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## Updating the Crash Modification Factors and Calibrating the IHSDM for Indiana



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## EXECUTIVE SUMMARY

## UPDATING THE CRASH MODIFICATION FACTORS AND CALIBRATING THE IHSDM FOR INDIANA

## Introduction

Reducing the number of severe injuries and fatalities on Indiana roads can be accomplished through comprehensive consideration of safety in transportation planning, design, management, and operations. To accomplish this goal, knowledge of the safety factors and countermeasures that may be applied to improve safety are needed, as well as tools for facilitating application of that knowledge. The main components of the safety knowledge are crash reduction factors (CRFs) and the associated crash modification factors (CMFs), which can be utilized to estimate the benefit cost ratio ( BCR ) and the net benefit (B-C) of safety projects in the planning, design, and management stages. There is a need to update the CRFs and CMFs applicable to Indiana conditions. This study addressed this concern by updating the CRFs/CMFs for various traffic, geometrics, and other improvements that may be applied in Indiana. Furthermore, the study calibrated the components of the Interactive Highway Safety Design Model (IHSDM) to better reflect Indiana conditions (FHWA, n.d.a).

## Findings

A set of criteria was developed for determining the existing CRFs and CMFs that are most suitable for Indiana conditions.

This research identified more than 80 safety countermeasures and their associated CRFs/CMFs for various geometric, traffic, pavement, and other characteristics. The identified CRFs/CMFs are applicable to different crash types and severities at urban and rural segments, intersections, and interchanges. CRFs and CMFs presented as functions were discretized for various levels of the change in safety in order to provide ease of implementation in Indiana.

Additionally, a comprehensive approach for calibrating the predictive components of the Highway Safety Manual (HSM) method was developed that fits within the constraints of the IHSDM. This included calibrating the tool's default parameters for SPFs and CMFs for rural and urban segments, as well as updating the default crash proportions to reflect Indiana conditions. In some cases, the Indiana parameters and crash proportions show similarities with their HSM counterparts. However, the results also show considerable differences that highlight the need for calibrating the crash prediction method for local conditions. The presented example studies show how the HSM default parameters may understate or overstate the safety performance of road facilities in comparison to using parameters developed specifically for Indiana.

## Implementation

A comprehensive table of CRFs and CMFs that may be implemented in Indiana was presented. Furthermore, the study provides the Indiana specifications of the IHSDM CMFs, SPFs, and crash proportions, both in tabular form and in files that may be implemented directly in the software by the user.
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## 1. INTRODUCTION

### 1.1 Background

More than 30,000 people are killed annually in motorvehicle crashes in the United States (BTS, 2017), or about one fatality every 17 minutes. The impact of these crashes is immense. The National Safety Council estimates that motor-vehicle crashes resulted in $\$ 430$ billion in economic, personal, and societal costs in the United States for 2016 alone (NSC, 2017). Hence, it has become the long-term goal of cities, states, and the nation to greatly reduce or even eliminate the number of severe injuries and fatalities occurring in motor-vehicle crashes. Many of these programs fall under the umbrella of the "Towards Zero Deaths" vision promoted by the Federal Highway Administration (FHWA, n.d.b). As part of this initiative, the Indiana Department of Transportation (INDOT) has developed a Strategic Highway Safety Plan with the objective of identifying highway safety problems and implementing general strategies for reducing or eliminating the effect of these problems on the crash, injury, and fatality risk (INDOT, 2016).

Reducing the number of severe injuries and fatalities on Indiana roads can be accomplished through comprehensive consideration of safety in transportation planning, design, management, and operations. To accomplish this goal, knowledge of the safety factors and countermeasures which may be applied to improve safety are needed, as well as tools for facilitating application of that knowledge (AASHTO, 2010). Crash reduction factors (CRFs) are a key component of the safety knowledge which can be used to estimate the benefit cost ratio (BCR) and the net benefit (B-C) of safety projects in the planning, design, and management stages. Accurately predicting the safety effects of engineering countermeasures by determining the CRFs will improve the transportation decisionmaking process from the safety perspective (Herbel, Laing, \& McGovern, 2010).

Tarko, Dey, and Romero (2015) conducted the last CRF study for Indiana in 2015. This study includes CRFs for geometric safety improvements on rural and urban road segments. However, there are CRFs for geometric and non-geometric safety improvements which are either outdated or not available for Indiana altogether. For these safety improvements, other regions with similar driving cultures and weather to Indiana have conducted recent CRF studies (AASHTO, 2010; FHWA \& UNC HSRC, 2017). There is a need for updating out-of-date existing Indiana CRFs and increasing the size of the CRF database by adopting applicable CRFs for other regions similar to Indiana.

INDOT recently revisited scoping road improvement and design projects and advancing their development with a new emphasis on using a systemic approach and cost-effectiveness. A new design paradigm based on "practical design" was formulated and is now being implemented in Indiana. Safety consideration is a central component in this newly adopted approach. With this greater focus on safety, INDOT engineers and road
designers are attempting to find improvement and design solutions which are budget-conscious while meeting a project's well-defined objectives. The goal is to build more and better roads within the limited budget.

This study generates results that are crucial for evaluating the safety effects of traffic control and road design decisions. One popular tool which may facilitate the implementation of these results is the Interactive Highway Safety Design Model (IHSDM), a tool developed by the FHWA which applies the Highway Safety Manual (HSM) crash prediction methodology. The IHSDM provides estimates of crash frequencies, types, and severity that can assist in identifying possible safety problems and evaluate the effects of various design improvements at the project-level. The tool can help justify the selection of one design improvement over another.

There are four main components of the HSM that are implemented through the IHSDM to predict crashes for different road facility types: (1) Safety performance functions (SPFs), (2) crash modification factors/functions (CMFs), (3) calibration factors, and (4) crash proportions. The predictive components must be calibrated in order to properly account for jurisdiction-specific conditions. However, the IHSDM imposes constraints which must be considered in the calibration of the HSM predictive method. The functional forms of the SPFs and CMFs (developed under certain base conditions) are fixed, may not be altered, and there are no provisions for adding new CMFs in the IHSDM. A comprehensive calibration method is needed which can facilitate the transfer of jurisdiction-specific CMFs to the IHSDM.

### 1.2 Scope of Work and Research Objectives

The scope of this project includes safety improvements implemented on INDOT-administered road elements (segments and intersections) in both rural and urban areas. The first objective of this study is to update the CRFs for various traffic, geometric, and other improvements which may be applied in Indiana. The comprehensive list of CRFs will be developed based on CRFs from Indiana and other applicable sources with conditions similar to Indiana. The other objective of this study is to calibrate the IHSDM tool for Indiana conditions. A new approach to this task will be proposed using all the available pieces of knowledge pertaining to Indiana while preserving consistency with the IHSDM, thus ensuring the integrity of the results. This will be done by implementing the results of the Indiana CMFs, whenever possible, into the IHSDM software through reconciliation with the default CMFs. This part of the study will also involve developing new Indiana SPFs that may be estimated in tandem with the CMFs and in a format compatible with the IHSDM. This study is expected to provide a method for supporting safety-related design and improvement decisions in Indiana.

### 1.3 Report Organization

This report is organized as follows:

- Chapter 1, Introduction
- Chapter 2, Existing Crash Reduction Factors Suitable for Indiana
- Chapter 3, Methodology for Calibrating the IHSDM
- Chapter 4, Calibration Data
- Chapter 5, Calibrating the IHSDM for Indiana
- Chapter 6, Summary and Conclusions
- Appendices


## 2. EXISTING CRASH REDUCTION FACTORS SUITABLE FOR INDIANA

### 2.1 Background

CRFs and the related CMFs provide a quantitative assessment of the impact on crash frequency for various types and severities of crashes. Whereas CRFs depict the percent change in crashes following the implementation of a countermeasure on a roadway facility, CMFs can be thought of as a multiplicative factor for determining the number of crashes after the implementation of the countermeasure (Scurry, n.d.). CMFs are related to CRFs through the relation shown in Equation 2.1:

$$
\begin{equation*}
C M F=1-\left(\frac{C R F}{100}\right) \tag{2.1}
\end{equation*}
$$

A variety of methods have been utilized for determining CRFs/CMFs, including cross-sectional studies (for example, SPF regression models), before-and-after studies, and expert panels, among others (Wu, Lord, \& Zou, 2015). In the case that a full SPF with all variables has been estimated, CMFs may be determined from the SPF coefficients as in Tarko et al. (2015). CMFs derived from before-and-after studies consider the safety performance before and after the application of one or more countermeasures at the considered sites (Wu et al., 2015). The empirical Bayes approach popularized by Hauer (1997) is one such method utilized in before-and-after studies to help account for the regression-to-the-mean effect (tending to cause an overestimation of the crash reduction potential) which may occur. In this research, studies that have used regression modeling, before-andafter studies, and other methods are consulted.

This chapter provides information on the existing CRFs and CMFs for various geometric, traffic, pavement, and other improvements that have been found to affect safety on roadway segments and intersections in
urban and rural areas. The majority of the factors/ functions were obtained from the Crash Modification Factors Clearinghouse, a continuously updated repository funded by the Federal Highway Administration and maintained by the University of North Carolina Highway Safety Research Center (FHWA \& UNC HSRC, 2017). The Clearinghouse provides more than 5000 CRFs for both urban and rural areas in the United States, Canada, and internationally. Many of the safety improvements have multiple CRF values based on multiple studies, and there are also similar safety improvements which differ only by the wording in their names. Thus, it is necessary for the user to make a judgement call on which is most appropriate for their situation. Various criteria were used to identify the factors/ functions most suitable for Indiana conditions. These criteria and a summary of the selected safety improvements and associated CRFs/CMFs are discussed in the sections that follow.

### 2.2 Criteria for Selecting CRFs/CMFs

Three criteria were utilized in determining CRFs suitable for segments and intersections in Indiana: the state or states where the CRF study was conducted, the star quality rating (from the CMF Clearinghouse), and the study timeframe. Based on these criteria, each CRF was classified in one of three criteria levels: first-tier, secondtier, or third-tier.

The first-tier criteria level includes Indiana and other nearby states that share a border and/or are expected to have similar environmental conditions and driving culture to Indiana (see Table 2.1). Additionally, CRFs in this level have a Clearinghouse star quality rating of 4 or 5 stars (out of a maximum 5 stars). A high star quality rating indicates a high-quality study design and estimation methodology, a large data sample from multiple years and sites, and data from a variety of states and geographies (FHWA \& UNC HSRC, 2017). These CRFs also have limited standard error (as compared to the CRF value) and control for potential biases. Most studies with a high star quality rating use a well-established methodology such as the Empirical Bayes or Full Bayes to account for the regression-to-the-mean bias and enhance the estimation accuracy. Finally, only CRFs from studies in the past 10 years are included in the first-tier criteria level so as to reduce the influence of changing conditions and driving culture over time.

If a CRF does not meet one or more of the first-tier criteria, then it is considered for the second-tier criteria level.

TABLE 2.1
Summary of Criteria used for Determining Most Suitable Existing CRFs

| Criteria level | States | CMF Clearinghouse <br> star quality rating | Study timeframe |
| :--- | :--- | :--- | :--- |
| First-tier | IL, IN, IA, KY, MI, MO, OH, WI | 4 or 5 stars | Past 10 years |
| Second-tier | AR, KS, MN, NE, NC, ND, OK, PA, SD, TN, VA, WV | 3 or more stars | Past 15 years |
| Third-tier | Not meeting first- or second-tier criteria |  |  |

This level includes states outside of the first-tier states and which do not immediately border Indiana. The environmental conditions and driving culture in these states is expected to be somewhat different than Indiana. Additionally, the CRFs must meet a star quality rating of at least 3 stars and come from a study conducted within the past 15 years to be classified on the secondtier criteria level. If a study does not meet one or more of the first- or second-tier criteria, then it is considered to be part of the third-tier criteria level.

The main purpose for differentiating among the three tiers is to gather all the available CMFs so they can be readily available for practitioners. The tiers do not affect the use of the CMF selection from Appendix A.

### 2.3 Safety Improvements and CRFs

A total of 82 safety improvements were identified under 16 different categories (see Table 2.2). The categories of safety improvements included access management, alignment, highway lighting, intersection geometry, intersection traffic control, ITS and advanced technology, pavement, pedestrians, railroads, roadside, road diet, roadway delineation, segments, shoulder treatment, signs, and speed management.

For each safety countermeasure, the CRF and CMF values for urban and/or rural conditions, state(s) where the study was conducted, and applicable crash and roadway types were noted. The complete CRF/CMF table is contained in Appendix A. The categories of safety countermeasures and the CRF/CMF studies are detailed below.

## A. Access Management

1. Install two-way left-turn lane (TWLTL). Persaud, Lyon, Eccles, Carter, et al. (2008) conducted a study evaluating the safety impacts of installing TWLTLs on two-lane roads in rural and urban areas in Arkansas, California, Illinois, and North Carolina. However, the safety impact was only found to be significant in the rural areas. The researchers developed CMFs for all crashes and injury crashes, as well as for rear-end crashes.
2. Replace TWLTL with raised median. Utilizing data from urban areas in Nevada, Mauga and Kaseko (2010) developed CMFs for the replacement of a TWLTL with a raised median on principal arterials, minor arterials, and collectors. CMFs were developed for total crashes, PDO crashes, and injury crashes. Furthermore, CMFs were estimated for rear-end, sideswipe, angle, and headon crashes.
3. Driveway density. For driveway density in rural areas, a study was conducted by Fitzpatrick, Park, and Schneider (2008) using data from Texas. The researchers developed separate CMFs in the form of functions for all crashes on two-lane and four-lane highways. For urban areas, CMFs in the form of functions were developed by Mauga and Kaseko (2010) for roads classified as principal arterials, minor arterials, or collectors in Nevada. Separate sets of CMFs were developed for facilities with TWLTLs and for facilities with raised medians. The CMFs were provided for all crashes, PDO crashes, and injury crashes. In addition, CMFs were estimated for rear-end and rightangle crashes.

## B. Alignment

1. Flatten crest of curve. Using data from Ohio, Hovey and Chowdhury (2005) developed CMFs for total and injury crashes occurring on rural arterials and collectors.
2. Reduce the average grade rate by $\mathrm{X} \%$. Tarko et al. (2015) presented CMFs for PDO and injury crashes on rural two-lane roads in Indiana. The average grade $\bar{G}$ along a segment of length $L$ is calculated based on splitting the entire segment into grades and vertical curves:

$$
\bar{G}=\frac{1}{2 L}\left[L_{1}\left(G_{1}+G_{2}\right)+L_{2}\left(G_{2}+G_{3}\right)+\ldots+L_{n}\left(G_{n}+G_{n+1}\right)\right]
$$

where: $n$ is the total number of sub-segments that are grades or vertical curves, $L$ is the entire segment length, $L_{i}$ is the length of sub-segment $i, G_{i}$ is the grade rate at the beginning of sub-segment $i$, and $G_{n+1}$ is the grade rate at the end of the entire segment. The expression gives an exact result.
3. Reduce the average degree of curve by X degrees. CMFs for PDO and injury crashes on Indiana rural two-lane roads were presented by Tarko et al. (2015). The average degree of curve $\bar{D}$ along a segment of length $L$ is calculated based on splitting the entire segment into tangents, spirals, and circular curves:

$$
\bar{D}=\frac{1}{2 L}\left[L_{1}\left(D_{1}+D_{2}\right)+L_{2}\left(D_{2}+D_{3}\right)+\ldots+L_{n}\left(D_{n}+D_{n+1}\right)\right]
$$

where: $n$ is the total number of sub-segments that are tangents, spirals, or circular curves, $L$ is the entire segment length, $L_{i}$ is the length of sub-segment $i, D_{i}$ is the degree of curve at the beginning of sub-segment $i, D_{n+1}$ is the degree of curve at the end of the entire segment. Although the degree of curve on a tangent is zero, these sub-segments are included in the equation to preserve the simplicity and consistency of the expression. The expression gives an exact result.

## C. Highway Lighting

1. Install lighting on a roadway segment. Harkey et al. (2008) presented CMFs for roadway lighting on segments, including for all crashes and injury crashes occurring during the nighttime.
2. Install lighting at a signalized intersection. Bullough, Donnell, and Rea (2013) examined the impact that lighting has on crashes at signalized intersections in Minnesota. Separate CMFs were developed for all crashes in rural and urban areas occurring during the daytime and nighttime.
3. Install lighting at a stop-controlled intersection. Bullough et al. (2013) also researched the effects of installing lighting at stop-controlled intersections located in rural and urban locations in Minnesota.
4. Install lighting at an interchange. CMFs were estimated for total and injury crashes on arterial and collector roads in Ohio by Hovey and Chowdhury (2005).

## D. Intersection Geometry

1. Add a left-turn lane on one major approach to a signalized intersection. Harwood et al. (2003) provided separate CMF values for three- and four-leg intersections in both rural and urban areas utilizing a broad dataset containing states from throughout the country.

TABLE 2.2
Summary of Identified Safety Countermeasures

| Category | Countermeasure |
| :---: | :---: |
| Access management | Install two-way left-turn lane (TWLTL) <br> Replace TWLTL with raised median <br> Reduce driveway density by X driveways per mile |
| Alignment | Flatten crest of curve <br> Reduce the average grade rate by $\mathrm{X} \%$ <br> Reduce the average degree of curve by X degrees |
| Highway lighting | Install lighting on a roadway segment <br> Install lighting at a signalized intersection Install lighting at a stop-controlled intersection Install lighting at an interchange |
| Intersection geometry | Add a left-turn lane on one major approach to a signalized intersection Add a left-turn lane on one major approach to an unsignalized intersection Add a right-turn lane on one major approach to a signalized intersection Add a right-turn lane on one major approach to an unsignalized intersection Convert diamond interchange to diverging diamond interchange (DDI) Convert intersection on low-speed road to a roundabout Convert intersection on high-speed road to a roundabout Convert intersection to a single-lane roundabout Convert intersection to a multilane roundabout Convert two-way stop-controlled intersection to a roundabout Convert all-way stop-controlled intersection to a roundabout Convert signalized intersection to a roundabout Convert a non-controlled or yield-controlled intersection to a roundabout Convert two-way stop-controlled intersection to J-turn intersection Improve left-turn lane offset to create positive offset Improve intersection sight distance |
| Intersection traffic control | Change left-turn phasing on one approach from permitted to protected/permitted phasing Change left-turn phasing on more than one approach from permitted to protected/permitted phasing <br> Change left-turn phasing from permitted or permitted/protected to protected-only phasing Supplement left-turn phasing from at least one permitted approach with flashing yellow arrow Change left-turn phasing from protected/permitted to flashing yellow arrow <br> Change left-turn phasing from protected to flashing yellow arrow <br> Convert two-way stop control to all-way stop control <br> Improve signal visibility <br> Increase yellow change interval (1.0 seconds) <br> Increase all-red clearance interval (average of 1.1 seconds) <br> Increase yellow interval (average of 0.8 seconds) and add all-red interval (average of 1.2 seconds) <br> Install transverse rumble strips on approaches to stop-controlled intersection <br> Install new traffic signal at previously stop-controlled intersection <br> Replace standard stop sign with flashing LED stop sign <br> Retime signal change intervals to Institute of Transportation Engineers (ITE) standards |
| ITS and advanced technology | Install actuated advance intersection warning system at high-speed intersection <br> Install changeable horizontal curve speed warning signs <br> Install variable speed limit signs <br> Install "Vehicle Entering When Flashing" (VEWF) system with advance post mounted signs on major approach and loops on minor approach |
| Pavement | Improve pavement condition from poor (critical condition index below 60) to good (critical condition index above 70) |

TABLE 2.2
(Continued)

| Category | Countermeasure |
| :---: | :---: |
| Pedestrians | Construct pedestrian bridge or tunnel <br> Install High intensity Activated crossWalK (HAWK) at intersection Install sidewalk |
| Railroads | Build grade-separated crossing Eliminate railroad crossing Install gates at crossings with signs Upgrade signs to flashing lights |
| Roadside | Increase median width from 10 feet to X feet <br> Install guardrail <br> Install cable median barrier (high-tensioned) on depressed median of 50 feet wide or wider <br> Install concrete median barrier <br> Change in sideslope from $1 \mathrm{~V}: 3 \mathrm{H}$ to $1 \mathrm{~V}: 4 \mathrm{H}$ <br> Change in sideslope from $1 \mathrm{~V}: 4 \mathrm{H}$ to $1 \mathrm{~V}: 6 \mathrm{H}$ <br> Remove or relocate fixed objects outside of clear zone |
| Road diet | Re-stripe four-lane undivided road to three-lane (with TWLTL) |
| Roadway delineation | Add no passing striping <br> Install centerline rumble strips <br> Install shoulder rumble strips <br> Install centerline plus shoulder rumble strips <br> Install edgeline pavement markings on curves <br> Install edgeline pavement markings on tangent sections Install raised pavement markers |
| Segments | Increase in number of through lanes by X lanes <br> Convert two-lane roadway to four-lane divided roadway <br> Convert 12 foot lanes and 6 foot shoulders to X foot lanes and Y foot shoulders <br> Extend on-ramp acceleration lane by 30 meters (about 100 feet) <br> Extend off-ramp deceleration lane by 30 meters (about 100 feet) <br> Install passing relief lane <br> Increase lane width by X feet |
| Shoulder treatment | Increase right shoulder width by X feet Increase left/inside shoulder width by X feet |
| Signs | Install chevron signs on horizontal curves Increase retroreflectivity of stop signs Install flashing beacons at stop-controlled intersections |
| Speed management | Change posted speed by X mph Set appropriate speed limit |

