**Technical Report Documentation Page** 

1. Report No. FHWA/TX-12/5-6386-01-1	2. Government Accession	ı No.	3. Recipient's Catalog No	).
4. Title and Subtitle IMPLEMENTATION OF NEW PA PREDICTION MODELS IN PMIS	VEMENT PERFC REPORT	PRMANCE	5. Report Date August 2012 Published: Nove	mber 2012
			6. Performing Organizati	on Code
<ul> <li><sup>7. Author(s)</sup></li> <li>Nasir Gharaibeh, Andrew Wimsatt,</li> <li>Menendez, Angela Jannini Weissma</li> <li>Carlos Chang-Albitres</li> </ul>	Siamak Salimineja ann, Jose Weissma	d, Jose Rafael nn, and	8. Performing Organizati Report 5-6386-01	on Report No.  -1
9. Performing Organization Name and Address Texas A&M Transportation Institut	e		10. Work Unit No. (TRAI	S)
College Station, Texas 77843-3135			11. Contract or Grant No. Project 5-6386-0	1
12. Sponsoring Agency Name and Address Texas Department of Transportation Research and Technology Impleme	1 ntation Office		13. Type of Report and Pe Technical Report October 2011 – A	eriod Covered : August 2012
P.O. Box 5080 Austin, Texas 78763-5080			14. Sponsoring Agency C	ode
<ul> <li>15. Supplementary Notes</li> <li>Project performed in cooperation w. Administration.</li> <li>Project Title: Implementation of Ne URL: http://tti.tamu.edu/documents</li> <li>16. Abstract</li> <li>Pavement performance prediction n enable managers and engineers to p</li> <li>This report describes TxDOT's effor Management Information System (I introducing the new performance pre- managers through a webinar worksl survey and follow-up interviews wir optimization procedure. In most car reasonable by TxDOT pavement pra- optimization process. Minor discreption replicate of the PMIS optimization part and the Ride Score models in PMIS</li> <li>17. Key Words</li> <li>Pavement, Distress, PMIS, Loading Asphalt, Concrete</li> </ul>	ith the Texas Depart w Pavement Perfor /5-6386-01-1.pdf nodels and mainten lan and prioritize p prts to implement an PMIS). Specifically rediction models (d nop, (b) assessing th th TxDOT engineer ses, the new pavem actitioners. No ma pancies were found process (developed may require further , Hot-Mix	tment of Transport mance Prediction I ance and rehabilita avement M&R acti- nd improve these car , this report describ eveloped in Project ne reasonableness of rs and managers, ar ent performance pr jor errors were four between the output by the researchers er evaluation and in 18. Distribution Statemen No restrictions. T public through N' National Technic Alexandria, Virgi http://www.ntis.g	tation and the Fede Models in PMIS tion (M&R) optimi vities in a cost-effe apabilities in the Pa bes the processes and co-6386) to TxDO of these models thread (c) evaluating the rediction models which are done of the trediction models which are done of the to f PMIS and the big suggesting that the provement. this document is av TIS: al Information Service inia 22312	ral Highway ization processes ective manner. wement nd results of (a) T engineers and ough an online he PMIS ere found he PMIS output of a he needs analysis
19. Security Classif. (of this report) Unclassified	20. Security Classif. (of the Unclassified	iis page)	21. No. of Pages 86	22. Price

Form DOT F 1700.7 (8-72) Reproduction of completed page authorized

## IMPLEMENTATION OF NEW PAVEMENT PERFORMANCE PREDICTION MODELS IN PMIS: REPORT

by

Nasir Gharaibeh Assistant Professor Department of Civil Engineering, Texas A&M University

Andrew Wimsatt Materials and Pavements Division Head Texas A&M Transportation Institute

Siamak Saliminejad Graduate Research Assistant Texas A&M Transportation Institute Jose Rafael Menendez Graduate Research Assistant Texas A&M Transportation Institute

Angela Jannini Weissmann Transportation Researcher University of Texas at San Antonio

Jose Weissmann Professor University of Texas at San Antonio

Carlos Chang-Albitres Assistant Professor University of Texas at El Paso

Report: 5-6386-01-1 Project: 5-6386-01 Project Title: Implementation of New Pavement Performance Prediction Models in PMIS

> Performed in cooperation with the Texas Department of Transportation and the Federal Highway Administration

> > August 2012 Published: November 2012

TEXAS A&M TRANSPORTATION INSTITUTE College Station, Texas 77843-3135

# DISCLAIMER

This research was performed in cooperation with the Texas Department of Transportation (TxDOT) and the Federal Highway Administration (FHWA). The contents of this report reflect the views of the authors, who are responsible for the facts and the accuracy of the data presented herein. The contents do not necessarily reflect the official view or policies of the FHWA or TxDOT. This report does not constitute a standard, specification, or regulation.

# ACKNOWLEDGMENTS

This project was conducted in cooperation with TxDOT and FHWA. The authors thank Mr. Bryan Stampley (Project Director) and Dr. Jenny Li (Project Advisor) of the Construction Division for their support and assistance during the course of this project. The authors also thank the TxDOT personnel who participated in the webinars and web survey.

# **TABLE OF CONTENTS**

List of Figures	ix
List of Tables	X
Chapter 1 Introduction Overview of Newly Developed Pavement Performance Prediction Models Overview of PMIS Optimization Process	<b>1</b> 
Chapter 2 Feedback from TxDOT Practitioners on Newly Developed Pavement Performance Prediction Models	<b>9</b> 
Chapter 3 Evaluation of PMIS Optimization Process Stage 1: Evaluation of the Needs Analysis Step Stage 2: Evaluation of the Ranking Step Stage 3: Evaluation of the Optimization Process as a Whole	<b>21</b> 22 23 23 24
Chapter 4 Summary and Findings ACP Performance Prediction Models CRCP and JCP Performance Prediction Models Evaluation of the PMIS Optimization Process	27 27 27 27 28
References	
Appendix A: Web Survey	A-1
Appendix B: Calibrated ACP Performance Model Coefficients	B-1
Appendix C: Calibrated CRCP Performance Model Coefficients	C-1
Appendix D: Calibrated JCP Performance Model Coefficients	<b>D-</b> 1

# LIST OF FIGURES

Figure 1. General Form of TxDOT's Pavement Condition Prediction Models	3
Figure 2. Climate and Subgrade Zones for Performance Prediction Models.	3
Figure 3. Calibrated and Original DS Prediction Models (Zone 1, Pavement Family A, &	
HR) (Number of data points (n)= 1647; Average 20-year ESALs = 4.74 million)	5
Figure 4. Flowchart of the Main Steps of PMIS's Optimization Process	6
Figure 5. Example Figure from Web Survey Showing How the Models Account for the	
Effect of Traffic Level on Pavement Deterioration after Applying Heavy	
Rehabilitation to Pavement Family A in Zone 1.	9
Figure 6. Example Figure from Web Survey Showing How the Models Account for the	
Effect of M&R Type on Pavement Deterioration (Pavement Family A in Zone 1)	10
Figure 7. Example Figure from Web Survey Showing How the Models Account for the	
Contribution of Each Individual Distress Type on Pavement Deterioration (Zone 1,	
Pavement Family B, and Medium Traffic).	11
Figure 8. Opinions of TxDOT's Practitioners of Newly-Developed Pavement	
Performance Prediction Models.	12
Figure 9. Actual vs. Predicted DS (Zone 1, Pavement Family A, Low Traffic, PM)	14
Figure 10. Actual vs. Predicted DS (Zone 1, Pavement Family A, Medium Traffic, PM)	15
Figure 11. Actual vs. Predicted DS (Zone 2, Pavement Family A, Medium Traffic, PM)	15
Figure 12. Actual vs. Predicted DS (Zone 2, Pavement Family C, Medium Traffic, PM)	15
Figure 13. Actual vs. Predicted DS (Zone 3, Pavement Family A, Medium Traffic, PM)	16
Figure 14. Actual vs. Predicted DS (Zone 3, Pavement Family A, Medium Traffic, MR)	16
Figure 15. Actual vs. Predicted DS (Zone 3, Pavement Family A, High Traffic, PM)	16
Figure 16. Actual vs. Predicted DS (Zone 3, Pavement Family A, High Traffic, MR)	17
Figure 17. Actual vs. Predicted DS (Zone 3, Pavement Family A, High Traffic, HR).	17
Figure 18. Actual vs. Predicted DS (Zone 3, Pavement Family C, Medium Traffic, PM)	17
Figure 19. Actual vs. Predicted DS (Zone 3, Pavement Family C, Medium Traffic, MR)	18
Figure 20. Actual vs. Predicted DS (Zone 4, Pavement Family C, Low Traffic, PM)	18
Figure 21. Actual vs. Predicted DS (Zone 4, Pavement Family C, High Traffic, LR)	18
Figure 22. Illustration of PMIS Optimization Process and Evaluation Stages.	21
Figure 23. Needed and Funded Investments for Bryan District, Obtained from PMIS (in	
Million Dollars).	22
Figure 24. Investment in Funded Projects within Each Treatment Category for Bryan	
District in 2011 (in Million Dollars).	23
Figure 25. Lane-Miles of Each Treatment Category in 2011 (Bryan District)	23
Figure 26. PMIS and Replicated Total Funded Projects in 4 Years (in Million Dollars)	24
Figure 27. PMIS and Replicate Total Lane-Miles of Each Treatment Category for 4	
Years.	25

# LIST OF TABLES

Table 1. Condition Effects and Unit Costs for Treatment Categories Considered in PMIS	
Optimization Process.	6
Table 2. Summary of Responses Indicating Highttp://tti.tamu.edu/about/marketing-	
communications/publication-services/txdot-deliverables-preparation-tools/hly over	
or under Prediction of Pavement Condition by the New Models.	13
Table 3. Roadway Segments Provided by the Respondents as Representative of Typical	
Performance.	14
Table 4. Lane-Miles of Treatment According to PMIS and Replicate Needs Analyses for	
2011	22
Table 5. Funds Allocation from PMIS Output and Replicate in (in Million Dollars)	24
Table 6. PMIS Output and Replicate Yearly Lane-Miles of Each Treatment Category	25
Table 7. Comparison of Benefit and Cost Parameters for the Four Treatment Categories	
for an Example Pavement Section.	26
Table 8. Average Distress, Ride and Condition Scores from PMIS Output and Replicate	26

## **CHAPTER 1 INTRODUCTION**

The Texas Department of Transportation (TxDOT) initiated the work described in this report as part of its efforts to implement and improve its pavement performance prediction models and pavement management optimization process. These models and optimization process can enable TxDOT managers and engineers to plan and prioritize pavement maintenance and rehabilitation (M&R) activities in a cost-effective manner.

