# DEVELOPING A METHOD TO IDENTIFY HORIZONTAL CURVE SEGMENTS WITH HIGH CRASH OCCURRENCES USING THE HAF ALGORITHM 

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16. Abstract

Crashes occur every day on Utah's highways. Curves can be particularly dangerous as they require driver focus due to potentially unseen hazards. Often, crashes occur on curves due to poor curve geometry, a lack of warning signs, or poor surface conditions. This can create conditions in which vehicles are more prone to leave the roadway, and possibly roll over. These types of crashes are responsible for many severe injuries and a few fatalities each year, which could be prevented to a large degree. This highlights a need for identification of curves with high crash occurrences.

The Horizontal Alignment Finder (HAF) Algorithm created by a BYU team in 2014 was improved to achieve 87-100 percent accuracy in finding curved segments of UDOT's highways, depending on highway type. A tool was then developed through Microsoft Excel Visual Basic (VBA) to sort through curve and crash data to determine the number of severe and total crashes that occurred along each curve. The tool displays a list of curves with high crash occurrences. The user can sort curves by several different parameters, including various rates and numbers of crashes. Many curves with high crash rates have already been identified, some of which will be shown in this report. This tool will help UDOT determine which highway curves warrant improvement projects.

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## LIST OF ACRONYMS

| AADT | Annual Average Daily Traffic |
| :--- | :--- |
| AASHTO | American Association of State Highway and Transportation Officials |
| AGRC | Automated Geographic Reference Center |
| BYU | Brigham Young University |
| CARS | Curve Advisory Reporting Service |
| DBBI | Digital Ball-Bank Indicator |
| DUI | Driving Under the Influence |
| FHWA | Federal Highway Administration |
| GIS | Geographic Information System |
| GPS | Global Positioning System |
| HAF | Horizontal Alignment Finder |
| LiDAR | Light Detection and Ranging |
| MP | Milepost |
| MVMT | Million Vehicle-Miles Travelled |
| PC | Point of Curvature |
| PT | Point of Tangency |
| TLTW | Two-Lane Two-Way |
| UCPM | Utah Crash Prediction Model |
| UCSM | Utah Crash Severity Model |
| UDOT | Utah Department of Transportation |
| VBA | Visual Basic for Applications |
| VMT | Vehicle-Miles Travelled |

## EXECUTIVE SUMMARY

The purposes of this research can be summarized in three main objectives, including testing an algorithm designed to identify curves on rural two-lane, two-way highways for its accuracy on other highway types, improving the overall accuracy of the algorithm, and writing a new algorithm to combine curve data with crash data in order to generate lists of curves with their respective crash histories.

In the testing phase, the current algorithm was found to correctly identify highway curves with 71-96 percent accuracy, depending on highway type. Calibration was done by comparing the algorithm's results with measurements obtained from drawing curves in AutoCAD across satellite imagery. Additionally, the algorithm was able to calculate curve length with 91-96 percent accuracy. From these results, it was determined that the core concept of the algorithm did not need to be modified in order to accommodate different highway types.

The improvements to the algorithm involved targeting six specific errors. These improvements were found to increase the accuracy of curve identification to 87-100 percent, depending on highway type. Curve length calculation accuracy was improved to 97-98 percent. In addition, the algorithm was modified in order to run newer data that it could not accept previously due to changes in the data's formatting from 2014 to 2015. Three of the six errors were effectively reduced or eliminated through the improvements outlined in this report.

Finally, a new program was developed to combine curve, roadway, and crash data in order to prepare the way for future analysis. The roadway data included annual average daily traffic, functional class, speed limit, urban code, and lane parameters. These parameters were applied to each curve to determine which of them had an effect on crash rates. Total and severe crashes, as well as their corresponding crash rates, were calculated for each curve segment. Through this process, highway curves with high crash occurrences were identified. This list is intended for further crash prediction and modeling analysis.

### 1.0 INTRODUCTION

### 1.1 Problem Statement

As part of the previous research funded by UDOT, an algorithm called the Horizontal Alignment Finder (HAF) was developed to identify horizontal curves along with their points of curvature (PC), points of tangency (PT), and radii (Cook et al. 2015). This algorithm takes advantage of the horizontal alignment data provided by UDOT's light detection and ranging (LiDAR)-based asset management program. The raw LiDAR data were highly segmented and were not ready to be used for crash prediction modeling. The HAF Algorithm was created as a means of identifying horizontal curves based on post-processing of the LiDAR data. Properly locating the PC, PT, and radius is important for crash prediction modeling and curve segment hot spot identification.

For the past several years, BYU researchers have developed Bayesian-based crash prediction models, including the Utah Crash Prediction Model (UCPM) and Utah Crash Severity Model (UCSM). These advanced statistical models account for the uncertainty inherent with random crash events and help safety engineers identify and prioritize hot spots. Prior to the HAF Algorithm research, there was no automated or semi-automated method to identify whether hot spots identified by the models were part of curve segments. The HAF Algorithm can help safety engineers identify horizontal curve segments with high crash histories on state highways.

The HAF Algorithm was originally developed for rural two-lane, two-way (TLTW) highways. Hence, it was necessary to test its robustness for other highway types in both rural and urban areas. The accuracy of the original HAF Algorithm was approximately 85 percent. An error value of 15 percent is an issue when applied to the entire state highway system. The original HAF Algorithm requires human intervention to make sure it correctly identified the horizontal curve segments.

The purposes of the research described in this paper were to improve accuracy of the original HAF Algorithm, test its application to types of roadways other than rural TLTW, and create a new tool for combining curve and crash data to produce a list of curves with high crash occurrences.

### 1.2 Objectives

The study objectives were to:

- Test if the current HAF Algorithm, developed to analyze horizontal curves on rural TLTW highways, can be used for all other types of highways owned by UDOT
- Modify the current HAF Algorithm to make it useable for other types of highways owned by UDOT
- Improve the HAF Algorithm from its current level of 85 percent accuracy
- Develop a methodology to identify curved segments of state highways with high crash occurrences using the improved HAF Algorithm
- List horizontal curve segments of state highways with high crash occurrences and identify any pertinent physical features such as curve radius, curve length, superelevation, and annual average daily traffic (AADT).


### 1.3 Scope

This project can be broken down into three primary tasks:

- Calibrating the current HAF Algorithm to test whether or not it works for all highway types
- Improving accuracy of the original HAF Algorithm
- Combining the final curve, roadway, and to generate a list of curve segments with high crash occurrences.


### 1.4 Outline of Report

This report begins in Chapter 2 with a comprehensive summary of previous research done on the topic of identifying highway curves. This summary includes methods of data collection most appropriate for accurately covering a large road network. It also includes a review of different methods of identifying curves and determining relevant curve parameters. An overview of the methodology used for this research is presented in Chapter 3.

Summaries of the calibration process and results follow in Chapter 4 and 5, respectively. Chapter 4 details how the HAF Algorithm results were compared with measured results from satellite imagery side-by-side. It also describes how curves from different highway types were analyzed separately. Accuracy and error results are then discussed in Chapter 5. Chapter 6 then presents the reasoning for a determination that the core concept of the HAF Algorithm does not require modifications to accommodate other highway types.

The report then covers the sources of error and the improvements made to the HAF Algorithm in Chapter 7. Six types of error are discussed that provided a basis for making changes to the algorithm. This discussion also includes error sources and the fixes made. The results of the improvements are presented in Chapter 8, with a comparison of the accuracy of the original algorithm to the enhanced one.

Finally, an outline of the process that was used to combine curve, roadway and crash data is presented in Chapter 9, along with an examination of a few particular curve segments of interest. This chapter contains information about the VBA program that was created to combine the data, as well as a few lists of curves with high crash occurrences. This chapter concludes with a summary of the information gained from the lists.

### 2.0 LITERATURE REVIEW

### 2.1 Overview

Several studies have been done on identifying highway curvature through a variety of methods. This review is divided into three separate subjects, including data collection, curve identification methods, and determination of other curve parameters.

### 2.2 Data Collection

Various methods have been used in data collection to map road networks. The most common of these is the use of a vehicle-mounted global positioning system (GPS) sensor, but other approaches are viable as well, including data collection by LiDAR, visual methods that include mapping from satellite imagery and still photos, and inertial measurement devices.

### 2.2.1 GPS

GPS sensors are widely-used in collecting horizontal alignment data, which makes them useful in determining geometric parameters. Many road databases already exist created from GPS data for use in GIS software, especially in Europe (Svenson et al. 2016, Garach et al. 2014, Andrášik et al. 2013). An example of the road database in Sweden is shown in Figure 2.1. As can be seen, mapping horizontal alignment data relies on a series of data points, or points where data were collected, as shown on the right of Figure 2.1.


Figure 2.1 Swedish Road Database (Svenson et al. 2016)

Collecting GPS data also works well due to its low cost and widespread application. Carlson et al. (2005) performed a study that compared eight different methods of mapping horizontal alignments including using inertial measurement devices and traditional surveying. The study found that using a GPS would be most beneficial to researchers due to the fact that it is relatively inexpensive and that it works well over a large network of roads. It is also fairly accurate, and the results that were obtained came close to data taken from plan sheets. GPS data collection can also be safe in comparison to traditional surveying methods as work crews are not required to put themselves in harm's way when a GPS device is mounted on a moving vehicle (Williams and Hawkins 2011).

One disadvantage to using GPS data is that the data points follow the path of the data collection vehicle rather than the road itself, although some studies have been done to determine what paths drivers take (Imran et al. 2006). This means that the calculated alignment is subject to change depending on whether or not the driver kept to the center of the lane or whether lane changes were forced due to passing maneuvers, road construction, or other hazards (OseiAsamoah 2015). Another disadvantage is that GPS data are often inconsistent, especially in the vertical direction (Svenson et al. 2016, Williams and Hawkins 2011, Jiménez et al. 2009). This makes it difficult to measure vertical curve parameters and means that multiple runs must be taken in order for the results to be very accurate.

Overall, GPS data collection works well compared to traditional surveying methods because of its low cost, accessibility, and ease of use. Traditional methods require a lot of time and effort when applied to large-scale road networks, while GPS typically requires the use of a single vehicle driving across a large area. In addition, GPS data can be used to map horizontal alignments on rail networks (Tong et al. 2010).

### 2.2.2 LiDAR

LiDAR data collection is the method used in this study. A point cloud image from UDOT is shown in Figure 2.2. Collection is done through driving a vehicle across a road or road network just as it is in GPS-based data collection, which means it works well for large-scale studies. LiDAR technology is fairly new in transportation research, and its potential has not yet been fully explored (Cook et al. 2015).


Figure 2.2 LiDAR Point Cloud Image (Ellsworth, P. 2013)

One advantage that LiDAR data have over GPS data is that they represent the path of the road itself rather than the path taken by a single driver. This allows for increased accuracy in determining horizontal curve parameters. Kim et al. (2008) determined in a study in South Korea that terrestrial laser scanning, which is similar to LiDAR, is more accurate than most other available methods.

Mapping roadways from LiDAR data is done through edge detection. Painted lines on the road are identified and used to approximate a centerline that can be imported into geographic information system (GIS) software. From this centerline, an algorithm can be applied to separate curves from tangents and determine curve parameters such as curvature, radius, and curve length. LiDAR data can also be used to map vertical curves (Svenson et al. 2016).

The primary disadvantage to using LiDAR data in terms of accuracy is that painted lane boundaries are not always parallel to the centerline of a road (Cook et al 2015). This is complicated further due to the fact that lanes and shoulders may taper. Additionally, while it may work well to find true road geometry, it does not reflect the path that drivers actually take.

However, despite these disadvantages, LiDAR remains a viable option for use in safety studies as it works accurately over a large area unlike some other methods of data collection.

### 2.2.3 Visual

Visual means of data collection cover a wide variety of sources, including satellite imagery, photos, and videos. Roads are typically mapped through edge detection, similar to the process used in LiDAR. The primary advantage of these methods is the extremely low cost of the equipment used.

Satellite imagery has been used previously to determine horizontal curve parameters. As it is inexpensive and widely available, multiple studies have been done to determine whether or not it could be used. Unlike other methods of data collection, it does not require driving across large road networks or surveying. Dong et al. (2007) performed a study to map horizontal alignments using satellite imagery and an edge detection algorithm. It found that mapping was semi-automated, or that it required human input. The algorithm cannot detect roadways, and it requires the user to specify a starting point after which the road shape can be followed (Easa et al. 2007). An illustration of the road extraction process is shown in Figure 2.3, where an imagebased program extracts areas with road-like features to approximate a road system. An additional challenge is that trees and other objects often obscure the edge of the pavement, further complicating the process (Zhao et al. 2002). While it works well for small road segments, this method should not be applied across a large road network.


Figure 2.3 Satellite Image Road Extraction (Zhao et al. 2002)

Other studies have been done to map horizontal alignments using still photography. This typically involves photos being taken from a moving vehicle. One advantage to it is that it is very inexpensive and can be done using a simple digital camera without any complicated equipment (Tsai et al. 2010). It works using an edge detection program similar to those used in extracting
curve geometry from satellite imagery. However, it cannot be used efficiently to cover a large road network.

Smartphones have also been used as a means to map horizontal alignments. Higuera de Frutos and Castro (2014) performed a study to determine the effectiveness of smartphones as a low-cost mapping tool. The study found that they were a viable option for larger road networks. Besides the fact that smartphones are so widely used, they also contain a lot of equipment including video recording capability, GPS sensors, and accelerometers. This enables them to map roads similarly to GPS and inertial measurement devices. Its primary disadvantage, however, is its accuracy. The study found that horizontal alignments could be mapped with an average error of 2.2 meters in either direction, which pales in comparison to other, more accurate methods of data collection.

### 2.2.4 Inertial Measurement Devices

Inertial measurement devices, such as ball-bank indicators and accelerometers, are able to map horizontal alignments by collecting data from lateral acceleration. This method works well for short segments on low-speed roads, but cumulative error becomes too great after driving for a distance of about 1500 meters for it to be used properly. When performed on roads with a higher speed limit, the acceptable distance for measurement after which the error becomes too great is reduced significantly (Jiménez 2011).

Ball-bank indicators, which are a type of inertial measurement device, are widely used in the United States. A study performed by Green et al. (2017), using a digital ball-bank indicator (DBBI), found that they provided valuable information for determining advisory speeds on horizontal curves, but that they provided more accurate information when used in conjunction with a GPS sensor. This system that used an inertial measurement device in conjunction with a GPS sensor is called the Curve Advisory Reporting Service (CARS), and a comparison of curve advisory speeds calculated with both methods is shown in Figure 2.4. As can be seen, the calculated advisory speeds differed by as much as 10-15 miles per hour. Jiménez et al. (2009) confirmed that a combination of the two methods might be better by stating that inertial measurement data combined with GPS information have the potential to be very accurate.


Figure 2.4 Absolute Differences in Advisory Speeds Determined with and without GPS Sensor (Green et al. 2017)

### 2.3 Methods of Curve Identification

Once the data points have been collected and run through a mapping program, the next step is to run a program to separate curve segments from tangent segments. The three dominant methods to do this include curve identification through change in heading, development of a spline approximation, and identification of a curve through geometric parameters such as radius or length.

### 2.3.1 Heading Change

Several algorithms differentiate curves from tangents by analyzing direction change beyond a certain threshold, an example of which is shown in Figure 2.5. Camacho-Torregrosa et al. (2015) compared different methods of identifying horizontal curvature along highway segments and found that the heading change method was the most accurate among the tested methods, did not require smoothing, and was less susceptible to measurement errors. While the radius values extracted from this method were found to be consistent with those calculated by other methods, the curve length was significantly more accurate, as shown in Figure 2.6.


Figure 2.5: Curve Identification via Heading Change (Li et al. 2015)


Figure 2.6 Heading Change v. Curvature Method (Camacho-Torregrosa et al. 2015)

A study done by Li et al. (2012) developed an algorithm that was able to identify curves and tangent segments (not their parameters) with 97 percent accuracy. The disadvantage to this method, however, is that direction changes are frequent in tangent sections, which means that additional care must be taken in order to distinguish curves from tangents (Xu and Wei 2016). However, if this issue can be overcome, the heading change method has the potential to identify curves accurately over a large network (Li et al. 2015).

### 2.3.2 Spline Approximation

Spline approximation differs from other methods in that it does not identify curves themselves, but rather aids in mapping them. Splines are mathematical functions that provide a
smooth, fluid connection between different points. This method works well in matching a road centerline between two directions of travel and in creating a smooth, continuous curve (Castro et al. 2006, Ben-Arieh et al. 2004). Two illustrations of this compared with an actual road design are shown in Figure 2.7 and Figure 2.8, with a vertical and horizontal alignment, respectively.


Figure 2.7 Comparison of Spline with Existing Vertical Alignment (Ben-Arieh et al. 2004)


Figure 2.8 Comparison of Existing Horizontal Alignment with Spline Centerline (Castro et al. 2006)

The issue with spline functions, however, is that it becomes more difficult to extract curve parameters from them and it requires additional algorithms to do so. Garach et al. (2014)
performed a study in which curve parameters were determined from mapping done via a spline function. Spiral and circular curves were approximated using trapezoids, and the results returned an average error rate of less than 10 percent. Splines work well for mapping horizontal alignments, but not as well for separating curves from tangents and identifying curve geometry. Some studies have also been done to determine curve geometry from various fitting algorithms (Bassani et al. 2016).

### 2.3.3 Geometric Curve Parameters

Several studies have been done that differentiate curves from tangents based on geometric parameters. The study that is the basis for this research used this method to identify horizontal curves (Cook et al. 2015). It used a weighting system consisting of three different thresholds including segment length, radius, and a radius/length ratio to determine whether a particular segment was a curve or a tangent, as shown in a flowchart in Figure 2.9. This method worked with 84-93 percent accuracy on TLTW highways.


Figure 2.9 Curve Weighting Diagram (Cook et al. 2015)

Andrásik and Bíl (2014) used a simple radius threshold of 200 meters with an overall success rate of 90 percent in a study done in the Czech Republic. An illustration of this is shown in Figure 2.10. Ai and Tsai (2015) performed a similar study in the state of Georgia and
produced the same identification accuracy rate. Geometric parameter calculation accuracy usually depends on the length of the curve (Bogenreif et al. 2012). The main issue with this method, however, is that it is difficult to differentiate intersections from mountain curves with small radius values. However, identifying curves from threshold values, according to these studies, seems to be a viable option. The advantage to this method is that thresholds can be adjusted easily to fit a given set of circumstances (Cook et al. 2015).


Figure 2.10 A Circular Curve Determined by its Radius and Angle (Andrášik and Bíl 2014)

### 2.4 Other Curve Parameters

Studies have been performed on methods to gather roadway parameters other than those associated with horizontal curvature. Some studies identified and measured vertical curves, while others measured road superelevation. These studies are summarized below.

### 2.4.1 Vertical Curves

Automatic extraction of vertical alignments can also be useful in safety research. Identifying vertical curves and their characteristics is necessary for determining sight distance (Figure 2.11). This is traditionally done through surveying, but improvements made in technology in recent years allow for faster, more efficient means to do so. Standards have changed in terms of passing sight distance requirements (Williams and Hawkins 2011), which means a method that can be implemented on a large scale is needed to determine which vertical curves do not meet the new requirements.


Figure 2.11 Vertical Sight Distance Diagram (Santiago-Chaparro et al. 2012)

Williams and Hawkins (2011) performed a study in which multiple passes were made in a GPS-equipped vehicle to gain elevation points and construct a vertical alignment using quadratic fitting. Santiago-Chaparro et al. (2012) performed a similar study using photologs as a data collection means. Photologs are similar in nature to Google Streetview, in that photos are taken at set intervals from a vehicle. The difficulty with determining vertical alignments, however, is that mapping them does not work as accurately as mapping horizontal alignments (Svenson et al. 2016). This suggests a need for further research.

### 2.4.2 Superelevation

Several studies have also been done on acquiring superelevation data. This is useful in safety-related research as it is important to know how a road has been designed. Luo et al. (2016) performed a study in which superelevation information was gathered by lasers mounted on the back of a vehicle while GPS and lateral acceleration data were collected simultaneously (Figure 2.12). This method works well for a large road network without using time-consuming traditional surveying methods.


Figure 2.12 Measuring Superelevation (Luo et al. 2016).

The difficulty in measuring superelevation is that when traversing a curve, the chassis of the measuring vehicle is not always parallel to the road surface. This is particularly true in vehicles with softer suspension, and is often difficult to compensate for. Jiménez (2011) performed a study in which superelevation was measured using an inertial measurement device. An algorithm was developed to attempt to compensate for body roll. This was successful, and the data gathered were more accurate.

### 2.5 Chapter Summary

Identifying curve segments accurately is beneficial to safety research. Being able to identify what attributes of a road that contribute to crashes could save many lives. Various viable means of data collection and analysis are available for doing this. GPS, LiDAR, visual, and inertial measurement methods have been reviewed for this purpose. According to the studies included in this literature review, GPS and LiDAR data collection appear to be the best methods for use over a large road network because of their accuracy, widespread use, and convenience over other forms of gathering information.

Identifying curves through change in heading direction and through use of geometric threshold values are both valid methods. The advantage to the heading change method is that it is generally more accurate, while the geometric threshold method is more easily adjustable to fit
specific needs. The original HAF Algorithm is based off this method, and provides a good foundation for further development.

Many studies have also been done to identify other road parameters, such as vertical curve characteristics and superelevation. These are good options for further research into road attributes that may contribute to crashes. From this literature review, it can be seen that valuable research has been done on the topic of horizontal curve identification and that it provides a solid basis from which more can be learned.

### 3.0 METHODOLOGY

### 3.1 Overview

This chapter contains an overview of the methodology behind the research in this report. The methodology consists of three parts, including (1) the calibration of the current HAF Algorithm to determine its errors and whether it works for all highway types, (2) a presentation of the sources of these errors and the improvements made to correct them, and (3) a summary of how the curve data were combined with crash data in a new program.

### 3.2 Calibration

The current HAF Algorithm was calibrated by comparing the calculated parameters of the output file against measured parameters found through overlaying arcs on satellite imagery in AutoCAD. Three primary performance measures were tested, including curve length calculation accuracy, radius calculation accuracy, and curve identification accuracy. A total of 100 segments were chosen at random to test from each highway type, including urban interstate, rural interstate, urban multilane, rural multilane, urban TLTW, and rural TLTW.

### 3.3 HAF Errors and Improvements

During the testing of the current HAF Algorithm, a total of six major errors were found, including curve length miscalculation, curve fragment identification, tangent identification, intersection identification, tangent-curve-tangent errors, and compound curve errors. The details of these errors will be described in Chapter 5. To reduce the number of tangents identified as curves, the code of the HAF Algorithm was altered to implement radius thresholds at a nonlinear scale. To reduce large curve length calculation errors, changes were made to improve the accuracy at which the PC and PT of curves were selected. To reduce the number of intersections identified as curves, an existing ArcMap model was modified to eliminate curves from consideration below a certain radius value if the curves were within certain municipality boundaries.

### 3.4 Crash Data Combination

After the HAF Algorithm was improved, curve data were combined with roadway data and crash data through the use of a new tool. The combination took place by aligning common milepoints and route numbers. The roadway data included AADT, functional classifications, speed limits, urban codes, and the number of through lanes. Some additional measures had to be taken to compensate for segments where data were not available. Individual segments with abnormally high crash rates were then analyzed based on the characteristics of the curves and the types of crashes that occurred on them.

### 3.5 Chapter Summary

To summarize, there are three primary components to the methodology of this study: (1) calibrate the existing HAF Algorithm to see if it works for all highway types, (2) identify the errors of the existing HAF Algorithm and make improvements as necessary to increase overall accuracy, and (3) combine curve data with roadway and crash data to generate a list of curves with high crash occurrences. This is the basic outline of how the study was performed, and these components will be explored in depth in the coming chapters.

### 4.0 HAF ALGORITHM CALIBRATION PROCESS

### 4.1 Overview

This research tested the original HAF Algorithm to determine how well it identifies curves and estimates curve parameters for roadway types other than rural TLTW. Calibration of the algorithm for these other roadway types provided some understanding into how it could be improved. In this calibration process, approximately 100 curve segments were randomly selected for each of six highway categories - urban and rural interstates, urban and rural multilane highways, and urban and rural TLTW highways. 2013 and 2014 Mandli datasets were used in the calibration process. Included in this chapter is an overview of how the program works and the methodology detailing how curve segments were calibrated.

### 4.2 How the HAF Algorithm Works

In order to understand the calibration process of the HAF Algorithm, its workings must be understood first. LiDAR data in a shapefile format provide the algorithm input. The HAF Algorithm itself does not use image detection techniques common in LiDAR data analysis. Rather, it uses lines and curves that have already been post-processed by Mandli (the company performing the LiDAR survey for UDOT). The HAF Algorithm is necessary because the data are fragmented and several segments with slightly different parameters will often be contained within a single curve, making it not ideal for analyzing curves across a vast roadway network. These data contain curve length and radius information about each segment, and the HAF Algorithm's role is to combine and clean up the data to present them in the form of curves and tangents (Cook et al. 2015).

The HAF Algorithm accomplishes this task by analyzing each segment and weighting its parameters as more curve-like or more tangent-like. This means, for example, that segments with large radius values are more likely to be classified as a tangent rather than a curve. Additionally, adjacent curve segments that bend in the same direction are combined into a single curve. The starting point of the first curve segment and the ending point of the last curve segment are
considered to be the PC and PT of the new curve, respectively. It is important to mention that while the algorithm is fully capable of combining segments together from the input data, it is not able to divide segments. This is because the algorithm analyzes data in table form, in which only the starting point and end point of each segment are available rather than continuous location information.

### 4.3 Calibration Procedures

This section contains a comprehensive description of the process involved in calibrating curve segments. It includes filtering the curve shapefile into separate road types, randomizing the samples used, and determining true curve parameters by drawing arcs across satellite imagery in AutoCAD.

### 4.3.1 Determination of Segments to be Used

The first step was to segment the list of curves into separate lists of curves from each highway type. The HAF Algorithm can determine curve parameters but is not able to distinguish between different types of highways. This task was accomplished by using ArcMap's Select by Attributes function. Interstates were filtered by selecting route names corresponding with known interstate routes, as shown in Figure 4.1. Other road types were filtered by using a lanes shapefile from UDOT that shows whether a facility is multilane or not.


