## Statistical M odels of At-Grade

 Intersection Accidents—Addendum
## FOREWORD

This report is an addendum to the published Report, FHWA-RD-96-125, titled Statistical Models of At-Grade Intersection Accidents. The objective of both reports is to develop accident prediction models relating total intersection accidents to highway design elements. The design elements considered include functional class, traffic flow, channelization, traffic control type, median, access control, terrain type, number of lanes, lane width, shoulder width, and lighting. While the previously published report is only for multi-vehicle accidents, this report includes all collision types (single and multi-vehicle). The result is a preliminary effort in the development of the Interactive Highway Safety Design Model (IHSDM), which is a Federal Highway Administration (FHWA) objective to develop a highway safety evaluation tool.

Based on retrospective analysis, several statistical modeling techniques were tried. Besides using innovative statistical techniques (e.g., Poisson and negative binomial regression models), five preliminary accident models were developed for at-grade intersections: (1) Rural, four-leg, STOP-controlled; (2) Rural, three-leg, STOP-controlled; (3) Urban, fourleg, STOP-controlled; (4) Urban, three-leg, STOP-controlled; and (5) Urban, four-leg, signalized.

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Research and Development

Technical Report Documentation Page

15. Supplementary Notes

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16. Abstract

This report is an addendum to the work published in FHWA-RD-96-125 titled "Statistical Models of At-Grade Intersection Accidents." The objective of both research studies was to develop statistical models of the relationship between traffic accidents and highway geometric elements for at-grade intersections. While the previously published report used only multiple-vehicle accidents in developing predictive models, this addendum presents models based on all collision types (including both multiple-vehicle and single-vehicle accidents).

The statistical modeling approaches used in the research included lognormal, Poisson, and negative binomial regression analyses. The models for all collision types are similar to those developed in the previous report for multiplevehicle accidents. The regression models of the relationships between accidents and intersection geometric design, traffic control, and traffic volume variables were found to explain between 16 and 39 percent of the variability in the accident data. However, most of that variability was explained by the traffic volume variables considered (major road and crossroad ADTs). Geometric design variables accounted for only a small additional portion of the variability.

Generally, negative binomial regression models were developed to fit the accident data at rural, three- and four-leg, STOP-controlled intersections and urban, three-leg, STOP-controlled intersections. On the other hand, lognormal regression models were found more appropriate for modeling accidents at urban, four-leg, STOP-controlled and urban, four-leg, signalized intersections. The decision to use negative binomial or lognormal regression analysis was based on evaluation of the accident frequency distribution for the specific categories of intersections.

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## 1. INTRODUCTION

This technical report presents the results of statistical analyses of accident experience for atgrade intersections. This report is an addendum to the previously published FHWA Report No. FHWA-RD-96-125 titled "Statistical Models of At-Grade Intersection Accidents." ${ }^{(1)}$ In that study, only multiple-vehicle accidents were modeled. The analyses reported here include all collision types (i.e., both multiple- and single-vehicle accidents) using 3-year accident frequencies (1990 to 1992) and geometric design, traffic control, and traffic volume data from a database provided by the California Department of Transportation (Caltrans). The data used for the analyses reported in this addendum are in all respects identical to those used for Report No. FHWA-RD-96-125, except that all collision types were included in the accident frequencies used as the dependent variable in modeling.

This report is organized similarly to Section 5 of the previous report. To minimize repetition between the two reports, the general discussion of the statistical methods has been abbreviated here (the reader is referred to the previous report for details). ${ }^{(1)}$ Statistical modeling results for five specific types of intersections are discussed in this report:

- Rural, four-leg, STOP-controlled intersections
- Rural, three-leg, STOP-controlled intersections
- Urban, four-leg, STOP-controlled intersections
- Urban, three-leg, STOP-controlled intersections
- Urban, four-leg, signalized intersections

Section 2 of this report provides detailed accident frequency distributions for the five types of intersections. Section 3 presents the results from various statistical models that were developed with negative binomial and lognormal regressions. Section 4 presents the conclusions of the study. Detailed data on accident type and severity distribution are presented in an appendix.
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## 2. ACCIDENT FREQUENCY DISTRIBUTIONS

This section of the report summarizes the accident statistics for all collision types for the intersections that were used in developing the models presented in this report. The purpose of these frequency distributions is to illustrate the reasons for selecting the statistical modeling approach used for each of the five intersection types. More detailed distributions that show the accident data broken down by accident type and accident severity are presented in the appendix.

Prior to beginning the statistical modeling activities, the general shape of each accident frequency distribution was assessed for each of the five intersection types of interest. This was done visually by plotting the data for the 3-year totals and by calculating basic statistics. For each of the five intersection categories, Table 1 shows yearly and 3-year total accident statistics (minimum, median, mean, maximum) for total accidents. Total accident counts, as well as fatal and injury accident counts, are shown separately. Table 1 also shows the total number of accidents of each type in each given year. For each type of intersection, 3 -year totals are also shown for multiple-vehicle accidents only. The percentages of total accidents that were multiple-vehicle and single-vehicle accidents were computed for all five intersection categories for total accidents. Generally, multiple-vehicle accidents represent a large proportion of all accidents, except for those occurring at rural, three-leg, STOPcontrolled intersections.

Next, the frequency data are plotted separately for each type of accident and each type of intersection in Figures 1 through 5. The plots shown in Figures 1 through 5 highlight the different shapes of accident frequencies. With large numbers of intersections with no or low accident experience, the distribution tends to follow the shape of a Poisson distribution. This observation clearly applies to rural, four- and three-leg, STOP-controlled intersections and to urban, three-leg, STOP-controlled intersections. When the number of intersections with no or low accident experience is relatively small, the distribution tends to follow the shape of a lognormal distribution. This is clearly seen in the case of urban, four-leg, signalized intersections and also in the case of urban, four-leg, STOP-controlled intersections.
Table 1. Annual Accident Statistics, All Collision Types, 1990-1992

| Year | Total accidents |  |  |  |  | Fatal and injury accidents |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Minimum | Median | Mean | Maximum | Total | Minimum | Median | Mean | Maximum | Total |
| Rural, Four-Leg, STOP-Controlled-1,434 Intersections |  |  |  |  |  |  |  |  |  |  |
| 1990 | 0 | 1 | 1.39 | 15 | 1,996 | 0 | 0 | 0.68 | 9 | 980 |
| 1991 | 0 | 1 | 1.26 | 16 | 1,802 | 0 | 0 | 0.61 | 10 | 880 |
| 1992 | 0 | 1 | 1.28 | 19 | 1,833 | 0 | 0 | 0.63 | 8 | 899 |
| 1990-92 | 0 | 2 | 3.93 | 49 | 5,631 | 0 | 1 | 1.92 | 27 | 2,759 |
| (86 percent multiple-vehicle accidents, 14 percent single-vehicle accidents) |  |  |  |  |  |  |  |  |  |  |
| Rural, Three-Leg, STOP-Controlled-2,692 Intersections |  |  |  |  |  |  |  |  |  |  |
| 1990 | 0 | 0 | 0.84 | 21 | 2,250 | 0 | 0 | 0.38 | 12 | 1,028 |
| 1991 | 0 | 0 | 0.76 | 15 | 2,053 | 0 | 0 | 0.34 | 8 | 928 |
| 1992 | 0 | 0 | 0.78 | 26 | 2,096 | 0 | 0 | 0.35 | 11 | 949 |
| 1990-92 | 0 | 1 | 2.38 | 59 | 6,399 | 0 | 0 | 1.08 | 25 | 2,905 |
| (76 percent multiple-vehicle accidents, 24 percent single-vehicle accidents) |  |  |  |  |  |  |  |  |  |  |
| Urban, Four-Leg, STOP-Controlled-1,342 Intersections |  |  |  |  |  |  |  |  |  |  |
| 1990 | 0 | 2 | 2.71 | 26 | 3,641 | 0 | 1 | 1.13 | 12 | 1,521 |
| 1991 | 0 | 2 | 2.35 | 19 | 3,158 | 0 | 1 | 1.07 | 9 | 1,434 |
| 1992 | 0 | 2 | 2.38 | 21 | 3,190 | 0 | 1 | 1.07 | 12 | 1,440 |
| 1990-92 | 0 | 5 | 7.44 | 57 | 9,989 | 0 | 2 | 3.27 | 24 | 4,395 |
| (88 percent multiple-vehicle accidents, 12 percent single-vehicle accidents) |  |  |  |  |  |  |  |  |  |  |
| Urban, Three-Leg, STOP-Controlled-3,057 Intersections |  |  |  |  |  |  |  |  |  |  |
| 1990 | 0 | 1 | 1.62 | 33 | 4,939 | 0 | 0 | 0.65 | 12 | 1,984 |
| 1991 | 0 | 1 | 1.50 | 31 | 4,571 | 0 | 0 | 0.64 | 10 | 1,951 |
| 1992 | 0 | 1 | 1.43 | 31 | 4,359 | 0 | 0 | 0.61 | 18 | 1,867 |
| 1990-92 | 0 | 3 | 4.54 | 81 | 13,869 | 0 | 1 | 1.90 | 28 | 5,802 |
| (86 percent multiple-vehicle accidents, 14 percent single-vehicle accidents) |  |  |  |  |  |  |  |  |  |  |

Table 1 (Continued)

| Year | Total accidents |  |  |  |  | Fatal and injury accidents |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Minimum | Median | Mean | Maximum | Total | Minimum | Median | Mean | Maximum | Total |
| Urban, Four-Leg, Signalized-1,306 Intersections |  |  |  |  |  |  |  |  |  |  |
| 1990 | 0 | 7 | 8.49 | 49 | 11,087 | 0 | 3 | 3.32 | 23 | 4,330 |
| 1991 | 0 | 6 | 7.77 | 54 | 10,152 | 0 | 3 | 3.19 | 20 | 4,167 |
| 1992 | 0 | 6 | 7.17 | 58 | 9,364 | 0 | 2 | 3.06 | 20 | 4,002 |
| 1990-92 | 0 | 19 | 23.43 | 151 | 30,603 | 0 | 8 | 9.57 | 51 | 12,499 |




Figure 1. Accident Frequency Distributions at Rural, Four-Leg, STOP-Controlled Intersections



Figure 2. Accident Frequency Distributions at Rural, Three-Leg, STOP-Controlled Intersections



Figure 3. Accident Frequency Distributions at Urban, Four-Leg, STOP-Controlled Intersections


Fatal and Injury Accidents
at urban three-leg STOP-controlled intersections


Figure 4. Accident Frequency Distributions at Urban, Three-Leg, STOP-Controlled Intersections



Figure 5. Accident Frequency Distributions at Urban, Four-Leg, Signalized Intersections

## 3. STATISTICAL MODELING

## Lognormal and Loglinear Regression Models

Several candidate analysis methods were investigated for application to the accident frequencies in the five types of at-grade intersections in this study. The analysis approach was driven by both the actual distribution of accident frequencies and by recommendations and practices in the field of accident data analysis. The frequency distributions of total fatal and injury accidents in the 3-year study period are shown in Figures 1 through 5 above. The percentages of intersections with zero or one accident in the 3-year period are:

|  | Percent of intersections <br> with 0 or 1 total accident <br> in 3-year period | Percent of intersections <br> with 0 or 1 fatal and <br> injury accident in <br> 3-year period |
| :--- | :---: | :---: | :---: |
| Intersection type | 37.9 | 59.3 |
| Rural, four-leg, STOP-controlled | 55.2 | 75.6 |
| Rural, three-leg, STOP-controlled | 17.9 | 38.2 |
| Urban, four-leg, STOP-controlled | 33.5 | 58.1 |
| Urban, three-leg, STOP-controlled | 2.8 | 8.2 |

For most types of intersections, a large proportion of the intersections experienced at most one accident over the three-year period. This observation is not true for urban, four-leg, signalized intersections, where about 50 percent of the intersections experienced 19 or more total accidents over the 3 -year period, and only 10 percent of the intersections had 5 or fewer accidents. Also, the pattern for urban, four-leg, STOP-controlled intersections differs somewhat from the two extreme situations in that only eight percent of the intersections experienced no accidents and about half of the intersections experienced at least four accidents in the three-year period. These same patterns also apply to fatal and injury accidents.