A new set of pavement performance prediction models were recently developed as part of Research Project 0-6386 (Gharaibeh et al. 2012). These new models were developed by calibrating the original ones (Stampley et al. 1995) to pavement condition field data that represent the various pavement types used by TxDOT and the diverse climatic, subgrade, and traffic conditions in Texas.

TxDOT has implemented the new models in the Pavement Management Information System (PMIS). To build confidence in these models, they needed to be introduced to and reviewed by TxDOT's pavement managers and engineers. Also, the optimization process in PMIS has shown signs of instability (e.g., occasionally producing unrealistic results) and thus needed detailed evaluation to determine if there are errors in the computer code of this process.

The objectives of this implementation project are:

- Introduce the prediction models developed in Project 0-6386 to TxDOT pavement practitioners (experts) through a webinar workshop.
- Obtain feedback from TxDOT pavement practitioners on the reasonableness of the new prediction models through an online survey and follow-up interviews.
- Evaluate the PMIS optimization procedure and propose improvements, if needed.

Accomplishing the above objectives will enhance the utilization of PMIS and its analytical capabilities for early identification and planning of M&R activities and for estimation of future funding needs.

# OVERVIEW OF NEWLY DEVELOPED PAVEMENT PERFORMANCE PREDICTION MODELS

TxDOT measures pavement surface condition in terms of the following indicators (Stampley et al. 1995):

- Density of individual distress types (*L<sub>i</sub>*): this represents the density of each distress in the pavement section. Density is expressed as quantity of distress per mile, quantity of distress per section area, quantity of distress per 100-ft, etc. (depending on the distress type). PMIS computes an *L<sub>i</sub>* value for each distress based on distress quantities recorded by the field raters and then normalized for section length.
- Distress Score (DS): this is a composite index that combines multiple  $L_i$ 's using mathematical utility functions. DS has a 1–100 scale (with 100 representing no or minimal distress).

• Condition Score (CS): this is a broad composite index that combines the DS and ride quality. CS has a 1–100 scale (with 100 representing no or minimal distress and roughness).

Each distress Li is converted into a 0-1 utility value, as follows:

$$U_{i} = \begin{cases} 1.0 & \text{when } L_{i} = 0\\ 1 - \alpha e^{-\left(\frac{\rho}{L_{i}}\right)^{\beta}} & \text{when } L_{i} > 0 \end{cases}$$
(1)

 $U_i$  ranges between zero and 1.0 and represents the quality of a pavement in terms of overall usefulness (e.g., a  $U_i$  of 1.0 indicates that distress type *i* is not present and thus is most useful). The  $\alpha$  (Maximum Loss factor),  $\beta$  (Slope factor), and  $\rho$  (Prolongation factor) control the location of the utility curve's inflection point and the slope of the curve at that point.

DS is computed as aggregated index of the  $U_i$  values of multiple distress types, and CS is computed as a broader index that combines DS and a ride utility value ( $U_{Ride}$ ), as shown in Equations 2 and 3.

$$DS = 100 \times \prod_{i=1}^{n} U_{i}$$

$$CS = U_{\text{Ride}} \times DS$$
(2)
(3)

The original  $L_i$ , DS, and CS prediction models (which were previously coded in PMIS) were developed in the 1980s–1990s (Stampley et al. 1995) based on solely engineering judgment due to lack of field data at that time. These original models were calibrated using actual pavement condition field data in TxDOT Project 0-6386. The calibration process produced new model coefficients that minimize the difference between predicted performance and actual (observed) performance of the pavement. These new models predict distress density and ride loss ( $L_i$ ) (and consequently DS and CS) using the general form shown in Equation 4.

$$L_i = \alpha e^{-\left(\frac{A}{Age}\right)^{\beta}}$$
(4)

where  $L_i$ : represents the density of distress *i* (i.e., distress quantity normalized for section length) or percent ride quality lost. *Age*: number of years since last construction on the pavement section;  $\alpha$ : maximum loss factor which controls the maximum Li;  $\beta$ : slope factor which controls how steeply  $L_i$  increases in the middle of the curve; A: prolongation factor controls the location of the  $L_i$  curve's inflection point. Note that  $\alpha$  and  $\beta$  in Equation 4 are not the same  $\alpha$  and  $\beta$  in Equation 1. The general shape of this model is shown in Figure 1.

For Equation 4, separate values of  $\alpha$ ,  $\beta$ , and A were developed in Project 0-6386 for all combinations of pavement type, distress type, subgrade type, climate and traffic level (TxDOT 2012).



Figure 1. General Form of TxDOT's Pavement Condition Prediction Models.

Families of pavement sections with uniform characteristics were formed to reduce the combinations of model coefficients. These characteristics included climate, subgrade quality, pavement type, M&R type, traffic loading level, and distress type.

Four climate-subgrade zones that represent different combinations of subgrade and climate in terms of its effect on pavement performance were formed, as follows:

- Zone 1: This zone represents wet-cold climate, and poor, very poor, or mixed subgrade.
- Zone 2: This zone represents wet-warm climate, and poor, very poor, or mixed subgrade.
- Zone 3: This zone represents dry-cold climate, and good, very good, or mixed subgrade.
- Zone 4: This zone represents dry-warm climate, and good, very good, or mixed subgrade.

These zones are depicted in the color-coded map shown in Figure 2.



Figure 2. Climate and Subgrade Zones for Performance Prediction Models.

Only asphalt concrete pavement (ACP) families A, B, and C were included in the web-based survey. These pavement families represent the majority of the pavement network throughout TxDOT's districts. The pavement families considered in the survey are as follows:

- Pavement Family A: This pavement family includes thick ACP (PMIS Pavement Type 4), Intermediate ACP (PMIS Pavement Type 5), and overlaid ACP (PMIS Pavement Type 9).
- Pavement Family B: This pavement family includes composite pavement (PMIS Pavement Type 7) and concrete pavement overlaid with ACP (PMIS Pavement Type 8).
- Pavement Family C: This pavement family includes thin ACP (PMIS Pavement Type 6) and thin-surfaced ACP (PMIS Pavement Type 10).

Each pavement type has its own distress types. For example, asphalt pavements have seven distress types: shallow rutting, deep rutting, patching, failures, block cracking, alligator cracking, and longitudinal cracking.

M&R actions that are applied to pavement are classified into four categories of preventive maintenance (PM), light rehabilitation (LR), medium rehabilitation (MR) and heavy rehabilitation (HR). The M&R treatment types associated with these categories for flexible pavement are as follows:

- PM: Seal coats (chip seals), thin overlays (less than 2 inches), and micro-surfacing treatments.
- LR: HMA overlay with thickness between 2 and less than 3 inches; pavement widening and application of full width seal coat, base repair and seal; milling, sealing and thin overlay.
- MR: Mill and inlay; mill, stabilize base and seal; level up and overlay; widen pavement, level up and overlay or seal coat; 3- to 5-inch HMA overlay; thick overlay (without any other activity such as milling); mill, patch, under seal and inlay; base repair, spot seal, edge repair and overlay; mill, cement stabilize base and overlay or seal.
- HR: Includes reconstruction of the base and surface, milling, and thick overlay or similar activities that restore the pavement functional and structural condition to nearly original conditions.

The above definitions of M&R categories were derived from Murphy and Zhang (2009). Also, these definitions were verified through an online survey of TxDOT districts that was conducted as part of TxDOT Project 0-6683.

Traffic divisions include three loading levels, as follows:

- Low Traffic Loading: This level includes pavement sections that have a 20-year projected cumulative Equivalent Single Axle Load (ESAL) of less than 1.0 million ESALs.
- Medium Traffic Loading: This level includes pavement sections that have a 20-year projected cumulative ESAL greater than or equal to 1.0 million ESALs and less than 10 million ESALs.
- Heavy Traffic Loading: This level includes pavement sections that have a 20-year projected cumulative ESAL greater than or equal to 10 million ESALs.

The model calibration process was applied to hot-mix asphalt concrete pavement (ACP) due to the availability of historical field data. It was less applicable to continuously reinforced concrete pavement (CRCP) and jointed plain concrete pavement (JPCP) due to limited availability of field data. Figure 3 shows an example calibrated model for Distress Score for pavement family A [thick ACP (PMIS Pavement Type 4), Intermediate ACP (PMIS Pavement Type 5), and overlaid ACP (PMIS Pavement Type 9)].