Figure 4.1 ArcMap Select by Attributes Function (Esri 2017)

Once this had been done, the selected segments were then exported to an Excel spreadsheet where each segment was assigned a random number through Excel's random number generator function. These segments were sorted in ascending order from the random number assigned to them, which then randomized the segments to get a more accurate representation of the population as a whole. Rural and urban areas were analyzed separately. Urban segments were defined as any highway inside the Salt Lake City (which includes Davis and Weber counties), Provo-Orem, Cedar City, and St. George metropolitan areas. A
municipality shapefile downloaded from the Utah Automated Geographic Reference Center (AGRC) was used to determine which segments fall within those urban boundaries.

### 4.3.2 Comparing Satellite Imagery

After the curve segments were categorized, the next step was to calibrate them. A satellite imagery basemap was applied to the ArcMap file from which the location of a particular curve segment could be determined. The corresponding segment was then found in Google Earth through comparing the two images side-by-side, as shown in Figure 4.2. The Google Earth image is at the top and the ArcMap image is at the bottom. Two pins were then placed on opposite ends of the curve in Google Earth, forming a box from which to take a screenshot and import an image into AutoCAD.

### 4.3.3 Determining Actual Curve Parameters

This screenshot was used as the basis for recreating the curve (see Figure 4.3). A line was then drawn between the two pins in AutoCAD for scaling purposes. The distance between the two pins was measured on Google Earth to find the true distance across the image (see Figure 4.4). The distance obtained from Google Earth divided by the length of the line between the same two points in the pasted image in AutoCAD was used to determine the scale of the image, from which a scaling factor was obtained.


Figure 4.2 Google Earth (a)/ArcMap (b) Comparison (Google 2017, Esri 2017)


Figure 4.3 AutoCAD Image (Autodesk 2017)


Figure 4.4 Google Earth Distance Measurement (Google 2017)

After the image had been scaled, a 3-point arc was drawn in AutoCAD. The PC and PT of the curve were matched as closely as possible to the ones identified in ArcMap (see Figure 4.5). Drawing this arc introduced a potential source of human error as it is difficult to match the exact road centerline. However, it is still a fairly accurate method of determining actual curve parameters.


Figure 4.5 AutoCAD Arc Drawing (Autodesk 2017)

Once the arc was drawn, radius and curve length values were obtained from the properties table as shown on the left of Figure 4.5. These values were then multiplied by the scaling factor obtained earlier to reflect their true measurement. The measured radius and curve length were then compared with the radius and curve length that the HAF Algorithm had calculated to determine the accuracy.

### 4.4 Chapter Summary

In order for the capability of the existing HAF Algorithm to identify curves along all highway types to be evaluated, a calibration process had to be developed. This was done through matching curves determined by the HAF Algorithm to measurements taken from satellite
imagery. Parameters such as radius and curve length were taken into consideration in determining the accuracy of the HAF Algorithm.

### 5.0 TYPES OF ERRORS IN THE ORIGINAL HAF ALGORITHM

### 5.1 Overview

This chapter includes a description of six problems with the existing HAF Algorithm. Some of these errors were known before this research was started, and others were discovered during the process of calibration. The first three errors deal with problems in calculating curve parameters, and the last three entail problems with identification of highway curves. Identifying these problems with the algorithm provided a starting point from which to improve it. These six errors include tangent-curve-tangent, compound curve, curve length calculation, intersection, tangent, and curve fragment errors. Curve length calculation, curve fragment, and intersection errors were reduced significantly, while the tangent error was also reduced to some degree. The improvements made to resolve these errors are detailed in Chapter 7.

### 5.2 Tangent-Curve-Tangent Error

Tangents and curves are often combined into single segment elements in the raw data. This is shown in Figure 5.1, and was found to be fairly common, especially along non-interstate highways. This particular curve segment exists along SR-115 in Spanish Fork. As can be seen, the PC and PT points do not line up where they should. The approximate PC and PT points as judged by the researcher have been marked. In this case, the data fed into the algorithm are flawed. As mentioned previously, the algorithm is not set up for dividing segments, nor can it be modified to do so. Due to this flaw, the actual radius value differs from the calculated values, both from the calibration and the algorithm itself. This shortcoming in the data is difficult to address, as the algorithm assumes all inputs are either a complete curve or a segment of a curve and therefore cannot address combined curve-tangent sections.


Figure 5.1 Tangent-Curve-Tangent Error (Esri 2017)

### 5.3 Compound Curve Error

A second type of error exists in attempting to calibrate compound curves, or multiple curves of different radius values combined together into a single segment. This type of error exists occasionally on mountain roads where broad curves will often be followed by sharp ones, as illustrated in Figure 5.2. This particular segment is on SR-153 near Beaver, UT. As can be seen, the issue is not that tangents are connected to the curve, but rather that there are two distinct curves adjacent to each other. The approximate PC and PT points have again been marked. This makes calibration difficult, as the algorithm is set up to produce simple circular curves, which cannot be fitted properly in a scenario such as this. The HAF Algorithm determines radius values on compound curves through a weighted average, which would be difficult to properly check for accuracy. Fortunately, this type of error is not common.


Figure 5.2 Compound Curve (Esri 2017)

### 5.4 Curve Length Calculation Error

A third type of error can occur when using the HAF Algorithm to calculate curve length. The HAF Algorithm calculates smoothed curve length by summing the individual curve lengths from the segments in the original data. This particular kind of error is not more common in one particular road type than in another. Human error was successfully ruled out in these situations through comparing the calibration's curve length to a rough approximation done by the path component of Google Earth's distance tool. Errors of this type often ranged from 100-500 percent. Table 5.1 contains four examples of this error and as can be seen, the HAF-calculated curve length is much larger than it should be. These errors occurred because the HAF Algorithm identified the wrong milepoints for the PC and PT locations, which is explained in Chapter 7.

Table 5.1 Curve Length Calculation Error

|  | Route Name | Actual (ft) | Calculated (ft) | Error |
| :---: | :--- | ---: | ---: | :---: |
| Rural Multilane | 0091P | 317.4 | 1348 | $325 \%$ |
|  | 0189 P | 265 | 1628 | $514 \%$ |
| Urban TLTW | 0108 P | 227.3 | 525.4 | $131 \%$ |
|  | 0186 P | 198.7 | 744.5 | $274 \%$ |

### 5.5 Intersection Error

A fourth error occurs because intersections are often included in the final output of the HAF Algorithm. In certain locations, route alignments often make a $90^{\circ}$ turn at intersections that should not be classified as a curve. A process in the ArcMap model was added to compensate for this but it often fails to distinguish between intersections and sharp mountain curves. Figure 5.3 contains an illustration of the issue. This particular segment exists in front of the State Capitol building at the intersection of 300 North and State Street (SR-186), in Salt Lake City.


Figure 5.3 Intersection Error (Esri 2017)

### 5.6 Tangent Error

Tangent error is not unique to a particular type of road, with the exception of TLTW rural highways where it does not occur as often, and frequently involves a short segment that has been classified as a curve rather than a tangent. This error is demonstrated in Figure 5.4. This curve segment is along I-70 near Green River, UT. It is clearly a tangent, but it was assigned a radius value of 2770 feet, which is fairly typical for a freeway curve. Errors of this type were often due to small curve length values from the data. Additionally, this type of error often occurs on highway segments where the road widens to accommodate an additional lane. Because the centerline of the road changes, the HAF Algorithm classifies it as a curve and assigns it radius and curve length values.


Figure 5.4 Tangent Error (Esri 2017)

### 5.7 Curve Fragment Error

The sixth type of error to be addressed in this chapter is a problem with curve fragments. In many instances, a small segment of a curve will be identified rather than the whole. This issue is illustrated in Figure 5.5. The segment in question is highlighted in cyan on the left with an
arrow pointing to it, and lies along I-15 near Nephi. The HAF Algorithm appropriately identified the curve to the right of it, but poorly estimated the PC and PT points on the left. This error was attributed to the same cause as the curve length calculation error, and occurred on between 3-5 percent of curves identified by the algorithm.


Figure 5.5 Curve Fragment Error (Esri 2017)

### 5.8 Chapter Summary

These six errors provided a basis upon which to improve the HAF Algorithm. While some errors were more difficult to correct than others due to problems with the data and limits of the program's ability, most of these errors were reduced to some degree. This process is explained further in Chapter 7.

### 6.0 HAF ALGORITHM CALIBRATION RESULTS

### 6.1 Overview

With the potential sources of larger error established, this chapter presents the results of the HAF Algorithm calibration process. It is important to note that there is some human error inherent in the outlined calibration process, particularly with fitting three-point arcs over satellite imagery. However, this error should not be large enough to have a significant impact on the final results. From these results, it was determined that the HAF Algorithm does not require modification to make it compatible with all highway types. This chapter contains a summary of the HAF Algorithm's accuracy in calculating radius and curve length, an overview of the curve identification accuracy, and a section on the analysis of the sample sizes used for the calibration.

### 6.2 Curve Parameter Calculation Accuracy

Table 6.1 contains a summary of the curve parameter error results obtained from comparing the different types of roads. Segments with intersection errors, tangent errors, or curve fragment errors were not included because these problems correspond more to the issue of curve identification rather than curve parameters. The other errors listed above, however, do affect the results of Table 6.1. Included in this table are basic averages for all errors in a particular road type, 95 percent confidence intervals, median error, and the percentage of segments that exceed an arbitrary 5 percent error threshold. The purpose behind this percent error threshold is to show a better representation of how well the segments meet a basic standard while simultaneously reducing the effect from data outliers. The percentage exceeding the threshold is presented rather than the percentage meeting it to keep some consistency with the other parts of the table (i.e. smaller percentages mean less error). The actual calibration data are contained in Table A. 1 through Table A. 6 in Appendix A, where increasing mileposts (to the north and east) indicate a positive direction while decreasing mileposts indicate a negative direction.
Table 6.1 Error Summary

|  | Interstate |  | Multilane Bighway |  | Two-Way Two-Lane <br>  <br>  <br>  <br> Highway |  | Total <br> Average |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Average | Urban | Rural | Urban | Rural | Urban | Rural |  |
| Arc Length | $5.3 \%$ | $6.1 \%$ | $8.2 \%$ | $15.1 \%$ | $7.0 \%$ | $5.5 \%$ | $7.9 \%$ |
| $95 \%$ CI | $2.8-7.8 \%$ | $4.6-7.6 \%$ | $3.7-12.7 \%$ | $3.6-26.6 \%$ | $3.2-10.8 \%$ | $4.1-6.9 \%$ | $\mathbf{5 . 7 - 1 0 . 1 \%}$ |
| Standard Deviation | $13.4 \%$ | $7.8 \%$ | $22.9 \%$ | $59.9 \%$ | $19.5 \%$ | $7.2 \%$ | $28.6 \%$ |
| Radius | $13.8 \%$ | $28.3 \%$ | $59.6 \%$ | $28.5 \%$ | $25.3 \%$ | $61.1 \%$ | $36.1 \%$ |
| $95 \%$ CI | $10.7-16.9 \%$ | $19.8-36.8 \%$ | $45.8-73.4 \%$ | $20.4-36.6 \%$ | $7.1-45.3 \%$ | $40.3-81.9 \%$ | $\mathbf{3 0 . 5 - 4 1 . 7 \%}$ |
| Standard Deviation | $16.3 \%$ | $43.2 \%$ | $70.6 \%$ | $42.4 \%$ | $92.6 \%$ | $106.0 \%$ | $70.1 \%$ |



Table 6.1 provides some interesting results on errors across different road types. The HAF Algorithm produces the most accurate results for interstate curves, followed by TLTW highways and multilane highways. It is immediately apparent that curve length calculations are far more accurate than radius calculations, which could be due in part to the fact that radius values are more affected by the larger sources of error discussed in Chapter 5. Urban segments appear to be generally more accurate, while the average values are sometimes worse than rural averages. This would seem to suggest the presence of large outliers affecting the results, especially in urban settings. This could be due to tangent-curve-tangent errors, although more analysis would need to be done to provide a definitive answer as to the reason why. Another interesting point is that many of the larger errors occurred in rural TLTW highway segments despite the fact that the HAF Algorithm was designed specifically for that road type. In other words, the algorithm produced more accurate results for interstate highways than it did for other road types.

Table 6.2 contains a summary of errors not included in Table 6.1 and the total identification accuracy for each road type. These errors include misidentified intersections, misidentified tangent segments, and curve fragments. If a segment included any of these three errors, it was marked as misidentified. The error values were calculated by taking the number of errors for each type and dividing it by the number of segments used in the sample. It is important to acknowledge the fact that the errors mentioned in Table 6.2 were very infrequent, so the sample sizes may not have been large enough to be certain how common they were.

Table 6.2 Identification Accuracy

|  | Interstate |  | Multilane Highway |  | TLTW Highway |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
|  | Urban | Rural | Urban | Rural | Urban | Rural |
| Intersection | $0.0 \%$ | $0.0 \%$ | $10.3 \%$ | $0.0 \%$ | $8.6 \%$ | $3.8 \%$ |
| Tangent | $2.4 \%$ | $0.0 \%$ | $14.4 \%$ | $5.3 \%$ | $5.2 \%$ | $0.0 \%$ |
| Curve Fragment | $2.4 \%$ | $3.9 \%$ | $4.1 \%$ | $1.8 \%$ | $0.0 \%$ | $1.9 \%$ |
| Total Accuracy | $95.2 \%$ | $96.1 \%$ | $71.2 \%$ | $92.9 \%$ | $86.2 \%$ | $94.3 \%$ |

As can be seen from Table 6.2, interstate curve segments were found to be generally more accurately identified than other road types. This is likely due in part to a lack of complications associated with intersections. The most striking difference presented in these data is the gap between urban and rural segments. While the difference between the two is almost
negligible in interstates, it is very large in other types of highways. This is especially true in intersection and tangent errors.

The required sample sizes for each road type for three different tolerance levels in accuracy are contained in Table 6.3. These different tolerances can be accepted by engineers at the 95 percent confidence level. Table 6.3 also contains the approximate number of usable segments for each road type, which is the limiting factor. One hundred segments were used for each road type. Instances where the requirement was not met are highlighted in blue.

Table 6.3 Adequacy Check of Required Sample Sizes

| Curve Length |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Tolerance | $5 \%$ | $7.5 \%$ | $\mathbf{1 0 \%}$ | Number of Usable Segments |
| Urban Interstate | 28 | 12 | 7 | 210 |
| Rural Interstate | 9 | 4 | 2 | 770 |
| Urban Multilane | 81 | 36 | 20 | 490 |
| Rural Multilane | 552 | 245 | 138 | 370 |
| Urban TLTW | 58 | 26 | 15 | 255 |
| Rural TLTW | 8 | 4 | 2 | 12000 |


| Radius |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | :---: | :---: | :---: | :---: |
| Tolerance | $\mathbf{5 \%}$ |  |  |  |  | $\mathbf{7 . 5} \%$ | $\mathbf{1 0 \%}$ | Number of Usable Segments |
| Urban Interstate | 41 | 18 | 10 | 210 |  |  |  |  |
| Rural Interstate | 287 | 127 | 72 | 770 |  |  |  |  |
| Urban Multilane | 766 | 340 | 191 | 490 |  |  |  |  |
| Rural Multilane | 277 | 123 | 69 | 370 |  |  |  |  |
| Urban TLTW | 1318 | 586 | 329 | 255 |  |  |  |  |
| Rural TLTW | 1725 | 767 | 431 | 12000 |  |  |  |  |

While the number of segments calibrated frequently fails to meet the requirement for radius data collection, it does meet the requirement in most road types for curve length data collection. The one exception, rural multilane, does not have enough usable segments in the state of Utah in order to meet the 5 percent tolerance level, so that one was left as is without calibrating more segments.

### 6.3 Chapter Summary

The HAF Algorithm is best suited for identifying curves and determining their parameters along interstates. While it generally does better in calculating curve parameters in urban settings across different road types, curve identification is stronger in rural ones, for which the HAF Algorithm was originally developed. Overall, the absence of large error percentages in the presented results confirms that the HAF Algorithm is suitable across all six highway types and that new algorithms for each highway type were not warranted.

### 7.0 HAF ALGORITHM IMPROVEMENTS

### 7.1 Overview

After calibrating the HAF Algorithm and discovering error sources, the next step was to make improvements to the algorithm. This chapter contains a summary of improvements designed to improve both curve identification and curve parameter determination. This includes solutions to errors that existed in the original algorithm, refinements made to the code to improve accuracy, and changes made to the ArcMap model to make final improvements on curve identification. The six primary errors that these improvements target were detailed in Chapter 5. The first three deal with curve identification, including curve fragment, tangent, and intersection errors. The last three errors pertain to curve parameter determination, and include tangent-curvetangent, curve length calculation, and compound curve errors. These last three have an impact on the radius and length of a curve, which makes meaningful crash analysis difficult.

The curve fragment, tangent, intersection, and curve length errors were resolved to varying degrees. Their corrective measures are presented in this chapter. An examination of the remaining two errors - tangent-curve-tangent and compound curve - is also presented for future research consideration.

This chapter also includes an outline of the changes made to the code to be able to accept more recent LiDAR data as an input to the HAF Algorithm. Because the data fields contain changes in formatting of some sort every time the data are collected, the expectation is that the algorithm is prepared to deal with field omissions or symbol changes without the code needing to be changed further from year to year in order to adapt to new data setups. The HAF Algorithm is now able to run 2012, 2014, and 2015 data. The solutions are presented in the following sections.

### 7.2 Curve Fragment/Curve Length Calculation Fix

The curve fragment and curve length calculation errors stemmed from the same cause and had the same solution. These errors are caused by an error in the HAF Algorithm's code.

The error affected 3-13 percent of segments, depending on highway type. The cause of this error was non-sequential milepost ordering, which disrupted the curve combination process.

This issue is illustrated in Table 7.1. The segments shown were all combined into a single curve that lies along I-80 near Park City. Originally, the algorithm was programmed with the expectation that each segment within a curve would be ordered with a string of increasing or decreasing mileposts. For instance, the end milepost of one segment would match the beginning milepost of the next and the pattern would continue. However, the example in Table 7.1 shows the beginning milepost of the first segment matching with the end milepost of the second. When combining the segments into a single curve, the algorithm would adopt the beginning milepost of the first segment and the end milepost of the last segment as the PC and PT, respectively, as highlighted in red in Table 7.1. This error leads to an incorrect overall curve length of 2,302 feet. The true curve length is 1.138 miles ( 6,009 feet), which is the difference in the green highlighted values. " N " in the third column indicates a negative direction, which in this case signifies that the direction of travel is to the west (for a road traveling north-south, " N " signifies a southerly direction).

Table 7.1 Curve Fragment Error Source

| ID | Route | Direction | Beg. MP | End MP | Curve Length (ft) |
| ---: | :--- | :--- | ---: | ---: | ---: |
| 322350 | 0080 N | N | 141.249 | 140.802 | 2358.14 |
| 322349 | 0080 N | N | 141.281 | 141.249 | 166.919 |
| 322348 | 0080 N | N | 141.368 | 141.281 | 462.944 |
| 322347 | 0080 N | N | 141.395 | 141.368 | 139.49 |
| 322346 | 0080 N | N | 141.441 | 141.395 | 244.689 |
| 322345 | 0080 N | N | 141.563 | 141.441 | 641.621 |
| 322344 | 0080 N | N | 141.604 | 141.563 | 219.504 |
| 322343 | 0080 N | N | 141.685 | 141.604 | 427.59 |
| 322342 | 0080 N | N | 141.94 | 141.685 | 1345.065 |

Because the wrong starting and ending points were used as inputs in ArcMap, measurements of several curves were much shorter than they should have been. The problem was compounded further by the fact that while the starting and ending points shortened the curve, the listed curve length was a value calculated by the algorithm rather than by ArcMap as a simple sum of each segment's length regardless of milepost order. This meant that the calculated
curve length was often 50-300 percent larger than the measured value and while correct, produced a large error in calibration.

To solve this problem, an "if-then" conditional statement was coded into the HAF Algorithm to examine the order of the mileposts. If the segment mileposts increased from beginning to end individually while the curve mileposts decreased as a whole (or vice versa), the endpoint of the first segment was assigned as the PC and the beginning point of the last segment was assigned as the PT. Error! Reference source not found. shows a flowchart of how the logic works.


Figure 7.1 If/Then Curve Fix Diagram
The same conditional statement was also applied to the curve's latitude, longitude, and elevation coordinates. This solution effectively eliminated the curve fragment and curve length calculation errors without affecting segments that did not experience a curve fragment error. A comparison of a curve near Park City along I-80 before and after the fix is shown in Figure 7.2 and Figure 7.3, respectively.


Figure 7.2 Before Curve Fragment Fix (Esri 2017)


Figure 7.3 After Curve Fragment Fix (Esri 2017)
The curve segment in question is highlighted in cyan in both Error! Reference source not found. and
. The curve in Error! Reference source not found. covers only a small portion of the actual curve, especially when compared to the curve in the opposite direction that did not encounter this error. Additionally, the curve in the opposite direction remains unaffected by this change, which is a demonstration of the effectiveness of the fix.

An additional problem resolved with the fix was that on occasion, some curves would have no length at all. This problem pertains to the way segment mileposts are ordered in the LiDAR data. This situation was unique to curves that consisted of two segments. Since the beginning milepost of the first segment would occasionally be the same as the end milepost of
the second, the starting and ending points of the curve would be exactly the same. Error!
Reference source not found. shows an example of the error located along I-70, with the starting and ending points identified by the original HAF Algorithm highlighted in red and the starting and ending points identified by the improved HAF Algorithm highlighted in green. This error meant that because ArcMap was expecting a line feature with a length, nothing on the map would be created, as if the curve did not exist. This is also no longer an issue.

Table 7.2 Missing Segment Error

| ID | Route | Direction | Beg. MP | End MP | Curve Length (ft) |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 321683 | 0070 N | N | 70.945 | 70.899 | 239.497 |
| 321682 | 0070 N | N | 70.984 | 70.945 | 206.118 |

### 7.3 Tangent Refinement

While the original HAF Algorithm is fairly accurate at identifying curves, there are occasions when tangent segments are identified as curves. To understand part of the cause of this error, a basic explanation of the curve weighting system in the algorithm is required. The user enters certain threshold values to assist in identifying curves, including radius, length, and the ratio between the two. A positive weight is assigned to segments that are more curve-like, and a negative weight is assigned to segments that are more tangent-like. For instance, in the original HAF Algorithm, a tangent would have its weight reduced by 1 for each multiple of the threshold that it exceeded. If the radius threshold were 6,000 and a segment had a radius of 6,001 feet, its weight would be -1 . If the segment's radius was 12,001 feet, it would have a weight of -2 , and so on.

While the threshold was acceptable and a few curve segments did have radii above 6,000 feet that were weighted positive due to them meeting other thresholds, tangent segments would slip through on occasion. Error! Reference source not found. contains a tangent segment identified as a curve along SR-173 in Taylorsville. This segment has a radius of 11,137 feet, which is well above the 6,000 -foot threshold. After further examination, it was found that nearly all segments with a radius beyond 10,500 feet were tangents.


Figure 7.4 Large-Radius Tangent Error (Esri 2017)

This issue prompted the idea of introducing a non-linear weighting system with larger negative weights being imposed for each successive breach of a threshold. This way, segments with radii values fairly close to the threshold still had an opportunity to be considered a curve while segments with a radius that far exceeded the threshold would be removed from consideration entirely. For each successive threshold breached, a negative weight that exceeded the previous weight by one would be assigned. This was done using an arithmetic series. The scale at which each successive threshold (not the weight itself) was determined was $1.75^{\mathrm{n}}$, the reason being that 6,000 multiplied by 1.75 reached the 10,500 value beyond which nearly every segment was a tangent.

To clarify how this non-linear weighting system works, an example of ranges will be presented with an assumed initial radius threshold of 6,000 feet. For segments with a radius between 6,000 and 10,500 feet, a weight of -1 was assigned. For radius values between 10,500 and 18,375 , a weight of -3 ( -1 minus 2 ) was assigned. For radius values between 18,375 and 32,156 feet, a weight of $-6(-1$ minus 2 minus 3 ) was assigned, and the pattern continues. The ranges for which the thresholds were adjusted were determined using a formula independent of the series used for the weights themselves.

This was found to reduce the number of tangent segments identified as curves. As an additional bonus, a few tangent-curve-tangent errors were resolved. The remaining tangents had parameters similar to those of curves in terms of radius and curve length, which made them much more difficult to isolate. However, this was an effective step in improving the performance of the algorithm.

### 7.4 Intersection Elimination

While steps were taken in the original HAF Algorithm to prevent the identification of intersections where highways changed direction as curves, it was not entirely successful and several intersections remained. An ArcMap model was developed to remove curves with a total length below a specified threshold, and it was effective to some degree. The issue with the remaining intersections, however, was that the ArcMap model and the HAF Algorithm were unable to differentiate between intersections and sharp curves on mountainous highways because the radii of the two are largely similar. Attempting to separate the two types of curves with a short radius (a true intersection and a sharp curve on a mountainous highway) by change in elevation was unsuccessful as many sharp mountain curves have small differences in elevation.

An alternative method was evaluated that involved isolating curves by location instead. Because urban areas lack sharp mountain curves, it seemed to be a feasible starting point from which to improve the model. A Utah municipality shapefile was downloaded from the Utah AGRC data portal. Upon closer inspection, it was found that very few sharp curves existed within urban municipalities and that many intersections were assigned a radius of less than 225 feet. This was further backed up by the AASHTO Greenbook in Table 3-9 (AASHTO 2011), which shows that such small radius values accompanied with a maximum design superelevation of 6 percent are rare and are only used with speeds of 25 mph or lower. UDOT uses a maximum superelevation of 6 percent for designing horizontal curves on state highways. With this information, a new addition to the ArcMap model was developed, as shown in Error! Reference source not found.


Figure 7.5 ArcMap Model (Esri 2017)


Figure 7.5 (Continued)

The complexity of the ArcMap model was increased significantly from the original one.
A new shapefile was created as a modified version of the municipality file mentioned earlier that only included urban municipalities. This new shapefile was added to the ArcMap model and removed curves with a radius of less than 225 feet from urban areas. This reduced the number of intersections identified as curves in the final output, increasing the overall identification accuracy. However, many intersections remained, particularly in rural areas. The possibility of removing all highway segments identified as curves from within any city limits below a certain radius threshold was explored but it was found that several sharp mountain curves existed within rural municipality boundaries, especially in Park City and Brian Head.

To resolve this issue, a new shapefile was created that excluded all municipalities that contained sharp mountainous curves. This was done by selecting all curves within all municipalities with a radius of less than 225 feet and viewing which cities contained mountainous curves. With this new information, the radius thresholds and municipality boundaries were applied and the number of intersections identified as curves was reduced from

25 to 20. In checking the effectiveness of these changes, it was found that no actual curves were removed in the process.