As was done in the previous study, two general types of statistical models were applied to the accident data in this study: (1) a lognormal regression model for all urban, four-leg intersections (both STOP-controlled and signalized); and (2) a loglinear regression model-a Poisson regression followed by a negative binomial regression model-for all rural STOP-controlled (three- and four-leg) and urban, three-leg, STOP-controlled intersections. These models are briefly described next.

Consider a set of n intersections of a given class (e.g., rural, four-leg, STOP-controlled intersections). Associated with each intersection i is a set of q parameters ( $\mathrm{X}_{\mathrm{i} 1}, \mathrm{X}_{\mathrm{i} 2}, \ldots, \mathrm{X}_{\mathrm{iq}}$ ) describing the geometric design, traffic control, traffic volume, and other related
characteristics of that intersection. Let the number of accidents occurring at the ith intersection during a 3 -year period be denoted by $Y_{i}$, where $i=1, \ldots, n$. Next, denote by $y_{i}$ the actual observation of $Y_{i}$ during the 3-year period, that is, $y_{i}=0,1,2, \ldots$ and $i=1, \ldots, n$.

The objective of a statistical model is to provide a relationship between a function of the expected number of accidents, $\mathrm{E}\left(\mathrm{Y}_{\mathrm{i}}\right)=\mu_{\mathrm{i}}$, at the ith intersection and the q intersection parameters, $\mathrm{X}_{\mathrm{i}}, \mathrm{X}_{\mathrm{i} 2}, \ldots, \mathrm{X}_{\mathrm{iq}}$. This relationship can be formulated through a general linear model of the form:

$$
\begin{equation*}
\operatorname{Function}\left(\mu_{\mathrm{i}}\right)=\beta_{0}+\beta_{1} X_{\mathrm{i} 1}+\ldots+\beta_{\mathrm{q}} \mathrm{X}_{\mathrm{iq}} \tag{1}
\end{equation*}
$$

where the regression coefficients, $\beta_{0}, \beta_{1}, \beta_{2}, \ldots \beta_{\mathrm{q}}$, are to be estimated from the data. The estimation procedure used to obtain the regression coefficients is dependent on the assumption made about the distribution of the $\mathrm{Y}_{\mathrm{i}}$.

Note: Throughout this report, all logarithms are natural logarithms and are denoted by $\log$ in all equations.

## Lognormal Regression Models

Lognormal regression models are based on the assumption that the natural logarithm of $Y_{i}$ follows a normal distribution with mean $\mu_{\mathrm{i}}$ and variance $\sigma^{2}$. In other words, it is assumed that $\mathrm{Y}_{\mathrm{i}}$ follows a lognormal distribution, a reasonable choice whenever the data are inherently non-negative, suggesting that a model with positive skewness is needed and the mean is relatively large. This model also ensures that $\mu_{\mathrm{i}}$, the expected number of accidents, remains positive.

In this case, the relationship between the expected number of accidents at the ith intersection and the q predictor variables, $\mathrm{X}_{1}, \ldots, \mathrm{X}_{\mathrm{q}}$, can be written as:

$$
\begin{equation*}
\log \left(\mu_{\mathrm{i}}\right)=\beta_{0}+\beta_{1} X_{\mathrm{i} 1}+\beta_{2} \mathrm{X}_{\mathrm{i} 2}+\ldots+\beta_{\mathrm{q}} X_{\mathrm{iq}} \tag{2}
\end{equation*}
$$

or alternatively, in the multiplicative form, as

$$
\begin{equation*}
\mu_{\mathrm{i}}=\exp \left(\beta_{0}\right) \exp \left(\beta_{1} X_{\mathrm{i} 1}\right) \exp \left(\beta_{2} \mathrm{X}_{\mathrm{i} 2}\right) \ldots \exp \left(\beta_{\mathrm{q}} \mathrm{X}_{\mathrm{iq}}\right) \tag{3}
\end{equation*}
$$

where the $\log$ (number of accidents) is assumed to follow a normal distribution with mean $\mu_{\mathrm{i}}$ and variance $\sigma^{2}$. The coefficients, $\beta_{0}, \beta_{1}, \beta_{2}, \ldots \beta_{q}$, are the linear regression coefficients to be estimated by the ordinary least-squares method.

## Loglinear Regression Models

As was done in the previous study, two loglinear models were considered for application to at-grade accident frequencies: the Poisson and the negative binomial models. Their general forms are described below.

Poisson Model. When the average number of accidents at an intersection becomes small, the assumption of a lognormal distribution is no longer valid. The Poisson model then becomes a natural choice as it models the occurrence of rare discrete events well. The relationship between the expected number of accidents occurring at the ith intersection and the q intersection parameters, $\mathrm{X}_{\mathrm{i} 1}, \mathrm{X}_{\mathrm{i} 2}, \ldots, \mathrm{X}_{\mathrm{iq}}$, is assumed to be of the same form as shown in Equation (2):

$$
\begin{equation*}
\log \left(\mu_{\mathrm{i}}\right)=\beta_{0}+\beta_{1} X_{\mathrm{i} 1}+\beta_{2} X_{\mathrm{i} 2}+\ldots+\beta_{\mathrm{q}} X_{\mathrm{iq}} \tag{4}
\end{equation*}
$$

However, the assumption is now made that the number of accidents, $\mathrm{Y}_{\mathrm{i}}$, follows a Poisson distribution with mean $\mu_{\mathrm{i}}$.

Negative Binomial Model. A limitation of the Poisson distribution is that the mean equals the variance of the distribution. Previous work in the field of accident research has shown that this is not always the case. Suppose a Poisson model is used for modeling accidents and the variance, or dispersion, of the data exceeds the estimated mean of the accident data distribution. The data are then said to be overdispersed, and the underlying assumption of the variance being equal to the mean for the Poisson distribution is violated. The negative binomial, which is a discrete distribution, provides an alternative model to deal with overdispersion in count data such as accident frequencies.

As for the Poisson model above, the relationship between the expected number of accidents occurring at the ith intersection and the q intersection parameters, $\mathrm{X}_{\mathrm{i}}, \mathrm{X}_{\mathrm{i} 2}, \ldots, \mathrm{X}_{\mathrm{iq}}$, is still taken to be:

$$
\begin{equation*}
\log \left(\mu_{\mathrm{i}}\right)=\beta_{0}+\beta_{1} \mathrm{X}_{\mathrm{i} 1}+\beta_{2} \mathrm{X}_{\mathrm{i} 2}+\ldots+\beta_{\mathrm{q}} \mathrm{X}_{\mathrm{iq}} \tag{5}
\end{equation*}
$$

However, the assumption is now made that the number of accidents, $\mathrm{Y}_{\mathrm{i}}$, follows a negative binomial distribution with parameters $\alpha$ and k (with $0 \leq \alpha \leq 1$ and $\mathrm{k} \geq 0$ ).

For both the Poisson and negative binomial models, the regression coefficients, $\beta_{0}, \beta_{1}$, $\beta_{2}, \ldots \beta_{q}$, are estimated by the method of maximum likelihood. The statistical analysis system (SAS) provides a procedure, PROC GENMOD (a generalized linear model procedure), that can be used to estimate the regression coefficients of Equations (4) and (5) by specifying the appropriate type of distribution.

## Treatment of ADT Variables in Regression Models

In all models in this study, the natural logarithm of the major-road and crossroad average daily traffic (ADT) variables was used. This parallels the approach taken by other researchers where accident counts rather than accident rates are modeled. On the log-scale, the ratio of accident counts over ADT becomes the difference between $\log$ (accident counts) and $\log (A D T)$. The difference here is that it is assumed that the coefficient of $\log (A D T)$ is not equal to one, but rather is a coefficient to be estimated through analysis. Thus, in the lognormal and Poisson and negative binomial models described above, $\mathrm{X}_{1}$ and $\mathrm{X}_{2}$ generally represent $\log \left(\mathrm{ADT}_{\text {major road }}\right)$ and $\log \left(\mathrm{ADT}_{\text {crossroad }}\right)$, respectively. The multiplicative model relating the expected accident counts and independent variables can thus be rewritten as:

$$
\begin{equation*}
\mu_{\mathrm{i}}=\exp \left(\beta_{0}\right)\left(\mathrm{ADT}_{\text {major road }}\right)^{\beta 1}\left(\mathrm{ADT}_{\text {crossroad }}\right)^{\beta 2} \exp \left(\beta_{3} \mathrm{X}_{\mathrm{i} 3}\right) \cdot \ldots \cdot \exp \left(\beta_{\mathrm{q}} \mathrm{X}_{\mathrm{iq}}\right) \tag{6}
\end{equation*}
$$

Note: For further details, the reader is referred to Section 5 of the previous report, which also contains a list of statistical references. ${ }^{(1)}$

## Accident Modeling Results

The following sections present the modeling results separately for each of the five selected types of intersections:

- Rural, four-leg, STOP-controlled
- Rural, three-leg, STOP-controlled
- Urban, four-leg, STOP-controlled
- Urban, three-leg, STOP-controlled
- Urban, four-leg, signalized


## Rural, Four-Leg, STOP-Controlled Intersections

The first step in the analysis of rural, four-leg, STOP-controlled intersections was to select candidate independent variables for that particular group of intersections. Both engineering judgment and sample size requirements for the levels of each candidate variable were involved in the decision as to whether a particular variable was included in the modeling effort. A small number of independent categorical variables were not included in the full model because either all or nearly all intersections fell into one level of that variable. The variables originally considered that were not included for these reasons were:

- Major-road left-turn prohibition (all intersections had permitted left turns)
- Crossroad left-turn channelization (none of the intersections had left-turn lanes)
- Crossroad left-turn prohibition (none of the intersections had left turns prohibited)
- Number of lanes on the crossroad (99.8 percent had two lanes)

Table 2 identifies the variables that were selected for modeling of rural, four-leg, STOP-controlled intersections. This table also provides descriptive statistics for three types of variables: (1) total and fatal and injury accident frequencies in the 3-year study period (i.e., the dependent variables for the modeling effort); (2) all independent continuous variables considered; and (3) all independent categorical variables considered. Minimum, mean, median, and maximum values are given for the first two types of variables. For categorical variables, the percent of intersections within each level is given.

Next, using all the continuous and categorical variables shown in Table 2, a negative binomial regression model was fitted separately to the data for total and fatal and injury accidents. The analyses were performed using the SAS GENMOD procedure with the negative binomial distribution and the appropriate deviance functions and variance adjustment factor, $\mathrm{k} .{ }^{(1,2,3)}$ The significance of each regression coefficient was examined. If a coefficient was not significant at the 10 percent level, the corresponding variable was deleted from the model, and the negative binomial regression was rerun. In addition, while it was not considered appropriate to include independent variables with significance levels above 10 percent in the models presented in this report, the text of the report identifies those independent variables that were found to have significance levels between 10 percent and 20 percent. This significance level, $\alpha$, is indicated for each such variable.

Table 2. Descriptive Statistics for Rural, Four-Leg, STOP-Controlled Intersections


Conversion: $1 \mathrm{~km} / \mathrm{h}=0.621 \mathrm{mi} / \mathrm{h} ; 1 \mathrm{~m}=3.28 \mathrm{ft}$

The final model diagnostics for the reduced negative binomial regression model are shown in Table 3. The model diagnostics, which are shown separately for each type of accident considered, include both basic statistics and goodness-of-fit criteria. The following model statistics are shown:

## Model Statistic Explanation

## Basic Statistics

Number of intersections, $n \quad$ Total sample size in that category of intersections
Number of parameters in Total number of independent variables, both categorical model

Parameters degrees of freedom, p
k factor and continuous

Each continuous independent variable has one degree of freedom; the number of degrees of freedom associated with each categorical variable equals the number of levels minus one. The intercept has one degree of freedom. The sum of these degrees of freedom is denoted as $p$.

Only applicable to the negative binomial distribution. The use of this factor results in a ratio of the deviance to its degrees of freedom of approximately one.

## Criteria for Assessing Goodness of Fit

$\left.\begin{array}{ll}\text { Deviance } /(\mathrm{n}-\mathrm{p}) & \begin{array}{l}\text { The deviance of the model containing all the parameters } \\ \text { (including the intercept) divided by its degrees of freedom, } \\ \mathrm{n}-\mathrm{p} . \text { This statistic (mean deviance) provides a test for } \\ \text { overdispersion and a measure of fit of the model. }\end{array} \\ \text { Asymptotically, this value tends toward one. }\end{array}\right\}$

Two goodness-of-fit measures, the mean deviance and the Pearson chi-square ratio (the Pearson chi-square value divided by its degrees of freedom), were used to assess the fit of the model. Generally, if the Pearson chi-square ratio is between 0.8 and 1.2 , this is an indication that the model can be assumed to be appropriate in modeling the data.