Figure 3. Calibrated and Original DS Prediction Models (Zone 1, Pavement Family A, & HR) (Number of data points (n)= 1647; Average 20-year ESALs = 4.74 million).

## **OVERVIEW OF PMIS OPTIMIZATION PROCESS**

The PMIS optimization process is described in the PMIS Technical Manual published in December 2011 (TxDOT 2011). According to the technical manual, the optimization process consists of 10 steps; however six of them are the most critical: establishing distress quantities for the analysis base year, treatment selection from decision tress, "after treatment" distress ratings and ride quality, computation of benefits and effective life, cost effectiveness ratio calculations, and selection of pavement sections to be funded. The sequence of these critical steps is illustrated in Figure 4.

Treatments considered in this process are categorized as PM, LR, MR, HR, and Needs Nothing (NN). The definitions of these treatment categories were discussed earlier in the previous section of this report. Predefined decision trees are used for identifying needed treatment category for each pavement section. Each treatment category is associated with a reason code as a function of seven factors: pavement type, distress ratings, Ride Score, average daily traffic per lane, functional class, average county rainfall, and time since last surfacing. These decision trees and associated reason codes are provided in PMIS technical manual.



Figure 4. Flowchart of the Main Steps of PMIS's Optimization Process.

The effect of each treatment category on pavement performance is measured in terms of reduction in distress ratings and gain in ride score. Once a treatment category is selected, distress rating and ride score are adjusted according Table 1. The unit costs of these treatment categories may vary depending on local factors such as project location and size. The unit costs used in this study are shown in Table 1.

	-		
Treatment Category	Gain in Distress Utility	Gain in Ride Score	Unit Cost, \$/lane-mile (used in this study)
Stop gap or need nothing	No change in distress ratings	No change in Ride Score	None
РМ	Reset distress ratings to zero	Increase Ride Score by 0.5	29,000
LR	Reset distress ratings to zero	Increase Ride Score by 1.5	173,000
MR	Reset distress ratings to zero	Increase Ride Score by 4.8	237,000
HR	Reset distress ratings to zero	Increase Ride Score by 4.8	442,000

 Table 1. Condition Effects and Unit Costs for Treatment Categories Considered in PMIS

 Optimization Process.

Benefits are measured as the area between the distress or ride utility curves before and after the suggested treatment is applied. Four possible scenarios for before and after utility curves are analyzed.

- Curves intersect before the age of 20 years.
- Curves are parallel, in which case treatment life is set to 20 years.
- Curves approach each other very closely (a difference equal to or less than 0.0001 utility units), but they do not intersect.
- Curves reach the failure criterion of 0.6 distress utility and 0.3 ride utility.

According to the PMIS technical manual, the area is calculated using a trapezoidal approximation. In this investigation, the area between the before and after utility curves was calculated by integration using the following equation.

$$Area_{after} = \int_0^A 1 - e^{\left[ -\left(\frac{\rho_d}{Age_d}\right)^{\beta_d} \right]} dx = Age_d - \frac{\rho_d \Gamma\left(-\frac{1}{\beta_d} \left(\frac{\rho_d}{Age_d}\right)^{\beta_d}\right)}{\beta_d}$$
(5)

To calculate the overall (or total) benefit, distress area  $(A_D)$  and ride score area  $(A_R)$  are added up considering equal weight for each one. In other words, total benefit (B) is computed using the following equation and with weights  $W_D$  and  $W_R$  set to 50.

$$B = 2\left[\frac{W_D}{100}A_D + \frac{W_R}{100}A_R\right]$$
(6)

The cost effectiveness ratio is calculated for each section based on the benefit of the selected treatment, treatment effective life (predicted using the performance prediction models discussed earlier), treatment uniform annual cost, section lane-miles, and vehicle miles traveled on the pavement section. The mathematical expression for computing this ratio is as follows:

$$CERatio = 10000x \left[\frac{LMxB}{EffLife \ x \ UACost}\right] x \ log_{10}VMT \tag{7}$$

CERatio	=	Cost-Effectiveness Ratio.
LM	=	Lane Miles.
В	=	Benefit.
EffLife	=	Effective Life of the Needs Estimate treatment, in years.
UACost	=	Uniform Annual Cost of the Needs Estimate treatment, in dollars.
		$UACost = TCost x \left[ \frac{DRate(1 + DRate)^{EffLife}}{(1 + DRate)^{Efflife} - 1} \right]$
UACost	=	Uniform Annual Cost of the Needs Estimate treatment, in dollars.
TCost	=	Treatment Cost (current or future) of the Needs Estimate treatment
		$TCost = UCostx(1 + InfRate)^n$
DRate	=	Discount Rate, in percent per year; DRate=6.5%.
InfRate	=	Inflation Rate, in percent per year.
n	=	Number of years that the Unit Cost has been projected.
VMT	=	Vehicle Miles Traveled.

Finally the pavement sections are sorted in order of decreasing cost-effectiveness ratio. Sections are funded in this order until the available budget is depleted. Sections that are not selected to receive any treatment are classified as Stop Gap.

#### CHAPTER 2 FEEDBACK FROM TXDOT PRACTITIONERS ON NEWLY DEVELOPED PAVEMENT PERFORMANCE PREDICTION MODELS

Two webinars on the newly-developed performance prediction models were conducted for TxDOT practitioners from various districts throughout the state. The webinars provided an overview of the mathematical forms, calibration process, and sensitivity and accuracy of these models. The first webinar covered the ACP performance prediction models. The second webinar covered the continuously reinforced concrete pavement (CRCP) and jointed concrete pavement (JCP) prediction models. The webinar presentations are contained in Product 5-6386-01-P1.

#### **ACP PERFORMANCE PREDICTION MODELS**

Following the introductory webinar for the ACP performance prediction models, a series of webbased surveys were prepared and launched to obtain feedback from TxDOT's practitioners on the reasonableness and accuracy of the ACP prediction curves based on their practical experiences. To account for differences in pavement performance among the different climate-subgrade zones of TxDOT's districts, a separate survey was conducted for each zone, with a total of four surveys.

Each of the four web surveys presented the developed performance prediction curves in several ways so that the participants can evaluate the reasonableness of the developed curves under different combinations of pavement type, M&R type, and traffic level. Specifically, within each survey (one survey for each of the four climate-subgrade zones), and for each pavement family (there are three pavement families), the following figures are presented to the respondents:

First, the web survey starts with four figures (for four different M&R types) consisting of the performance prediction curves of pavements with similar type, M&R treatment, and subgradeclimate, but different traffic levels. Each one of these figures includes three curves (for three different traffic levels) as well as the original performance curve. These figures are used to: (1) show how the models account for the effect of traffic level on pavement deterioration, and (2) compare the new curves with original ones. Figure 5 is an example of these figures.



Figure 5. Example Figure from Web Survey Showing How the Models Account for the Effect of Traffic Level on Pavement Deterioration after Applying Heavy Rehabilitation to Pavement Family A in Zone 1.

Second, the web survey has three figures consisting of the ACP performance prediction curves of pavements with similar pavement family, traffic level, and subgrade-climate, but different M&R treatment. These figures are used to: (1) show how the models account for the effect of M&R type on pavement deterioration, and (2) compare the developed curves with original ones. Figure 6 is an example of these figures.



Figure 6. Example Figure from Web Survey Showing How the Models Account for the Effect of M&R Type on Pavement Deterioration (Pavement Family A in Zone 1).

Third, the web survey ends with 12 figures (for all combinations of four M&R types and three traffic levels) consisting of the utility curves of each individual ACP distress type. These curves are used to show how the models account for the contribution of each individual distress type on pavement deterioration. Figure 7 is an example of these figures.



#### Figure 7. Example Figure from Web Survey Showing How the Models Account for the Contribution of Each Individual Distress Type on Pavement Deterioration (Zone 1, Pavement Family B, and Medium Traffic).

In some cases, some curves have not been developed due to the lack of historical condition data and thus were not presented in the survey. The four web surveys are presented in Appendix A.

#### ACP MODEL SURVEY RESULTS AND FOLLOW-UP EFFORTS

A total of 17 survey responses were received for the ACP models, including five responses from Zone 1, four responses from Zone 2, six responses from Zone 3, and two responses from Zone 4. These responses are from transportation and pavement engineers and managers from the districts of Abilene, Brownwood, Bryan, Childress, Corpus Christi, Dallas, Fort Worth, Lubbock, Odessa, Paris, and Wichita Falls.

As can be seen from Figure 8, a large majority of all responses (93 percent) rated the performance curves as either reasonable or slightly over or under predicting. This suggests that, in most cases, the respondents believe that the model predictions of pavement condition agree with or slightly differ from their own experience. Only 7 percent of all responses indicated that the models predictions are unreasonable (i.e., highly over or under predict pavement condition). This suggests that only in a few cases the respondents believe that the model predictions of pavement condition are considerably lower or higher than their own experience. These cases are shown in Table 2.



Figure 8. Opinions of TxDOT's Practitioners of Newly-Developed Pavement Performance Prediction Models.