2. Add a left-turn lane on one major approach to an unsignalized intersection. CMF values from the Harwood et al. (2003) study were also given for three- and four-leg unsignalized intersections.
3. Add a right-turn lane on one major approach to a signalized intersection. A CMF value was estimated by Harwood et al. (2003) for four-leg intersections in urban areas.
4. Add a right-turn lane on one major approach to an unsignalized intersection. A CMF value was estimated by Harwood et al. (2003) for four-leg intersections in rural areas.
5. Convert diamond interchange to diverging diamond interchange (DDI). Utilizing data from Kentucky, Missouri, New York, and Tennessee, Hummer et al. (2016) developed CMFs for total, injury, angle, rear-end, sideswipe, and single-vehicle crashes in urban areas.
6. Convert intersection on low-speed road to a roundabout. Utilizing data from Wisconsin, Qin, Bill, Chitturi, and Noyce (2013) calculated CMF values for intersection conversions on low-speed roads (posted speeds less than 45 mph on all approaches). The values were determined for all crashes and injury crashes and applicable for either urban or rural areas.
7. Convert intersection on high-speed road to a roundabout. The same study by Qin, Bill, et al. (2013) also determined CMF values for intersection conversions where at least one of the approaches was high-speed (speeds of 45 mph or greater).
8. Convert intersection to a single-lane roundabout. Qin, Bill, et al. (2013) estimated CMFs for all crashes and injury crashes for intersection conversions to a singlelane roundabout.
9. Convert intersection to a multilane roundabout. Qin, Bill, et al. (2013) estimated CMFs for all crashes and injury crashes for intersection conversions to a multilane roundabout.
10. Convert two-way stop-controlled intersection to a roundabout. Rodegerdts et al. (2007) and Qin, Bill et al. (2013) estimated CMFs applicable for urban and rural conversions of two-way stop-controlled intersections to roundabouts. The former study used data from a variety of states spread across the US, while the latter used data from Wisconsin. The CMFs were developed for total and injury crashes.
11. Convert all-way stop-controlled intersection to a roundabout. Rodegerdts et al. (2007) and Qin, Bill, et al. (2013) developed CMFs for total and injury crashes, applicable for urban and rural conversions of all-way stop-controlled intersections to roundabouts.
12. Convert signalized intersection to a roundabout. Rodegerdts et al. (2007), Gross, Lyon, Persaud, and Srinivasan (2013), and Qin, Bill, et al. (2013) employed data from across the US to evaluate the impact of converting signalized intersections to roundabouts. The Rodegerdts et al. (2007) and Qin, Bill, et al. (2013) studies were developed for total and injury crashes in urban and rural areas, while the Gross et al. (2013) study was applicable for total and injury crashes in urban areas.
13. Convert a non-controlled or yield-controlled intersection to a roundabout. Qin, Bill, et al. (2013) utilized urban and rural Wisconsin data to determine CMFs for total and injury crashes following the conversion of non-controlled or yield-controlled intersections to roundabouts.
14. Convert two-way stop-controlled intersection to J-turn intersection. CMFs were estimated by Edara, Sun, and

Breslow (2014) for total and injury crashes following the installation of J-turn intersections located on rural fourlane divided, high-speed roads in Missouri.
15. Improve left-turn lane offset to create positive offset. Persaud, Lyon, Eccles, Lefler, and Gross (2009) estimated CMFs for total, injury, left-turn, and rear-end crashes using data from four-leg intersections in Wisconsin.
16. Improve intersection sight distance. Gan, Shen, and Rodriguez (2005) provided CMFs for intersection sight distance improvements. CMFs were given for total, right-angle, left-turn, and sideswipe crashes. Depending on the type of crash, the CMFs were developed based on data from Alaska, Arizona, California, Iowa, Kentucky, Minnesota, and Missouri.

## E. Intersection Traffic Control

1. Change left-turn phasing on one approach from permitted to protected/permitted phasing. Utilizing North Carolina and Canadian data, Srinivasan et al. (2011) developed CMFs for urban total, injury, left-turn, and rear-end crashes at four-leg signalized intersections.
2. Change left-turn phasing on more than one approach from permitted to protected/permitted phasing. Srinivasan et al. (2011) developed CMFs total, injury, left-turn, and rear-end crashes at urban four-leg signalized intersections.
3. Change left-turn phasing from permitted or permitted/ protected to protected-only phasing. Utilizing data from North Carolina, Harkey et al. (2008) provided CMFs for total and left-turn crashes for urban signalized intersections.
4. Supplement left-turn phasing from at least one permitted approach with flashing yellow arrow. Srinivasan et al. (2011) used data from urban four-leg signalized intersections in North Carolina, Oregon, and Washington to estimate CMFs for total and left-turn crashes.
5. Change left-turn phasing from protected/permitted to flashing yellow arrow. Srinivasan et al. (2011) developed CMFs for total and left-turn crashes occurring at fourleg signalized intersections in urban areas.
6. Change left-turn phasing from protected to flashing yellow arrow. CMFs were developed for total and leftturn crashes at urban four-leg signalized intersections by Srinivasan et al. (2011).
7. Convert two-way stop control to all-way stop control. Simpson and Hummer (2010) developed CMFs for the total, injury, frontal impact, and ran stop sign crash types at four-leg intersections in North Carolina.
8. Improve signal visibility. El-Basyouny, Sayed, El Esawey, and Pump (2012) estimated CMFs for the application of a variety of signal improvements at Canadian four-leg intersections in urban areas. The CMFs were developed for daytime and nighttime PDO and injury crashes.
9. Increase yellow change interval ( 1.0 seconds). CMFs were estimated by Srinivasan et al. (2011) using data from urban three- and four-leg signalized intersections in California and Maryland. The CMFs were provided for total, injury, rear-end, and angle crashes.
10. Increase all-red clearance interval (average of 1.1 seconds). The study by Srinivasan et al. (2011) was consulted. CMFs were developed for total, injury, rear-end, and angle crashes at urban three- and four-leg signalized intersections.
11. Increase yellow interval (average of 0.8 seconds) and add all-red interval (average of 1.2 seconds). In the study by Srinivasan et al. (2011), the authors estimated the CMFs
for total, injury, rear-end, and angle crashes at urban three- and four-leg signalized intersections.
12. Install transverse rumble strips on approaches to stopcontrolled intersection. Using data from Iowa and Minnesota, Srinivasan et al. (2010) developed CMFs for total crashes and different crash severity levels at rural three-leg and four-leg intersections (located on major collector roads).
13. Install new traffic signal at previously stop-controlled intersection. CMFs were provided by McGee, Taori, and Persaud (2003) for urban areas (using California, Florida, Maryland, Virginia, Wisconsin, and Canadian data) and by Harkey et al. (2008) for rural areas (using California and Minnesota data). The urban CMFs were given separately for total injury, right-angle injury, and rear-end injury crashes at three-leg and four-leg intersections. The rural CMFs were given for total, right-angle, rear-end, and left-turn crashes, applicable for three-leg or four-leg intersections.
14. Replace standard stop sign with flashing LED stop sign. A study by Davis, Hourdos, and Xiong (2014) involved the estimation of a CMF for right-angle crashes on twolane Minnesota roads in which a flashing LED stop sign had been installed.
15. Retime signal change intervals to the Institute of Transportation Engineers (ITE) standards. Retting, Chapline, and Williams (2002) developed CMFs for urban fourleg signalized intersections using data from New York. Separate CMFs were developed for the overall total and injury crashes, as well as total and injury crashes of the following types: rear-end, right-angle, and vehicle/bicycle and vehicle/pedestrian.

## F. ITS and Advanced Technology

1. Install actuated advance intersection warning system at high-speed intersection. Using data from Nebraska, Appiah, Naik, Wojtal, and Rilett (2011) developed CMFs for total, injury, rear-end, and right-angle crashes applicable to intersections where the major road was a highspeed four-lane divided highway.
2. Install changeable horizontal curve speed warning signs. Hallmark, Hawkins, and Smadi (2015) developed a CMF for total crashes on rural two-lane roads using data from a number of states spread across the country.
3. Install variable speed limit signs. A CMF was estimated for total crashes by Bham et al. (2010) using data from urban principal arterial interstates in Missouri.
4. Install "Vehicle Entering When Flashing" (VEWF) system with advance post mounted signs on major approach and loops on minor approach. Simpson and Troy (2013) estimated CMFs for total, injury, and target crashes (angle, head-on, left-turn, and right-turn) occurring on North Carolina highways with mainline approach speeds of $35-55 \mathrm{mph}$.

## G. Pavement

1. Improve pavement condition from poor (critical condition index below 60) to good (critical condition index above 70). Zeng, Fontaine, and Smith (2014) estimated CMFs for total crashes and for injury crashes on rural two-lane roads in Virginia.

## H. Pedestrians

1. Construct pedestrian bridge or tunnel. Gan et al. (2005) provided a CMF for pedestrian-related crashes in urban areas based on data from Alaska, Arizona, Kentucky, and Missouri.
2. Install High intensity Activated crossWalK (HAWK) at intersection. Fitzpatrick and Park (2010) developed CMFs for total, severe injury, and pedestrian-related crashes in urban areas utilizing Arizona data. The analyzed sites were for crosswalks crossing four- to six-lane roads.
3. Install sidewalk. Gan et al. (2005) provided an urban CMF for pedestrian-related crashes based on data from Alaska, Arizona, Kentucky, Missouri, and Oklahoma.

## I. Railroads

1. Build grade-separated crossing. Based on results from Iowa, Gan et al. (2005) provided a CMF for total crashes that may be expected after a grade-separated railroad crossing has been built.
2. Eliminate railroad crossing. Additionally, Gan et al. (2005) provided a CMF for total crashes for the elimination of a railroad crossing.
3. Install gates at crossings with signs. Park and Saccomanno (2005) utilized data from Canada to estimate a CMF applicable to total crashes on arterials, collectors, and local roads.
4. Upgrade signs to flashing lights. The same study by Park and Saccomanno (2005) estimated a CMF for total crashes on arterials, collectors, and local roads based on the Canadian data.

## J. Roadside

1. Increase median width. Stamatiadis, Pigman, Sacksteder, Ruff, and Lord (2009) developed CMFs for increasing the median width on rural four-lane divided highways using data from California, Kentucky, and Minnesota.
2. Install guardrail. Gan et al. (2005) provided CMFs for total, minor injury, severe injury, and run-off-the-road crashes based on data from Arizona, Iowa, Indiana, Kentucky, and Missouri.
3. Install cable median barrier (high-tensioned) on depressed median of 50 feet wide or wider. Villwock, Blond, and Tarko (2009) developed CMFs for rural principal arterial interstates in Indiana. CMF values were provided for multiple-vehicle, opposite direction crashes and for single-vehicle crashes.
4. Install concrete median barrier. Tarko, Villwock, and Blond (2008) estimated CMFs for single-vehicle and multiple-vehicle crashes on rural interstates using an extensive dataset from states across the country, including Indiana.
5. Change in sideslope from $1 \mathrm{~V}: 3 \mathrm{H}$ to $1 \mathrm{~V}: 4 \mathrm{H}$. Elvik and Vaa (2004) provided CMFs for PDO and injury crashes in rural areas.
6. Change in sideslope from $1 \mathrm{~V}: 4 \mathrm{H}$ to $1 \mathrm{~V}: 6 \mathrm{H}$. Elvik and Vaa (2004) provided CMFs for PDO and injury crashes in rural areas.
7. Remove or relocate fixed objects outside of clear zone. Hovey and Chowdhury (2005) estimated CMFs for total and injury crashes on arterials and collectors in Ohio.

## K. Road Diet

1. Re-stripe four-lane undivided road to three-lane (with TWLTL). Using data from California, Iowa, and Washington, Harkey et al. (2008) developed a CMF applicable to total crashes occurring on minor arterials in urban areas.

## L. Roadway Delineation

1. Add no passing striping. The CMFs for no passing striping came from a study by Gan et al. (2005). The authors provided a CMF for total crashes on rural roads based on data from Montana. Furthermore, CMFs for head-on and sideswipe crashes on rural roads (based on Kentucky and Missouri data) were given in the report.
2. Install centerline rumble strips. CMFs for the installation of centerline rumble strips were developed for rural and urban two-lane roads in a study by Torbic et al. (2009). The authors used data from a variety of states spread across the county. The CMFs were for total and injury crashes on the rural roads, as well for total and injury target crashes (head-on and opposite-direction sideswipe). For urban roads, the significant CMFs were for total and injury target crashes.
3. Install shoulder rumble strips. The same study by Torbic et al. (2009) was consulted for CMFs associated with the installation of shoulder rumble strips on rural two-lane roads and rural freeways. Data from Minnesota, Missouri, and Pennsylvania was used for estimating the CMFs, which were provided for both total and injury single-vehicle run-off-the-road crashes.
4. Install centerline plus shoulder rumble strips. Kay et al. (2015) and Lyon, Persaud, and Eccles (2015) developed rural CMFs for the installation of centerline rumble strips in combination with shoulder rumble strips. Using data from Michigan, Kay et al. (2015) developed a CMF for total crashes on two-lane roads. The study by Lyon et al. (2015) utilized data from Kentucky, Missouri, and Pennsylvania to develop CMFs for total, injury, head-on, run-off-the-road, and opposite-direction sideswipe crashes.
5. Install edgeline pavement marking on curves. Tsyganov, Warrenchuk, and Machemehl (2009) estimated CMFs for edgeline installations on curves for rural two-lane roads. Using data from Texas, the CMFs were developed for total, run-off-the-road, and speed-related (nighttime) crashes.
6. Install edgeline pavement markings on tangent sections. Similarly, Tsyganov et al. (2009) developed CMFs for edgeline installations on tangent sections of rural twolane roads. CMFs were provided for total, run-off-theroad, and speed-related (nighttime) crashes.
7. Install raised pavement markers. Bahar et al. (2004) estimated CMFs for total nighttime crashes on rural two-lane highways and four-lane freeways. Data from the two-lane facilities was obtained from Illinois, New Jersey, New York, and Pennsylvania, while data from the four-lane facilities was obtained from Missouri, New York, Pennsylvania, and Wisconsin. Separate CMFs were provided based on the road's AADT and the curve radius $(\mathrm{R}=>1640$ feet or $\mathrm{R}<1640$ feet) for two-lane highways and based solely on the road's AADT for fourlane freeways.

Note: To apply this countermeasure to a two-lane highway segment with multiple curves, the segment
would need to be subdivided into the part(s) of the segment with $\mathrm{R}=>1640$ feet (which includes tangent sections) and the part(s) of the segment with $\mathrm{R}<1640$ feet. The separate CMFs for the different curve radii R may be applied to these distinct parts.

## M. Segments

1. Increase in number of through lanes. Based on Indiana conditions, Tarko et al. (2015) presented CMFs for PDO and injury crashes for urban multilane roadway segments.
2. Convert two-lane roadway to four-lane divided roadway. Using Florida data, Ahmed, Abdel-Aty, and Park (2015) developed CMFs for urban and rural total, PDO, and injury crashes, applicable for the conversion of a twolane roadway to a four-lane divided roadway.
3. Change in lane and shoulder width from 12 foot lane width and 6 foot shoulder width. CMFs for the effect of changing the lane and shoulder width from base conditions of 12 foot lane width and 6 foot shoulder width were developed by Gross, Jovanis, Eccles, and Chen (2009) using data from rural two-lane roadways in Pennsylvania. The CMFs were applicable for run-off-the-road, head-on, and sideswipe crashes. Furthermore, Le and Porter (2013) developed CMFs for lane and shoulder width combinations using data from urban and suburban arterials in Illinois. The researchers provided the CMFs as functions for injury crashes.
4. Extend on-ramp acceleration lane by 30 meters (about 100 feet) at grade-separated junction. Elvik and Vaa (2004) presented a CMF for total crashes. The CMF applied only to lanes up to 200 meters ( 656 feet) in length.
5. Extend off-ramp deceleration lane by 30 meters (about 100 feet) at grade-separated junction. A CMF for total crashes was given by Elvik and Vaa (2004), applicable for lanes up to 200 meets ( 656 feet) in length.
6. Install passing relief lane. Bagdade et al. (2012) estimated CMFs for rural two-lane roads using Michigan data. The researchers determined CMFs for total, injury, target (headon, rear-end, run-off-the-road, and sideswipe), peak month (June, July, and August) and off-peak month crashes for passing relief lanes between 1.0 and 2.9 miles long.
7. Increase in lane width. Tarko et al. (2015) developed CMFs for PDO and injury crashes for urban and rural two-lane and multilane roadway segments, using data from Indiana.

## N. Shoulder Treatment

1. Increase right shoulder width. Based on data from Indiana, Tarko et al. (2015) developed CMFs for urban and rural two-lane and multilane facilities. The urban CMFs were for PDO crashes on two-lane and multilane roads, and the rural CMFs were for PDO and injury crashes on two-lane roads and injury crashes on multilane roads.
2. Increase left/inside shoulder width. Tarko et al. (2015) provided CMFs for injury crashes on urban multilane roads and PDO and injury crashes on rural multilane roads in Indiana.

## O. Signs

1. Install chevron signs on horizontal curves. Srinivasan et al. (2009) developed CMFs for rural total, injury,
lane departure, nighttime, and nighttime lane departure crashes utilizing data from Washington State.
2. Increase retroreflectivity of stop signs. Persaud, Lyon, Eccles, Lefler, and Amjadi (2008) estimated CMFs for total, injury, right-angle, rear-end, daytime, and nighttime crashes for stop-controlled intersections in Connecticut and South Carolina, which included both three- and fourleg intersections.
3. Install flashing beacons at stop-controlled intersections. Srinivasan et al. (2008) determined CMFs for total crashes in rural and urban areas utilizing data from two-lane highways in North Carolina and South Carolina.

## P. Speed Management

1. Change posted speed limit. CMFs for lowering or raising the posted speed limit in various increments were estimated by Parker (1997) using data from twenty-two states across the US.
2. Set appropriate speed limit. A CMF value for total crashes was provided by Gan et al. (2005) based on Kentucky, Missouri, and Montana data.

## 3. METHODOLOGY FOR CALIBRATING THE IHSDM

### 3.1 Background

Among the main components of the HSM predictive method, SPFs play perhaps the greatest role in predicting crashes. Calibration efforts focusing on updating the HSM SPFs have been conducted by researchers for several states, including Kansas (Lubliner, 2011; Lubliner \& Schrock, 2012), Missouri (Sun, Brown, Edara, Claros, \& Nam, 2013), Oregon (Dixon, Monsere, Xie, \& Gladhill, 2012), South Dakota (Qin, Rahman Shaon, \& Chen, 2016), Utah (Brimley, Saito, \& Schultz, 2012), and Virginia (Kweon, Lim, Turpin, \& Read, 2014). Some researchers have also developed jurisdic-tion-specific SPFs that have additional variables beyond the base HSM exposure variables, including the following: shoulder width, presence of rumble strips, speed limit, truck percentages, and regional variables (Brimley et al., 2012; Qin et al., 2016). More accurate results may be possible by developing the SPFs with the full functional form rather than adding CMFs separately to the base SPF. However, it is not possible to modify the SPF structure in the IHSDM, so calibration must be consistent with the constraints of the software.

CMFs comprise the second component of the HSM predictive method. The HSM CMFs are compiled from a variety of sources which do not necessarily have the same base conditions. National and international studies have found that the HSM CMFs may not be suitable for their particular area (Abdel-Aty et al., 2014; Sacchi, Persaud, \& Bassani, 2012). These results indicate the need for calibrating not only the SPFs but also the CMFs to local conditions. The IHSDM expresses CMFs in various forms that differ across the CMFs and may be inconsistent with the format used by others in past studies. In order to facilitate transferring the past
research results to the IHSDM, a calibration procedure should be able to deal with these differences.

Calibration factors are the third component of the HSM predictive method. Numerous researchers have updated the calibration factors for their respective jurisdictions (Banihashemi, 2011; Fitzpatrick, Schneider, \& Carvell, 2006; Mehta, \& Lou, 2013; Persaud, Lord, \& Palmisano, 2002; Shin, Lee, \& Dadvar, 2014; Sun, Magri, Shirazi, Gillella, \& Li, 2011; Xie, Gladhill, Dixon, \& Monsere, 2011). Researchers have found that calibration factors may vary not only across different parts of a region, but also based on geometric characteristics (for instance, tangent versus horizontal curve segments) (Fitzpatrick, Schneider, et al., 2006). Mehta and Lou (2013) proposed an approach that involves calibration factor estimation as a special case of SPF estimation. The authors also developed an area-specific SPF (including AADT, segment length, lane width, and speed limit) which they found to outperform the adjusted base SPFs with calibration factors.

