.). Synchro is one of the most widely used signal timing optimization software and has gained much attention in transportation industry because of its user friendly applications and creditable results. In addition, a micro-simulation program SimTraffic is complied with Synchro for evaluating the recommended optimal time plans. The project team of this study is therefore select Synchro and SimTraffic for modeling and simulating two studied signalized arterials (e.g., Route 23 and Route 42/322) for NJDOT.

## APPENDIX B: AEROGRAPHIC INFORMATION FOR THE STUDIED INTERSECTIONS

Route 23


Figure B-1. Intersection of Route 23 and Vernon Stockholm Rd. (Rt. 515)


Figure B-2. Intersection of Route 23 and Canister Rd.


Figure B-3. Intersection of Route 23 and Reservoir Rd.


Figure B-4. Intersection of Route 23 and Doremus Rd.


Figure B-5. Intersection of Route 23 and Paradise Rd.


Figure B-6. Intersection of Route 23 and Oak Ridge Rd.


Figure B-7. Intersection of Route 23 and Clinton Rd.


Figure B-8. Intersection of Route 23 and Larue Rd. (NB)


Figure B-9. Intersection of Route 23 and Larue Rd. (SB)


Figure B-10. Intersection of Route 23 and Kanhouse (Old Rt. 23)


Figure B-11. Intersection of Route 23 and Echo Lake Rd.


Figure B-12. Intersection of Route 23 and Center Court


Figure B-13. Intersection of Route 23 and Kiel Ave. \& Ramp CC


Figure B-14. Intersection of Route 23 and Kiel Ave. \& Ramp CC


Figure B-15. Intersection of Route 23 and Kakeout Connector \& Kinnelon Rd.


Figure B-16. Intersection of Route 23 and Cascade Way


Figure B-17. Intersection of Route 23 and Boonton Ave.


Figure B-18. Intersection of Route 23 and Morse Ave.


Figure B-19. Intersection of Route 23 and Cotluss Ave.

Route 42/322


Figure B-20. Intersection of Route 42/322 and Shopping Center Dr.


Figure B-21. Intersection of Route 42/322 and Green tree Rd.


Figure B-22. Intersection of Route 42/322 and Whitman Dr.


Figure B-23. Intersection of Route 42 and Gantown Rd.


Figure B-24. Intersection of Route 42 and Johnson Rd (NB)


Figure B-25. Intersection of Route 42/322 and Fries Mill Rd. (SB)


Figure B-26. Intersection of Route 42/322 and Watson Dr.


Figure B-27. Intersection of Route 42/322 and Tuchahoe Rd. - Stagecoach Rd.


Figure B-28. Intersection of Route 42/322 and Berlin Cross Keys Rd.


Figure B-29. Intersection of Route 42/322 and Kennedy Dr. (SB)


Figure B-30. Intersection of Route 42/322 and Lake Ave.


Figure B-31. Intersection of Route 42/322 and Sicklerville Rd.


Figure B-32. Intersection of Route 42/322 and Poplar St. - New Brooklyn Rd.


Figure B-33. Intersection of Route 42/322 and Main St. (Rt. 322)


Figure B-34. Intersection of Route $42 / 322$ and Corkery Ln. (Rt. 322)


Figure B-35. Intersection of Route 42/322 and Malaga Rd. (Rt. 322)


Figure B-36. Intersection of Route 42/322 and White Hall Rd. - Corkery Ln.

## APPENDIX C: ROUTE 23 TIMING DIRECTIVES

1903102

Page 1 of 2

Directive No. 266-03

Route 23 and County Road 515
(Vernon-Stockholm Road)
Hardyston Twp., Sussex Co.


Hours of Operation:

$$
\begin{array}{ll}
\text { 160-Second Cycle - } & \text { 5:30 A.M. to 9:00 A.M. (Monday-Friday) } \\
\text { 140-Second Cycle - } & \text { 3:00 P.M. to 7:30 P.M. (Monday-Friday) } \\
\text { 90-Second Cycle - } & \text { All other times. }
\end{array}
$$

(T-III) *From 5:30 A.M. to 9:00 A.M., Monday-Friday, an offset of 81 seconds is to be provided measured from the beginning of yellow to Route 23 at Echo Lake Road to the beginning of yellow to Route 23 traffic at this intersection.
**From 3:00 P.M. to 7:30 P.M., Monday-Friday, an offset of 82 seconds is to be provided measured from the beginning of yellow to Route 23 at Echo Lake Road to the beginning of yellow to Route 23 traffic at this intersection.
(T-I)
*** All other times (90-Second Cycle) an offset of 39 seconds is to be provided measured from the beginning of yellow to Route 23 at Echo Lake Road to the beginning of yellow to Route 23 traffic at this intersection.

The Movements 3 and 4 vehicular memories are to be disconnected and their extensions set at 2.0 seconds.

Pedestrian push button is to provide minimum calls to Movements 3 and 4.

Manual control is to be removed

1903102
Page 2 of 2

Directive No. 266-03

Route 23 and County Road 515
(Vernon-Stockholm Road)
Hardyston Twp., Sussex Co.

EMERGENCY PRE-EMPTION SEQUENCE

| Movement |  | Signals |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & 1-6, \\ & 12,13 \end{aligned}$ | 7,8,11 | 9,10 | Timing |  |
|  |  |  | Route 23 R.O.W. |  |  |  |
| 2 | Route 23 | G | R | R | - | Minimum |
|  |  |  | Upon | ilroad | uation | of 10 |
| 2 | Route 23 | G | R | R | - | Seconds |
|  | Change | Y | R | R | 6 |  |
|  | Clearance | R | R | R | 3 |  |
| 3 | County Road 515 | R | G | R | 10 |  |
|  | Change | R | Y | R | 3 |  |
|  | Clearance | R | R | R | 3 |  |
| 2 | Route 23 (Rail R.O.W.) | G | R | R | - | (Hold until released) |
|  |  |  | Resume Normal Operation |  |  |  |
|  |  |  | Ramp 515 R.O.W. |  |  |  |
| 3 | County Road 515 | R | G | R | , | Minimum |
|  |  |  | Upon Railroad Actuation |  |  |  |
|  | County Road 515 | R | G | R | - | 10 Seconds |
|  | Change | R | Y | R | 3 |  |
|  | Clearance | R | R | R | 3 |  |
| 2 | Route 23 (Rail R.O.W.) | G | R | R | - | (Hold until released) |
|  |  |  | Resume Normal Operation |  |  |  |
|  |  |  | Ramp "CR-A" R.O.W. |  |  |  |
| 4 | Ramp "CR-A" | R | R |  |  | Total |
|  |  |  | Upon Railroad Actuation |  |  |  |
| 4 | Ramp "CR-A" | R | R | G | - | 10 Seconds |
|  | Change | R | R | Y | 6 |  |
|  | Clearance | R | R | R | 3 |  |
| 3 | County Road 515 | R | G | R | 10 |  |
|  | Change | R | Y | R | 3 |  |
|  | Clearance | R | R | R | 3 |  |
| 2 | Route 23 (Rail R.O.W.) | G | R | R | - | (Hold until released) |
|  |  |  | Resume Normal Operation |  |  |  |

Route 23 and Canistear Road West Milford Twp., Passaic Co.

Directive No. 265-03

(T-III) *From 5:30 A.M. to 9:00 A.M., Monday-Friday, an offset of 122 seconds is to be measured from the beginning of yellow to Route 23 at Echo Lake Road to the beginning of yellow to Route 23 at this intersection.
(T-II) **From 3:00 P.M. to 7:30 P.M., Monday-Friday, an offset of 15 seconds is to be measured from the beginning of yellow to Route 23 at Echo Lake Road to the beginning of yellow to Route 23 at this intersection.
(T-I) ***An offset of 80 seconds is to be measured from the beginning of yellow to Route 23 at Echo Lake Road to the beginning of yellow to Route 23 at this intersection.

The memory is to be disconnected for Phase B and the vehicle extension time is to be set at 2 seconds.

Actuation of pedestrian push button is to guarantee 15 seconds of green time during Phase $B$.
Phase A recall shall be in the "ON" position.
Phase B recall is to be in the "OFF" position.

Manual control is to be disconnected.

| Hours of Operation: | 160-second cycle is to be in effect from 5:30 A.M. to 9:00 A.M., Monday-Friday. <br>  <br>  <br> 140-second cycle is to be in effect from 3:00 P.M. to 7:30 P.M., Monday-Friday. <br> 90-second cycle is to be in effect all other times. |
| :--- | :--- |
| Emergency Flashing Operation: $\quad$Flash yellow to Route 23 (Signal Faces \#1-8). |  |
|  | Flash red to Canistear Road (Signal Faces \#9-12). |

Route 23 and Reservoir Road
West Milford Twp., Passaic Co.

Directive No. 264-03

|  |  | Signals |  | Timing |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1-9 | 10-14 | 90 Seconds |  | 140 Seconds |  | $\begin{gathered} \text { III } \\ 160 \text { Seconds } \end{gathered}$ |  |
| Phase |  |  |  |  |  |  |  |  |  |
| A. | Route 23 R.O.W. | G | R | 70 | - 61 | 120 | - | 103 | 140-128 |
|  | Change | Y | R | 6 | *** | 6 | ** |  | 6 * |
|  | Clearance | R | R | 2 |  | 2 |  |  | 2 |
| B. | Reservoir Road R.O.W. | R | G | 7 | - 16 | 7 | - | 24 | 7-19 |
|  | Change | R | Y | 3 |  | 3 |  |  | 3 |
|  | Clearance | R | R | 2 |  | 2 |  |  | 2 |

(T-III) *From 5:30 A.M. to 9:00 A.M., Monday-Friday, an offset of 24 seconds is to be measured from the beginning of yellow to Route 23 at Echo Lake Road to the beginning of yellow to Route 23 at this intersection.
(T-II) **From 3:00 P.M. to 7:30 P.M., Monday-Friday, an offset of 65 seconds is to be measured from the beginning of yellow to Route 23 at Echo Lake Road to the beginning of yellow to Route 23 at this intersection.
(T-I) $\quad{ }^{* * *}$ An offset of 80 seconds is to be measured from the beginning of yellow to Route 23 at Echo Lake Road to the beginning of yellow to Route 23 at this intersection.

The memory is to be disconnected for Phase B and the vehicle extension time is to be set at $\mathbf{2}$ seconds.

Actuation of pedestrian push button is to guarantee 15 seconds of green time during Phase $B$.
Phase A recall shall be in the "ON" position.
Phase B recall is to be in the "OFF" position.

Manual control is to be disconnected.

Hours of Operation:
160-second cycle is to be in effect from 5:30 A.M. to 9:00 A.M., Monday-Friday.
140-second cycle is to be in effect from 3:00 P.M. to 7:30 P.M., Monday-Friday. 90-second cycle is to be in effect all other times.

Route 23 and Doremus Road West Milford Twp., Passaic Co.

Directive No. 263-03

| Phase |  | Signals |  |  | Timing |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1-8 | 9-12 | 90 Seconds | II 140 Seconds | III 160 Seconds |
| A. | Route 23 R.O.W. | G | R | 70-62 | 120-108 | 140-124 |
|  | Change | Y | R | 6 *** | 6 ** | 6 * |
|  | Clearance | R | R | 2 | 2 | 2 |
| B. | Doremus Road R.O.W. | R | G | $7-15$ | 7-19 | 7-23 |
|  | Change | R | Y | 3 | 3 | 3 |
|  | Clearance | R | R | 2 | 2 | 2 |
| (T-III) | *From 5:30 A.M. to 9:00 A.M., Monday-Friday, an offset of 75 seconds is to be measured from the beginning of yellow to Route 23 at Echo Lake Road to the beginning of yellow to Route 23 at this intersection. |  |  |  |  |  |
| (T-II) | **From 3:00 P.M. to 7:30 P.M., Monday-Friday, an offset of 60 seconds is to be measured from the beginning of yellow to Route 23 at Echo Lake Road to the beginning of yellow to Route 23 at this intersection. |  |  |  |  |  |
| (T-I) | ${ }^{* * *}$ An offset of 58 seconds is to be measured from the beginning of yellow to Route 23 at Echo Lake Road to the beginning of yellow to Route 23 at this intersection. |  |  |  |  |  |

The memory is to be disconnected for Phase B and the vehicle extension time is to be set at $\mathbf{2}$ seconds.

Actuation of pedestrian push button is to guarantee 15 seconds of green time during Phase $B$.
Phase A recall shall be in the "ON" position.
Phase B recall is to be in the "OFF" position.

Manual control is to be disconnected.

Hours of Operation:
160-second cycle is to be in effect from 5:30 A.M. to 9:00 A.M., Monday-Friday.
140-second cycle is to be in effect from 3:00 P.M. to 7:30 P.M., Monday-Friday.
90 -second cycle is to be in effect all other times.

Emergency Flashing Operation:
Flash yellow to Route 23 (Signal Faces \#1-8).
Flash red to Doremus Road (Signal Faces \#9-12).

Route 23 and Paradise Road West Milford Twp., Passaic Co.

Directive No. 262-03


The memory is to be disconnected for Phase B and the vehicle extension time is to be set at $\mathbf{3}$ seconds.
Actuation of pedestrian push button is to guarantee 15 seconds of green time during Phase B.

Phase A recall shall be in the "ON" position.

Phase B recall is to be in the "OFF" position.

Manual control is to be disconnected.

Hours of Operation:
160-second cycle is to be in effect from 5:30 A.M. to 9:00 A.M., Monday-Friday.
140-second cycle is to be in effect from 3:00 P.M. to 7:30 P.M., Monday-Friday.
90 -second cycle is to be in effect all other times.
Emergency Flashing Operation:
Flash yellow to Route 23 (Signal Faces \#1-6).
Flash red to Paradise Road (Signal Faces \#7-18).

NOTE: A call on Oak Ridge Road will also call minimum green to Paradise Road.

Route 23 and Oak Ridge Road West Milford Twp., Passaic Co.

Directive No. 261-03

(T-III) *From 5:30 A.M. to 9:00 A.M., Monday-Friday, an offset of 135 seconds is to be measured from the beginning of yellow to Route 23 at Echo Lake Road to the beginning of yellow to Route 23 at this intersection.
(T-II) **From 3:00 P.M. to 7:30 P.M., Monday-Friday, an offset of 87 seconds is to be measured from the beginning of yellow to Route 23 at Echo Lake Road to the beginning of yellow to Route 23 at this intersection.
(T-I) $\quad{ }^{* * *}$ An offset of 52 seconds is to be measured from the beginning of yellow to Route $\mathbf{2 3}$ at Echo Lake Road to the beginning of yellow to Route 23 at this intersection.

The memory is to be disconnected for Phase B and the vehicle extension time is to be set at 2 seconds.

Actuation of pedestrian push button is to guarantee 15 seconds of green time during Phase $B$.

Phase A recall shall be in the "ON" position.

Phase B recall is to be in the "OFF" position.

Manual control is to be disconnected.

Hours of Operation:
160-second cycle is to be in effect from 5:30 A.M. to 9:00 A.M., Monday-Friday.
140-second cycle is to be in effect from 3:00 P.M. to 7:30 P.M., Monday-Friday.
90 -second cycle is to be in effect all other times.

Route 23 N/B and Clinton Road West Milford Twp., Passaic Co.

Directive No. 259-03

|  |  | Signal |  |  |  |  | ming |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Phase |  | 11-13 | 14-20 | $90 \mathrm{Se}$ | I <br> conds | $140 \mathrm{Se}$ | II <br> conds | $160 \text { S }$ | III conds |
| A. | Route 23 R.O.W. | G | R | 70 | - 56 | 120 | - 103 | 140 | - 123 |
|  | Change | Y | R | 6 | *** | 6 | ** | 6 | * |
|  | Clearance | R | R | 2 |  | 2 |  | 2 |  |
| B. | Clinton Road R.O.W. | R | G | 7 | - 21 | 7 | - 24 | 7 | - 24 |
|  | Change | R | Y | 3 |  | 3 |  | 3 |  |
|  | Clearance | R | R | 2 |  | 2 |  | 2 |  |

(T-III) *From 5:30 A.M. to 9:00 A.M., Monday-Friday, an offset of 110 seconds is to be measured from the beginning of yellow to Route 23 at Echo Lake Road to the beginning of yellow to Route 23 at this intersection.
(T-II) **From 3:00 P.M. to 7:30 P.M., Monday-Friday, an offset of 92 seconds is to be measured from the beginning of yellow to Route 23 at Echo Lake Road to the beginning of yellow to Route 23 at this intersection.
(T-I) ***An offset of 32 seconds is to be measured from the beginning of yellow to Route 23 at Echo Lake Road to the beginning of yellow to Route 23 at this intersection.

The memory is to be disconnected for Phase B and the vehicle extension time is to be set at $\mathbf{2}$ seconds.

Actuation of pedestrian push button is to guarantee 15 seconds of green time during Phase $B$.
Phase A recall shall be in the "ON" position.
Phase B recall is to be in the "OFF" position.

Manual control is to be disconnected.

Hours of Operation:
160-second cycle is to be in effect from 5:30 A.M. to 9:00 A.M., Monday-Friday.
140-second cycle is to be in effect from 3:00 P.M. to 7:30 P.M., Monday-Friday.
90 -second cycle is to be in effect all other times.

## Emergency Flashing Operation:

Flash yellow to Route 23 (Signal Faces \#11-13).
Flash red to Clinton Road (Signal Faces \#14-20).

Route 23 S/B and Clinton Road West Milford Twp., Passaic Co.

Directive No. 260-03

|  |  | Signals |  | Timing |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Phase |  | 11-13 | 14-20 | 90 Se | I conds | II 140 Seconds | III 320 Seconds |
| A. | Route 23 R.O.W. | G | R | 70 | - 56 | 120-103 | 300-283 |
|  | Change | Y | R | 6 | *** | 6 ** | 6 * |
|  | Clearance | R | R | 2 |  | 2 | 2 |
| B. | Clinton Road R.O.W. | R | G | 7 | - 21 | 7-24 | 7-24 |
|  | Change | R | Y | 3 |  | 3 | 3 |
|  | Clearance | R | R | 2 |  | 2 | 2 |

(T-III) *From 5:30 A.M. to 9:00 A.M., Monday-Friday, an offset of 110 seconds is to be measured from the beginning of yellow to Route 23 at Echo Lake Road to the beginning of yellow to Route 23 at this intersection.
(T-II) **From 3:00 P.M. to 7:30 P.M., Monday-Friday, an offset of 92 seconds is to be measured from the beginning of yellow to Route 23 at Echo Lake Road to the beginning of yellow to Route 23 at this intersection.
(T-I) ***An offset of 32 seconds is to be measured from the beginning of yellow to Route 23 at Echo Lake Road to the beginning of yellow to Route 23 at this intersection.