Almost all of the "highly over/under predicting" responses are from the three districts of Paris, Bryan, and Brownwood. Within these cases, the Paris District responses suggest that the models predictions are highly optimistic; the Brownwood District responses suggest that the models predictions are highly pessimistic; and the Bryan District responses are mixed (suggesting that the models are highly optimistic in some cases and highly pessimistic in other cases). Follow-up phone calls were made to the respondents who indicated that at least one curve highly over/under predicts pavement performance. They were asked to specify example roadway segments that, in their opinion, represent the typical pavement performance in their districts for certain combinations of climate, subgrade, traffic, pavement type, and M&R history. The researchers extracted the historical pavement condition data for these typical roadway segments from PMIS and compared it to the condition data predicted by the new models.

Table 3 presents the provided typical roadway segment. Historical pavement condition data (i.e., DS) of the specified segments were extracted from PMIS database. Their M&R and construction data were extracted from TxDOT's Design and Construction Information System (DCIS) database. The extracted condition data are then plotted versus their corresponding prediction curves and presented in Figures 8 through 20. Each point in the graphs represents the average DS of all PMIS sections that compose the specified segment. As can be seen from these figures, the actual condition data for most of the typical segments match the models predictions reasonably.

	Performan	ce Curve	Response			
Zone	Pavement Family	M&R Type	Traffic	Model Rating	District	
1	А	MR	Low	Highly Overpredicts	Paris	
1	А	HR	Low	Highly Overpredicts	Paris	
1	А	HR	Medium	Highly Overpredicts	Paris	
1	А	HR	High	Highly Overpredicts	Paris	
1	В	PM	Medium	Highly Overpredicts	Paris	
1	В	LR	Medium	Highly Overpredicts	Paris	
1	В	MR	Medium	Highly Overpredicts	Paris	
1	В	HR	Medium	Highly Overpredicts	Paris	
2	A	MR	Low	Highly Underpredicts	Corpus Christi	
2	В	PM	Low	Highly Underpredicts	Bryan	
2	В	PM	Medium	Highly Underpredicts	Bryan	
2	В	LR	Low	Highly Underpredicts	Bryan	
2	В	LR	Medium	Highly Underpredicts	Bryan	
2	В	MR	Low	Highly Underpredicts	Bryan	
2	В	MR	Medium	Highly Underpredicts	Bryan	
3	А	HR	Medium	Highly Overpredicts	-	
3	А	HR	High	Highly Overpredicts	-	
3	А	PM	Low	Highly Underpredicts	Brownwood	
3	А	PM	Medium	Highly Underpredicts	Brownwood	
3	А	PM	High	Highly Underpredicts	Brownwood	
3	А	LR	High	Highly Underpredicts	Brownwood	
3	А	MR	High	Highly Underpredicts	Brownwood	
3	В	PM	Low	Highly Underpredicts	Brownwood	
3	В	LR	Low	Highly Underpredicts	Brownwood	
3	В	HR	Low	Highly Underpredicts	Brownwood	

 Table 2. Summary of Responses Indicating Highly over or under Prediction of Pavement

 Condition by the New Models.

District	County	Highway Name	BRM	ERM
Paris	Delta	SH-24	218	224
Paris	Lamar	FM-195	658	668
Paris	Fannin	SH-121	210	216
Bryan	Brazos County	US-190	686	692
Bryan	Madison	I-45	134	152
Corpus Christi	San Patricio	FM-2986	602	604
Corpus Christi	San Patricio	SH-188	538	570
Brownwood	Eastland	nd IH-20		340
Brownwood	Lampasas	US190	540	550
Brownwood	Coleman	US-84	520	528
Brownwood	Brown	US-84	568	574
Brownwood	McCulloch	US190	460	468
Abilene	Scurry	US-84	384	426
Odessa	Midland	IH-20	122	136
Odessa	Reeves	IH-10	204	209
Odessa	Martin	SH-349	288	344
Odessa	Pecos	BI-10G	236	455

 Table 3. Roadway Segments Provided by the Respondents as Representative of Typical Performance.



Figure 9. Actual vs. Predicted DS (Zone 1, Pavement Family A, Low Traffic, PM).



Figure 10. Actual vs. Predicted DS (Zone 1, Pavement Family A, Medium Traffic, PM).



Figure 11. Actual vs. Predicted DS (Zone 2, Pavement Family A, Medium Traffic, PM).



Figure 12. Actual vs. Predicted DS (Zone 2, Pavement Family C, Medium Traffic, PM).



Figure 13. Actual vs. Predicted DS (Zone 3, Pavement Family A, Medium Traffic, PM).



Figure 14. Actual vs. Predicted DS (Zone 3, Pavement Family A, Medium Traffic, MR).



Figure 15. Actual vs. Predicted DS (Zone 3, Pavement Family A, High Traffic, PM).



Figure 16. Actual vs. Predicted DS (Zone 3, Pavement Family A, High Traffic, MR).



Figure 17. Actual vs. Predicted DS (Zone 3, Pavement Family A, High Traffic, HR).



Figure 18. Actual vs. Predicted DS (Zone 3, Pavement Family C, Medium Traffic, PM).



Figure 19. Actual vs. Predicted DS (Zone 3, Pavement Family C, Medium Traffic, MR).



Figure 20. Actual vs. Predicted DS (Zone 4, Pavement Family C, Low Traffic, PM).



Figure 21. Actual vs. Predicted DS (Zone 4, Pavement Family C, High Traffic, LR).

#### **CRCP AND JCP PERFORMANCE PREDICTION MODELS**

The second webinar presented the CRCP and JCP performance prediction models to TxDOT personnel that had experience with these pavement types. The webinar presentations are contained in Product 5-6386-01-P1. The general consensus among TxDOT participants in that webinar was that the models as presented did not need any changes at this time.

However, in the future, TxDOT personnel indicated that coarse aggregate type be included for the CRCP performance prediction models in the future, since CRCP performance is affected by coarse aggregate type. Currently, the PMIS database does not contain coarse aggregate type for CRCP.

In addition, TxDOT personnel indicated that JCP performance is highly dependent on variations in subgrade and environmental conditions. In addition, several participants indicated problems with JCP that had no load transfer devices (i.e., poor load transfer efficiency) or poor subbase support. Currently, the PMIS database does not contain load transfer or subbase support information for JCP.

#### **CHAPTER 3 EVALUATION OF PMIS OPTIMIZATION PROCESS**

This chapter provides an evaluation of the logic of the PMIS optimization process. This process was programmed in a spreadsheet (called "replicate" henceforth) and the results of this replicate were compared to the output of PMIS. The replicate spreadsheet includes all of the optimization process steps described in the PMIS Technical Manual (TxDOT 2011). The evaluation was conducted using data from the Bryan District and was divided into three stages, as illustrated in Figure 22.



Figure 22. Illustration of PMIS Optimization Process and Evaluation Stages.

Figure 23 shows the needed and funded M&R investments (obtained from PMIS output) for the years 2011–2014 for Bryan District. The funded investments were used as annual budgets in the replicate. While the analysis was done for a 10-year period, only the results of the first four years (2011–2014) are presented here for simplicity and to be consistent with TxDOT approach of developing 4-year pavement management plans. Table 4 shows the allocations of these investments among the four treatment categories (PM, LR, MR, and HR), as determined by PMIS.



Figure 23. Needed and Funded Investments for Bryan District, Obtained from PMIS (in Million Dollars).

#### STAGE 1: EVALUATION OF THE NEEDS ANALYSIS STEP

The purpose of this stage is to evaluate the needs analysis component of the optimization process by comparing the needed treatments in 2011 (obtained from PMIS output) to those obtained from the replicate.

Table 4 presents the agreements and differences between PMIS and the replicate in terms of needed lane-miles of each treatment category in 2011. For example, PMIS and the replicate agree on 766 lanes-miles of PM; but differ on one lane-mile (identified by PMIS as "needs PM" and by the replicate as "needs LR"). This one lane-mile discrepancy is located on FM0179 (MR 246+02.0 to 246+01.5). This section's Ride Score in 2011 was 2.447. According to the decision tree reason code A200, this section needs LR (since Ride Score is less than 2.5); but PMIS indicates that it does not need any M&R action.

As can be seen from Table 4, there are minor differences between PMIS and the replicate in terms treatments identified by the needs analysis. Most of these discrepancies occur in sections that are classified by PMIS as "Need Nothing" but classified by the replicate as PM, and ones that are classified by PMIS as LR but classified by the replicate as MR. This suggests that PMIS may not be adhering strictly to the decision trees (documented in the PMIS technical manual).

Table 4. Lane-Miles of Treatment According to PMIS and Replicate Needs Analyses for	r
2011.	

		According to Replicate					
		PM	LR	MR	HR	NN	
According to PMIS	PM	766	1.0	-	-	-	
	LR	-	20.1	4.0	-	-	
	MR	-	-	96.9	1.0	-	
	HR	-	-	-	25.4	-	
	NN	3.4	1	0	0	1,001.9	

#### **STAGE 2: EVALUATION OF THE RANKING STEP**

The purpose of this stage is to evaluate the ranking step of the optimization process. The needed treatments, predicted performance, and cost-effectiveness calculations are obtained directly from the PMIS output. Thus, any differences between the PMIS output and the replicate spreadsheet output can be attributed to differences in the ranking step (i.e., prioritizing pavement sections that need M&R treatment based on their cost-effectiveness ratio). As can be seen from Figures 24 and 25, PMIS and the replicate agree in terms of allocated funds and lane-miles of each treatment category. Minor differences can be attributed to minor simplifying assumptions that were made in the replicate spreadsheets. This suggests that the ranking step of the optimization process is coded properly in PMIS.