Finally, other researchers have examined the applicability of the IHSDM within and outside of the US, as well as its calibration scope (Bansen \& Passetti, 2005; Dominguez-Lira, Castro, Pardillo-Mayora, \& GascónVarón, 2010; Donnell, Gross, Stodart, \& Opiela, 2009; Koorey, 2010; Marchionna, Perco, \& Falconetti, 2012; Martinelli, La Torre, \& Vadi, 2009). Donnell et al. (2009) provided recommendations on the need to expand the capabilities of the IHSDM's design consistency module to consider low-speed, complex alignments. Koorey (2010) incorporated crash proportions data from New Zealand's rural two-lane highways to predict crashes using the IHSDM, finding it to provide superior "local calibration" than by using sub-national calibration parameters. Bansen and Passetti (2005) used the IHSDM in evaluating the impacts of various geometric design alternatives on a 23-mile long corridor. The authors discussed the intensive data needs of the IHSDM, for this reason suggesting that its use may be better suited to the design community where data is more readily available.

There has been a substantial amount of work directed towards calibrating the HSM for regional/state conditions. The majority of previous studies focused on calibrating the SPFs. Separate estimation of SPFs and CMFs is questionable. Furthermore, the previous literature highlighted some of the constraints of implementing the HSM predictive method in the IHSDM. A methodology is needed that estimates the SPFs and CMFs and allows incorporation of CMFs from past research into a form compatible with the IHSDM.

### 3.2 Methodological Framework

To meet the identified void in the IHSDM calibration methodology, a comprehensive approach to calibrating the components of the HSM predictive method is proposed here that regards the structure of the IHSDM. First, the CMFs in their IHSDM format are adjusted to the local data and past results. Then, those CMFs are converted to an overall CMF and incorporated
in the comprehensive safety model as an offset variable to estimate the expected crash frequency. This method preserves the crash prediction consistency, and the step to estimate the calibration parameter is eliminated.

Chapters 10 and 11 of the HSM (AASHTO, 2010) present the general form of the crash prediction model for rural two-lane and rural multilane roadway facilities. The model is presented here in Equation 3.1. The model form is similar for urban/suburban arterials, with the addition of terms for vehicle-pedestrian and vehiclebicycle collisions.

$$
\begin{equation*}
N_{p}=N_{s p f} \cdot\left(C M F_{1} \cdot C M F_{2} \cdot \ldots \cdot C M F_{x}\right) \cdot C \tag{3.1}
\end{equation*}
$$

where:
$N_{p}$ is the predicted average crash frequency for an individual roadway facility for a specific year,
$N_{s p f}$ is the predicted average crash frequency under base conditions for an individual roadway facility,
$C M F_{1}, C M F_{2}, \ldots, C M F_{x}$ are the HSM crash modification factors for road features $x$, and
$C$ is the calibration factor for roadway facilities of a specific type to account for the discrepancy between the actual safety in a specific jurisdiction or geographical areas and its prediction.

The first step in the methodology involves reconciling the HSM CMFs in IHSDM format with those obtained from local data and past results. In this step, CMFs for local conditions must have the same base conditions $b$ as the HSM CMFs. Let the local CMF for road feature $x$ and containing other confounding variables $y$ (for example, AADT) be given as $C M F_{\text {local }}(x, y, b)$. The corresponding HSM CMF for road feature $x$, confounding variables $z$, and parameters $\beta$ can be represented as $C M F_{H S M}(x, z, \beta, b)$. The $\beta$ parameters of the HSM CMF may be adjusted so as to minimize the overall discrepancy between the factors, where $i=1 \ldots m$ applies to observations in the sample used for fitting the CMFs:
$\min _{\{\beta\}} \sum_{i=1}^{m}\left[C M F_{\text {local }}\left(x_{i}, y_{i}, b\right)-C M F_{H S M}\left(x_{i}, z_{i}, \beta, b\right)\right]^{2}$
The obtained adjusted parameter values, $\hat{\beta}$, may be entered into the IHSDM for the CMF being considered. The same procedure is repeated for each CMF from $j=1 \ldots n$ contained in the IHSDM and for which a corresponding local CMF is available. CMFs that are a part of the IHSDM, but for which local CMFs are not available utilize the HSM CMFs with default $\beta$ parameters. The overall $C M F_{\text {All }}$ including adjusted parameters $\hat{\beta}$ is calculated with Equation 3.3 for each observation in the sample to be used to calibrate the SPF:

$$
\begin{equation*}
C M F_{A l l}=\Pi_{j=1}^{n} C M F_{H S M}\left(x_{j}, z_{j}, \hat{\beta}_{j}, b_{j}\right) \tag{3.3}
\end{equation*}
$$

In the second step, $C M F_{A l l}$ is incorporated as an offset variable in the estimation of the calibrated SPF
for local conditions. The SPF is shown here for roadway segments.

$$
\begin{equation*}
S P F=e^{\alpha_{0}} \cdot A A D T^{\alpha_{1}} \cdot L^{\alpha_{2}} \cdot C M F_{A l l} \cdot e^{\varepsilon} \tag{3.4}
\end{equation*}
$$

where:
$S P F$ is the safety performance function calibrated for local conditions,
$A A D T$ is the annual average daily traffic (veh/day), $L$ is the segment length (mi.),
$\alpha_{0}, \alpha_{1}, \alpha_{2}$ are the parameter estimates based on local data, and
$e^{\varepsilon}$ is the error term that follows gamma distribution with mean equal to 1 and variance equal to the overdispersion.

The format of the SPF is consistent with that of the IHSDM for rural multilane divided segments, and the $\alpha$ parameters may be entered directly into the IHSDM. For rural two-lane undivided segments, the SPF must be rearranged slightly after estimation so that its format is compatible with the IHSDM.

## 4. CALIBRATION DATA

The highway facilities examined in this research include rural two-lane undivided segments, rural multilane divided segments, and urban/suburban arterial segments. The data available for these segments included three years (2013-2015) of crash data, road geometrics, and traffic volumes. Police-reported crashes were retrieved through the Automated Reporting Information Exchange System (ARIES) crash portal. The road geometrics and traffic volumes came from records maintained by the Indiana Department of Transportation (INDOT). The calibration procedure could not be completed for the intersections as the minor approach AADT data is not available in the current data portal.

For rural two-lane undivided segments, the total annual crash frequency had a mean of 1.84 and a standard deviation of 3.08 , with a maximum of 72 crashes. Segment lengths vary from relatively short ( 0.02 mi .) to around a mile ( 0.99 mi.$)$, with an average segment length of 0.65 mi . Only tangent segments were used to model the crash data and CMF calibration. The mean corridor AADT was $3623 \mathrm{veh} / \mathrm{day}$ for two-lane. The Indiana average is lower than the HSM base condition for lane width and shoulder width. Developing jurisdiction-specific SPFs with a very small sample size may yield impractical results and undermine safety effects. Therefore, all the data from Indiana rural two-lane undivided segments has been used to develop the SPF and calibrating CMF parameters for use in the IHSDM. Table 4.1 shows the summary statistics of the crash, geometric, and traffic data for rural twolane undivided segments. The table also presents the HSM base conditions for different geometric variables.

The HSM recommends to update the default proportions for severity levels and collision types based on local data for a particular jurisdiction as part of the calibration process. The related crash percentage is $100.00 \%$ for Indiana, since Indiana roadway segments consist of only the crashes that are defined as related

TABLE 4.1
Summary of Crash Data, Road Geometrics, and Traffic Volumes for Rural Two-Lane Undivided Segments

| Data type | Average | Min | Max | Std. dev. | HSM base condition |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Crashes (3 years) | 1.84 | 0 | 72 | 3.08 | - |
| AADT (veh/day) | 3623 | 60 | 17460 | 2638 | - |
| Segment length (mi.) | 0.65 | 0.02 | 0.99 | 0.21 | 12 |
| Lane width (ft) | 11.30 | 8.5 | 13 | 12 | 6 |
| Shoulder width (ft) | 3.94 | 0 | 13 | 2.56 | 5774 |
| Number of segments |  |  |  |  |  |

TABLE 4.2
Indiana and HSM Crash Severity Distribution on Rural Two-Lane Undivided Segments (All Values in Percent)

| Crash severity level | Indiana | HSM default |
| :--- | ---: | ---: |
| Fatal | 1.06 | 1.3 |
| Incapacitating Injury | 5.09 | 5.4 |
| Nonincapacitating injury | 10.30 | 10.9 |
| Possible injury | 1.34 | 14.5 |
| Total fatal plus injury | 17.79 | 32.1 |
| Property damage only | 82.20 | 67.9 |
| Total | 100 | 100 |

TABLE 4.3
Indiana and HSM Collision Type Distribution for Rural Two-Lane Undivided Segments (All Values in Percent)

| Crash Types | Fatal and injury |  | PDO |  | Total |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Indiana | HSM | Indiana | HSM | Indiana | HSM |
| Single Vehicle |  |  |  |  |  |  |
| Collision with animal | 4.81 | 3.8 | 45.77 | 18.4 | 38.48 | 12.1 |
| Collision with bicycle | 0.48 | 0.4 | 0.02 | 0.1 | 0.10 | 0.2 |
| Collision with pedestrian | 0.90 | 0.7 | 0.05 | 0.1 | 0.20 | 0.3 |
| Overturned | 7.08 | 3.7 | 2.50 | 1.5 | 3.32 | 2.5 |
| Ran off road | 44.48 | 54.5 | 21.16 | 50.5 | 25.31 | 52.1 |
| Other single-vehicle crash | 1.32 | 0.7 | 4.84 | 2.9 | 4.21 | 2.1 |
| Total single-vehicle crashes | 59.06 | 63.8 | 74.34 | 73.5 | 71.62 | 69.3 |
| Multiple Vehicle |  |  |  |  |  |  |
| Angle collision | 6.02 | 10.1 | 2.32 | 7.2 | 2.98 | 8.5 |
| Head-on collision | 8.45 | 3.4 | 0.81 | 0.3 | 2.17 | 1.6 |
| Rear-end collision | 14.47 | 16.5 | 9.08 | 12.2 | 10.04 | 14.2 |
| Sideswipe collision | 7.45 | 3.8 | 5.13 | 3.8 | 5.55 | 3.7 |
| Other multi-vehicle collision | 4.54 | 2.6 | 8.31 | 3.0 | 7.64 | 2.7 |
| Total multiple-vehicle crashes | 40.94 | 36.4 | 25.66 | 26.5 | 28.38 | 30.7 |
| Total crashes | 100 | 100 | 100 | 100 | 100 | 100 |

crashes in the HSM. Table 4.2 and Table 4.3 provide the Indiana percentages for crash severity and collision types for rural two-lane undivided segments. These tables are used to separate the crash frequencies into components by severity level and collision type. The tables also present the HSM's default percentages for severity levels and collision types. Table 4.2 shows that the percentage of possible injury crashes in Indiana is very low compared to the HSM default. The definition of possible injury is subject to the interpretation of the
police officer, and this could be the primary reason for the notable difference. The Indiana crash percentages also can be found in Appendix B.

As shown in Table 4.4, the total annual crash frequency had a mean of 3.21 and a standard deviation of 4.67 , with a maximum of 48 crashes on rural multilane divided segments. The mean corridor AADT was 11,969 veh/day for multilane divided segments. Segment lengths vary from relatively short ( 0.04 mi .) to around a mile ( 0.99 mi .), with an average segment length of 0.64 mi .

TABLE 4.4
Summary of Crash Data, Road Geometrics, and Traffic Volumes for Rural Multilane Divided Segments

| Data type | Average | Min | Max | Std. dev. | HSM base condition |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Crashes (3 years) | 3.21 | 0 | 48 | 4.67 | - |
| AADT (veh/day) | 11969 | 2220 | 29390 | 6275 | - |
| Segment length (mi.) | 0.64 | 0.04 | 0.99 | - | 12 |
| Lane width (ft) | 11.91 | 11 | 13 | 0.30 | 8 |
| Shoulder width (ft) | 9.54 | 0 | 14 | 2.47 | 13.84 |
| Median width (ft) | 48.83 | 3 | 100 | 782 |  |
| Number of segments |  |  |  |  |  |

TABLE 4.5
Indiana and HSM Crashes by Collision Type and Crash Severity Level for Rural Multilane Divided Segments (All Values in Percent)

| Collision type | Total |  | Fatal and injury |  | Fatal and injury* |  | PDO |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Indiana | HSM | Indiana | HSM | Indiana | HSM | Indiana | HSM |
| Head-on | 0.68 | 0.6 | 1.55 | 1.3 | 1.47 | 1.8 | 0.46 | 0.2 |
| Sideswipe | 7.23 | 4.3 | 6.02 | 2.7 | 6.11 | 2.2 | 7.52 | 5.3 |
| Rear-end | 17.84 | 11.6 | 29.13 | 16.3 | 28.42 | 11.4 | 15.14 | 8.8 |
| Angle | 4.76 | 4.3 | 10.68 | 4.8 | 10.53 | 4.5 | 3.34 | 4.1 |
| Single | 64.58 | 76.8 | 49.52 | 72.7 | 50.32 | 77.8 | 68.18 | 79.2 |
| Other | 4.91 | 2.4 | 3.11 | 2.2 | 3.16 | 2.3 | 5.34 | 2.4 |

*Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

TABLE 4.6
Summary of Crash Data, Road Geometrics, and Traffic Volumes for Urban/Suburban Arterial Segments

| Data type | Average | Min | Max | Std. dev. |
| :--- | :---: | :---: | :---: | :---: |
| Hultiple-vehicle non-driveway crashes | 2.45 | 0 | 215 | 11.02 |
| Single-vehicle crashes | 1.53 | 0 | 2.90 | - |
| AADT (veh/day) | 16045 | 790 | - | - |
| Segment length (mi.) | 0.56 | 0.03 | 0.99 | 0.23 |
| Lane width (ft) | 11.51 | 9 | 13 | 1.25 |
| Shoulder width (ft) | 4.83 | 0 | 13 | 3.91 |
| Median width (ft) | 29.76 | 2 | 100 | 20.55 |
| Number of segments |  |  | 820 |  |

The Indiana average is slightly lower than the HSM base condition for lane width but higher for shoulder width and median width. Developing jurisdiction-specific SPFs with a very small sample size may yield impractical results and undermine safety effects. Therefore, all the data from Indiana multilane segments has been used to develop the SPF and calibrating CMF parameters for use in the IHSDM. Table 4.4 shows the summary statistics of the crash, geometric, and traffic data for rural multilane divided segments. The HSM base conditions for different geometric variables are also provided.

The Indiana related crash percentage is $100.00 \%$, the same as for rural two-lane undivided segments. Indiana percentages by collision type and severity on rural multilane divided segments are presented in Table 4.5. Furthermore, the table presents the HSM's default percentages for collision types and severity levels. Appendix B also
contains the Indiana crash percentages for rural multilane divided segments.

Multiple-vehicle non-driveway collisions are more frequent than the single-vehicle crashes on urban/suburban arterial segments. The mean corridor AADT was 16,045 veh/day for urban/suburban arterial segments. Segment lengths vary from relatively short ( 0.03 mi .) to around a mile ( 0.99 mi.$)$, with an average segment length of 0.56 mi . The Indiana average is lower than the HSM base condition for lane width and shoulder width but higher for median width. Table 4.6 shows the summary statistics of the crash, geometric, and traffic data for urban/suburban arterial segments, as well as the HSM's base condition for different geometric variables.

Table 4.7 provides the Indiana percentages for multiple-vehicle non-driveway crashes on urban/suburban arterial segments. This table is used to separate the

TABLE 4.7
Indiana Crash Distributions for Urban/Suburban Arterial Segments (All Values in Percent)

|  |  | Multiple-vehicle non-driveway crashes |  |  |  |  |  |
| :--- | :--- | :--- | :---: | ---: | :---: | :---: | :---: |

crash frequencies into components by severity level and collision type. Appendix B also contains the Indiana crash percentages for urban/suburban arterial segments.

## 5. CALIBRATING THE IHSDM FOR INDIANA

To preserve the IHSDM structure, the calibration process presented in this report involves fitting the HSM CMF's to local data or CMFs and calibrating the SPFs to data with the already fitted CMFs included as offset variables. All these calibrated CMF and SPF parameters and updated crash distributions and proportions must be entered in the IHSDM Administration Tool. Appendix C presents the updated IHSDM Administration Tool with the Indiana configuration. Table 5.1 presents the CMFs that could be calibrated for the various facility types based on the available Indiana data.

Indiana CMFs were obtained from a report by Tarko et al. (2015), and these CMFs were reconciled with the HSM CMFs to better reflect current Indiana conditions in the IHSDM tool. Note that the Indiana CMFs have an exponential form and are based on the difference between the actual lane width or shoulder width and the corresponding HSM base condition. Whereas the HSM CMFs are based on the AADT and other cofounding variables for different geometric features. Table 5.2 shows the Indiana and HSM CMFs for lane width and shoulder width.
where:
$L W$ and $S W$ are the lane width and shoulder width (both in ft ), respectively,
$L W_{b t}, S W_{b t}, L W_{b m}$, and $S W_{b m}$, are the HSM base conditions for lane width on rural two-lane undivided segments ( 12 ft ), shoulder width on rural two-lane undivided segments ( 6 ft ), lane width on rural multilane divided segments ( 12 ft ), and shoulder width on rural multilane divided segments ( 8 ft ), respectively,
$C M F_{R A}$ is the CMF for related crash types (run-offroad, head-on, and sideswipe crashes),
$p_{R A}$ is the proportion of total crashes which are related crashes, and
$a, b, c, d$ are parameters.
It should be noted that $C M F_{R A}$ is presented based on three different AADT levels for lane and shoulder

TABLE 5.1
Available CMFs from Indiana for Various Facility Types

| Facility type | CMF |
| :--- | :--- |
| Rural two-lane undivided segments | Lane width <br> Shoulder width <br> Rural multilane divided segments |
| Lane width <br> Shoulder width |  |

width on rural two-lane undivided segments and for lane width on rural multilane divided segments. These AADT levels are as follows: low if AADT $<400$, moderate if $400 \leq \mathrm{AADT} \leq 2000$, and high if AADT $>2000$. For the low and high AADT categories, the $b$ and $c$ parameters have default values of 0 and the equation includes only parameter $a$. The majority of Indiana's rural two-lane undivided segments and all of the multilane undivided segments fall within the high AADT category. For the moderate AADT category, the $a$ and $b$ parameters may be fitted by minimizing the sum of squared discrepancies in Equation 3.2. Since the Indiana CMFs are not dependent on AADT, the optimization process fitted only the $a$ parameter while setting the $b$ parameter (associated with the AADT in $C M F_{R A}$ ) to zero.

The form of the Indiana CMFs are such that they are compatible with the HSM base condition. Hence, the CMF equation that associates total and related crashes for Indiana may be written as shown in Equation 5.1. In the equation, the proportion of total crashes which are related crashes for Indiana is given as $p_{\text {Ind }} \cdot p_{\text {Ind }}$ is represented as 1 since Indiana roadway segments consist of only the crashes that are defined as related crashes in the HSM.

$$
\begin{equation*}
C M F_{\text {Ind }}=\left(C M F_{R A}-1.0\right) \cdot p_{\text {Ind }}+1.0 \tag{5.1}
\end{equation*}
$$

This equation may be solved for $C M F_{R A}$ and rewritten with the Indiana CMF substituted into the equation:

$$
\begin{equation*}
C M F_{R A}=\frac{e^{\beta_{W}\left(W-W_{b}\right)}-1}{p_{\text {Ind }}}+1 \tag{5.2}
\end{equation*}
$$

where:
$\beta_{W}$ is the Indiana coefficient for lane width or shoulder width,

TABLE 5.2
CMFs from Indiana and the HSM for different facility types

| Variable | Indiana | HSM |
| :---: | :---: | :---: |
| Rural two-lane undivided segments |  |  |
| Lane width | $C M F_{\text {Ind }}=e^{-0.08125\left(L W-L W_{b t}\right)}$ | $\begin{aligned} & C M F_{H S M}=\left(C M F_{R A}-1.0\right) \cdot p_{R A}+1.0, \\ & \text { where } C M F_{R A}=a+\left(b \cdot 10^{c} \cdot(A A D T-d)\right) \end{aligned}$ |
| Shoulder width | $C M F_{\text {Ind }}=e^{-0.0256\left(S W-S W_{b l}\right)}$ | $\begin{aligned} & C M F_{H S M}=\left(C M F_{R A}-1.0\right) \cdot p_{R A}+1.0 \\ & \text { where } C M F_{R A}=a+\left(b \cdot 10^{c} \cdot(A A D T-d)\right) \end{aligned}$ |
| Rural multilane divided segments |  |  |
| Lane width | $C M F=e^{-0.2164\left(L W-L W_{b m}\right)}$ | $\begin{aligned} & C M F=\left(C M F_{R A}-1.0\right) \cdot p_{R A}+1.0, \\ & \text { where } C M F_{R A}=a+\left(b \cdot 10^{c} \cdot(A A D T-d)\right) \end{aligned}$ |
| Shoulder width | $C M F=e^{-0.0412\left(S W-S W_{b m}\right)}$ | $C M F=1.18 \text { for } S W=0 \mathrm{ft}$ $C M F=1.00 \text { for } S W \geq 8 \mathrm{ft}$ |

TABLE 5.3
Calibrated and Default CMF $_{\text {RA }}$ for Lane Width on Rural Two-Lane Undivided Segments

|  |  |  | Default $\boldsymbol{C M F}_{\boldsymbol{R A}}$ |  |
| :--- | :---: | :---: | :---: | :---: |
| Lane width (ft) | Calibrated $\boldsymbol{C M F}_{\boldsymbol{R} \boldsymbol{A}}$ | $<\mathbf{4 0 0}$ AADT | 400 to 2000 AADT | $>$ 2000 AADT |
| 9 | 1.28 | 1.05 | $(1.05-1.50)$ | 1.50 |
| 10 | 1.18 | 1.02 | $(1.02-1.30)$ | 1.30 |
| 11 | 1.08 | 1.01 | $(1.01-1.05)$ | 1.05 |
| 12 | 1.00 | 1.00 | 1.00 | 1.00 |

TABLE 5.4
Calibrated and Default CMF $_{\text {RA }}$ for Shoulder Width on Rural Two-Lane Undivided Segments

|  |  |  | Default $\boldsymbol{C M F} \boldsymbol{R \boldsymbol { A }}$ |  |
| :--- | :---: | :---: | :---: | :---: |
| Shoulder width (ft) | Calibrated $\boldsymbol{C M F}_{\boldsymbol{R} \boldsymbol{A}}$ | $<\mathbf{4 0 0}$ AADT | $\mathbf{4 0 0}$ to 2000 AADT | $>\mathbf{2 0 0 0}$ AADT |
| 0 | 1.17 | 1.10 | $(1.10-1.50)$ | 1.50 |
| 2 | 1.11 | 1.07 | $(1.07-1.30)$ | 1.30 |
| 4 | 1.05 | 1.02 | $(1.02-1.15)$ | 1.15 |
| 6 | 1.00 | 1.00 | 1.00 | 1.00 |
| 8 or more | 0.95 | 0.98 | $(0.98-0.87)$ | 0.87 |

$W$ is the lane width or shoulder width ( ft ), and
$W_{b}$ is the HSM base condition for lane width or shoulder width (ft).