The memory is to be disconnected for Phase B and the vehicle extension time is to be set at $\mathbf{2}$ seconds.

Actuation of pedestrian push button is to guarantee 15 seconds of green time during Phase $B$.
Phase A recall shall be in the "ON" position.
Phase B recall is to be in the "OFF" position.

Manual control is to be disconnected.

Hours of Operation:
160-second cycle is to be in effect from 5:30 A.M. to 9:00 A.M., Monday-Friday.
140-second cycle is to be in effect from 3:00 P.M. to 7:30 P.M., Monday-Friday.
90 -second cycle is to be in effect all other times.

## Emergency Flashing Operation:

Flash yellow to Route 23 (Signal Faces \#11-13).
Flash red to Clinton Road (Signal Faces \#14-20).

Route 23 N/B and LaRue Road Jefferson Twp., Morris Co.

Directive No. 258-03

|  |  | Signals |  |  | Timing |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Phase |  | 1-2,11 | 3-10 | 90 Seconds | II 140 Seconds | III 160 Seconds |
| A. | Route 23 S/B R.O.W. | G | R | $70-59$ | 120-108 | 140-127 |
|  | Change | Y | R | 6 *** | 6 ** | 6 * |
|  | Clearance | R | R | 2 | 2 | 2 |
| B. | LaRue Road R.O.W. | R | G | $7-18$ | 7-19 | 7-20 |
|  | Change | R | Y | 3 | 3 | 3 |
|  | Clearance | R | R | 2 | 2 | 2 |
| (T-III) | *From 5:30 A.M. to 9:00 A.M., Monday-Friday, an offset of 129 seconds is to be measured from the beginning of yellow to Route 23 at Echo Lake Road to the beginning of yellow to Route 23 at this intersection. |  |  |  |  |  |
| (T-II) | **From 3:00 P.M. to 7:30 P.M., Monday-Friday, an offset of 97 seconds is to be measured from the beginning of yellow to Route 23 at Echo Lake Road to the beginning of yellow to Route 23 at this intersection. |  |  |  |  |  |
| (T-I) | ${ }^{* * *}$ An offset of 8 seconds is to be measured from the beginning of yellow to Route 23 at Echo Lake Road to the beginning of yellow to Route 23 at this intersection. |  |  |  |  |  |

The memory is to be disconnected for Phase B and the vehicle extension time is to be set at $\mathbf{2}$ seconds.
Actuation of pedestrian push button is to guarantee 15 seconds of green time during Phase $B$.

Phase A recall shall be in the "ON" position.

Phase B recall is to be in the "OFF" position.

Manual control is to be disconnected.

Hours of Operation:
160-second cycle is to be in effect from 5:30 A.M. to 9:00 A.M., Monday-Friday.
140-second cycle is to be in effect from 3:00 P.M. to 7:30 P.M., Monday-Friday.
90 -second cycle is to be in effect all other times.
Emergency Flashing Operation:
Flash yellow to Route 23 S/B (Signal Faces \#1,2,11).
Flash red to LaRue Road (Signal Faces \#3-10).

Route 23 S/B and LaRue Road Jefferson Twp., Morris Co.

Directive No. 257-03

## BACKGROUND CYCLES

|  |  | Signals |  | Timing |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Phase |  | 1-2,11 | 3-10 | 90 Se | I <br> conds | II 140 Seconds | III 160 Seconds |
| A. | Route 23 S/B R.O.W. | G | R | 70 | - 59 | 120-108 | 140-127 |
|  | Change | Y | R | 6 | *** | 6 ** | 6 * |
|  | Clearance | R | R | 2 |  | 2 | 2 |
| B. | LaRue Road R.O.W. | R | G | 7 | - 18 | 7-19 | 7-20 |
|  | Change | R | Y | 3 |  | 3 | 3 |
|  | Clearance | R | R | 2 |  | 2 | 2 |

(T-III) *From 5:30 A.M. to 9:00 A.M., Monday-Friday, an offset of 129 seconds is to be measured from the beginning of yellow to Route 23 at Echo Lake Road to the beginning of yellow to Route 23 at this intersection.
(T-II) **From 3:00 P.M. to 7:30 P.M., Monday-Friday, an offset of 97 seconds is to be measured from the beginning of yellow to Route 23 at Echo Lake Road to the beginning of yellow to Route 23 at this intersection.
(T-I)
*** An offset of 8 seconds is to be measured from the beginning of yellow to Route 23 at Echo Lake Road to the beginning of yellow to Route 23 at this intersection.

The memory is to be disconnected for Phase B and the vehicle extension time is to be set at $\mathbf{2}$ seconds.

Actuation of pedestrian push button is to guarantee 15 seconds of green time during Phase $B$.
Phase A recall shall be in the "ON" position.
Phase B recall is to be in the "OFF" position.

Manual control is to be disconnected.

Hours of Operation:
160-second cycle is to be in effect from 5:30 A.M. to 9:00 A.M., Monday-Friday. 140-second cycle is to be in effect from 3:00 P.M. to 7:30 P.M., Monday-Friday. 90 -second cycle is to be in effect all other times.

Emergency Flashing Operation:
Flash yellow to Route 23 S/B (Signal Faces \#1,2,11).
Flash red to LaRue Road (Signal Faces \#3-10).

Route 23 and Old Route 23
(Kanouse Road)
West Milford Twp., Passaic Co.

Directive No. 256-03

## BACKGROUND CYCLES

|  |  | Signals |  |  | Timing |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Phase |  | $\begin{aligned} & 1-3, \\ & 6,7,11 \end{aligned}$ | $\begin{aligned} & 4,5 \\ & 8-10 \end{aligned}$ | 90 Seconds | II 140 Seconds | III 160 Seconds |
| A. | Route 23 R.O.W. | G | R | 70-56 | 120-103 | 140-125 |
|  | Change | Y | R | 6 *** | 6 ** | 6 * |
|  | Clearance | R | R | 2 | 2 | 2 |
| B. | Old Route 23 R.O.W. | R | G | $7-21$ | 7-24 | 7-22 |
|  | Change | R | Y | 3 | 3 | 3 |
|  | Clearance | R | R | 2 | 2 | 2 |
| (T-III) | *From 5:30 A.M. to 9:00 A.M., Monday-Friday, an offset of 73 seconds is to be measured from the beginning of yellow to Route 23 at Echo Lake Road to the beginning of yellow to Route 23 at this intersection. |  |  |  |  |  |
| (T-II) | **From 3:00 P.M. to 7:30 P.M., Monday-Friday, an offset of 85 seconds is to be measured from the beginning of yellow to Route 23 at Echo Lake Road to the beginning of yellow to Route 23 at this intersection. |  |  |  |  |  |
| (T-I) | ${ }^{* * *}$ An offset of 44 seconds is to be measured from the beginning of yellow to Route 23 at Echo Lake Road to the beginning of yellow to Route 23 at this intersection. |  |  |  |  |  |

The memory is to be disconnected for Phase B and the vehicle extension time is to be set at 4 seconds.

Actuation of pedestrian push button is to guarantee 15 seconds of green time during Phase $B$.

Phase A recall shall be in the "ON" position.

Phase B recall is to be in the "OFF" position.

Manual control is to be disconnected.

## Hours of Operation:

160-second cycle is to be in effect from 5:30 A.M. to 9:00 A.M., Monday-Friday. 140-second cycle is to be in effect from 3:00 P.M. to 7:30 P.M., Monday-Friday. 90 -second cycle is to be in effect all other times.

Emergency Flashing Operation:
Flash yellow to Route 23 (Signal Faces \#1-3,6,7,11).
Flash red to Old Route 23 (Signal Faces \#4,5,8-10).

Route 23 and Echo Lake Road West Milford Twp., Passaic Co.

Directive No. 255-03

## BACKGROUND CYCLES

|  |  | Signals |  |  | Timing |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Phase |  | $\begin{aligned} & 1-5, \\ & 12-18 \end{aligned}$ | $\begin{aligned} & 6-11 \\ & 19-26 \end{aligned}$ | 90 Seconds | II 140 Seconds | III 160 Seconds |
| A. | Route 23 R.O.W. | G | R | 67-60 | 117-115 | 137-120 |
|  | Change | Y | R | 6 *** | 6 ** | 6 * |
|  | Clearance | R | R | 2 | 2 | 2 |
| B. | Echo Lake Road R.O.W. | R | G | 10-17 | 10-12 | 10-27 |
|  | Change | R | Y | 3 | 3 | 3 |
|  | Clearance | R | R | 2 | 2 | 2 |
| (T-III) | *From 5:30 AM to 9:00 AM, Monday-Friday, an offset of 0 seconds is to be measured from the beginning of yellow to Route 23 at this intersection. |  |  |  |  |  |
| (T-II) | **From 3:00 PM to 7:30 PM, Monday-Friday, an offset of 0 seconds is to be measured from the beginning of yellow to Route 23 at this intersection. |  |  |  |  |  |
| (T-I) | ***An offset of 0 seconds at this intersection. | is to be | measur | from the begin | ning of yellow | Route 23 |

The memory is to be disconnected for Phase B and the vehicle extension time is to be set at $\mathbf{3}$ seconds.
Actuation of pedestrian push button is to guarantee 15 seconds of green time during Phase $B$.

Phase A recall shall be in the "ON" position.

Phase B recall is to be in the "OFF" position.
Manual control is to be disconnected.

## Hours of Operation:

160-Second Cycle is to be in effect from 5:30 AM to 9:00 AM, Monday-Friday.
140-Second Cycle is to be in effect from 3:00 PM to 7:30 PM, Monday-Friday.
90 -Second Cycle is to be in effect all other times.

Emergency Flashing Operation:
Flash yellow to Route 23 (Signal Faces \#1-5, 12-18).
Flash red to Echo Lake Road (Signal Faces \#6-11, 19-26).

Route 23 and Center Court - Ramp "DD" Butler Boro., Morris Co.

## BACKGROUND CYCLES

Phase
1)
2)
(T-I) From 5:30-9:30 A.M., Monday - Friday, an offset of 92 seconds is to be measured from the beginning of yellow to Route 23 at Boonton Avenue to the beginning of yellow to Route 23 at this intersection.
(T-III)
${ }^{* * *}$ An offset of 83 seconds is to be measured from the beginning of yellow to Route 23 at Boonton Avenue to the beginning of yellow to Route 23 at this intersection.

## Vehicle Extension-2 Seconds

Recall - Off

Memory - Off
Pedestrian actuation is to provide a minimum green of 27 seconds to Phase 2.

The manual cord is to be disconnected.

Flashing Operation:
Indications \#1-6 / Yellow
Indications \#7-11 / Red

Hours of Operation:
The 150-second cycle is to be in effect 5:30-9:30 a.m. and 3:00-7:30 P.M., Monday - Friday. The 90 - second cycle is to be in effect all other times.

Flashing "Red Signal Ahead" sign is to begin flashing 11 seconds prior to the beginning of yellow to Route 23 at this intersection and stop flashing upon the beginning of green to Route 23 at this intersection.

Route 23 Ramp "AA" - Kakeout Connector and Kinnelon Road Kinnelon Boro., Morris Co.

## BACKGROUND CYCLES



Vehicle Actuation

| 1) | Kinnelon Road | G | R | DW | 131 | - 109 | 131-113 | 71 | - 61 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Change | Y | R | DW | 5 | * | 5 ** | 5 | *** |
|  | Clearance | R | R | DW | 2 |  | 2 | 2 |  |
| 2) | Ramp "AA" - Kakeout Connector | R | G | DW | 7 | - 29 | 7-25 | 7 | - 17 |
|  | Change | R | Y | DW | 3 |  | 3 | 3 |  |
|  | Clearance | R | R | DW | 2 |  | 2 | 2 |  |

Pedestrian Actuation (Ramp "AA")

| 1) | Kinnelon Road | G | R | DW | 121 | - 109 | 121-113 | 61 | - 57 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Change | Y | R | DW | 5 | * | 5 ** | 5 | *** |
|  | Clearance | R | R | DW | 2 |  | 2 | 2 |  |
| 2) | Ramp "AA" - Kakeout Connector | R | G | W | 7 |  | 7 | 7 |  |
|  | Pedestrian Clearance | R | G | FDW | 10 |  | 10 | 10 |  |
|  | Vehicle Clearance | R | G | DW | 0 | - 12 | 0-8 | 0 | - 4 |
|  | Change | R | Y | DW | 3 |  | 3 | 3 |  |
|  | Clearance | R | R | DW | 2 |  | 2 | 2 |  |
|  | Emergency Flashing Operation | Y | R | DARK |  |  |  |  |  |

(T-I) *From 5:30-9:30 A.M., Monday - Friday, an offset of 70 seconds is to be measured from the beginning of yellow to Route 23 at Boonton Avenue to the beginning of yellow to Kinnelon Road at this intersection.
(T-II) **From 3:00-7:30 P.M., Monday - Friday, an offset of 77 seconds is to be measured from the beginning of yellow to Route 23 at Boonton Avenue to the beginning of yellow to Kinnelon Road at this intersection.
(T-III) ***All other time, an offset of 46 seconds is to be measured from the beginning of yellow to Route 23 at Boonton Avenue to the beginning of yellow to Kinnelon Road at this intersection.

Vehicle Extension-2 Seconds

Recall - Off
Memory - Off

The manual cord is to be disconnected.

Route 23 \& Kiel Avenue-Kinnelon Road Butler Boro., Morris Co.

## BACKGROUND CYCLES

| Phase |  | Signals |  |  |  | Timing |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & 1-6, \\ & 19,20 \end{aligned}$ | 7-10 | 11-14 | 15-18 | $\begin{gathered} \text { I } \\ 150 \mathrm{Sec} . \end{gathered}$ | $\begin{gathered} \text { II } \\ 150 \text { Sec. } \end{gathered}$ |  | III <br> Sec. |
| 1) | Route 23 ROW | G | R | W | DW | 109-85 | 109-74 | 49 | - 29 |
|  | Pedestrian Clearance | G | R | FDW | DW | 19 | 19 | 19 |  |
|  | Change | Y | R | DW | DW | 5 * | 5 ** | 5 | *** |
|  | Clearance | R | R | DW | DW | 2 | 2 | 2 |  |
| 2) | Kinnelon Rd.-Kiel Ave. ROW | R | G | DW | DW | 7-31 | 7-42 | 7 | 27 |
|  | Change | R | Y | DW | DW | 5 | 5 | 5 |  |
|  | Clearance | R | R | DW | DW | 3 | 3 | 3 |  |
| Pedestrian Actuation |  |  |  |  |  |  |  |  |  |
| 1) | Route 23 ROW | G | R | W | DW | 76 | 76-74 | 16 |  |
|  | Pedestrian Clearance | G | R | FDW | DW | 19 | 19 | 19 |  |
|  | Change | Y | R | DW | DW | 5 | 5 | 5 |  |
|  | Clearance | R | R | DW | DW | 2 | 2 | 2 |  |
| 2) | Kinnelon Rd.-Kiel Ave. ROW | R | G | DW | W | 7 | 7 | 7 |  |
|  | Pedestrian Clearance | R | G | DW | FDW | 33 | 33 | 33 |  |
|  | Vehicle Extension | R | G | DW | DW | 0 | 0-2 | 0 |  |
|  | Change | R | Y | DW | DW | 5 | 5 | 5 |  |
|  | Clearance | R | R | DW | DW | 3 | 3 | 3 |  |

I *From 5:30-9:30 A.M., Monday - Friday, an offset of 93 seconds is to be measured from the beginning of yellow to Route 23 at Boonton Avenue to the beginning of yellow to Route 23 at this intersection.

II **From 3:00-7:30 P.M., Monday - Friday, an offset of 88 seconds is to be measured from the beginning of yellow to Route 23 at Boonton Avenue to the beginning of yellow to Route 23 at this intersection.

III ***An offset of 52 seconds is to be measured from the beginning of yellow to Route 23 at Boonton Avenue to the beginning of yellow to Route 23 at this intersection.

## Actuated Phases:

Vehicle Extension - 2 Seconds
Recall - Off
Memory - Off
The manual control is to be disconnected.

Flashing Operation:
Indications \#1-6, 19, 20 / Yellow
Indications \#7-10 / Red
Indications \#11-18 / Dark

Hours of Operation:
The 150-second cycle is to be in effect 5:30-9:30 A.M. and 3:00-7:30 P.M., Monday - Friday.
The 90 -second cycle is to be in effect all other times.

(T-I) *From 5:30-9:30 A.M., Monday - Friday, an offset of 112 seconds is to be measured from the beginning of yellow to Route 23 at Boonton Avenue to the beginning of yellow to Kiel Avenue at this intersection.
(T-II) **From 3:00-7:30 P.M., Monday - Friday, an offset of 73 seconds is to be measured from the beginning of yellow to Route 23 at Boonton Avenue to the beginning of yellow to Kiel Avenue at this intersection.
(T-III) ***All other time, an offset of 16 seconds is to be measured from the beginning of yellow to Route 23 at Boonton Avenue to the beginning of yellow to Kiel Avenue at this intersection.