Figure 24. Investment in Funded Projects within Each Treatment Category for Bryan District in 2011 (in Million Dollars).



Figure 25. Lane-Miles of Each Treatment Category in 2011 (Bryan District).

#### **STAGE 3: EVALUATION OF THE OPTIMIZATION PROCESS AS A WHOLE**

The purpose of this stage is to evaluate the optimization process as a whole. As can be seen from Figures 26, noticeable differences exist between PMIS and the replicate in terms of total allocated funds for LR and HR over the 2011–2014 period. These differences between PMIS and the replicate exist in all treatment categories when these funds are evaluated on a year-by-year basis (see Table 5). A similar pattern exists in terms of lane-miles of each treatment category (Figure 27 and Table 6).



Figure 26. PMIS and Replicated Total Funded Projects in 4 Years (in Million Dollars).

Year		PM		LR		MR		HR	
		PMIS	Rep.	PMIS	Rep.	PMIS	Rep.	PMIS	Rep.
2011	Needed	22.2	22.3	4.2	3.8	23.3	24.0	11.2	11.9
	Funded	5.9	6.2	0.0	2.6	16.1	12.8	4.1	4.5
2012	Needed	17.3	8.3	0.7	0.1	2.0	4.4	5.7	0.4
	Funded	8.8	8.3	0.3	0.1	0.5	4.4	5.6	0.4
2013	Needed	8.6	9.4	1.3	0.0	5.6	0.0	0.2	0.4
	Funded	3.4	4.4	0.4	0.0	0.5	0.0	0.1	0.0
2014	Needed	5.2	14.6	3.8	0.9	8.8	0.0	7.4	0.4
	Funded	2.4	8.5	0.0	0.0	6.1	0.0	0.0	0.0

Table 5. Funds Allocation from PMIS Output and Replicate in (in Million Dollars).



Figure 27. PMIS and Replicate Total Lane-Miles of Each Treatment Category for 4 Years.

	PM		LR		MR		HR	
	PMIS	Rep.	PMIS	Rep.	PMIS	Rep.	PMIS	Rep.
2011	203	214	0	15	68	54	9	10
2012	302	268	2	1	2	18	13	1
2013	117	141	2	0	2	0	0	0
2014	83	282	0	0	26	0	0	0

Table 6. PMIS Output and Replicate Yearly Lane-Miles of Each Treatment Category.

In both outputs (PMIS and replicate) the funded pavement sections are predominantly PM. This behavior may be explained by (a) the limited influence that "effective life" has on the cost-effectiveness ratio (Note that effective life affects both the numerator and denominator of the equation of the cost-effectiveness ratio, which diminishes its effect), and (b) the relative benefit differences and the relative cost differences among these four treatment categories. Table 7 shows the unit costs, annual benefit, annual cost, and CERatio for the four treatment categories for an example pavement section (Highway BS0011H, Beginning Reference Marker 336, 0.3-mile long, 4 lanes, and ADT of 3,400 vehicles per day). The rehabilitation categories (LR, MR and HR) have much higher unit costs and uniform annual costs compared to the PM category. Thus, to be selected by the optimization procedure (i.e., to have higher CERatio), these rehabilitation categories must have very high benefits. For example, for HR to be selected over PM in this case, its benefit must be at least 10.2 times the benefit of PM. This explains the predominant selection of PM compared to the rehabilitation categories. The implication of this observation is that PMIS's optimization process appears to favor low-cost treatments over long- life treatments.

# Table 7. Comparison of Benefit and Cost Parameters for the Four Treatment Categories for<br/>an Example Pavement Section.

Attribute	PM	LR	MR	HR
Unit Cost, \$/lane mile	29,000	173,000	237,000	442,000
Uniform Annual Cost, \$	47.06	47.72	47.86	53.69
Annual Benefit	3,803.02	20,102.68	25,004.78	44,445.23
Effective Life, years	11	13	15	17
VMT	372,300	372,300	372,300	372,300
CERatio	123.74	23.74	19.14	12.08

Table 8 shows the average Distress Score, Ride Score, and Condition Score after the selected treatments are applied in each year. As can be seen from this table, PMIS and the replicate agree in terms of average condition of the network for all indicators. Minor differences between PMIS and the replicate in terms of these indexes averages can be explained by minor discrepancies in the needs analysis (see discussion of Stage 2), minor simplifying assumptions used in the replicate, and discrepancies in the Ride Score performance prediction models.

Table 8. Average Distress, Ride and Condition Scores from PMIS Output and Replicate.

Year	PMIS			Replicate		
	DS	Ride	CS	DS	Ride	CS
2011	89.85	3.66	87.31	89.85	3.65	87.31
2012	93.78	4.61	92.21	97.23	4.41	90.89
2013	95.76	4.32	94.33	97.96	4.33	96.16
2014	96.60	4.28	94.56	97.32	4.25	93.33
### **CHAPTER 4 SUMMARY AND FINDINGS**

The research team presented the ACP, CRCP, and JCP performance prediction models to TxDOT personnel through two webinars and an ACP model web survey. The researchers also evaluated the logic and output of PMIS optimization process.

### **ACP PERFORMANCE PREDICTION MODELS**

Following the webinar for the ACP performance prediction models, a series of web-based surveys were prepared and launched to obtain feedback from TxDOT's practitioners on the reasonableness and accuracy of the ACP prediction curves based on their practical experiences. To account for differences in pavement performance among the different climate-subgrade zones of TxDOT's districts, a separate survey was conducted for each zone, with a total of four surveys.

A total of 17 survey responses were received for the ACP models from the Abilene, Brownwood, Bryan, Childress, Corpus Christi, Dallas, Fort Worth, Lubbock, Odessa, Paris, and Wichita Falls Districts. A large majority of all responses (93 percent) rated the performance curves as either reasonable or slightly over or under predicting. Only 7 percent of all responses indicated that the models predictions are unreasonable (i.e., highly over or under predict pavement condition).

Almost all of the "highly over/under predicting" responses are from the Paris, Bryan, and Brownwood Districts. Follow-up phone calls were made to the respondents who indicated that at least one curve highly over/under predicts pavement performance. They were asked to specify example roadway segments that, in their opinion, represent the typical pavement performance in their districts for certain combinations of climate, subgrade, traffic, pavement type, and M&R history. The researchers extracted the historical pavement condition data for these typical roadway segments from PMIS and compared it to the condition data predicted by the new models. The actual condition data for most of these segments match the model predictions.

Based on the above findings, the research team concluded that the ACP pavement performance prediction models do not need modification at this time. Appendix B contains the ACP performance model coefficients.

### **CRCP AND JCP PERFORMANCE PREDICTION MODELS**

The second webinar presented the CRCP and JCP performance prediction models to TxDOT personnel that had experience with these pavement types. The general consensus among TxDOT participants in that webinar was that the models as presented did not need any changes at this time.

However, in the future, TxDOT personnel indicated that coarse aggregate type should be included for the CRCP performance prediction models in the future, since CRCP performance is affected by coarse aggregate type. Currently, the PMIS database does not contain coarse aggregate type for CRCP.

TxDOT personnel indicated that JCP performance is highly dependent on variations in subgrade and environmental conditions. In addition, several participants indicated problems with JCP that had no load transfer devices (i.e., poor load transfer efficiency) or poor subbase support. Currently, the PMIS database does not contain load transfer or subbase support information for JCP.

Appendix C contains the CRCP performance model coefficients. Appendix D contains the JCP performance model coefficients.

### **EVALUATION OF THE PMIS OPTIMIZATION PROCESS**

The research team also evaluated the logic of the PMIS optimization process. This process was programmed in a spreadsheet (called replicate) and the results of this replicate were compared to the output of PMIS. The replicate spreadsheet includes all of the optimization process steps described in the PMIS Technical Manual (TxDOT 2011). The evaluation was conducted using data from the Bryan district. PMIS and the replicate were found to agree in terms of M&R treatments, needed and allocated budgets, and condition indicators in the first year of the planning period. However, minor differences began to appear and accumulate in future years of the planning period. These differences can be explained by minor discrepancies in the needs analysis, minor simplifying assumptions used in the replicate, and discrepancies in the Ride Score performance prediction models.

In both outputs (PMIS and replicate) the funded pavement sections are predominantly PM. This behavior may be explained by (a) the limited influence that "effective life" has on the cost-effectiveness ratio, and (b) the relative benefit differences and the relative cost differences among these four treatment categories. The implication of this observation is that PMIS's optimization process appears to favor low-cost treatments over long- life treatments.

#### REFERENCES

Gharaibeh, N., T. Freeman, S. Saliminejad, C. Chang-Albitres, J. Weissman, A. Weissman, A. Wimsatt, and C. Gurganus (2012). *Evaluation and Development of Pavement Scores, Performance Models and Needs Estimates for the TxDOT Pavement Management Information System*. Final Report No. FHWA/TX-12/0-6386-3, Texas Transportation Institute, Texas A&M University System, College Station, Texas, 2012.

Murphy, M. and Zhang, Z. (2009). Assumptions Used in Selecting Project Class (PMIS Treatment Types) for the District 4-year Pavement Management Plans. Draft Report to TxDOT.

Stampley, B. E., Miller, B., Smith, R. E., and Scullion, T. (1995). *Pavement Management Information System Concepts, Equations, and Analysis Models*. Report No. TX-96/1989-1, Texas Transportation Institute and Texas Department of Transportation.