Table 3. Model Diagnostics for Total and Fatal and Injury Accidents at Rural, Four-Leg, STOP-Controlled Intersections

|  | Negative binomial regression (reduced model) |
| :---: | :---: |
| Total Accidents (3-year period) |  |
| Number of intersections (n) | 1,434 |
| Total number of parameters considered | 14 |
| Number of parameters in reduced model | 9 |
| Parameters degrees of freedom ${ }^{\text {a }}$ (p) | 12 |
| $k$ factor | 0.65 |
| Deviance/(n-p) | 1.00 |
| Pearson chi-square/( $n-p$ ) | 0.95 |
| $\mathrm{R}^{2}$ (percent) | 37.26 |
| $\mathrm{R}_{\text {FT }}$ (percent) | 39.32 |
| Fatal and Injury Accidents (3-year period) |  |
| Number of intersections (n) | 1,434 |
| Total number of parameters considered | 14 |
| Number of parameters in reduced model | 7 |
| Parameters degrees of freedom ${ }^{\text {a }}$ (p) | 10 |
| k factor | 0.70 |
| Deviance/(n-p) | 0.99 |
| Pearson chi-square/( $\mathrm{n}-\mathrm{p}$ ) | 1.00 |
| $\mathrm{R}^{2}$ (percent) | 31.14 |
| $\mathrm{R}_{\text {FT }}^{2}$ (percent) | 30.47 |

${ }^{\text {a }}$ Includes one degree of freedom for the intercept.
Of the 14 original independent variables considered, only 9 remain statistically significant in the final negative binomial model for total accidents. A variance stabilizing factor, k , of 0.65 was needed to achieve a mean deviance of approximately one, indicating that the data are neither overdispersed nor underdispersed relative to the model. The Pearson chi-square ratio equals approximately 0.95 , a value within the acceptable range of 0.8 to 1.2. These two goodness-of-fit results indicate that the choice of the negative binomial model appears appropriate. The two additional measures of goodness of fit, $\mathrm{R}^{2}$ and $\mathrm{R}_{\mathrm{FT}}^{2}$, are approximately 37 percent and 39 percent, respectively, for total accidents.

Of the five independent variables considered in the full, but not in the final, reduced negative binomial model, only one variable-major-road left-turn channelization $(\alpha=$ 0.16 )—was not significant at the 10 percent level, but would have been significant at the 20 percent level.

The use of the negative binomial model had a similar impact on the results for fatal and injury accidents. Of the 14 original independent variables considered, only 7 remain statistically significant in the final negative binomial model for fatal and injury accidents. A variance stabilizing factor, k , of 0.70 was needed to achieve a mean deviance of approximately one. The Pearson chi-square ratio equals approximately one, a value within the acceptable range of 0.8 to 1.2. Again, the two goodness-of-fit results provide an indication that the choice of the negative binomial model appears appropriate. The two additional measures of goodness of fit, $\mathrm{R}^{2}$ and $\mathrm{R}_{\mathrm{FT}}^{2}$, are approximately 31 percent and 30 percent, respectively, for fatal and injury accidents.

Of the seven independent variables considered in the full, but not in the final, reduced negative binomial model, only two variables-access control on major road $(\alpha=0.12)$ and major-road left-turn channelization $(\alpha=0.12)$ —were not significant at 10 percent, but would have been significant at the 20 percent level.

Tables 4 and 5 summarize the regression results for the final negative binomial model for total accidents and fatal and injury accidents, respectively. Each table identifies the:

- Statistically significant variables remaining in the final model
- Chi-square statistic for each remaining variable; all of these chi-square statistics are statistically significant at the 10 percent significance level or better
- Levels of each statistically significant categorical variable
- Direction of the effect if the effect was inverse to the expected direction
- Value of the regression coefficient for each continuous variable or each level of each categorical variable in the model
- Relative effect of a unit change in each variable on the expected accident frequency in a 3 -year period (this is simply $\mathrm{e}^{\beta}$, where $\beta$ is the coefficient given in the table)
- Lower and upper 90 percent confidence limits of the regression coefficient

In each table, the independent variables are listed in decreasing order of their ability to explain the variations in intersection accident frequencies as indicated by the chi-square value, which represents the strength of the relationship of each variable to accident frequency, taking into account all other variables in the model.
Table 4. Negative Binomial Regression Results for Total Accidents
at Rural, Four-Leg, STOP-Controlled Intersections

| Independent variable ${ }^{\text {a }}$ | Chi square statistic ${ }^{\text {b }}$ | Variable level | Direction of effect ${ }^{\text {c }}$ | Coefficient | Relative effect ${ }^{\text {d }}$ | 90 percent confidence limits ${ }^{e}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Lower | Upper |
| Intercept |  |  |  | -10.025 |  | -10.846 | -9.211 |
| Crossroad ADT (log) | 361.52 |  | - | 0.532 | 1.70 | 0.484 | 0.579 |
| Major-road ADT (log) | 347.76 |  | - | 0.758 | 2.13 | 0.689 | 0.827 |
| Number of lanes on major road | 15.25 | 3 or less | - | 0.321 | 1.38 | 0.186 | 0.455 |
|  | 11.19 | 4 or more | - | 0.009 | 1.01 | 0.005 | 0.014 |
| Access control on major road | 5.78 | None | - | 0.200 | 1.22 | 0.063 | 0.336 |
|  |  | Partial | - | 0 |  |  |  |
| Functional class of major road | 7.26 | Principal arterial | - | 0 |  |  |  |
|  |  | Minor arterial | - | 0.181 | 1.20 | 0.070 | 0.292 |
|  |  | Major collector | - | 0.173 | 1.19 | 0.0005 | 0.347 |
| Lighting | 3.68 | $\begin{aligned} & \text { No } \\ & \text { Yes } \end{aligned}$ |  | $\begin{aligned} & 0.122 \\ & 0 \end{aligned}$ | 1.13 | 0.017 | 0.226 |
| Terrain | 4.81 | Flat | 1 | 0.053 | 1.05 | 0.055 | 0.160 |
|  |  | Rolling | 1 | 0 |  |  |  |
|  |  | Mountainous | 1 | -0.159 | 0.85 | -0.328 | 0.011 |
| Major-road right-turn channelization | 2.78 | No free right-turn lane Provision for free right-turns | - | $\begin{aligned} & 0.157 \\ & 0 \end{aligned}$ | 1.17 | 0.002 | 0.310 |

[^0]Table 5. Negative Binomial Regression Results for Fatal and Injury Accidents at Rural, Four-Leg, STOP-Controlled Intersections

| Independent variable ${ }^{\text {a }}$ | Chi square statistic ${ }^{b}$ | Variable level | Direction of effect ${ }^{\circ}$ | Coefficient | Relative effect ${ }^{\text {d }}$ | 90 percent confidence limits ${ }^{\circ}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Lower | Upper |
| Intercept |  |  |  | -10.294 |  | -11.244 | -9.356 |
| Crossroad ADT (log) | 282.17 |  | - | 0.546 | 1.73 | 0.491 | 0.602 |
| Major-road ADT ( log ) | 201.92 |  | - | 0.680 | 1.97 | 0.599 | 0.762 |
| Number of lanes on major road | 18.17 | 3 or less | - | 0.385 | 1.47 | 0.237 | 0.533 |
|  |  | 4 or more | - | 0 |  |  |  |
| Design speed on major road | 16.60 |  | - | 0.013 | 1.01 | 0.008 | 0.019 |
| Terrain | 15.98 | Flat | 1 | 0.183 | 1.20 | 0.060 | 0.306 |
|  |  | Rolling | I | 0 |  |  |  |
|  |  | Mountainous | 1 | -0.234 | 0.79 | -0.442 | -0.026 |
| Functional class of major road | 11.87 | Principal arterial | - | 0 |  |  |  |
|  |  | Minor arterial | - | 0.261 | 1.30 | 0.136 | 0.386 |
|  |  | Major collector | - | 0.170 | 1.18 | -0.030 | 0.370 |
| Lighting | 9.03 | $\begin{aligned} & \text { No } \\ & \text { Yes } \end{aligned}$ | - | $0.219$ | 1.24 | 0.099 | 0.339 |

[^1]To predict the average accident frequency at rural, four-leg, STOP-controlled intersections, one replaces the regression coefficients, $\beta_{0}, \beta_{1}, \beta_{2}, \ldots \beta_{q}$, with the estimated values found in the table, and the variables $X_{1}, X_{2}, \ldots, X_{q}$, with their appropriate values or levels. For example, the expected 3-year total accident frequency can be estimated using the model presented in Table 4 as:

$$
\begin{align*}
\mathrm{Y}= & \mathrm{e}^{-10.025}\left(\mathrm{X}_{1}\right)^{0.532}\left(\mathrm{X}_{2}\right)^{0.758} \exp \left(0.321 \mathrm{X}_{3}\right) \exp \left(0.009 \mathrm{X}_{4}\right) \exp \left(0.200 \mathrm{X}_{5}\right)  \tag{7}\\
& \exp \left(0.181 \mathrm{X}_{6}\right) \exp \left(0.173 \mathrm{X}_{7}\right) \exp \left(0.122 \mathrm{X}_{8}\right) \exp \left(-0.053 \mathrm{X}_{9}\right) \exp \left(0.159 \mathrm{X}_{10}\right) \\
& \exp \left(0.157 \mathrm{X}_{11}\right)
\end{align*}
$$

where:
$\mathrm{Y}=$ expected number of total accidents in a 3-year period
$\mathrm{X}_{1}=\mathrm{ADT}$ of the crossroad (veh/day)
$\mathrm{X}_{2}=\mathrm{ADT}$ of the major road (veh/day)
$X_{3}=1$ if the major road has 3 or fewer lanes in both direction of travel combined; 0 if 4 or more
$\mathrm{X}_{4}=$ design speed on major road ( $\mathrm{mi} / \mathrm{h}$ )
$X_{5}=1$ if the major road has no access control; 0 if access control is partial
$X_{6}=1$ if the major road is a minor arterial; 0 otherwise
$\mathrm{X}_{7}=1$ if the major road is a major collector; 0 otherwise
$\mathrm{X}_{8}=1$ if the intersection is lighted; 0 otherwise
$X_{9}=1$ if terrain is flat; 0 otherwise
$\mathrm{X}_{10}=1$ if terrain is mountainous; 0 otherwise
$X_{11}=1$ if no right-turn lane is present on the major road; 0 otherwise
Note that when the level of a categorical variable is 0 , the multiplicative term in Equation (7) becomes $\mathrm{e}^{0}=1$ and is therefore omitted from the model.

The relative effect of each variable, all other variables being held constant, can be calculated by simply taking the exponent of the corresponding coefficient. For example, the relative effect of having a major road with three lanes or fewer as opposed to four lanes or more is $\exp (0.321)=1.38$. In other words, decreasing the number of lanes on the major road from 4 or more to 3 or less, with all other factors being held constant, would increase the expected number of accidents by a factor of 1.38 or by 38 percent. Similarly, intersections on major roads without access control were found to have 22 percent more accidents than intersections on major roads with partial access control.

The results of the negative binomial regression modeling shown in Tables 4 and 5 show that most of the variables of interest have effects in the direction expected. However, the observed effect of terrain is not in the expected direction since the results imply that intersections in flat terrain have more accidents than intersections in rolling terrain which, in turn, have more accidents than intersections in mountainous terrain. Such effects that are opposite the direction expected can represent situations in which a variable, for which data
are available, is correlated with and serves as a surrogate for another variable for which data are not available.

Figure 6 illustrates the influence of the major-road and crossroad ADT on the annual number of accidents at rural, four-leg, STOP-controlled intersections with the typical geometrics identified in the box below the figure. Each curve in the figure represents combinations of major-road and crossroad ADT that would be expected to result in a specific annual number of accidents, ranging from 0.5 to 5 accidents per year.