## Vehicle Extension-2 Seconds

Recall - Off

Memory - Off
The manual cord is to be disconnected.
Flashing Operation:
Indications \#21-24 / Yellow
Indications \#25, 26 / Red
Indications \#27, 28 / Dark

Hours of Operation:
The 150-second cycle is to be in effect 5:30-9:30 A.M. and 3:00-7:30 P.M., Monday - Friday.
The 90 -second cycle is to be in effect all other times.

| 1405118 | Directive No. 250-03 |
| :--- | :--- |
| Page 1 of 2 | Route 23 and Ramp "Y"-Adalist Street <br> Butler Boro., Morris Co. |

## BACKGROUND CYCLES

| Phase |  | Signals |  |  |  |  |  |  |  | Timing |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1-3 | 4,5 | 6-8 | 9,10 | 13-15 | 18,19 | $\underline{20,21}$ | $\begin{gathered} \text { I } \\ 150 \text { Sec. } \end{gathered}$ | $\begin{gathered} \text { II } \\ 150 \text { Sec. } \end{gathered}$ |  | III <br> Sec. |
| 1 | Route 23 ROW | G | G | R | G | G | R | DW | 126-115 | 126-115 | 66 | - 58 |
|  | Outside Change | Y | G | R | G | Y | R | DW | 5 * | $5^{\text {** }}$ | 5 | *** |
|  | Inside Change | R | Y | R | Y | R | R | DW | 5 | 5 | 5 |  |
|  | Clearance | R | R | R | R | R | R | DW | 2 | 2 | 2 |  |
| 3 | Ramp "Y" ROW | R | R | G | R | R | R | DW | 7-18 | 7-18 | 7 |  |
|  | Change | R | R | Y | R | R | R | DW | 3 | 3 | 3 |  |
|  | Clearance | R | R | R | R | R | R | DW | 2 | 2 | 2 |  |

PEDESTRIAN ACTUATION

| 1 | Route 23 ROW | G | G | R | G | G | R | DW | 104 | 104 | 44 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Outside Change | Y | G | R | G | Y | R | DW | 5 | 5 | 5 |
|  | Inside Change | R | Y | R | Y | R | R | DW | 5 | 5 | 5 |
|  | Clearance | R | R | R | R | R | R | DW | 2 | 2 | 2 |
| 3 | Ramp "Y" ROW | R | R | G | R | R | R | W | 7 | 7 | 7 |
|  | Ped. Clearance | R | R | G | R | R | R | FDW | 22 | 22 | 22 |
|  | Change | R | R | Y | R | R | R | DW | 3 | 3 | 3 |
|  | Clearance | R | R | R | R | R | R | DW | 2 | 2 | 2 |

## EMERGENCY VEHICLE OPERATION

## ROW TO ROUTE 23

| Route 23 ROW | G | G | R | G | G | R | DW | 7 Min. | 7 Min. |  | 7 Min. |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Outside Change | Y | G | R | G | Y | R | DW | 5 |  | 5 | 5 |
| Inside Change | R | Y | R | G | R | R | DW | 5 |  | 5 | 5 |
| Clearance | R | R | R | G | R | R | DW | 2 | 2 | 2 |  |

Call Phase 4

ROW TO RAMP "Y"

| 3 | Ramp "Y" ROW | R | R | G | R | R | R | DW | 7 Min. | 7 Min. | 7 Min . |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Change | R | R | Y | R | R | R | DW | 3 | 3 | 3 |
|  | Clearance | R | R | R | R | R | R | DW | 2 | 2 | 2 |

Call Phase 4

PHASE 4

| Adalist St. (Emer. ROW) $\mathbf{R}$ | $\mathbf{R}$ | $\mathbf{R}$ | $\mathbf{G}$ | $\mathbf{R}$ | $\mathbf{G}$ | DW | 18 | 18 | 18 |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | ---: | ---: |
| Change | $\mathbf{R}$ | $\mathbf{R}$ | $\mathbf{R}$ | $\mathbf{G}$ | $\mathbf{R}$ | $\mathbf{Y}$ | DW | 3 | 3 | 3 |
| Clearance | $\mathbf{R}$ | $\mathbf{R}$ | $\mathbf{R}$ | $\mathbf{G}$ | $\mathbf{R}$ | $\mathbf{R}$ | DW | 5 | 5 | 5 |

Resume Normal Operation

Route 23 and Ramp " Y "-Adalist Street Butler Boro., Morris Co.

## Notes:

If call to Phase 4 during pedestrian interval of Phase 3, a minimum of 7 seconds "Walk" and 22 seconds flashing "Don't Walk" will be given in Phase 3.

Signal to rest in Phase 1.
(T-I) *From 5:30-9:30 A.M., Monday - Friday, an offset of 3 seconds is to be measured from the beginning of yellow to Route 23 at Boonton Avenue to the beginning of yellow to Route 23 at this intersection.
(T-II) **From 3:00-7:30 P.M., Monday - Friday, an offset of 31 seconds is to be measured from the beginning of yellow to Route 23 at Boonton Avenue to the beginning of yellow to Route 23 at this intersection.
(T-III) ***All other time, an offset of 11 seconds is to be measured from the beginning of yellow to Route 23 at Boonton Avenue to the beginning of yellow to Route 23 at this intersection.

Vehicle Extension-2 Seconds

Recall - Off

## Memory - Off

The manual cord is to be disconnected.

## Flashing Operation:

Indications \#1-5, 9, 10, 13-15/Yellow
Indications \#6-8, 18, 19 / Red
Indications \#20, 21 / Dark

## Hours of Operation:

The 150-second cycle is to be in effect 5:30-9:30 A.M. and 3:00-7:30 P.M., Monday Friday.
The 90-second cycle is to be in effect all other times.

Route 23 \& Boonton Avenue Butler Borough
Morris County
Directive No. 249-03

Background Cycles

(T-I) *From 5:30-9:30am, Monday - Friday, an offset of 0 seconds is to be measured from the beginning of yellow to Route 23 at this intersection.
(T-II) **From 3:00-7:30pm, Monday - Friday, an offset of 0 seconds is to be measured from the beginning of yellow to Route 23 at this intersection.
(T-III) ***An offset of 0 seconds is to be measured from the beginning of yellow to Route 23 at this intersection.
Actuated Phases: Vehicle Extension-2 Seconds
Recall - Off
Memory - Off

Hours of Operation: The 150 second cycle is to be in effect 5:30-9:30am and 3:00-7:30pm, Monday - Friday. The 90 second cycle is to be in effect all other times.

The Red Signal Ahead Electric sign is to begin flashing 21 seconds before the beginning of yellow to Route 23 at Boonton Avenue and stop flashing upon the beginning of green to Route 23 traffic at Boonton Avenue.

## 1405119

Directive No. 248-03

Route 23 and Ramp "W" - Morse Avenue Butler Boro., Morris Co.

## BACKGROUND CYCLE

Phase

| 1-6 | 7-12 | $\begin{gathered} \text { I } \\ 150 \mathrm{Sec} . \end{gathered}$ |  | II |  | $\begin{gathered} \text { III } \\ 90 \mathrm{Sec} . \end{gathered}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| G | R | 131-112 | 131 | - | 112 | 71 | - | 58 |
| Y | R | 5 * | 5 | ** |  | 5 | *** |  |
| R | R | 1 | 1 |  |  | 1 |  |  |
| R | G | 7-26 | 7 | - | 26 | 7 | - | 20 |
| R | Y | 3 | 3 |  |  | 3 |  |  |
| R | R | 3 | 3 |  |  | 3 |  |  |

(T-I) *From 5:30-9:30 A.M., Monday - Friday, an offset of 36 seconds is to be measured from the beginning of yellow to Route 23 at Boonton Avenue to the beginning of yellow to Route 23 at this intersection.
(T-II) **From 3:00-7:30 P.M., Monday - Friday, an offset of 133 seconds is to be measured from the beginning of yellow to Route 23 at Boonton Avenue to the beginning of yellow to Route 23 at this intersection.
***All other time, an offset of 54 seconds is to be measured from the beginning of yellow to Route 23 at
(T-III) Boonton
Avenue to the beginning of yellow to Route 23 at this intersection.

Vehicle Extension-2 Seconds
Phase 2 - Recall - Off
Phase 2 - Memory - Off

Pedestrian actuation is to provide a minimum green of 26 seconds to Phase 2.

The manual cord is to be disconnected.

Flashing Operation:
Indications \# 1-6 / Yellow
Indications \# 7-12 / Red

Hours of Operation:
The 150-second cycle is to be in effect 5:30-9:30 A.M., and 3:00-7:30 P.M., Monday - Friday.
The 90 -second cycle is to be in effect all other times.

1405117

Page 1 of 2

Directive No. 247-03

Route 23 and Cotlass Road - Ramp T Riverdale Boro., Morris Co.

## BACKGROUND CYCLES

| Phase |  | Signals |  |  |  |  | Timing |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & 1-6, \\ & 12 \end{aligned}$ | $\begin{aligned} & 7, \\ & 8,10 \end{aligned}$ | 11,14 | 9 | 13 | $\begin{gathered} \text { I } \\ 150 \mathrm{Sec} . \end{gathered}$ | $\begin{gathered} \text { II } \\ 150 \mathrm{Sec} . \end{gathered}$ |  |  | III Sec. |
| 1 | Route 23 ROW | G | R | R | R | R | 122-114 | 122 - | 108 | 62 | - 42 |
|  | Change | Y | R | R | R | R | 5 * | 5 ** |  | 5 | *** |
|  | Clearance | R | R | R | R | R | 1 | 1 |  | 1 |  |
| 2 | Cotlass Road | R | G/<G- | R | R | G | 5-9 | 5-9 |  | 5 | - 10 |
|  | Change | R | Y | R | R | Y | 3 | 3 |  | 3 |  |
|  | Clearance | R | R | R | R | R | 3 | 3 |  | 3 |  |
| 3 | Ramp T | R | R | G/<G- | G | R | 5-9 | 5-15 |  | 5 | - 20 |
|  | Change | R | R | Y | Y | R | 3 | 3 |  | 3 |  |
|  | Clearance | R | R | R | R | R | 3 | 3 |  | 3 |  |
|  | Emergency Flash | Y | R | R | R | R | - | - |  | - |  |

(T-I) *From 5:30-9:30 A.M., Monday - Friday, an offset of 85 seconds is to be measured from the beginning of yellow to Route 23 at Boonton Avenue to the beginning of yellow to Route 23 at this intersection.
(T-II) **From 3:00-7:30 P.M., Monday - Friday, an offset of 80 seconds is to be measured from the beginning of yellow to Route 23 at Boonton Avenue to the beginning of yellow to Route 23 at this intersection.
(T-III) $\quad{ }^{* * *}$ All other time, an offset of 88 seconds is to be measured from the beginning of yellow to Route 23 at Boonton Avenue to the beginning of yellow to Route 23 at this intersection.

Vehicle Extension-2 Seconds

Phases 2/3-Recall - Off

Phases 2/3-Memory - Off

Actuation of pedestrian push-button \#1 is to provide a minimum green of 26 seconds to Phase 2.

Actuation of pedestrian push-button \#2 is to provide a minimum green of 26 seconds to Phase 3.
The manual cord is to be disconnected.

## Hours of Operation:

The 150-second cycle is to be in effect 5:30-9:30 A.M. and 3:00-7:30 P.M., Monday - Friday.
The 90 -second cycle is to be in effect all other times.

1405117

Page 2 of 2

Directive No. 247-03

Route 23 and Cotlass Road - Ramp T
Riverdale Boro., Morris Co.

Pre-Emption Notes

1. The intersection shall have a controller with internal pre-emption features.
2. Remote control pre-emption is permitted from the Route 23 northbound approach and the Cotluss Road - Ramp T westbound approach.
3. The device shall only select a phase displayed in the normal operation.
4. The controller shall guarantee all vehicular and pedestrian minimums, change and clearance times.
5. Normal operation shall commence at the point in the sequence where pre-emption was terminated and coordination shall be re-established.
6. A minimum guaranteed green time of 25 seconds shall be provided to either approach before servicing a pre-emption ROW to another direction (phase).
7. Pre-emption from one of the permitted approaches shall provide ROW only to that approach.
8. Pre-emption shall occur by remote control.
9. Pre-emption ROW on either approach is to be held until the emergency vehicle clears the intersection.

## APPENDIX D: ROUTE 42/322 TIMING DIRECTIVES

| 0803104 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Route 42 \& Shopping Center Drive/ Jughandle/ Bus Garage Access |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
| Washington Township |  |  |  |  |  |  |  |  |
| Gloucester County 110/90 Second Background Cycle |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
| SIGNAL FACES |  |  |  |  |  |  |  |  |
| PHASE |  |  | 9,10, |  | $\underset{A}{\text { TIME }}$ | $\begin{gathered} \text { TIME } \\ \mathbf{B} \end{gathered}$ | $\underset{\mathrm{C}}{\mathrm{TIME}}$ | $\underset{\mathrm{D}}{\text { TIME }}$ |
|  |  | 1-8 | 11,13 | 12,14,15 | 110-SEC. | 110-SEC. | 110-SEC. | 90-SEC. |
| A. | Route 42 | G | R | R | 78-72 | 78-70 | 78-73 | 58-53 |
|  | Change | Y | R | R | 6 | 6 | 6 | 6 |
|  | Clearance | R | R | R | 2 | 2 | 2 | 2 |
| B. | Shopping Center Drive and Jughandles | R | G | R | 7-13 | 7-15 | 7-12 | 7-12 |
|  | Change | R | Y | R | 3 | 3 | 3 | 3 |
|  | Clearance | R | R | R | 2 | 2 | 2 | 2 |
| c. | Bus Garage | R | R | G | 7 | 7 | 7 | 7 |
|  | Change | R | R | Y | 3 | 3 | 3 | 3 |
|  | Clearance | R | R | R | 2 | 2 | 2 | 2 |
|  | EMERGENCY FLASH | Y | R | R | - | - | - | - |

## HOURS OF

OPERATION

| Cycle <br> Length <br> (second <br> s) | Offset <br> (seconds) |
| :---: | :---: |
| 110 | 0 |
| 110 | 0 |
| 110 | 0 |
| 90 | 0 |

Offsets (in seconds) are measured from the beginning of yellow to Route 42 traffic at this intersection.

The manual control is to be disconnected.

The memory circuit is to be disconnected and the vehicle interval is to be $\mathbf{2}$ seconds for Phase $B$. The memory circuit is to be disconnected and the vehicle interval is to be 5 seconds for Phase $C$.

Actuation of a pedestrian push button shall guarantee 20 seconds of green time to Phase B.

## 0803103

Route 42 \& Greentree Road (County Road 651)
Washington Township
Gloucester County
110/90 Second Background Cycle


Offsets (in seconds) are measured from the beginning of yellow to Route 42 traffic at Shopping Center Drive/Bus Garage Access to the beginning of yellow to Route 42 traffic at this intersection.

An actuation of pedestrian push buttons will operate signal head \#15 and place a call for Phase C (both vehicle and pedestrian Intervals)
The memory circuit is to be disconnected, and the vehicle interval is to be set at $\mathbf{2}$ seconds for Phases $B$ and $C$.
The manual control is to remain connected.
The controller is to be capable of skipping phases not actuated.

0803102
Route 42 \& Whitman Drive
Washington Township
Gloucester County
110/90 Second Background Cycle

|  |  | SIGNAL FACES |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PHASE |  |  |  |  | TIME A | $\begin{gathered} \text { TIME } \\ \text { B } \end{gathered}$ | TIME C | $\underset{\mathrm{D}}{\text { TIME }}$ |
|  |  | 1-8 | 9,10 | 11-13 | 110 SEC. | 110 SEC. | 110 SEC. | 90 SEC. |
| A. | Route 42 | G | R | R | 79-70 | 79-69 | 79-73 | 59-46 |
|  | Change | Y | R | R | 5 | 5 | 5 | 5 |
|  | Clearance | R | R | R | 2 | 2 | 2 | 2 |
| B. | Jughandle | R | G | R | 7-12 | 7-8 | 7-12 | 7-15 |
|  | Change | R | Y | R | 3 | 3 | 3 | 3 |
|  | Clearance | R | R | R | 2 | 2 | 2 | 2 |
| C. | Whitman Drive | R | R | G | 7-11 | 7-16 | 7-8 | 7-12 |
|  | Change | R | R | Y | 3 | 3 | 3 | 3 |
|  | Clearance | R | R | R | 2 | 2 | 2 | 2 |
|  | EMERGENCY FLASH | Y | R | R | - | - | - | - |


|  | Hours of Operation | Cycle Length | Offset (Seconds) |
| :--- | :--- | :---: | :---: |
| TIME A | 6 AM - 10 AM M-F | 110 | 78 |
|  |  |  |  |
| TIME B | 10AM - 3 PM M-F | 110 | 19 |
|  |  <br> Sun |  |  |
| TIME C | 3PM-7 PM M-F | 110 | 44 |
|  |  |  |  |
| TIME D | All Other Times | 90 | 34 |

Offsets (in seconds) are measured from the beginning of yellow to Route 42 traffic at Shopping Center Drive/Bus Garage Access to the beginning of yellow to Route 42 traffic at this intersection.
The memory circuits are to be disconnected.
The manual control is to be connected.
The vehicle interval is to be 2 seconds.

Actuation of a pedestrian push button shall guarantee 21 seconds of green time to Phase B.

0803107
Route 42 Ganttown Road Shopping Center Drive
Washington Twp.
Washington Twp.
Gloucester County


|  | Hours of Operation | Cycle <br> Length |  | Offset <br> (Seconds) |
| :---: | :---: | :---: | :---: | :---: |
| TIME A | 6 AM - 10 AM M-F | 110 |  | 92 |
|  |  |  |  |  |
| TIME B | 10AM - 3 PM M-F | 110 |  | 32 |
|  | 8AM-6PM, Sat\& Sun |  |  |  |
| Time C | 3PM-7 PM M-F | 110 |  | 75 |
|  |  |  |  |  |
| Time D | All Other Times | 90 |  | 58 |

Offsets (in seconds) are measured from the beginning of yellow to Route 42 traffic at Shopping Center Drive/Bus Garage Access to the beginning of yellow to Route 42 traffic at this intersection.

The manual control and memory circuits are to be disconnected.
The vehicle interval is to be 2 seconds.

The left-turn slots (Phase A) are to be separate phases but concurrently timed if actuation occurs in both slots. Each left-turn slot is to have the capability of terminating or extending independently of each other, thereby reverting the timing to the non-conflicting Phase B movement.