The calibrated and default values of the CMFs for lane width and shoulder width are presented in the sections for rural two-lane undivided segments and rural multilane divided segments. The next sections also presents the calibrated SPFs for different facility types.

### 5.1 Rural Two-Lane Undivided Segments

### 5.1.1 CMF Calibration

The calibrated and default values of $C M F_{R A}$ for lane width are presented in Table 5.3 for rural two-lane undivided segments. The calibrated and default $C M F_{R A}$ for lane width on rural two-lane undivided segments are relatively similar.

Table 5.4 presents the calibrated and default values of $C M F_{R A}$ for shoulder width on rural two-lane undivided segments. The calibrated values of $C M F_{R A}$ for shoulder width are within the range of the default values across all shoulder widths.

### 5.1.2 SPF Calibration

Equation 3.3 may be utilized to calculate the overall $C M F_{\text {All }}$ for rural two-lane undivided segments based on the calibrated CMFs for Indiana conditions. As calculated in Equation 3.4, the SPF's for these road facilities predict crashes using AADT and segment length as exposure and $C M F_{A l l}$ as the offset variable. SPF modeling was done with generalized linear modeling using the SAS GENMOD procedure (SAS Institute Inc., 2009). Table 5.5 presents the SPFs for total crashes on rural two-lane undivided segments. Note that the exposure

TABLE 5.5
Safety Performance Function for on Rural Two-Lane Undivided Segments Total Crashes using CMF All $^{\text {as an }}$ Offset Variable

| Parameter | Estimate | Std. Error | t-statistic |
| :--- | :---: | :---: | :---: |
| Intercept | -6.711 | 0.188 | -35.77 |
| AADT | 0.814 | 0.023 | $<.0001$ |
| Length $L$ (mi.) | 0.886 | 0.046 | $<.0001$ |
| Dispersion | 0.985 | 0.034 | 19.46 |
| Offset Variable |  | 28.63 |  |
| AIC |  | $C M F_{A L L}$ |  |
| Pearson chi-square/DF |  | 19581 |  |

TABLE 5.6
Comparison of the Safety Performance Function Parameters for Rural Two-Lane Undivided Segments-Total Crashes

| Facility type | Calibrated SPF | Default SPF |
| :--- | :--- | :--- |
| Segments | $A A D T^{0.814} \times$ Length $^{0.886} \times 365 \times 10^{-6} \times e^{1.204} \times C M F$ | AAD $T^{1} \times$ Length $^{1} \times 365 \times 10^{-6} \times e^{-0.312}$ |

TABLE 5.7
Predicted Crashes for Rural Two-Lane Undivided Segment using Calibrated and Default Parameters

| State Road 49 | Calibrated Parameters | Default Parameters |
| :--- | :---: | :---: |
| Total crashes (3 years) | 3.18 | 3.37 |
| Fatal and injury (FI) crashes | 0.57 | 1.08 |
| Property damage only (PDO) crashes | 2.61 | 2.29 |

TABLE 5.8
Calibrated and Default $\mathbf{C M F}_{\text {RA }}$ for Lane Width on Rural Multilane Divided Segments

|  |  |  | Default $\boldsymbol{C M F} \boldsymbol{F} \boldsymbol{R A}$ |  |
| :--- | :---: | :---: | :---: | :---: |
| Lane width (ft) | Calibrated $\boldsymbol{C M F}_{\boldsymbol{R} \boldsymbol{A}}$ | $<\mathbf{4 0 0}$ AADT | $\mathbf{4 0 0}$ to 2000 AADT | $>\mathbf{2 0 0 0}$ AADT |
| 9 | 1.91 | 1.03 | $(1.03-1.25)$ | 1.25 |
| 10 | 1.54 | 1.01 | $(1.01-1.15)$ | 1.15 |
| 11 | 1.24 | 1.01 | $(1.01-1.03)$ | 1.03 |
| 12 | 1.00 | 1.00 | 1.00 |  |

variables are statistically significant for this facility type.

The model structure of the safety performance function for the rural two-lane undivided segments must be rearranged (as shown in Table 5.6) slightly so that it is consistent with the format of the IHSDM and can be implemented in the tool.

### 5.1.3 Example Case

A segment of State Road 49 in Northwest Indiana was examined. This 2000 -foot segment had an AADT of 10,350 , lane width of 11 feet, and shoulder width of 5 feet. Table 5.7 provides a comparison of the crash prediction results using the calibrated and default parameters.

For the selected roadway segment, the predicted number of total crashes was slightly lower when using
the calibrated parameters versus the default parameters. When splitting the crashes by severity, however, it can be seen that using the default parameters led to an overstated number of FI crashes and an understated number of PDO crashes.

### 5.2 Rural Multilane Divided Segments

### 5.2.1 CMF Calibration

Table 5.8 presents the calibrated and default $C M F_{R A}$ for lane width on rural multilane divided segments. It is interesting to note that the calibrated and default $C M F_{R A}$ for lane width on rural multilane divided segments are considerably different. This result shows the importance of calibrating the default values to regionspecific values. Although the calibrated CMF values are not sensitive to the AADT due to the lack of Indiana data
to preserve this differentiation, the considerable difference between the calibrated and default results prompts for applying simple but correct models instead of more elaborated models that are not supported by local data. The presented example illustrates a practical strategy of simplifying a model if necessary due to the lack of data while following the IHSDM overall structure and making the results still implementable via the IHSDM.

TABLE 5.9
Calibrated and Default CMF for Shoulder Width on Rural Multilane Divided Segments

| Shoulder width (ft) | Calibrated $\boldsymbol{C M F}$ | Default $\boldsymbol{C M F}$ |
| :--- | :---: | :---: |
| 0 | 1.39 | 1.18 |
| 2 | 1.28 | 1.13 |
| 4 | 1.17 | 1.09 |
| 6 | 1.08 | 1.04 |
| 8 or more | 1.00 | 1.00 |

Table 5.9 presents the calibrated and default $C M F$ for shoulder width on rural multilane divided segments. The calibrated CMF values for shoulder width are higher than the default values. In this case, the CMF values may be directly replaced with the Indiana CMF values in the IHSDM since the base conditions are consistent.

### 5.2.2 SPF Calibration

Table 5.10 presents the safety performance model results for total crashes on rural multilane divided segments. For rural multilane divided segments, this model structure assumes the SPF format of the IHSDM, and the estimated parameters may be entered directly into the software.

Table 5.11 summarizes the results for KABC and KAB crash severities on rural multilane divided segments. Note that the exposure variables are also statistically significant for different severity types.

Table 5.12 summarizes the calibrated and default SPFs for total, KABC and KAB crashes rural multilane

TABLE 5.10
Safety Performance Function for Rural Multilane Divided Segments-Total Crashes using CMF all as an Offset Variable

| Parameter | Estimate | Std E | t-statistic |
| :--- | :---: | :---: | :---: |
| Intercept | -10.074 | 0.749 | -13.43 |
| AADT | 1.139 | 0.080 | 14.11 |
| Length $L$ (mi.) | 0.749 | 0.110 | 6.81 |
| Dispersion | 1.083 | 0.086 | 12.58 |
| Offset Variable |  |  | $C M F_{A L L}$ |
| AIC |  | 3359 | $<.0001$ |
| Pearson chi-square/DF |  | 1.05 |  |

TABLE 5.11
Safety Performance Functions for Rural Multilane Divided Segments-KABC and KAB Crashes using CMF ALL $^{\text {as }}$ an Offset Variable

| Parameter | Rural Multilane Divided KABC |  |  |  | Rural Multilane Divided KAB |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Estimate | Std E | t-statistic | p-value | Estimate | Std E | t-statistic | p-value |
| Intercept | -12.736 | 1.096 | -11.62 | <. 0001 | -12.717 | 1.106 | -11.49 | $<.0001$ |
| AADT | 1.238 | 0.116 | 10.68 | <. 0001 | 1.230 | 0.117 | 10.52 | <. 0001 |
| Length $L$ (mi.) | 0.608 | 0.169 | 3.60 | <. 0003 | 0.669 | 0.172 | 3.88 | 0.0001 |
| Dispersion | 0.806 | 0.148 | 5.43 |  | 0.708 | 0.144 | 4.49 |  |
| Offset Variable | $C M F_{A L L}$ |  |  |  | $C M F_{A L L}$ |  |  |  |
| AIC | 1527 |  |  |  | 1454 |  |  |  |
| Pearson chi-square/DF | 1.05 |  |  |  | 1.04 |  |  |  |

TABLE 5.12
Comparison of the SPF Parameters for Rural Multilane Divided Segments-Total Crashes

| Severity level | Calibrated SPFs | Default SPFs |
| :--- | :---: | :---: |
| Total crashes | $\exp (-10.074+1.139 \times \ln (A A D T)$ | $\exp (-9.025+1.049 \times \ln (A A D T)$ |
|  | $+0.749 \times \ln ($ Length $)) \times \mathrm{CMF}$ | $+\ln (\operatorname{Length}))$ |
| KABC crashes | $\exp (-12.736+1.238 \times \ln (A A D T)$ | $\exp (-8.837+0.958 \times \ln (A A D T)$ |
|  | $+0.608 \times \ln ($ Length $)) \times \mathrm{CMF}$ | $+\ln (\operatorname{Length}))$ |
| KAB crashes | $\exp (-12.717+1.230 \times \ln (A A D T)$ | $\exp (-8.505+0.874 \times \ln (A A D T)$ |
|  | $+0.669 \times \ln ($ Length $)) \times \mathrm{CMF}$ | $+\ln (\operatorname{Length}))$ |

divided segments. The parameter estimates for different severity levels reveal that there is a significant difference between the calibrated and default SPFs.

### 5.2.3 Example Case

A segment of US Highway 30 in Northeast Indiana was examined. This 3060 -foot segment had an AADT of 17,220 , lane width of 11 feet, shoulder width of 7 feet, and median width of 40 feet. The crash prediction results obtained by utilizing the calibrated and default parameters are shown in Table 5.13.

The predicted number of total crashes was greater when using the calibrated parameters versus the default parameters. Similarly as for the rural two-lane undivided segment, it can be seen that using the default parameters overstated the number of FI crashes while understating the number of PDO crashes.

### 5.3 Urban/Suburban Arterial Segments

The SPF's for urban/suburban arterial segments predict crashes using AADT and segment length as exposure and $C M F_{\text {All }}$ as the offset variable. Due to the unavailability of the minor road AADT data, the SPF calibration could not be conducted for urban/suburban intersections. Also, the HSM-specified CMF variables

TABLE 5.13
Predicted Crashes for Rural Multilane Divided Segments using Calibrated and Default Parameters

| US Highway 30 | Calibrated <br> parameters | Default <br> parameters |
| :--- | :---: | :---: |
| Total crashes (3 years) | 7.17 | 5.96 |
| Fatal and injury (FI) crashes | 1.41 | 2.96 |
| Property damage only (PDO) crashes | 5.76 | 3.00 |

were not available in the Indiana data, therefore all CMFs were assumed to have default values as the base condition. Urban/suburban arterial segment SPFs are developed based on five different geometry cases, three levels of severity and collision types. The next section presents all the calibrated SPFs within the data constraints.

### 5.3.1 SPF Calibration

Table 5.14 presents the safety performance model results for multiple-vehicle non-driveway total crashes, PDO and FI crashes on two-lane undivided roads. Safety performance model results for multiple-vehicle nondriveway total crashes, PDO and FI crashes on four-lane undivided roads are shown in Table 5.15. Finally, safety performance model results are depicted in Table 5.16 for Multiple-vehicle non-driveway total crashes, PDO and FI crashes on four-lane divided roads.

Table 5.17 presents the safety performance model results for single-vehicle non-driveway total crashes, PDO and FI crashes on two-lane undivided roads. Finally, Table 5.18 presents the safety performance model results for single-vehicle non-driveway total crashes, PDO crashes, and FI crashes on four-lane divided roads.

Table 5.19 summarizes the calibrated and default SPFs for total, KABC, and KAB multiple-vehicle nondriveway crashes on different types of urban/suburban arterial segments. The parameter estimates for different severity levels reveal that there is a significant difference between the calibrated and default SPFs for Indiana.

Calibrated and default SPFs for total, KABC, and KAB single-vehicle crashes on different types of urban/ suburban arterial segments are presented side by side in Table 5.20 for comparison. The parameter estimates for different severity levels and facility configurations show that there is a significant difference between the calibrated and default SPFs for Indiana.

TABLE 5.14
Safety Performance Functions for Multiple-Vehicle Non-Driveway Crashes on Urban/Suburban Two-Lane Undivided Segments

| Parameter |  | Estimate | Std E | t-statistic | p-value |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Total Crashes | Intercept | -13.357 | 1.384 | -9.65 | <. 0001 |
|  | AADT | 1.452 | 0.151 | 9.62 | <. 0001 |
|  | Length $L$ (mi.) | 0.307 | 0.096 | 3.21 | 0.0013 |
|  | Dispersion | 1.813 | 0.209 | 8.68 |  |
| PDO Crashes | Intercept | -14.117 | 1.546 | -9.13 | <. 0001 |
|  | AADT | 1.502 | 0.168 | 8.93 | <. 0001 |
|  | Length $L$ (mi.) | 0.287 | 0.104 | 2.77 | 0.0055 |
|  | Dispersion | 2.110 | 0.265 | 7.95 |  |
| FI Crashes | Intercept | -13.864 | 1.989 | -6.97 | <. 0001 |
|  | AADT | 1.366 | 0.216 | 6.33 | <. 0001 |
|  | Length $L$ (mi.) | 0.437 | 0.153 | 2.86 | 0.0042 |
|  | Dispersion | 2.240 | 0.465 | 4.82 |  |

Number of Observations

TABLE 5.15
Safety Performance Functions for Multiple-Vehicle Non-Driveway Crashes on Urban/Suburban Four-Lane Undivided Segments

| Parameter |  | Estimate | Std E | t-statistic | p-value |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Total Crashes | Intercept | -16.691 | 4.598 | -3.63 | 0.0003 |
|  | AADT | 1.811 | 0.475 | 3.82 | 0.0001 |
|  | Length L (mi.) | 0.658 | 0.221 | 2.98 | 0.0029 |
|  | Dispersion | 1.901 | 0.462 | 4.12 |  |
| PDO Crashes | Intercept | -19.510 | 5.230 | -3.73 | 0.0002 |
|  | AADT | 2.087 | 0.543 | 3.84 | 0.0001 |
|  | Length L (mi.) | 0.747 | 0.251 | 2.98 | 0.0029 |
|  | Dispersion | 2.013 | 0.518 | 3.89 |  |
| FI Crashes | Intercept | -14.163 | 4.839 | -2.93 | 0.0034 |
|  | AADT | 1.401 | 0.497 | 2.82 | 0.0048 |
|  | Length L (mi.) | 0.689 | 0.241 | 2.86 | 0.0043 |
|  | Dispersion | 1.343 | 0.613 | 2.19 |  |
| Number of Observations |  | 77 |  |  |  |

TABLE 5.16
Safety Performance Functions for Multiple-Vehicle Non-Driveway Crashes on Urban/Suburban Four-Lane Divided Segments

| Parameter |  | Estimate | Std E | t-statistic |
| :--- | :--- | :---: | :--- | :---: |
| Total Crashes | Intercept | -9.896 | 1.393 | -3.63 |
|  | AADT | 1.093 | 0.140 | 3.82 |
|  | Length $L$ (mi.) | 0.664 | 0.107 | 2.98 |
|  | Dispersion | 2.145 | 0.200 | 4.12 |
| PDO Crashes | Intercept | -10.105 | 1.441 | -9.13 |
|  | AADT | 1.092 | 0.144 | 8.93 |
| FI Crashes | Length $L$ (mi.) | 0.677 | 0.113 | 2.77 |
|  | Dispersion | 2.337 | 0.230 | 7.95 |
|  | Intercept | -11.124 | 1.900 | -6.97 |
|  | 1.054 | 0.189 | 6.33 | $<.0001$ |
|  | AADT | 0.594 | 0.318 | 4.86 |

TABLE 5.17
Safety Performance Functions for Single-Vehicle Non-Driveway Crashes on Urban/Suburban Two-Lane Undivided Segments

| Parameter |  | Estimate | Std E | t-statistic |
| :--- | :--- | :--- | :--- | :--- |
| Total Crashes | Intercept | -2.624 | 1.066 | -2.46 |
|  | AADT | 0.300 | 0.117 | 2.56 |
|  | Length $L$ (mi.) | 0.980 | 0.117 | 8.37 |
|  | Dispersion | 1.156 | 0.171 | 6.74 |
| PDO Crashes | Intercept | -2.051 | 1.152 | -1.78 |
|  | AADT | 0.217 | 0.127 | 1.71 |
| FI Crashes | Length $L$ (mi.) | 0.979 | 0.125 | 7.86 |
|  | Dispersion | 1.214 | 0.192 | 6.33 |
|  | Intercept | -9.934 | 1.856 | -5.35 |
|  | 0.896 | 0.200 | 4.49 |  |
|  | AADT | 0.994 | 0.216 | 4.61 |

TABLE 5.18
Safety Performance Functions for Single-Vehicle Non-Driveway Crashes on Urban/Suburban Four-Lane Divided Segments

| Parameter |  | Estimate | Std E | t-statistic | p-value |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Total Crashes | Intercept | -7.583 | 1.164 | -6.52 | <. 0001 |
|  | AADT | 0.824 | 0.116 | 7.11 | <. 0001 |
|  | Length $L$ (mi.) | 1.184 | 0.105 | 11.30 | <. 0001 |
|  | Dispersion | 1.051 | 0.136 | 7.71 |  |
| PDO Crashes | Intercept | -7.217 | 1.231 | -5.86 | <. 0001 |
|  | AADT | 0.776 | 0.123 | 6.33 | <. 0001 |
|  | Length $L$ (mi.) | 1.272 | 0.116 | 11.01 | <. 0001 |
|  | Dispersion | 1.132 | 0.153 | 7.41 |  |
| FI Crashes | Intercept | -12.905 | 1.758 | -7.34 | <. 0001 |
|  | AADT | 1.143 | 0.171 | 6.70 | <. 0001 |
|  | Length $L$ (mi.) | 0.862 | 0.155 | 5.58 | <. 0001 |
|  | Dispersion | 0.244 | 0.180 | 1.36 |  |
| Number of Observations |  | 366 |  |  |  |