## Rural, Three-Leg, STOP-Controlled Intersections

The statistical analysis approach used for rural, three-leg, STOP-controlled intersections was identical to that used for rural, four-leg, STOP-controlled intersections. The median number of total accidents at any single intersection was 1 accident in the 3-year study period, with a maximum of 59 accidents in the 3-year period. As shown in Figure 2, approximately 55 percent of all 2,692 rural, three-leg, STOP-controlled intersections in the study experienced either no accidents or 1 accident in the 3-year period. Thus, the negative binomial model appeared to be a logical choice for analysis of this data set.

The selection of independent variables was done in a fashion similar to that described earlier in Section 3. Table 6 identifies the variables that were selected for modeling accidents at rural, three-leg, STOP-controlled intersections. As before, a small number of independent categorical variables were not included in the full model because either all or nearly all intersections fell into one level of that variable. The variables originally considered that were not included for this reason were:

- Major-road left-turn prohibition (no intersections had left turns prohibited)
- Crossroad left-turn channelization (none of the intersections had left-turn lanes)
- Crossroad left-turn prohibition (none of the intersections had left turns prohibited)
- Number of lanes on the crossroad (99.7 percent had two lanes)

As shown in the table, 14 independent variables, both continuous and categorical, were considered in the full negative binomial regression model. Of these 14 variables, 7 were found to have a statistically significant effect on accidents (both total and fatal and injury multiple-vehicle) at the 10 percent significance level. A reduced negative binomial model was then rerun using only the seven statistically significant variables.


| Major road characteristics: | Other: |
| :---: | :---: |
| - 3 lanes or less | - No lighting |
| - Design speed of $89 \mathrm{~km} / \mathrm{h}(55 \mathrm{mi} / \mathrm{h})$ | - Flat terrain |
| - No access control |  |
| - No free right turns |  |

Figure 6. Number of Accidents per Year as a Function of Traffic Volumes for Typical Rural, Four-Leg, STOP-Controlled Intersections
Table 6. Descriptive Statistics for Rural, Three-Leg, STOP-Controlled Intersections

Conversion: $1 \mathrm{~km} / \mathrm{h}=0.621 \mathrm{mi} / \mathrm{h} ; 1 \mathrm{~m}=3.28 \mathrm{ft}$

A final, reduced negative binomial regression model was used with a variance adjustment factor, k , of 0.70 for total and 0.55 for fatal and injury accidents, respectively. The model diagnostics are summarized in Table 7. In each case, this approach resulted in a mean deviance of approximately one, and a Pearson chi-square ratio of 1.07 for total accidents and 1.15 for fatal and injury accidents. Of the original 14 independent variables considered for modeling, only 7 remained statistically significant at the 90 percent confidence level for total accidents. A slightly different set of 7 variables remained statistically significant at the 90 percent confidence level for fatal and injury accidents.

Table 7. Model Diagnostics for Total and Fatal and Injury Accidents at Rural, Three-Leg, STOP-Controlled Intersections

|  | Negative binomial <br> regression <br> (reduced model) |
| :--- | :---: |
| Total Accidents (3-year period) |  |
| Number of intersections (n) | 2,692 |
| Total number of parameters considered | 14 |
| Number of parameters in reduced model | 7 |
| Parameters degrees of freedom ${ }^{\text {a }}$ (p) | 11 |
| k factor | 0.70 |
| Deviance/(n - p) | 1.01 |
| Pearson chi-square/(n - $p$ ) | 1.07 |
| $R^{2}$ (percent) | 34.00 |
| $R^{2}$ FT (percent) | 34.09 |
| Fatal and Injury Accidents (3-year period) |  |
| Number of intersections (n) |  |
| Total number of parameters considered | 2,692 |
| Number of parameters in reduced model | 14 |
| Parameters degrees of freedom ${ }^{2}$ (p) | 7 |
| k factor | 10 |
| Deviance/(n - $p$ ) | 0.55 |
| Pearson chi-square/(n - $p$ ) | 1.00 |
| $R^{2}$ (percent) | 1.15 |
| $R^{2}$ (pT (percent) | 26.46 |

${ }^{\text {a }}$ Includes one degree of freedom for the intercept.

Of the 7 independent variables considered in the full, but not in the final, reduced negative binomial model for total accidents, only 3 variables-average lane width on major $\operatorname{road}(\alpha=0.15)$, lighting $(\alpha=0.18)$, and number of lanes on major road $(\alpha=0.20)$ —were not significant at the 10 percent level, but would have been at the 20 percent level. Of the 7 independent variables considered in the full, but not in the final, reduced negative binomial model for fatal and injury accidents, 4 variables-crossroad right-turn channelization ( $\alpha=$
0.11 ), design speed ( $\alpha=0.12$ ), average lane width or major road ( $\alpha=0.15$ ), and terrain ( $\alpha$ $=0.18$ )—were not significant at the 10 percent level, but would have been at the 20 percent level.

Tables 8 and 9 summarize the regression results for the final negative binomial model for total accidents and fatal and injury accidents, respectively. The tables show that for rural, three-leg, STOP-controlled intersections, all of the independent variables evaluated in the total accident models had effects in the direction expected. The variable for crossroad right-turn channelization in the model for fatal and injury accidents has an effect opposite the direction expected since the model implies that an intersection without free right-turn channelization would experience fewer accidents than an intersection with free right-turn channelization.

Figure 7 illustrates the variations of the annual number of accidents with major-road and crossroad ADT for rural, three-leg, STOP-controlled intersections of the type specified at the upper right of the figure.

## Urban, Four-Leg, STOP-Controlled Intersections

The statistical analysis approach used for urban, four-leg, STOP-controlled intersections was at first identical to that used for rural, four- and three-leg, STOP-controlled intersections. The median number of total accidents at any intersection was 5 accidents in the 3-year study period with a maximum of 57 accidents in the 3-year period. As shown in Figure 3, only approximately 8 percent of all 1,342 urban, four-leg, STOP-controlled intersections in the study experienced no accidents in the 3-year period.

The selection of independent variables was done in a fashion similar to that described earlier. Table 10 identifies the variables that were selected for modeling accidents at urban, four-leg, STOP-controlled intersections. As before, a small number of independent categorical variables were not included in the full model because either all or nearly all intersections fell into one level of that variable. The variables originally considered that were not included for this reason were:

- Crossroad left-turn prohibition (only 4 percent of the intersections had left turns prohibited; in addition, this variable showed a high negative correlation of -0.73 with the equivalent variable on the major road)
- Number of lanes on the crossroad (99.9 percent had 2 lanes)
Table 8. Negative Binomial Regression Results for Total Accidents
at Rural, Three-Leg, STOP-Controlled Intersections

| Independent variable ${ }^{\text {a }}$ | Chi square statistic ${ }^{\text {b }}$ | Variable level | Direction of effect ${ }^{\text { }}$ | Coefficient | Relative effect ${ }^{\text {d }}$ | 90 percent confidence limits ${ }^{e}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Lower | Upper |
| Intercept |  |  |  | -9.178 |  | -9.746 | -8.616 |
| Major-road ADT (log) | 772.08 |  | - | 0.830 | 2.29 | 0.778 | 0.882 |
| Crossroad road ADT (log) | 301.33 |  | - | 0.383 | 1.47 | 0.345 | 0.420 |
| Major-road left-turn channelization | 15.73 | No left-turn lane | - | 0.213 | 1.24 | 0.124 | 0.301 |
|  |  | Painted left-turn lane | - | 0 |  |  |  |
|  |  | Curbed left-turn lane | - | 0.124 | 1.13 | -0.120 | 0.374 |
| Access control on major road | 7.31 | None | - | 0.225 | 1.25 | 0.089 | 0.362 |
|  |  | Partial | - | 0 |  |  |  |
| Functional class of major road | 7.27 | Principal arterial | - | 0 |  |  |  |
|  |  | Minor arterial | - | 0.145 | 1.16 | 0.048 | 0.242 |
|  |  | Major collector | - | 0.211 | 1.23 | 0.059 | 0.363 |
| Outside shoulder width on major road | 4.63 |  |  | -0.017 | 0.98 | -0.030 | -0.004 |
| Terrain | 5.32 | Flat | - | -0.045 | 0.96 | -0.130 | 0.041 |
|  |  | Rolling | - | 0 |  |  |  |
|  |  | Mountainous | - | 0.095 | 1.10 | -0.004 | 0.195 |

[^2]Table 9. Negative Binomial Regression Results for Fatal and Injury Accidents at Rural, Three-Leg, STOP-Controlled Intersections

| Independent variable ${ }^{\text {a }}$ | Chi square statistic ${ }^{\text {b }}$ | Variable level | Direction of effect ${ }^{\text {© }}$ | Coefficient | Relative effect ${ }^{d}$ | 90 percent confidence limits ${ }^{e}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Lower | Upper |
| Intercept |  |  |  | -9.141 |  | -9.841 | -8.447 |
| Major-road ADT (log) | 517.56 |  | - | 0.781 | 2.18 | 0.722 | 0.841 |
| Crossroad ADT (log) | 217.64 |  | - | 0.384 | 1.47 | 0.341 | 0.428 |
| Outside shoulder width on major road | 11.61 |  | - | -0.030 | 0.97 | -0.044 | -0.015 |
| Lighting | 9.35 | $\begin{aligned} & \text { No } \\ & \text { Yes } \end{aligned}$ | - | $\begin{aligned} & 0.169 \\ & 0 \end{aligned}$ | 1.18 | 0.078 | 0.261 |
| Major-road left-turn channelization | 8.89 | No left-turn lane | - | 0.180 | 1.20 | 0.080 | 0.279 |
|  |  | Painted left-turn lane Curbed left-turn lane | - | 00062 | 1.06 | -0.194 | 0.318 |
| Functional class of major road | 6.90 | Principal arterial | - | 0 |  |  |  |
|  |  | Minor arterial | - | 0.164 | 1.18 | 0.058 | 0.270 |
|  |  | Major collector | 1 | 0.192 | 1.21 | 0.021 | 0.362 |
| Crossroad right-turn channelization | 2.74 | No free right turns Provision for free right turns | I | $\begin{gathered} -0.219 \\ 0 \end{gathered}$ | 0.80 | -0.437 | -0.001 |

Note: This analysis is based on the set of 2,692 intersections for which summary statistics are shown in Table 6 .
a All variables significant at the 90 percent confidence level or higher
Chi-square likelihood ratio statistic for testing the significance of the effect of the variable; with 1 degree of freedom for continuous variables; with ( $p-1$ ) degrees of freedom for categorical variables with $p$ levels
Relative effect of unit change in the variable on the expected number of accidents, equals exp(coefficient) 90 percent lower and upper confidence limits of the estimated coefficient


| Major road characteristics: | Other: |
| :--- | :--- |
| $\quad$ No left-turn lane | $\rightarrow$ Flat terrain |
| $\quad$ No access control |  |
| $\quad$Minor arterial <br> $\quad$ Outside shoulder width of $1.8 \mathrm{~m}(6 \mathrm{ft})$ |  |

Figure 7. Number of Accidents per Year as a Function of Traffic Volumes for Typical Rural, Three-Leg, STOP-Controlled Intersections
Table 10. Descriptive Statistics for Urban, Four-Leg, STOP-Controlled Intersections


As is shown in Table 10, 16 independent variables, both continuous and categorical, were considered in the full regression model. Based on the shape of the accident data distributions (see Figure 3), a lognormal rather than a negative binomial regression model was used to model accidents at this type of intersection. The natural logarithm of the accident counts was modeled using the full set of 16 independent variables. All modeling was performed using the SAS stepwise regression procedure.

The model diagnostics are summarized in Table 11. In this case, the root mean squared error (RMSE) has been added as a measure of fit of the model to the data. This statistic provides an estimate of the standard deviation of the error term (on the log scale).