### 7.5 Thoughts on Remaining Two Errors

The two remaining errors that did not appear to have an immediate solution are the tangent-curve-tangent and compound curve errors. In the vast majority of cases related to the tangent-curve-tangent error, the problem lies in the data themselves. In this case, small tangents are often attached to curves as part of a single segment. Because the HAF Algorithm is designed to combine data segments and not divide them, this is an issue that could not be resolved. Dividing segments would necessitate further research and would be extremely difficult due to the fact that the starting and ending points of each segment are the only points that are given in the LiDAR attribute table. Any solution to remedy this would likely need to be done through ArcMap and would require a complex procedure.

To resolve the compound curve problem, a change in the approach to calibration was made to reflect what the HAF Algorithm does. While compound curves are relatively rare, provisions were made to accommodate them. Rather than drawing a single circular arc over the road in AutoCAD, compound curves were overlaid with two or three simple circular arcs, depending on the needs of the situation. Each individual curve length was added as part of a sum, and each radius was included in part of a weighted average based on segment length, which is what the HAF Algorithm does. In further research, the HAF Algorithm could possibly be altered to separate compound curves and populate another sheet designed specifically for them.

### 7.6 New Data Adaptation

After the HAF Algorithm was improved, it needed to be modified to accept more recent data. The original HAF Algorithm was designed to run on 2012 LiDAR data. However, the order and names of the different columns included in the attribute table changed from the 2012 to 2014 data, which meant that the algorithm had to be revamped to include a new interface that required more user input. These changes meant that the algorithm was capable of running two years'
worth of curve data despite the differences in format. However, the algorithm was not capable of running 2015 data due to further changes in formatting.

The new data omitted a segment ID column, which had been used previously to check if the segments had been ordered sequentially. This part of the code was removed from the algorithm as it was simply a redundancy designed to find errors and it was found to be unnecessary. The new 2015 data had "+" and "-" signs to indicate positive and negative milepost direction while 2012 and 2014 data had used "P" and "N" to indicate direction. This had been used in the original HAF Algorithm to confirm that directional errors did not exist in the data. To resolve the difference in route direction symbology, a VLookup function was added to the main interface to sort through the direction column in the data to find unique values of direction indication, which were then populated to a hidden sheet within the Excel file.

After the unique values had been found, the different options were made available for selection through the Data Validation function. Error! Reference source not found. shows the updated interface. In this updated interface, the user specifies the input and output file locations in addition to checking column headings as had been done in the original HAF Algorithm. After the "Apply" button has been pressed, the user then specifies what signs are used to indicate positive and negative milepost direction, the units in which the curve length is given, and the threshold parameters. After these have been filled, the HAF Algorithm is ready to be run.


Figure 7.6 Updated HAF Algorithm Interface

The direction selection procedure is illustrated in Error! Reference source not found.. In this particular example, 2015 data are being run through the algorithm, which has a direction column filled with plus and minus signs. During the run of the program, the direction signs that the user had specified would be swapped with "P" for "+" and "N" for "-" in the output data for positive and negative directions, respectively.

## Select Direction Placeholder



Figure 7.7 Direction Drop-Down Arrow

Another change in the 2015 data from previous years was that the units of segment length were different. In 2012 and 2014 data, every length measurement had been done in feet, while the 2015 data were in units of miles. The units were verified using a comparison of the ArcMap shapefile to Google Earth's path measurement tool. To account for this change, a part of the
program to convert miles into feet was written in the code and it would be activated should the user specify that the curve length units were in miles, as shown in Error! Reference source not found.


## Figure 7.8 Units Drop-Down Arrow

These changes in the programming and the interface allowed the updated HAF Algorithm to run 2012, 2014, and 2015 data. The program now requires more user input, but contains easy-to-follow steps to ensure it runs smoothly.

An additional change that was made to the HAF Algorithm to allow for 2015 input data involved removing duplicate segments. These caused a problem on interstates in which two segments with the exact same parameters would overlap. The HAF Algorithm would identify them as two halves of the same curve and combine their respective curve lengths. This meant that the calculated curve length was exactly double what it was supposed to be. To resolve this issue, Excel's built-in "Remove Duplicates" function was implemented into the code and it searched for segments that had the exact same attributes as a previous one. Once these segments were identified, duplicates were removed, leaving the input data as they should have been.

The final change that was made to adapt to 2015 input data involved an isolated error that occurred along SR-201 in Salt Lake City. A situation in which two segments of the highway with the same direction ran parallel to each other disrupted the milepost order, which led to a 13-mile gap in the mileposts. One of the curves ended at an intersection and should have been classified as a tangent. This issue caused a large amount of the highway to be considered a single curve. This error was resolved through adding a stipulation that removed segments from curve consideration if there was more than a 5-mile gap between the PC and PT.

While the program is now able to run 2015 data effectively, the primary concern is that the data might change further in future years, which might prevent the algorithm from working properly. Unfortunately, it is not possible to predict what changes will occur. It was only after
the directional issue was fixed that it was discovered that the 2015 segment lengths were in units of miles. This indicates that it is possible for large, unforeseen differences to appear in future datasets. This would require further alterations to the code and possible changes to the interface. A full list of what data the HAF Algorithm requires as well as the general formatting that is expected is detailed in the HAF Algorithm user's manual.

### 7.7 Chapter Summary

Six errors were targeted in order to make improvements to the existing HAF Algorithm, including curve fragment, curve length calculation, tangent, intersection, compound curve, and tangent-curve-tangent errors. Curve fragment and curve length calculation errors were both effectively reduced as they had the same cause. Intersection errors were also reduced due to new provisions being made in the updated ArcMap model. Tangent errors were reduced less effectively, although the new weighting system did eliminate some tangents from being identified as curves. The other two errors could not be resolved by making improvements to the HAF Algorithm. The results of the improvements to the HAF Algorithm are discussed in Chapter 8.

### 8.0 RESULTS OF HAF IMPROVEMENTS

### 8.1 Overview

Significant improvements were made to the HAF Algorithm. In addition to using newer data, errors were resolved to increase overall accuracy. Contained in this chapter is a summary of the curve length and radius calibration, an overview of the curve identification accuracy, and a review of the required sample sizes for each highway type. The results of the original algorithm do differ from those presented in the Chapter 5 due to the elimination of human error in the calibration process. Curves with larger errors were reviewed separately by a researcher who had not calibrated the segment the first time. This was done to verify that the calibration had been performed properly. Changes were made to both the original and improved algorithm results accordingly.

### 8.2 Curve Parameter Results

This section covers the results of curve parameter calculation and compares the outputs of both the original and improved algorithm. Table 8.1 contains a summary of the results for interstate calibration. Averages, 95 percent confidence intervals, standard deviations, and medians are included in these results. Additionally, a section was created that shows the percentage of segments that met a 5 percent error threshold. The average curve length error decreased in both urban and rural settings.

Rural interstate segments had an 18 percent improvement in the number of segments that now meet the 5 percent curve length error threshold. However, the median error remained relatively constant. This is because HAF Algorithm improvements for curve length specifically targeted larger errors that would be classified as outliers, which includes the curve length calculation error. The other improvements relate more to curve identification and adapting to more recent data. This also explains the lack of change in radius error.

Table 8.1 Interstate Calibration Result Comparison

|  | Urban |  | Rural |  |
| :--- | ---: | ---: | ---: | ---: |
| Average | Original | Improved | Original | Improved |
| Curve Length | $4.0 \%$ | $3.0 \%$ | $4.2 \%$ | $2.4 \%$ |
| $95 \%$ CI | $2.4-5.6 \%$ | $2.4-3.6 \%$ | $3.1-5.3 \%$ | $1.9-2.9 \%$ |
| Standard Deviation | $8.34 \%$ | $2.93 \%$ | $5.57 \%$ | $2.31 \%$ |
| Radius | $12.3 \%$ | $10.1 \%$ | $13.1 \%$ | $16.0 \%$ |
| $95 \%$ CI | $9.9-14.7 \%$ | $8.0-12.2 \%$ | $11.3-14.9 \%$ | $13.1-18.9 \%$ |
| Standard Deviation | $12.46 \%$ | $10.57 \%$ | $9.09 \%$ | $14.61 \%$ |


|  | Urban |  | Rural |  |
| :--- | ---: | ---: | ---: | ---: |
| Median | Original | Improved | Original | Improved |
| Curve Length | $1.7 \%$ | $2.2 \%$ | $2.7 \%$ | $1.7 \%$ |
| Radius | $8.6 \%$ | $7.2 \%$ | $10.2 \%$ | $12.1 \%$ |


|  | Urban |  | Rural |  |
| :--- | ---: | ---: | ---: | ---: |
| <5\% Threshold | Original | Improved | Original | Improved |
| Curve Length | $84.1 \%$ | $86.1 \%$ | $73.0 \%$ | $91.0 \%$ |
| Radius | $36.6 \%$ | $33.7 \%$ | $14.0 \%$ | $13.0 \%$ |

Table 8.2 contains a summary of the calibration results for multilane highways. The reduction in average curve length error is 4.6 percent for urban areas and 7.0 percent for rural areas. This is again due to the targeting of outliers that the original HAF Algorithm produced on occasion. The median error values for both radius and curve length have remained consistent, adding credence to this explanation. The percentage of segment curve lengths that meet the 5 percent error threshold has increased by 16.0 percent for urban areas and 21.1 percent for rural areas. The radius averages have also improved, which could be due to the use of newer data. It is also worth pointing out that the standard deviations have decreased for all categories except for the 5 percent error threshold in rural areas, which generally suggests increased consistency.

Table 8.2 Multilane Highway Calibration Result Comparison

|  | Urban |  | Rural |  |
| :--- | ---: | ---: | ---: | ---: |
| Average | Original | Improved | Original | Improved |
| Curve Length | $6.6 \%$ | $2.0 \%$ | $8.8 \%$ | $1.8 \%$ |
| $95 \%$ CI | $2.4-10.8 \%$ | $1.7-2.3 \%$ | $2.2-15.4 \%$ | $1.4-2.2 \%$ |
| Standard Deviation | $20.89 \%$ | $1.75 \%$ | $33.93 \%$ | $1.91 \%$ |
| Radius | $27.9 \%$ | $17.0 \%$ | $24.4 \%$ | $12.7 \%$ |
| $95 \%$ CI | $16.1-39.7 \%$ | $13.8-20.2 \%$ | $16.7-32.1 \%$ | $10.5-14.9 \%$ |
| Standard Deviation | $58.86 \%$ | $16.30 \%$ | $39.67 \%$ | $11.02 \%$ |


|  | Urban |  | Rural |  |
| :--- | ---: | ---: | ---: | ---: |
| Median | Original | Improved | Original | Improved |
| Curve Length | $2.4 \%$ | $1.6 \%$ | $2.5 \%$ | $1.1 \%$ |
| Radius | $11.5 \%$ | $11.4 \%$ | $13.4 \%$ | $9.7 \%$ |


|  | Urban |  | Rural |  |
| :--- | ---: | ---: | ---: | ---: |
| <5\% Threshold | Original | Improved | Original | Improved |
| Curve Length | $78.0 \%$ | $94.0 \%$ | $70.9 \%$ | $92.0 \%$ |
| Radius | $23.0 \%$ | $15.0 \%$ | $15.5 \%$ | $31.0 \%$ |

Table 8.3 contains a comparison of the improved HAF Algorithm with the original for TLTW highways. The results are similar to that of interstates and multilane highways, in that averages improved while medians remained fairly consistent for both radius and curve length. While there is some overlap in the 95 percent confidence intervals, the average curve length error decreased as a whole. The number of segment curve lengths that met the error threshold has improved in both cases, which means that all highway types with the exception of urban interstate have at least 90 percent of segments with an error of 5 percent or less.

Table 8.3 TLTW Highway Calibration Result Comparison

|  | Urban |  | Rural |  |
| :---: | :---: | :---: | :---: | :---: |
| Average | Original | Improved | Original | Improved |
| Curve Length | 6.2\% | 2.2\% | 4.6\% | 1.9\% |
| 95\% CI | 2.4-10.0\% | 1.8-2.6\% | 3.3-5.9\% | 1.5-2.3\% |
| Standard Deviation | 19.09\% | 1.90\% | 6.65\% | 2.06\% |
| Radius | 25.3\% | 21.9\% | 49.6\% | 27.0\% |
| 95\% CI | 13.6-37.0\% | 17.8-26.0\% | 30.4-68.8\% | 19.8-34.2\% |
| Standard Deviation | 59.34\% | 20.96\% | 96.86\% | 36.76\% |
|  | Urban |  | Rural |  |
| Median | Original | Improved | Original | Improved |
| Curve Length | 1.8\% | 1.7\% | 2.4\% | 1.2\% |
| Radius | 18.8\% | 18.9\% | 20.3\% | 19.1\% |
|  | Urban |  | Rural |  |
| <5\% Threshold | Original | Improved | Original | Improved |
| Curve Length | 85.0\% | 92.0\% | 74.0\% | 93.0\% |
| Radius | 15.0\% | 15.0\% | 9.0\% | 12.0\% |

The curve length errors presented in Table 8.1, Table 8.2, and Table 8.3 are low, to the point that these percentages could be influenced by human error in the calibration process. This would suggest that no further improvements are warranted to improve the accuracy of curve length calculation. Additionally, these improvements have brought the accuracy of multilane and TLTW highways to a level similar to that of interstates, meaning that the HAF Algorithm is nearly equally effective across all highway types.

### 8.3 Curve Identification Results

This section focuses on the improved HAF Algorithm's ability to correctly identify curves. Table 8.4 presents errors that are associated with curve identification rather than curve parameters, specifically for interstate highways. As can be seen from the total accuracy row, there is a general trend toward improvement. The curve fragment fix was effective in eliminating those errors almost completely. While the number of tangents was reduced, tangent errors were uncommon for interstate highways to begin with, which means that more tests would need to be performed to determine whether the fix was effective.

Table 8.4 Interstate Identification Error Comparison

|  | Urban |  | Rural |  |
| :--- | ---: | ---: | ---: | ---: |
|  | Original | Improved | Original | Improved |
| Intersection | $0.0 \%$ | $0.0 \%$ | $0.0 \%$ | $0.0 \%$ |
| Tangent | $2.4 \%$ | $1.4 \%$ | $0.0 \%$ | $0.0 \%$ |
| Curve Fragment | $2.4 \%$ | $0.0 \%$ | $3.9 \%$ | $0.0 \%$ |
| Total Error | $4.8 \%$ | $1.4 \%$ | $3.9 \%$ | $0.0 \%$ |
| Total Accuracy | $95.2 \%$ | $98.6 \%$ | $96.1 \%$ | $100.0 \%$ |

Table 8.5 contains a curve identification error comparison for multilane highways. While urban multilane segments showed a trend of improvement, rural segments remained relatively consistent as the number of errors was very low to begin with. While a 3.3 percent intersection error occurred in the improved algorithm results, it was found that these specific errors would have occurred under the original algorithm as well. The increase in error was a result of the randomness of the segments selected for comparison purposes. The most pronounced improvement came in the elimination of intersections identified as curves along urban multilane highways. This is because the revised ArcMap model targeted municipality areas, which make up the entirety of urban regions. This improvement brought the total accuracy of urban multilane segments to 87.3 percent from its original accuracy of 71.2 percent.

Table 8.5 Multilane Highway Identification Error Comparison

|  | Urban |  | Rural |  |
| :--- | ---: | ---: | ---: | ---: |
|  | Original | Improved | Original | Improved |
| Intersection | $10.3 \%$ | $1.8 \%$ | $0.0 \%$ | $3.3 \%$ |
| Tangent | $14.4 \%$ | $10.9 \%$ | $5.3 \%$ | $5.0 \%$ |
| Curve Fragment | $4.1 \%$ | $0.0 \%$ | $1.8 \%$ | $0.0 \%$ |
| Total Error | $28.8 \%$ | $12.7 \%$ | $7.1 \%$ | $8.3 \%$ |
| Total Accuracy | $71.2 \%$ | $87.3 \%$ | $92.9 \%$ | $91.7 \%$ |

Table 8.6 contains an identification error comparison for TLTW highways. In both urban and rural settings, the number of intersections identified as curves has been reduced. However, the percentage of tangents identified as curves increased in urban TLTW highways. This could be due to the fact that the sample size of curves with this error was too small to provide a definitive conclusion. After further examination of this type of error, it was determined that the
segments that were identified as tangents in the improved HAF Algorithm would have likewise been identified as tangents in the original HAF Algorithm (with alterations made to adapt to 2015 data). Several of these errors occurred at locations where a highway was widened to accommodate a left-turn lane, which means that the centerline of a highway would have been adjusted at that point. Many of these tangents were assigned a radius of approximately 2,000 feet, which makes them virtually indistinguishable from curves from a data standpoint. Despite this, there is a general trend towards improvement.

Table 8.6 TLTW Highway Identification Error Comparison

|  | Urban |  | Rural |  |
| :--- | ---: | ---: | ---: | ---: |
|  | Original | Improved | Original | Improved |
| Intersection | $8.6 \%$ | $1.8 \%$ | $3.8 \%$ | $2.4 \%$ |
| Tangent | $5.2 \%$ | $10.5 \%$ | $0.0 \%$ | $0.0 \%$ |
| Curve Fragment | $0.0 \%$ | $0.0 \%$ | $1.9 \%$ | $0.0 \%$ |
| Total Error | $13.8 \%$ | $12.3 \%$ | $5.7 \%$ | $2.4 \%$ |
| Total Accuracy | $86.2 \%$ | $87.7 \%$ | $94.3 \%$ | $97.6 \%$ |

In summary, it can be concluded that the curve fragment and intersection improvements were effective, while the tangent fix was less effective than expected.

### 8.4 Adequacy Check of Required Sample Sizes

When performing assessments of improvement efficacy, the data must be examined in order to determine if the minimum sample size was met. Table 8.7 provides an adequacy check of required sample sizes for curve length calculation for $5,7.5$, and 10 percent tolerance levels. The column on the very right shows the total number of useable curves listed for each highway type. The formula used to calculate the required sample size is outlined in Equation 8-1:

$$
\begin{equation*}
N=\frac{z^{2} \sigma^{2}}{E^{2}} \tag{8-1}
\end{equation*}
$$

Where:

[^0]Approximately 100 curves were calibrated in each situation, and road types that did not meet the requirement are highlighted in blue. The original HAF Algorithm met the required number of segments for all highway types except for rural multilane in the 5 percent tolerance in accuracy at the 95 percent confidence level. The improved HAF Algorithm met the requirement for each highway type, due to small standard deviations in terms of error.

Table 8.7 Curve Length Adequacy Check of Required Sample Sizes

| Tolerance | $\mathbf{5}$ Percent |  | $\mathbf{7 . 5}$ Percent |  | $\mathbf{1 0}$ Percent |  | \# of <br> Segments |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| HAF Status | Original | Improved | Original | Improved | Original | Improved |  |
| Urban Interstate | 11 | 2 | 5 | 2 | 3 | 2 | 210 |
| Rural Interstate | 5 | 2 | 2 | 2 | 2 | 2 | 770 |
| Urban Multilane | 67 | 2 | 30 | 2 | 17 | 2 | 490 |
| Rural Multilane | 177 | 2 | 79 | 2 | 44 | 2 | 370 |
| Urban TLTW | 56 | 2 | 25 | 2 | 14 | 2 | 255 |
| Rural TLTW | 7 | 2 | 3 | 2 | 2 | 2 | 12000 |

Table 8.8 contains a similar adequacy check of required sample sizes for radius calculations in each road type. Radius errors varied far more, which meant that much larger sample sizes were required. In many cases, the required sample size for the original algorithm exceeded the number of usable segments available in a particular road type. However, the improved HAF Algorithm met the required sample size in every road type with the exception of rural TLTW, which means that average radius errors presented in Table 8.1, Table 8.2, and Table 8.3 are an accurate representation of the actual error percentage. It is worth mentioning that the LiDAR data seem to be more accurate in calculating curve length than they are at calculating radius values. At minimum 100 samples were again used for each highway type.

Table 8.8 Radius Adequacy Check of Required Sample Sizes

| Tolerance | 5 Percent |  | 7.5 Percent |  | 10 Percent |  | \# of <br> Segments |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| HAF Status | Original | Improved | Original | Improved | Original | Improved |  |
| Urban Interstate | 24 | 17 | 11 | 8 | 6 | 4 | 210 |
| Rural Interstate | 13 | 33 | 6 | 15 | 3 | 8 | 770 |
| Urban Multilane | 532 | 41 | 237 | 18 | 133 | 10 | 490 |
| Rural Multilane | 242 | 19 | 107 | 8 | 60 | 5 | 370 |
| Urban TLTW | 541 | 68 | 240 | 30 | 135 | 17 | 255 |
| Rural TLTW | 1442 | 208 | 641 | 92 | 360 | 52 | 12000 |

### 8.5 Chapter Summary

Overall, the new HAF Algorithm is an improvement over its predecessor. It shows a reduction of error both in terms of curve identification and curve parameter calculation. Of the six errors mentioned at the beginning of the chapter, four were effectively reduced or eliminated, including intersection, tangent, curve length calculation, and curve fragment errors. Compound curve errors require a change in calibration approach, and tangent-curve-tangent errors could not be reduced due to the way the LiDAR data is reported. While some tangents were eliminated, others remained due to issues with the data displaying an incorrect radius value. This may warrant further research, although it would be difficult to remedy because these tangents are virtually indistinguishable from curves when viewed in table form.

The new algorithm was also effective in adapting to 2015 data. Changes were made both to the interface and to the code itself, with more options for the user to specify in order to ensure that it runs properly. With these alterations, it should be prepared to accept future data.

Most significantly, the average curve length error was reduced across each road type. The improved HAF Algorithm is very accurate in determining curve length, and the presence of any curve length error is likely due in part to human error in the process of calibration. The improvements made to the algorithm, combined with newer data, have made curve identification and parameter calculation very accurate. With the improvements achieved, the next step was to combine curve, roadway, and crash data to identify curve segments with high crash occurrences.

### 9.0 HAF CRASH ANALYSIS

### 9.1 Overview

While the HAF Algorithm is effective at identifying curves and their attributes, it cannot process crash data and show the user crash hotspots. For this reason, a new program was needed to combine curve, roadway, and crash data. This chapter presents the process and results of that combination. It also includes several case study examples. Users of the program should be able to use output files to determine which highway curves warrant improvements to make them safer. Additionally, this program prepares the way for further crash analysis in the UCPM and UCSM so that curve parameters can be analyzed to determine if there is a correlation between those parameters and crash rates.

### 9.2 Excel VBA Program - Combining Road Data with Crash Data

This section contains an explanation of the VBA program designed to combine curve, roadway, and crash data. An overview of the program's function is included, as well as a look into the main interface and some of the features contained in it. A simplified explanation of how the code works in combining roadway and crash data is also included, as well as a discussion on how superelevation transition segments can be considered when determining the crash histories of each curve.

### 9.2.1 Overview of the Program's Function

The function of the VBA program is to format and clean up roadway data, and combine them with curve data and crash data in order to generate lists of curves with their parameters and crash histories. The algorithm loops through each dataset and identifies fields that are common between them, including route name, milepost, and direction, depending on the dataset. The first five input data files contain roadway data and were obtained from the UDOT Data Portal (UDOT 2017). The final four contain crash data that are not publicly available but also come from UDOT. All input files are listed as follows:

- AADT (Open Data)
- Functional Class
- Approximate Speed Limit (2015)
- Urban Code
- Lanes (2014)
- Crash_data_2010-2015
- Crash_Location_2010-2015
- Crash_Rollups_2010-2015
- Vehicle_2010-2015

The four crash data files were combined into a single file through the use of a program titled "Roadway and Crash Data Preparation" created earlier by a research team at BYU (Schultz et al. 2017).

### 9.2.2 Program Interface

The VBA program user interface is shown in Figure 9.1. The new program works similar to the HAF Algorithm in that there are areas at the top to specify the output file location. There are also places to match headings to ensure that the different data headings are picked up correctly. Additionally, several buttons are placed to allow the user to select input files for the various types of road data and crash data, with status indicators that signal when the data files have finished importing. The interface also allows the user to specify the minimum UDOT severity level for a crash to be considered severe, as well as choose whether superelevation transition segments will be considered in the total curve length.


Figure 9.1 Excel Program User Interface

In this program, the user first specifies the folder directory in which the output file will be stored as well as the name of the output file. After this has been completed, the user selects the .csv files to be used as the input files. Seven total datasets are placed in separate sheets before the combination phase. The user will then press the "Check" button, which will initiate a program to check the headings of the input files. If an expected heading is not found, it will appear under the "Match Headings" section with a description of the proper heading. The user can then select the corresponding input heading from a drop-down list. Once the user clicks the "Run" button, the new headings are applied to the input sheet for the program to keep track of which columns correspond to their respective data fields. Like in the HAF Algorithm, the heading check section is necessary because data headings often change from year to year.

### 9.2.3 Roadway Data Combination

The program takes about two minutes using a Core2 processor to run through 16,000 curve segments, and copies necessary fields from the roadway data sheets to the Output Data sheet. The data are sorted first by route name, then by direction, and finally by beginning milepost. This puts the segments in consecutive order. The curve segments are the first to be
copied to the output sheet because they are the main focus of the study. The program loops through each curve segment multiple times to place each road parameter with its respective curves. The data is combined through route name and milepoint. The program loops consecutively through each roadway sheet to determine which road parameter segment the curve segment lies within. If a curve segment is separated by two different road parameter segments, the data from the first segment is adopted and placed in the output sheet. Direction is also taken into consideration in some datasets. For instance, the speed limit for some segments varies depending on direction. The program takes this into account.

Some VLookup functions are required as county codes from station numbers are matched with their respective county names in a sheet entitled "Key." A similar process is done in looking up the description for each functional class to give a better idea of the type of highways being analyzed.

A correction is applied to the speed limits of certain segments. In some cases, the speed limit is listed as 0 or 10 , which is an error with the data. Should this happen, the program obtains a speed limit based on the segment's functional class. In this case, a VLookup function is used in which to replace the erroneous speed limit with an average speed limit for each functional class from the Key sheet. After the data have been corrected, the program then calculates fields such as total truck percentage and VMT. These fields are necessary for full statistical analysis.

An additional correction is also applied to the Lanes sheet. Because of the nature of the file, this data is largely fragmented and contains several overlaps. A provision is made in the program to consolidate the data and organize it such that one segment starts where the previous one ends. The difficulty is that overlapping segments often have conflicting data. Because it is not possible to determine which segment is correct from the data alone, the number of through lanes from the first segment is adopted for the final output file.

### 9.2.4 Superelevation Transition Calculation

The final step the program takes before combining the crash data is to calculate superelevation according to recommended guidelines given in the Greenbook (AASHTO 2011).