TABLE 5.19
Safety Performance Functions for Multiple-Vehicle Non-Driveway Crashes on Urban/Suburban Arterial Segments

| Facility type |  | Calibrated SPFs | Default SPFs |
| :---: | :---: | :---: | :---: |
| Two-lane undivided arterials (2U) | Total | $\begin{gathered} \exp (-13.357+1.452 \times \ln (A A D T) \\ \quad+0.307 \times \ln (\text { Length })) * \mathrm{CMF} \end{gathered}$ | $\begin{aligned} & \exp (-15.22+1.68 \times \ln (A A D T) \\ & \quad+\ln (\text { Length })) \end{aligned}$ |
|  | KABC | $\exp (-14.117+1.502 \times \ln (A A D T)$ | $\exp (-16.22+1.66 \times \ln (A A D T)$ |
|  |  | $+0.287 \times \ln ($ Length $)$ ) $*$ CMF | $+\ln ($ Length $)$ ) |
|  | PDO | $\begin{gathered} \exp (-13.864+1.366 \times \ln (A A D T) \\ +0.437 \times \ln (\text { Length })) * \mathrm{CMF} \end{gathered}$ | $\begin{aligned} & \exp (-15.62+1.37 \times \ln (A A D T) \\ & \quad+\ln (\text { Length })) \end{aligned}$ |
| Four-lane undivided arterials (4U) | Total | $\exp (-16.691+1.811 \times \ln (A A D T)$ | $\exp (-11.63+1.33 \times \ln (A A D T)$ |
|  |  | $+0.658 \times \ln ($ Length $)$ ) $*$ CMF | $+\ln ($ Length $)$ ) |
|  | KABC | $\exp (-19.510+2.087 \times \ln (A A D T)$ | $\exp (-12.08+1.25 \times \ln (A A D T)$ |
|  |  | $+0.747 \times \ln ($ Length $)) *$ CMF | $+\ln ($ Length $)$ ) |
|  | PDO | $\exp (-14.163+1.401 \times \ln (A A D T)$ | $\exp (-12.53+1.38 \times \ln (A A D T)$ |
|  |  | $+0.689 \times \ln ($ Length $)$ ) $* \mathrm{CMF}$ | $+\ln ($ Length $)$ ) |
| Four-lane divided arterials (4D) | Total | $\exp (-9.896+1.093 \times \ln (A A D T)$ | $\exp (-12.34+1.36 \times \ln (A A D T)$ |
|  |  | $+0.664 \times \ln ($ Length $)$ ) $* \mathrm{CMF}$ | $+\ln ($ Length $)$ ) |
|  | KABC | $\exp (-10.105+1.092 \times \ln (A A D T)$ | $\exp (-12.76+1.28 \times \ln (A A D T)$ |
|  |  | $+0.677 \times \ln ($ Length $)$ ) $*$ CMF | $+\ln ($ Length $)$ ) |
|  | PDO | $\exp (-11.124+1.054 \times \ln (A A D T)$ | $\exp (-12.81+1.38 \times \ln (A A D T)$ |
|  |  | $+0.594 \times \ln (\text { Length })) * \mathrm{CMF}$ | $+\ln (\text { Length }))$ |

TABLE 5.20
Safety Performance Functions for Single-Vehicle Crashes on Urban/Suburban Arterial Segments

| Facility type |  | Calibrated SPFs | Default SPFs |
| :---: | :---: | :---: | :---: |
| Two-lane undivided arterials (2U) | Total | $\begin{aligned} & \exp (-2.624+0.300 \times \ln (A A D T) \\ & \quad+0.980 \times \ln (\text { Length })) * \mathrm{CMF} \end{aligned}$ | $\begin{aligned} & \exp (-5.47+0.56 \times \ln (A A D T) \\ & \quad+\ln (\text { Length })) \end{aligned}$ |
|  | KABC | $\exp (-2.051+0.217 \times \ln (A A D T)$ | $\exp (-3.96+0.23 \times \ln (A A D T)$ |
|  |  | $+0.979 \times \ln ($ Length $)$ ) $*$ CMF | $+\ln ($ Length $)$ ) |
|  | PDO | $\exp (-9.934+0.896 \times \ln (A A D T)$ | $\exp (-6.51+0.64 \times \ln (A A D T)$ |
|  |  | $+0.994 \times \ln ($ Length $)) * \mathrm{CMF}$ | $+\ln ($ Length $)$ ) |
| Four-lane divided arterials (4D) | Total | $\exp (-7.583+0.824 \times \ln (A A D T)$ | $\exp (-5.05+0.47 \times \ln (A A D T)$ |
|  |  | $+1.184 \times \ln ($ Length $)$ ) $*$ CMF | $+\ln ($ Length $)$ ) |
|  | KABC | $\exp (-7.217+0.776 \times \ln (A A D T)$ | $\exp (-8.71+0.66 \times \ln (A A D T)$ |
|  |  | $+1.272 \times \ln (\text { Length })) * \mathrm{CMF}$ | $+\ln (\text { Length }))$ |
|  | PDO | $\exp (-12.905+1.143 \times \ln (A A D T)$ | $\exp (-5.04+0.45 \times \ln (A A D T)$ |
|  |  | $+0.862 \times \ln ($ Length $)$ ) $*$ CMF | $+\ln (\text { Length }))$ |

## 6. SUMMARY AND CONCLUSIONS

Safety of Indiana road facilities may be enhanced through the consideration of safety countermeasures in the transportation planning, design, management, and operations stages. Implementation of the safety knowledge may be facilitated through the IHSDM, a tool which may be utilized to assess the safety impact of project-level design decisions by implementing the HSM crash prediction methodology. SPFs, CMFs, calibration factors, and crash proportions are utilized in predicting the number, severity, and type of crashes occurring on various types of roadway facilities. The crash prediction method must be calibrated in order to accurately assess the impact of design decisions for Indiana conditions.

In this report, a comprehensive approach to calibrating the HSM predictive method within the constraints of the IHSDM is presented. First, the parameters of the tool's default CMFs are calibrated so that they are consistent with the CMFs from past research and local data. Second, the method jointly estimates the SPFs and CMFs, thus preserving crash prediction consistency. Proper calibration of the CMFs and SPFs eliminates the necessity of calibration factors. The developed methodology allows users to utilize the IHSDM to determine the safety impacts of road designs while incorporating local data and past results in forms which may differ from the IHSDM.

This study also updated and expanded the database of CRFs applicable to Indiana conditions for various geometric, traffic, pavement, and other characteristics of Indiana road facilities. CRFs/CMFs for various types and severities of crashes were identified for around 80 safety countermeasures applied on urban and rural segments, intersections, and interchanges. Most of these CRFs/CMFs were available as values, and those provided as functions were discretized for various levels of the change in safety. This comprehensive CRFs/CMFs database is helpful to get the quick notion about the benefit of a selected countermeasure outside IHSDM analysis.

For the comprehensive analysis of a selected countermeasure or design changes in the IHSDM, the results of the developed methodology are implemented in the tool to reflect local Indiana conditions. Calibrated SPF and CMF parameters, as well as crash proportions were included in IHSDM for rural two-lane undivided segments, rural multilane divided segments, and urban/ suburban arterial segments. The application of these calibrated parameters was demonstrated for Indiana rural two-lane undivided segments and rural multilane divided segments.

The calibrated $C M F_{R A}$ values for lane width on rural two-lane undivided segments are relatively similar to the default $C M F_{R A}$. On the other hand, the calibrated $C M F_{R A}$ values are considerably higher than the defaults for rural multilane divided segments. The calibrated $C M F_{R A}$ for shoulder width on rural two-lane undivided segments are within the range of defaults for all shoulder widths. On the other hand, the calibrated $C M F$ for
shoulder width on rural multilane divided segments are higher than the defaults. The total $C M F_{A l l}$ is determined based on the individual CMFs and is included as an offset variable in the SPF to predict crashes, along with the AADT and segment length as exposure.

Finally, example studies were performed to compare the predictive performance of the IHSDM using the calibrated and default Indiana parameters for both facility types. Although the predicted total crashes was marginally lower when using the calibrated versus default parameters on the rural two-lane undivided segment, using the default parameters overstated the FI crashes while understating the PDO crashes. For the rural multilane divided segment, the predicted number of total crashes was greater with the calibrated Indiana parameters as compared to the default parameters. Again, the calculations with the default parameters overstated the FI crashes while understating the PDO crashes, this time to a greater extent than for rural two-lane undivided segments. This comparison indicated that, at least in Indiana, the calibration resulted in considerably different crash estimates than based on the default parameters for the studied segments.

The findings from this report highlight the need for calibrating the parameters in the IHSDM to local conditions. In order to preserve the integrity of the presented method, SPFs should be calibrated every 2 to 3 years to accommodate changes in the traffic and/or changes in road conditions. Furthermore, CMFs should be updated as new studies are conducted for Indiana or other nearby states. Such an effort may be conducted as a part of a research project conducted under the assistance of Purdue University and/or INDOT's Research and Development Division.

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APPENDIX A. CRASH REDUCTION FACTORS AND CRASH MODIFICATION FACTORS SUITABLE FOR INDIANA
This appendix presents the CRFs/CMFs for safety countermeasures that were identified as being the most suitable for Indiana based on the criteria presented in Chapter 2. Table A.1 contains 82 safety countermeasures spanning 16 different categories. For each countermeasure, the applicable area type urban and/or rura), facility type, and CRF/CMF values for various crash types and severities are presented. Finally, the state(s) where each study was conducted and the corresponding reference are provided in the table.
TABLE A. 1
CRFs and CMFs Most Suitable for Indiana

|  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Category | Countermeasure | Area type | Facility type | Crash type | CRF |
| (reference number) |  |  |  |  |  |

TABLE A. 1

| Category | Countermeasure | Area type | Facility type | Crash type | CRF | CMF | States and (reference number) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Access management | Reduce driveway density by 10 driveways per mile* | Urban | Principal arterials, minor arterials, or collectors with raised medians | Total | 9.2 | 0.908 | NV (24) |
|  |  |  |  | PDO | 6.9 | 0.931 |  |
|  |  |  |  | KABC | 5.7 | 0.943 |  |
|  |  |  |  | Rear-end | 3.0 | 0.970 |  |
|  |  |  |  | Angle | 8.3 | 0.917 |  |
|  |  |  | Principal arterials, minor arterials, or collectors with TWLTLs | Total | 8.6 | 0.914 |  |
|  |  |  |  | PDO | 9.0 | 0.910 |  |
|  |  |  |  | KABC | 2.6 | 0.974 |  |
|  |  |  |  | Rear-end | 7.4 | 0.926 |  |
|  |  |  |  | Angle | 8.1 | 0.919 |  |
| Access management | Reduce driveway density by 15 driveways per mile* | Urban | Principal arterials, minor arterials, or collectors with raised medians | Total | 13.4 | 0.866 | NV (24) |
|  |  |  |  | PDO | 10.1 | 0.899 |  |
|  |  |  |  | KABC | 8.5 | 0.915 |  |
|  |  |  |  | Rear-end | 4.4 | 0.956 |  |
|  |  |  |  | Angle | 12.2 | 0.878 |  |
|  |  |  | Principal arterials, minor arterials, or collectors with TWLTLs | Total | 12.6 | 0.874 |  |
|  |  |  |  | PDO | 13.2 | 0.868 |  |
|  |  |  |  | KABC | 3.8 | 0.962 |  |
|  |  |  |  | Rear-end | 10.9 | 0.891 |  |
|  |  |  |  | Angle | 11.8 | 0.882 |  |
| Access management | Reduce driveway density by 20 driveways per mile* | Urban | Principal arterials, minor arterials, or collectors with raised medians | Total | 17.5 | 0.825 | NV (24) |
|  |  |  |  | PDO | 13.2 | 0.868 |  |
|  |  |  |  | KABC | 11.1 | 0.889 |  |
|  |  |  |  | Rear-end | 5.8 | 0.942 |  |
|  |  |  |  | Angle | 16.0 | 0.840 |  |
|  |  |  | Principal arterials, minor arterials, or collectors with TWLTLs | Total | 16.5 | 0.835 |  |
|  |  |  |  | PDO | 17.1 | 0.829 |  |
|  |  |  |  | KABC | 5.1 | 0.949 |  |
|  |  |  |  | Rear-end | 14.3 | 0.857 |  |
|  |  |  |  | Angle | 15.5 | 0.845 |  |
| Alignment | Flatten crest of curve | Rural | Arterials, collectors | Total | 19.6 | 0.804 | OH (19) |
|  |  |  |  | KABC | 51.2 | 0.488 |  |
| Alignment | Reduce the average grade rate by $1 \%$ * | Rural | Two-lane roads | PDO | 2.0 | 0.980 | IN (42) |
|  |  |  |  | KABC | 1.9 | 0.981 |  |
| Alignment | Reduce the average grade rate by $2 \%$ * | Rural | Two-lane roads | PDO | 4.0 | 0.960 | IN (42) |
|  |  |  |  | KABC | 3.8 | 0.962 |  |
| Alignment | Reduce the average grade rate by $3 \%$ * | Rural | Two-lane roads | PDO | 6.0 | 0.940 | IN (42) |
|  |  |  |  | KABC | 5.7 | 0.943 |  |
| Alignment | Reduce the average grade rate by 4\%* | Rural | Two-lane roads | PDO | 7.9 | 0.921 | IN (42) |
|  |  |  |  | KABC | 7.5 | 0.925 |  |

TABLE A. 1
(Continued)

| Category | Countermeasure | Area type | Facility type | Crash type | CRF | CMF | States and (reference number) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Alignment | Reduce the average grade rate by 5\%* | Rural | Two-lane roads | PDO <br> KABC | $\begin{aligned} & 9.7 \\ & 9.3 \end{aligned}$ | $\begin{aligned} & 0.903 \\ & 0.907 \end{aligned}$ | IN (42) |
| Alignment | Reduce the average degree of curve by 1 degree* | Rural | Two-lane roads | $\begin{aligned} & \text { PDO } \\ & \text { KABC } \end{aligned}$ | $\begin{aligned} & 1.9 \\ & 2.9 \end{aligned}$ | $\begin{aligned} & 0.981 \\ & 0.971 \end{aligned}$ | IN (42) |
| Alignment | Reduce the average degree of curve by 2 degrees* | Rural | Two-lane roads | PDO <br> KABC | $\begin{aligned} & 3.8 \\ & 5.7 \end{aligned}$ | $\begin{aligned} & 0.962 \\ & 0.943 \end{aligned}$ | IN (42) |
| Alignment | Reduce the average degree of curve by 3 degrees* | Rural | Two-lane roads | PDO <br> KABC | $\begin{aligned} & 5.7 \\ & 8.4 \end{aligned}$ | $\begin{aligned} & 0.943 \\ & 0.916 \end{aligned}$ | IN (42) |
| Alignment | Reduce the average degree of curve by 4 degrees* | Rural | Two-lane roads | $\begin{aligned} & \text { PDO } \\ & \text { KABC } \end{aligned}$ | $\begin{array}{r} 7.5 \\ 11.1 \end{array}$ | $\begin{aligned} & 0.925 \\ & 0.889 \end{aligned}$ | IN (42) |
| Alignment | Reduce the average degree of curve by 5 degrees* | Rural | Two-lane roads | PDO <br> KABC | $\begin{array}{r} 9.3 \\ 13.6 \end{array}$ | $\begin{aligned} & 0.907 \\ & 0.864 \end{aligned}$ | IN (42) |
| Highway lighting | Install lighting on a roadway segment | Urban and rural | Not specified | Nighttime Nighttime KABC | $\begin{aligned} & 20.0 \\ & 29.0 \end{aligned}$ | $\begin{aligned} & 0.800 \\ & 0.710 \end{aligned}$ | Not specified (17) |
| Highway lighting | Install lighting at a signalized intersection | Urban <br> Rural | Not specified Not specified | Daytime <br> Nighttime <br> Daytime <br> Nighttime | $\begin{array}{r} -3.0 \\ 3.0 \\ 2.0 \\ 2.0 \end{array}$ | $\begin{aligned} & 1.030 \\ & 0.970 \\ & 0.980 \\ & 0.980 \end{aligned}$ | MN (6) |
| Highway lighting | Install lighting at a stop-controlled intersection | Urban <br> Rural | Not specified Not specified | Daytime <br> Nighttime <br> Daytime <br> Nighttime | $\begin{array}{r} -5.0 \\ 9.0 \\ -9.0 \\ -7.0 \end{array}$ | $\begin{aligned} & 1.050 \\ & 0.910 \\ & 1.090 \\ & 1.070 \end{aligned}$ | MN (6) |
| Highway lighting | Install lighting at an interchange | Urban and rural | Arterials, collectors | Total KABC | $\begin{aligned} & 50.4 \\ & 26.0 \end{aligned}$ | $\begin{aligned} & 0.496 \\ & 0.740 \end{aligned}$ | OH (19) |
| Intersection geometry | Add a left-turn lane on one major approach to a signalized intersection | Urban <br> Rural | Three-leg intersections Four-leg intersections Three-leg intersections Four-leg intersections | Total <br> Total <br> Total <br> Total | $\begin{array}{r} 7.0 \\ 10.0 \\ 15.0 \\ 18.0 \end{array}$ | $\begin{aligned} & 0.930 \\ & 0.900 \\ & 0.850 \\ & 0.820 \end{aligned}$ | $\begin{aligned} & \text { IA, IL, LA, MN, } \\ & \text { NE, NC, OR, } \\ & \text { VA (18) } \end{aligned}$ |
| Intersection geometry | Add a left-turn lane on one major approach to an unsignalized intersection | Urban <br> Rural | Three-leg intersections Four-leg intersections Three-leg intersections Four-leg intersections | Total <br> Total <br> Total <br> Total | $\begin{aligned} & 33.0 \\ & 27.0 \\ & 44.0 \\ & 28.0 \end{aligned}$ | $\begin{aligned} & 0.670 \\ & 0.730 \\ & 0.560 \\ & 0.720 \end{aligned}$ | $\begin{aligned} & \text { IA, IL, LA, MN, } \\ & \text { NE, NC, OR, } \\ & \text { VA (18) } \end{aligned}$ |
| Intersection geometry | Add a right-turn lane on one major approach to a signalized intersection | Urban | Four-leg intersections | Total | 4.0 | 0.960 | $\begin{aligned} & \text { IA, IL, LA, MN, } \\ & \text { NE, NC, OR, } \\ & \text { VA (18) } \end{aligned}$ |

TABLE A. 1

| Category | Countermeasure | Area type | Facility type | Crash type | CRF | CMF | States and (reference number) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection geometry | Add a right-turn lane on one major approach to an unsignalized intersection | Rural | Four-leg intersections | Total | 14.0 | 0.860 | IA, IL, LA, MN, NE, NC, OR, VA (18) |
| Intersection geometry | Convert diamond interchange to diverging diamond interchange (DDI) | Urban | Principal arterial, other freeways and expressways | Total <br> Injury <br> Angle <br> Rear-end <br> Sideswipe <br> Single-vehicle | $\begin{array}{r} 33 \\ 41 \\ 67 \\ 36 \\ -27 \\ 24 \end{array}$ | $\begin{aligned} & 0.67 \\ & 0.59 \\ & 0.33 \\ & 0.64 \\ & 1.27 \\ & 0.76 \end{aligned}$ | $\begin{aligned} & \text { KY, MO, NY, } \\ & \text { TN (20) } \end{aligned}$ |
| Intersection geometry | Convert intersection on low-speed road to a roundabout | Urban and rural | Intersections where all approaches are low-speed (less than 45 mph ) | Total KABC | $\begin{array}{r} -9.9 \\ 52.7 \end{array}$ | $\begin{aligned} & 1.099 \\ & 0.473 \end{aligned}$ | WI (31) |
| Intersection geometry | Convert intersection on high-speed road to a roundabout | Urban and rural | Intersections where at least one approach is high-speed ( 45 mph or greater) | Total KABC | $\begin{aligned} & 34.1 \\ & 49.4 \end{aligned}$ | $\begin{aligned} & 0.659 \\ & 0.506 \end{aligned}$ | WI (31) |
| Intersection geometry | Convert intersection to a single-lane roundabout | Urban and rural | Intersections with low- and high-speed approaches | Total KABC | $\begin{aligned} & 36.0 \\ & 18.2 \end{aligned}$ | $\begin{aligned} & 0.640 \\ & 0.818 \end{aligned}$ | WI (31) |
| Intersection geometry | Convert intersection to a multilane roundabout | Urban and rural | Intersections with low- and high-speed approaches | Total KABC | $\begin{aligned} & -6.2 \\ & 63.3 \end{aligned}$ | $\begin{aligned} & 1.062 \\ & 0.367 \end{aligned}$ | WI (31) |
| Intersection geometry | Convert two-way stop-controlled intersection to a roundabout | Urban <br> Rural | Intersections on two- or four-lane roads <br> Intersections on two- or four-lane roads | Total <br> KABC <br> Total <br> KABC | $\begin{aligned} & 27.0 \\ & 58.1 \\ & 48.2 \\ & 61.2 \end{aligned}$ | $\begin{aligned} & 0.730 \\ & 0.419 \\ & 0.518 \\ & 0.388 \end{aligned}$ | CA, CO, CT, FL, KS, MD, ME, MI, MO, MS, NV, OR, SC, UT, VT, WA WI $(31,33)$ |
| Intersection geometry | Convert all-way stop-controlled intersection to a roundabout | Urban and rural | Intersections on two- or four-lane roads | Total KABC | $\begin{array}{r} -7.4 \\ 8.7 \end{array}$ | $\begin{aligned} & 1.074 \\ & 0.913 \end{aligned}$ | CA, CO, CT, FL, KS, MD, ME, MI, MO, MS, NV, OR, SC, UT, VT, WA WI $(31,33)$ |
| Intersection geometry | Convert signalized intersection to a roundabout | $\begin{aligned} & \text { Urban } \\ & \text { Rural } \end{aligned}$ | Intersections on two- or four-lane roads <br> Intersections on two- or four-lane roads | Total <br> KABC <br> Total <br> KABC | $\begin{aligned} & 12.4 \\ & 66.1 \\ & 26.2 \\ & 71.5 \end{aligned}$ | $\begin{aligned} & 0.876 \\ & 0.339 \\ & 0.738 \\ & 0.285 \end{aligned}$ | CA, CO, CT, FL, IN, KS, MD, ME, MI, MO, MS, NC, NV, NY, OR, SC, UT, VT, WA, WI $(15,31,33)$ |