Table 11. Model Diagnostics for Total and Fatal and Injury Accidents at Urban, Four-Leg, STOP-Controlled Intersections

|  | Lognormal Regression (reduced model) |
| :---: | :---: |
| Total Accidents (3-year period) |  |
| Number of intersections ( n ) | 1,342 |
| Total number of parameters considered | 16 |
| Number of parameters in reduced model | 9 |
| Parameters degrees of freedom ${ }^{\text {a }}$ (p) | 12 |
| Deviance/(n-p) | 0.96 |
| Pearson chi-square/( $n-p$ ) | 0.96 |
| $\mathrm{R}^{2}$ (percent) | 21.12 |
| $\mathrm{R}^{2}{ }_{\text {FT }}$ (percent) | na |
| Root mean square error | 0.96 |
| Fatal and Injury Accidents (3-year period) |  |
| Number of intersections ( n ) | 1,342 |
| Total number of parameters considered | 16 |
| Number of parameters in reduced model | 9 |
| Parameters degrees of freedom ${ }^{\text {a }}(\mathrm{p})$ | 12 |
| Deviance/(n-p) | 0.80 |
| Pearson chi-square/(n-p) | 0.80 |
| $\mathrm{R}^{2}$ (percent) | 18.70 |
| $\mathrm{R}_{\mathrm{FT}}^{2}$ (percent) | na |
| Root mean square error | 0.80 |

${ }^{\text {a }}$ Includes one degree of freedom for the intercept
The mean deviance, the Pearson chi-square ratio, and the RMSE are all identical, with values of 0.96 and 0.80 for total and fatal and injury accidents, respectively. The $R^{2}$ values are approximately 21 percent for total accidents and approximately 19 percent for fatal and injury accidents. These measures of fit, however, are relatively poor compared to those obtained for the previous types of intersections.

Of the original 16 independent variables considered for modeling, only 9 remained statistically significant at the 90 percent confidence level for total accidents. A slightly different set of 9 variables remained statistically significant at the 90 percent confidence level for fatal and injury accidents.

Of the 7 independent variables considered in the full, but not in the final, reduced lognormal model for total accidents, only 2 variables-outside shoulder width ( $\alpha=0.13$ ) and terrain ( $\alpha=0.19$ )-were not significant at the 10 percent level, but would have been at the 20 percent level. Of the 7 independent variables considered in the full, but not in the final, reduced lognormal model for fatal and injury accidents, only 1 variable-crossroad left-turn channelization $(\alpha=0.15)$-was not significant at the 10 percent level, but would have been at the 20 percent level.

Tables 12 and 13 summarize the regression results for the final lognormal model for total accidents and fatal and injury accidents, respectively. The tables indicate that no statistically significant effect on accidents was found for major-road left-turn channelization. The average lane width on the major road was found to have an effect on intersection accidents in the expected direction (i.e., for each decrease of $0.3 \mathrm{~m}(1 \mathrm{ft})$ in lane width on the major-road approaches, intersection-related accidents increased by 9.1 percent). Three of the variables evaluated had effects that were inverse to the direction expected: access control on the major road, crossroad right-turn channelization, and intersection lighting.

Figure 8 illustrates the variation of the annual number of intersection accidents with major-road and crossroad ADT for urban, four-leg, STOP-controlled intersections with the typical conditions specified in the figure.

## Urban, Three-Leg, STOP-Controlled Intersections

The statistical analysis approach used for urban, three-leg, STOP-controlled intersections was identical to that used for rural, four- and three-leg, STOP-controlled intersections. The median number of total accidents at any 1 intersection was 3 accidents in the 3-year study period with a maximum of 81 accidents in the 3-year period. As shown in Figure 4, approximately 47 percent of all 3,057 urban, three-leg, STOP-controlled intersections in the study experienced 2 or fewer accidents in the 3-year period. Thus, the negative binomial model appeared to be a logical choice for analysis of this data set.

The selection of independent variables was done in a fashion similar to that described in earlier sections. Table 14 identifies the variables that were selected for modeling accidents at urban, three-leg, STOP-controlled intersections. None of the variables considered for modeling was deleted due to small sample sizes. Although the percentage of intersections in some levels is relatively small (e.g, 0.7 percent of intersections had 4 or more lanes), the large number of intersections $(3,057)$ in this category justified the inclusion of these variables and their levels in the analysis.
Table 12. Lognormal Regression Results for Total Accidents at Urban, Four-Leg, STOP-Controlled Intersections

| Independent variable ${ }^{\text {a }}$ | Chi square statistic ${ }^{\text {b }}$ | Variable level | Direction of effect ${ }^{\text {c }}$ | Coefficient | Relative effect ${ }^{d}$ | 90 percent confidence limits ${ }^{\text {e }}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Lower | Upper |
| Intercept |  |  |  | -4.664 |  | -5.783 | -3.545 |
| Major-road ADT (log) | 132.18 |  | - | 0.620 | 1.86 | 0.532 | 0.709 |
| Crossroad ADT (log) | 88.36 |  | - | 0.281 | 1.32 | 0.232 | 0.330 |
| Major-road left-turn prohibition | 31.64 | Left turns prohibited | - | -0.941 | 0.39 | -1.216 | -0.666 |
|  |  | Left turns permitted | - | 0 |  |  |  |
| Average lane width on major road | 16.28 |  | - | -0.097 | 0.91 | -0.136 | -0.057 |
| Number of lanes on major road | 14.99 | 3 or less | - | 0.401 | 1.49 | 0.179 | 0.623 |
|  |  | 4 or 5 | - | 0.120 | 1.13 | -0.064 | 0.304 |
|  |  | 6 or more | - | 0 |  |  |  |
| Access control on major road | 8.49 | None | 1 | -0.437 | 0.65 | -0.683 | -0.190 |
|  |  | Partial | I | 0 |  |  |  |
| Crossroad right-turn channelization | 6.01 | No free right turns | 1 | -0.384 | 0.68 | -0.641 | -0.126 |
|  |  | Provision for free right turns | I | 0 |  |  |  |
| Lighting | 3.48 | No | 1 | -0.160 | 0.85 | -0.302 | -0.019 |
|  |  | Yes | 1 | 0 |  |  |  |
| Functional class of major road | 2.95 | Principal arterial | - | 0 |  |  |  |
|  |  | Minor arterial | - | -0.153 | 0.86 | -0.332 | 0.025 |
|  |  | Major collector | - | -0.229 | 0.80 | -0.593 | 0.135 |

[^3]Table 13. Lognormal Regression Results for Fatal and Injury Accidents at Urban, Four-Leg, STOP-Controlled Intersections

| Independent variable ${ }^{\text {a }}$ | Chi square statistic ${ }^{\text {b }}$ | Variable level | Direction of effect ${ }^{\text {c }}$ | Coefficient | Relative effect ${ }^{\text {d }}$ | 90 percentconfidence limits |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Lower | Upper |
| Intercept |  |  |  | -4.693 |  | -5.790 | -3.597 |
| Major-road ADT (log) | 117.44 |  | - | 0.584 | 1.79 | 0.495 | 0.672 |
| Crossroad ADT (log) | 48.45 |  | - | 0.206 | 1.23 | 0.157 | 0.255 |
| Major-road left-turn prohibition | 19.95 | Left turns prohibited | - | -0.747 | 0.47 | -1.022 | -0.472 |
|  |  | Left turns permitted | - | 0 |  |  |  |
| Average lane width on major road | 11.36 |  | - | -0.081 | 0.92 | -0.121 | -0.042 |
| Access control on major road | 7.31 | None | 1 | -0.382 | 0.68 | -0.615 | -0.150 |
|  |  | Partial | I | 0 |  |  |  |
| Number of lanes on major road | 9.88 | 3 or less | - | 0.282 | 1.33 | 0.059 | 0.504 |
|  |  | 4 or 5 | - | 0.049 | 1.05 | -0.137 | 0.234 |
|  |  | 6 or more | - | 0 |  |  |  |
| Outside shoulder width on major road | 5.94 |  | - | -0.020 | 0.98 | -0.033 | -0.006 |
| Crossroad right-turn channelization | 3.66 | No free right turns | 1 | -0.300 | 0.74 | -0.557 | -0.042 |
|  |  | Provision for free right turns | 1 | 0 |  |  |  |
| Functional class of major road | 3.71 | Principal arterial | - | 0 |  |  |  |
|  |  | Minor arterial | - | -0.079 | 0.92 | -0.257 | 0.100 |
|  |  | Major collector | - | -0.401 | 0.67 | -0.766 | -0.037 |

[^4]

| Major road characteristics: <br> Left turns permitted <br> Average lane width of $3.6 \mathrm{~m}(12 \mathrm{ft})$ <br> 4 or 5 lanes <br> No access control <br> Principal arterial | Crossroad characteristics: <br> - No free right turns | Other: <br> Lighting |
| :---: | :---: | :---: |

Figure 8. Number of Accidents per Year as a Function of Traffic Volumes for Typical Urban, Four-Leg, STOP-Controlled Intersections
Table 14. Descriptive Statistics for Urban, Three-Leg, STOP-Controlled Intersections


As shown in the table, 18 independent variables, both continuous and categorical, were considered in the full negative binomial regression model. Of these 18 variables, 8 were found to have a statistically significant effect on either total or fatal and injury accidents at the 10 percent significance level. A negative binomial regression model was then used with a variance adjustment factor, k , of 0.86 for total and 0.79 for fatal and injury accidents. The final model diagnostics are summarized in Table 15. In each case, this approach resulted in a mean deviance of approximately 1 , and a Pearson chi-square ratio of 1.08 for total accidents and 1.00 for fatal and injury accidents. For both types of accidents, the models produced relatively poor results based on the two $\mathrm{R}^{2}$ values, all in the range of 16 to 18 percent.

Table 15. Model Diagnostics for Total and Fatal and Injury Accidents at Urban, Three-Leg, STOP-Controlled Intersections

|  | Negative binomial regression (reduced model) |
| :---: | :---: |
| Total Accidents (3-year period) |  |
| Number of intersections ( n ) | 3,057 |
| Total number of parameters considered | 18 |
| Number of parameters in reduced model | 8 |
| Parameters degrees of freedom ${ }^{\text {a }}$ (p) | 10 |
| $k$ factor | 0.86 |
| Deviance/(n-p) | 1.00 |
| Pearson chi-square/(n-p) | 1.08 |
| $\mathrm{R}^{2}$ (percent) | 16.66 |
| $\mathrm{R}_{\text {FT }}^{2}$ (percent) | 17.67 |
| Fatal and Injury Accidents (3-year period) |  |
| Number of intersections (n) | 3,057 |
| Total number of parameters considered | 18 |
| Number of parameters in reduced model | 8 |
| Parameters degrees of freedom ${ }^{\text {a }}$ (p) | 10 |
| k factor | 0.79 |
| Deviance/(n-p) | 1.00 |
| Pearson chi-square/(n-p) | 1.00 |
| $\mathrm{R}^{2}$ (percent) | 16.21 |
| $\mathrm{R}_{\text {FT }}^{2}$ (percent) | 15.66 |

${ }^{\text {a }}$ Includes one degree of freedom for the intercept.
Of the original 18 independent variables considered for modeling, only 8 remained statistically significant at the 90 percent confidence level for total accidents. A slightly different set of 8 variables remained statistically significant at the 90 percent confidence level for fatal and injury accidents.

Of the 10 independent variables considered in the full, but not in the final, reduced negative binomial model for total accidents, none that was not significant at the 10 percent level would have been significant at the 20 percent level. Of the 10 independent variables considered in the full, but not in the final, reduced negative binomial model for fatal and injury accidents, only 3 variables were not significant at the 10 percent level, but would have been at the 20 percent level. These variables were lighting ( $\alpha=0.12$ ); number of lanes on crossroad ( $\alpha=0.19$ ); and access control on major road ( $\alpha=0.20$ ).

Tables 16 and 17 summarize the regression results for the final negative binomial model for total accidents and fatal and injury accidents, respectively. The tables show an effect in the expected direction for the presence of a median on the major road; intersections on divided highways appear to have 14 percent fewer accidents than intersections on undivided highways. A concern with the models developed is that the effect on safety of major-road left-turn and right-turn channelization is opposite the direction expected.

Figure 9 shows the variation of the annual number of intersection accidents with majorroad and crossroad ADT for urban, three-leg, STOP-controlled intersections with the typical conditions specified in the figure.

## Urban, Four-Leg, Signalized Intersections

Accident frequencies at urban, four-leg, signalized intersections are shown in Figure 5, for both total and fatal and injury accidents. A clear departure from a Poisson distribution is visible in these distribution plots. Only 19 out of 1,306 intersections (or 1.5 percent) experienced no accidents in the 3-year study period. Approximately half of all intersections in this category experienced 19 accidents or more in the 3-year period, with a maximum of 151 total accidents. Given these high accident frequencies and the shape of the distribution for both types of accidents, a lognormal regression model presented a logical choice. Thus, the statistical analysis approach used for urban, four-leg, signalized intersections was identical to that used for urban, four-leg, STOP-controlled intersections.