Superelevation runoff is calculated using Equation 3-23 in the Greenbook, which is outlined in Equation 9-1.

$$
\begin{equation*}
L_{r}=\frac{\left(w n_{1}\right) e_{d}}{\Delta}\left(b_{w}\right) \tag{9-1}
\end{equation*}
$$

Where:
$L_{r}=$ superelevation runoff
$w=$ width of one traffic lane (assumed to be 12 ft )
$n_{l}=$ number of lanes to be rotated
$e_{d}=$ design superelevation
$\Delta=$ maximum relative gradient
$b_{w}=$ lane adjustment factor
Because the number of lanes to be rotated is difficult to determine due to the existence of divided highways, $n_{l}$ is assumed to be 1 while $b_{w}$ is given a conservative value of 1.0. This has been done because transition length does not need to be completely accurate as the PC and PT of identified curves often differ slightly from where they are actually located.

Design superelevation $\left(\mathrm{e}_{\mathrm{d}}\right)$ is a value that is looked up from Table 3-9 in the Greenbook, assuming a maximum superelevation of 6 percent used by UDOT (UDOT 2012). This table has been replicated in the Superelevation Tables sheet, where superelevation is determined based on the speed limit and the radius of the curve. Figure 9.2 shows a screenshot of part of this table. Design superelevation is on the left, and is looked up based on design speed from the top row and an approximate radius value.

| Design Superelevation, $\mathrm{e}_{\text {max }}=6 \%$ |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Speed Lim | PH) |  |  |  |  |  |  |
| $\mathrm{e}_{\mathrm{d}}$ | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 |
| 2 | 868 | 1580 | 2290 | 3130 | 4100 | 5230 | 6480 | 7870 |
| 2 | 614 | 1120 | 1630 | 2240 | 2950 | 3770 | 4680 | 5700 |
| 2.2 | 543 | 991 | 1450 | 2000 | 2630 | 3370 | 4190 | 5100 |
| 2.4 | 482 | 884 | 1300 | 1790 | 2360 | 3030 | 3770 | 4600 |
| 2.6 | 430 | 791 | 1170 | 1610 | 2130 | 2740 | 3420 | 4170 |
| 2.8 | 384 | 709 | 1050 | 1460 | 1930 | 2490 | 3110 | 3800 |
| 3 | 341 | 635 | 944 | 1320 | 1760 | 2270 | 2840 | 3480 |
| 3.2 | 300 | 566 | 850 | 1200 | 1600 | 2080 | 2600 | 3200 |
| 3.4 | 256 | 498 | 761 | 1080 | 1460 | 1900 | 2390 | 2940 |
| 3.6 | 209 | 422 | 673 | 972 | 1320 | 1740 | 2190 | 2710 |
| 3.8 | 176 | 358 | 583 | 864 | 1190 | 1590 | 2010 | 2490 |
| 4 | 151 | 309 | 511 | 766 | 1070 | 1440 | 1840 | 2300 |
| 4.2 | 131 | 270 | 452 | 684 | 960 | 1310 | 1680 | 2110 |

Figure 9.2 Design Superelevation Table with $e_{\text {max }}=6$ Percent

The program sorts through the table first by determining what column the speed limit matches. It then loops down the column to find the radius value that most closely matches the radius of the curve. After that, it finds the row this radius value is on, and determines the corresponding design superelevation. If the radius is greater than the value on the top row, a provision is made that sets the design superelevation as 2 percent. The maximum relative gradient $(\Delta)$ is determined by looking up a value in Table 3-15 from the Greenbook by correlating the speed limit with the maximum relative gradient. From these values, the superelevation runoff distance is calculated.

Tangent runout then is calculated by using equation 3-24 in the Greenbook, which is outlined in Equation 9-2.

$$
\begin{equation*}
L_{t}=\frac{e_{n c}}{e_{d}} L_{r} \tag{9-2}
\end{equation*}
$$

Where:
$L_{t}=$ tangent runout
$e_{n c}=$ normal crown superelevation
All other variables have been previously defined. Two thirds of the superelevation runoff and the whole tangent runout distance are then added together to produce a transition length, which can
then be added to or subtracted from milepost values to have curves with transition segments included. New curve lengths are then calculated. The user is able to choose whether or not transition lengths are included by checking a box on the lower right-hand corner of the interface.

### 9.2.5 Crash Data Combination

The crash data are then combined with the roadway data by looping through each segment and determining the number of crashes that have occurred within the curve. This is done by comparing the mile point of a crash to the beginning and ending mile points of a curve. The number of crashes per segment is determined by counting the number of crashes with a mile point that is between the beginning and end of a curve. The number of severe crashes is determined by the user selecting a minimum UDOT crash severity level to be considered "severe."

After the number of total and severe crashes has been counted for each segment, the total and severe crash rates are calculated as the number of crashes/ 1 million VMT. This is done using the formula outlined in Equation 9-3.

$$
\begin{equation*}
R=\frac{C \times 10^{6}}{365 V N L} \tag{9-3}
\end{equation*}
$$

Where:
$R=$ total or severe crash rate
$C=$ number of total or severe crashes in a given segment
$V=$ the average AADT for the six years' worth of data
$N=$ the number of years included in the data (typically six)
$L=$ the segment length in miles.
Because intersections have a tendency to skew results to some degree as crashes occur more frequently near intersections, code was added to the program to show the user the total and severe crash rates with and without intersection-related crashes. From here, the user can sort the data to eliminate crashes in intersections from consideration.

In the output file, the user is able to order the segments however they like and apply constraints such as looking at curves only in a particular region. This requires some knowledge of Excel and the ability to use Excel's sort and filter functions.

### 9.3 Crash Analysis

This section contains lists of curves with crash histories, as well as examples of a few curves of interest that had particularly high crash rates. Lists of curves ordered by the total crash rate and severe crash rate are included, as well as a list that includes superelevation transition segments in the total curve length and a list that applies a threshold to remove segments with low traffic volumes from consideration. In the examples of curves with high crash occurrences, the crash type and information about each curve are included in the analysis.

### 9.3.1 Segments Ordered by Severe Crash Rate

Lists of segments with the highest crash rates were generated following the creation of the output file. In this case, a severe crash is considered to be any crash with a level 3 or higher UDOT severity ranking. The UDOT severity ranking system is presented in Error! Reference source not found.. A rating of 1 is applied to crashes with no injury, while a rating of 5 is applied to crashes with at least one fatality.

Table 9.1 UDOT Severity Ranking

| Severity Ranking | Description |
| :---: | :--- |
| 1 | Non-injury |
| 2 | Possible injury |
| 3 | Non-incapacitating evident injury |
| 4 | Incapacitating injury |
| 5 | Fatal |

One of these lists is shown in Table 9.2, which contains details about the 20 curves with the highest severe crash rates in the state of Utah, including location information, VMT, and crash data. The presence of intersections does not affect the ranking. Segments highlighted in green will be analyzed further in this chapter on an individual basis. At least one segment of interest from each UDOT Region is included in this section. The severe crash rate is expressed in terms of the number of severe crashes per 1 million VMT. It is worth pointing out that several of these segments in Table 9.2 made this list due to extremely low AADT values paired with a single crash. This is particularly the case along SR-153, which is an unpaved mountain road in Beaver County.
Table 9.2 Curves Organized by Severe Crash Rate

| Route | Beg MP | Length <br> (mi) | County | Region | VMT <br> (/day) | Total \# of <br> Crashes | \# of Severe <br> Crashes | Severe Rate <br> (\#/MVMT) | Segment <br> \# |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 0066 | 2.469 | 0.074 | Morgan | 1 | 33 | 3 | 3 | 4 |  |
| 0095 | 48.868 | 0.066 | San Juan | 4 | 11 | 1 | 1 | 45.9 |  |
| 0066 | 4.944 | 0.082 | Morgan | 1 | 36 | 4 | 3 | 45.4 |  |
| 0092 | 18.548 | 0.044 | Utah | 3 | 29 | 2 | 2 | 41.4 |  |
| 0123 | 11.322 | 0.079 | Carbon | 4 | 13 | 1 | 1 | 41.4 |  |
| 0153 | 3.645 | 0.059 | Beaver | 4 | 13 | 1 | 1 | 38.5 |  |
| 0226 | 0.446 | 0.058 | Weber | 1 | 14 | 1 | 1 | 35.6 |  |
| 0066 | 1.978 | 0.036 | Morgan | 1 | 16 | 1 | 1 | 35.1 |  |
| 0153 | 10.046 | 0.07 | Beaver | 4 | 16 | 1 | 1 | 31.5 |  |
| 0144 | 2.079 | 0.046 | Utah | 3 | 17 | 2 | 1 | 29.0 |  |
| 0144 | 0.008 | 0.047 | Utah | 3 | 18 | 4 | 1 | 28.8 |  |
| 0153 | 13.396 | 0.077 | Beaver | 4 | 17 | 1 | 1 | 27.3 |  |
| 0072 | 31.03 | 0.166 | Sevier | 4 | 19 | 1 | 1 | 27.1 |  |
| 0153 | 10.263 | 0.081 | Beaver | 4 | 18 | 1 | 1 | 25.9 |  |
| 0012 | 40.771 | 0.157 | Garfield | 4 | 120 | 9 | 7 | 24.9 |  |
| 0072 | 10.002 | 0.182 | Sevier | 4 | 21 | 2 | 1 | 24.7 |  |
| 0035 | 18.541 | 0.218 | Wasatch | 3 | 86 | 5 | 5 | 24.6 |  |
| 0022 | 4.432 | 0.092 | Garfield | 4 | 21 | 1 | 1 | 24.4 |  |
| 0035 | 44.852 | 0.082 | Duchesne | 3 | 42 | 3 | 2 | 2 |  |
| 0035 | 5.939 | 0.082 | Summit | 2 | 64 | 4 | 3 | 2 |  |

A discussion of applied constraints to eliminate segments like these is presented later in Section 9.3.4. For this reason, only segments with at least three severe crashes will be analyzed individually in this section. The vast majority of the curves listed are along TLTW rural highways. VMT numbers are low because of short segment lengths.

The following sections contain descriptions of the segments highlighted in green in Table 9.2. They include additional information about the types of crashes that were typical of the curve, as well as images of the curves and details about their properties and locations.

### 9.3.1.1 Segment 1: SR-66, MP 2.47, Morgan - Region 1

Figure 9.3 contains images of a curve located just above East Canyon Reservoir near Morgan. The curve in question is highlighted in yellow. Three crashes occurred on this curve between the years of 2010 and 2015, and all of them were severe. The image on the top righthand corner shows that it is a blind curve with a steep cut on one side and a steep drop-off with a guardrail on the other. Overturn/rollover crashes accounted for two out of the three crashes. There are presently no curve advisory signs warning drivers of the curve. As illustrated by the red dots in the lower left-hand corner of Figure 9.3, all crashes on this segment occurred in the middle of the curve at approximately the same location.

### 9.3.1.2 Segment 2: SR-12, MP 40.77, Escalante - Region 4

Figure 9.4 contains images of a compound curve located along SR- 12 between Henrieville and Escalante. This particular curve had nine crashes between the years of 2010 and 2015, seven of which were classified as severe. While there were no fatalities, five crashes involved incapacitating injuries, most of which were motorcycle-related. This location has two sharp, blind curves directly adjacent to each other. A steep, tall cut exists on one side with a steep drop off on the other, partially protected by a guardrail. There is also a grade on this curve. While there are chevron signs along the outside of the curve, there are no advanced warning or advisory speed signs. Roadway departure was the most common type of crash.


Figure 9.3 Segment 1: SR-66, MP 2.47, Morgan - Region 1 (Esri 2017, Google 2017, and UDOT 2017)


Figure 9.4 Segment 2: SR-12, MP 40.77, Escalante - Region 4 (Esri 2017, Google 2017, and UDOT 2017)

### 9.3.1.3 Segment 3: SR-35, MP 18.54, Wolf Creek Pass - Region 3

Figure 9.5 contains images of a curve near Wolf Creek Pass, just south of the Uinta mountain range. This particular curve lies in Region 3. Five severe crashes (also five total) crashes have occurred at this location between the years of 2010 and 2015. As can be seen, this is a horseshoe curve with chevron signs marking the outer edge. Curve advisory speed signs indicating a curve were present as of 2015. A noticeable grade is also present. Driving under the influence (DUI) and high speed were involved in some crashes, and many of the crashes were also motorcycle-related.


Figure 9.5 Segment 3: SR-35, MP 18.54, Hanna - Region 3 (Esri 2017, UDOT 2015, and UDOT 2017)

### 9.3.1.4 Segment 4: SR-35, MP 5.939, Francis - Region 2

Figure 9.6 shows a curve located near Francis, in Region 2. Out of four total crashes between 2010 and 2015, three were considered to be severe. While this is a gradual curve, the steep cut on the inside makes it a blind curve. Trees line the outside of the curve close to the roadway. According to AGRC crash data (crashmapping.utah.gov), some crashes involved trees
or shrubbery (UDOT 2015). DUI, high speed, and adverse road conditions were also common contributing factors.


Figure 9.6 Segment 4: SR-35, MP 5.939, Francis - Region 2 (Esri 2017, UDOT 2015, and UDOT 2017)

### 9.3.1.5 Segment 5: SR-171, MP 8.728, West Valley City

Figure 9.7 contains images of a gradual curve at the intersection of 3300 South and Cultural Center Drive, West Valley City. This segment was not listed in Table 9.2 because it did not have a high enough crash rate to be listed in the top 20 curves. However, it was deemed worthy of further analysis because it is the curve with the highest severe crash rate out of any urban area. The crash rate is 11.2 severe crashes/ 1 million VMT, with a total of 25 severe crashes between 2010 and 2015. The vast majority of crashes were intersection-related.


Figure 9.7 Segment 5: SR-171, MP 8.728, West Valley City (Esri 2017, Google 2017, and UDOT 2017)

### 9.3.2 Segments Ordered by Total Crash Rate

Table 9.3 contains a list of the top 20 segments organized by total crash rate, expressed in terms of total crashes per 1 million VMT. This list includes curves affected by intersections. There is some overlap between segments listed in Table 9.2 and Table 9.3. However, most curves are unique to their respective tables. The segments highlighted in green will again be analyzed. Table 9.3 is more affected by intersections than Table 9.2 and it also contains curves located in urban areas. SR-153 in Beaver is a particular standout in this list again, primarily because it experiences very little traffic and its low AADT values have a tendency to exaggerate the total crash rate. For this reason, it will not be examined further in this report.
Table 8.9 Curves Organized by Total Crash Rate

| Route | Beg MP | Length <br> (mi) | County | Region | $\begin{aligned} & \text { VMT } \\ & \text { (/day) } \end{aligned}$ | Total \# of Crashes | \# of Severe Crashes | Total Rate (\#/MVMT) | Segment \# |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0153 | 22.894 | 0.043 | Piute | 4 | 1 | 1 | 0 | 490.1 |  |
| 0153 | 21.953 | 0.121 | Piute | 4 | 3 | 1 | 0 | 174.2 |  |
| 0144 | 0.008 | 0.047 | Utah | 3 | 18 | 4 | 1 | 115.1 |  |
| 0153 | 37.891 | 0.204 | Piute | 4 | 5 | 1 | 0 | 103.3 |  |
| 0057 | 2.982 | 0.091 | Emery | 4 | 13 | 2 | 0 | 74.3 |  |
| 0030 | 121.383 | 0.122 | Rich | 1 | 99 | 13 | 4 | 62.7 | 6 |
| 0102 | 10.449 | 0.048 | Box Elder | 1 | 18 | 3 | 1 | 61.7 |  |
| 0029 | 9.589 | 0.035 | Emery | 4 | 9 | 1 | 0 | 59.5 |  |
| 0092 | 21.956 | 0.046 | Utah | 3 | 30 | 3 | 0 | 59.4 |  |
| 0144 | 2.079 | 0.046 | Utah | 3 | 17 | 2 | 1 | 58.8 |  |
| 0066 | 4.944 | 0.082 | Morgan | 1 | 36 | 4 | 3 | 55.2 |  |
| 0161 | 2.79 | 0.039 | Millard | 4 | 4 | 1 | 0 | 55.1 |  |
| 0029 | 5.848 | 0.04 | Emery | 4 | 11 | 1 | 0 | 52.1 |  |
| 0072 | 10.002 | 0.182 | Sevier | 4 | 21 | 2 | 1 | 49.4 |  |
| 0101 | 14.093 | 0.044 | Cache | 1 | 18 | 2 | 0 | 48.2 |  |
| 0153 | 7.258 | 0.044 | Beaver | 4 | 10 | 1 | 0 | 47.7 |  |
| 0065 | 14.396 | 0.043 | Morgan | 1 | 17 | 2 | 0 | 47.6 |  |
| 0066 | 2.469 | 0.074 | Morgan | 1 | 33 | 3 | 3 | 45.9 |  |
| 0095 | 48.868 | 0.066 | San Juan | 4 | 11 | 1 | 1 | 45.4 |  |
| 0022 | 3.994 | 0.051 | Garfield | 4 | 11 | 1 | 0 | 44.0 |  |

### 9.3.2.1 Segment 6: SR-30, MP 121.38, Laketown

Figure 9.8 shows a curve located near Bear Lake in Region 1. This is a 90 -degree blind curve with steep cuts on both sides and a runaway truck ramp tangent to it. A 7 percent grade exists south of the curve. Thirteen crashes occurred along this curve between 2010 and 2015, primarily at the beginning and end points. Roadway departure and overturn/rollover were the most common crash types. Many were motorcycle-related and speed-related and some occurred in adverse weather conditions. Chevron and curve advisory speed signs are present. The advisory speed is 30 mph for traffic going east and south (uphill), while the advisory speed is 20 mph for traffic going north and west (downhill).


Figure 9.8 Segment 6: SR-30, MP 121.38, Laketown (Esri 2017, Google 2017, and UDOT 2017)

### 9.3.3 Segments Ordered by Severe Crash Rate with Superelevation Transition

Table 9.4 is similar to Table 9.2 in that it contains a list of the curves with the highest severe crash rates. The difference is that the curves listed in Table 9.4 add superelevation transition segments to the total curve length, increasing the potential for more crashes to be included within the curves. Segments highlighted in blue match those listed in Table 9.2, so as to provide an idea of how much including superelevation transition segments alters the ranking.

Three of the curves in Table 9.4 are not listed in Table 9.2. The segment highlighted in green will be examined further in this section.

### 9.3.3.1 Segment 7: SR-68, MP 11.74, Elberta

Figure 9.9 shows a curve on the southwest side of Utah Lake near Elberta, in Region 3. Eight severe crashes occurred either on the curve or in the superelevation transition segments between 2010 and 2015. As shown in the lower right-hand corner of the figure, many of the crashes occurred at the beginning and end of the curve. This is why this particular segment was not ranked in the 20 curves with the highest severe crash rate. The most common crash types were road departure and overturn/rollover. This curve is located after a particularly long straight segment, possibly catching drivers unaware. There are curve advisory speed signs located on both ends of the curve. Speed-related crashes were common, and many involved either motorcycles or commercial vehicles. Adverse weather conditions were also a factor.
Table 9.4 Curves Organized by Severe Crash Rate with Superelevation Transition

| Route | Beg MP | Length <br> $(\mathbf{m i})$ | County | Region | VMT <br> $(\mathbf{d a y})$ | Total \# of <br> Crashes | \# of Severe <br> Crashes | Severe Rate <br> (\#/MVMT) | Segment <br> \# |
| :--- | :--- | :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 0095 | 48.855 | 0.091 | San Juan | 4 | 11 | 1 | 1 | 32.9 |  |
| 0066 | 2.45 | 0.113 | Morgan | 1 | 33 | 3 | 3 | 30.2 |  |
| 0153 | 3.624 | 0.084 | Beaver | 4 | 11 | 1 | 1 | 25.5 |  |
| 0066 | 4.918 | 0.134 | Morgan | 1 | 36 | 4 | 3 | 25.3 |  |
| 0092 | 18.533 | 0.073 | Utah | 3 | 29 | 3 | 2 | 24.8 |  |
| 0123 | 11.198 | 0.126 | Carbon | 4 | 13 | 1 | 1 | 24.2 |  |
| 0144 | 2.07 | 0.063 | Utah | 3 | 17 | 2 | 1 | 21.4 |  |
| 0072 | 31.006 | 0.213 | Sevier | 4 | 19 | 1 | 1 | 21.1 |  |
| 0057 | 3.487 | 0.161 | Emery | 4 | 18 | 1 | 1 | 21.0 |  |
| 0153 | 10.031 | 0.1 | Beaver | 4 | 16 | 1 | 1 | 20.9 |  |
| 0035 | 18.517 | 0.267 | Wasatch | 3 | 86 | 5 | 5 | 20.2 |  |
| 0153 | 10.251 | 0.106 | Beaver | 4 | 18 | 1 | 1 | 19.8 |  |
| 0012 | 40.74 | 0.198 | Garfield | 4 | 120 | 9 | 7 | 19.7 |  |
| 0153 | 13.381 | 0.107 | Beaver | 4 | 17 | 1 | 1 | 19.6 |  |
| 0068 | 11.74 | 0.163 | Utah | 3 | 127 | 13 | 8 | 19.4 | 7 |
| 0226 | 0.422 | 0.105 | Weber | 1 | 14 | 1 | 1 | 19.4 |  |
| 0072 | 9.977 | 0.233 | Sevier | 4 | 21 | 2 | 1 | 19.3 |  |
| 0144 | 0.0 | 0.076 | Utah | 3 | 18 | 4 | 1 | 17.8 |  |
| 0226 | 0.485 | 0.119 | Weber | 1 | 18 | 1 | 1 | 17.2 |  |
| 0066 | 1.999 | 0.123 | Morgan | 1 | 16 | 1 | 1 | 17.1 |  |



Figure 9.9 Segment 7: SR-68, MP 11.74, Elberta (Esri 2017, Google 2017, and UDOT 2017)

### 9.3.4 Example of Using Filtering Constraints

A problem with these lists is that curves with very little traffic sometimes pair with a single severe crash that causes their crash rate to rank highly. One possible solution to this problem would be to apply constraints to eliminate segments with very few crashes from consideration. This would be up to the user's discretion. This technique is effective in filtering out curves that are ranked highly due to low VMT values. Table 9.5 contains a list of segments organized by severe crash rate with a minimum number of three severe crashes per segment. This was done using Microsoft Excel's Filter tool by unchecking boxes next to 0, 1, and 2 for the severe crash column. Segments highlighted in blue are also included in Table 9.2, which does not apply the constraint. Segments highlighted in green are discussed further.
Table 9．5 Curves Organized by Severe Crash Rate with Constraint

|  |  |  |  |  |  |  |  |  |  |  | $\infty$ |  |  |  | 응 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $19$ | $\underset{\sim}{7}$ |  |  |  |  |  |  |  | $\xrightarrow{\sim}$ | $\stackrel{\square}{\square}$ | $\circ$ | $\cdots$ | 9 | － | N | 9 | $\bigcirc$ | 9 | $\stackrel{-}{\square}$ |
|  |  | m | N | n | m | in | m | － | － |  | m | m | $+$ | m | in | in | － | m | ＋ | n |
|  |  | ＋ | $a$ | n | ＋ | $a$ | m |  | － |  | ＋ | － | $\bigcirc$ | ＋ | $\exists$ | $\stackrel{\sim}{\sim}$ | $\bigcirc$ | 응 | n | U |
| 昆荋 |  | m | 윽 | $\infty$ | \％ | 윽 | 0 | 2 | J | \％ | 긴 | N | $\left\lvert\, \begin{gathered} \underset{\sim}{n} \\ \underset{N}{2} \end{gathered}\right.$ | $\bigcirc$ | ${ }_{\sim}^{\sim}$ | $\underset{\sim}{\circ}$ | $\underset{\mathrm{N}}{\mathrm{O}}$ | $\frac{0}{2}$ | a | － |
|  |  | － | $+$ | m | $N$ | m | － | $\rightarrow$ | m | N | m | ＋ | m | m | m | N | － | $N$ |  | N |
| $\begin{aligned} & \text { 宿 } \\ & \text { 0 } \end{aligned}$ | $\begin{array}{\|c\|} \text { 哥 } \\ 0 \\ \vdots \\ \vdots \end{array}$ | 嵒 |  |  | 䓵 | 吉 | $\begin{aligned} & \text { y } \\ & 0 \\ & 0 \\ & 3 \end{aligned}$ | $\begin{array}{\|c} \stackrel{9}{4} \\ \text { un } \end{array}$ | $\stackrel{\text { n }}{\substack{5}}$ |  | $\begin{array}{\|l\|} \hline \text { ⿹ㅔ } \\ \stackrel{y}{5} \\ \hline \end{array}$ | $\begin{array}{r} \text { a } \\ \text { 可 } \end{array}$ | $\begin{array}{\|c} \stackrel{7}{7} \\ \stackrel{y}{5} \\ \hline \end{array}$ | 喿 | 尔 | 克 | 吉 |  | － | 皆 |
|  | $\begin{aligned} & 2 \\ & 0 \\ & 0 \end{aligned}$ | $0$ | $0$ | $\stackrel{\infty}{2}$ | $\begin{aligned} & \infty \\ & 0 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{array}{\|c} 0 \\ 0 \\ 0 \\ \hline \end{array}$ | 筞 | त | $\xrightarrow{\text { N }}$ | $\left\lvert\, \begin{gathered} n \\ 0 \\ 0 \\ 0 \end{gathered}\right.$ | $\begin{aligned} & 2 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | $\left\lvert\, \begin{gathered} \hat{n} \\ 0 \\ \hline \end{gathered}\right.$ | $\begin{gathered} \infty \\ 0 \\ 0 \\ \hline \end{gathered}$ | ？ | N | $\begin{aligned} & N \\ & 0 \\ & 0 \end{aligned}$ | $\stackrel{\circ}{0}$ | $0$ | － | in |
|  | $\begin{array}{\|c\|} 0 \\ 0 \\ \vdots \\ i \end{array}$ | $\begin{aligned} & 7 \\ & 9 \\ & 7 \end{aligned}$ | $\begin{aligned} & \underset{\sim}{\mathrm{N}} \\ & \mathrm{O} \\ & \mathrm{O} \end{aligned}$ | $\begin{aligned} & -7 \\ & 1 \\ & n \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{gathered} c \\ 0 \\ n \\ n \end{gathered}$ | $\begin{aligned} & \infty \\ & \infty \\ & \vdots \\ & \hline \end{aligned}$ | － | $\begin{gathered} \infty \\ \underset{\sim}{\infty} \\ \underset{\sim}{2} \end{gathered}$ | $\begin{aligned} & \overrightarrow{7} \\ & 9 \\ & \end{aligned}$ |  | $\begin{gathered} \hat{6} \\ \hat{0} \\ \underset{\sim}{9} \end{gathered}$ | $\begin{gathered} \hat{o} \\ 0 \\ 0 \\ 0 \\ \hline \end{gathered}$ | $\begin{aligned} & \stackrel{\infty}{\infty} \\ & \underset{\sim}{2} \end{aligned}$ | $\begin{aligned} & \infty \\ & n \\ & n \\ & m \\ & - \end{aligned}$ | $\begin{aligned} & \text { I } \\ & \underset{\sim}{n} \end{aligned}$ | $\begin{gathered} \infty \\ 0 \\ 0 \\ \hdashline \end{gathered}$ | － | $\underset{\substack{7 \\ \underset{0}{2} \\ \hline}}{ }$ | $\stackrel{\infty}{\text { N }}$ | com |
|  | $\left\lvert\, \begin{array}{l\|} \hline 8 \\ 8 \\ \hline 8 \end{array}\right.$ | $\begin{aligned} & \circ \\ & \hline 8 \\ & \hline 8 \end{aligned}$ | $3$ | $\begin{aligned} & n \\ & \\ & 0 \end{aligned}$ | $\begin{aligned} & n \\ & 0 \\ & 8 \end{aligned}$ | $0$ | $\begin{aligned} & 0 \\ & 8 \\ & 8 \end{aligned}$ | $\begin{aligned} & 0 \\ & \hline 0 \\ & 8 \end{aligned}$ | O | $\overrightarrow{0}$ | $\left\lvert\, \begin{array}{l\|} \hline 8 \\ \hline 8 \\ \hline \end{array}\right.$ | $\underset{\infty}{n}$ | $0$ | $\begin{aligned} & \circ \\ & \hline 8 \\ & \hline 8 \end{aligned}$ | $0$ | N | $\frac{7}{8}$ | 잉 | O | 잉 |

Only the top five segments in Table 9.5 are listed in Table 9.2. A few urban segments make the list in Table 9.5 now that there is a minimum crash number criterion. Curves from Region 3 now account for 35 percent of the segments listed in Table 9.5 and curves from Region 4 now make up 15 percent. In Table 9.2, curves from Region 3 make up 25 percent and Region 4 makes up 50 percent. This illustrates that different constraints yield quite different results.