080312
Route 42 \& Johnson Road
Washington Township
Gloucester County
110/90 Second Background Cycle
SIGNAL FACES

| PHASE |  | 1,2,3 | 4,5,6 | $\begin{aligned} & 7,8, \\ & 9,10 \\ & \hline \end{aligned}$ | $\begin{array}{r} 11,12 \\ 13,14, \\ \hline \underline{15} \end{array}$ | $\begin{gathered} \frac{\text { TIME }}{\mathrm{A}} \\ \frac{110}{\text { sec }} \end{gathered}$ | $\begin{gathered} \text { TIME } \\ \hline \text { B } \\ \frac{110}{\text { sec }} \end{gathered}$ | $\begin{gathered} \text { TIME } \\ \frac{110}{\text { sec }} \end{gathered}$ | $\begin{gathered} \frac{\text { TIME }}{D} \\ 90 \mathrm{sec} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |
| A. | Route 42 Left Turns | <G- | G | R | R | 7-23 | 7-17 | 7-18 | 7-15 |
|  | Route 42 SB Change | <Y- | G | R | R | 5 | 5 | 5 | 5 |
|  | Route 42 SB Clearance | <R- | G | R | R | 2 | 2 | 2 | 2 |
| B. | Route 42 | <R- | G | G | R | 76-54 | 76-66 | 76-62 | 56-40 |
|  | Route 42 NB Change | $<\mathrm{R}$ - | $\mathrm{Y}(1)$ | Y | R | 5 | 5 | 5 | 5 |
|  | Route 42 NB Clearance | $<$ R- | R(1) | R | R | 2 | 2 | 2 | 2 |
| C. | Johnson Road | <R- | R | R | G | 7-13 | 7 | 7-10 | 7-15 |
|  | Change | $<$ R- | R | R | Y | 4 | 4 | 4 | 4 |
|  | Clearance | $<\mathrm{R}$ - | R | R | R | 2 | 2 | 2 | 2 |
|  | EMERGENCY FLASH | <R- | Y | Y | R |  |  |  |  |

(1) Indication to remain G if Phase C is skipped.

|  | Hours of Operation | Cycle <br> Length | Offset <br> (Seconds) |
| :---: | :---: | ---: | ---: |
| Time A | 6 AM -10 AM M-F | 110 | 78 |
|  |  |  |  |
| Time B | 10AM - 3 PM M-F | 110 | 18 |
|  | 8AM-6PM, Sat\& Sun |  |  |
| Time C | 3PM-7 PM M-F | 110 | 65 |
|  |  |  |  |
| Time D | All Other Times | 90 | 38 |

Offsets (in seconds) are measured from the beginning of yellow to Route 42 traffic at Shopping Center Drive/Bus Garage Access to the beginning of yellow to Route 42 traffic at this intersection.

The manual control and memory circuits are to be disconnected.
The vehicle interval shall be 2 seconds.
Actuation of a pedestrian push button shall guarantee 21 seconds of green time to Phase C
An internal fire pre-emption sequence shall be provided.
Upon actuation of the emergency button, a delay of 15 seconds shall be provided before acceptance of the preemption.

Upon actuation of the fire pre-emption, all minimum green, yellow change, red clearance and pedestrain intervals shall be guaranteed followed by 40 seconds of green time to signal heads numbered 11,12 and 15 .

The phasing for southbound Route 42 shall be an independent overlap, thereby omitting northbound Route 42 should a preemption occur during Phase A.
(NOTE: Phase B minimum green time to be 10 seconds.)

0803106
Route NJ 42 and Fries Mill Road (CR 655)
Washington Twp., Gloucester Co.

| Phase |  | 110/90 Second Background Cycle |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | SIGNAL FACES |  | $\begin{gathered} \text { Times } \\ \underline{A} \\ 110-\text { Sec. } \end{gathered}$ | $\begin{gathered} \text { Times } \\ \underline{\mathrm{B}} \\ 110-\mathrm{Sec} . \end{gathered}$ | $\begin{gathered} \text { Times } \\ \underline{C} \\ 110-\text { Sec. } . \end{gathered}$ | Time 90-Sec. |
|  |  | 1-6 | 7-9 |  |  |  |  |
| A) | Route NJ 42 | G | R | 82-60 | 82-65 | 82-53 | 62-56 |
|  | Change | Y | R | 5 | 5 | 5 | 5 |
|  | Clearance | R | R | 2 | 2 | 2 | 2 |
| B) | Fries Mill Road | R | G | 16-38 | 16-33 | 16-45 | 16-22 |
|  | Change | R | Y | 3 | 3 | 3 | 3 |
|  | Clearance | R | R | 2 | 2 | 2 | 2 |
|  | Emergency Flash | Y | R | - | - | - | - |

## Hours of Operation

|  | Time Period | Cycle <br> Length | Offset <br> (Seconds) |
| :---: | :---: | :---: | :---: |
| Time A | 6 AM - 10 AM M-F | 110 | 34 |
|  |  |  |  |
| Time B | 10AM - 3 PM M-F | 110 | 93 |
|  | 8AM-6PM, Sat\& Sun |  |  |
| Time C | 3PM-7 PM M-F | 110 | 28 |
| Time D | All Other Times | 90 | 85 |

Offsets (in seconds) are measured from the beginning of yellow to Route 42 traffic at Shopping Center Drive/Bus Garage Access to the beginning of yellow to Route 42 traffic at this intersection.

The memory circuit for Phase B is to be connected.
The manual control is to be disconnected.
The vehicle interval for Phase B is to be set at 5 seconds.

Signal shall operate in minimum recall to Phase B.

0803111
Route NJ 42 \& Watson Drive
Washington Township
Gloucester County
Page 1 of
2

| 110/90 Second Background Cycle |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Signal Faces |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Phase |  | 1,4,6 | 2,3,5 | 7,8,20 | 9,10,19 | 11,12 | 13,14 | 15,16 | 17,18 | $\begin{gathered} \text { Time } \\ \underline{110} \end{gathered}$ | Time 110 sec . | Time 110 sec . | $\begin{gathered} \text { Time } \\ 90 \text { sec. } \end{gathered}$ |
|  |  |  |  |  |  |  |  |  |  | $\frac{\overline{\sec }}{\mathrm{A}}$ | B | C | D |
| No Pedestrian Actuation |  |  |  |  |  |  |  |  |  |  |  |  |  |
| A. | Route 42 | <G- | <G- | R | R | R | R | DW | DW | 5-21 | 5-13 | 5-20 | 5-16 |
|  | Change | <Y- | <Y- | R | R | R | R | DW | DW | 3 | 3 | 3 | 3 |
|  | Clearance | <R- | <R- | R | R | R | R | DW | DW | 2 | 2 | 2 | 2 |
| B. | Route 42 | <R- | <R- | G | G | R | R | DW | W | 49-20 | 49-27 | 49-31 | 29-9 |
|  | Pedestrian | $<$ R- | $<$ R- | G | G | R | R | DW | FL- | 17 | 17 | 17 | 17 |
|  | Clearance Change | <R- | <R- | Y | Y | R | R | DW | DW | 5 | 5 | 5 | 5 |
|  | Clearance | <R- | <R- | R | R | R | R | DW | DW | 2 | 2 | 2 | 2 |
| C. | Watson | $<$ R- | $<$ R- | R | R | G | R | DW | DW | 7-15 | 7-20 | 7-10 | 7-13 |
|  | Drive |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Change | <R- | <R- | R | R | Y | R | DW | DW | 4 | 4 | 4 | 4 |
|  | Clearance | <R- | <R- | R | R | R | R | DW | DW | 3 | 3 | 3 | 3 |
| D. | Car Wash | <R- | <R- | R | R | R | G | DW | DW | 7-12 | 7-8 | 7 | 7-10 |
|  | Change | <R- | <R- | R | R | R | Y | DW | DW | 3 | 3 | 3 | 3 |
|  | Clearance | <R- | <R- | R | R | R | R | DW | DW | 3 | 3 | 3 | 3 |
|  | Emergency <br> Flash | <R- | <R- | Y | Y | R | R | Dark | Dark | - | - | - | - |

With Pedestrian Actuation

| Phase |  | 1,4,6 | 2,3,5 | 7,8,20 | $\underline{9,10,19}$ | 11,12 | 13,14 | 15,16 | 17,18 | $\begin{gathered} \text { Time } \\ 110 \\ \hline \end{gathered}$ | $\begin{gathered} \text { Time } \\ 110 \text { sec. } \end{gathered}$ | $\begin{gathered} \text { Time } \\ 110 \text { sec. } \end{gathered}$ | $\begin{gathered} \text { Time } \\ 90 \mathrm{sec} . \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  | $\frac{\text { sec. }}{\mathrm{A}}$ | B | C | D |
| A. | Route 42 | <G- | <G- | R | R | R | R | DW | DW | 5-21 | 5-13 | 5-15 | 5-16 |
|  | Left |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Change | $<\mathrm{Y}$ - | <Y- | R | R | R | R | DW | DW | 3 | 3 | 3 | 3 |
|  | Clearance | <R- | <R- | R | R | R | R | DW | DW | 2 | 2 | 2 | 2 |
| B. | Route 42 | <R- | <R- | G | G | R | R | DW | W | 41-20 | 41-27 | 41-31 | 21-10 |
|  | Pedestrian Clearance | <R- | <R- | G | G | R | R | DW | FL- <br> DW | 17 | 17 | 17 | 17 |
|  | Change | <R- | <R- | Y | Y | R | R | DW | DW | 5 | 5 | 5 | 5 |
|  | Clearance | <R- | <R- | R | R | R | R | DW | DW | 2 | 2 | 2 | 2 |
| C. | Watson Drive | <R- | <R- | R | R | G | R | W | DW | 7 | 7 | 7 | 7 |
|  | Pedestrian Clearance | <R- | <R- | R | R | G | R | FL-DW | DW | 8 | 8 | 8 | 8 |
|  | Vehicle Extension | $<$ R- | $<$ R- | R | R | G | R | DW | DW | 0 | 0-5 | 0 | 0 |
|  | Change | <R- | $<$ R- | R | R | Y | R | DW | DW | 4 | 4 | 4 | 4 |


|  | Clearance | <R- | <R- | R | R | R | R | DW | DW | 3 | 3 | 3 | 3 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D. | Car Wash | <R- | <R- | R | R | R | G | DW | DW | 7-12 | 7-8 | 7 | 7 |
|  | Change | <R- | <R- | R | R | R | Y | DW | DW | 3 | 3 | 3 | 3 |
|  | Clearance | <R- | <R- | R | R | R | R | DW | DW | 3 | 3 | 3 | 3 |
|  | Emergency Flash | <R- | <R- | Y | Y | R | R | Dark | Dark |  |  | - | - |

Route NJ 42 \& Watson Drive Washington Township Gloucester County

Page 2 of
2

|  | Hours of Operation | Cycle <br> Length | Offset (Seconds) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Time A | 6 AM - 10 AM M-F | $110-S e c o n d$ <br> Cycle | 82 |  |  |
| Time B | 10AM-3 PM M-F | $110-S e c o n d$ <br> Cycle |  | 33 |  |
|  | 8AM-6PM, Sat\& Sun |  |  |  |  |
| Time C | 3PM-7 PM M-F | $110-S e c o n d ~$ <br> Cycle | 90 |  |  |
| Time D | All Other Times | $90-S e c o n d$ <br> Cycle |  | 46 |  |

Offsets (in seconds) are measured from the beginning of yellow to Route 42 traffic at Shopping Center Drive/Bus Garage Access to the beginning of yellow to Route 42 traffic at this intersection.

1 The manual control and memory circuits are to be disconnected.

2 The vehicle interval is to be set at 2 seconds for actuated phases.

3 Left-turn slots (Phase A) are to be separate phases but concurrently timed if actuations occurs in both slots. Each left-turn slot is to have the capability of terminating or extending independently of each other, thereby reverting the timing to the non- conflicting Phase B movement.

## 0803108

Route NJ 42 \& Stage Coach Road / Tuckahoe
Road
Washington Township
Gloucester County
Page 1 of 2

## 110/90 Second Background Cycle

Signal Faces

| Phase |  |  |  |  |  |  | 12, | 15, | 18,19 | 22,23 |  | Time | Time | Time | Time |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1,4 | 5,6 | 2,3 | 7,8,9 | 10,11 | 13,14 | 16,17 | 20,21 | 26,27 | 24,25 | $\frac{\frac{110-}{\operatorname{Secs}}}{A}$ | $\frac{\frac{110-}{\operatorname{Secs}}}{B}$ | $\begin{gathered} \frac{110-}{\operatorname{Secs}} \\ C \end{gathered}$ | $\frac{\frac{90}{\operatorname{Sec}}}{\mathrm{D}}$ |
| A. | Normal Operation - No Pedestrian Actuation |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Route 42 Left Turns | <G- | <G- | R | R | R/-G> | R | R | DW | DW | DW | 5-6 | 5-6 | 5 | 5 |
|  | Change | <Y- | <Y- | R | R | R/-G> | R | R | DW | DW | DW | 3 | 3 | 3 | 3 |
|  | Clearance | <R- | <R- | R | R | R/-G> | R | R | DW | DW | DW | 3 | 3 | 3 | 3 |
| B. | Route 42 | $<$ R- | <R- | G | G | G/-G> | R | R | DW | W | DW | 31-19 | 31-17 | 31-17 | 11-7 |
|  | Pedestrian Clearance | <R- | <R- | G | G | G/-G> | R | R | DW | FLDW | DW | 30 | 30 | 30 | 30 |
|  | Change | <R- | <R- | Y | Y | Y/-G> | R | R | DW | DW | DW | 6 | 6 | 6 | 6 |
|  | Clearance | <R- | <R- | R | R | R/-G> | R | R | DW | DW | DW | 2 | 2 | 2 | 2 |
| C. | Stage Coach Road | <R- | <R- | R | R | R/-G> | G | R | DW | DW | DW | 7-8 | 7-8 | 7-16 | 7-9 |
|  | Change | <R- | <R- | R | R | R/-G> | Y | R | DW | DW | DW | 5 | 5 | 5 | 5 |
|  | Clearance | <R- | <R- | R | R | R/-G> | R | R | DW | DW | DW | 3 | 3 | 3 | 3 |
| D. | Tuckahoe Road | <R- | <R- | R | R | R/-G> | R | G | DW | DW | DW | 7-17 | 7-19 | 7-12 | 7-9 |
|  | Change | <R- | <R- | R | R | R/-G> | R | Y | DW | DW | DW | 5 | 5 | 5 | 5 |
|  | Clearance | <R- | <R- | R | R | R/-G> | R | R | DW | DW | DW | 3 | 3 | 3 | 3 |
|  |  | Pedestrian Actuation |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Phase |  | 1,4 | 5,6 | 2,3, | 7,8,9 | 10,11 | $\begin{gathered} 12, \\ 13,14 \\ \hline \end{gathered}$ | $\begin{gathered} 15, \\ 16,17 \\ \hline \end{gathered}$ | $\begin{array}{r} 18,19 \\ \underline{20,21} \\ \hline \end{array}$ | $\begin{aligned} & 22,23 \\ & \mathbf{2 6 , 2 7} \\ & \hline \end{aligned}$ | 24,25 | $\begin{aligned} & \text { Time } \\ & \frac{110-}{\text { Secs }} \end{aligned}$ | $\begin{aligned} & \text { Time } \\ & \frac{110-}{\text { Secs }} \end{aligned}$ | $\begin{aligned} & \text { Time } \\ & \frac{110-}{\text { Secs }} \\ & \hline C \end{aligned}$ | $\begin{gathered} \text { Time } \\ \frac{110}{\text { Sec }} \end{gathered}$ |
| A. | Route 42 Left Turns | <G- | <G- | R | R | R/-G> | R | R | DW | DW | DW | 5 | 5 | 5 | 5 |
|  | Change | $<\mathrm{Y}$ - | <Y- | R | R | R/-G> | R | R | DW | DW | DW | 3 | 3 | 3 | 3 |
|  | Clearance | <R- | <R- | R | R | R/-G> | R | R | DW | DW | DW | 3 | 3 | 3 | 3 |
| B. | Route 42 | <R- | <R- | G | G | G/-G> | R | R | DW | W | DW | 8 | 8 | 8 | 8 |
|  | Pedestrian Clearance | <R- | <R- | G | G | G/-G> | R | R | DW | FLDW | DW | 30 | 30 | 30 | 30 |
|  | Change | <R- | <R- | Y | Y | Y | R | R | DW | DW | DW | 6 | 6 | 6 | 6 |
|  | Clearance | <R- | <R- | R | R | R | R | R | DW | DW | DW | 2 | 2 | 2 | 2 |
| C. | Stage Coach Road | <R- | <R- | R | R | R | G | R | DW | DW | W | 7 | 7 | 7 | 7 |
|  | Pedestrian Clearance | <R- | <R- | R | R | R | G | R | DW | DW | FDW | 5 | 5 | 5 | 5 |
|  | Change | <R- | <R- | R | R | R | Y | R | DW | DW | DW | 5 | 5 | 5 | 5 |
|  | Clearance | <R- | <R- | R | R | R | R | R | DW | DW | DW | 3 | 3 | 3 | 3 |
| D. | Tuckahoe Road | <R- | <R- | R | R | R | R | G | W | DW | DW | 7 | 7 | 7 | 7 |
|  | Pedestrian Clearance | <R- | <R- | R | R | R | R | G | FDW | DW | DW | 18 | 18 | 18 | 18 |


| Change | <R- | <R- | R | R | R | R | Y | DW | DW | w | 5 | 5 | 5 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Clearance | <R- | <R- | R | R | R | R | R | DW | DW | DW | 3 | 3 | 3 |
| EMERGENCY FLASH | <R- | <R- | Y | Y | Y | R | R | DARK | DARK | DARK |  |  |  |

Route NJ 42 \& Stage Coach Road / Tuckahoe Road
Washington Township
Gloucester County

## Page 2 of 2

|  | Hours of Operation | Cycle <br> Length |  | Offset (Seconds) |
| :--- | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| TIME A | 6 AM - 10 AM M-F | 110 |  | 31 |
|  |  |  |  |  |
| TIME B | 10AM - 3 PM M-F | 110 |  | 88 |
|  | 8AM-6PM, Sat\& Sun |  |  |  |
| Time C | 3PM-7 PM M-F | 110 |  | 13 |
|  |  |  |  |  |
| Time D | All Other Times | 90 |  | 88 |

Offsets (in seconds) are measured from the beginning of yellow to Route 42 traffic at Shopping Center Drive/Bus Garage Access to the beginning of yellow to Route 42 traffic at this intersection.