The selection of independent variables was done in a fashion similar to that described earlier in Section 3. Table 18 identifies the variables that were selected for modeling accidents at urban, four-leg, signalized intersections. As before, a small number of independent categorical variables was not included in the full model because either all or nearly all intersections fell into one level of that variable. The variables originally considered that were not included for this reason were:

- Lighting (all intersections were lighted)
- Presence of major-road signal mast arm (a mast arm was present on all intersections)
- Major-road left-turn prohibition (no intersections had left turns prohibited)
Table 16. Negative Binomial Regression Results for Total Accidents at Urban, Three-Leg, STOP-Controlled Intersections

| Independent variable ${ }^{\text {a }}$ | Chi square statistic ${ }^{\text {b }}$ | Variable level | Direction of effect ${ }^{\text {c }}$ | Coefficient | Relative effect ${ }^{\text {d }}$ | 90 percent confidence limits ${ }^{\text {e }}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Lower | Upper |
| Intercept |  |  |  | -5.557 |  | -6.281 | -4.834 |
| Major-road ADT (log) | 325.80 |  | - | 0.683 | 1.98 | 0.620 | 0.745 |
| Crossroad ADT (log) | 147.31 |  | - | 0.245 | 1.28 | 0.211 | 0.278 |
| Crossroad right-turn channelization | 29.28 | No free right turns | 1 | -0.559 | 0.57 | -0.742 | -0.383 |
|  |  | Provision for free right turns | I | 0 |  |  |  |
| Major-road left-turn prohibition | 27.51 | Left turns prohibited | - | -0.402 | 0.67 | -0.528 | -0.276 |
|  |  | Left turns permitted | - | 0 |  |  |  |
| Major-road left-turn channelization | 12.60 | No left-turn lane | - | 0.019 | 1.02 | -0.075 | 0.113 |
|  |  | Painted left-turn lane | - | 0 |  |  |  |
|  |  | Curbed left-turn lane | I | 0.210 | 1.23 | 0.112 | 0.310 |
| Design speed of major road | 8.15 |  | - | -0.006 | 0.99 | -0.009 | -0.002 |
| Presence of median on major road | 6.10 | Divided | - | -0.147 | 0.86 | -0.245 | -0.049 |
|  |  | Undivided | - | 0 |  |  |  |
| Average lane width on major road | 4.60 |  | - | -0.037 | 0.96 | -0.066 | -0.009 |

[^5]Table 17. Negative Binomial Regression Results for Fatal and Injury Accidents at Urban, Three-Leg, STOP-Controlled Intersections

| Independent variable ${ }^{\text {a }}$ | Chi square statistic ${ }^{\text {b }}$ | Variable level | Direction of effect ${ }^{\text {c }}$ | Coefficient | Relative effect ${ }^{d}$ | 90 percent confidence limits ${ }^{\text {e }}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Lower | Upper |
| Intercept |  |  |  | -6.618 |  | -7.449 | -5.792 |
| Major-road ADT (log) | 257.57 |  | - | 0.696 | 2.01 | 0.623 | 0.769 |
| Crossroad ADT (log) | 112.32 |  | - | 0.238 | 1.27 | 0.201 | 0.275 |
| Crossroad right-turn channelization | 26.95 | No free right turns | 1 | -0.581 | 0.56 | -0.773 | -0.394 |
|  |  | Provision for free right turns | I | 0 |  |  |  |
| Major-road left-turn prohibition | 21.19 | Left turns prohibited | - | -0.393 | 0.68 | -0.533 | -0.253 |
| Major-road left-turn channelization | 13.06 | Left turns permitted No left-turn lane | - | -0 | 0.94 | -0.161 | 0.047 |
| Major-road lefturn channelizaion |  | Painted left-turn lane | I | 0 |  |  |  |
|  |  | Curbed left-turn lane | 1 | 0.209 | 1.23 | 0.103 | 0.316 |
| Presence of median on major road | 7.53 | Divided | - | -0.182 | 0.83 | -0.292 | -0.073 |
|  |  | Undivided | - | 0 |  |  |  |
| Average lane width on major road | 6.01 |  | - | -0.048 | 0.95 | -0.080 | -0.016 |
| Lighting | 3.01 | No | - | 0.094 | 1.10 | 0.005 | 0.184 |

[^6]

| Major road characteristics: |  |
| :--- | :--- |
| Left turns permitted |  |
| No left-turn lane |  |\(\left.\quad \begin{array}{c}Crossroad characteristics: <br>

No free right turns\end{array}\right\}\)

Figure 9. Number of Accidents per Year as a Function of Traffic Volumes for Typical Urban, Three-Leg, STOP-Controlled Intersections
Table 18. Descriptive Statistics for Urban, Four-Leg, Signalized Intersections

| Parameter | Level | Percent of intersections | Minimum | Mean | Median | Maximum |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total accidents; 1990 through 1992 combined Fatal and injury accidents; 1990 through 1992 combined |  |  | $\begin{aligned} & 0 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{array}{r} 23.4 \\ 9.6 \\ \hline \end{array}$ | $\begin{array}{r}19 \\ 8 \\ \hline\end{array}$ | $\begin{array}{r} 151 \\ 51 \\ \hline \end{array}$ |
| Major-road ADT (veh/day) Crossroad ADT (veh/day) Design speed of major road (mi/h) Outside shoulder width on major road (ft) Average lane width on major road (ft) |  |  | $\begin{array}{r} 2,400 \\ 101 \\ 25 \\ 0 \\ 8 \\ \hline \end{array}$ | $\begin{array}{r} 31,995 \\ 8,061 \\ 51 \\ 7.0 \\ 12.0 \\ \hline \end{array}$ | $\begin{array}{r} 31,000 \\ 5,501 \\ 50 \\ 8 \\ 12 \\ \hline \end{array}$ | $\begin{array}{r} 79,000 \\ 48,000 \\ 70 \\ 15 \\ 15 \\ \hline \end{array}$ |
| Terrain | Flat <br> Rolling or mountainous | $\begin{aligned} & 80 \\ & 20 \\ & \hline \end{aligned}$ |  |  |  |  |
| Functional class of major road | Principal arterial Minor arterial | $\begin{gathered} 96 \\ 4.1 \\ \hline \end{gathered}$ |  | 1,306 in | ections |  |
| Signal timing | Pretimed <br> Semiactuated <br> Fully actuated | $\begin{gathered} 2.5 \\ 13 \\ 85 \\ \hline \end{gathered}$ |  |  |  |  |
| Signal phasing | Two-phase Multiphase | $\begin{aligned} & 21 \\ & 79 \\ & \hline \end{aligned}$ |  |  |  |  |
| Major-road left-turn channelization | No left-turn lane Painted left-turn lane Curbed left-turn lane | $\begin{aligned} & 4.7 \\ & 40 \\ & 56 \\ & \hline \end{aligned}$ |  |  |  |  |
| Major-road right-turn channelization | No free right turns Provision for free right turns | $\begin{array}{r} 74 \\ 26 \\ \hline \end{array}$ |  |  |  |  |
| Number of lanes on major road | $\begin{aligned} & 3 \text { or less } \\ & 4 \text { or } 5 \\ & 6 \text { or more } \\ & \hline \end{aligned}$ | $\begin{aligned} & 7.9 \\ & 72 \\ & 20 \\ & \hline \end{aligned}$ |  |  |  |  |
| Presence of crossroad signal mast arm | Mast arm not present Mast arm present | $\begin{aligned} & 27 \\ & 73 \end{aligned}$ |  |  |  |  |



The natural logarithm of the accident counts was modeled using the full set of 19 independent variables listed in Table 18. All modeling was performed using the SAS stepwise regression procedure.

Of the original 19 independent variables considered for modeling, only 9 remained statistically significant at the 90 percent confidence level for total accidents. A slightly different set of 8 variables remained statistically significant at the 90 percent confidence level for fatal and injury accidents. The lognormal model was rerun using only the statistically significant variables to obtain the regression coefficients, their 90 percent confidence intervals, and other regression statistics.

Table 19 presents the model statistics for the final, reduced lognormal model. Although the lognormal models are significant at the 90 percent confidence level for both types of accidents, the percent variance explained by the model is relatively low, with an $\mathrm{R}^{2}$ value of approximately 25 percent for total accidents and approximately 24 percent for fatal and injury accidents. Also, the Pearson chi-square ratios ( 0.69 and 0.68 , respectively, for both types of accidents) are below the 0.8 to 1.2 range, indicating that the lognormal model might not provide the best fit.

Of the 10 independent variables considered in the full, but not in the final, reduced lognormal model for total accidents, only 1 variable-presence of crossroad signal mast arm ( $\alpha=0.11$ )—was not significant at the 10 percent level, but would have been at the 20 percent level. Of the 11 independent variables considered in the full, but not in the final, reduced lognormal model for fatal and injury accidents, only 1 variable-average lane width on major road $(\alpha=0.15)$-was not significant at the 10 percent level, but would have been at the 20 percent level.

Tables 20 and 21 summarize the regression results for the final lognormal model for total accidents and fatal and injury accidents, respectively. No statistically significant effect on accidents was found for either the major-road or crossroad left-turn channelization variable. However, it should be noted that major-road left-turn channelization could not be evaluated effectively because only 5 percent of the intersections had no left-turn lanes on the major road approaches. The only variables that appeared to have effects in the direction opposite to that expected were access control on the major road (for both models) and major-road right-turn channelization (for the total accident model only).

Table 19. Model Diagnostics for Total and Fatal and Injury Accidents at Urban, Four-Leg, Signalized Intersections

|  | Lognormal <br> regression <br> (reduced model) |
| :--- | ---: |
| Total Accidents (3-year period) |  |
| Number of intersections (n) |  |
| Total number of parameters considered | 1,306 |
| Number of parameters in reduced model |  |
| Parameters degrees of freedom ${ }^{\text {a }}$ (p) in final model | 19 |
| Deviance/(n - p) | 9 |
| Pearson chi-square/(n - p) | 12 |
| $R^{2}$ (percent) | 0.69 |
| $R^{2}$ (percent) | 0.69 |
| Root mean squared error | 24.77 |
| Fatal and Injury Accidents (3-year period) | 0.69 |
| Number of intersections (n) |  |
| Total number of parameters considered | 1,306 |
| Number of parameters in reduced model | 19 |
| Parameters degrees of freedom ${ }^{\text {a }}$ (p) in final model | 8 |
| Deviance/(n - p) | 11 |
| Pearson chi-square/(n - $p$ ) | 0.68 |
| $R^{2}$ (percent) | 0.68 |
| $R^{2}$ (percent) | 24.40 |
| Root mean squared error | 0.68 |

${ }^{\text {a }}$ Includes one degree of freedom for the intercept.
Figure 10 shows the variation of the annual number of intersection accidents with major-road and crossroad ADT for urban, four-leg, signalized intersections with the typical conditions specified in the figure. As shown in the figure, typical accident experience at these intersections, in the range of data for which model predictions appear valid, extends up to 12 accidents per year.
Table 20. Lognormal Regression Results for Total Accidents at Urban, Four-Leg, Signalized Intersections

| Independent variable ${ }^{\text {a }}$ | Chi square statistic ${ }^{\text {b }}$ | Variable level | Direction of effect ${ }^{\text { }}$ | Coefficient | Relative effect ${ }^{\text {d }}$ | 90 percent confidence limits ${ }^{\text {e }}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Lower | Upper |
| Intercept |  |  |  | -3.428 |  | -4.871 | -1.985 |
| Crossroad ADT (log) | 57.08 |  | - | 0.224 | 1.25 | 0.175 | 0.273 |
| Signal timing | 56.06 | Pretimed | - | 0.063 | 1.06 | -0.259 | 0.384 |
|  |  | Semiactuated | - | 0 |  |  |  |
|  |  | Fully actuated | - | 0.622 | 1.86 | 0.475 | 0.770 |
| Major-road ADT (log) | 50.31 |  | - | 0.503 | 1.65 | 0.387 | 0.620 |
| Signal phasing | 7.13 | Two-phase Multiphase | - | $\begin{gathered} 0 \\ -0.200 \end{gathered}$ | 0.82 | -0.324 | -0.077 |
| Access control on major road | 6.64 | None | 1 | -0.310 | 0.73 | -0.508 | -0.112 |
|  |  | Partial | I | 0 |  |  |  |
| Number of lanes on crossroad | 3.92 | 3 or less | - | -0.130 | 0.88 | -0.238 | -0.022 |
|  |  | 4 or more | - | 0 |  |  |  |
| Average lane width on major road | 3.46 |  | - | -0.053 | 0.95 | -0.100 | -0.006 |
| Major-road right-turn channelization | 3.01 | No free right turns | 1 | -0.115 | 0.89 | -0.225 | -0.006 |
|  |  | Provision for free right turns | I | 0 |  |  |  |
| Number of lanes on major road | 3.44 | 3 or less | - | -0.225 | 0.80 | -0.457 | -0.006 |
|  |  | 4 or 5 | - | -0.130 | 0.88 | -0.257 | -0.003 |
|  |  | 6 or more | - | 0 |  |  |  |

[^7]Table 21. Lognormal Regression Results for Fatal and Injury Accidents


[^8]

| Major road characteristics: | Crossroad characteristics: <br> - No access control | Other: <br> - Average lane width of $3.6 \mathrm{~m}(12 \mathrm{ft})$ |
| :--- | :--- | :--- |
| - 3 Fully-actuated signal timing or less |  |  |
| - No free right turns |  | Multiphase signal phasing |
| -4 or 5 lanes |  |  |

Figure 10. Number of Accidents per Year as a Function of Traffic Volumes for Typical Urban, Four-Leg, Signalized Intersections
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## 4. CONCLUSIONS

The following conclusions were reached as a result of the statistical analysis of relationships between traffic accidents and geometric design features of at-grade intersections conducted in this research.