### 9.3.4.1 Segments 8, 9, and 10: US-6, MP 143.12-143.75, Eureka

Figure 9.10 contains images of three curves; all of them lie within close proximity of each other along US-6 between Eureka and Goshen. These curves warranted a closer look because all of them separately make the list of segments in Table 9.5. This section of road contains sharp, winding curves with a steep grade. While some advisory signs do exist, a total of 11 severe crashes occurred between the years of 2010 and 2015. The crash types were most commonly overturn/rollover or roadway departure. Eastbound drivers encounter a steep downgrade and must slow down carefully while navigating consecutive curves.


Figure 9.10 Segments 8, 9, and 10: US-6, MP 143.12-143.75, Eureka (Esri 2017, Google 2017, and UDOT 2017)

### 9.4 Chapter Summary

Table 9.2 through Table 9.5 show that TLTW rural highway curves frequently show up in lists of curves organized by crash rates. The analysis presented in this chapter shows that many severe injuries stem from motorcycle-related crashes. Additionally, the most common types of crashes for curves with high crash rates without intersections appear to be roadway departure and overturn/rollover. Blind curves were also present in many of the curves analyzed. Interestingly, no interstates made the lists of curves with the highest crash rate, likely due to high traffic volumes. While curves with intersections were included in these lists, the user could also order segments by crash rate without intersections if they wished.

The program to combine crash data with curve data works well. Curves with high crash occurrences can be identified in order to make improvements to them. Additionally, particular attributes of different curves can be analyzed to identify correlations between a certain property
and crashes. Curves with the highest severe crash rates often had several motorcycle-related crashes, which is something that could be explored further. The program provides flexible filtering options and choices for analyzing curves.

### 10.0 CONCLUSIONS AND RECOMMENDATIONS

### 10.1 Summary

This research was effective in testing and improving the original HAF Algorithm, as well as combining curve data with crash data. The study objectives were met, including testing the HAF Algorithm's ability to cover types of highways other than rural TLTW, improving its accuracy, combining curve data with crash data to identify highway curves with high crash occurrences, and combining curve data with roadway parameters such as radius, curve length, AADT, and other fields to aid in future analysis. The HAF Algorithm was tested for other (i.e. non-TLTW) highway types by comparing the calculated results to results obtained by measuring curve parameters using satellite imagery. The algorithm was improved by making changes to the code that targeted a few specific errors and updating the code to make it compatible with more recent data. Finally, a VBA program was developed to combine curve data with crash data and other roadway parameters like AADT, functional class, speed limit, urban code, and the number of lanes.

Included in this chapter are a summary of the findings and some limitations inherent with the raw LiDAR data and the HAF Algorithm.

### 10.2 Findings

This section contains research findings, separated into three parts: (1) results of the HAF Algorithm calibration to determine whether it works across all highway types, (2) results of the improved HAF Algorithm accuracy compared to the original algorithm, and (3) an outline of the findings from the curve and crash data combination.

### 10.2.1 Results of HAF Algorithm Tests for Other Highway Types

After an initial calibration phase, it was determined that the HAF Algorithm did not need to be modified to accommodate types of highways other than rural TLTW. Curve identification
accuracy ranged from 71-96 percent, depending on highway type. Additionally, curve length calculation accuracy ranged from 91-96 percent.

### 10.2.2 Results of HAF Algorithm Improvements

Six specific errors were targeted to improve the HAF Algorithm - tangent-curve-tangent, tangent identification, curve fragment, curve length calculation, intersection identification, and compound curve errors. The details of these errors are explained in depth in Chapter 5. Intersection, curve fragment, and curve length calculation errors were reduced significantly, while the tangent fix was less effective. The compound curve error was reduced by changing the calibration process to allow for compound curves, and the tangent-curve-tangent error could not be resolved due to problems with the raw LiDAR data.

Curve identification accuracy now ranges from 87 to near 100 percent, depending on highway type. These improvements are due primarily to resolving curve fragment and intersection identification errors. Curve length calculation accuracy now lies within 97-98 percent. At this point, human error in the calibration process has the potential to affect these results, so no further improvement to curve length calculation is warranted. The elimination of the arc length calculation error was one of the primary causes of this improvement. Radius accuracy could not be improved due to the limitations of the input data. Additionally, as part of the process of improving the HAF Algorithm, changes were made to the code and interface to allow the program to run 2015 data.

### 10.2.3 Curve Data/Crash Data Combination

The new VBA program written to combine curve data with crash data was successful. Each curve segment lists the total number of crashes and the number of crashes in each severity type that occurred within a specified time span as well as their respective crash rates. Additionally, roadway data such as AADT, functional class, speed limit, urban code, and lanes have been effectively combined in order to display the roadway parameters associated with each curve. Superelevation transition segments can also be accounted for in the new algorithm.

### 10.3 Limitations and Challenges

There are still some limitations to the accuracy of the HAF Algorithm despite the improvements made in this research. The algorithm itself can only be as accurate as the data inputs. While the provided LiDAR data are very accurate, there are occasional issues that surface, particularly in determining the start and end points of each segment. This was primarily responsible for the tangent-curve-tangent error, which the algorithm was not able to overcome because it cannot divide individual segments. Additionally, improving radius calculation accuracy is difficult due to errors in the data. These types of errors are likely to be reduced best by trying to obtain more accurate input data in the future.

### 10.4 Recommendations

Possibilities exist for this research to be furthered. For example, the radius calculation has room for improvement. While improving the radius calculation accuracy in the HAF Algorithm itself may not be possible, further research could be done into developing a tool in ArcMap that automatically calculates curve radius. This would likely require advanced Python scripting, but it may be possible.

Further research could also be done into motorcycle related crashes. Many of the segments listed in Chapter 9 had high numbers of severe motorcycle related crashes. This type of research could provide a basis on which to identify motorcycle safety improvements.

Additionally, further research could be done into common causes of crashes along Utah highway curves. While curves with worse crash histories have been identified, no statistical analysis has been done to determine which curve parameters correlate with higher crash rates. This would certainly be worthy of a study of its own as it has the potential to aid UDOT in constructing and maintaining safer highway curves. Because several parameters are affixed to each curve in the output of the new VBA program, this research provides a good starting point from which to do further analysis of crashes on curves.

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## APPENDIX A: HAF CALIBRATION DATA

This appendix includes data that were used for the HAF calibration portion of the project. This table includes comparisons of the measured and HAF-calculated results for each highway type. The results include curve length, radius, and percent error for the original algorithm, and the data used were obtained from 2012 Mandli data.

Table A. 1 contains the calibration results for urban interstates, Table A. 2 contains results for rural interstates, Table A. 3 contains results for urban multilane highways, Table A. 4 contains results for rural multilane highways, Table A. 5 contains results for urban TLTW highways, and Table A. 6 contains results for rural TLTW highways.

Table A. 1 Urban Interstate Calibration.

| $\boldsymbol{n} \#$ | ID | Route <br> Name | PC | PT | AutoCAD | ArcMap | Error <br> $\%$ | AutoCAD | ArcMap | Error \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 320696 | 0015 P | 258.0 | 258.5 | 2940 | -3089 | $5.1 \%$ | 2900 | 2916 | $0.6 \%$ |
| 2 | 320710 | 0015 P | 267.3 | 267.6 | 1794 | -2148 | $19.7 \%$ | 1460 | 1521 | $4.1 \%$ |
| 3 | 316369 | 0215 N | 7.6 | 7.4 | 1922 | 2802 | $45.8 \%$ | 877 | 808 | $7.8 \%$ |
| 4 | 296796 | 0084 N | 81.8 | 81.6 | 2308 | 2997 | $29.9 \%$ | 1041 | 1086 | $4.3 \%$ |
| 5 | 321167 | 0015 N | 267.5 | 267.2 | 1740 | 2226 | $27.9 \%$ | 1531 | 1560 | $1.9 \%$ |
| 6 | 316402 | 0215 N | 0.6 | 0.3 | 2454 | -2440 | $0.6 \%$ | 1645 | 1727 | $4.9 \%$ |
| 7 | 316323 | 0215 N | 22.8 | 22.7 | 2547 | 4806 | $88.7 \%$ | 691 | 711 | $2.9 \%$ |
| 8 | 320716 | 0015 P | 270.0 | 270.4 | 3055 | 4182 | $36.9 \%$ | 1841 | 1775 | $3.6 \%$ |
| 9 | 320508 | 0015 P | 0.0 | 0.1 | 3173 | 5005 | $57.7 \%$ | 631 | 674 | $6.8 \%$ |
| 10 | 316352 | 0215 N | 11.4 | 11.3 | 3124 | 2247 | $28.1 \%$ | 527 | 535 | $1.4 \%$ |
| 11 | 321068 | 0015 N | 307.1 | 306.8 | 1878 | 2040 | $8.7 \%$ | 1627 | 1649 | $1.4 \%$ |
| 12 | 295990 | 0080 P | 124.6 | 124.7 | 4380 | 5034 | $14.9 \%$ | 519 | 497 | $4.2 \%$ |
| 13 | 316284 | 0215 P | 13.7 | 14.6 | 3213 | 3236 | $0.7 \%$ | 4857 | 4859 | $0.1 \%$ |
| 14 | 316311 | 0215 P | 28.3 | 28.9 | 1545 | -2312 | $49.7 \%$ | 3405 | 3296 | $3.2 \%$ |
| 15 | 321031 | 0015 N | 318.7 | 318.5 | 1854 | 2730 | $47.2 \%$ | 881 | 951 | $7.9 \%$ |
| 16 | 320518 | 0015 P | 5.8 | 6.8 | 5341 | 5082 | $4.8 \%$ | 4941 | 4897 | $0.9 \%$ |
| 17 | 320707 | 0015 P | 266.8 | 267.2 | 2400 | 2485 | $3.6 \%$ | 1704 | 1664 | $2.4 \%$ |
| 18 | 320510 | 0015 P | 2.9 | 3.0 | 3916 | -935 | $76.1 \%$ | 757 | 1598 | $111.1 \%$ |
| 19 | 322474 | 0080 N | 119.6 | 119.3 | 854 | -935 | $9.4 \%$ | 1684 | 1598 | $5.1 \%$ |
| 20 | 316404 | 0215 N | 0.3 | 0.2 | 2028 | 2541 | $25.3 \%$ | 714 | 672 | $5.9 \%$ |
| 21 | 320748 | 0015 P | 286.0 | 286.4 | 2533 | 3600 | $42.2 \%$ | 2121 | 2044 | $3.6 \%$ |
| 22 | 296526 | 0084 P | 88.9 | 89.1 | 1639 | -2079 | $26.8 \%$ | 969 | 1006 | $3.8 \%$ |


|  |  |  |  |  | RADIUS |  |  | CURVE LENGTH |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | ID | Route <br> Name | PC | PT | AutoCAD | ArcMap | $\begin{gathered} \text { Error } \\ \% \end{gathered}$ | AutoCAD | ArcMap | Error \% |
| 23 | 321063 | 0015N | 307.8 | 307.7 | 1467 | 2514 | 71.4\% | 547 | 498 | 8.9\% |
| 24 | 296798 | 0084N | 81.2 | 80.9 | 2652 | 2847 | 7.3\% | 1724 | 1751 | 1.6\% |
| 25 | 321000 | 0015N | 340.2 | 339.9 | 2801 | -2955 | 5.5\% | 1890 | 1918 | 1.5\% |
| 26 | 295963 | 0080P | 106.7 | 107.1 | 2252 | 2994 | 33.0\% | 2391 | 2299 | 3.8\% |
| 27 | 316321 | 0215N | 26.5 | 26.3 | 3623 | -4725 | 30.4\% | 1002 | 954 | 4.8\% |
| 28 | 320990 | 0015N | 343.5 | 343.3 | 1712 | 2050 | 19.7\% | 982 | 918 | 6.4\% |
| 29 | 316252 | 0215P | 3.9 | 4.1 | 1688 | -2058 | 21.9\% | 1024 | 928 | 9.3\% |
| 30 | 320521 | 0015P | 7.6 | 7.9 | 5103 | -5120 | 0.3\% | 1321 | 1353 | 2.5\% |
| 31 | 321007 | 0015N | 335.9 | 335.7 | 5480 | 4739 | 13.5\% | 645 | 644 | 0.2\% |
| 32 | 320694 | 0015P | 257.6 | 257.6 | 5536 | 5231 | 5.5\% | 400 | 323 | 19.3\% |
| 33 | 316274 | 0215P | 11.4 | 11.7 | 2833 | 2917 | 3.0\% | 1253 | 1261 | 0.6\% |
| 34 | 320998 | 0015N | 340.7 | 340.6 | 2877 | 2908 | 1.1\% | 485 | 453 | 6.6\% |
| 35 | 316398 | 0215N | 1.1 | 0.8 | 2299 | 2547 | 10.8\% | 1391 | 1390 | 0.1\% |
| 36 | 316317 | 0215N | 27.4 | 27.2 | 1219 | 1309 | 7.4\% | 1327 | 1319 | 0.6\% |
| 37 | 296781 | 0084N | 86.0 | 85.9 | 5379 | 4902 | 8.9\% | 780 | 705 | 9.6\% |
| 38 | 320778 | 0015P | 299.2 | 299.6 | 3351 | 3213 | 4.1\% | 1928 | 1886 | 2.2\% |
| 39 | 320798 | 0015P | 306.9 | 307.2 | 2208 | 2228 | 0.9\% | 1822 | 1799 | 1.3\% |
| 40 | 316340 | 0215N | 13.3 | 12.9 | 2317 | 2371 | 2.3\% | 2224 | 2076 | 6.7\% |
| 41 | 320739 | 0015P | 280.4 | 280.7 | 3358 | 3454 | 2.9\% | 2026 | 2002 | 1.2\% |
| 42 | 321145 | 0015N | 272.5 | 272.9 | 3818 | 3686 | 3.5\% | 1867 | 2982 | 59.7\% |
| 43 | 296801 | 0084N | 80.6 | 80.5 | 2166 | 2283 | 5.4\% | 485 | 496.5 | 2.4\% |
| 44 | 320880 | 0015P | 340.7 | 340.8 | 2993 | 3464 | 15.7\% | 576 | 548 | 4.9\% |
| 45 | 316307 | 0215P | 26.8 | 27.4 | 2922 | 3036 | 3.9\% | 3473 | 3454 | 0.5\% |
| 46 | 320516 | 0015P | 4.5 | 4.9 | 2383 | 2476 | 3.9\% | 1731 | 1704 | 1.6\% |
| 47 | 296522 | 0084P | 85.9 | 86.4 | 2922 | 3086 | 5.6\% | 2399 | 2420 | 0.9\% |
| 48 | 321015 | 0015N | 329.6 | 329.3 | 4894 | 4652 | 4.9\% | 1555 | 1574 | 1.2\% |
| 49 | 320775 | 0015P | 298.6 | 299.0 | 4638 | 4622 | 0.3\% | 2150 | 2183 | 1.5\% |
| 50 | 320853 | 0015P | 326.6 | 326.6 | 5457 | 4015 | 26.4\% | 272 | 268 | 1.5\% |
| 51 | 316338 | 0215N | 14.0 | 14.6 | 3317 | 3447 | 3.9\% | 3352 | 5056 | 50.8\% |
| 52 | 295979 | 0080P | 119.6 | 119.8 | 1820 | 1946 | 6.9\% | 935 | 927 | 0.9\% |
| 53 | 321116 | 0015N | 286.2 | 285.8 | 2769 | 2977 | 7.5\% | 1866 | 1889 | 1.2\% |
| 54 | 321080 | 0015N | 303.3 | 303.1 | 3010 | 2964 | 1.5\% | 1022 | 997 | 2.4\% |
| 55 | 320994 | 0015N | 342.5 | 341.8 | 2822 | 2819 | 0.1\% | 3558 | 3560 | 0.1\% |
| 56 | 320984 | 0015N | 346.0 | 345.7 | 3772 | 4717 | 25.1\% | 1464 | 1426 | 2.6\% |
| 57 | 316278 | 0215P | 12.1 | 12.7 | 3822 | 4321 | 13.1\% | 2850 | 2852 | 0.1\% |
| 58 | 316258 | 0215P | 7.4 | 7.5 | 3047 | 2931 | 3.8\% | 877 | 862 | 1.7\% |
| 59 | 320893 | 0015P | 346.4 | 346.7 | 3802 | 4306 | 13.3\% | 1284 | 1291 | 0.5\% |
| 60 | 321196 | 0015N | 249.0 | 248.5 | 5975 | 5051 | 15.5\% | 2644 | 2616 | 1.1\% |
| 61 | 320864 | 0015P | 329.5 | 329.7 | 5123 | 4631 | 9.6\% | 1472 | 1468 | 0.3\% |


|  |  |  |  |  | RADIUS |  |  | CURVE LENGTH |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | ID | Route Name | PC | PT | AutoCAD | ArcMap | $\begin{gathered} \text { Error } \\ \% \end{gathered}$ | AutoCAD | ArcMap | Error \% |
| 62 | 316375 | 0215N | 4.1 | 4.0 | 1943 | 1999 | 2.9\% | 1073 | 1041 | 3.0\% |
| 63 | 320977 | 0015N | 350.6 | 350.4 | 5860 | 4892 | 16.5\% | 1264 | 1278 | 1.1\% |
| 64 | 296786 | 0084N | 85.1 | 85.6 | 2870 | 3556 | 23.9\% | 2545 | 3202 | 25.8\% |
| 65 | 321011 | 0015N | 330.7 | 330.4 | 2112 | 2174 | 2.9\% | 1688 | 1681 | 0.4\% |
| 66 | 296524 | 0084P | 88.2 | 88.3 | 2850 | 2954 | 3.6\% | 813 | 790 | 2.8\% |
| 67 | 320523 | 0015P | 8.7 | 9.3 | 3734 | 4055 | 8.6\% | 2778 | 2746 | 1.2\% |
| 68 | 316269 | 0215P | 10.9 | 11.2 | 2051 | 2110 | 2.9\% | 1205 | 1183 | 1.8\% |
| 69 | 321378 | 0015N | 6.8 | 5.9 | 5570 | 4954 | 11.1\% | 4457 | 4408 | 1.1\% |
| 70 | 316247 | 0215P | 3.0 | 3.4 | 3969 | 4316 | 8.7\% | 1978 | 1953 | 1.3\% |
| 71 | 322476 | 0080N | 118.8 | 118.7 | 3330 | 3011 | 9.6\% | 475 | 466 | 1.9\% |
| 72 | 321369 | 0015N | 13.7 | 13.3 | 5603 | 5047 | 9.9\% | 2482 | 2499 | 0.7\% |
| 73 | 295999 | 0080P | 127.1 | 127.4 | 1098 | 1267 | 15.4\% | 1284 | 1272 | 0.9\% |
| 74 | 316229 | 0215P | 0.0 | 0.2 | 2166 | 2411 | 11.3\% | 888 | 1142 | 28.6\% |
| 75 | 320878 | 0015P | 340.0 | 340.4 | 2745 | 2813 | 2.5\% | 1824 | 1833 | 0.5\% |
| 76 | 320861 | 0015P | 328.9 | 329.3 | 2941 | 3095 | 5.2\% | 2481 | 2467 | 0.6\% |
| 77 | 322470 | 0080N | 122.6 | 122.2 | 1052 | 1092 | 3.8\% | 1654 | 1760 | 6.4\% |
| 78 | 295971 | 0080P | 118.1 | 118.3 | 3756 | 4720 | 25.7\% | 950 | 961 | 1.2\% |
| 79 | 316348 | 0215N | 11.9 | 11.8 | 2786 | 3088 | 10.8\% | 750 | 732 | 2.4\% |
| 80 | 321181 | 0015N | 264.5 | 264.4 | 4611 | 3511 | 23.9\% | 609 | 618 | 1.5\% |
| 81 | 320988 | 0015N | 343.9 | 343.6 | 2056 | 2176 | 5.8\% | 1822 | 1796 | 1.4\% |
| 82 | 316315 | 0215N | 28.8 | 28.4 | 1460 | 1452 | 0.5\% | 2011 | 2058 | 2.3\% |
| 83 | 320982 | 0015N | 346.6 | 346.3 | 3872 | 4097 | 5.8\% | 1340 | 1341 | 0.1\% |
| 84 | 320703 | 0015P | 264.5 | 264.6 | 3884 | 3930 | 1.2\% | 666 | 683 | 2.6\% |
| 85 | 316357 | 0215N | 10.9 | 10.7 | 1933 | 2135 | 10.5\% | 1173 | 1159 | 1.2\% |
| 86 | 320824 | 0015P | 312.4 | 312.8 | 2208 | 2390 | 8.2\% | 1824 | 1844 | 1.1\% |
| 87 | 321192 | 0015N | 257.5 | 257.4 | 5999 | 4925 | 17.9\% | 479 | 456 | 4.8\% |
| 88 | 320792 | 0015P | 304.2 | 304.3 | 2902 | 2847 | 1.9\% | 604 | 596 | 1.3\% |
| 89 | 320839 | 0015P | 318.6 | 318.7 | 1644 | 1831 | 11.4\% | 977 | 996 | 1.9\% |
| 90 | 320813 | 0015P | 310.4 | 310.5 | 5172 | 4624 | 10.6\% | 581 | 561 | 3.4\% |
| 91 | 320859 | 0015P | 328.5 | 328.7 | 4646 | 4543 | 2.2\% | 1200 | 1197 | 0.3\% |
| 92 | 320770 | 0015P | 297.9 | 298.0 | 5832 | 5244 | 10.1\% | 1001 | 979 | 2.2\% |
| 93 | 320512 | 0015P | 3.6 | 3.9 | 5781 | 5398 | 6.6\% | 1102 | 1379 | 25.2\% |
| 94 | 322472 | 0080N | 119.8 | 119.7 | 1169 | 1276 | 9.2\% | 668 | 666 | 0.3\% |
| 95 | 321021 | 0015N | 327.2 | 327.0 | 3732 | 4362 | 16.9\% | 1341 | 1333 | 0.6\% |
| 96 | 316355 | 0215N | 11.2 | 11.0 | 1831 | 1915 | 4.6\% | 1072 | 1084 | 1.2\% |
| 97 | 320735 | 0015P | 279.8 | 280.1 | 3126 | 3273 | 4.7\% | 1779 | 1724 | 3.1\% |
| 98 | 320895 | 0015P | 347.1 | 347.2 | 3797 | 4412 | 16.2\% | 744 | 696 | 6.4\% |
| 99 | 320811 | 0015P | 309.7 | 310.0 | 2825 | 2838 | 0.4\% | 1310 | 1317 | 0.6\% |
| 100 | 321119 | 0015N | 285.1 | 285.0 | 5144 | 5350 | 4.0\% | 578 | 561 | 3.0\% |


| $\boldsymbol{n}$ | RADIUS |  |  |  | CURVE LENGTH |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | ID | Route <br> Name | PC | PT | AutoCAD | ArcMap | Error <br> $\%$ | AutoCAD | ArcMap | Error \% |
| 101 | 320730 | 0015 P | 278.1 | 278.3 | 5942 | 4600 | $22.6 \%$ | 1227 | 1219 | $0.7 \%$ |
| 102 | 321013 | 0015 N | 330.3 | 330.1 | 2106 | 2243 | $6.5 \%$ | 1047 | 1067 | $1.9 \%$ |
| 103 | 296003 | 0080 P | 127.9 | 128.1 | 2678 | 3258 | $21.7 \%$ | 1280 | 1268 | $0.9 \%$ |
| 104 | 322466 | 0080 N | 124.0 | 123.9 | 5120 | 5257 | $2.7 \%$ | 397 | 404 | $1.7 \%$ |
| 105 | 322460 | 0080 N | 126.1 | 125.9 | 2429 | 2473 | $1.8 \%$ | 665 | 634 | $4.6 \%$ |
| 106 | 316245 | 0215 P | 2.6 | 2.7 | 5226 | 4842 | $7.4 \%$ | 502 | 493 | $1.8 \%$ |
| 107 | 295975 | 0080 P | 118.7 | 118.8 | 2897 | 2934 | $1.3 \%$ | 485 | 483 | $0.3 \%$ |