TxDOT (2011). *PMIS Technical Manual*. Prepared by Texas Department of Transportation Construction Division, Materials and Pavements Section, December 2011.

### **APPENDIX A: WEB SURVEY**

**TxDOT Project** 

### **Calibration of PMIS Pavement Performannce Prediction Models**

Conducted as part of TxDOT Project 0-6386

### Zone 1



General

### General

#### Q1. Please provide your contact information below:

Name (required)	
District	
Title	
E-mail	

Pvt Family A

### **Definitions**

**Zone 1:** wet-cold climate, and poor, very poor, or mixed subgrade



#### **Pavement Family A:**

Thick ACP (PMIS Pavement Type 4)
Intermediate ACP (PMIS Pavement Type 5)
Overlaid ACP (PMIS Pavement Type 9)

**Age0:**The age when distress first appears **Age70:**The age when DS drops into 70

DS15:DS at the age of 15 years

Low Traffic: 20-year projected cumulative ESAL of lass than 1.0 million ESALs. Medium Traffic: 20-year projected cumulative ESAL of between1.0 million and 10 million ESALs. High Traffic: 20-year projected cumulative ESAL of higher than 10 million ESALs.



### Performance Curves for Zone 1, Pvt Family A, and Preventive Maintenance (PM)

Number of data points (n)= 2068; Average 20-year ESALs = 5.12 million

#### Q2. Please rate the above curves as follows:

	Highly Overpredicts (The curve should be shifted down or left)	Slightly Overpredicts (The curve should be shifted down or left)	Reasonable	Slightly Undepredicts (The curve should be shifted up or right)	Highly Undepredicts (The curve should be shifted up or right)
Low Traffic	0	0	0	0	0
Medium Traffic	0	•	0	0	•
High Traffic	0	0	0	0	0



### Performance Curves for Zone 1, Pvt Family A, and Light Rehabilitation (LR)

Number of data points (n)= 742; Average 20-year ESALs = 6.83 million

### Q3. Please rate the above curves as follows:

	Highly Overpredicts (The curve should be shifted down or left)	Slightly Overpredicts (The curve should be shifted down or left)	Reasonable	Slightly Undepredicts (The curve should be shifted up or right)	Highly Undepredicts (The curve should be shifted up or right)
Low Traffic	۲	۲	0	0	0
Medium Traffic	•	0	0	0	0
High Traffic	0	0	0	0	0



### Performance Curves for Zone 1, Pvt Family A, and Medium Rehabilitation (MR)

Number of data points (n)= 647; Average 20-year ESALs = 5.82 million

### Q4. Please rate the above curves as follows:

	Highly Overpredicts (The curve should be shifted down or left)	Slightly Overpredicts (The curve should be shifted down or left)	Reasonable	Slightly Undepredicts (The curve should be shifted up or right)	Highly Undepredicts (The curve should be shifted up or right)
Low Traffic	0	0	0	0	0
Medium Traffic	0	•	•	•	•
High Traffic	0	•	•	0	0



### Performance Curves for Zone 1, Pvt Family A, and Heavy Rehabilitation (HR)

Number of data points (n)= 1647; Average 20-year ESALs = 4.74 million

### **Q5.** Please rate the above curves as follows:

	Highly Overpredicts (The curve should be shifted down or left)	Slightly Overpredicts (The curve should be shifted down or left)	Reasonable	Slightly Undepredicts (The curve should be shifted up or right)	Highly Undepredicts (The curve should be shifted up or right)
Low Traffic	0	۲	•	0	0
Medium Traffic	0	•	•	0	0
High Traffic	0	0	•	0	0

### **Comments:**

### Comparison of Zone1 and Pavement Family A Models Grouped by Treatment Types and Traffic Levels



Q6. Please review the above curves and provide any comments you might have.

### Comparison of Utility Curves for Various Distresses (Grouped by Treatment Types) for Zone 1, Pavement Family A and Low Traffic



**Q7.** Please review the above curves and provide any comments you might have.

Comparison of Utility Curves for Various Distresses (Grouped by Treatment Types) for Zone 1, Pavement Family A and Medium Traffic



**Q8.** Please review the above curves and provide any comments you might have.

### Comparison of Utility Curves for Various Distresses (Grouped by Treatment Types) for Zone 1, Pavement Family A and High Traffic



**Q9.** Please review the above curves and provide any comments you might have.

#### Pvt Family B

### **Definitions**

Zone 1: wet-cold climate, and poor, very poor, or mixed subgrade



#### **Pavement Family B:**

Composite pavement (PMIS Pavement Type 7)
Concrete pavement overlaid with ACP (PMIS Pavement Type 8)

Age0:The age when distress first appears Age70:The age when DS drops into 70 DS15:DS at the age of 15 years

Low Traffic: 20-year projected cumulative ESAL of lass than 1.0 million ESALs. Medium Traffic: 20-year projected cumulative ESAL of between 1.0 million and 10 million ESALs. High Traffic: 20-year projected cumulative ESAL of higher than 10 million ESALs.



### Performance Curves for Zone 1, Pvt Family B, and Preventive Maintenance (PM)

Number of data points (n)= 738; Average 20-year ESALs = 4.66 million

#### Q10. Please rate the above curves as follows:

	Highly Overpredicts (The curve should be shifted down or left)	Slightly Overpredicts (The curve should be shifted down or left)	Reasonable	Slightly Undepredicts (The curve should be shifted up or right)	Highly Undepredicts (The curve should be shifted up or right)
Low Traffic	۲	0	0	0	0
Medium Traffic	•	•	•	0	0
High Traffic	•	0	0	0	0



### Performance Curves for Zone 1, Pvt Family B, and Light Rehabilitation (LR)

# pavement

Number of data points (n)= 210; Average 20-year ESALs = 6.08 million

### Q11. Please rate the above curves as follows:

	Highly Overpredicts (The curve should be shifted down or left)	Slightly Overpredicts (The curve should be shifted down or left)	Reasonable	Slightly Undepredicts (The curve should be shifted up or right)	Highly Undepredicts (The curve should be shifted up or right)
Low Traffic	۲	0	0	0	0
Medium Traffic	•	•	•	0	0
High Traffic	•	0	0	0	0

#### Districts 100 PAR 90 80 FTW 70 DAL Distress Score (DS) ۱ Calibrated-LowT 60 Calibrated-MedT TYL ۱ 50 Calibrated-HighT ATL ۱ Original 40 Data Traffic Data Points 30 Curve Ageo Age<sub>70</sub> DS15 20 Low 5 12 62 10 9 >15 92 0 High 5 8.5 37 0 1 3 5 6 10 11 12 13 14 15 2 4 7 8 9 Age (years)

### Performance Curves for Zone 1, Pvt Family B, and Medium Rehabilitation (MR)

### Composite or

### overlaid concrete

pavement Number of data points (n)= 68; Average 20-year ESALs = 2.96 million

### Q12. Please rate the above curves as follows:

	Highly Overpredicts (The curve should be shifted down or left)	Slightly Overpredicts (The curve should be shifted down or left)	Reasonable	Slightly Undepredicts (The curve should be shifted up or right)	Highly Undepredicts (The curve should be shifted up or right)
Low Traffic	0	0	۲	0	0
Medium Traffic	0	0	0	0	0
High Traffic	•	•	•	0	•



### Performance Curves for Zone 1, Pvt Family B, and Heavy Rehabilitation (HR)

## overlaid concrete

pavement

Number of data points (n)= 466; Average 20-year ESALs = 5.44 million

### Q13. Please rate the above curves as follows:

	Highly Overpredicts (The curve should be shifted down or left)	Slightly Overpredicts (The curve should be shifted down or left)	Reasonable	Slightly Undepredicts (The curve should be shifted up or right)	Highly Undepredicts (The curve should be shifted up or right)
Low Traffic	0	0	۲	0	0
Medium Traffic	0	•	•	0	0
High Traffic	0	0	0	0	0

### **Comments:**

### Comparison of Zone 1 and Pavement Family B Models Grouped by Treatment Types and Traffic Levels



Q14. Please review the above curves and provide any comments you might have.

Comparison of Utility Curves for Various Distresses (Grouped by Treatment Types) for Zone 1, Pavement Family B and Low Traffic



Q15. Please review the above curves and provide any comments you might have.

Comparison of Utility Curves for Various Distresses (Grouped by Treatment Types) for Zone 1, Pavement Family B and Medium Traffic



Q16. Please review the above curves and provide any comments you might have.

### Comparison of Utility Curves for Various Distresses (Grouped by Treatment Types) for Zone 1, Pavement Family B and High Traffic



#### Q17. Please review the above curves and provide any comments you might have.

#### Pvt Family C

### **Definitions**

Zone 1: wet-cold climate, and poor, very poor, or mixed subgrade



**Pavement Family C:**  Thin ACP (PMIS Pavement Type 6) •Thin-surfaced ACP (PMIS Pavement Type 10)

Age0: The age when distress first appears Age70: The age when DS drops into 70 DS15:DS at the age of 15 years

Low Traffic: 20-year projected cumulative ESAL of lass than 1.0 million ESALs. Medium Traffic: 20-year projected cumulative ESAL of between 1.0 million and 10 million ESALs. High Traffic: 20-year projected cumulative ESAL of higher than 10 million ESALs.