1. The modeling results for accidents if all collision types are combined are similar to those that were found for multiple-vehicle accidents only, published in FHWA-RD-96-125, "Statistical Models of At-Grade Intersection Accidents." ${ }^{(1)}$
2. The negative binomial and lognormal distributions appear to be better suited to modeling of accident relationships than the normal distribution. As found in the previous study, the form of the statistical distribution selected for modeling any particular type of intersection should be chosen based on a review of the accident frequency distribution for that type of intersection. Due to overdispersion observed in the accident data, the negative binomial distribution was preferred over the Poisson distribution when using a loglinear model.
3. The lognormal and negative binomial regression models developed to represent relationships between accidents of all collision types and intersection geometric design, traffic control, and traffic volume variables explained between 16 and 39 percent of the variability in the accident data.
4. Models developed to predict accidents for all severity levels combined generally performed slightly better than did models for fatal and injury accidents.
5. In all regression models, the major-road ADT and crossroad ADT variables accounted for most of the variability in accident data that was explained by the models. Generally, geometric design variables accounted for only a small additional portion of the variability.
6. For rural, three- and four-leg, STOP-controlled intersections and urban, three-leg, STOP-controlled intersections, the geometric design features of at-grade intersections whose effects on safety were statistically significant in the negative binomial regression models included number of lanes on major road, presence of major-road left-turn prohibition, type of access control on major road, width of major-road outside shoulder, presence of major-road and crossroad right-turn channelization, design speed of major road, presence of a median, presence of major-road left-turn channelization, and average lane width on major road. The type of the terrain, functional class of major road, and presence of lighting at the intersection were also found to be statistically significant. In some cases, however, the observed effects on accidents of the geometric design and other variables identified above were in the opposite direction to that expected.
7. For urban, four-leg, signalized and STOP-controlled intersections, the lognormal distribution was found to be an appropriate choice for modeling of intersection accidents. These urban intersections experienced many more accidents than the other types of intersection evaluated, and only a small number of them experienced no accidents in the 3-year period. Geometric design features whose effects on safety were found to be statistically significant included number of lanes on major
road and crossroad, width of outside shoulder on major road, average lane width on major road, presence of major-road and crossroad right-turn channelization, presence of major-road left-turn prohibition, design speed of major road, and access control on major road. Traffic control features that were significant at signalized intersections included signal timing and signal phasing. The functional class of the major road and the presence of lighting at the intersection were also found to be statistically significant in some models. In some cases, however (as mentioned above), the observed effects on accidents of the above-identified variables were in the direction opposite that expected.
8. While the models presented in this report are the best that can be developed from the available data, they do not appear to be of direct use to practitioners. The models do not include effects for all geometric variables of potential interest to highway designers, and some of the effects they do include are in a direction opposite to that expected. Furthermore, the goodness of fit of the models is not as high as would be desired. Therefore, the models presented here are appropriate as a guide to future research, but do not appear appropriate for direct application in the field.

## APPENDIX ACCIDENT TYPE AND SEVERITY DISTRIBUTIONS

Tables 22 through 26 present distributions of accident type and severity for the 5 intersection types whose accident experience has been modeled in this report. For multiplevehicle accidents, the accident type distribution is based primarily on standard Caltrans categories for collision type. However, all collisions that involve one or more left-turning or U-turning vehicles have been classified as left-turn accidents, and all collisions that involve one or more right-turning vehicles (but no left- or U-turning vehicles) have been classified as right-turn collisions. For single-vehicle accidents, the collision type has been based on standard Caltrans data for type of collision, movement preceding collision, and object struck. Accident severity is classified into three categories based on the most serious injury sustained in the accident: fatal, injury, and property-damage-only. Data were not available to subdivide injury accidents further by severity level.

Tables 22 through 26 include all accidents that occurred during a 3-year period at the intersections whose accident experience has been modeled in this report. The multiplevehicle accidents shown in the tables are the accidents that were used in development of the models presented in Report No. FHWA-RD-96-125. ${ }^{(1)}$

Table 22. Distribution of Accident Type and Accident Severity for
Rural, Four-Leg, STOP-Controlled Intersections Rural, Four-Leg, STOP-Controlled Intersections

| Accident Type | Number (percentage) of accidents by severity level |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Fatal |  | Injury |  | Property damage only |  | Total |  |
| Single-Vehicle Accidents |  |  |  |  |  |  |  |  |
| Ran off road | 4 | (2.6) | 28 | (1.1) | 27 | (0.9) | 59 | (1.0) |
| Overturned in road | 1 | (0.7) | 27 | (1.0) | 21 | (0.7) | 49 | (0.9) |
| Other noncollision | 0 | (0.0) | 18 | (0.7) | 73 | (2.5) | 91 | (1.6) |
| Collision with parked car | 1 | (0.7) | 14 | (0.5) | 81 | (2.8) | 96 | (1.7) |
| Collision with train | 0 | (0.0) | 0 | (0.0) | 0 | (0.0) | 0 | (0.0) |
| Collision with pedestrian | 0 | (0.0) | 0 | (0.0) | 0 | (0.0) | 0 | (0.0) |
| Collision with bicycle | 0 | (0.0) | 1 | (0.0) | 0 | (0.0) | 1 | (0.0) |
| Collision with animal | 0 | (0.0) | 4 | (0.2) | 2 | (0.1) | 6 | (0.1) |
| Collision with fixed object | 3 | (2.0) | 81 | (3.1) | 189 | (6.6) | 273 | (4.8) |
| Other single-vehicle collision | 4 | (2.6) | 81 | (3.1) | 113 | (3.9) | 198 | (3.5) |
| Total single-vehicle accidents | 13 | (8.5) | 254 | (9.7) | 506 | (17.6) | 773 | (13.7) |
| Multiple-Vehicle Accidents |  |  |  |  |  |  |  |  |
| Head-on collision | 6 | (3.9) | 27 | (1.0) | 19 | (0.7) | 52 | (0.9) |
| Sideswipe collision | 1 | (0.7) | 39 | (1.5) | 130 | (4.5) | 170 | (3.0) |
| Rear-end collision | 3 | (2.0) | 251 | (9.6) | 369 | (12.8) | 623 | (11.1) |
| Right-angle collision | 85 | (55.6) | 1,000 | (38.4) | 671 | (23.4) | 1,756 | (31.2) |
| Right-turn collision | 1 | (0.7) | 84 | (3.2) | 226 | (7.9) | 311 | (5.5) |
| Left-turn collision | 34 | (22.2) | 816 | (31.3) | 840 | (29.2) | 1,690 | (30.0) |
| Other multiple-vehicle collision | 10 | (6.5) | 135 | (5.2) | 111 | (3.9) | 256 | (4.5) |
| Total multiple-vehicle accidents | 140 | (91.5) | 2,352 | (90.3) | 2,366 | (82.4) | 4,858 | (86.3) |
| Total Accidents | 153 | (100.0) | 2,606 | (100.0) | 2,872 | (100.0) | 5,631 | (100.0) |

Note: Numbers in parentheses are column percentages.

Table 23. Distribution of Accident Type and Accident Severity for Rural, Three-Leg, STOP-Controlled Intersections

| Accident Type | Number (percentage) of accidents by severity level |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Fatal |  | Injury |  | Property damage only |  | Total |  |
| Single-Vehicle Accidents |  |  |  |  |  |  |  |  |
| Ran off road | 5 | (5.1) | 84 | (3.0) | 42 | (1.2) | 131 | (2.0) |
| Overturned in road | 1 | (1.0) | 73 | (2.6) | 35 | (1.0) | 109 | (1.7) |
| Other noncollision | 1 | (1.0) | 46 | (1.6) | 85 | (2.4) | 132 | (2.1) |
| Collision with parked car | 0 | (0.0) | 34 | (1.2) | 81 | (2.3) | 115 | (1.8) |
| Collision with train | 0 | (0.0) | 0 | (0.0) | 0 | (0.0) | 0 | (0.0) |
| Collision with pedestrian | 0 | (0.0) | 0 | (0.0) | 0 | (0.0) | 0 | (0.0) |
| Collision with bicycle | 0 | (0.0) | 0 | (0.0) | 1 | (0.0) | 1 | (0.0) |
| Collision with animal | 0 | (0.0) | 3 | (0.1) | 9 | (0.3) | 12 | (0.2) |
| Collision with fixed object | 5 | (5.1) | 196 | (7.0) | 294 | (8.4) | 495 | (7.7) |
| Other single-vehicle collision | 11 | (11.1) | 256 | (9.1) | 268 | (7.7) | 535 | (8.4) |
| Total single-vehicle accidents | 23 | (23.2) | 692 | (24.7) | 815 | (23.3) | 1,530 | (23.9) |
| Multiple-Vehicle Accidents |  |  |  |  |  |  |  |  |
| Head-on collision | 12 | (12.1) | 74 | (2.6) | 36 | (1.0) | 122 | (1.9) |
| Sideswipe collision | 2 | (2.0) | 52 | (1.9) | 231 | (6.6) | 285 | (4.5) |
| Rear-end collision | 4 | (4.0) | 391 | (13.9) | 601 | (17.2) | 996 | (15.6) |
| Right-angle collision | 8 | (8.1) | 212 | (7.6) | 233 | (6.7) | 453 | (7.1) |
| Right-turn collision | 1 | (1.0) | 107 | (3.8) | 278 | (8.0) | 386 | (6.0) |
| Left-turn collision | 36 | (36.4) | 1,129 | (40.2) | 1,172 | (33.5) | 2,337 | (36.5) |
| Other multiple-vehicle collision | 13 | (13.1) | 149 | (5.3) | 128 | (3.7) | 290 | (4.5) |
| Total multiple-vehicle accidents | 76 | (76.8) | 2,114 | (75.3) | 2,679 | (76.7) | 4,869 | (76.1) |
| Total Accidents | 99 | (100.0) | 2,806 | (100.0) | 3,494 | (100.0) | 6,399 | (100.0) |

Note: Numbers in parentheses are column percentages.