Table A.2: Rural Interstate Calibration

|  |  |  |  |  | RADIUS |  |  | CURVE LENGTH |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | ID | Route <br> Name | PC | PT | AutoCAD | ArcMap | $\begin{gathered} \text { Error } \\ \% \\ \hline \end{gathered}$ | AutoCAD | ArcMap | $\begin{gathered} \text { Error } \\ \% \\ \hline \end{gathered}$ |
| 1 | 294673 | 0070P | 7.1 | 7.3 | 1313 | 1394 | 6.1\% | 1062 | 1091 | 2.7\% |
| 2 | 294683 | 0070P | 11.5 | 11.9 | 1702 | 1908 | 12.1\% | 1484 | 1964 | 32.4\% |
| 3 | 294697 | 0070P | 14.8 | 15.2 | 2100 | 2217 | 5.6\% | 2384 | 2370 | 0.6\% |
| 4 | 294727 | 0070P | 24.2 | 24.7 | 2801 | 3036 | 8.4\% | 2722 | 2718 | 0.1\% |
| 5 | 294734 | 0070P | 28.6 | 28.8 | 2889 | 3105 | 7.5\% | 1434 | 1351 | 5.8\% |
| 6 | 294747 | 0070P | 32.6 | 32.8 | 2562 | 3024 | 18.0\% | 1247 | 1195 | 4.1\% |
| 7 | 294759 | 0070P | 37.9 | 38.2 | 2405 | 2957 | 22.9\% | 1444 | 1382 | 4.3\% |
| 8 | 294772 | 0070P | 47.6 | 47.7 | 1924 | 4674 | 143.0\% | 891 | 833 | 6.6\% |
| 9 | 294774 | 0070P | 48.7 | 48.9 | 3632 | 4953 | 36.4\% | 1117 | 1324 | 18.6\% |
| 10 | 294799 | 0070P | 60.9 | 61.2 | 2101 | 3079 | 46.5\% | 1554 | 1705 | 9.7\% |
| 11 | 294812 | 0070P | 64.1 | 64.2 | 2969 | 3097 | 4.3\% | 607 | 606 | 0.2\% |
| 12 | 294834 | 0070P | 67.7 | 67.9 | 3427 | 4444 | 29.7\% | 1171 | 1311 | 11.9\% |
| 13 | 294863 | 0070P | 71.8 | 71.9 | 1715 | 3837 | 123.7\% | 546 | 363 | 33.6\% |
| 14 | 294871 | 0070P | 72.7 | 72.9 | 2842 | 2991 | 5.2\% | 1546 | 1380 | 10.8\% |
| 15 | 294887 | 0070P | 76.2 | 76.5 | 2064 | 2339 | 13.3\% | 1281 | 1294 | 1.0\% |
| 16 | 294896 | 0070P | 79.0 | 79.2 | 2545 | 3209 | 26.1\% | 721 | 760 | 5.4\% |
| 17 | 294906 | 0070P | 80.4 | 80.5 | 1957 | 1625 | 16.9\% | 516 | 515 | 0.1\% |
| 18 | 294918 | 0070P | 82.6 | 83.0 | 2266 | 2450 | 8.1\% | 1699 | 1739 | 2.3\% |
| 19 | 294927 | 0070P | 84.1 | 84.4 | 2791 | 3051 | 9.3\% | 1364 | 1483 | 8.7\% |
| 20 | 294932 | 0070P | 84.7 | 84.8 | 1666 | 3211 | 92.8\% | 691 | 660 | 4.6\% |
| 21 | 294962 | 0070P | 96.0 | 96.5 | 1548 | 1884 | 21.7\% | 2038 | 2252 | 10.5\% |
| 22 | 294968 | 0070P | 99.9 | 100.0 | 5234 | 4770 | 8.9\% | 687 | 684 | 0.5\% |
| 23 | 294982 | 0070P | 106.1 | 106.8 | 3832 | 4292 | 12.0\% | 3698 | 3689 | 0.3\% |
| 24 | 294998 | 0070P | 113.1 | 113.2 | 2407 | 4536 | 88.4\% | 695 | 510 | 26.6\% |
| 25 | 295029 | 0070P | 118.6 | 118.9 | 2638 | 2892 | 9.6\% | 1318 | 1434 | 8.8\% |
| 26 | 295031 | 0070P | 119.0 | 119.3 | 2823 | 2920 | 3.4\% | 1540 | 1495 | 2.9\% |


|  |  |  |  |  | RADIUS |  |  | CURVE LENGTH |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | ID | Route <br> Name | PC | PT | AutoCAD | ArcMap | $\begin{gathered} \text { Error } \\ \% \end{gathered}$ | AutoCAD | ArcMap | $\begin{gathered} \text { Error } \\ \% \end{gathered}$ |
| 27 | 295044 | 0070P | 123.7 | 124.1 | 2754 | 2892 | 5.0\% | 1832 | 1866 | 1.8\% |
| 28 | 295050 | 0070P | 131.1 | 131.4 | 5826 | 4938 | 15.2\% | 1674 | 1643 | 1.9\% |
| 29 | 295053 | 0070P | 132.5 | 132.9 | 4772 | 5125 | 7.4\% | 2294 | 2317 | 1.0\% |
| 30 | 295066 | 0070P | 140.3 | 141.0 | 1753 | 1860 | 6.1\% | 3240 | 3263 | 0.7\% |
| 31 | 295085 | 0070P | 144.1 | 144.6 | 1135 | 1224 | 7.9\% | 2461 | 2562 | 4.1\% |
| 32 | 295087 | 0070P | 144.7 | 145.0 | 1355 | 1660 | 22.6\% | 1525 | 1571 | 3.0\% |
| 33 | 295094 | 0070P | 145.6 | 145.7 | 1585 | 1845 | 16.4\% | 542 | 546 | 0.7\% |
| 34 | 295106 | 0070P | 162.6 | 163.1 | 2857 | 2971 | 4.0\% | 2904 | 2914 | 0.3\% |
| 35 | 295110 | 0070P | 167.9 | 168.2 | 5743 | 4967 | 13.5\% | 1600 | 1654 | 3.4\% |
| 36 | 295116 | 0070P | 181.9 | 182.0 | 5641 | 5031 | 10.8\% | 912 | 891 | 2.3\% |
| 37 | 295118 | 0070P | 187.7 | 188.2 | 2835 | 3023 | 6.7\% | 2976 | 2930 | 1.6\% |
| 38 | 295953 | 0080P | 62.2 | 62.9 | 4556 | 4804 | 5.4\% | 3361 | 3320 | 1.2\% |
| 39 | 296048 | 0080P | 132.9 | 133.0 | 1048 | 2415 | 130.4\% | 448 | 439 | 1.8\% |
| 40 | 296057 | 0080P | 133.7 | 134.1 | 1267 | 1339 | 5.7\% | 2207 | 2221 | 0.6\% |
| 41 | 296080 | 0080P | 136.3 | 136.7 | 1760 | 1861 | 5.7\% | 2453 | 2515 | 2.6\% |
| 42 | 296167 | 0080P | 150.2 | 150.3 | 1065 | 1309 | 22.9\% | 758 | 783 | 3.3\% |
| 43 | 296192 | 0080P | 153.6 | 153.7 | 1110 | 1324 | 19.3\% | 585 | 557 | 4.8\% |
| 44 | 296196 | 0080P | 155.2 | 155.7 | 2324 | 2459 | 5.8\% | 2864 | 2868 | 0.1\% |
| 45 | 296477 | 0084P | 14.8 | 15.1 | 2136 | 2829 | 32.4\% | 1949 | 1810 | 7.2\% |
| 46 | 296487 | 0084P | 26.0 | 26.2 | 2045 | 4836 | 136.4\% | 622 | 634 | 1.9\% |
| 47 | 296497 | 0084P | 29.3 | 29.4 | 3469 | 4975 | 43.4\% | 923 | 892 | 3.4\% |
| 48 | 296499 | 0084P | 29.9 | 30.1 | 5188 | 4632 | 10.7\% | 732 | 728 | 0.5\% |
| 49 | 296505 | 0084P | 31.4 | 31.5 | 5566 | 5079 | 8.7\% | 804 | 865 | 7.6\% |
| 50 | 296540 | 0084P | 90.5 | 90.6 | 1921 | 2050 | 6.7\% | 661 | 685 | 3.6\% |
| 51 | 296553 | 0084P | 91.5 | 91.6 | 1673 | 1790 | 7.0\% | 553 | 548 | 0.8\% |
| 52 | 296618 | 0084P | 111.9 | 112.3 | 1434 | 1480 | 3.2\% | 1714 | 1774 | 3.5\% |
| 53 | 296620 | 0084P | 112.3 | 112.4 | 1108 | 3713 | 235.2\% | 251 | 257 | 2.6\% |
| 54 | 296665 | 0084N | 111.4 | 111.0 | 1323 | 1545 | 16.8\% | 1647 | 1844 | 11.9\% |
| 55 | 296684 | 0084N | 107.1 | 106.8 | 1072 | 1319 | 23.0\% | 1689 | 1620 | 4.1\% |
| 56 | 296686 | 0084N | 106.8 | 106.4 | 1257 | 1371 | 9.0\% | 2121 | 2129 | 0.4\% |
| 57 | 296716 | 0084N | 96.9 | 96.6 | 1907 | 2038 | 6.9\% | 1558 | 1489 | 4.4\% |
| 58 | 296724 | 0084N | 94.0 | 93.8 | 1718 | 2196 | 27.8\% | 1066 | 1046 | 1.9\% |
| 59 | 296760 | 0084N | 89.5 | 89.5 | 1414 | 1633 | 15.4\% | 391 | 401 | 2.7\% |
| 60 | 320533 | 0015P | 14.3 | 14.6 | 2272 | 2452 | 7.9\% | 1433 | 1404 | 2.0\% |
| 61 | 320556 | 0015P | 35.4 | 35.4 | 4130 | 4310 | 4.4\% | 317 | 240 | 24.4\% |
| 62 | 320603 | 0015P | 138.9 | 139.5 | 2856 | 2877 | 0.7\% | 3119 | 3274 | 5.0\% |
| 63 | 320605 | 0015P | 139.8 | 139.9 | 3559 | 3773 | 6.0\% | 700 | 737 | 5.3\% |
| 64 | 320609 | 0015P | 140.0 | 140.3 | 1915 | 2345 | 22.5\% | 1189 | 1175 | 1.2\% |
| 65 | 320611 | 0015P | 140.3 | 140.8 | 1796 | 1964 | 9.3\% | 2392 | 2390 | 0.1\% |


|  |  |  |  |  | RADIUS |  |  | CURVE LENGTH |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | ID | Route Name | PC | PT | AutoCAD | ArcMap | $\begin{gathered} \hline \text { Error } \\ \% \\ \hline \end{gathered}$ | AutoCAD | ArcMap | $\begin{gathered} \text { Error } \\ \% \\ \hline \end{gathered}$ |
| 66 | 320900 | 0015P | 352.1 | 352.2 | 1335 | 3158 | 136.6\% | 578 | 612 | 6.0\% |
| 67 | 320911 | 0015P | 357.9 | 358.1 | 7255 | 5093 | 29.8\% | 1261 | 1325 | 5.1\% |
| 68 | 320974 | 0015N | 352.1 | 352.0 | 1246 | 2915 | 134.0\% | 564 | 559 | 0.9\% |
| 69 | 321224 | 0015N | 224.5 | 224.2 | 2356 | 2961 | 25.7\% | 1358 | 1430 | 5.3\% |
| 70 | 321252 | 0015N | 184.5 | 185.0 | 4639 | 4858 | 4.7\% | 2721 | 3924 | 44.2\% |
| 71 | 321269 | 0015N | 140.1 | 139.9 | 2083 | 2540 | 22.0\% | 1165 | 1268 | 8.8\% |
| 72 | 321318 | 0015N | 105.3 | 104.8 | 3594 | 4627 | 28.7\% | 2842 | 2879 | 1.3\% |
| 73 | 321351 | 0015N | 34.9 | 34.8 | 3085 | 2960 | 4.0\% | 1071 | 974 | 9.0\% |
| 74 | 321414 | 0070N | 182.0 | 181.9 | 1513 | 4782 | 216.0\% | 464 | 374 | 19.4\% |
| 75 | 321416 | 0070N | 172.4 | 171.9 | 4911 | 5085 | 3.5\% | 2991 | 2957 | 1.1\% |
| 76 | 321449 | 0070N | 145.0 | 144.7 | 1483 | 1654 | 11.5\% | 1492 | 1540 | 3.2\% |
| 77 | 321459 | 0070N | 143.0 | 142.5 | 1492 | 1579 | 5.8\% | 2852 | 2691 | 5.7\% |
| 78 | 321461 | 0070N | 142.3 | 142.0 | 1760 | 1911 | 8.6\% | 1367 | 1375 | 0.6\% |
| 79 | 321535 | 0070N | 112.4 | 112.2 | 6137 | 5337 | 13.0\% | 882 | 868 | 1.6\% |
| 80 | 321550 | 0070N | 107.5 | 108.0 | 4592 | 4653 | 1.3\% | 2837 | 3235 | 14.0\% |
| 81 | 321582 | 0070N | 95.6 | 95.2 | 4267 | 5142 | 20.5\% | 1920 | 1891 | 1.5\% |
| 82 | 321624 | 0070N | 83.1 | 82.7 | 2233 | 2388 | 6.9\% | 1650 | 1738 | 5.3\% |
| 83 | 321638 | 0070N | 80.9 | 80.7 | 1669 | 2011 | 20.5\% | 1402 | 1272 | 9.2\% |
| 84 | 321648 | 0070N | 78.8 | 78.6 | 2278 | 2690 | 18.1\% | 1136 | 1162 | 2.3\% |
| 85 | 321658 | 0070N | 75.6 | 75.4 | 1561 | 2576 | 65.1\% | 1090 | 1039 | 4.7\% |
| 86 | 321668 | 0070N | 73.0 | 72.8 | 3066 | 2992 | 2.4\% | 1831 | 1357 | 25.9\% |
| 87 | 321674 | 0070N | 72.2 | 72.0 | 1573 | 1683 | 7.0\% | 879 | 818 | 7.0\% |
| 88 | 321705 | 0070N | 68.0 | 67.7 | 3851 | 4402 | 14.3\% | 1347 | 1323 | 1.8\% |
| 89 | 321752 | 0070N | 55.0 | 54.8 | 3643 | 4877 | 33.9\% | 1191 | 1216 | 2.1\% |
| 90 | 321775 | 0070N | 45.0 | 44.8 | 3904 | 4872 | 24.8\% | 832 | 791 | 5.0\% |
| 91 | 321815 | 0070N | 23.1 | 22.8 | 2617 | 3003 | 14.7\% | 1651 | 1524 | 7.7\% |
| 92 | 321850 | 0070N | 12.6 | 12.2 | 1702 | 1861 | 9.3\% | 2022 | 2098 | 3.8\% |
| 93 | 322221 | 0080N | 186.2 | 185.8 | 3800 | 4440 | 16.8\% | 1839 | 2063 | 12.1\% |
| 94 | 322231 | 0080N | 180.6 | 180.4 | 2686 | 2787 | 3.8\% | 956 | 977 | 2.1\% |
| 95 | 322260 | 0080N | 171.5 | 171.3 | 1317 | 2121 | 61.0\% | 889 | 1051 | 18.2\% |
| 96 | 322293 | 0080N | 153.2 | 153.1 | 1229 | 1425 | 15.9\% | 647 | 601 | 7.1\% |
| 97 | 322313 | 0080N | 150.4 | 150.2 | 977 | 1226 | 25.5\% | 1031 | 1122 | 8.8\% |
| 98 | 322410 | 0080N | 132.5 | 132.3 | 1415 | 1580 | 11.7\% | 996 | 984 | 1.2\% |
| 99 | 322432 | 0080N | 129.9 | 129.8 | 999 | 1750 | 75.2\% | 676 | 742 | 9.8\% |
| 100 | 322434 | 0080N | 129.5 | 129.3 | 2413 | 2607 | 8.1\% | 1185 | 1138 | 3.9\% |

Table A.3: Urban Multilane Calibration

|  |  |  |  |  | RADIUS |  |  | CURVE LENGTH |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | ID | Route Name | PC | PT | AutoCAD | ArcMap | $\begin{gathered} \text { Error } \\ \% \\ \hline \end{gathered}$ | AutoCAD | ArcMap | $\begin{gathered} \text { Error } \\ \% \\ \hline \end{gathered}$ |
| 1 | 294237 | 0068P | 27.4 | 27.5 | 966 | -1369 | 41.6\% | 486 | 484 | 0.4\% |
| 2 | 299372 | 0089P | 348.9 | 348.8 | 166 | 597 | 260.6\% | 213 | 196 | 7.9\% |
| 3 | 310457 | 0154P | 4.6 | 4.5 | 2192 | 3356 | 53.1\% | 570 | 553 | 3.1\% |
| 4 | 303448 | 0106P | 7.0 | 7.0 | 1637 | -536 | 67.3\% | 1953 | 370 | 81.1\% |
| 5 | 304147 | 0115P | 6.9 | 6.8 | 661 | -922 | 39.4\% | 650 | 717 | 10.3\% |
| 6 | 310359 | 0154P | 20.5 | 20.7 | 2060 | 2929 | 42.2\% | 1325 | 1276 | 3.7\% |
| 7 | 298239 | 0089P | 383.1 | 383.3 | 1759 | 1861 | 5.8\% | 893 | 983 | 10.0\% |
| 8 | 303910 | 0114P | 0.5 | 0.6 | 822 | -1536 | 86.8\% | 698 | 793 | 13.6\% |
| 9 | 314758 | 0198P | 8.6 | 8.7 | 1507 | 2449 | 62.4\% | 314 | 310 | 1.2\% |
| 10 | 294612 | 0068P | 25.1 | 25.0 | 1114 | 1777 | 59.6\% | 368 | 384 | 4.4\% |
| 11 | 314787 | 0198P | 13.4 | 13.5 | 3836 | -2521 | 34.3\% | 488 | 670 | 37.3\% |
| 12 | 292084 | 0051P | 0.1 | 0.0 | 621 | -698 | 12.5\% | 514 | 512 | 0.4\% |
| 13 | 303743 | 0111P | 6.1 | 6.4 | 4602 | -4850 | 5.4\% | 1622 | 1568 | 3.3\% |
| 14 | 310408 | 0154P | 18.8 | 18.7 | 1987 | -2136 | 7.5\% | 471 | 495 | 5.0\% |
| 15 | 306982 | 0140P | 0.0 | 0.1 | 166 | -218 | 31.8\% | 389 | 362 | 7.0\% |
| 16 | 291767 | 0048P | 11.6 | 11.4 | 1390 | 1376 | 1.0\% | 1209 | 1174 | 2.9\% |
| 17 | 305075 | 0126P | 0.4 | 0.3 | 966 | 4300 | $345.2 \%$ | 215 | 217 | 0.8\% |
| 18 | 294114 | 0067P | 5.4 | 5.6 | 2497 | 4496 | 80.0\% | 840 | 815 | 2.9\% |
| 19 | 295656 | 0073P | 36.8 | 36.9 | 164 | -260 | 58.2\% | 272 | 268 | 1.4\% |
| 20 | 315454 | 0209P | 11.5 | 11.8 | 2039 | 2874 | 40.9\% | 1654 | 1679 | 1.5\% |
| 21 | 323823 | 0201N | 15.1 | 15.0 | 2014 | 4817 | 139.2\% | 534 | 519 | 2.8\% |
| 22 | 295310 | 0071P | 3.2 | 3.0 | 1346 | 1603 | 19.1\% | 1011 | 984 | 2.7\% |
| 23 | 292746 | 0060P | 6.5 | 6.4 | 809 | 764 | 5.6\% | 677 | 625 | 7.7\% |
| 24 | 292729 | 0060P | 7.1 | 7.2 | 1466 | 2696 | 83.9\% | 483 | 513 | 6.2\% |
| 25 | 285334 | 0026P | 1.8 | 1.9 | 2124 | -3062 | 44.1\% | 251 | 265 | 5.5\% |
| 26 | 294206 | 0068P | 24.7 | 24.7 | 1217 | 2946 | 142.0\% | 140 | 256 | 82.4\% |
| 27 | 303674 | 0109P | 1.1 | 1.2 | 746 | 903 | 21.1\% | 245 | 254 | 4.0\% |
| 28 | 305081 | 0126P | 0.1 | 0.0 | 887 | -553 | 37.7\% | 239 | 231 | 3.2\% |
| 29 | 310468 | 0154P | 2.0 | 1.6 | 2400 | -2378 | 0.9\% | 1912 | 1810 | 5.4\% |
| 30 | 299505 | 0089N | 327.8 | 327.7 | 368 | -1681 | 356.8\% | 618 | 604 | 2.2\% |
| 31 | 292691 | 0060P | 3.6 | 3.7 | 1168 | -2955 | 153.1\% | 510 | 516 | 1.2\% |
| 32 | 311973 | 0168P | 0.4 | 0.2 | 1213 | 1647 | 35.7\% | 752 | 787 | 4.7\% |
| 33 | 312504 | 0186P | 4.0 | 4.0 | 256 | 250 | 2.2\% | 467 | 381 | 18.3\% |
| 34 | 295140 | 0071P | 3.5 | 3.8 | 2262 | 2255 | 0.3\% | 1318 | 1304 | 1.1\% |
| 35 | 315418 | 0209P | 6.9 | 6.9 | 3439 | 4599 | 33.7\% | 444 | 445 | 0.1\% |
| 36 | 298152 | 0089P | 349.2 | 349.5 | 1439 | 1614 | 12.2\% | 1319 | 1354 | 2.6\% |
| 37 | 308112 | 0145P | 3.0 | 3.1 | 2000 | 2461 | 23.1\% | 922 | 911 | 1.2\% |


|  |  |  |  |  | RADIUS |  |  | CURVE LENGTH |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | ID | Route Name | PC | PT | AutoCAD | ArcMap | $\begin{gathered} \text { Error } \\ \% \end{gathered}$ | AutoCAD | ArcMap | Error \% |
| 38 | 299482 | 0089P | 331.7 | 331.6 | 3272 | 2817 | 13.9\% | 565 | 535 | 5.3\% |
| 39 | 295158 | 0071P | 5.8 | 5.8 | 1545 | 1620 | 4.9\% | 301 | 296 | 1.7\% |
| 40 | 323751 | 0201P | 8.9 | 8.9 | 6042 | 3409 | 43.6\% | 279 | 265 | 5.0\% |
| 41 | 318284 | 0265P | 2.4 | 2.5 | 3318 | 3583 | 8.0\% | 698 | 687 | 1.6\% |
| 42 | 294376 | 0068P | 64.6 | 64.8 | 6135 | 5257 | 14.3\% | 1012 | 969 | 4.3\% |
| 43 | 298247 | 0089P | 384.6 | 384.7 | 3705 | 3150 | 15.0\% | 463 | 416 | 10.1\% |
| 44 | 294122 | 0067P | 7.7 | 7.9 | 2090 | 2313 | 10.6\% | 1141 | 1132 | 0.8\% |
| 45 | 323838 | 0201 N | 8.9 | 9.1 | 4360 | 5106 | 17.1\% | 1123 | 1667 | 48.4\% |
| 46 | 303745 | 0111P | 6.6 | 7.2 | 3397 | 3757 | 10.6\% | 3413 | 3470 | 1.7\% |
| 47 | 312676 | 0189P | 6.9 | 7.2 | 5400 | 5607 | 3.8\% | 1400 | 1436 | 2.6\% |
| 48 | 310300 | 0154P | 0.1 | 0.4 | 1018 | 759 | 25.4\% | 1305 | 1332 | 2.1\% |
| 49 | 304967 | 0126P | 2.9 | 3.0 | 5523 | 5452 | 1.3\% | 545 | 548 | 0.5\% |
| 50 | 308123 | 0145P | 4.6 | 4.8 | 1081 | 1149 | 6.3\% | 883 | 850 | 3.8\% |
| 51 | 292098 | 0052P | 1.6 | 1.7 | 4108 | 4891 | 19.1\% | 329 | 332 | 1.0\% |
| 52 | 298091 | 0089P | 336.1 | 336.1 | 1222 | 1144 | 6.4\% | 436 | 450 | 3.3\% |
| 53 | 310324 | 0154P | 8.3 | 8.6 | 2632 | 2639 | 0.3\% | 1807 | 1774 | 1.8\% |
| 54 | 292327 | 0056P | 56.1 | 55.9 | 1565 | 1754 | 12.1\% | 945 | 934 | 1.1\% |
| 55 | 323753 | 0201P | 9.0 | 9.4 | 5646 | 5138 | 9.0\% | 1864 | 1851 | 0.7\% |
| 56 | 298089 | 0089P | 336.0 | 336.0 | 1427 | 1425 | 0.1\% | 321 | 316 | 1.5\% |
| 57 | 310354 | 0154P | 19.1 | 19.2 | 2438 | 2381 | 2.3\% | 521 | 523 | 0.4\% |
| 58 | 283030 | 0018P | 6.8 | 7.0 | 1450 | 1584 | 9.3\% | 1082 | 1067 | 1.4\% |
| 59 | 299238 | 0089N | 397.7 | 397.4 | 2345 | 2386 | 1.7\% | 1693 | 1673 | 1.2\% |
| 60 | 310440 | 0154P | 9.2 | 8.9 | 2892 | 2866 | 0.9\% | 1894 | 1867 | 1.4\% |
| 61 | 295665 | 0073P | 35.7 | 35.6 | 4429 | 4357 | 1.6\% | 406 | 396 | 2.4\% |
| 62 | 310381 | 0154P | 23.9 | 23.9 | 4462 | 3435 | 23.0\% | 258 | 252 | 2.3\% |
| 63 | 308159 | 0145P | 3.3 | 3.3 | 2792 | 3305 | 18.4\% | 196 | 188 | 4.0\% |
| 64 | 283028 | 0018P | 6.2 | 6.4 | 3119 | 2909 | 6.7\% | 814 | 796 | 2.2\% |
| 65 | 318461 | 0266P | 2.7 | 2.7 | 2143 | 1342 | 37.4\% | 190 | 192 | 1.1\% |
| 66 | 294120 | 0067P | 7.0 | 7.4 | 2086 | 2253 | 8.0\% | 1990 | 2052 | 3.1\% |
| 67 | 313062 | 0190P | 0.5 | 0.7 | 855 | 911 | 6.5\% | 1247 | 1238 | 0.7\% |
| 68 | 295138 | 0071P | 3.0 | 3.2 | 1580 | 1733 | 9.7\% | 1020 | 1031 | 1.1\% |
| 69 | 282991 | 0018P | 1.6 | 1.8 | 1904 | 1892 | 0.6\% | 1347 | 1345 | 0.2\% |
| 70 | 310404 | 0154P | 19.9 | 19.7 | 2845 | 2682 | 5.7\% | 1105 | 1099 | 0.5\% |
| 71 | 310470 | 0154P | 1.3 | 0.9 | 2294 | 2310 | 0.7\% | 1813 | 1765 | 2.7\% |
| 72 | 299233 | 0089P | 405.7 | 405.8 | 2496 | 3261 | 30.7\% | 520 | 1492 | 187.0\% |
| 73 | 299240 | 0089 N | 396.1 | 396.0 | 2694 | 2950 | 9.5\% | 484 | 481 | 0.6\% |
| 74 | 295294 | 0071P | 5.9 | 5.9 | 1986 | 2661 | 34.0\% | 313 | 303 | 3.1\% |
| 75 | 310314 | 0154P | 3.8 | 3.9 | 3184 | 3340 | 4.9\% | 423 | 423 | 0.1\% |
| 76 | 309267 | 0151P | 2.6 | 2.6 | 1864 | 2027 | 8.7\% | 449 | 445 | 1.0\% |