### Performance Curves for Zone 1, Pvt Family C, and Preventive Maintenance (PM)



surfaced ACP

Number of data points (n)= 1761; Average 20-year ESALs = 0.23 million

### Q18. Please rate the above curves as follows:

Note that the models for medium and high traffic are not developed due to insufficient data.

	Highly Overpredicts (The curve should be shifted down or left)	Slightly Overpredicts (The curve should be shifted down or left)	Reasonable	Slightly Undepredicts (The curve should be shifted up or right)	Highly Undepredicts (The curve should be shifted up or right)
Low Traffic	0	0	0	0	0

### Performance Curves for Zone 1, Pvt Family C, and Light Rehabilitation (LR)



surfaced ACP

Number of data points (n)= 501; Average 20-year ESALs = 0.27 million

#### Q19. Please rate the above curves as follows:

Note that the models for medium and high traffic are not developed due to insufficient data.

	Highly Overpredicts (The curve should be shifted down or left)	Slightly Overpredicts (The curve should be shifted down or left)	Reasonable	Slightly Undepredicts (The curve should be shifted up or right)	Highly Undepredicts (The curve should be shifted up or right)
Low Traffic	0	۲	0	0	0

### Performance Curves for Zone 1, Pvt Family C, and Medium Rehabilitation (MR)



Number of data points (n)= 581; Average 20-year ESALs = 0.23 million

### **Q20.** Please rate the above curves as follows:

Note that the models for medium and high traffic are not developed due to insufficient data.

	Highly Overpredicts (The curve should be shifted down or left)	Slightly Overpredicts (The curve should be shifted down or left)	Reasonable	Slightly Undepredicts (The curve should be shifted up or right)	Highly Undepredicts (The curve should be shifted up or right)
Low Traffic	0	0	0	0	0



Performance Curves for Zone 1, Pvt Family C, and Heavy Rehabilitation (HR)

Number of data points (n)= 1055; Average 20-year ESALs = 0.2 million

#### Q21. Please rate the above curves as follows:

Note that the models for medium and high traffic are not developed due to insufficient data.

	Highly Overpredicts (The curve should be shifted down or left)	Slightly Overpredicts (The curve should be shifted down or left)	Reasonable	Slightly Undepredicts (The curve should be shifted up or right)	Highly Undepredicts (The curve should be shifted up or right)	
Low Traffic	0	۲	0	0	0	

### Comments:

### Comparison of Zone 1 and Pavement Family C Models Grouped by Treatment Types and Traffic Levels



**Q22.** Please review the above curves and provide any comments you might have. Note that the models for medium and high traffic are not developed due to insufficient data.

### Comparison of Utility Curves for Various Distresses (Grouped by Treatment Types) for Zone 1, Pavement Family C and Low Traffic



#### Q23. Please review the above curves and provide any comments you might have.

# **Q24**. Please provide the information of the candidate roadway section(s) that can be used for improving the models:

	Section 1	Section 2	Section 3	Section 4	Section 5
County Name					
Highway Name					
Beginning Reference Marker					
Ending Reference Marker					

#### **Comments:**

#### **Q25.** Please provide the suggestions you might have on the groups with insufficient data.

#### Submit

By clicking on the Next button, your responses will be submitted and the survey ends here.

### APPENDIX B CALIBRATED ACP PERFORMANCE MODEL COEFFICIENTS

NOTE: For the following tables, Low Traffic is defined as having a projected 20 year 18KESAL forecast below 1,000,000; Medium Traffic is between 1,000,000 and 10,000,000; and High Traffic is greater than or equal to 10,000,000.