Table 24. Distribution of Accident Type and Accident Severity for Urban, Four-Leg, STOP-Controlled Intersections

| Accident Type | Number (percentage) of accidents by severity level |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Fatal |  | Injury |  | Property damage only |  | Total |  |
| Single-Vehicle Accidents |  |  |  |  |  |  |  |  |
| Ran off road | 0 | (0.0) | 8 | (0.2) | 10 | (0.2) | 18 | (0.2) |
| Overturned in road | 0 | (0.0) | 38 | (0.9) | 9 | (0.2) | 47 | (0.5) |
| Other noncollision | 0 | (0.0) | 40 | (0.9) | 93 | (1.7) | 133 | (1.3) |
| Collision with parked car | 3 | (3.9) | 81 | (1.9) | 351 | (6.3) | 435 | (4.4) |
| Collision with train | 0 | (0.0) | 0 | (0.0) | 0 | (0.0) | 0 | (0.0) |
| Collision with pedestrian | 0 | (0.0) | 1 | (0.0) | 0 | (0.0) | 1 | (0.0) |
| Collision with bicycle | 0 | (0.0) | 1 | (0.0) | 1 | (0.0) | 2 | (0.0) |
| Collision with animal | 0 | (0.0) | 0 | (0.0) | 0 | (0.0) | 0 | (0.0) |
| Collision with fixed object | 1 | (1.3) | 56 | (1.3) | 162 | (2.9) | 219 | (2.2) |
| Other single-vehicle collision | 0 | (0.0) | 115 | (2.7) | 225 | (4.0) | 340 | (3.4) |
| Total single-vehicle accidents | 4 | (5.2) | 340 | (7.9) | 851 | (15.2) | 1,195 | (12.0) |
| Multiple-Vehicle Accidents |  |  |  |  |  |  |  |  |
| Head-on collision | 0 | (0.0) | 31 | (0.7) | 26 | (0.5) | 57 | (0.6) |
| Sideswipe collision | 0 | (0.0) | 82 | (1.9) | 361 | (6.5) | 443 | (4.4) |
| Rear-end collision | 1 | (1.3) | 989 | (22.9) | 1,249 | (22.3) | 2,239 | (22.4) |
| Right-angle collision | 21 | (27.3) | 870 | (20.1) | 927 | (16.6) | 1,818 | (18.2) |
| Right-turn collision | 1 | (1.3) | 255 | (5.9) | 417 | (7.5) | 673 | (6.7) |
| Left-turn collision | 14 | (18.2) | 1,201 | (27.8) | 1,499 | (26.8) | 2,714 | (27.2) |
| Other multiple-vehicle collision | 36 | (46.8) | 550 | (12.7) | 264 | (4.7) | 850 | (8.5) |
| Total multiple-vehicle accidents | 73 | (94.8) | 3,978 | (92.1) | 4,743 | (84.8) | 8,794 | (88.0) |
| Total Accidents | 77 | (100.0) | 4,318 | (100.0) | 5,594 | (100.0) | 9,989 | (100.0) |

Note: Numbers in parentheses are column percentages.

Table 25. Distribution of Accident Type and Accident Severity for Urban, Three-Leg, STOP-Controlled Intersections

| Accident Type | Number (percentage) of accidents by severity level |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Fatal |  | Injury |  | Property damage only |  | Total |  |
| Single-Vehicle Accidents |  |  |  |  |  |  |  |  |
| Ran off road | 2 | (1.8) | 15 | (0.3) | 12 | (0.1) | 29 | (0.2) |
| Overturned in road | 0 | (0.0) | 52 | (0.9) | 14 | (0.2) | 66 | (0.5) |
| Other noncollision | 1 | (0.9) | 56 | (1.0) | 111 | (1.4) | 168 | (1.2) |
| Collision with parked car | 2 | (1.8) | 105 | (1.8) | 501 | (6.2) | 608 | (4.4) |
| Collision with train | 0 | (0.0) | 0 | (0.0) | 0 | (0.0) | 0 | (0.0) |
| Collision with pedestrian | 0 | (0.0) | 1 | (0.0) | 0 | (0.0) | 1 | (0.0) |
| Collision with bicycle | 0 | (0.0) | 2 | (0.0) | 1 | (0.0) | 3 | (0.0) |
| Collision with animal | 0 | (0.0) | 4 | (0.1) | 6 | (0.1) | 10 | (0.1) |
| Collision with fixed object | 8 | (7.1) | 114 | (2.0) | 245 | (3.0) | 367 | (2.6) |
| Other single-vehicle collision | 10 | (8.9) | 216 | (3.8) | 439 | (5.4) | 665 | (4.8) |
| Total single-vehicle accidents | 23 | (20.5) | 565 | (9.9) | 1,329 | (16.5) | 1,917 | (13.8) |
| Multiple-Vehicle Accidents |  |  |  |  |  |  |  |  |
| Head-on collision | 7 | (6.3) | 69 | (1.2) | 43 | (0.5) | 119 | (0.9) |
| Sideswipe collision | 2 | (1.8) | 141 | (2.5) | 684 | (8.5) | 827 | (6.0) |
| Rear-end collision | 5 | (4.5) | 1,710 | (30.1) | 2,370 | (29.4) | 4,085 | (29.5) |
| Right-angle collision | 7 | (6.3) | 414 | (7.3) | 584 | (7.2) | 1,005 | (7.2) |
| Right-turn collision | 1 | (0.9) | 381 | (6.7) | 599 | (7.4) | 981 | (7.1) |
| Left-turn collision | 26 | (23.2) | 1,813 | (31.9) | 2,190 | (27.1) | 4,029 | (29.1) |
| Other multiple-vehicle collision | 41 | (36.6) | 597 | (10.5) | 268 | (3.3) | 906 | (6.5) |
| Total multiple-vehicle accidents | 89 | (79.5) | 5,125 | (90.1) | 6,738 | (83.5) | 11,952 | (86.2) |
| Total Accidents | 112 | (100.0) | 5,690 | (100.0) | 8,067 | (100.0) | 13,869 | (100.0) |

Note: Numbers in parentheses are column percentages.

Table 26. Distribution of Accident Type and Accident Severity for
Urban, Four-Leg, Signalized Intersections

| Accident Type | Number (percentage) of accidents by severity level |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Fatal |  | Injury |  | Property damage only |  | Total |  |
| Single-Vehicle Accidents |  |  |  |  |  |  |  |  |
| Ran off road | 0 | (0.0) | 9 | (0.1) | 7 | (0.0) | 16 | (0.1) |
| Overturned in road | 0 | (0.0) | 95 | (0.8) | 30 | (0.2) | 125 | (0.4) |
| Other noncollision | 0 | (0.0) | 65 | (0.5) | 92 | (0.5) | 157 | (0.5) |
| Collision with parked car | 1 | (1.0) | 56 | (0.5) | 310 | (1.7) | 367 | (1.2) |
| Collision with train | 0 | (0.0) | 0 | (0.0) | 0 | (0.0) | 0 | (0.0) |
| Collision with pedestrian | 0 | (0.0) | 3 | (0.0) | 0 | (0.0) | 3 | (0.0) |
| Collision with bicycle | 0 | (0.0) | 2 | (0.0) | 3 | (0.0) | 5 | (0.0) |
| Collision with animal | 0 | (0.0) | 0 | (0.0) | 4 | (0.0) | 4 | (0.0) |
| Collision with fixed object | 2 | (2.1) | 105 | (0.8) | 399 | (2.2) | 506 | (1.7) |
| Other single-vehicle collision | 9 | (9.3) | 237 | (1.9) | 768 | (4.2) | 1,014 | (3.3) |
| Total single-vehicle accidents | 12 | (12.4) | 572 | (4.6) | 1,613 | (8.9) | 2,197 | (7.2) |
| Multiple-Vehicle Accidents |  |  |  |  |  |  |  |  |
| Head-on collision | 1 | (1.0) | 57 | (0.5) | 61 | (0.3) | 119 | (0.4) |
| Sideswipe collision | 0 | (0.0) | 253 | (2.0) | 1,446 | (8.0) | 1,699 | (5.6) |
| Rear-end collision | 7 | (7.2) | 4,405 | (35.5) | 6,163 | (34.6) | 10,575 | (34.6) |
| Right-angle collision | 21 | (21.6) | 1,803 | (14.5) | 1,991 | (11.0) | 3,815 | (12.5) |
| Right-turn collision | 5 | (5.2) | 993 | (8.0) | 1,730 | (9.6) | 2,728 | (8.9) |
| Left-turn collision | 19 | (19.6) | 3,298 | (26.6) | 4,305 | (23.8) | 7,622 | (24.9) |
| Other multiple-vehicle collision | 32 | (33.0) | 1,021 | (8.2) | 795 | (4.4) | 1,848 | (6.0) |
| Total multiple-vehicle accidents | 85 | (87.6) | 11,830 | (95.4) | 16,491 | (91.1) | 28,406 | (92.8) |
| Total Accidents | 97 | (100.0) | 12,402 | (100.0) | 18,104 | (100.0) | 30,603 | (100.0) |

Note: Numbers in parentheses are column percentages.

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[^0]:    All variables significant at the 90 percent confidence level or higher effect of the variable; with 1 degree of freedom for continuous variables; with (p-1) degrees of freedom for categorical variables with $p$ levels

    Direction of effect: I = Inverse of expected direction
    Relative effect of unit change in the variable on the expected number of accidents, equals exp(coefficient)
    90 percent lower and upper confidence limits of the estimated coefficient
    e 90 percent lower and upper confidence limits of the estimated coefficient

[^1]:    Note: This analysis is based on the set of 1,434 intersections for which summary statistics are shown in Table 2.
    b Chi-square likelihood ratio statistic for testing the significance of the effect of the variable; with 1 degree of freedom for continuous variables; with ( $p-1$ ) degrees of freedom for categorical variables with $p$ levels

    Relative effect of unit change in the variable on the expected number of accidents, equals exp(coefficient)
    90 percent lower and upper confidence limits of the estimated coefficient

[^2]:    Note: This analysis is based on the set of 2,692 intersections for which summary statistics are shown in Table 6. ${ }^{\text {a }}$
    b Chi-square likelihood ratio statistic for ( $p-1$ ) degrees of freedom for categorical variables with $p$ levels
    d Relative effect of unit change in the variable on the expected number of accidents, equals exp(coefficient) 90 percent lower and upper confidence limits of the estimated coefficient

[^3]:    Note: This analysis is based on the set of 1,342 intersections for which summary statistics are shown in Table 10.
    b Chi-square likelihood ratio statistic for testing the significance of the effect of the variable; with 1 degree of freedom for continuous variables; with ( $\mathrm{p}-1$ ) degrees of freedom for categorical variables with $p$ levels
    d Relative effect of unit change in the variable on the expected number of accidents, equals exp(coefficient) e 90 percent lower and upper confidence limits of the estimated coefficient

[^4]:    Note: This analysis is based on the set of 1,342 intersections for which summary statistics are shown in Table 10.
    b Al variables significant at the 90 percencel or higher (p-1) degrees of freedom for categorical variables with $p$ levels
    c Direction of effect: I = Inverse of expected direction
    d Relative effect of unit change in the variable on the expected number of accidents, equals exp(coefficient)

[^5]:    Note: This analysis is based on the set of 3,057 intersections for which summary statistics are shown in Table 14. a All variables significant at the 90 percent confidence level or higher

    Chi-square likelihood ratio statistic for testing the significance of the effect of the variable; with 1 degree of freedom for continuous variables; with
    Direction of effect: I = Inverse of expected direction
    d Relative effect of unit change in the variable on the expected number of accidents, equals exp(coefficient)
    e 90 percent lower and upper confidence limits of the estimated coefficient

[^6]:    Note: This analysis is based on the set of 3,057 intersections for which summary statistics are shown in Table 14.
    b Chi-square likelihood ratio statistic for testing the significance of the effect of the variable; with 1 degree of freedom for continuous variables; with (p-1) degrees of freedom for categorical variables with $p$ levels
    c Direction of effect: I = Inverse of expected direction
    d Relative effect of unit change in the variable on the expected number of accidents, equals exp(coefficient)
    e 90 percent lower and upper confidence limits of the estimated coefficient

[^7]:    Note: This analysis is based on the set of 1,306 intersections for which summary statistics are shown in Table 18.
    b Chi-square likelihood ratio statistic for testing the significance of the effect of the variable; with 1 degree of freedom for continuous variables; with ( $p-1$ ) degrees of freedom for categorical variables with $p$ levels
    c Direction of effect: I = Inverse of expected direction
    d Relative effect of unit change in the variable on the expected number of accidents, equals exp(coefficient)
    e 90 percent lower and upper confidence limits of the estimated coefficient

[^8]:    Note: This analysis is based on the set of 1,306 intersections for which summary statistics are shown in Table 18.
    ${ }^{b}$ Chi-square likelihood ratio statistic for testing the significance of the effect of the variable; with 1 degree of freedom for continuous variables; with ( $p-1$ ) degrees of freedom for categorical variables with p levels
    c Direction of effect: I = Inverse of expected direction
    d Relative effect of unit change in the variable on the expected number of accidents, equals exp(coefficient)
    e 90 percent lower and upper confidence limits of the estimated coefficient