|  |  |  |  |  | RADIUS |  |  | CURVE LENGTH |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | ID | Route <br> Name | PC | PT | AutoCAD | ArcMap | $\begin{gathered} \text { Error } \\ \% \end{gathered}$ | AutoCAD | ArcMap | $\begin{gathered} \text { Error } \\ \% \end{gathered}$ |
| 77 | 299217 | 0089P | 410.4 | 410.3 | 2434 | 1789 | 26.5\% | 766 | 763 | 0.4\% |
| 78 | 294132 | 0067P | 8.4 | 8.1 | 2117 | 2132 | 0.7\% | 1453 | 1418 | 2.4\% |
| 79 | 298236 | 0089P | 382.5 | 382.8 | 2126 | 2152 | 1.2\% | 1465 | 1399 | 4.5\% |
| 80 | 310453 | 0154P | 5.7 | 6.0 | 3056 | 3678 | 20.4\% | 1644 | 2055 | 25.0\% |
| 81 | 324739 | 0079P | 0.1 | 0.0 | 814 | 1025 | 25.9\% | 477 | 510 | 7.0\% |
| 82 | 292115 | 0052P | 4.0 | 3.8 | 1174 | 1172 | 0.2\% | 728 | 730 | 0.3\% |
| 83 | 312666 | 0189P | 5.4 | 5.7 | 7919 | 7225 | 8.8\% | 1313 | 1316 | 0.2\% |
| 84 | 280301 | 0008P | 1.2 | 1.0 | 1280 | 1550 | 21.1\% | 930 | 920 | 1.1\% |
| 85 | 303352 | 0104P | 2.6 | 2.7 | 1947 | 1780 | 8.6\% | 738 | 856 | 16.0\% |
| 86 | 315336 | 0204P | 0.1 | 0.0 | 718 | 602 | 16.1\% | 291 | 291 | 0.0\% |
| 87 | 294567 | 0068P | 32.8 | 32.9 | 3274 | 4267 | 30.3\% | 372 | 614 | 65.2\% |
| 88 | 303781 | 0111P | 6.4 | 6.1 | 5329 | 4918 | 7.7\% | 1198 | 1192 | 0.5\% |
| 89 | 310391 | 0154N | 21.3 | 21.2 | 5667 | 5081 | 10.3\% | 484 | 469 | 3.0\% |
| 90 | 279269 | 0006P | 174.0 | 174.2 | 4319 | 3838 | 11.1\% | 832 | 782 | 6.1\% |
| 91 | 304962 | 0126P | 1.9 | 2.1 | 6503 | 4683 | 28.0\% | 934 | 924 | 1.1\% |
| 92 | 316791 | 0225P | 0.1 | 0.3 | 1244 | 1245 | 0.1\% | 1024 | 995 | 2.9\% |
| 93 | 294142 | 0067P | 5.5 | 5.3 | 12601 | 5035 | 60.0\% | 578 | 610 | 5.5\% |
| 94 | 294126 | 0067P | 10.4 | 10.6 | 4969 | 4621 | 7.0\% | 1059 | 1059 | 0.0\% |
| 95 | 299351 | 0089P | 362.7 | 362.6 | 728 | 2484 | 241.2\% | 643 | 607 | 5.6\% |
| 96 | 304954 | 0126P | 0.6 | 0.7 | 3160 | 2827 | 10.5\% | 295 | 284 | 3.6\% |
| 97 | 279277 | 0006P | 177.6 | 177.8 | 1120 | -1218 | 8.7\% | 1201 | 1228 | 2.2\% |
| 98 | 319511 | 0284P | 1.3 | 1.3 | 271 | 336 | 23.7\% | 254 | 263 | 3.5\% |
| 99 | 299383 | 0089P | 347.8 | 347.7 | 541 | -659 | 21.7\% | 415 | 425 | 2.5\% |
| 100 | 292679 | 0060P | 2.8 | 2.9 | 1114 | 5142 | 361.5\% | 409 | 404 | 1.2\% |

Table A.4: Rural Multilane Calibration

|  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\#$ | ID | Route <br> Name | PC | PT | AutoCAD | ArcMap | Error <br> $\%$ | AutoCAD | ArcMap | Error <br> $\%$ |
| 1 | 316644 | 0224 P | 8.6 | 8.8 | 1244 | 1173 | $5.7 \%$ | 1294 | 1212 | $6.4 \%$ |
| 2 | 280938 | 0010 P | 47.6 | 48.1 | 1602 | 1635 | $2.0 \%$ | 2636 | 2600 | $1.3 \%$ |
| 3 | 288417 | 0036 P | 65.8 | 66.1 | 1256 | -2326 | $85.2 \%$ | 1276 | 1312 | $2.9 \%$ |
| 4 | 290172 | 0040 P | 139.0 | 139.3 | 2860 | 4511 | $57.7 \%$ | 1338 | 1371 | $2.5 \%$ |
| 5 | 311764 | 0165 P | 6.7 | 6.6 | 1422 | 2904 | $104.2 \%$ | 463 | 490 | $6.0 \%$ |
| 6 | 313887 | 0191 P | 128.9 | 129.0 | 1915 | -2928 | $52.9 \%$ | 386 | 318 | $17.7 \%$ |
| 7 | 297857 | 0089 P | 256.1 | 256.2 | 897 | -866 | $3.5 \%$ | 442 | 435 | $1.6 \%$ |
| 8 | 317072 | 0248 P | 4.2 | 4.3 | 82983 | -5049 | $93.9 \%$ | 428 | 394 | $8.0 \%$ |


|  |  |  |  |  | RADIUS |  |  | CURVE LENGTH |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | ID | Route Name | PC | PT | AutoCAD | ArcMap | $\begin{gathered} \text { Error } \\ \% \end{gathered}$ | AutoCAD | ArcMap | $\begin{gathered} \text { Error } \\ \% \end{gathered}$ |
| 9 | 280786 | 0009P | 6.7 | 6.5 | 2428 | 2766 | 13.9\% | 1128 | 1051 | 6.8\% |
| 10 | 300517 | 0091P | 37.6 | 37.9 | 4521 | -4312 | 4.6\% | 1552 | 1557 | 0.4\% |
| 11 | 312748 | 0189P | 14.2 | 14.4 | 1198 | -1570 | 31.0\% | 1292 | 1346 | 4.2\% |
| 12 | 280794 | 0009P | 3.6 | 3.5 | 1445 | 1517 | 5.0\% | 645 | 596 | 7.6\% |
| 13 | 300432 | 0091P | 7.8 | 7.9 | 2075 | 2796 | 34.7\% | 696 | 632 | 9.3\% |
| 14 | 312961 | 0189P | 12.2 | 12.0 | 782 | 1060 | 35.5\% | 591 | 668 | 13.1\% |
| 15 | 312715 | 0189P | 11.1 | 11.3 | 3218 | -1535 | 52.3\% | 1996 | 771 | 61.4\% |
| 16 | 312778 | 0189P | 17.4 | 17.5 | 1470 | -1562 | 6.2\% | 693 | 626 | 9.6\% |
| 17 | 312701 | 0189P | 9.2 | 9.4 | 1053 | -1214 | 15.2\% | 897 | 969 | 8.0\% |
| 18 | 312893 | 0189P | 18.3 | 18.2 | 886 | -1085 | $22.4 \%$ | 656 | 623 | 5.1\% |
| 19 | 280321 | 0009P | 2.0 | 2.5 | 4472 | 4904 | 9.7\% | 2744 | 2642 | 3.7\% |
| 20 | 280790 | 0009P | 4.4 | 4.2 | 2722 | -2903 | 6.6\% | 1296 | 1263 | 2.5\% |
| 21 | 312901 | 0189P | 17.5 | 17.4 | 1388 | 1465 | 5.5\% | 701 | 625 | 10.9\% |
| 22 | 312776 | 0189P | 17.1 | 17.2 | 1375 | -1707 | 24.2\% | 492 | 550 | 11.8\% |
| 23 | 312915 | 0189P | 15.7 | 15.6 | 840 | -968 | 15.2\% | 808 | 805 | 0.4\% |
| 24 | 323277 | 0191P | 128.7 | 128.5 | 983 | 1102 | 12.1\% | 1056 | 1039 | 1.7\% |
| 25 | 312783 | 0189P | 18.0 | 18.1 | 1422 | -976 | 31.3\% | 1531 | 831 | 45.7\% |
| 26 | 299166 | 0089P | 426.3 | 426.0 | 2472 | 3079 | 24.6\% | 1229 | 1194 | 2.8\% |
| 27 | 312720 | 0189P | 11.8 | 11.9 | 1993 | 1636 | 18.0\% | 442 | 479 | 8.2\% |
| 28 | 304366 | 0118P | 5.7 | 5.5 | 1753 | -2121 | 21.0\% | 733 | 769 | 4.9\% |
| 29 | 300437 | 0091P | 8.7 | 8.9 | 1397 | 1613 | 15.4\% | 1365 | 1367 | 0.2\% |
| 30 | 280796 | 0009P | 3.4 | 3.0 | 1877 | -2030 | 8.1\% | 2284 | 2204 | 3.5\% |
| 31 | 304486 | 0120P | 3.3 | 3.4 | 1162 | 1207 | 3.9\% | 607 | 399 | 34.2\% |
| 32 | 290256 | 0040P | 145.3 | 145.1 | 964 | -1243 | 29.0\% | 936 | 958 | 2.3\% |
| 33 | 312965 | 0189P | 11.6 | 11.3 | 2663 | -3278 | 23.1\% | 1276 | 1383 | 8.4\% |
| 34 | 300578 | 0091P | 6.7 | 6.8 | 1160 | -4057 | 249.8\% | 317 | 1348 | 324.6\% |
| 35 | 312779 | 0189P | 17.5 | 17.8 | 1283 | 3159 | 146.2\% | 265 | 1628 | 514.1\% |
| 36 | 312916 | 0189P | 15.6 | 15.3 | 938 | 106 | 88.7\% | 1327 | 1350 | 1.8\% |
| 37 | 290275 | 0040P | 140.7 | 140.8 | 1962 | -3484 | 77.6\% | 756 | 1154 | 52.7\% |
| 38 | 300588 | 0091P | 4.8 | 4.7 | 1749 | -2519 | 44.0\% | 494 | 543 | 10.0\% |
| 39 | 279558 | 0006P | 232.6 | 233.2 | 2245 | 2483 | 10.6\% | 3426 | 3459 | 1.0\% |
| 40 | 323271 | 0191P | 131.0 | 130.5 | 1830 | 1974 | 7.9\% | 2455 | 2495 | 1.6\% |
| 41 | 312897 | 0189P | 17.9 | 17.8 | 760 | 988 | 29.9\% | 529 | 511 | 3.4\% |
| 42 | 279949 | 0006P | 188.1 | 187.9 | 2000 | -2384 | 19.2\% | 920 | 813 | 11.6\% |
| 43 | 300593 | 0091P | 4.2 | 4.0 | 2642 | -2902 | 9.9\% | 1054 | 1162 | 10.3\% |
| 44 | 317141 | 0248P | 5.5 | 5.3 | 2252 | 2875 | 27.7\% | 1148 | 1252 | 9.1\% |
| 45 | 316694 | 0224P | 5.0 | 5.1 | 910 | -2523 | 177.4\% | 418 | 798 | 91.1\% |
| 46 | 310998 | 0160P | 1.7 | 1.8 | 895 | -1154 | 28.8\% | 650 | 642 | 1.3\% |


|  |  |  |  |  | RADIUS |  |  | CURVE LENGTH |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | ID | Route Name | PC | PT | AutoCAD | ArcMap | $\begin{gathered} \text { Error } \\ \% \\ \hline \end{gathered}$ | AutoCAD | ArcMap | $\begin{gathered} \text { Error } \\ \% \end{gathered}$ |
| 47 | 313788 | 0191P | 104.8 | 105.5 | 5253 | 5568 | 6.0\% | 3624 | 3548 | 2.1\% |
| 48 | 312973 | 0189P | 10.2 | 10.1 | 791 | -1155 | 46.1\% | 471 | 536 | 13.6\% |
| 49 | 317243 | 0252P | 0.7 | 0.7 | 1207 | -4209 | 248.9\% | 247 | 230 | 7.0\% |
| 50 | 311731 | 0165P | 6.6 | 6.7 | 1939 | -3216 | 65.8\% | 629 | 594 | 5.6\% |
| 51 | 290137 | 0040P | 113.9 | 114.1 | 575 | -716 | 24.6\% | 804 | 754 | 6.2\% |
| 52 | 280792 | 0009P | 4.1 | 3.7 | 1425 | 1469 | 3.1\% | 2070 | 2011 | 2.8\% |
| 53 | 279672 | 0006P | 243.4 | 243.2 | 5650 | 4178 | 26.0\% | 764 | 754 | 1.3\% |
| 54 | 312768 | 0189P | 16.0 | 16.1 | 874 | 1111 | 27.1\% | 500 | 501 | 0.2\% |
| 55 | 298356 | 0089P | 426.0 | 426.3 | 3046 | 3441 | 13.0\% | 1349 | 1343 | 0.5\% |
| 56 | 317064 | 0248P | 2.9 | 3.1 | 860 | 970 | 12.8\% | 719 | 717 | 0.3\% |
| 57 | 284368 | 0024P | 60.1 | 60.2 | 555 | 763 | 37.4\% | 645 | 624 | 3.2\% |
| 58 | 300443 | 0091P | 9.8 | 10.1 | 1981 | 2030 | 2.5\% | 1315 | 1430 | 8.7\% |
| 59 | 297855 | 0089P | 256.0 | 256.1 | 481 | 591 | 23.0\% | 588 | 582 | 1.1\% |
| 60 | 299638 | 0089P | 277.3 | 276.9 | 1664 | 1633 | 1.9\% | 1700 | 1660 | 2.4\% |
| 61 | 299163 | 0089P | 426.7 | 426.5 | 2841 | 3078 | 8.3\% | 984 | 996 | 1.2\% |
| 62 | 288412 | 0036P | 62.0 | 62.2 | 2992 | 3150 | 5.3\% | 851 | 865 | 1.7\% |
| 63 | 316650 | 0224P | 10.4 | 10.5 | 2962 | 2893 | 2.3\% | 747 | 732 | 2.0\% |
| 64 | 312944 | 0189P | 13.6 | 13.5 | 1632 | 1748 | 7.1\% | 334 | 327 | 2.1\% |
| 65 | 280765 | 0009P | 11.9 | 11.8 | 1886 | 2059 | 9.2\% | 763 | 739 | 3.2\% |
| 66 | 316667 | 0224P | 10.2 | 9.9 | 2721 | 2892 | 6.3\% | 1679 | 1675 | 0.3\% |
| 67 | 312955 | 0189P | 12.6 | 12.5 | 984 | 1240 | 26.0\% | 399 | 385 | 3.4\% |
| 68 | 300389 | 0091P | 3.4 | 3.8 | 1456 | 1432 | 1.7\% | 1891 | 1816 | 3.9\% |
| 69 | 300572 | 0091P | 7.6 | 7.2 | 1423 | 1594 | 12.0\% | 2085 | 2081 | 0.2\% |
| 70 | 312711 | 0189P | 10.3 | 10.5 | 1311 | 1470 | 12.1\% | 805 | 809 | 0.5\% |
| 71 | 323580 | 0191P | 51.5 | 51.3 | 962 | 1018 | 5.9\% | 949 | 936 | 1.4\% |
| 72 | 290316 | 0040P | 114.1 | 114.0 | 589 | 634 | 7.6\% | 703 | 672 | 4.4\% |
| 73 | 312703 | 0189P | 9.5 | 9.6 | 1430 | 1568 | 9.6\% | 410 | 434 | 5.8\% |
| 74 | 298378 | 0089P | 433.3 | 433.5 | 2984 | 2865 | 4.0\% | 1166 | 1177 | 0.9\% |
| 75 | 289797 | 0040P | 14.9 | 15.2 | 2877 | 2942 | 2.3\% | 1727 | 1681 | 2.7\% |
| 76 | 300429 | 0091P | 7.2 | 7.6 | 1397 | 1660 | 18.8\% | 1938 | 2018 | 4.1\% |
| 77 | 300498 | 0091P | 25.3 | 25.7 | 3084 | 5371 | 74.1\% | 1955 | 1970 | 0.7\% |
| 78 | 304305 | 0118P | 5.4 | 5.5 | 1439 | 1287 | 10.5\% | 510 | 546 | 7.1\% |
| 79 | 297852 | 0089P | 254.8 | 255.0 | 944 | 1031 | 9.2\% | 774 | 769 | 0.7\% |
| 80 | 300580 | 0091P | 6.4 | 5.9 | 1958 | 2048 | 4.6\% | 2489 | 2431 | 2.3\% |
| 81 | 300270 | 0089P | 64.2 | 64.1 | 304 | 354 | 16.5\% | 583 | 564 | 3.2\% |
| 82 | 312742 | 0189P | 13.8 | 13.8 | 1579 | 1986 | 25.8\% | 325 | 324 | 0.3\% |
| 83 | 298389 | 0089P | 459.9 | 459.9 | 700 | 1210 | 72.8\% | 212 | 212 | 0.2\% |
| 84 | 290176 | 0040P | 140.6 | 140.9 | 2744 | 3225 | 17.5\% | 1203 | 1197 | 0.5\% |
| 85 | 312724 | 0189P | 12.2 | 12.3 | 933 | 1115 | 19.5\% | 573 | 567 | 1.0\% |


|  |  |  |  |  | RADIUS |  |  | CURVE LENGTH |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | ID | Route <br> Name | PC | PT | AutoCAD | ArcMap | $\begin{gathered} \text { Error } \\ \% \end{gathered}$ | AutoCAD | ArcMap | $\begin{gathered} \text { Error } \\ \% \end{gathered}$ |
| 86 | 312837 | 0189P | 28.8 | 28.9 | 590 | 594 | 0.6\% | 217 | 222 | 2.1\% |
| 87 | 311762 | 0165P | 6.9 | 6.8 | 2767 | 2928 | 5.8\% | 533 | 526 | 1.4\% |
| 88 | 311023 | 0160P | 1.8 | 1.7 | 1046 | 1263 | 20.7\% | 727 | 697 | 4.1\% |
| 89 | 299136 | 0089P | 460.5 | 460.4 | 1382 | 1497 | 8.3\% | 578 | 557 | 3.6\% |
| 90 | 300453 | 0091P | 14.8 | 14.9 | 5504 | 5010 | 9.0\% | 471 | 508 | 7.9\% |
| 91 | 290607 | 0040P | 16.5 | 16.4 | 908 | 1188 | 30.9\% | 327 | 325 | 0.6\% |
| 92 | 300284 | 0089P | 63.1 | 63.3 | 2748 | 3842 | 39.8\% | 840 | 1518 | 80.6\% |
| 93 | 298359 | 0089P | 426.5 | 426.7 | 2988 | 3145 | 5.2\% | 1004 | 1008 | 0.4\% |
| 94 | 299134 | 0089P | 460.8 | 460.7 | 1513 | 1616 | 6.8\% | 953 | 967 | 1.4\% |
| 95 | 300385 | 0091P | 2.3 | 2.6 | 1881 | 2044 | 8.7\% | 1379 | 1384 | 0.4\% |
| 96 | 312738 | 0189P | 13.5 | 13.6 | 1526 | 1867 | 22.3\% | 371 | 359 | 3.2\% |
| 97 | 288435 | 0036P | 55.8 | 55.7 | 3197 | 2862 | 10.5\% | 190 | 189 | 0.7\% |
| 98 | 312707 | 0189P | 9.9 | 10.1 | 973 | 1130 | 16.1\% | 920 | 944 | 2.6\% |
| 99 | 300411 | 0091P | 5.0 | 5.1 | 1655 | 2029 | 22.6\% | 317 | 336 | 5.8\% |
| 100 | 312983 | 0189P | 9.1 | 9.0 | 912 | 1088 | 19.3\% | 658 | 655 | 0.5\% |
| 101 | 300399 | 0091P | 4.3 | 4.6 | 2793 | 3191 | 14.3\% | 1538 | 1640 | 6.6\% |
| 102 | 324399 | 0012P | 59.8 | 59.7 | 748 | 773 | 3.4\% | 664 | 679 | 2.3\% |
| 103 | 289795 | 0040P | 13.8 | 14.0 | 5390 | 4670 | 13.4\% | 859 | 860 | 0.1\% |
| 104 | 280332 | 0009P | 4.2 | 4.4 | 3030 | 2928 | 3.4\% | 1171 | 1157 | 1.2\% |
| 105 | 300418 | 0091P | 5.9 | 6.4 | 1922 | 2103 | 9.4\% | 2357 | 2389 | 1.3\% |

Table A.5: Urban TLTW Calibration

|  |  |  |  |  | RADIUS |  |  | CURVE LENGTH |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | ID | Route <br> Name | PC | PT | AutoCAD | ArcMap | Error <br> \% | AutoCAD | ArcMap | $\begin{gathered} \text { Error } \\ \% \\ \hline \end{gathered}$ |
| 1 | 308369 | 0147P | 11.8 | 11.8 | 386 | -741 | 92.0\% | 309 | 303 | 1.9\% |
| 2 | 313515 | 0190P | 2.2 | 2.1 | 800 | 1161 | 45.2\% | 453 | 437 | 3.7\% |
| 3 | 315505 | 0209P | 12.1 | 11.9 | 1136 | 1286 | 13.2\% | 973 | 963 | 1.0\% |
| 4 | 292717 | 0060P | 5.3 | 5.4 | 1849 | 1419 | 23.3\% | 790 | 379 | 52.0\% |
| 5 | 303450 | 0106P | 7.1 | 7.2 | 287 | -985 | 242.8\% | 366 | 361 | 1.5\% |
| 6 | 308263 | 0146P | 2.6 | 2.4 | 1476 | -1657 | 12.3\% | 956 | 929 | 2.9\% |
| 7 | 304135 | 0115P | 8.0 | 8.0 | 493 | -543 | 10.1\% | 271 | 265 | 2.2\% |
| 8 | 295746 | 0074P | 1.3 | 1.5 | 3109 | 2362 | 24.0\% | 962 | 947 | 1.6\% |
| 9 | 314852 | 0198P | 4.1 | 3.9 | 1461 | -2107 | 44.2\% | 803 | 783 | 2.5\% |
| 10 | 312450 | 0186P | 0.7 | 0.7 | 1423 | -2892 | 103.3\% | 441 | 490 | 11.1\% |
| 11 | 308278 | 0146P | 0.9 | 0.9 | 1345 | -1005 | 25.3\% | 396 | 406 | 2.5\% |
| 12 | 294126 | 0067P | 10.4 | 10.6 | 2768 | -4621 | 66.9\% | 1095 | 1059 | 3.3\% |


|  |  |  |  |  | RADIUS |  |  | CURVE LENGTH |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | ID | Route Name | PC | PT | AutoCAD | ArcMap | $\begin{gathered} \text { Error } \\ \% \end{gathered}$ | AutoCAD | ArcMap | $\begin{gathered} \text { Error } \\ \% \end{gathered}$ |
| 13 | 315935 | 0210P | 2.9 | 2.8 | 1152 | 1106 | 4.0\% | 976 | 772 | 21.0\% |
| 14 | 294151 | 0067P | 0.8 | 0.4 | 2188 | 2163 | 1.1\% | 2023 | 1994 | 1.4\% |
| 15 | 304143 | 0115P | 8.0 | 8.0 | 665 | 537 | 19.3\% | 280 | 270 | 3.5\% |
| 16 | 309331 | 0152N | 1.1 | 0.8 | 16529 | -5261 | 68.2\% | 1273 | 1246 | 2.1\% |
| 17 | 315944 | 0210P | 1.6 | 1.5 | 1212 | 1064 | 12.2\% | 868 | 844 | 2.7\% |
| 18 | 294584 | 0068P | 27.5 | 27.4 | 1050 | 1218 | 15.9\% | 445 | 438 | 1.6\% |
| 19 | 312623 | 0186P | 0.9 | 1.0 | 1043 | -3167 | 203.7\% | 227 | 525 | 131.1\% |
| 20 | 292725 | 0060P | 6.6 | 6.8 | 1497 | -1465 | 2.2\% | 1271 | 1095 | 13.8\% |
| 21 | 312995 | 0189P | 7.6 | 7.5 | 794 | -899 | 13.2\% | 723 | 706 | 2.4\% |
| 22 | 313076 | 0190P | 2.1 | 2.2 | 672 | -1017 | 51.4\% | 386 | 371 | 3.7\% |
| 23 | 315937 | 0210P | 2.5 | 2.4 | 1562 | -2070 | 32.5\% | 868 | 824 | 5.0\% |
| 24 | 308368 | 0147P | 11.9 | 11.8 | 197 | 345 | 74.9\% | 218 | 205 | 5.9\% |
| 25 | 294206 | 0068P | 24.7 | 24.7 | 1171 | 2946 | 151.7\% | 248 | 256 | 3.3\% |
| 26 | 307031 | 0140P | 0.5 | 0.5 | 993 | -2194 | 120.9\% | 198 | 187 | 5.5\% |
| 27 | 295755 | 0074P | 4.9 | 4.7 | 1176 | -1282 | 9.0\% | 1134 | 1121 | 1.1\% |
| 28 | 315458 | 0209P | 11.9 | 12.1 | 1087 | -1317 | 21.2\% | 987 | 984 | 0.3\% |
| 29 | 292719 | 0060P | 5.5 | 5.7 | 1623 | -1930 | 19.0\% | 789 | 794 | 0.6\% |
| 30 | 303690 | 0109P | 2.7 | 2.7 | 1644 | -2569 | 56.3\% | 495 | 485 | 2.0\% |
| 31 | 294251 | 0068P | 29.1 | 29.2 | 1003 | 1196 | 19.3\% | 934 | 897 | 4.0\% |
| 32 | 312340 | 0173P | 0.5 | 0.3 | 912 | 1114 | 22.1\% | 725 | 733 | 1.0\% |
| 33 | 303677 | 0109P | 1.3 | 1.5 | 2833 | 2904 | 2.5\% | 1035 | 1029 | 0.6\% |
| 34 | 292668 | 0060P | 2.3 | 2.4 | 477 | -3672 | 669.4\% | 525 | 535 | 1.9\% |
| 35 | 292746 | 0060P | 6.5 | 6.4 | 711 | 764 | 7.4\% | 653 | 625 | 4.2\% |
| 36 | 294223 | 0068P | 26.4 | 26.6 | 4103 | -4006 | 2.4\% | 1256 | 1290 | 2.7\% |
| 37 | 298016 | 0089P | 322.4 | 322.7 | 2548 | 3226 | 26.6\% | 1523 | 1507 | 1.0\% |
| 38 | 304046 | 0114P | 3.3 | 3.2 | 12712 | 3162 | 75.1\% | 619 | 593 | 4.2\% |
| 39 | 308280 | 0146P | 0.8 | 0.7 | 808 | 1024 | 26.7\% | 391 | 400 | 2.3\% |
| 40 | 311695 | 0164P | 2.7 | 2.7 | 342 | 422 | 23.2\% | 365 | 344 | 5.8\% |
| 41 | 294448 | 0068P | 65.9 | 66.0 | 1742 | 7662 | 339.8\% | 487 | 428 | 12.0\% |
| 42 | 292666 | 0060P | 2.1 | 2.2 | 400 | -481 | 20.4\% | 450 | 456 | 1.3\% |
| 43 | 306985 | 0140P | 0.2 | 0.2 | 931 | 567 | 39.1\% | 254 | 256 | 1.1\% |
| 44 | 292742 | 0060P | 7.1 | 7.0 | 1165 | 1503 | 29.0\% | 605 | 558 | 7.8\% |
| 45 | 292721 | 0060P | 6.1 | 6.4 | 679 | 747 | 10.0\% | 1172 | 1175 | 0.3\% |
| 46 | 306982 | 0140P | 0.0 | 0.1 | 178 | -218 | 23.0\% | 385 | 362 | 6.0\% |
| 47 | 323838 | 0201N | 8.9 | 9.1 | 3856 | 5106 | 32.4\% | 1072 | 1667 | 55.5\% |
| 48 | 299270 | 0089N | 383.7 | 383.6 | 1047 | 1466 | 40.1\% | 789 | 792 | 0.4\% |
| 49 | 292695 | 0060P | 3.7 | 3.9 | 806 | 2096 | 159.9\% | 702 | 737 | 5.0\% |
| 50 | 315572 | 0210P | 1.5 | 1.7 | 1234 | -1269 | 2.8\% | 980 | 1027 | 4.8\% |
| 51 | 294610 | 0068P | 25.2 | 25.2 | 747 | -1541 | 106.3\% | 355 | 421 | 18.6\% |