TABLE A. 1
(Continued)

| Category | Countermeasure | Area type | Facility type | Crash type | CRF | CMF | States and (reference number) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection geometry | Convert a non-controlled or yield-controlled intersection to a roundabout | Urban and rural | Intersections on two- or four-lane roads | Total KABC | $\begin{gathered} -24.2 \\ 100.0 \end{gathered}$ | $\begin{aligned} & 1.242 \\ & 0.000 \end{aligned}$ | WI (31) |
| Intersection geometry | Convert two-way stop-controlled intersection to J-turn intersection | Rural | Intersections of four-lane divided, high-speed roads and minor roads | Total KABC | $\begin{aligned} & 34.8 \\ & 53.7 \end{aligned}$ | $\begin{aligned} & 0.652 \\ & 0.463 \end{aligned}$ | MO (8) |
| Intersection geometry | Improve left-turn lane offset to create positive offset | Urban and rural | Four-leg intersections | Total <br> KABC <br> Left-turn <br> Rear-end | $\begin{aligned} & 33.8 \\ & 35.6 \\ & 38.0 \\ & 31.7 \end{aligned}$ | $\begin{aligned} & 0.662 \\ & 0.644 \\ & 0.620 \\ & 0.683 \end{aligned}$ | WI (30) |
| Intersection geometry | Improve intersection sight distance | Urban and rural | Not specified | Total <br> Right-angle <br> Left-turn <br> Sideswipe | $\begin{aligned} & 33.0 \\ & 21.0 \\ & 13.0 \\ & 43.0 \end{aligned}$ | $\begin{aligned} & 0.670 \\ & 0.790 \\ & 0.870 \\ & 0.570 \end{aligned}$ | Based on AK, AZ, CA, IA, KY, MO (13) <br> Based on AZ, MO, MN (13) <br> Based on AZ, MO (13) <br> Based on AK, MO (13) |
| Intersection traffic control | Change left-turn phasing on one approach from permitted to protected/permitted phasing | Urban | Four-leg intersections | Total <br> KABC <br> Left-turn <br> Rear-end | $\begin{array}{r} -8.1 \\ 0.5 \\ 7.5 \\ -9.4 \end{array}$ | $\begin{aligned} & 1.081 \\ & 0.995 \\ & 0.925 \\ & 1.094 \end{aligned}$ | NC, Toronto (39) |
| Intersection traffic control | Change left-turn phasing on more than one approach from permitted to protected/permitted phasing | Urban | Four-leg intersections | Total <br> KABC <br> Left-turn <br> Rear-end | $\begin{array}{r} 4.2 \\ 8.6 \\ 21.3 \\ -5.0 \end{array}$ | $\begin{aligned} & 0.958 \\ & 0.914 \\ & 0.787 \\ & 1.050 \end{aligned}$ | NC, Toronto (39) |
| Intersection traffic control | Change left-turn phasing from permitted or permitted/protected to protected-only phasing | Urban | Signalized intersections | Total Left-turn | $\begin{array}{r} 1 \\ 99 \end{array}$ | $\begin{aligned} & 0.99 \\ & 0.01 \end{aligned}$ | NC (17) |
| Intersection traffic control | Supplement left-turn phasing from at least one permitted approach with flashing yellow arrow | Urban | Four-leg intersections | Total <br> Left-turn | $\begin{aligned} & 24.7 \\ & 36.5 \end{aligned}$ | $\begin{aligned} & 0.753 \\ & 0.635 \end{aligned}$ | NC, OR, WA (39) |
| Intersection traffic control | Change left-turn phasing from protected/permitted to flashing yellow arrow | Urban | Four-leg intersections | Total <br> Left-turn | $\begin{array}{r} 7.8 \\ 19.4 \end{array}$ | $\begin{aligned} & 0.922 \\ & 0.806 \end{aligned}$ | NC, OR, WA (39) |
| Intersection traffic control | Change left-turn phasing from protected to flashing yellow arrow | Urban | Four-leg intersections | Total Left-turn | $\begin{array}{r} -33.8 \\ -124.2 \end{array}$ | $\begin{aligned} & 1.338 \\ & 2.242 \end{aligned}$ | NC, OR, WA (39) |

TABLE A. 1
(Continued)

| Category | Countermeasure | Area type | Facility type | Crash type | CRF | CMF | States and (reference number) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection traffic control | Convert two-way stop control to all-way stop control | Urban and rural | Four-leg intersections | Total | 68 | 0.32 | NC (34) |
|  |  |  |  | KABC | 77 | 0.23 |  |
|  |  |  |  | Frontal impact | 75 | 0.25 |  |
|  |  |  |  | Ran stop sign | 15 | 0.85 |  |
| Intersection traffic control | Improve signal visibility | Urban | Four-leg intersections on three- to four-lane roads | Daytime PDO | 9.9 | 0.901 | British Columbia (9) |
|  |  |  |  | Daytime KABC | -0.4 | 1.004 |  |
|  |  |  |  | Nighttime PDO | 13.3 | 0.867 |  |
|  |  |  |  | Nighttime KABC | 9.8 | 0.902 |  |
| Intersection traffic control | Increase yellow change interval (1.0 seconds) | Urban | Three- and four-leg intersections | Total | -14.1 | 1.141 | CA, MD (39) |
|  |  |  |  | KABC | -7.3 | 1.073 |  |
|  |  |  |  | Rear-end | 6.6 | 0.934 |  |
|  |  |  |  | Angle | -7.6 | 1.076 |  |
| Intersection traffic control | Increase all-red clearance interval (average of 1.1 seconds) | Urban | Three- and four-leg intersections | Total | 20.2 | 0.798 | CA, MD (39) |
|  |  |  |  | KABC | 13.7 | 0.863 |  |
|  |  |  |  | Rear-end | 19.6 | 0.804 |  |
|  |  |  |  | Angle | 3.4 | 0.966 |  |
| Intersection traffic control | Increase yellow interval (average of 0.8 seconds) and add all-red interval (average of 1.2 seconds) | Urban | Three- and four-leg intersections | Total | 1.0 | 0.990 | CA, MD (39) |
|  |  |  |  | KABC | -2.0 | 1.020 |  |
|  |  |  |  | Rear-end | -11.7 | 1.117 |  |
|  |  |  |  | Angle | 3.9 | 0.961 |  |
| Intersection traffic control | Install transverse rumble strips on approaches to stop-controlled intersection | Rural | Three-leg intersections on major collectors | Total | -22.3 | 1.223 | IA, MN (38) |
|  |  |  |  | PDO | -28.4 | 1.284 |  |
|  |  |  |  | KA | 59 | 0.41 |  |
|  |  |  | Four-leg intersections on major collectors | Total | -6.6 | 1.066 |  |
|  |  |  |  | PDO | -13.8 | 1.138 |  |
|  |  |  |  | KA | 34.8 | 0.652 |  |
| Intersection traffic control | Install new traffic signal at previously stop-controlled intersection | Urban | Three-leg intersections | KABC | 14 | 0.86 | CA, FL, MD, VA, WI, Toronto (25) |
|  |  |  |  | Right-angle KABC | 34 | 0.66 |  |
|  |  |  |  | Rear-end KABC | -50 | 1.50 |  |
|  |  |  | Four-leg intersections | KABC | 23 | 0.77 |  |
|  |  |  |  | Right-angle KABC | 67 | 0.33 |  |
|  |  |  |  | Rear-end KABC | -38 | 1.38 |  |
|  |  | Rural | Three- and four-leg intersections | Total | 44 | 0.56 | CA, MN (17) |
|  |  |  |  | Right-angle | 77 | 0.23 |  |
|  |  |  |  | Rear-end | -58 | 1.58 |  |
|  |  |  |  | Left-turn | 60 | 0.40 |  |

Intersection traffic Replace standard stop sign with Urban and Two-lane highways control
TABLE A. 1
(Continued)

| Category | Countermeasure | Area type | Facility type | Crash type | CRF | CMF | States and (reference number) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection traffic control | Retime signal change intervals to Institute of Transportation Engineers (ITE) standards | Urban | Four-leg intersections | Total | 8 | 0.92 | NY (32) |
|  |  |  |  | KABC | 12 | 0.88 |  |
|  |  |  |  | Rear-end | -12 | 1.12 |  |
|  |  |  |  | Rear-end KABC | -8 | 1.08 |  |
|  |  |  |  | Angle | 4 | 0.96 |  |
|  |  |  |  | Angle KABC | -6 | 1.06 |  |
|  |  |  |  | Vehicle/bicycle and vehicle/ pedestrian | 37 | 0.63 |  |
|  |  |  |  | Vehicle/bicycle and vehicle/ pedestrian KABC | 37 | 0.63 |  |
| ITS and advanced technology | Install actuated advance intersection warning system at high-speed intersection | Urban and rural | Four-lane high-speed divided highways (major road) | Total | 8.2 | 0.918 | NE (2) |
|  |  |  |  | KABC | 11.3 | 0.887 |  |
|  |  |  |  | Rear-end | 1.2 | 0.988 |  |
|  |  |  |  | Right-angle | 43.6 | 0.564 |  |
| ITS and advanced technology | Install changeable horizontal curve speed warning signs | Rural | Two-lane highways | Total | 5.0 | 0.950 | $\begin{aligned} & \text { AZ, FL, IA, OH, } \\ & \text { OR, TX, WA (16) } \end{aligned}$ |
| ITS and advanced technology | Install variable speed limit signs | Urban | Principal arterial interstates | Total | 8.0 | 0.920 | MO (5) |
| ITS and advanced technology | Install"Vehicle Entering When Flashing" (VEWF) system with advance post mounted signs on major approach and loops on minor approach | Urban and rural | Highways with 35-55 mph mainline approach speeds | Total <br> KABC <br> Target (angle, head-on, left-turn, and right-turn) | $\begin{aligned} & 32 \\ & 27 \\ & 32 \end{aligned}$ | $\begin{aligned} & 0.68 \\ & 0.73 \\ & 0.68 \end{aligned}$ | NC (35) |
| Pavement | Improve pavement condition from poor (critical condition index below 60) to good (critical condition index above 70) | Rural | Two-lane highways | Total KABC | $\begin{gathered} -3.0 \\ 26.0 \end{gathered}$ | $\begin{aligned} & 1.030 \\ & 0.740 \end{aligned}$ | VA (46) |
| Pedestrians | Construct pedestrian bridge or tunnel | Urban | Not specified | Pedestrian | 86 | 0.14 | Based on AK, AZ, KY, MO (13) |
| Pedestrians | Install High intensity Activated crossWalK (HAWK) at intersection | Urban | Crossings of four- to six-lane roads | Total <br> KA <br> Pedestrian | $\begin{aligned} & 29 \\ & 15 \\ & 69 \end{aligned}$ | $\begin{aligned} & 0.71 \\ & 0.85 \\ & 0.31 \end{aligned}$ | AZ (12) |
| Pedestrians | Install sidewalk | Urban | Not specified | Pedestrian | 74 | 0.26 | Based on AK, AZ, KY, MO, OK (13) |
| Railroads | Build grade-separated crossing | Urban and rural | Not specified | Total | 39 | 0.61 | Based on IA (13) |
| Railroads | Eliminate railroad crossing | Urban and rural | Not specified | Total | 75 | 0.25 | Based on IA (13) |

TABLE A. 1
(Continued)

\begin{tabular}{|c|c|c|c|c|c|c|c|}
\hline Category \& Countermeasure \& Area type \& Facility type \& Crash type \& CRF \& CMF \& States and (reference number) \\
\hline Railroads \& Install gates at crossings with signs \& Urban and rural \& Arterials, collectors, local roads \& Total \& 93 \& 0.07 \& Canada (26) \\
\hline Railroads \& Upgrade signs to flashing lights \& Urban and rural \& Arterials, collectors, local roads \& Total \& 77 \& 0.23 \& Canada (26) \\
\hline Roadside \& Increase median width from 10 feet to 20 feet \& Rural \& Four-lane divided highways \& Multiple vehicle \& 9 \& 0.91 \& CA, KY, MN (40) \\
\hline Roadside \& Increase median width from 10 feet to 30 feet \& Rural \& Four-lane divided highways \& Multiple vehicle \& 17 \& 0.83 \& CA, KY, MN (40) \\
\hline Roadside \& Increase median width from 10 feet to 40 feet \& Rural \& Four-lane divided highways \& Multiple vehicle \& 25 \& 0.75 \& CA, KY, MN (40) \\
\hline Roadside \& Increase median width from 10 feet to 50 feet \& Rural \& Four-lane divided highways \& Multiple vehicle \& 32 \& 0.68 \& CA, KY, MN (40) \\
\hline Roadside \& Increase median width from 10 feet to 60 feet \& Rural \& Four-lane divided highways \& Multiple vehicle \& 38 \& 0.62 \& CA, KY, MN (40) \\
\hline Roadside \& Increase median width from 10 feet to 70 feet \& Rural \& Four-lane divided highways \& Multiple vehicle \& 43 \& 0.57 \& CA, KY, MN (40) \\
\hline Roadside \& Increase median width from 10 feet to 80 feet \& Rural \& Four-lane divided highways \& Multiple vehicle \& 49 \& 0.51 \& CA, KY, MN (40) \\
\hline Roadside \& Install guardrail \& Urban and rural \& Not specified \& \begin{tabular}{l}
Total \\
BC \\
KA \\
Run-off-the-road
\end{tabular} \& \[
\begin{aligned}
\& 11 \\
\& 40 \\
\& 65 \\
\& 30
\end{aligned}
\] \& \[
\begin{aligned}
\& 0.89 \\
\& 0.60 \\
\& 0.35 \\
\& 0.70
\end{aligned}
\] \& \begin{tabular}{l}
Based on AZ, IA, \\
IN, KY, \\
MO (13)
\end{tabular} \\
\hline Roadside \& Install cable median barrier (hightensioned) on depressed median of 50 feet wide or wider \& Rural \& Principal arterial interstates \& \begin{tabular}{l}
Multiple-vehicle, opposite direction (cross median, frontal and opposing direction sideswipe, head-on) \\
Single-vehicle crashes (fixed object, run-off-the-road)
\end{tabular} \& 96

-72 \& $$
0.04
$$

$$
1.72
$$ \& IN (45) <br>

\hline Roadside \& Install concrete median barrier \& Rural \& Interstates \& | Single-vehicle |
| :--- |
| Multiple-vehicle, same direction |
| Multiple-vehicle opposite direction | \& \[

$$
\begin{array}{r}
-120 \\
20 \\
100
\end{array}
$$

\] \& \[

$$
\begin{aligned}
& 2.20 \\
& 0.80 \\
& 0.00
\end{aligned}
$$

\] \& | CO, IL, IN, MO, |
| :--- |
| NY, OH, OR, WA (41) | <br>

\hline Roadside \& Change in sideslope from $1 \mathrm{~V}: 3 \mathrm{H}$ to

\[
1 \mathrm{~V}: 4 \mathrm{H}

\] \& Rural \& Not specified \& | PDO |
| :--- |
| KABC | \& \[

$$
\begin{aligned}
& 29 \\
& 42
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.71 \\
& 0.58
\end{aligned}
$$
\] \& Not specified (10) <br>

\hline Roadside \& Change in sideslope from $1 \mathrm{~V}: 4 \mathrm{H}$ to 1V:6H \& Rural \& Not specified \& | PDO |
| :--- |
| KABC | \& \[

$$
\begin{aligned}
& 24 \\
& 22
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.76 \\
& 0.78
\end{aligned}
$$
\] \& Not specified (10) <br>

\hline Roadside \& Remove or relocate fixed objects outside of clear zone \& Urban and rural \& Arterials, collectors \& Total KABC \& $$
\begin{aligned}
& 38.2 \\
& 38.1
\end{aligned}
$$ \& \[

$$
\begin{aligned}
& 0.618 \\
& 0.619
\end{aligned}
$$
\] \& OH (19) <br>

\hline
\end{tabular}

TABLE A. 1
(Continued)

| Category | Countermeasure | Area type | Facility type | Crash type | CRF | CMF | States and (reference number) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Road diet | Re-stripe four-lane undivided road to three-lane (with TWLTL) | Urban | Minor arterials | Total | 29 | 0.71 | CA, IA, WA (17) |
| Roadway delineation | Add no passing striping | Rural | Not specified | Total <br> Head-on <br> Sideswipe | $\begin{aligned} & 53 \\ & 40 \\ & 40 \end{aligned}$ | $\begin{aligned} & 0.47 \\ & 0.60 \\ & 0.60 \end{aligned}$ | Based on MT (13) Based on KY, MO (13) |
| Roadway delineation | Install centerline rumble strips | Urban <br> Rural | Two-lane roads | Target (head-on, oppositedirection sideswipe) <br> Target KABC <br> Total <br> KABC <br> Target <br> Target KABC | $\begin{array}{r} 40 \\ 64 \\ 9 \\ 12 \\ 30 \\ 44 \end{array}$ | $\begin{aligned} & 0.60 \\ & 0.36 \\ & 0.91 \\ & 0.88 \\ & 0.70 \\ & 0.56 \end{aligned}$ | CA, CO, DE, MD, MN, OR, PA, WA (43) |
| Roadway delineation | Install shoulder rumble strips | Rural | Two-lane roads <br> Freeways | Run-off-the-road <br> Run-off-the-road KABC <br> Run-off-the-road <br> Run-off-the-road KABC | $\begin{aligned} & 15 \\ & 29 \\ & 11 \\ & 16 \end{aligned}$ | $\begin{aligned} & 0.85 \\ & 0.71 \\ & 0.89 \\ & 0.84 \end{aligned}$ | MN, MO, PA (43) |
| Roadway delineation | Install centerline plus shoulder rumble strips | Rural | Two-lane roads | Total <br> KABC <br> Head-on <br> Run-off-the-road <br> Opposite-direction sideswipe | $\begin{aligned} & 18.6 \\ & 22.9 \\ & 36.8 \\ & 25.8 \\ & 23.3 \end{aligned}$ | $\begin{aligned} & 0.814 \\ & 0.771 \\ & 0.632 \\ & 0.742 \\ & 0.767 \end{aligned}$ | $\begin{gathered} \text { KY, MI, MO, } \\ \text { PA }(21,23) \end{gathered}$ |
| Roadway delineation | Install edgeline pavement markings on curves | Rural | Two-lane highways | Total <br> Run-off-the-road Speed-related (nighttime) | $\begin{array}{r} 25.9 \\ 11.0 \\ 3.7 \end{array}$ | $\begin{aligned} & 0.741 \\ & 0.890 \\ & 0.963 \end{aligned}$ | TX (44) |
| Roadway delineation | Install edgeline pavement markings on tangent sections | Rural | Two-lane highways | Total <br> Run-off-the-road <br> Speed-related (nighttime) | $\begin{array}{r} 6.1 \\ 13.4 \\ 3.4 \end{array}$ | $\begin{aligned} & 0.939 \\ & 0.866 \\ & 0.966 \end{aligned}$ | TX (44) |

TABLE A. 1
(Continued)

| Category | Countermeasure | Area type | Facility type | Crash type | CRF | CMF | States and (reference number) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Roadway delineation | Install raised pavement markers | Rural | $\begin{aligned} & \text { Two-lane highways with AADT } \\ & 0-5000, \text { curve radius } \\ & \mathrm{R} \geq 1640 \mathrm{ft} \end{aligned}$ | Nighttime | -16 | 1.16 | $\begin{gathered} \text { IL, NJ, NY, } \\ \text { PA (4) } \end{gathered}$ |
|  |  |  | Two-lane highways with AADT 5001-15000, curve radius $\mathrm{R} \geq 1640 \mathrm{ft}$ | Nighttime | 1 | 0.99 |  |
|  |  |  | Two-lane highways with AADT 15001-20000, curve radius $\mathrm{R} \geq 1640 \mathrm{ft}$ | Nighttime | 24 | 0.76 |  |
|  |  |  | $\begin{aligned} & \text { Two-lane highways with AADT } \\ & 0-5000, \text { curve radius } \\ & \mathrm{R}<1640 \mathrm{ft} \end{aligned}$ | Nighttime | -43 | 1.43 |  |
|  |  |  | Two-lane highways with AADT 5001-15000, curve radius $\mathrm{R}<1640 \mathrm{ft}$ | Nighttime | -26 | 1.26 |  |
|  |  |  | Two-lane highways with AADT <br> 15001-20000, curve radius $\mathrm{R}<1640 \mathrm{ft}$ | Nighttime | -3 | 1.03 |  |
|  |  |  | Four-lane freeways with AADT $\leq 20000$ | Nighttime | -13 | 1.13 | $\begin{aligned} & \text { MO, NY, PA, } \\ & \text { WI (4) } \end{aligned}$ |
|  |  |  | Four-lane freeways with AADT 20001-60000 | Nighttime | 6 | 0.94 |  |
|  |  |  | $\begin{aligned} & \text { Four-lane freeways with AADT } \\ & >60000 \\ & \hline \end{aligned}$ | Nighttime | 33 | 0.67 |  |
| Segments | Increase in number of through lanes by 1 lane* | Urban | Multilane | $\begin{aligned} & \text { PDO } \\ & \text { KABC } \end{aligned}$ | $\begin{aligned} & 61.3 \\ & 66.5 \end{aligned}$ | $\begin{aligned} & 0.387 \\ & 0.335 \end{aligned}$ | IN (42) |
| Segments | Convert two-lane roadway to four-lane divided roadway | Urban | Before: Two-lane roadway | Total | 65.9 | 0.341 | FL (1) |
|  |  |  | After: Four-lane divided | PDO | 64.9 | 0.351 |  |
|  |  |  | roadway | KABC | 63.3 | 0.367 |  |
|  |  | Rural | Before: Two-lane roadway | Total | 28.8 | 0.712 |  |
|  |  |  | After: Four-lane divided | PDO | 30.9 | 0.691 |  |
|  |  |  | roadway | KABC | 45.1 | 0.549 |  |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 11 foot lanes and 7 foot shoulders | Rural | Two-lane highways | Run-off-the-road, head-on, sideswipe | 10 | 0.90 | PA (14) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 10 foot lanes and 8 foot shoulders | Rural | Two-lane highways | Run-off-the-road, head-on, sideswipe | 62 | 0.38 | PA (14) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 12 foot lanes and 5 foot shoulders | Rural | Two-lane highways | Run-off-the-road, head-on, sideswipe | 13 | 0.87 | PA (14) |