Vehicle interval set at 2 seconds
The memory circuits OFF.
Recall OFF Phases A, C and D.
Pedestrian call on Push Button \#1 to call Phase D.
Pedestrian call on Push Button \#2 to call Phase C.
The Route 42 left-turn slots are to operate simultaneously and independently. Upon termination of either left turn phase, due to no vehicle demand, the opposing non-conflicting movements shall commence.

The manual control is to be disconnected.

## EMERGENCY FLASH:

## Route 42 Yellow.

Route 42 left-turn slots Red.
Stage Coach Road/Tuckahoe Road
Red.
Pedestrian indications DARK.

0803105
TIMING SCHEDULE
State Route 42 (Black Horse Pike) and County Route 689 (Berlin-Cross Keys Road)
Townships of Monroe and Washington, Gloucester County

## 110/90 Second Background Cycle

|  |  | Normal Operation |  |  |  | Signal Faces |  |  |  |  | $\underset{\mathbf{A}}{\text { TIME }}$ | $\underset{B}{\text { TIME }}$ | $\begin{gathered} \text { TIME } \\ \mathrm{C} \end{gathered}$ | $\underset{\mathrm{D}}{\mathrm{TIME}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | 1-3 | 4-6 | 7-9 | 10 | $\frac{11-1}{\underline{13}}$ | 14-15 | 16-17 | 18-21 | 22-25 | $\begin{aligned} & \frac{110}{\text { SEC. }} \\ & \hline \end{aligned}$ | $\begin{aligned} & \frac{110}{\text { SEC. }} \\ & \hline \end{aligned}$ | $\begin{aligned} & \frac{110}{\text { SEC. }} \\ & \hline \end{aligned}$ | $\begin{gathered} \frac{90}{\text { SEC. }} \end{gathered}$ |
| A. | Route 42 Through | G | G | R | R | R | <R- | <R- | W | DW | 52-38 | 52-31 | 52-23 | 32-17 |
|  | Pedestrian Clearance | G | G | R | R | R | <R- | <R- | FL- | DW | 18 | 18 | 18 | 18 |
|  | Change | Y | Y | R | R | R | <R- | <R- | DW | DW | 5* | 5* | 5* | 5* |
|  | Clearance | R | R | R | R | R | <R- | <R- | DW | DW | 2 | 2 | 2 | 2 |
| B. | Berlin-Cross Keys Rd WBD Lead Left | R | R | $\mathrm{G} /<\mathrm{G}$ | G | R | <R- | <R- | DW | DW | 5-10 | 5-8 | 5-15 | 5-10 |
|  | Lead Change | R | R | G/<Y- | G | R | <R- | <R- | DW | DW | 3 | 3 | 3 | 3 |
| C. | Berlin-Cross Keys Rd | R | R | G | G | G | <R- | <R- | DW | DW | 7-11 | 7-9 | 7-12 | 7 |
|  | Change | R | R | Y | Y | Y | <R- | <R- | DW | DW | 5 | 5 | 5 | 5 |
|  | Clearance | R | R | R | R | R | <R- | <R- | DW | DW | 3 | 3 | 3 | 3 |
| D. | Route 42 Left Turn | R | R | R | R | R | <G- | <G- | DW | DW | 5-10 | 5-21 | 5-19 | 5-15 |
|  | Change | R | R | R | R | R | < Y - | < Y - | DW | DW | 3 | 3 | 3 | 3 |
|  | Clearance | R | R | R | R | R | <R- | <R- | DW | DW | 2 | 2 | 2 | 2 |
|  |  | Pedestrian Actuation |  |  |  |  |  |  |  |  | TIME | TIME | TIME | TIME |
|  |  | 1-3 | 4-6 | 7-9 | 10 | 11- | 14-15 | 16-17 | 18-21 | 22-25 | 110 | 110 | 110 | 90 |
|  |  |  |  |  |  | $\underline{13}$ |  |  |  |  | SEC. | SEC. | SEC. | SEC. |
| A. | Route 42 Through | G | G | R | R | R | <R- | <R- | W | DW | 34 | 34-31 | 34-23 | 14-9 |
|  | Pedestrian Clearance | G | G | R | R | R | <R- | <R- | FLDW | DW | 18 | 18 | 18 | 18 |
|  | Change | Y | Y | R | R | R | <R- | <R- | DW | DW | 5* | 5* | 5* | 5* |
|  | Clearance | R | R | R | R | R | <R- | <R- | DW | DW | 2 | 2 | 2 | 2 |
| B. | Berlin-Cross Keys Rd WBD Lead | R | R | G/<G | G | R | <R- | <R- | DW | DW | 5 | 5 | 5 | 5-10 |
|  | Lead Change | R | R | G/<Y- | G | R | <R- | <R- | DW | DW | 3 | 3 | 3 | 3 |
| c. | Berlin-Cross Keys Rd | R | R | G | G | G | <R- | <R- | DW | w | 7 | 7 | 7 | 7 |
|  | Pedestrian Clearance | R | R | G | G | G | <R- | <R- | DW | FDW | 18 | 18 | 18 | 18 |
|  | Change | R | R | Y | Y | Y | <R- | <R- | DW | DW | 5 | 5 | 5 | 5 |
|  | Clearance | R | R | R | R | R | <R- | <R- | DW | DW | 3 | 3 | 3 | 3 |
| D. | Route 42 Left Turn | R | R | R | R | R | <G- | <G- | DW | DW | 5 | 5-12 | 5-16 | 5 |
|  | Change | R | R | R | R | R | <Y- | <Y- | DW | DW | 3 | 3 | 3 | 3 |
|  | Clearance | R | R | R | R | R | <R- | <R- | DW | DW | 2 | 2 | 2 | 2 |
|  | EMERGENCY FLASH | Y | Y | R | R | R | <R- | <R- | DARK | DARK |  |  |  |  |


|  | HOURS OF OPERATION |  | Cycle <br> Length <br> (Seconds) |  | Offset <br> (Seconds) |
| :--- | :---: | :---: | :---: | :---: | :---: |
| TIME A | 6 AM - 10 AM M-F |  | 110 |  | 76 |
|  |  |  |  |  |  |
| TIME B | 10AM - 3 PM M-F |  | 110 |  | 104 |
| TIME C | 8AM-6PM, Sat\& Sun |  | 110 |  | 16 |
|  | 3PM-7 PM M-F |  |  |  |  |
| TIME D | All Other Times |  | 90 |  | 64 |

## NOTES

1 The vehicle interval is to be set at 2 seconds for Phase B, C, and D.
2 Any unactuated phase will be skipped.
3 The left turn slots (Phase D) are to be separate phases but concurrently timed if actuation
occurs in both slots.
Each left turn slot is to have the capability of terminating or extending independently of each other, thereby reverting the timing to the non- conflicting Phase A movement.
4 Phase C shall always follow Phase B.
5 The manual control and memory circuits are to be disconnected.
*6 Offsets (in seconds) are measured from the beginning of yellow to Route 42 traffic at Shopping Center Drive/Bus Garage Access to the beginning of yellow to Route 42 traffic at this intersection.
7 Detector switching shall be provided such that the detection within the left turn slots on County Route 689 are capable of extending the Phase C through movement.
8 Phase B shall never follow Phase C.

0803110
Route 42 \&Kennedy Avenue
Monroe Township
Gloucester County

| PHASE |  | SIGNAL FACES |  |  |  | TIME | TIME | TIME |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | (SECONDS) | (SECONDS) | (SECONDS) |
|  |  | 1,2 | 3,4 | 5,6,7 | 8,9 | $\frac{A, B}{-110 \operatorname{secs}}$ | $\frac{\underline{C}}{-110 \text { secs }}$ | $\underset{90 \text { secs }}{\underline{\mathrm{D}}}$ |
| A. | Route NJ 42 NBD Lead |  |  |  |  | <G- | G | R | R | 5-15 | 5-16 | 5-10 |
|  | Change | < Y - | G | R | R | 3 | 3 | 3 |
|  | Clearance | <R- | G | R | R | 2 | 2 | 2 |
| B. | Route NJ 42 | <R- | G | G | R | 79-59 | 79-52 | 59-45 |
|  | Change | <R- | $\mathrm{Y}(1)$ | Y | R | 5 | 5 | 5 |
|  | Clearance | <R- | R(1) | R | R | 2 | 2 | 2 |
| c. | Kennedy Avenue | <R- | R | R | G | 7-17* | 7-23* | 7-16* |
|  | Change | <R- | R | R | Y | 3 | 3 | 3 |
|  | Clearance | <R- | R | R | R | 4 | 4 | 4 |
|  | EMERGENCY FLASH | <R- | Y | Y | R | -- | -- | -- |


|  | Hours of <br> Operation | Cycle <br> Length | Offset <br> (Seconds <br> ) |
| :---: | :---: | :---: | :---: |
| TIME A | 6 AM - 10 AM M-F | 110 | 10 |
| TIME B | 10AM - 3 PM M-F <br>  <br> Sun | 110 | 0 |
| TIME C | 3PM-7 PM M-F | 110 | 34 |
| TIME D | All Other Times | 90 | 32 |

Offsets (in seconds) are measured from the beginning of yellow to Route 42 traffic at Shopping Center Drive/Bus Garage Access to the beginning of yellow to Route 42 traffic at this intersection.
(1) To remain green if Phase $\mathbf{C}$ is skipped.

* Activation of a pedestrian push button shall guarantee 16 seconds of green time to Phase C.

The manual control and the memory circuits are to be disconnected.
The vehicle intervals shall be set at 2 seconds.

## 0803109

Route 42 \& Lake Avenue
Monroe Township
Gloucester County
110/90 Second Background Cycle

|  |  |  | TIME | TIME | TIME |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 110-sec. | 110-sec) | 90-sec) |
| 1,2,5,6 | 3,4,7,8 | $\underline{9,10,11,12}$ | A,B | C | D |

PHASE
A.
Route NJ 42 Left

| $<G-$ | $R$ |
| :--- | :--- |
|  | R |

R
5-17
5-16 5-12

Change
$<Y-\quad R$
R
3
3
3
Clearance
$<$ R- R
R
2
2
2
B.
Route NJ 42
$<$ R- G
R
79-55
79-54
59-45
Change
$<$ R-
R
5
5
5
Clearance <R- R R
2
2
2
C.

| Lake Ave. | $<$ R- | R | G |
| :--- | :---: | :---: | :---: |
| Change | $<R-$ | $R$ | $\mathbf{Y}$ |
| Clearance | $<R-$ | $R$ | $R$ |
| EMERGENCY FLASH | $<R-$ | $Y$ | $R$ |

7-19*
7-21*
7-14*
3
3

Hours of Operation
Cycle Length Offset
6 AM - 10 AM M-F
TIME A
TIME B
TIME C

TIME D
10AM - 3 PM M-F
8AM-6PM, Sat\& Sun
3PM-7 PM M-F
1100

All Other Times
90
0

Offsets (in seconds) are measured from the beginning of yellow to Route 42 traffic at Shopping Center Drive/Bus Garage Access to the beginning of yellow to Route 42 traffic at this intersection.

* Activation of a pedestrian push button shall guarantee 16 seconds of green time to Phase $\mathbf{C}$.

The manual control and the memory circuits are to be disconnected.

The vehicle intervals shall be set at $\mathbf{2}$ seconds.

The Phase A left turn slots shall be separate phases but concurrently times should actuations occur in both slots.

Each left turn slot shall have the capability of terminating or extending independently, thereby reverting the timing to the non-conflicting Phase B movement.

0803101
Route 42 / 322 \& Sicklerville Road (CR 536)
Monroe Township
Gloucester County

| 110/90 Second Background Cycle |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NORMAL OPERATION |  |  |  |  | time A | TIME B | TIMEC | TIME D |
| PHASE |  | Signal F | ces |  | 110 SEC. | 110 SEC. | 110 SEC. | 90 SEC. |
|  |  | 1,2,3,4, | 7,8,9,10, | 10,11,12, | CYCLE | CYCLE | CYCLE | CYCLE |
|  |  | 5,6 | 13,14 | 15 |  |  |  |  |
| A. | Route 42/322 ROW | G | R | R | 75-45 | 75-44 | 75-44 | 55-29 |
|  | Change | Y | R | R | 5 | 5 | 5 | 5 |
|  | Clearance | R | R | R | 2 | 2 | 2 | 2 |
| B. | Sicklerville Rd (CR 536) | R | G | R | 7-18* | 7-27* | 7-28* | 7-20* |
|  | Change | R | Y | R | 5 | 5 | 5 | 5 |
|  | Clearance | R | R | R | 2 | 2 | 2 | 2 |
| c. | Route US 322 | R | R | G | 7-26** | 7-18** | 7-17** | 7-20** |
|  | Change | R | R | Y | 5 | 5 | 5 | 5 |
|  | Clearance | R | R | R | 2 | 2 | 2 | 2 |

## HOURS OF OPERATION

|  | Hours of Operation | Cycle <br> Length | Offset <br> (Seconds) |
| :--- | :---: | ---: | ---: |
| TIME A | 6 AM - 10 AM M-F | 110 | 4 |
|  |  |  |  |
| TIME B | 10AM - 3 PM M-F | 110 | 7 |
|  | 8AM-6PM, Sat\& Sun |  |  |
| TIME C | 3PM-7 PM M-F | 110 | 20 |
|  |  |  |  |
| TIME D | All Other Times | 90 | 52 |

Offsets (in seconds) are measured from the beginning of yellow to Route 42 traffic at Shopping Center Drive/Bus Garage Access to the beginning of yellow to Route 42 traffic at this intersection.
The manual control and the memory circuits are to be disconnected.
The vehicle intervals shall be set at $\mathbf{2}$ seconds.
Any unactuated phase shall be skipped.
*Actuation of pedestrian push button " $B$ " shall guarantee 32 seconds of green time to Phase B.
*Actuation of pedestrian push button " C " shall guarantee 32 seconds of green time to Phase $\mathbf{C}$.

0826105
Route US 322 \& Poplar Street \& New Brooklyn Road
Monroe Township Gloucester

County

## 110/90 Second Background Cycle

| Phase |  | NORMAL OPERATION <br> Signal Faces |  |  |  |  |  |  | TIME A <br> 110 Sec <br> Cycle | TIME B <br> 110 Sec Cycle | TIME C <br> 110 Sec Cycle | TIME <br> D <br> 90 Sec <br> Cycle |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1,2, | 3,4, | 5,6 | 7,8 | $\frac{9,10}{13,14}$ | 11-12 | 15,16 |  |  |  |  |
| A. | Route US 322 | <G- | R | <G- | R | R | DW | DW | 5-9 | 5-12 | 5-13 | 5-10 |
|  | Change | <Y- | R | <Y- | R | R | DW | DW | 3 | 3 | 3 | 3 |
|  | Clearance | <R- | R | <R- | R | R | DW | DW | 2 | 2 | 2 | 2 |
| B. | Route US 322 | <R- | G | <R- | G | R | DW | W | 64-39 | 64-37 | 64-38 | 44-26 |
|  | Pedestrian Clearance | <R- | G | <R- | G | R | DW | FDW | 15 | 15 | 15 | 15 |
|  | Change | <R- | Y | <R- | Y | R | DW | DW | 5 | 5 | 5 | 5 |
|  | Clearance | $<$ R- | R | $<$ R- | R | R | DW | DW | 2 | 2 | 2 | 2 |
| c. | New Brooklyn RoadPoplar Street | <R- | R | <R- | R | G | DW | DW | 7-28 | 7-27 | 7-25 | 7-20 |
|  | Change | <R- | R | <R- | R | Y | DW | DW | 4 | 4 | 4 | 4 |
|  | Clearance | <R- | R | <R- | R | R | DW | DW | 3 | 3 | 3 | 3 |
|  | Emergency Flash | <R- | Y | <R- | Y | R | DARK | DARK |  |  |  |  |

WITH PEDESTRIAN ACTUATION
Signal Faces
TIME A TIME B TIME C TIME D
110 Sec 110 Sec 110 Sec 90 Sec
Phase

| Phase |  | $\frac{1,2,}{\text { NOR }}$ | $\frac{3,4}{\mathrm{OPE}}$ | $\frac{5,6}{\text { IION }}$ | 7,8 | $\frac{9,10}{13,14}$ | 11-12 | 15,16 | 110 Sec Cycle | 110 Sec Cycle | 110 Sec Cycle | 90 Sec Cycle |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A. | Route US 322 Lead Left | <G- | R | <G- | R | R | DW | DW | 5-9 | 5-12 | 5-13 | 5-10 |
|  | Change | $<\mathrm{Y}$ - | R | < Y - | R | R | DW | DW | 3 | 3 | 3 | 3 |
|  | Clearance | <R- | R | <R- | R | R | DW | DW | 2 | 2 | 2 | 2 |
| B. | Route US 322 | <R- | G | <R- | G | R | DW | W | 64-39 | 64-37 | 64-38 | 27-22 |
|  | Pedestrian Clearance | <R- | G | <R- | G | R | DW | FDW | 15 | 15 | 15 | 15 |
|  | Change | <R- | Y | <R- | Y | R | DW | DW | 5 | 5 | 5 | 5 |
|  | Clearance | <R- | R | <R- | R | R | DW | DW | 2 | 2 | 2 | 2 |
| C. | New Brooklyn RoadPoplar Street | <R- | R | <R- | R | G | W | DW | 7 | 7 | 7 | 7 |
|  | Pedestrian Clearance | <R- | R | <R- | R | G | FDW | DW | 17 | 17 | 17 | 17 |
|  | Vehicle Extension | <R- | R | <R- | R | G | DW | DW | 0-4 | 0-3 | 0-1 | 0 |
|  | Change | <R- | R | <R- | R | Y | DW | DW | 4 | 4 | 4 | 4 |
|  | Clearance | <R- | R | $<\mathrm{R}-$ | R | R | DW | DW | 3 | 3 | 3 | 3 |
|  | Emergency Flash | <R- | Y | <R- | Y | R | DARK | DARK |  |  |  |  |

HOURS OF OPERATION

|  | Hours of Operation |  | Cycle Length | Offset Seconds) |
| :--- | :--- | :--- | :--- | :--- |
| TIME A | 6 AM - 10 AM M-F |  | 110 | 104 |
|  |  |  |  |  |
| TIME B | 10AM - 3 PM M-F |  | 110 | 100 |
|  | 8AM-6PM, Sat\& Sun |  |  |  |
| TIME C | 3PM-7 PM M-F |  | 110 | 12 |
|  |  |  |  |  |
| TIME D | All Other Times |  | 90 | 24 |

Offsets (in seconds) are measured from the beginning of yellow to Route 42 traffic at Shopping Center Drive/Bus Garage Access to the beginning of yellow to Route 42 traffic at this intersection.
The vehicle intervals are to be set at 2 seconds.
The left-turn slots (Phase A) are to be separate phases but concurrently timed should actuation occur in both slots.
Each slot shall have the capability of terminating or extending independently of each other, thereby reverting the timing to the non-conflicting Phase B movement.
Any unactuated phases are to be skipped.
The manual control and the memory circuits shall be disconnected.