|  |  |  |  |  | RADIUS |  |  | CURVE LENGTH |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | ID | Route <br> Name | PC | PT | AutoCAD | ArcMap | Error \% | AutoCAD | ArcMap | Error \% |
| 52 | 308207 | 0146P | 2.2 | 2.3 | 706 | -838 | 18.7\% | 731 | 747 | 2.1\% |
| 53 | 303408 | 0106P | 0.1 | 0.2 | 668 | -2195 | 228.7\% | 293 | 299 | 1.9\% |
| 54 | 314741 | 0198P | 4.5 | 4.6 | 2625 | -3435 | 30.9\% | 849 | 938 | 10.5\% |
| 55 | 295782 | 0075P | 1.7 | 1.7 | 870 | -3261 | 274.7\% | 197 | 198 | 0.3\% |
| 56 | 311975 | 0168P | 0.1 | 0.0 | 2235 | 2281 | 2.1\% | 215 | 219 | 1.7\% |
| 57 | 308327 | 0147P | 13.2 | 13.2 | 2140 | 3137 | 46.6\% | 199 | 190 | 4.7\% |
| 58 | 279994 | 0006P | 178.1 | 177.9 | 1130 | 1281 | 13.4\% | 834 | 857 | 2.7\% |
| 59 | 279277 | 0006P | 177.6 | 177.8 | 1185 | 1218 | 2.8\% | 1238 | 1228 | 0.8\% |
| 60 | 312617 | 0186P | 1.3 | 1.2 | 735 | 791 | 7.6\% | 244 | 245 | 0.5\% |
| 61 | 304137 | 0115P | 8.1 | 8.1 | 330 | 540 | 63.9\% | 268 | 283 | 5.4\% |
| 62 | 303707 | 0109P | 0.8 | 0.8 | 584 | 775 | 32.7\% | 279 | 278 | 0.2\% |
| 63 | 292059 | 0051P | 0.0 | 0.1 | 695 | 659 | 5.2\% | 608 | 615 | 1.1\% |
| 64 | 292679 | 0060P | 2.8 | 2.9 | 1087 | 5142 | 373.0\% | 419 | 404 | 3.5\% |
| 65 | 292707 | 0060P | 4.4 | 4.5 | 646 | 765 | 18.4\% | 445 | 459 | 3.2\% |
| 66 | 302640 | 0097P | 2.8 | 2.7 | 923 | 1117 | 21.0\% | 771 | 756 | 1.9\% |
| 67 | 303724 | 0110P | 1.2 | 1.2 | 1035 | 1586 | 53.2\% | 279 | 266 | 4.5\% |
| 68 | 295748 | 0074P | 2.2 | 2.3 | 2455 | 2513 | 2.3\% | 642 | 631 | 1.7\% |
| 69 | 308240 | 0146P | 5.0 | 5.0 | 4739 | 3144 | 33.7\% | 176 | 180 | 2.1\% |
| 70 | 308198 | 0146P | 0.7 | 0.8 | 868 | 943 | 8.6\% | 368 | 363 | 1.5\% |
| 71 | 294595 | 0068P | 26.4 | 26.6 | 3315 | 4188 | 26.3\% | 470 | 1041 | 121.5\% |
| 72 | 303469 | 0106P | 8.7 | 8.7 | 1501 | 1558 | 3.8\% | 263 | 256 | 2.5\% |
| 73 | 312191 | 0173P | 0.0 | 0.3 | 955 | 977 | 2.3\% | 1354 | 1334 | 1.5\% |
| 74 | 306761 | 0134P | 7.1 | 7.0 | 1331 | 1481 | 11.3\% | 380 | 360 | 5.3\% |
| 75 | 318414 | 0266P | 7.0 | 6.9 | 1291 | 1318 | 2.1\% | 553 | 544 | 1.6\% |
| 76 | 292787 | 0060P | 3.3 | 3.2 | 1023 | 1249 | 22.0\% | 319 | 304 | 4.7\% |
| 77 | 292744 | 0060P | 6.8 | 6.6 | 1308 | 1386 | 6.0\% | 1002 | 1031 | 2.9\% |
| 78 | 294215 | 0068P | 25.5 | 25.6 | 2890 | 3433 | 18.8\% | 573 | 578 | 0.9\% |
| 79 | 314838 | 0198P | 7.9 | 7.8 | 1577 | 1697 | 7.6\% | 666 | 674 | 1.3\% |
| 80 | 299516 | 0089P | 326.5 | 326.2 | 2350 | 2461 | 4.7\% | 1382 | 1372 | 0.7\% |
| 81 | 312193 | 0173P | 0.4 | 0.5 | 927 | 1061 | 14.4\% | 671 | 680 | 1.3\% |
| 82 | 295777 | 0075P | 0.7 | 0.8 | 6724 | 5121 | 23.8\% | 827 | 824 | 0.4\% |
| 83 | 303625 | 0108P | 12.8 | 12.6 | 1337 | 1470 | 10.0\% | 738 | 739 | 0.2\% |
| 84 | 292067 | 0051P | 2.2 | 2.4 | 1403 | 1454 | 3.6\% | 920 | 923 | 0.3\% |
| 85 | 303497 | 0106P | 8.0 | 7.9 | 329 | 382 | 16.3\% | 663 | 644 | 2.9\% |
| 86 | 294586 | 0068P | 27.3 | 27.2 | 1995 | 1860 | 6.8\% | 448 | 442 | 1.3\% |
| 87 | 314850 | 0198P | 4.6 | 4.5 | 1153 | 1309 | 13.6\% | 843 | 846 | 0.4\% |
| 88 | 315491 | 0209P | 13.9 | 13.8 | 1818 | 2007 | 10.4\% | 505 | 512 | 1.4\% |
| 89 | 308238 | 0146P | 5.3 | 5.2 | 534 | 751 | 40.6\% | 465 | 462 | 0.6\% |
| 90 | 303940 | 0114P | 2.0 | 2.2 | 2584 | 2271 | 12.1\% | 1226 | 1209 | 1.4\% |


|  |  |  |  |  | RADIUS |  |  | CURVE LENGTH |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | $\begin{gathered} \text { ID } \\ 314787 \end{gathered}$ | Route Name 0198P | $\begin{gathered} \text { PC } \\ 13.4 \end{gathered}$ | $\begin{gathered} \text { PT } \\ 13.5 \end{gathered}$ | $\begin{gathered} \text { AutoCAD } \\ 2744 \end{gathered}$ | ArcMap $2521$ | $\begin{gathered} \text { Error } \\ \boldsymbol{\%} \\ 8.1 \% \end{gathered}$ | $\begin{gathered} \text { AutoCAD } \\ 667 \end{gathered}$ | ArcMap $670$ | $\begin{gathered} \text { Error } \\ \% \\ 0.5 \% \end{gathered}$ |
| 92 | 295853 | 0077P | 6.4 | 6.6 | 959 | 1046 | 9.1\% | 944 | 937 | 0.7\% |
| 93 | 298023 | 0089P | 323.0 | 323.2 | 5847 | 5284 | 9.6\% | 1126 | 1100 | 2.3\% |
| 94 | 306765 | 0134P | 6.3 | 6.3 | 1912 | 2486 | 30.0\% | 280 | 278 | 0.6\% |
| 95 | 303701 | 0109P | 1.3 | 1.5 | 2735 | 3194 | 16.8\% | 778 | 1171 | 50.5\% |
| 96 | 308246 | 0146P | 4.3 | 4.2 | 2037 | 1822 | 10.5\% | 321 | 319 | 0.8\% |
| 97 | 319586 | 0287P | 0.3 | 0.2 | 1172 | 1306 | 11.4\% | 652 | 664 | 1.9\% |
| 98 | 314734 | 0198P | 3.6 | 3.7 | 2442 | 2088 | 14.5\% | 199 | 193 | 3.2\% |
| 99 | 292757 | 0060P | 4.9 | 4.8 | 1035 | 1405 | 35.8\% | 357 | 351 | 1.5\% |
| 100 | 312455 | 0186P | 1.2 | 1.3 | 1034 | -309 | 70.1\% | 226 | 224 | 1.1\% |

Table A.6: Rural TLTW Calibration

|  |  |  |  |  | RADIUS |  |  | CURVE LENGTH |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | ID | Route <br> Name | PC | PT | AutoCAD | ArcMap | Error $\%$ | AutoCAD | ArcMap | $\begin{gathered} \text { Error } \\ \% \end{gathered}$ |
| 1 | 307903 | 0143P | 12.5 | 12.5 | 500 | 2019 | 303.5\% | 441 | 418 | 5.1\% |
| 2 | 314495 | 0191P | 390.8 | 390.9 | 518 | 588 | 13.6\% | 790 | 794 | 0.6\% |
| 3 | 291499 | 0046P | 11.7 | 11.8 | 4259 | 2992 | 29.7\% | 797 | 629 | 21.0\% |
| 4 | 305015 | 0126P | 21.6 | 21.4 | 860 | 1044 | 21.4\% | 855 | 973 | 13.9\% |
| 5 | 294623 | 0068P | 22.3 | 22.3 | 1387 | 2402 | 73.2\% | 277 | 218 | 21.3\% |
| 6 | 292936 | 0062P | 34.8 | 35.0 | 2684 | 4118 | 53.5\% | 1498 | 1459 | 2.6\% |
| 7 | 306384 | 0132P | 29.8 | 30.0 | 1821 | 3003 | 65.0\% | 973 | 1103 | 13.4\% |
| 8 | 281841 | 0012P | 110.0 | 110.1 | 2535 | -504 | 80.1\% | 683 | 556 | 18.6\% |
| 9 | 288050 | 0035P | 25.9 | 25.9 | 735 | 1187 | 61.6\% | 374 | 359 | 4.1\% |
| 10 | 282967 | 0017P | 1.5 | 1.4 | 718 | 907 | 26.5\% | 514 | 506 | 1.7\% |
| 11 | 291642 | 0046P | 8.4 | 8.2 | 2240 | 2827 | 26.2\% | 1035 | 995 | 3.9\% |
| 12 | 321951 | 0072P | 11.2 | 11.3 | 807 | -983 | 21.7\% | 1023 | 980 | 4.1\% |
| 13 | 302580 | 0096P | 3.3 | 3.0 | 1187 | 1000 | 15.8\% | 1336 | 1442 | 7.9\% |
| 14 | 287441 | 0035P | 20.4 | 20.5 | 720 | -3956 | 449.1\% | 739 | 739 | 0.1\% |
| 15 | 305233 | 0128P | 10.6 | 10.6 | 862 | -3956 | 358.7\% | 584 | 739 | 26.5\% |
| 16 | 307635 | 0143P | 47.7 | 47.5 | 1388 | 1654 | 19.2\% | 864 | 731 | 15.4\% |
| 17 | 282691 | 0014P | 6.2 | 6.1 | 1272 | 1654 | 30.0\% | 623 | 731 | 17.3\% |
| 18 | 281536 | 0012P | 74.2 | 74.3 | 255 | -107 | 58.1\% | 358 | 387 | 8.0\% |
| 19 | 291486 | 0046P | 10.4 | 10.5 | 974 | -1619 | 66.3\% | 623 | 633 | 1.6\% |
| 20 | 319741 | 0302P | 2.3 | 2.3 | 785 | 643 | 18.1\% | 232 | 256 | 10.2\% |
| 21 | 304390 | 0119P | 0.0 | 0.0 | 136 | -150 | 9.8\% | 212 | 224 | 5.5\% |
| 22 | 301154 | 0092P | 21.7 | 21.7 | 57 | -221 | 284.5\% | 186 | 189 | 1.7\% |


|  |  |  |  |  | RADIUS |  |  | CURVE LENGTH |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | ID | Route Name | PC | PT | AutoCAD | ArcMap | $\begin{gathered} \text { Error } \\ \% \end{gathered}$ | AutoCAD | ArcMap | $\begin{gathered} \text { Error } \\ \% \end{gathered}$ |
| 23 | 324672 | 0012P | 6.5 | 6.3 | 1729 | -1400 | 19.1\% | 1301 | 1316 | 1.1\% |
| 24 | 281252 | 0012P | 25.3 | 25.6 | 1406 | -1526 | 8.5\% | 1627 | 1597 | 1.9\% |
| 25 | 307948 | 0143P | 9.0 | 8.9 | 1087 | -2520 | 131.9\% | 355 | 370 | 4.3\% |
| 26 | 289234 | 0039P | 62.7 | 62.8 | 979 | -4584 | 368.1\% | 865 | 844 | 2.4\% |
| 27 | 296378 | 0083P | 19.7 | 19.8 | 975 | -1382 | 41.7\% | 681 | 680 | 0.2\% |
| 28 | 309033 | 0150P | 23.4 | 23.3 | 1438 | 2038 | 41.7\% | 720 | 710 | 1.4\% |
| 29 | 324255 | 0012P | 79.2 | 79.1 | 556 | 1289 | 131.8\% | 366 | 408 | 11.5\% |
| 30 | 310589 | 0157P | 2.4 | 2.5 | 1375 | 2335 | 69.7\% | 316 | 272 | 13.9\% |
| 31 | 309924 | 0153P | 31.9 | 31.8 | 148 | 205 | 38.5\% | 260 | 236 | 9.3\% |
| 32 | 317769 | 0261P | 5.8 | 5.7 | 914 | 1270 | 38.9\% | 721 | 691 | 4.1\% |
| 33 | 306944 | 0138P | 3.0 | 2.6 | 1826 | 2035 | 11.5\% | 2460 | 2454 | 0.2\% |
| 34 | 306290 | 0132P | 0.5 | 0.6 | 975 | 1386 | 42.1\% | 496 | 501 | 0.9\% |
| 35 | 308916 | 0150P | 38.9 | 38.8 | 1376 | -2498 | 81.6\% | 773 | 722 | 6.6\% |
| 36 | 308910 | 0150P | 40.6 | 40.4 | 1771 | 1977 | 11.6\% | 1212 | 1182 | 2.5\% |
| 37 | 323907 | 0012P | 120.0 | 119.9 | 845 | 1251 | 48.0\% | 509 | 582 | 14.2\% |
| 38 | 289091 | 0039P | 43.0 | 43.1 | 997 | 1245 | 24.9\% | 779 | 794 | 1.9\% |
| 39 | 282221 | 0014P | 8.5 | 8.7 | 1324 | 1184 | 10.6\% | 834 | 851 | 2.1\% |
| 40 | 285906 | 0030P | 18.9 | 19.1 | 2611 | -2872 | 10.0\% | 832 | 797 | 4.2\% |
| 41 | 305980 | 0128P | 7.5 | 7.2 | 1324 | 1497 | 13.1\% | 1351 | 1282 | 5.1\% |
| 42 | 307402 | 0143P | 18.6 | 18.9 | 1891 | -2579 | 36.3\% | 1426 | 1522 | 6.7\% |
| 43 | 318809 | 0276P | 60.6 | 60.8 | 3570 | -5262 | 47.4\% | 961 | 966 | 0.5\% |
| 44 | 322877 | 0191P | 294.3 | 294.2 | 902 | -1263 | 39.9\% | 542 | 483 | 10.9\% |
| 45 | 290948 | 0044P | 26.3 | 26.6 | 1862 | -2037 | 9.4\% | 1594 | 1584 | 0.7\% |
| 46 | 305574 | 0128P | 41.3 | 41.4 | 2355 | -1556 | 33.9\% | 301 | 275 | 8.7\% |
| 47 | 324252 | 0012P | 79.4 | 79.3 | 866 | 1024 | 18.3\% | 736 | 702 | 4.7\% |
| 48 | 296952 | 0087P | 14.5 | 14.7 | 595 | -648 | 8.8\% | 1022 | 1036 | 1.4\% |
| 49 | 304115 | 0115P | 2.2 | 2.2 | 1789 | -2682 | 49.9\% | 378 | 318 | 16.0\% |
| 50 | 314163 | 0191P | 284.0 | 284.4 | 3375 | -3366 | 0.3\% | 2171 | 2136 | 1.6\% |
| 51 | 279219 | 0006P | 143.6 | 143.7 | 470 | 3670 | 680.3\% | 495 | 511 | 3.2\% |
| 52 | 306020 | 0128P | 3.0 | 3.0 | 1427 | 1808 | 26.7\% | 296 | 295 | 0.4\% |
| 53 | 319358 | 0279P | 2.0 | 1.7 | 1239 | 1320 | 6.6\% | 1252 | 1205 | 3.7\% |
| 54 | 287422 | 0035P | 18.9 | 19.0 | 857 | 2297 | 168.0\% | 577 | 601 | 4.2\% |
| 55 | 299740 | 0089P | 242.5 | 242.4 | 2682 | 2883 | 7.5\% | 637 | 635 | 0.3\% |
| 56 | 307980 | 0143P | 4.1 | 4.0 | 1146 | 1387 | 21.0\% | 476 | 478 | 0.3\% |
| 57 | 302528 | 0096P | 10.7 | 10.5 | 683 | 767 | 12.3\% | 1318 | 1319 | 0.1\% |
| 58 | 311115 | 0162P | 7.6 | 7.9 | 2828 | 2904 | 2.7\% | 1372 | 1694 | 23.5\% |
| 59 | 319979 | 0313P | 6.0 | 6.2 | 1243 | 1071 | 13.8\% | 666 | 648 | 2.7\% |
| 60 | 303281 | 0102P | 9.5 | 9.4 | 315 | 385 | 22.1\% | 573 | 602 | 5.0\% |
| 61 | 323064 | 0191P | 268.7 | 268.6 | 2814 | 4160 | 47.8\% | 255 | 248 | 2.9\% |


|  |  |  |  |  | RADIUS |  |  | CURVE LENGTH |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | ID | Route <br> Name | PC | PT | AutoCAD | ArcMap | $\begin{gathered} \text { Error } \\ \% \end{gathered}$ | AutoCAD | ArcMap | $\begin{gathered} \text { Error } \\ \% \end{gathered}$ |
| 62 | 287731 | 0035P | 55.6 | 55.7 | 841 | 1149 | $36.7 \%$ | 234 | 318 | 35.7\% |
| 63 | 308007 | 0144P | 0.3 | 0.4 | 936 | 3477 | 271.5\% | 253 | 251 | 0.6\% |
| 64 | 311235 | 0162P | 31.2 | 31.4 | 1030 | 1197 | 16.2\% | 930 | 915 | 1.7\% |
| 65 | 287669 | 0035P | 50.2 | 50.3 | 2492 | 2538 | 1.9\% | 293 | 288 | 1.5\% |
| 66 | 323174 | 0191P | 254.9 | 254.8 | 1923 | 2313 | 20.3\% | 437 | 460 | 5.3\% |
| 67 | 279854 | 0006P | 206.6 | 206.4 | 964 | 1081 | 12.1\% | 892 | 887 | 0.6\% |
| 68 | 305391 | 0128P | 25.6 | 25.7 | 1966 | 2263 | 15.1\% | 268 | 265 | 1.3\% |
| 69 | 317700 | 0261P | 10.6 | 10.5 | 1033 | 1326 | 28.4\% | 497 | 496 | 0.2\% |
| 70 | 299533 | 0089P | 312.6 | 312.5 | 1012 | 1154 | 14.0\% | 445 | 456 | 2.4\% |
| 71 | 284838 | 0024P | 89.4 | 89.2 | 524 | 629 | 20.1\% | 850 | 861 | 1.3\% |
| 72 | 293248 | 0065P | 8.2 | 8.3 | 384 | 224 | 41.7\% | 393 | 406 | 3.4\% |
| 73 | 323644 | 0191P | 26.5 | 26.3 | 1419 | 1527 | 7.6\% | 721 | 680 | 5.6\% |
| 74 | 317640 | 0261P | 29.9 | 29.9 | 2168 | 2792 | 28.8\% | 328 | 326 | 0.5\% |
| 75 | 285680 | 0029P | 17.9 | 18.0 | 1033 | 1233 | 19.4\% | 634 | 632 | 0.3\% |
| 76 | 282335 | 0014P | 20.1 | 20.4 | 2890 | 2945 | 1.9\% | 1140 | 1141 | 0.1\% |
| 77 | 292847 | 0062P | 0.6 | 0.7 | 2127 | 2290 | 7.7\% | 783 | 786 | 0.4\% |
| 78 | 314666 | 0196P | 17.7 | 17.9 | 5642 | 5482 | 2.8\% | 1147 | 1143 | 0.4\% |
| 79 | 300038 | 0089P | 103.0 | 103.5 | 5883 | 5293 | 10.0\% | 2887 | 3918 | 35.7\% |
| 80 | 300071 | 0089P | 97.5 | 97.5 | 2132 | 2566 | 20.4\% | 259 | 253 | 2.3\% |
| 81 | 314963 | 0199P | 12.7 | 12.7 | 565 | 1544 | 173.5\% | 234 | 225 | 4.0\% |
| 82 | 309804 | 0153P | 33.8 | 33.9 | 419 | 855 | 104.1\% | 536 | 539 | 0.6\% |
| 83 | 309880 | 0153P | 34.0 | 33.9 | 173 | 634 | 266.9\% | 378 | 432 | 14.3\% |
| 84 | 285923 | 0030P | 50.0 | 50.2 | 2844 | 2820 | 0.8\% | 1151 | 1146 | 0.4\% |
| 85 | 292344 | 0056P | 43.6 | 43.5 | 1305 | 1430 | 9.6\% | 918 | 877 | 4.5\% |
| 86 | 305969 | 0128P | 8.7 | 8.6 | 1000 | 1311 | 31.1\% | 544 | 536 | 1.4\% |
| 87 | 290571 | 0040P | 25.5 | 25.4 | 1284 | 1469 | 14.4\% | 777 | 744 | 4.3\% |
| 88 | 314343 | 0191P | 370.6 | 370.7 | 659 | 828 | 25.7\% | 582 | 592 | 1.7\% |
| 89 | 303876 | 0113P | 6.7 | 6.7 | 979 | 1248 | 27.5\% | 282 | 278 | 1.3\% |
| 90 | 300357 | 0089P | 5.5 | 5.2 | 5892 | 4783 | 18.8\% | 1833 | 1837 | 0.2\% |
| 91 | 295491 | 0072P | 15.0 | 14.9 | 1689 | 1910 | 13.1\% | 659 | 638 | 3.2\% |
| 92 | 281706 | 0012P | 96.1 | 96.2 | 546 | 868 | 58.9\% | 558 | 555 | 0.5\% |
| 93 | 289966 | 0040P | 52.4 | 52.8 | 3827 | 4528 | 18.3\% | 1731 | 1733 | 0.1\% |
| 94 | 283081 | 0018P | 23.4 | 23.6 | 2276 | 2329 | 2.3\% | 1065 | 1110 | 4.3\% |
| 95 | 295849 | 0077P | 3.7 | 3.7 | 537 | 717 | 33.6\% | 358 | 355 | 0.9\% |
| 96 | 310850 | 0158P | 10.3 | 10.2 | 772 | 2408 | 211.7\% | 326 | 293 | 10.1\% |
| 97 | 297364 | 0089P | 86.4 | 86.7 | 2301 | 2435 | 5.8\% | 1250 | 1225 | 2.0\% |
| 98 | 312882 | 0189P | 21.0 | 20.5 | 1042 | 1077 | 3.4\% | 2635 | 2647 | 0.5\% |
| 99 | 290978 | 0044P | 22.8 | 22.7 | 1344 | 1748 | $30.1 \%$ | 318 | 306 | 3.7\% |
| 100 | 284609 | 0024P | 106.1 | 106.4 | 1125 | 1197 | 6.4\% | 1901 | 1787 | 6.0\% |


[^0]:    $\mathrm{N}=$ the required sample size for a given confidence interval
    $\mathrm{z}=1.96$ for a 95 percent confidence interval
    $\sigma=$ the standard deviation
    $\mathrm{E}=$ the tolerance level expressed in decimal form