TABLE A. 1
(Continued)

| Category | Countermeasure | Area type | Facility type | Crash type | CRF | CMF | States and (reference number) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 11 foot lanes and 6 foot shoulders | Rural | Two-lane highways | Run-off-the-road, head-on, sideswipe | 16 | 0.84 | PA (14) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 10 foot lanes and 7 foot shoulders | Rural | Two-lane highways | Run-off-the-road, head-on, sideswipe | -96 | 1.96 | PA (14) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 12 foot lanes and 4 foot shoulders | Rural | Two-lane highways | Run-off-the-road, head-on, sideswipe | -4 | 1.04 | PA (14) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 11 foot lanes and 5 foot shoulders | Rural | Two-lane highways | Run-off-the-road, head-on, sideswipe | -6 | 1.06 | PA (14) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 10 foot lanes and 6 foot shoulders | Rural | Two-lane highways | Run-off-the-road, head-on, sideswipe | 25 | 0.75 | PA (14) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 12 foot lanes and 3 foot shoulders | Rural | Two-lane highways | Run-off-the-road, head-on, sideswipe | -11 | 1.11 | PA (14) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 11 foot lanes and 4 foot shoulders | Rural | Two-lane highways | Run-off-the-road, head-on, sideswipe | -14 | 1.14 | PA (14) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 10 foot lanes and 5 foot shoulders | Rural | Two-lane highways | Run-off-the-road, head-on, sideswipe | -22 | 1.22 | PA (14) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 12 foot lanes and 2 foot shoulders | Rural | Two-lane highways | Run-off-the-road, head-on, sideswipe | -16 | 1.16 | PA (14) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 11 foot lanes and 3 foot shoulders | Rural | Two-lane highways | Run-off-the-road, head-on, sideswipe | -19 | 1.19 | PA (14) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 10 foot lanes and 4 foot shoulders | Rural | Two-lane highways | Run-off-the-road, head-on, sideswipe | -20 | 1.20 | PA (14) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 12 foot lanes and 1 foot shoulders | Rural | Two-lane highways | Run-off-the-road, head-on, sideswipe | -85 | 1.85 | PA (14) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 11 foot lanes and 2 foot shoulders | Rural | Two-lane highways | Run-off-the-road, head-on, sideswipe | -12 | 1.12 | PA (14) |

TABLE A. 1
(Continued)

| Category | Countermeasure | Area type | Facility type | Crash type | CRF | CMF | States and (reference number) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 10 foot lanes and 3 foot shoulders | Rural | Two-lane highways | Run-off-the-road, head-on, sideswipe | -13 | 1.13 | PA (14) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 12 foot lanes and 0 foot shoulders* | Urban | Urban and suburban arterials | Total | -42.7 | 1.427 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 12 foot lanes and 1 foot shoulders* | Urban | Urban and suburban arterials | Total | -34.5 | 1.345 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 12 foot lanes and 2 foot shoulders* | Urban | Urban and suburban arterials | Total | -26.7 | 1.267 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 12 foot lanes and 3 foot shoulders* | Urban | Urban and suburban arterials | Total | -19.4 | 1.194 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 12 foot lanes and 4 foot shoulders* | Urban | Urban and suburban arterials | Total | -12.6 | 1.126 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 12 foot lanes and 5 foot shoulders* | Urban | Urban and suburban arterials | Total | -6.1 | 1.061 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 12 foot lanes and 7 foot shoulders* | Urban | Urban and suburban arterials | Total | 5.8 | 0.942 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 12 foot lanes and 8 foot shoulders* | Urban | Urban and suburban arterials | Total | 11.2 | 0.888 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 12 foot lanes and 9 foot shoulders* | Urban | Urban and suburban arterials | Total | 16.3 | 0.837 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 12 foot lanes and 10 foot shoulders* | Urban | Urban and suburban arterials | Total | 21.1 | 0.789 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 10 foot lanes and 0 foot shoulders* | Urban | Urban and suburban arterials | Total | -270.5 | 3.705 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 10 foot lanes and 1 foot shoulders* | Urban | Urban and suburban arterials | Total | -248.4 | 3.484 | IL (22) |

TABLE A. 1
(Continued)

| Category | Countermeasure | Area type | Facility type | Crash type | CRF | CMF | States and (reference number) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 10 foot lanes and 2 foot shoulders* | Urban | Urban and suburban arterials | Total | -227.6 | 3.276 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 10 foot lanes and 3 foot shoulders* | Urban | Urban and suburban arterials | Total | -208 | 3.08 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 10 foot lanes and 4 foot shoulders* | Urban | Urban and suburban arterials | Total | -189.6 | 2.896 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 10 foot lanes and 5 foot shoulders* | Urban | Urban and suburban arterials | Total | -172.3 | 2.723 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 10 foot lanes and 6 foot shoulders* | Urban | Urban and suburban arterials | Total | -156 | 2.56 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 10 foot lanes and 7 foot shoulders* | Urban | Urban and suburban arterials | Total | -140.7 | 2.407 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 10 foot lanes and 8 foot shoulders* | Urban | Urban and suburban arterials | Total | -126.3 | 2.263 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 10 foot lanes and 9 foot shoulders* | Urban | Urban and suburban arterials | Total | -112.8 | 2.128 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 10 foot lanes and 10 foot shoulders* | Urban | Urban and suburban arterials | Total | -100.1 | 2.001 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 11 foot lanes and 0 foot shoulders* | Urban | Urban and suburban arterials | Total | -14.2 | 1.142 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 11 foot lanes and 1 foot shoulders* | Urban | Urban and suburban arterials | Total | -10.4 | 1.104 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 11 foot lanes and 2 foot shoulders* | Urban | Urban and suburban arterials | Total | -6.8 | 1.068 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 11 foot lanes and 3 foot shoulders* | Urban | Urban and suburban arterials | Total | -3.3 | 1.033 | IL (22) |

TABLE A. 1
(Continued)

| Category | Countermeasure | Area type | Facility type | Crash type | CRF | CMF | States and (reference number) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 11 foot lanes and 4 foot shoulders* | Urban | Urban and suburban arterials | Total | 0.1 | 0.999 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 11 foot lanes and 5 foot shoulders* | Urban | Urban and suburban arterials | Total | 3.4 | 0.966 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 11 foot lanes and 6 foot shoulders* | Urban | Urban and suburban arterials | Total | 6.6 | 0.934 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 11 foot lanes and 7 foot shoulders* | Urban | Urban and suburban arterials | Total | 9.7 | 0.903 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 11 foot lanes and 8 foot shoulders* | Urban | Urban and suburban arterials | Total | 12.6 | 0.874 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 11 foot lanes and 9 foot shoulders* | Urban | Urban and suburban arterials | Total | 15.5 | 0.845 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 11 foot lanes and 10 foot shoulders* | Urban | Urban and suburban arterials | Total | 18.3 | 0.817 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 13 foot lanes and 0 foot shoulders* | Urban | Urban and suburban arterials | Total | -23.8 | 1.238 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 13 foot lanes and 1 foot shoulders* | Urban | Urban and suburban arterials | Total | -16.8 | 1.168 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 13 foot lanes and 2 foot shoulders* | Urban | Urban and suburban arterials | Total | -10.1 | 1.101 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 13 foot lanes and 3 foot shoulders* | Urban | Urban and suburban arterials | Total | -3.8 | 1.038 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 13 foot lanes and 4 foot shoulders* | Urban | Urban and suburban arterials | Total | 2.1 | 0.979 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 13 foot lanes and 5 foot shoulders* | Urban | Urban and suburban arterials | Total | 7.6 | 0.924 | IL (22) |

TABLE A. 1
(Continued)

| Category | Countermeasure | Area type | Facility type | Crash type | CRF | CMF | States and (reference number) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 13 foot lanes and 6 foot shoulders* | Urban | Urban and suburban arterials | Total | 12.9 | 0.871 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 13 foot lanes and 7 foot shoulders* | Urban | Urban and suburban arterials | Total | 17.9 | 0.821 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 13 foot lanes and 8 foot shoulders* | Urban | Urban and suburban arterials | Total | 22.5 | 0.775 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 13 foot lanes and 9 foot shoulders* | Urban | Urban and suburban arterials | Total | 26.9 | 0.731 | IL (22) |
| Segments | Convert 12 foot lanes and 6 foot shoulders to 13 foot lanes and 10 foot shoulders* | Urban | Urban and suburban arterials | Total | 31.1 | 0.689 | IL (22) |
| Segments | Extend on-ramp acceleration lane by 30 meters (about 100 feet) | Urban and rural | Grade-separated junctions | Total | 11 | 0.89 | Not specified (10) |
| Segments | Extend off-ramp deceleration lane by 30 meters (about 100 feet) | $\begin{aligned} & \text { Urban and } \\ & \text { rural } \\ & \hline \end{aligned}$ | Grade-separated junctions | Total | 7 | 0.93 | Not specified (10) |
| Segments | Install passing relief lane | Rural | Two-lane highways | Total <br> KABC <br> Target (head-on, rear-end, run-off-the-road, sideswipe) <br> Peak month (June, July, August) Off-peak month | $\begin{aligned} & 33 \\ & 29 \\ & 47 \\ & 46 \\ & 28 \end{aligned}$ | $\begin{aligned} & 0.67 \\ & 0.71 \\ & 0.53 \\ & 0.54 \\ & 0.72 \end{aligned}$ | MI (3) |
| Segments | Increase lane width by 1 foot* | Urban Rural | Two-lane roads <br> Multilane roads <br> Two-lane roads <br> Multilane roads | $\begin{aligned} & \text { PDO } \\ & \text { KABC } \\ & \text { PDO } \\ & \text { KABC } \\ & \text { PDO } \\ & \text { KABC } \\ & \text { PDO } \\ & \text { KABC } \end{aligned}$ | 6.6 14.2 2.0 14.1 8.2 7.4 17.7 21.2 | $\begin{aligned} & 0.934 \\ & 0.858 \\ & 0.980 \\ & 0.859 \\ & 0.918 \\ & 0.926 \\ & 0.823 \\ & 0.788 \end{aligned}$ | IN (42) |
| Segments | Increase lane width by 2 feet* | Urban Rural | Two-lane roads <br> Multilane roads <br> Two-lane roads <br> Multilane roads | $\begin{aligned} & \text { PDO } \\ & \text { KABC } \\ & \text { PDO } \\ & \text { KABC } \\ & \text { PDO } \\ & \text { KABC } \\ & \text { PDO } \\ & \text { KABC } \end{aligned}$ | $\begin{array}{r} 12.7 \\ 26.3 \\ 4.0 \\ 26.2 \\ 15.7 \\ 14.3 \\ 32.2 \\ 37.9 \end{array}$ | $\begin{aligned} & 0.873 \\ & 0.737 \\ & 0.960 \\ & 0.738 \\ & 0.843 \\ & 0.857 \\ & 0.678 \\ & 0.621 \end{aligned}$ | IN (42) |

TABLE A. 1

| Category | Countermeasure | Area type | Facility type | Crash type | CRF | CMF | States and (reference number) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Segments | Increase lane width by 3 feet* | Urban | Two-lane roads | PDO | 18.4 | 0.816 | IN (42) |
|  |  |  |  | KABC | 36.8 | 0.632 |  |
|  |  |  | Multilane roads | PDO | 6.0 | 0.940 |  |
|  |  |  |  | KABC | 36.6 | 0.634 |  |
|  |  | Rural | Two-lane roads | PDO | 22.6 | 0.774 |  |
|  |  |  |  | KABC | 20.7 | 0.793 |  |
|  |  |  | Multilane roads | PDO | 44.2 | 0.558 |  |
|  |  |  |  | KABC | 51.1 | 0.489 |  |
| Segments | Increase lane width by 4 feet* | Urban | Two-lane roads | PDO | 23.8 | 0.762 | IN (42) |
|  |  |  |  | KABC | 45.7 | 0.543 |  |
|  |  |  | Multilane roads | PDO | 7.9 | 0.921 |  |
|  |  |  |  | KABC | 45.6 | 0.544 |  |
|  |  | Rural | Two-lane roads | PDO | 28.9 | 0.711 |  |
|  |  |  |  | KABC | 26.6 | 0.734 |  |
|  |  |  | Multilane roads | PDO | 54.0 | 0.460 |  |
|  |  |  |  | KABC | 61.5 | 0.385 |  |
| Shoulder treatment | Increase right shoulder width by 1 foot* | Urban | Two-lane roads Multilane roads Two-lane road | PDO | 1.7 | 0.983 | IN (42) |
|  |  |  |  | PDO | 1.6 | 0.984 |  |
|  |  | Rural |  | PDO | 2.3 | 0.977 |  |
|  |  |  |  | KABC | 2.8 | 0.972 |  |
|  |  |  | Multilane roads | KABC | 4.0 | 0.960 |  |
| Shoulder treatment | Increase right shoulder width by 2 feet* | Urban | Two-lane roads Multilane roads Two-lane roads | PDO | 3.5 | 0.965 | IN (42) |
|  |  |  |  | PDO | 3.1 | 0.969 |  |
|  |  | Rural |  | PDO | 4.6 | 0.954 |  |
|  |  |  |  | KABC | 5.4 | 0.946 |  |
|  |  |  | Multilane roads | KABC | 7.9 | 0.921 |  |
| Shoulder treatment | Increase right shoulder width by 3 feet* | Urban <br> Rural | Two-lane roads Multilane roads Two-lane roads Multilane roads | PDO | 5.1 | 0.949 | IN (42) |
|  |  |  |  | PDO | 4.7 | 0.953 |  |
|  |  |  |  | PDO | 6.8 | 0.932 |  |
|  |  |  |  | KABC | 8.0 | 0.920 |  |
|  |  |  |  | KABC | 11.6 | 0.884 |  |
| Shoulder treatment | Increase right shoulder width by 4 feet* | Urban <br> Rural | Two-lane roads Multilane roads Two-lane roads <br> Multilane roads | PDO | 6.8 | 0.932 | IN (42) |
|  |  |  |  | PDO | 6.2 | 0.938 |  |
|  |  |  |  | PDO | 8.9 | 0.911 |  |
|  |  |  |  | KABC | 10.6 | 0.894 |  |
|  |  |  |  | KABC | 15.2 | 0.848 |  |
| Shoulder treatment | Increase left/inside shoulder width by 1 foot* | Urban Rural | Multilane roads Multilane roads | KABC | 18.5 | 0.815 | IN (42) |
|  |  |  |  | PDO | 4.3 | 0.957 |  |
|  |  |  |  | KABC | 6.7 | 0.933 |  |

TABLE A. 1
(Continued)

| Category | Countermeasure | Area type | Facility type | Crash type | CRF | CMF | States and (reference number) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder treatment | Increase left/inside shoulder width by 2 feet* | Urban <br> Rural | Multilane roads Multilane roads | KABC | 33.6 | 0.664 | IN (42) |
|  |  |  |  | PDO | 8.5 | 0.915 |  |
|  |  |  |  | KABC | 13.0 | 0.870 |  |
| Shoulder treatment | Increase left/inside shoulder width by 3 feet* | Urban <br> Rural | Multilane roads Multilane roads | KABC | 45.9 | 0.541 | IN (42) |
|  |  |  |  | PDO | 12.4 | 0.876 |  |
|  |  |  |  | KABC | 18.9 | 0.811 |  |
| Shoulder treatment | Increase left/inside shoulder width by 4 feet* | Urban <br> Rural | Multilane roads Multilane roads | KABC | 56.0 | 0.440 | IN (42) |
|  |  |  |  | PDO | 16.2 | 0.838 |  |
|  |  |  |  | KABC | 24.3 | 0.757 |  |
| Signs | Install chevron signs on horizontal curves | Rural | Two-lane highways | Total | 4.3 | 0.957 | WA (37) |
|  |  |  |  | KABC | 16.4 | 0.836 |  |
|  |  |  |  | Lane departure | 5.9 | 0.941 |  |
|  |  |  |  | Nighttime | 24.5 | 0.755 |  |
|  |  |  |  | Nighttime lane departure | 22.1 | 0.779 |  |
| Signs | Increase retroreflectivity of stop signs | Urban and rural | Three- and four-leg stopcontrolled intersections | Total | 1.2 | 0.988 | CT, SC (28) |
|  |  |  |  | KABC | 6.7 | 0.933 |  |
|  |  |  |  | Right-angle | -1.2 | 1.012 |  |
|  |  |  |  | Rear-end | -2.2 | 1.022 |  |
|  |  |  |  | Nighttime | 4.4 | 0.956 |  |
|  |  |  |  | Daytime | -0.1 | 1.001 |  |
| Signs | Install flashing beacons at stopcontrolled intersections | Urban <br> Rural | Two-lane highways Two-lane highways | Angle | -12 | 1.12 | NC, SC (36) |
|  |  |  |  | Angle | 16 | 0.84 |  |
| Speed management | Lower posted speed by 15-20 mph | Urban and rural | Nonlimited access highways | Total | 6 | 0.94 | AZ, CA, CO, CT, DE, ID, IL, IN ME, MD, MA, MI, MS, NE, NJ, NM, OH, OK, TN, TX, VA, WV (27) |
| Speed management | Lower posted speed by 10 mph | Urban and rural | Nonlimited access highways | Total | 4 | 0.96 | AZ, CA, CO, CT DE, ID, IL, IN ME, MD, MA, MI, MS, NE, NJ, NM, OH, OK, TN, TX, VA, WV (27) |

TABLE A. 1
(Continued)

| Category | Countermeasure | Area type | Facility type | Crash type | CRF | CMF | States and (reference number) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Speed management | Lower posted speed by 5 mph | Urban and rural | Nonlimited access highways | Total | -17 | 1.17 | AZ, CA, CO, CT, DE, ID, IL, IN, ME, MD, MA, MI, MS, NE, NJ, NM, OH, OK, TN, TX, VA, WV (27) |
| Speed management | Raise posted speed by 5 mph | Urban and rural | Nonlimited access highways | Total | 8 | 0.92 | AZ, CA, CO, CT, DE, ID, IL, IN, ME, MD, MA, MI, MS, NE, NJ, NM, OH, OK, TN, TX, VA, WV (27) |
| Speed management | Raise posted speed by $10-15 \mathrm{mph}$ | Urban and rural | Nonlimited access highways | Total | 15 | 0.85 | $\mathrm{AZ}, \mathrm{CA}, \mathrm{CO}, \mathrm{CT}$, DE, ID, IL, IN, ME, MD, MA, MI, MS, NE, NJ, NM, OH, OK, TN, TX, VA, WV (27) |
| Speed management | Set appropriate speed limit | Urban and rural | Not specified | Total | 28 | 0.72 | Based on KY, MO, MT (13) |

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## APPENDIX B. CALIBRATED CMF, SPF, AND CRASH PERCENTAGES IMPLEMENTED IN THE IHSDM

This appendix summarizes the calibrated CMF and SPF parameters, as well as the updated crash

TABLE B. 1
Calibrated CMF RA for Lane Width and Shoulder Width on Rural Two-Lane Undivided Segments and Rural Multilane Divided Segments

| Countermeasure | Width <br> in feet | Rural two-lane <br> undivided | Rural multilane <br> divided |
| :--- | :---: | :---: | :---: |
| Lane width | 9 | 1.28 | 1.91 |
|  | 10 | 1.18 | 1.54 |
| Shoulder width | 11 | 1.08 | 1.24 |
|  | 12 | 1 | 1 |
|  | 0 | 1.17 | - |
|  | 2 | 1.11 | - |
|  | 4 | 1.05 | - |
|  | 6 | 1 | - |
|  | 8 or more | 0.95 | - |

TABLE B. 2
Calibrated CMF for Shoulder Width on Rural Multilane Divided Segments

| Shoulder width | Calibrated CMF |
| :--- | :---: |
| 0 | 1.39 |
| 2 | 1.28 |
| 4 | 1.17 |
| 6 | 1.08 |
| 8 or more | 1 |

percentages, which may be entered into the user interface of the IHSDM Administration Tool to reflect Indiana conditions. Table B. 1 presents the calibrated $\mathrm{CMF}_{\mathrm{RA}}$ (associated with related crash types) for lane width and shoulder width on rural two-lane undivided segments and for lane width on rural multilane divided segments. Furthermore, Table B. 2 gives the calibrated CMF for shoulder width on rural multilane divided segments. Table B. 3 provides the calibrated SPFs for all the rural and urban/suburban segment types under consideration. Table B. 4 and Table B. 5 give the general crash distributions and crash type percentages, respectively, for rural two-lane undivided segments. The crash type percentages are split be severity level for rural multilane divided segments in Table B.6; similarly, Table B. 7 provides the crash percentages by severity level for multiple-vehicle non-driveway crashes on urban/ suburban arterial segments.