## 0827103

Route US 322 \& Main Street
Monroe Twp.
Gloucester County

## 110/90 Second Background Cycle



|  | Hours of <br> Operation | Cycle <br> Length | Offset <br> (Seconds) |
| :--- | :--- | :--- | :--- |
| Time A | 6 AM -10 AM M-F | 110 | 10 |
|  |  |  |  |
| Time B | 10AM - 3 PM M-F | 110 | 98 |
|  |  <br> Sun |  |  |
| Time C | 3PM-7 PM M-F | 110 | 70 |
|  |  |  | 57 |
| Time D | All Other Times | 90 | 57 |

Offsets (in seconds) are measured from the beginning of yellow to Route 42 traffic at Shopping Center Drive/Bus Garage Access to the beginning of yellow to Route 42 traffic at this intersection. The manual control shall be disconnected.

The memory circuit is to be OFF.
The vehicle extension is to be $\mathbf{2}$ seconds.

Traffic signal to rest in Phase C green.

```
0827106
Route US 322 and Corkery Lane
Monroe Twp.,
Gloucester Co.
```



|  | Hours of Operation | Cycle <br> Length | Offset <br> (Seconds) |
| :--- | :--- | :--- | :--- |
| TIME A | 6 AM - 10 AM M-F | 110 | 16 |
|  |  |  |  |
| TIME B | 10AM - 3 PM M-F | 110 | 2 |
|  | 8AM-6PM, Sat\& Sun |  |  |
| TIME C | 3PM-7 PM M-F | 110 | 80 |
|  |  |  |  |
| TIME D | All Other Times | 90 | 61 |
|  |  |  |  |

Offsets (in seconds) are measured from the beginning of yellow to Route 42 traffic at Shopping Center Drive/Bus Garage Access to the beginning of yellow to Route 42 traffic at this intersection.

The manual control is to be disconnected.
The memory circuit is to be disconnected.
The vehicle interval is to be set at 2 seconds.
An actuation of a pedestrian push button is to guarantee 20 seconds of green time to Corkery Lane without causing recall.

```
0827101
Route US 322 & Malaga Road
Monroe Township
Gloucester County
110/90 SECOND BACKGROUND
```

|  |  | SIGNAL HEADS |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1,2,3, | 7,8, | TIME A | TIME B | TIME C | TIME D |
| PHASE |  | 4,5,6 | 9,10 | $\begin{aligned} & 110- \\ & \underline{\text { SECONDS }} \\ & \hline \end{aligned}$ | $\begin{aligned} & 110- \\ & \underline{\text { SECONDS }} \\ & \hline \end{aligned}$ | $\begin{aligned} & 110- \\ & \text { SECONDS } \\ & \hline \end{aligned}$ | $\begin{aligned} & \frac{90}{\text { SECONDS }} \\ & \hline \end{aligned}$ |
| A. | Route US 322 | G | R | 88-66 | 88-67 | 88-66 | 68-54 |
|  | Change | Y | R | 6 | 6 | 6 | 6 |
|  | Clearance | R | R | 2 | 2 | 2 | 2 |
| B. | Malaga Road | R | G | 7-29 | 7-28 | 7-29 | 7-21 |
|  | Change | R | Y | 5 | 5 | 5 | 5 |
|  | Clearance | R | R | 2 | 2 | 2 | 2 |
|  | FLASH | Y | R | - | - | - | - |
| TIME A | Hours of Operation 6 AM - 10 AM M-F | Cycle <br> Length <br> 110 | Offset (Seconds) 57 |  |  |  |  |
| TIME $B$ | 10AM - 3 PM M-F 8AM-6PM, Sat\& Sun | 110 | 48 |  |  |  |  |
| TIME C | 3PM-7 PM M-F | 110 | 6 |  |  |  |  |
| TIMED | All Other Times | 90 | 5 |  |  |  |  |

Offsets (in seconds) are measured from the beginning of yellow to Route 42 traffic at Shopping Center Drive/Bus Garage Access to the beginning of yellow to Route 42 traffic at this intersection.

The memory circuit is to be disconnected.
The manual control is to be disconnected.
The vehicle extension is to be set at $\mathbf{2}$ seconds.
Actuation of a pedestrian push button is to guarantee 17 seconds of green time to Malaga Road.

## 0827102

Route US 322 \& Corkery Lane
White Hall Road
Monroe Township
Gloucester County
110/90 Second Background Cycle

| NORMAL OPERATION |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | SIGNAL HEADS |  |  |  |  |  |  |
| PHASE |  | 1-4 | 5-9,12 | 10,11 | TIME A 110-SECONDS | $\begin{gathered} \text { TIME B } \\ \text { SECONDS } \\ \hline \end{gathered}$ | $\begin{gathered} \text { TIME C } \\ \text { SECONDS } \\ \hline \end{gathered}$ | $\begin{gathered} \text { TIME D } \\ \text { SECONDS } \\ \hline \end{gathered}$ |
| A. | Route US 322 | G | R | DW | 84-62 | 84-65 | 84-66 | 64-56 |
|  | Change | Y | R | DW | 6 | 6 | 6 | 6 |
|  | Clearance | R | R | DW | 2 | 2 | 2 | 2 |
| B. | Corkery Lane/ Whitehall Road | R | G | DW | 12-34 | 12-31 | 12-30 | 12-20 |
|  | Change | R | Y | DW | 4 | 4 | 4 | 4 |
|  | Clearance | R | R | DW | 2 | 2 | 2 | 2 |

WITH PEDESTRIAN ACTUATION

| A. | Route US 322 | G | R | DW | 60 | 60 | 60 | 40 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Change | Y | R | DW | 6 | 6 | 6 | 6 |
|  | Clearance | R | R | DW | 2 | 2 | 2 | 2 |
| B. | Corkery Lane/ Whitehall Road | R | G | w | 7 | 7 | 7 | 7 |
|  | Pedestrian Clearance | R | G | FDW | 29 | 29 | 29 | 29 |
|  | Change | R | Y | DW | 4 | 4 | 4 | 4 |
|  | Clearance | R | R | DW | 2 | 2 | 2 | 2 |
|  | $\begin{aligned} & \text { EMERGENCY } \\ & \text { FLASH } \end{aligned}$ | Y | R | DARK | - | - | - | - |

HOURS OF OPERATION

|  | Hours of Operation | Cycle <br> Length | Offset <br> (Seconds) <br> TIME A |
| :--- | :---: | :---: | :---: |
| TIME B | 6 AM - 10 AM M-F <br> 10AM - 3 PM M-F <br>  <br> Sun | 110 | 0 |
| TIME C | 3PM-7 PM M-F | 110 | 0 |
| TIME D | All Other Times | 90 | 0 |

The memory circuit is to be disconnected.
The manual control is to be connected.
The vehicle extension is to be set at 2 seconds.

Offsets (in seconds) are measured from the beginning of yellow to Route 42 traffic at Shopping Center Drive/Bus Garage Access to the beginning of yellow to Route 42 traffic at this intersection.

## APPENDIX E: SYNCHRO MOE RESULTS TABLES

Table E-1. MOEs Results for Route 23 (AM-EXISTING)

| Intersection | Signal Delay / Veh (s) | Total Signal Delay (hr) | Stops / Veh | Stops | Average Speed (mph) | $\begin{gathered} \text { Total } \\ \text { Travel } \\ \text { Time (hr) } \end{gathered}$ | Fuel Consumed (gal) | Emissions (kg) | NOx Emissions (kg) | $\stackrel{\text { VOC }}{\text { Emissions }}$ (kg) | Queuing Penalty (veh) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vernon Stockholm(Rt.515) | 27 | 15 | 0.62 | 1,245 | 7 | 18 | 35 | 2.44 | 0.47 | 0.56 | 349 |
| Canister Rd. | 58 | 40 | 0.90 | 2,246 | 4 | 44 | 70 | 4.87 | 0.95 | 1.13 | 646 |
| Reservior Rd. | 4 | 3 | 0.20 | 493 | 30 | 7 | 16 | 1.15 | 0.22 | 0.27 | 0 |
| Doremus Rd. | 4 | 3 | 0.39 | 922 | 30 | 6 | 22 | 1.56 | 0.30 | 0.36 | 24 |
| Paradise Rd. | 18 | 6 | 0.66 | 1,106 | 69 | 23 | 50 | 3.48 | 0.68 | 0.81 | 23 |
| OaK Ridge Rd. | 154 | 127 | 1.64 | 4,441 | 13 | 141 | 185 | 12.96 | 2.53 | 3.01 | 434 |
| Clinton Rd. | 50 | 36 | 0.98 | 2,856 | 18 | 40 | 77 | 5.37 | 1.05 | 1.24 | 427 |
| LaRue Rd. (NB) | 26 | 6 | 0.43 | 375 | 7 | 7 | 12 | 0.84 | 0.16 | 0.20 | 68 |
| LaRue Rd. (SB) | 86 | 83 | 1.20 | 4,150 | 11 | 106 | 164 | 11.44 | 2.23 | 2.65 | 1,187 |
| Kanouse (Old Route23) | 64 | 54 | 1.24 | 3,566 | 49 | 63 | 109 | 7.65 | 1.49 | 1.77 | 736 |
| Echo Lake Rd. | 163 | 86 | 1.57 | 3,284 | 6 | 93 | 123 | 8.64 | 1.68 | 2.00 | 1,056 |
| Center Court | 2 | 3 | 0.21 | 904 | 33 | 9 | 25 | 1.78 | 0.35 | 0.41 | 143 |
| Kinnelon Rd. (Rt. 618) | 13 | 18 | 0.50 | 2,480 | 17 | 28 | 68 | 4.74 | 0.92 | 1.10 | 297 |
| Kiel Ave. \& Ramp CC | 21 | 4 | 0.47 | 330 | 11 | 5 | 10 | 0.69 | 0.13 | 0.16 | 0 |
| Kakeout \& Kinnelon Rd. | 19 | 6 | 0.53 | 555 | 9 | 7 | 15 | 1.03 | 0.20 | 0.24 | 68 |
| Casecade Way | 23 | 31 | 1.09 | 5,258 | 29 | 43 | 123 | 8.63 | 1.68 | 2.00 | 623 |
| Boonton Ave. | 110 | 176 | 1.26 | 7,286 | 5 | 195 | 272 | 19.04 | 3.70 | 4.41 | 2,107 |
| Morse Ave. | 56 | 86 | 0.49 | 2,765 | 5 | 95 | 120 | 8.40 | 1.63 | 1.95 | 2,205 |
| Cotluss Rd. | 15 | 25 | 0.28 | 1,666 | 9 | 31 | 53 | 3.72 | 0.72 | 0.86 | 649 |
| Total | 828 | 808 | 0.77* | 45,928 | 19.1* | 961 | 1,549 | 108.43 | 21.09 | 25.13 | 11,042 |

Table E-2. MOEs Results for Route 23 (NOON-EXISTING)

| Intersection | Signal Delay / Veh (s) | Total Signal Delay (hr) | Stops / Veh | Stops | Average Speed (mph) |  | Fuel Consumed (gal) | CO Emissions (kg) | NOX Emissions (kg) | voc Emissions (kg) | Queuing Penalty (veh) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vernon Stockholm(Rt.515) | 7 | 3 | 0.33 | 543 | 20 | 6 | 13 | 0.92 | 0.18 | 0.21 | 0 |
| Canister Rd. | 6 | 3 | 0.36 | 713 | 23 | 7 | 17 | 1.19 | 0.23 | 0.28 | 0 |
| Reservior Rd. | 4 | 2 | 0.15 | 283 | 27 | 5 | 10 | 0.69 | 0.13 | 0.16 | 0 |
| Doremus Rd. | 2 | 1 | 0.17 | 304 | 35 | 4 | 10 | 0.70 | 0.14 | 0.16 | 0 |
| Paradise Rd. | 11 | 3 | 0.42 | 441 | 79 | 17 | 28 | 2.01 | 0.40 | 0.46 | 0 |
| OaK Ridge Rd. | 40 | 18 | 1.28 | 2,002 | 29 | 26 | 48 | 3.40 | 0.67 | 0.79 | 333 |
| Clinton Rd. | 14 | 6 | 0.63 | 894 | 37 | 9 | 21 | 1.42 | 0.27 | 0.33 | 100 |
| LaRue Rd. (NB) | 7 | 2 | 0.26 | 331 | 16 | 5 | 7 | 0.49 | 0.10 | 0.11 | 0 |
| LaRue Rd. (SB) | 3 | 1 | 0.14 | 188 | 44 | 10 | 18 | 1.26 | 0.24 | 0.29 | 0 |
| Kanouse (Old Route23) | 15 | 5 | 0.86 | 986 | 44 | 16 | 30 | 2.14 | 0.42 | 0.49 | 64 |
| Echo Lake Rd. | 10 | 4 | 0.45 | 641 | 48 | 9 | 15 | 1.03 | 0.20 | 0.24 | 18 |
| Center Court | 1 | 1 | 0.09 | 224 | 39 | 4 | 9 | 0.65 | 0.13 | 0.15 | 0 |
| Kinnelon Rd. (Rt. 618) | 13 | 13 | 0.50 | 1,832 | 14 | 18 | 41 | 2.90 | 0.56 | 0.67 | 221 |
| Kiel Ave. \& Ramp CC | 14 | 3 | 0.49 | 404 | 14 | 5 | 10 | 0.70 | 0.14 | 0.16 | 0 |
| Kakeout \& Kinnelon Rd. | 6 | 2 | 0.25 | 304 | 21 | 4 | 8 | 0.55 | 0.11 | 0.13 | 0 |
| Casecade Way | 6 | 5 | 0.38 | 1,252 | 63 | 13 | 37 | 2.54 | 0.50 | 0.59 | 0 |
| Boonton Ave. | 7 | 8 | 0.32 | 1,275 | 28 | 20 | 41 | 2.86 | 0.56 | 0.66 | 0 |
| Morse Ave. | 7 | 7 | 0.35 | 1,364 | 33 | 22 | 48 | 3.36 | 0.65 | 0.78 | 332 |
| Cotluss Rd. | 16 | 19 | 0.74 | 3,225 | 9 | 23 | 66 | 4.62 | 0.90 | 1.07 | 704 |
| Total | 189 | 106 | 0.43* | 17,206 | 32.8* | 223 | 477 | 33.43 | 6.53 | 7.73 | 1,772 |

Table E-3. MOEs Results for Route 23 (PM-EXISTING)

| Intersection | Signal Delay / Veh (s) | Total Signal Delay (hr) | Stops / Veh | Stops | Average Speed (mph) | $\begin{aligned} & \text { Total } \\ & \text { Travel } \\ & \text { Time (hr) } \end{aligned}$ | Fuel Consumed (gal) | $\underset{\text { Emissions }}{\mathrm{CO}}$ (kg) | NOx Emissions (kg) | $\stackrel{\text { VOC }}{\text { Emissions }}$ (kg) | Queuing Penalty (veh) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vernon Stockholm(Rt.515) | 8 | 4 | 0.32 | 614 | 20 | 7 | 17 | 1.18 | 0.23 | 0.27 | 0 |
| Canister Rd. | 4 | 3 | 0.15 | 388 | 32 | 7 | 16 | 1.12 | 0.22 | 0.26 | 0 |
| Reservior Rd. | 23 | 19 | 0.78 | 2,411 | 9 | 24 | 58 | 4.06 | 0.79 | 0.94 | 473 |
| Doremus Rd. | 12 | 10 | 0.67 | 1,997 | 15 | 14 | 45 | 3.14 | 0.61 | 0.73 | 259 |
| Paradise Rd. | 11 | 5 | 0.49 | 751 | 80 | 25 | 49 | 3.48 | 0.68 | 0.80 | 0 |
| OaK Ridge Rd. | 66 | 48 | 1.26 | 3,565 | 19 | 59 | 107 | 7.49 | 1.45 | 1.73 | 1,020 |
| Clinton Rd. | 92 | 74 | 1.64 | 4,528 | 14 | 81 | 135 | 9.46 | 1.84 | 2.19 | 1,081 |
| LaRue Rd. (NB) | 23 | 19 | 0.53 | 1,587 | 9 | 23 | 45 | 3.13 | 0.61 | 0.73 | 287 |
| LaRue Rd. (SB) | 6 | 2 | 0.32 | 334 | 40 | 9 | 18 | 1.26 | 0.24 | 0.29 | 0 |
| Kanouse (Old Route23) | 35 | 20 | 1.29 | 2,894 | 42 | 44 | 100 | 6.97 | 1.36 | 1.62 | 412 |
| Echo Lake Rd. | 67 | 55 | 1.30 | 3,566 | 24 | 61 | 105 | 7.33 | 1.43 | 1.70 | 713 |
| Center Court | 4 | 5 | 0.14 | 653 | 25 | 11 | 23 | 1.60 | 0.31 | 0.37 | 0 |
| Kinnelon Rd. (Rt. 618) | 23 | 41 | 0.75 | 4,780 | 8 | 49 | 117 | 8.21 | 1.60 | 1.90 | 1,252 |
| Kiel Ave. \& Ramp CC | 36 | 11 | 0.64 | 713 | 7 | 13 | 22 | 1.55 | 0.30 | 0.36 | 149 |
| Kakeout \& Kinnelon Rd. | 8 | 3 | 0.38 | 521 | 18 | 5 | 13 | 0.93 | 0.18 | 0.22 | 25 |
| Casecade Way | 22 | 34 | 0.93 | 5,087 | 35 | 46 | 125 | 8.71 | 1.69 | 2.02 | 1,175 |
| Boonton Ave. | 20 | 34 | 0.47 | 2,983 | 16 | 51 | 98 | 6.88 | 1.34 | 1.60 | 429 |
| Morse Ave. | 7 | 12 | 0.24 | 1,378 | 35 | 39 | 76 | 5.31 | 1.03 | 1.23 | 388 |
| Cotluss Rd. | 27 | 48 | 0.73 | 4,649 | 6 | 55 | 117 | 8.20 | 1.60 | 1.90 | 1,221 |
| Total | 494 | 447 | 0.69* | 43,399 | 23.9* | 623 | 1,286 | 90.01 | 17.51 | 20.86 | 8,884 |