TABLE B. 4
Indiana General Crash Distributions for Rural Two-Lane Undivided Segments (All Values in Percent)

| Crash severity level | Indiana |
| :--- | ---: |
| Related crash percentage | 100.00 |
| Fatal | 1.06 |
| Incapacitating injury | 5.09 |
| Nonincapacitating injury | 10.30 |
| Possible injury | 1.34 |

TABLE B. 3
Calibrated SPFs for Rural and Urban/Suburban Segments

| Area | Facility Type | Number of Vehicles | Crash <br> Type | Intercept | AADT | Length <br> $L$ (mi.) | Dispersion |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rural | Two-lane undivided | All | Total | 1.204* | 0.814 | 0.886 | 0.985 |
| Rural | Multilane divided | All | Total | -10.074 | 1.139 | 0.749 | 1.083 |
| Rural | Multilane divided | All | KABC | -12.736 | 1.238 | 0.608 | 0.806 |
| Rural | Multilane divided | All | KAB | -12.717 | 1.230 | 0.669 | 0.708 |
| Urban/suburban | Two-lane undivided | Multiple | Total | -13.357 | 1.452 | 0.307 | 1.813 |
| Urban/suburban | Two-lane undivided | Multiple | PDO | -14.117 | 1.502 | 0.287 | 2.110 |
| Urban/suburban | Two-lane undivided | Multiple | KABC | -13.864 | 1.366 | 0.437 | 2.240 |
| Urban/suburban | Four-lane undivided | Multiple | Total | -16.691 | 1.811 | 0.658 | 1.901 |
| Urban/suburban | Four-lane undivided | Multiple | PDO | -19.510 | 2.087 | 0.747 | 2.013 |
| Urban/suburban | Four-lane undivided | Multiple | KABC | -14.163 | 1.401 | 0.689 | 1.343 |
| Urban/suburban | Four-lane divided | Multiple | Total | -9.896 | 1.093 | 0.664 | 2.145 |
| Urban/suburban | Four-lane divided | Multiple | PDO | -10.105 | 1.092 | 0.677 | 2.337 |
| Urban/suburban | Four-lane divided | Multiple | KABC | -11.124 | 1.054 | 0.594 | 2.163 |
| Urban/suburban | Two-lane undivided | Single | Total | -2.624 | 0.300 | 0.980 | 1.156 |
| Urban/suburban | Two-lane undivided | Single | PDO | -2.051 | 0.217 | 0.979 | 1.214 |
| Urban/suburban | Two-lane undivided | Single | KABC | -9.934 | 0.896 | 0.994 | 0.576 |
| Urban/suburban | Four-lane divided | Single | Total | -7.583 | 0.824 | 1.184 | 1.051 |
| Urban/suburban | Four-lane divided | Single | PDO | -7.217 | 0.776 | 1.272 | 1.132 |
| Urban/suburban | Four-lane divided | Single | KABC | -12.905 | 1.143 | 0.862 | 0.244 |

[^1]TABLE B. 5
Indiana Crash Type Percentages for Rural Two-Lane Undivided Segments

| Crash types | Fatal and injury | PDO | Total |
| :---: | :---: | :---: | :---: |
| Single vehicle |  |  |  |
| Collision with animal | 4.81 | 45.77 | 38.48 |
| Collision with bicycle | 0.48 | 0.02 | 0.10 |
| Collision with pedestrian | 0.90 | 0.05 | 0.20 |
| Overturned | 7.08 | 2.50 | 3.32 |
| Ran off road | 44.48 | 21.16 | 25.31 |
| Other single-vehicle crash | 1.32 | 4.84 | 4.21 |
| Multiple vehicle |  |  |  |
| Angle collision | 6.02 | 2.32 | 2.98 |
| Head-on collision | 8.45 | 0.81 | 2.17 |
| Rear-end collision | 14.47 | 9.08 | 10.04 |
| Sideswipe collision | 7.45 | 5.13 | 5.55 |
| Other multi-vehicle collision | 4.54 | 8.31 | 7.64 |

Note: Related crash percentage for rural multilane divided segments: $100.00 \%$

TABLE B. 6
Indiana Crash Type Percentages by Severity Level for Rural Multilane Divided Segments

| Collision type | Total | Fatal and injury | Fatal and injury* | PDO |
| :--- | ---: | ---: | ---: | ---: |
| Head-on | 0.675 | 1.553 | 1.474 |  |
| Sideswipe | 7.234 | 6.019 | 6.105 |  |
| Rear-end | 17.841 | 29.126 | 28.421 | 1.524 |
| Angle | 4.760 | 10.680 | 10.526 | 5.142 |
| Single | 64.580 | 49.515 | 3.344 |  |
| Other | 4.910 | 3.107 | 3.158 | 5.384 |

*Using the KABCO scale, these include only KAB crashes. Crashes with severity level C (possible injury) are not included.

TABLE B. 7
Indiana Crash Type Percentages by Severity Level for Multiple-Vehicle Non-Driveway Crashes on Urban/Suburban Arterial Segments

| Facility type | Severity | Rear-end | Head-on | Angle | Sideswipe same <br> direction | Sideswipe opposite <br> direction |
| :--- | :--- | :--- | :---: | ---: | ---: | ---: |
| Two-lane undivided <br> arterials (2U) | KABC | PDO | 51.00 | 13.00 | 17.00 | 3.00 |
| Other |  |  |  |  |  |  |

## APPENDIX C. IMPLEMETING THE CALIBRATED INDIANA PARAMETERS IN THE IHSDM

The SPFs, CMFs, and crash proportions included in the HSM predictive method have been calibrated for Indiana conditions. These components may be incorporated in the IHSDM using the Administration Tool, shown in Figure C.1. The crash proportions are implemented under the "Crash Distribution Data Sets" module, while the SPF and CMF parameters are implemented under the "Model Data Sets" module.

This appendix illustrates how the Indiana-specific parameters may be implemented in the IHSDM Administration Tool and how this configuration is selected for use in the IHSDM crash prediction tool. The step-by-step procedures are detailed here for two cases. The first case involves transferring the prepared files containing the Indiana configuration to the Administration Tool interface. This case is applicable if the Administration Tool is in the default configuration (in other words, the HSM default is the only configuration available in the tool). In the second case, the user inputs the Indiana-specific parameters directly into the Administration Tool. This case is applicable if the Administration Tool is not in the default configuration (there are user-specified custom configurations already entered in the tool in addition to the HSM default).

## Case 1—Transferring the Indiana Configuration Files to the Administration Tool

Step 1: Locate and copy the files with the Indiana configuration. Two files that contain the Indiana configuration have been prepared, one that includes the updated crash proportions and the other which has the
parameters of the SPFs and CMFs. These files are named "config.cd.cpm.local_1" and "config.md.cpm. local_1," respectively, as shown in Figure C.2. They are available as supplements to this report and can be downloaded at https://doi.org/10.5703/1288284316646.

Step 2: Navigate to the IHSDM configuration folder. As displayed in Figure C.3, in this case, the folder is located in the C : drive under the following path: $\mathrm{C}:>$ IHSDM2017 $>$ config

Step 3: Paste the files with the Indiana configuration in the IHSDM configuration folder. This step is shown in Figure C.4. The configuration folder may then be closed.

Step 4: Open the IHSDM Administration Tool from the Start menu (Figure C.5). The software should open with both the default HSM configuration and Indiana configuration appearing under the "Crash Distribution Data Sets" and "Model Data Sets" (Figure C.6).

Step 5: Save backup copies of the Indiana configuration files. In order for the Indiana configuration to work properly and be compatible with any other custom configurations that the user may decide to add later, backup copies of the Indiana configuration files should be saved. Under the "Crash Distribution Data Sets" module, select the Indiana configuration and click the "Edit" button as displayed in Figure C.7.

The following dialogue box appears (Figure C.8). No changes need to be made in this box, as the appropriate Indiana crash proportions have already been entered. Simply click "Ok."

Even though no changes were made in the configuration, a backup configuration file was automatically created,


Figure C. 1 IHSDM Administration Tool.


Figure C. 2 Files with calibrated, Indiana-specific parameters.


Figure C. 3 IHSDM configuration folder.


Figure C. 4 Indiana configuration files in the IHSDM configuration folder.


Figure C. 5 Opening the IHSDM Administration Tool.


Figure C. 6 IHSDM Administration Tool with HSM and Indiana configurations.


Figure C. 7 Saving backup copy of the Indiana configuration for "Crash Distribution Data Sets."


Figure C. 8 Dialogue box for "Crash Distribution Data Sets" module.
in this case under the file path "C: $>$ IHSDM2017 $>$ users $>$ ihsdm_admin $>$ backup." The same procedure is followed for the Indiana configuration file containing the SPF and CMF parameters (located in the "Model Data Sets" module). Figure C. 9 shows what the Administration Tool should look like when finished.

## Case 2-Inputting the Indiana-specific Parameters Directly into the Administration Tool

In this case, the user may have their own previouslycreated custom configuration already entered in the Administration Tool in addition to the HSM configuration. The Indiana crash proportions and SPF and CMF parameters may be entered by the user into the IHSDM Administration Tool by creating a new custom configuration for Indiana.

Step 1: Open the IHSDM Administration Tool from the Start menu (Figure C.10). As shown in Figure C.11, the software should open with the HSM configuration and previously-saved custom configuration appearing under the "Crash Distribution Data Sets" and "Model Data Sets."

Step 2: Create the Indiana configuration under the "Crash Distribution Data Sets" module. This is most easily done by creating a copy of the HSM configuration and updating the crash proportions in this copy. Select the HSM configuration and click the "Copy" button (Figure C.12).

The dialogue box displayed in Figure C. 13 appears. For the "Title", the user may enter "Indiana Configuration" (or another name of personal preference). Similarly, under "Comment", the user may enter "Indiana Crash Distribution."

Step 3: Input the Indiana crash proportions into the tool. Under the dropdown "Data Set Attributes" on the left side of the screen, the "Rural Two-Lane Crash Distribution Data" is opened. The general crash distributions to be entered for segments may be found in Table B.4. This data is typed by the user into the appropriate boxes shown in Figure C. 14 below.

The crash type proportions to be entered for rural two-lane undivided segments may be found in Table B.5. This data is input by the user into the appropriate boxes displayed in Figure C.15.

A similar procedure is followed for rural multilane divided segments and urban/suburban arterial segments using data from Table B. 6 and Table B.7, respectively. Once the user has entered all of the crash proportions, click "Ok" to save the changes and return to the Administration Tool.

Step 4: Create the Indiana configuration under the "Model Data Sets" module. Again, this is most easily done be creating a copy of the HSM configuration and updating the SPF and CMF parameters in this copy. Once this has been done, the dialogue box in Figure C. 16 appears.


Model Data Sets

| Title | Comment | Last Update | Edit... |
| :--- | :---: | :---: | :--- |
| HSM Configuration | Default model c... | Oct 19, 2016 1:34:47 PM | \| |
| Indiana Configuration | Indiana SPFs | Oct 8,2017 2:58:41 PM | Delete... |
|  |  |  |  |

Economic Analysis Model Data Sets

| Title | Comment | Last Update |  | Edit |
| :---: | :---: | ---: | ---: | ---: |
| Economic Analv... Default Econom.... | Oct 5.2017 1:2... |  |  |  |


| Available Policies |  |  |
| :---: | :---: | :---: |
| Policy Title | Unit System | Last |
| AASHTO 1990 | U.S. Customary | Feb 1, |
| AASHTO 1994 | Metric | Feb 1, |
| AASHTO 2001 | U.S. Customary | Feb 1, |
| AASHTO 2001 ... | Metric | Feb 1, |
| AASHTO 2004 ... | U.S. Customary | Feb 1, |
| AASHTO 2004 | Metric | Feb 1, |
| AASHTO 2011 ... | Metric | Jan 6, |
| AASHTO 2011 | U.S. Customary | Jan 6, |

-Traffic Analysis Configuration Data Se

| Title | Comment | Las |
| :--- | :---: | ---: |
| Default | Default TAM con... | Oct 18 |

Driver/Vehicle Configuration Data Set:

| Title | Comment | Las |
| :--- | ---: | ---: |
| Deterministic A... | System default | Oct 18 |
| Deterministic | System default | Oct 19 |
| Deterministic A... | System default | Oct 18 |
| Deterministic A... | System default | Oct 18 |

Figure C. 9 IHSDM Administration Tool after saving backup files.


Figure C. 10 Opening the IHSDM Administration Tool.


Figure C. 11 IHSDM Administration Tool with HSM and custom configurations.


Figure C. 12 Creating a copy of the HSM configuration for "Crash Distribution Data Sets."


Figure C. 13 Dialogue box for "Crash Distribution Data Sets" module.


Figure C. 14 Indiana general crash distributions for rural two-lane undivided segments.

Step 5: Input the Indiana SPF and CMF parameters into the tool. The "Rural Two-Lane Model Data" is opened under the "Data Set Attributes" from the dropdown menu. The SPF parameters to be entered for rural two-lane undivided segments (as well as rural multilane divided and urban/suburban arterial segments) are found in Table B.3. The parameters for rural two-lane undivided segments are input by the user into the boxes shown in Figure C.17.

The CMF parameters to be entered for lane width and shoulder width on rural two-lane undivided segments (as well as for lane width on rural multilane
divided segments) are found in Table B.1. Figure C. 18 and Figure C. 19 display the boxes where the user may input the Indiana CMF parameters for lane width and shoulder width, respectively, on rural two-lane undivided segments.

Utilizing the data from Appendix B, a similar procedure is followed for inputting the available SPF and CMF parameters for rural multilane divided segments and urban/suburban arterial segments. Once the user is finished, click "Ok" to save the changes and return to the Administration Tool. It should now look as shown in Figure C. 20 .

| - Data Set Attributes <br> 曰 Rural Two-Lane Crash Distribution Data <br> General Segment Crash Distributions <br> Segment Collision Type Distributions <br> General Intersection Crash Distributions Intersection Collision Type Distributions <br> (T Rural Multi-Lane Crash Distribution Data <br> 田 Urban/Suburban Arterial Crash Distribution Data <br> (Treeway Crash Distribution Data | Segment Collision Type Distributions |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | This table represents data from HSM Ch. 10, Table 10-4; and the Crash Prediction on Rural Two-Lane Highways Engineer's Manual Table 7. |  |  |  |  |
|  | Segment Type | Collision Type | Model Class | Distribution (\%) | Edit. |
|  | Two-Lane Undivided | Collision with Animal | Total | 38.479 | Help. |
|  | Two-Lane Undivided | Collision with Animal | Fatal and Injury | 4.807 |  |
|  | Two-Lane Undivided | Collision with Animal | Property Dama... | 45.769 |  |
|  | Two-Lane Undivided | Collision with Bicycle | Total | 0.103 |  |
|  | Two-Lane Undivided | Collision with Bicycle | Fatal and Injury | 0.475 |  |
|  | Two-Lane Undivided | Collision with Bicycle | Property Dama... | 0.023 |  |
|  | Two-Lane Undivided | Collision with Pedestrian | Total | 0.197 |  |
|  | Two-Lane Undivided | Collision with Pedestrian | Fatal and Injury | 0.898 |  |
|  | Two-Lane Undivided | Collision with Pedestrian | Property Dama... | 0.046 |  |
|  | Two-Lane Undivided | Overturned | Total | 3.319 |  |
|  | Two-Lane Undivided | Overturned | Fatal and Injury | 7.079 |  |
|  | Two-Lane Undivided | Overturned | Property Dama... | 2.505 |  |
|  | Two-Lane Undivided | Run Off Road | Total | 25.308 |  |
|  | Two-Lane Undivided | Run Off Road | Fatal and Injury | 44.480 |  |
|  | Two-Lane Undivided | Run Off Road | Property Dama... | 21.157 |  |
|  | Two-Lane Undivided | Other Single-vehicle Collision | Total | 4.211 |  |
|  | Two-Lane Undivided | Other Single-vehicle Collision | Fatal and Injury | 1.321 |  |
|  | Two-Lane Undivided | Other Single-vehicle Collision | Property Dama... | 4.838 |  |
|  | Two-Lane Undivided | Angle Collision | Total | 2.980 |  |
|  | Two-Lane Undivided | Angle Collision | Fatal and Injury | 6.022 |  |
|  | Two-Lane Undivided | Angle Collision | Property Dama... | 2.322 |  |
|  | Two-Lane Undivided | Head-on Collision | Total | 2.172 |  |
|  | Two-Lane Undivided | Head-on Collision | Fatal and Injury | 8.452 |  |
|  | Two-Lane Undivided | Head-on Collision | Property Dama... | 0.812 |  |
|  | Two-Lane Undivided | Rear-end Collision | Total | 10.040 |  |
|  | Two-Lane Undivided | Rear-end Collision | Fatal and Injury | 14.474 |  |
|  | Two-Lane Undivided | Rear-end Collision | Property Dama... | 9.081 |  |
|  | Two-Lane Undivided | Sideswipe | Total | 5.547 |  |
|  | Two-Lane Undivided | Sideswipe | Fatal and Injury | 7.448 |  |
|  | Two-Lane Undivided | Sideswipe | Property Dama... | 5.135 |  |
|  | Two-Lane Undivided | Other Multiple-vehicle Collision | Total | 7.643 |  |
|  | Two-Lane Undivided | Other Multiple-vehicle Collision | Fatal and Injury | 4.543 |  |
|  | Two-Lane Undivided | Other Multiple-vehicle Collision | Property Dama... | 8.314 |  |

Figure C. 15 Indiana crash type proportions for rural two-lane undivided segments.


Figure C. 16 Dialogue box for "Model Data Sets" module.


Figure C. 17 Indiana SPF parameters for rural two-lane undivided segments.


Figure C. 18 Indiana CMF parameters for lane width on rural two-lane undivided segments.

## Selecting the Indiana Configuration for Use in the IHSDM Crash Prediction Tool

The final part of this appendix shows how the Indiana configuration is utilized for crash prediction in the IHSDM. It is assumed that the user has knowledge of the crash prediction tool, the IHSDM-HSM Predictive Method, and has created or input a rural or urban/ suburban arterial segments and initiated a crash prediction evaluation. Under the "Set crash prediction attributes"
dialogue box, the user is prompted to select the desired "Crash Distribution" and "Model/CMF" configurations. As seen in Figure C.21, the Indiana configuration is selected.

After the user has progressed through the setup for the crash prediction evaluation, the evaluation summary (Figure C.22) appears. The "Crash Distribution Configuration" and "Model/CMF Configuration" provide confirmation that the Indiana configuration has been selected.


Figure C. 19 Indiana CMF parameters for shoulder width on rural two-lane undivided segments.


Figure C. 20 IHSDM Administration Tool after creating Indiana configuration.


Figure C. 21 Selecting the Indiana configuration in a crash prediction evaluation.


Figure C. 22 Crash prediction evaluation summary.

## About the Joint Transportation Research Program (JTRP)

On March 11, 1937, the Indiana Legislature passed an act which authorized the Indiana State Highway Commission to cooperate with and assist Purdue University in developing the best methods of improving and maintaining the highways of the state and the respective counties thereof. That collaborative effort was called the Joint Highway Research Project (JHRP). In 1997 the collaborative venture was renamed as the Joint Transportation Research Program (JTRP) to reflect the state and national efforts to integrate the management and operation of various transportation modes.

The first studies of JHRP were concerned with Test Road No. 1—evaluation of the weathering characteristics of stabilized materials. After World War II, the JHRP program grew substantially and was regularly producing technical reports. Over 1,600 technical reports are now available, published as part of the JHRP and subsequently JTRP collaborative venture between Purdue University and what is now the Indiana Department of Transportation.

Free online access to all reports is provided through a unique collaboration between JTRP and Purdue Libraries. These are available at: http://docs.lib.purdue.edu/jtrp

Further information about JTRP and its current research program is available at: http://www.purdue.edu/jtrp

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[^0]:    countermeasure. The user is referred to the source (provided by the reference number) for the original functional form.

[^1]:    *Check Section 5.1.2 for explanation