*: Average

Table E-4. MOEs Results for Route 23 (AM-OPTIMIZED)

| Intersection | Signal Delay / Veh (s) | Total Signal Delay (hr) | Stops / Veh | Stops | Average Speed (mph) | $\begin{aligned} & \text { Total } \\ & \text { Travel } \\ & \text { Time (hr) } \end{aligned}$ | Fuel Consumed (gal) | Emissions (kg) | NOx Emissions (kg) | voc Emissions (kg) | Queuing Penalty (veh) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vernon Stockholm(Rt.515) | 26 | 15 | 0.62 | 1,252 | 8 | 18 | 35 | 2.42 | 0.47 | 0.56 | 341 |
| Canister Rd. | 50 | 35 | 0.68 | 1,691 | 4 | 38 | 57 | 3.99 | 0.78 | 0.93 | 442 |
| Reservior Rd. | 3 | 2 | 0.1 | 232 | 33 | 6 | 12 | 0.84 | 0.16 | 0.19 | 0 |
| Doremus Rd. | 3 | 2 | 0.13 | 309 | 34 | 6 | 12 | 0.86 | 0.17 | 0.2 | 0 |
| Paradise Rd. | 14 | 4 | 0 | 372 | 76 | 20 | 37 | 3 | 1 | 1 | 0 |
| OaK Ridge Rd. | 139 | 114 | 1.66 | 4,491 | 13 | 128 | 176 | 12.34 | 2.4 | 2.86 | 301 |
| Clinton Rd. | 25 | 20 | 0.77 | 2,182 | 34 | 23 | 54 | 3.8 | 0.74 | 0.88 | 166 |
| LaRue Rd. (NB) | 25 | 6 | 0.43 | 380 | 7 | 7 | 12 | 0.84 | 0.16 | 0.2 | 64 |
| LaRue Rd. (SB) | 59 | 56 | 1.07 | 3,684 | 15 | 80 | 137 | 9.58 | 1.86 | 2.22 | 548 |
| Kanouse (Old Route23) | 68 | 66 | 1.13 | 3,655 | 51 | 75 | 120 | 8.39 | 1.63 | 1.94 | 440 |
| Echo Lake Rd. | 98 | 74 | 1.63 | 4,294 | 9 | 80 | 130 | 9.06 | 1.77 | 2.1 | 1,131 |
| Center Court | 2 | 2 | 0.18 | 800 | 35 | 8 | 23 | 1.64 | 0.32 | 0.38 | 116 |
| Kinnelon Rd. (Rt. 618) | 16 | 5 | 0.32 | 333 | 11 | 6 | 11 | 0.74 | 0.14 | 0.17 | 66 |
| Kiel Ave. \& Ramp CC | 19 | 4 | 0.4 | 282 | 12 | 5 | 9 | 0.63 | 0.12 | 0.15 | 0 |
| Kakeout \& Kinnelon Rd. | 12 | 17 | 0.49 | 2,392 | 18 | 26 | 65 | 4.55 | 0.89 | 1.05 | 197 |
| Casecade Way | 8 | 10 | 0.42 | 2,039 | 54 | 23 | 59 | 4.15 | 0.81 | 0.96 | 66 |
| Boonton Ave. | 32 | 52 | 0.82 | 4,757 | 13 | 71 | 143 | 9.97 | 1.94 | 2.31 | 520 |
| Morse Ave. | 65 | 101 | 0.69 | 3,890 | 4 | 110 | 148 | 10.38 | 2.02 | 2.41 | 1,193 |
| Cotluss Rd. | 38 | 63 | 0.66 | 3,932 | 4 | 68 | 115 | 8.07 | 1.57 | 1.87 | 668 |
| Total | 702 | 648 | 0.66* | 40,967 | 22.9* | 798 | 1,355 | 94.81 | 18.45 | 21.97 | 6,259 |

Table E-5. MOEs Results for Route 23 (NOON-OPTIMIZED)

| Intersection | Signal Delay / Veh (s) | Total Signal Delay (hr) | Stops / Veh | Stops | Average Speed (mph) | Total Travel Time (hr) | Fuel Consumed (gal) | $\underset{\text { Emissions }}{\text { CO }}$ (kg) | NOx Emissions (kg) | $\stackrel{\text { VOC }}{\text { Emissions }}$ (kg) | Queuing Penalty (veh) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vernon Stockholm(Rt.515) | 8 | 4 | 0.34 | 566 | 19 | 6 | 14 | 0.95 | 0.19 | 0.22 | 0 |
| Canister Rd. | 5 | 3 | 0.25 | 487 | 25 | 6 | 13 | 0.92 | 0.18 | 0.21 | 0 |
| Reservior Rd. | 3 | 2 | 0.12 | 219 | 32 | 5 | 8 | 0.58 | 0.11 | 0.13 | 0 |
| Doremus Rd. | 1 | 1 | 0.07 | 132 | 42 | 3 | 7 | 0.49 | 0.09 | 0.11 | 0 |
| Paradise Rd. | 6 | 2 | 0.32 | 339 | 88 | 15 | 27 | 1.90 | 0.37 | 0.44 | 0 |
| OaK Ridge Rd. | 25 | 11 | 0.99 | 1,549 | 37 | 20 | 38 | 2.70 | 0.52 | 0.63 | 72 |
| Clinton Rd. | 11 | 4 | 0.46 | 670 | 44 | 9 | 17 | 1.18 | 0.23 | 0.27 | 103 |
| LaRue Rd. (NB) | 7 | 3 | 0.32 | 404 | 15 | 5 | 7 | 0.52 | 0.10 | 0.12 | 0 |
| LaRue Rd. (SB) | 6 | 2 | 0.17 | 237 | 40 | 11 | 20 | 1.39 | 0.27 | 0.32 | 0 |
| Kanouse (Old Route23) | 6 | 2 | 0.35 | 438 | 53 | 14 | 22 | 1.56 | 0.31 | 0.36 | 0 |
| Echo Lake Rd. | 11 | 4 | 0.55 | 759 | 47 | 9 | 17 | 1.18 | 0.23 | 0.28 | 15 |
| Center Court | 1 | 1 | 0.09 | 224 | 39 | 4 | 9 | 0.65 | 0.13 | 0.15 | 0 |
| Kinnelon Rd. (Rt. 618) | 12 | 12 | 0.45 | 1,634 | 15 | 18 | 38 | 2.66 | 0.52 | 0.62 | 219 |
| Kiel Ave. \& Ramp CC | 11 | 3 | 0.48 | 399 | 16 | 4 | 9 | 0.66 | 0.13 | 0.15 | 0 |
| Kakeout \& Kinnelon Rd. | 5 | 2 | 0.21 | 254 | 21 | 4 | 7 | 0.51 | 0.10 | 0.12 | 0 |
| Casecade Way | 4 | 3 | 0.17 | 570 | 75 | 11 | 24 | 1.71 | 0.33 | 0.40 | 0 |
| Boonton Ave. | 9 | 10 | 0.54 | 2,115 | 25 | 22 | 55 | 3.87 | 0.75 | 0.90 | 0 |
| Morse Ave. | 5 | 6 | 0.25 | 976 | 36 | 20 | 41 | 2.85 | 0.55 | 0.66 | 300 |
| Cotluss Rd. | 12 | 14 | 0.52 | 2,246 | 11 | 19 | 48 | 3.35 | 0.65 | 0.78 | 408 |
| Total | 148 | 89 | 0.35* | 14,218 | 35.8* | 205 | 421 | 29.63 | 5.76 | 6.87 | 1,117 |

*: Average

Table E-6. MOEs Results for Route 23 (PM-OPTIMIZED)

| Intersection | Signal Delay / Veh (s) | Total Signal Delay (hr) | Stops / Veh | Stops | Average Speed (mph) | $\begin{aligned} & \text { Total } \\ & \text { Travel } \\ & \text { Time (hr) } \end{aligned}$ | Fuel Consumed (gal) | $\underset{\text { Emissions }}{\mathrm{CO}}$ (kg) | $\begin{gathered} \text { NOx } \\ \text { Emissions } \\ (\mathrm{kg}) \end{gathered}$ | $\stackrel{\text { VOC }}{\text { Emissions }}$ (kg) | Queuing Penalty (veh) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vernon Stockholm(Rt.515) | 7 | 4 | 0.21 | 405 | 22 | 6 | 13 | 0.93 | 0.18 | 0.21 | 0 |
| Canister Rd. | 3 | 2 | 0.13 | 340 | 33 | 7 | 15 | 1.06 | 0.21 | 0.24 | 0 |
| Reservior Rd. | 5 | 4 | 0.13 | 409 | 24 | 8 | 16 | 1.14 | 0.22 | 0.26 | 0 |
| Doremus Rd. | 3 | 2 | 0.24 | 701 | 32 | 7 | 20 | 1.38 | 0.27 | 0.32 | 0 |
| Paradise Rd. | 8 | 3 | 0.21 | 285 | 84 | 25 | 42 | 2.97 | 0.58 | 0.69 | 0 |
| OaK Ridge Rd. | 28 | 24 | 0.95 | 2,786 | 42 | 34 | 77 | 5.40 | 1.06 | 1.25 | 1,072 |
| Clinton Rd. | 78 | 62 | 1.29 | 3,399 | 15 | 69 | 109 | 7.62 | 1.49 | 1.77 | 1,203 |
| LaRue Rd. (NB) | 20 | 17 | 0.55 | 1,643 | 10 | 21 | 44 | 3.10 | 0.60 | 0.72 | 522 |
| LaRue Rd. (SB) | 3 | 1 | 0.15 | 162 | 44 | 8 | 15 | 1.02 | 0.20 | 0.24 | 0 |
| Kanouse (Old Route23) | 26 | 14 | 1.06 | 2,360 | 49 | 38 | 87 | 6.09 | 1.19 | 1.41 | 274 |
| Echo Lake Rd. | 40 | 32 | 1.02 | 2,914 | 29 | 38 | 78 | 5.45 | 1.06 | 1.27 | 477 |
| Center Court | 3 | 4 | 0.11 | 514 | 30 | 9 | 20 | 1.37 | 0.27 | 0.32 | 0 |
| Kinnelon Rd. (Rt. 618) | 18 | 32 | 0.73 | 4,664 | 10 | 40 | 109 | 7.61 | 1.48 | 1.76 | 963 |
| Kiel Ave. \& Ramp CC | 34 | 10 | 0.64 | 709 | 8 | 12 | 22 | 1.51 | 0.29 | 0.35 | 143 |
| Kakeout \& Kinnelon Rd. | 7 | 3 | 0.20 | 272 | 20 | 4 | 9 | 0.63 | 0.12 | 0.15 | 0 |
| Casecade Way | 12 | 18 | 0.58 | 3,168 | 53 | 32 | 84 | 5.86 | 1.15 | 1.36 | 217 |
| Boonton Ave. | 37 | 65 | 0.72 | 4,516 | 10 | 81 | 144 | 10.08 | 1.96 | 2.34 | 1,172 |
| Morse Ave. | 5 | 8 | 0.14 | 835 | 39 | 35 | 64 | 4.51 | 0.88 | 1.04 | 378 |
| Cotluss Rd. | 17 | 30 | 0.59 | 3,797 | 9 | 36 | 91 | 6.33 | 1.23 | 1.47 | 1,124 |
| Total | 354 | 335 | 0.51* | 33,879 | 29.6* | 510 | 1,059 | 74.06 | 14.44 | 17.17 | 7,545 |

*: Average

Table E-7. MOEs Results for Route 42/322 (AM-EXISTING)

| Intersection | Signal Delay / Veh (s) | Total Signal Delay (hr) | Stops / Veh | Stops | Average Speed (mph) |  | Fuel Consumed (gal) | $\underset{\text { Emissions }}{\text { CO }}$ (kg) | NOx Emissions (kg) | $\stackrel{\text { VOC }}{\text { Emissions }}$ (kg) | Queuing Penalty (veh) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Shopping Center Dr. | 8 | 7 | 0.35 | 1,173 | 18 | 12 | 29 | 2.00 | 0.39 | 0.46 | 149 |
| Greentree Rd. | 65 | 61 | 1.02 | 3,470 | 4 | 69 | 93 | 6.49 | 1.26 | 1.50 | 1,086 |
| Whitman Dr. | 11 | 9 | 0.35 | 1,071 | 16 | 14 | 28 | 1.98 | 0.39 | 0.46 | 427 |
| Gantown Rd. | 45 | 40 | 0.93 | 2,951 | 4 | 44 | 74 | 5.16 | 1.00 | 1.20 | 909 |
| Johnson Rd.(NB) | 13 | 10 | 0.35 | 1,050 | 15 | 16 | 32 | 2.23 | 0.43 | 0.52 | 44 |
| Fries Mill Rd.(SB) | 28 | 15 | 0.52 | 1,031 | 11 | 20 | 29 | 1.99 | 0.39 | 0.46 | 438 |
| Watson Dr. | 26 | 14 | 0.78 | 1,485 | 20 | 24 | 46 | 3.24 | 0.63 | 0.75 | 102 |
| Tuckahoe Rd.-Stagecoach Rd. | 30 | 15 | 0.71 | 1,300 | 10 | 20 | 35 | 2.42 | 0.47 | 0.56 | 281 |
| Berlin Cross Keys Rd. | 27 | 15 | 0.68 | 1,392 | 15 | 25 | 41 | 2.85 | 0.55 | 0.66 | 170 |
| Kennedy Dr. (SB) | 5 | 2 | 0.27 | 345 | 31 | 5 | 11 | 0.77 | 0.15 | 0.18 | 0 |
| Lake Ave. | 7 | 3 | 0.36 | 513 | 35 | 10 | 21 | 1.45 | 0.28 | 0.34 | 2 |
| Sicklerville Rd. | 57 | 38 | 0.95 | 2,315 | 2 | 40 | 52 | 3.66 | 0.71 | 0.85 | 937 |
| Poplar St-New Brooklyn Rd. | 24 | 10 | 0.66 | 999 | 15 | 17 | 29 | 2.05 | 0.40 | 0.47 | 7 |
| Main St. (Rt.322) | 5 | 2 | 0.33 | 384 | 21 | 3 | 9 | 0.63 | 0.12 | 0.15 | 0 |
| Corkery Ln. | 12 | 5 | 0.52 | 695 | 20 | 9 | 19 | 1.30 | 0.25 | 0.30 | 0 |
| Malaga Rd. | 8 | 3 | 0.40 | 492 | 17 | 4 | 11 | 0.75 | 0.15 | 0.17 | 0 |
| White Hall Rd.-Corkery Ln. | 8 | 2 | 0.40 | 387 | 14 | 3 | 8 | 0.56 | 0.11 | 0.13 | 12 |
| Total | 379 | 251 | 0.56* | 21,053 | 15.7* | 335 | 567 | 39.53 | 7.68 | 9.16 | 4,564 |

Table E-8. MOEs Results for Route 42/322 (NOON-EXISTING)

| Intersection | Signal Delay / Veh (s) | Total Signal Delay (hr) | Stops / Veh | Stops | Average Speed (mph) | Total <br> Travel Time (hr) | Fuel Consumed (gal) | $\underset{\text { Emissions }}{\text { CO }}$ (kg) | NOx Emissions (kg) | $\stackrel{\text { VOC }}{\text { Emissions }}$ (kg) | Queuing Penalty (veh) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Shopping Center Dr. | 12 | 11 | 0.45 | 1,618 | 14 | 16 | 39 | 2.69 | 0.52 | 0.62 | 628 |
| Greentree Rd. | 52 | 55 | 0.72 | 2,763 | 5 | 64 | 80 | 5.57 | 1.08 | 1.29 | 1,195 |
| Whitman Dr. | 13 | 13 | 0.46 | 1,599 | 14 | 19 | 40 | 2.76 | 0.54 | 0.64 | 432 |
| Gantown Rd. | 32 | 33 | 0.68 | 2,572 | 6 | 39 | 68 | 4.74 | 0.92 | 1.10 | 1,138 |
| Johnson Rd.(NB) | 39 | 46 | 0.75 | 3,226 | 6 | 53 | 94 | 6.60 | 1.28 | 1.53 | 1,048 |
| Fries Mill Rd.(SB) | 15 | 13 | 0.52 | 1,584 | 19 | 21 | 41 | 2.88 | 0.56 | 0.67 | 538 |
| Watson Dr. | 16 | 13 | 0.63 | 1,863 | 26 | 29 | 61 | 4.30 | 0.84 | 1.00 | 112 |
| Tuckahoe Rd.-Stagecoach Rd. | 32 | 24 | 0.75 | 2,026 | 10 | 32 | 53 | 3.74 | 0.73 | 0.87 | 394 |
| Berlin Cross Keys Rd. | 26 | 19 | 0.65 | 1,737 | 15 | 33 | 54 | 3.74 | 0.73 | 0.87 | 429 |
| Kennedy Dr. (SB) | 6 | 3 | 0.34 | 671 | 29 | 8 | 20 | 1.42 | 0.28 | 0.33 | 0 |
| Lake Ave. | 9 | 4 | 0.42 | 780 | 34 | 14 | 31 | 2.14 | 0.42 | 0.50 | 10 |
| Sicklerville Rd. | 29 | 18 | 0.73 | 1,609 | 3 | 19 | 33 | 2.30 | 0.45 | 0.53 | 801 |
| Poplar St-New Brooklyn Rd. | 24 | 12 | 0.69 | 1,250 | 15 | 19 | 35 | 2.47 | 0.48 | 0.57 | 4 |
| Main St. (Rt.322) | 4 | 2 | 0.28 | 384 | 22 | 3 | 9 | 0.64 | 0.12 | 0.15 | 0 |
| Corkery Ln. | 9 | 3 | 0.42 | 513 | 24 | 6 | 15 | 1.02 | 0.20 | 0.24 | 0 |
| Malaga Rd. | 6 | 2 | 0.31 | 305 | 22 | 3 | 7 | 0.50 | 0.10 | 0.12 | 0 |
| White Hall Rd.-Corkery Ln. | 5 | 1 | 0.3 | 244 | 19 | 2 | 5 | 0.38 | 0.07 | 0.09 | 0 |
| Total | 329 | 272 | 0.54* | 24,744 | 16.6* | 380 | 685 | 47.89 | 9.32 | 11.12 | 6,729 |

Table E-9. MOEs Results for Route 42/322 (PM-EXISTING)

| Intersection | Signal Delay / Veh (s) | Total Signal Delay (hr) | Stops / Veh | Stops | Average Speed (mph) | Total Travel Time (hr) | Fuel Consumed (gal) | CO Emissions (kg) | $\xrightarrow{\text { NOx }}$ (kg) | VOC Emissions (kg) | Queuing Penalty (veh) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Shopping Center Dr. | 20 | 25 | 0.67 | 2,966 | 9 | 32 | 63 | 4.40 | 0.86 | 1.02 | 1,057 |
| Greentree Rd. | 60 | 72 | 0.87 | 3,734 | 5 | 82 | 105 | 7.36 | 1.43 | 1.71 | 1,724 |
| Whitman Dr. | 16 | 19 | 0.49 | 2,120 | 12 | 27 | 49 | 3.44 | 0.67 | 0.80 | 625 |
| Gantown Rd. | 63 | 82 | 0.94 | 4,413 | 3 | 89 | 115 | 8.06 | 1.57 | 1.87 | 1,256 |
| Johnson Rd.(NB) | 18 | 22 | 0.58 | 2,586 | 12 | 32 | 61 | 4.26 | 0.83 | 0.99 | 964 |
| Fries Mill Rd.(SB) | 15 | 15 | 0.49 | 1,762 | 16 | 24 | 42 | 2.93 | 0.57 | 0.68 | 841 |
| Watson Dr. | 28 | 23 | 0.76 | 2,259 | 18 | 39 | 68 | 4.75 | 0.92 | 1.10 | 284 |
| Tuckahoe Rd.-Stagecoach Rd. | 31 | 24 | 0.78 | 2,117 | 9 | 30 | 50 | 3.51 | 0.68 | 0.81 | 602 |
| Berlin Cross Keys Rd. | 38 | 35 | 0.79 | 2,672 | 12 | 55 | 76 | 5.34 | 1.04 | 1.24 | 486 |
| Kennedy Dr. (SB) | 11 | 7 | 0.49 | 1,214 | 21 | 15 | 30 | 2.12 | 0.41 | 0.49 | 21 |
| Lake Ave. | 10 | 5 | 0.46 | 861 | 29 | 17 | 31 | 2.14 | 0.42 | 0.50 | 17 |
| Sicklerville Rd. | 56 | 47 | 0.91 | 2,749 | 2 | 49 | 64 | 4.45 | 0.87 | 1.03 | 1,472 |
| Poplar St-New Brooklyn Rd. | 18 | 12 | 0.63 | 1,450 | 18 | 20 | 41 | 2.84 | 0.55 | 0.66 | 5 |
| Main St. (Rt.322) | 8 | 4 | 0.67 | 1,284 | 15 | 6 | 27 | 1.90 | 0.37 | 0.44 | 0 |
| Corkery Ln. | 9 | 4 | 0.45 | 715 | 23 | 8 | 20 | 1.43 | 0.28 | 0.33 | 2 |
| Malaga Rd. | 8 | 3 | 0.40 | 617 | 18 | 5 | 14 | 0.96 | 0.19 | 0.22 | 0 |
| White Hall Rd.-Corkery Ln. | 9 | 3 | 0.45 | 464 | 14 | 3 | 11 | 0.80 | 0.15 | 0.18 | 0 |
| Total | 418 | 402 | 0.64* | 33,983 | 13.9* | 533 | 867 | 60.69 | 11.81 | 14.07 | 9,356 |

Table E-10. MOEs Results for Route 42/322 (AM-OPTIMIZED)

| Intersection | Signal Delay / Veh (s) | Total Signal Delay (hr) | Stops / Veh | Stops | Average Speed (mph) | $\begin{aligned} & \text { Total } \\ & \text { Travel } \\ & \text { Time (hr) } \end{aligned}$ | Fuel Consumed (gal) | $\underset{\substack{\text { Emissions } \\(\mathrm{kg})}}{\mathrm{CO}}$ | NOx Emissions (kg) | $\underset{\text { Emissions }}{\text { VOC }}$ (kg) | Queuing Penalty (veh) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Shopping Center Dr. | 6 | 6 | 0.34 | 1,141 | 20 | 10 | 27 | 1.89 | 0.37 | 0.44 | 32 |
| Greentree Rd. | 25 | 24 | 0.71 | 2,400 | 9 | 31 | 60 | 4.20 | 0.82 | 0.97 | 1,319 |
| Whitman Dr. | 8 | 6 | 0.27 | 842 | 19 | 11 | 23 | 1.59 | 0.31 | 0.37 | 391 |
| Gantown Rd. | 13 | 12 | 0.48 | 1,535 | 12 | 16 | 35 | 2.43 | 0.47 | 0.56 | 138 |
| Johnson Rd.(NB) | 10 | 9 | 0.47 | 1,405 | 17 | 14 | 36 | 2.51 | 0.49 | 0.58 | 217 |
| Fries Mill Rd.(SB) | 12 | 7 | 0.44 | 863 | 20 | 11 | 21 | 1.48 | 0.29 | 0.34 | 356 |
| Watson Dr. | 18 | 9 | 0.56 | 1,080 | 24 | 19 | 38 | 2.64 | 0.51 | 0.61 | 59 |
| Tuckahoe Rd.-Stagecoach Rd. | 22 | 11 | 0.71 | 1,312 | 12 | 16 | 32 | 2.22 | 0.43 | 0.51 | 106 |
| Berlin Cross Keys Rd. | 24 | 14 | 0.64 | 1,312 | 16 | 24 | 38 | 2.66 | 0.52 | 0.62 | 119 |
| Kennedy Dr. (SB) | 4 | 2 | 0.17 | 223 | 32 | 5 | 9 | 0.64 | 0.12 | 0.15 | 0 |
| Lake Ave. | 8 | 3 | 0.30 | 429 | 34 | 10 | 20 | 1.38 | 0.27 | 0.32 | 2 |
| Sicklerville Rd. | 24 | 16 | 0.62 | 1,512 | 4 | 18 | 28 | 1.97 | 0.38 | 0.46 | 706 |
| Poplar St-New Brooklyn Rd. | 17 | 7 | 0.54 | 820 | 19 | 14 | 24 | 1.67 | 0.33 | 0.39 | 3 |
| Main St. (Rt.322) | 3 | 1 | 0.15 | 178 | 25 | 2 | 5 | 0.35 | 0.07 | 0.08 | 0 |
| Corkery Ln. | 17 | 6 | 0.53 | 709 | 17 | 11 | 20 | 1.40 | 0.27 | 0.32 | 2 |
| Malaga Rd. | 11 | 4 | 0.30 | 378 | 14 | 5 | 9 | 0.64 | 0.12 | 0.15 | 0 |
| White Hall Rd.-Corkery Ln. | 11 | 3 | 0.37 | 364 | 11 | 4 | 8 | 0.56 | 0.11 | 0.13 | 36 |
| Total | 233 | 140 | 0.45* | 16,503 | 17.9* | 221 | 433 | 30.23 | 5.88 | 7.00 | 3,486 |

Table E-11. MOEs Results for Route 42/322 (NOON-OPTIMIZED)

| Intersection | Signal Delay / Veh (s) | Total Signal Delay (hr) | Stops / Veh | Stops | Average Speed (mph) | $\begin{aligned} & \text { Total } \\ & \text { Travel } \\ & \text { Time (hr) } \end{aligned}$ | Fuel Consumed (gal) | $\underset{\substack{\text { Emissions } \\(\mathrm{kg})}}{\mathrm{CO}}$ | NOx Emissions (kg) | $\underset{\text { Emissions }}{\text { VOC }}$ (kg) | Queuing Penalty (veh) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Shopping Center Dr. | 11 | 11 | 0.47 | 1,658 | 15 | 16 | 39 | 2.70 | 0.53 | 0.63 | 618 |
| Greentree Rd. | 19 | 20 | 0.54 | 2,062 | 12 | 29 | 53 | 3.70 | 0.72 | 0.86 | 1,223 |
| Whitman Dr. | 11 | 10 | 0.43 | 1,492 | 16 | 16 | 36 | 2.49 | 0.48 | 0.58 | 529 |
| Gantown Rd. | 14 | 15 | 0.51 | 1,927 | 12 | 20 | 44 | 3.09 | 0.60 | 0.72 | 230 |
| Johnson Rd.(NB) | 17 | 20 | 0.59 | 2,527 | 12 | 28 | 65 | 4.54 | 0.88 | 1.05 | 733 |
| Fries Mill Rd.(SB) | 12 | 10 | 0.44 | 1,336 | 22 | 19 | 36 | 2.49 | 0.48 | 0.58 | 519 |
| Watson Dr. | 11 | 9 | 0.43 | 1,291 | 29 | 25 | 50 | 3.49 | 0.68 | 0.81 | 63 |
| Tuckahoe Rd.-Stagecoach Rd. | 25 | 19 | 0.76 | 2,030 | 12 | 26 | 50 | 3.50 | 0.68 | 0.81 | 247 |
| Berlin Cross Keys Rd. | 24 | 18 | 0.64 | 1,709 | 16 | 31 | 51 | 3.60 | 0.70 | 0.83 | 360 |
| Kennedy Dr. (SB) | 6 | 3 | 0.26 | 513 | 29 | 8 | 18 | 1.24 | 0.24 | 0.29 | 0 |
| Lake Ave. | 9 | 5 | 0.36 | 661 | 33 | 15 | 29 | 2.03 | 0.40 | 0.47 | 9 |
| Sicklerville Rd. | 21 | 13 | 0.57 | 1,248 | 4 | 14 | 24 | 1.68 | 0.33 | 0.39 | 491 |
| Poplar St-New Brooklyn Rd. | 20 | 10 | 0.55 | 998 | 17 | 17 | 30 | 2.09 | 0.41 | 0.49 | 4 |
| Main St. (Rt.322) | 4 | 2 | 0.19 | 256 | 22 | 3 | 7 | 0.48 | 0.09 | 0.11 | 0 |
| Corkery Ln. | 12 | 4 | 0.42 | 510 | 20 | 8 | 15 | 1.07 | 0.21 | 0.25 | 0 |
| Malaga Rd. | 8 | 2 | 0.2 | 198 | 19 | 3 | 6 | 0.39 | 0.08 | 0.09 | 0 |
| White Hall Rd.-Corkery Ln. | 7 | 2 | 0.28 | 227 | 15 | 2 | 5 | 0.38 | 0.07 | 0.09 | 0 |
| Total | 231 | 173 | 0.45* | 20,643 | 17.9* | 280 | 558 | 38.96 | 7.58 | 9.05 | 5,026 |

Table E-12. MOEs Results for Route 42/322 (PM-OPTIMIZED)

| Intersection | Signal Delay / Veh (s) | Total Signal Delay (hr) | Stops / Veh | Stops | Average Speed (mph) | $\begin{aligned} & \text { Total } \\ & \text { Travel } \\ & \text { Time (hr) } \end{aligned}$ | Fuel Consumed (gal) | CO Emissions (kg) | $\underset{\substack{\text { NOx } \\ \text { Emissions } \\(\mathrm{kg})}}{\substack{\text { ( } \\ \hline}}$ | VOC Emissions (kg) | Queuing Penalty (veh) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Shopping Center Dr. | 16 | 19 | 0.72 | 3,152 | 11 | 26 | 61 | 4.27 | 0.83 | 0.99 | 784 |
| Greentree Rd. | 46 | 55 | 0.83 | 3,590 | 6 | 65 | 88 | 6.14 | 1.20 | 1.42 | 709 |
| Whitman Dr. | 12 | 15 | 0.47 | 2,024 | 14 | 23 | 45 | 3.14 | 0.61 | 0.73 | 448 |
| Gantown Rd. | 33 | 43 | 0.80 | 3,757 | 6 | 51 | 83 | 5.81 | 1.13 | 1.35 | 879 |
| Johnson Rd.(NB) | 12 | 14 | 0.51 | 2,290 | 16 | 23 | 51 | 3.58 | 0.70 | 0.83 | 493 |
| Fries Mill Rd.(SB) | 10 | 9 | 0.32 | 1,147 | 21 | 18 | 30 | 2.10 | 0.41 | 0.49 | 530 |
| Watson Dr. | 16 | 13 | 0.63 | 1,871 | 24 | 30 | 56 | 3.93 | 0.76 | 0.91 | 165 |
| Tuckahoe Rd.-Stagecoach Rd. | 19 | 14 | 0.55 | 1,486 | 13 | 21 | 35 | 2.47 | 0.48 | 0.57 | 48 |
| Berlin Cross Keys Rd. | 30 | 28 | 0.75 | 2,550 | 14 | 48 | 70 | 4.87 | 0.95 | 1.13 | 439 |
| Kennedy Dr. (SB) | 11 | 8 | 0.42 | 1,041 | 21 | 15 | 28 | 1.99 | 0.39 | 0.46 | 49 |
| Lake Ave. | 12 | 6 | 0.44 | 831 | 28 | 17 | 31 | 2.15 | 0.42 | 0.50 | 15 |
| Sicklerville Rd. | 28 | 23 | 0.73 | 2,204 | 3 | 26 | 43 | 3.01 | 0.59 | 0.70 | 1,317 |
| Poplar St-New Brooklyn Rd. | 17 | 11 | 0.56 | 1,302 | 19 | 19 | 38 | 2.64 | 0.51 | 0.61 | 5 |
| Main St. (Rt.322) | 4 | 2 | 0.18 | 346 | 24 | 4 | 9 | 0.65 | 0.13 | 0.15 | 13 |
| Corkery Ln. | 13 | 6 | 0.46 | 732 | 19 | 10 | 22 | 1.52 | 0.30 | 0.35 | 10 |
| Malaga Rd. | 11 | 5 | 0.31 | 474 | 15 | 7 | 12 | 0.81 | 0.16 | 0.19 | 0 |
| White Hall Rd.-Corkery Ln. | 9 | 3 | 0.40 | 416 | 13 | 4 | 11 | 0.74 | 0.14 | 0.17 | 0 |
| Total | 299 | 274 | 0.53* | 29,213 | 15.7* | 407 | 713 | 49.82 | 9.71 | 11.55 | 5,904 |

Table E-13. MOEs Results for Route 42/322 (OFFPEAK-OPTIMIZED)

| Intersection | Signal Delay / Veh (s) | Total Signal Delay (hr) | Stops / Veh | Stops | Average Speed (mph) | Total Travel Time (hr) | Fuel Consumed (gal) | $\underset{\text { Emissions }}{\mathrm{CO}}$ (kg) | NOx Emissions (kg) | $\stackrel{\text { VOC }}{\text { Emissions }}$ (kg) | Queuing Penalty (veh) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Shopping Center Dr. | 5 | 2 | 0.26 | 304 | 23 | 3 | 8 | 0.54 | 0.10 | 0.12 | 0 |
| Greentree Rd. | 10 | 3 | 0.37 | 465 | 18 | 6 | 12 | 0.82 | 0.16 | 0.19 | 94 |
| Whitman Dr. | 7 | 2 | 0.32 | 376 | 20 | 4 | 9 | 0.66 | 0.13 | 0.15 | 97 |
| Gantown Rd. | 13 | 4 | 0.47 | 593 | 12 | 6 | 14 | 0.96 | 0.19 | 0.22 | 0 |
| Johnson Rd.(NB) | 7 | 3 | 0.32 | 466 | 21 | 5 | 13 | 0.90 | 0.17 | 0.21 | 0 |
| Fries Mill Rd.(SB) | 9 | 3 | 0.38 | 386 | 25 | 5 | 11 | 0.74 | 0.14 | 0.17 | 22 |
| Watson Dr. | 8 | 2 | 0.33 | 330 | 32 | 8 | 14 | 1.01 | 0.20 | 0.23 | 1 |
| Tuckahoe Rd.-Stagecoach Rd. | 16 | 4 | 0.57 | 511 | 16 | 7 | 13 | 0.89 | 0.17 | 0.21 | 24 |
| Berlin Cross Keys Rd. | 17 | 4 | 0.53 | 476 | 19 | 9 | 15 | 1.03 | 0.20 | 0.24 | 0 |
| Kennedy Dr. (SB) | 4 | 1 | 0.21 | 136 | 34 | 2 | 5 | 0.35 | 0.07 | 0.08 | 0 |
| Lake Ave. | 5 | 1 | 0.23 | 141 | 38 | 4 | 8 | 0.56 | 0.11 | 0.13 | 0 |
| Sicklerville Rd. | 15 | 3 | 0.52 | 379 | 5 | 4 | 7 | 0.47 | 0.09 | 0.11 | 11 |
| Poplar St-New Brooklyn Rd. | 13 | 2 | 0.45 | 275 | 21 | 5 | 8 | 0.58 | 0.11 | 0.13 | 0 |
| Main St. (Rt.322) | 4 | 0 | 0.16 | 74 | 24 | 1 | 2 | 0.14 | 0.03 | 0.03 | 0 |
| Corkery Ln. | 9 | 1 | 0.33 | 131 | 24 | 2 | 4 | 0.28 | 0.06 | 0.07 | 0 |
| Malaga Rd. | 6 | 1 | 0.23 | 77 | 21 | 1 | 2 | 0.13 | 0.03 | 0.03 | 0 |
| White Hall Rd.-Corkery Ln. | 6 | 0 | 0.26 | 70 | 18 | 1 | 2 | 0.11 | 0.02 | 0.02 | 0 |
| Total | 154 | 36 | 0.35* | 5,190 | 21.8* | 73 | 147 | 10.17 | 1.98 | 2.34 | 249 |

*: Average