Distress Type         Treatment Type         a         β         A         a         b         a         a         a         a         a         a         a         a         a         a         a         a         a         a         a <tha< th="">         a<th></th><th colspan="2">Low Traffic</th><th>с</th><th>M</th><th>edium Trai</th><th>ffic</th><th colspan="3">High Traffic</th></tha<>		Low Traffic		с	M	edium Trai	ffic	High Traffic			
PM         100.00         0.41         75.16         100.00         0.43         102.38         100.00         0.39         58.34           Shallow Rutting         LR         100.00         0.47         79.75         100.00         0.47         107.18         100.00         0.42         66.85           MR         100.00         0.52         80.38         100.00         0.55         121.09         100.00         0.47         67.14           HR         100.00         0.53         91.69         100.00         0.58         122.99         100.00         0.55         70.69           Deep Rutting         PM         100.00         0.55         101.18         100.00         0.80         68.37         100.00         0.65         113.20           MR         100.00         0.56         115.81         100.00         0.88         80.79         100.00         0.65         116.07           HR         100.00         1.11         23.48         20.00         1.30         19.85         20.00         3.61         8.86           Failures         LR         20.00         1.11         23.48         20.00         1.30         19.85         20.00         4.54         9.18 </th <th>Distress Type</th> <th>Treatment Type</th> <th>α</th> <th>β</th> <th>Α</th> <th>α</th> <th>β</th> <th>А</th> <th>α</th> <th>β</th> <th>Α</th>	Distress Type	Treatment Type	α	β	Α	α	β	А	α	β	Α
Shallow Rutting         LR         100.00         0.47         79.75         100.00         0.47         107.18         100.00         0.42         66.85           MR         100.00         0.52         80.38         100.00         0.55         121.09         100.00         0.47         67.14           HR         100.00         0.53         91.69         100.00         0.55         121.09         100.00         0.47         67.14           PM         100.00         0.54         88.24         100.00         0.55         100.00         0.55         101.00         0.58         122.99         100.00         0.55         70.69           Deep Rutting         LR         100.00         0.55         101.18         100.00         0.88         80.79         100.00         0.65         116.07           MR         100.00         0.57         133.23         100.00         1.01         83.07         100.00         0.65         116.07           HR         20.00         1.11         23.48         20.00         1.30         19.85         20.00         3.61         8.86           Failures         LR         20.00         1.26         27.30         20.00         1.49<		PM	100.00	0.41	75.16	100.00	0.43	102.38	100.00	0.39	58.34
Rutting         MR         100.00         0.52         80.38         100.00         0.55         121.09         100.00         0.47         67.14           HR         100.00         0.53         91.69         100.00         0.58         122.99         100.00         0.55         70.69           Deep Rutting         PM         100.00         0.55         101.18         100.00         0.76         60.35         100.00         0.55         113.20           Deep Rutting         IR         100.00         0.56         115.81         100.00         0.88         80.79         100.00         0.65         116.07           MR         100.00         0.57         133.23         100.00         1.01         83.07         100.00         0.65         112.10           HR         100.00         0.57         133.23         100.00         1.30         19.85         20.00         3.61         88.66           LR         20.00         1.17         24.55         20.00         1.33         20.51         20.00         4.54         9.18           Block Cracking         LR         100.00         3.73         114.51         100.00         1.63         47.93         100.00         <	Shallow	LR	100.00	0.47	79.75	100.00	0.47	107.18	100.00	0.42	66.85
HR         100.00         0.53         91.69         100.00         0.58         122.99         100.00         0.55         70.69           Deep Rutting         PM         100.00         0.55         101.18         100.00         0.66         63.35         100.00         0.58         95.02           LR         100.00         0.55         101.18         100.00         0.80         68.37         100.00         0.65         113.20           MR         100.00         0.56         115.81         100.00         0.88         80.79         100.00         0.65         116.07           HR         100.00         0.57         133.23         100.00         1.01         83.07         100.00         0.65         112.31           Failures         PM         20.00         1.11         23.48         20.00         1.33         20.51         20.00         3.61         88.66           HR         20.00         1.17         24.55         20.00         1.33         20.51         20.00         4.54         9.18           Block Cracking         PM         100.00         3.73         114.51         100.00         1.83         47.93         100.00         6.75         83.46 </td <td>Rutting</td> <td>MR</td> <td>100.00</td> <td>0.52</td> <td>80.38</td> <td>100.00</td> <td>0.55</td> <td>121.09</td> <td>100.00</td> <td>0.47</td> <td>67.14</td>	Rutting	MR	100.00	0.52	80.38	100.00	0.55	121.09	100.00	0.47	67.14
PM         100.00         0.54         88.24         100.00         0.76         60.35         100.00         0.58         95.02           Deep Rutting         I.R         100.00         0.55         101.18         100.00         0.80         68.37         100.00         0.60         113.20           MR         100.00         0.56         115.81         100.00         0.88         80.79         100.00         0.65         116.07           HR         100.00         0.57         133.23         100.00         1.01         83.07         100.00         0.73         123.10           Failures         PM         20.00         1.11         23.48         20.00         1.33         20.51         20.00         3.61         88.66           MR         20.00         1.26         27.30         20.00         1.33         20.50         4.54         9.18           Bock Cracking         I.R         100.00         3.73         114.51         100.00         1.83         47.93         100.00         4.54         9.18           Block Cracking         I.R         100.00         3.81         130.91         100.00         1.83         47.93         100.00         4.54 <t< td=""><td></td><td>HR</td><td>100.00</td><td>0.53</td><td>91.69</td><td>100.00</td><td>0.58</td><td>122.99</td><td>100.00</td><td>0.55</td><td>70.69</td></t<>		HR	100.00	0.53	91.69	100.00	0.58	122.99	100.00	0.55	70.69
Deep Rutting         L.R         100.00         0.55         101.18         100.00         0.80         68.37         100.00         0.60         113.20           MR         100.00         0.56         115.81         100.00         0.88         80.79         100.00         0.65         116.07           HR         100.00         0.57         133.23         100.00         1.01         83.07         100.00         0.73         123.10           Failures         PM         20.00         1.11         23.48         20.00         1.33         20.51         20.00         3.61         88.66           HR         20.00         1.26         27.30         20.00         1.33         20.51         20.00         4.54         9.18           HR         20.00         1.40         30.05         20.00         1.40         21.49         20.00         4.54         9.18           Block Cracking         LR         100.00         3.73         114.51         100.00         1.83         47.93         100.00         7.69         94.98           Alligator         LR         100.00         3.81         130.91         100.00         2.58         48.74         100.00         5.10 </td <td></td> <td>PM</td> <td>100.00</td> <td>0.54</td> <td>88.24</td> <td>100.00</td> <td>0.76</td> <td>60.35</td> <td>100.00</td> <td>0.58</td> <td>95.02</td>		PM	100.00	0.54	88.24	100.00	0.76	60.35	100.00	0.58	95.02
Deep Raking         MR         100.00         0.56         115.81         100.00         0.88         80.79         100.00         0.65         116.07           HR         100.00         0.57         133.23         100.00         1.01         83.07         100.00         0.73         123.10           Failures         PM         20.00         1.11         23.48         20.00         1.30         19.85         20.00         3.61         88.86           MR         20.00         1.17         24.55         20.00         1.33         20.51         20.00         3.88         9.10           MR         20.00         1.26         27.30         20.00         1.37         21.50         20.00         4.19         9.14           HR         20.00         1.40         30.05         20.00         1.40         21.49         20.00         4.54         9.18           Block Cracking         PM         100.00         3.81         130.91         100.00         1.83         47.93         100.00         7.69         94.98           Alligator         LR         100.00         4.46         142.20         100.00         2.58         48.74         100.00         4.24	Deen Rutting	LR	100.00	0.55	101.18	100.00	0.80	68.37	100.00	0.60	113.20
HR         100.00         0.57         133.23         100.00         1.01         83.07         100.00         0.73         123.10           Failures         PM         20.00         1.11         23.48         20.00         1.30         19.85         20.00         3.61         8.86           Failures         LR         20.00         1.17         24.55         20.00         1.33         20.51         20.00         3.88         9.10           MR         20.00         1.26         27.30         20.00         1.37         21.50         20.00         4.19         9.14           HR         20.00         1.40         30.05         20.00         1.40         21.49         20.00         4.54         9.18           Block Cracking         PM         100.00         3.73         114.51         100.00         0.96         45.92         100.00         6.75         83.46           LR         100.00         3.81         130.91         100.00         1.83         47.93         100.00         7.69         94.98           MR         100.00         4.46         142.20         100.00         3.14         58.32         100.00         10.10         125.49	Deep Rutting	MR	100.00	0.56	115.81	100.00	0.88	80.79	100.00	0.65	116.07
PM         20.00         1.11         23.48         20.00         1.30         19.85         20.00         3.61         8.86           LR         20.00         1.17         24.55         20.00         1.33         20.51         20.00         3.88         9.10           MR         20.00         1.26         27.30         20.00         1.37         21.50         20.00         4.19         9.14           HR         20.00         1.40         30.05         20.00         1.40         21.49         20.00         4.54         9.18           Block Cracking         PM         100.00         3.73         114.51         100.00         1.83         47.93         100.00         7.69         94.98           MR         100.00         4.46         142.20         100.00         2.58         48.74         100.00         8.80         108.82           HR         100.00         4.58         101.42         100.00         3.14         58.32         100.00         4.24         8.20           Alligator         LR         100.00         0.58         101.42         100.00         0.53         113.11         100.00         5.73         11.28           Alligat		HR	100.00	0.57	133.23	100.00	1.01	83.07	100.00	0.73	123.10
Failures         LR         20.00         1.17         24.55         20.00         1.33         20.51         20.00         3.88         9.10           MR         20.00         1.26         27.30         20.00         1.37         21.50         20.00         4.19         9.14           HR         20.00         1.40         30.05         20.00         1.40         21.49         20.00         4.54         9.18           Block Cracking         PM         100.00         3.73         114.51         100.00         0.96         45.92         100.00         6.75         83.46           Block Cracking         LR         100.00         4.46         142.20         100.00         2.58         48.74         100.00         8.80         108.82           HR         100.00         4.46         142.20         100.00         3.14         58.32         100.00         10.10         125.49           Alligator         PM         100.00         0.58         101.42         100.00         0.53         113.11         100.00         4.24         8.20           Alligator         LR         100.00         0.52         115.98         100.00         0.53         133.61         10		PM	20.00	1.11	23.48	20.00	1.30	19.85	20.00	3.61	8.86
MR         20.00         1.26         27.30         20.00         1.37         21.50         20.00         4.19         9.14           HR         20.00         1.40         30.05         20.00         1.40         21.49         20.00         4.54         9.18           Block Cracking         PM         100.00         3.73         114.51         100.00         0.96         45.92         100.00         6.75         83.46           Block Cracking         LR         100.00         3.81         130.91         100.00         1.83         47.93         100.00         7.69         94.98           MR         100.00         4.46         142.20         100.00         2.58         48.74         100.00         8.80         108.82           HR         100.00         0.58         101.42         100.00         3.14         58.32         100.00         4.24         8.20           Alligator         LR         100.00         0.58         101.42         100.00         0.53         113.11         100.00         5.10         9.67           Cracking         MR         100.00         0.72         115.98         100.00         0.53         113.11         100.00         5.1	Failures	LR	20.00	1.17	24.55	20.00	1.33	20.51	20.00	3.88	9.10
HR         20.00         1.40         30.05         20.00         1.40         21.49         20.00         4.54         9.18           Block Cracking         PM         100.00         3.73         114.51         100.00         0.96         45.92         100.00         6.75         83.46           Block Cracking         LR         100.00         3.81         130.91         100.00         1.83         47.93         100.00         7.69         94.98           MR         100.00         4.46         142.20         100.00         2.58         48.74         100.00         8.80         108.82           HR         100.00         4.98         146.76         100.00         3.14         58.32         100.00         10.10         125.49           Alligator         PM         100.00         0.58         101.42         100.00         0.49         96.93         100.00         4.24         8.20           Alligator         LR         100.00         0.62         104.61         100.00         0.58         133.61         100.00         5.73         11.28           Alligator         HR         100.00         0.72         115.98         100.00         0.55         159.49	i unuios	MR	20.00	1.26	27.30	20.00	1.37	21.50	20.00	4.19	9.14
PM         100.00         3.73         114.51         100.00         0.96         45.92         100.00         6.75         83.46           Block Cracking         LR         100.00         3.81         130.91         100.00         1.83         47.93         100.00         7.69         94.98           MR         100.00         4.46         142.20         100.00         2.58         48.74         100.00         8.80         108.82           HR         100.00         4.46         142.20         100.00         3.14         58.32         100.00         10.10         125.49           Alligator         PM         100.00         0.58         101.42         100.00         0.49         96.93         100.00         4.24         8.20           Alligator         LR         100.00         0.62         104.61         100.00         0.53         113.11         100.00         5.10         9.67           Cracking         MR         100.00         0.72         115.98         100.00         0.55         159.49         100.00         6.06         11.90           Longitudinal Cracking         MR         500.00         0.52         116.51         500.00         0.54         104.		HR	20.00	1.40	30.05	20.00	1.40	21.49	20.00	4.54	9.18
Block Cracking         LR         100.00         3.81         130.91         100.00         1.83         47.93         100.00         7.69         94.98           MR         100.00         4.46         142.20         100.00         2.58         48.74         100.00         8.80         108.82           HR         100.00         4.98         146.76         100.00         3.14         58.32         100.00         10.10         125.49           Alligator         PM         100.00         0.58         101.42         100.00         0.49         96.93         100.00         4.24         8.20           Alligator         LR         100.00         0.62         104.61         100.00         0.53         113.11         100.00         5.10         9.67           Cracking         MR         100.00         0.72         115.98         100.00         0.58         133.61         100.00         5.73         11.28           HR         100.00         0.73         135.90         100.00         0.53         90.24         500.00         0.60         139.92           Longitudinal Cracking         LR         500.00         0.67         146.86         500.00         0.54         104		PM	100.00	3.73	114.51	100.00	0.96	45.92	100.00	6.75	83.46
MR         100.00         4.46         142.20         100.00         2.58         48.74         100.00         8.80         108.82           HR         100.00         4.98         146.76         100.00         3.14         58.32         100.00         10.10         125.49           Alligator Cracking         PM         100.00         0.58         101.42         100.00         0.49         96.93         100.00         4.24         8.20           MR         100.00         0.62         104.61         100.00         0.53         113.11         100.00         5.10         9.67           Cracking         MR         100.00         0.72         115.98         100.00         0.58         133.61         100.00         5.73         11.28           HR         100.00         0.73         135.90         100.00         0.65         159.49         100.00         6.06         11.90           Longitudinal Cracking         LR         500.00         0.60         133.63         500.00         0.54         104.52         500.00         0.50         71.55           MR         500.00         0.67         146.86         500.00         0.56         123.32         500.00         0.51	Block Cracking	LR	100.00	3.81	130.91	100.00	1.83	47.93	100.00	7.69	94.98
HR         100.00         4.98         146.76         100.00         3.14         58.32         100.00         10.10         125.49           Alligator Cracking         PM         100.00         0.58         101.42         100.00         0.49         96.93         100.00         4.24         8.20           Alligator Cracking         LR         100.00         0.62         104.61         100.00         0.53         113.11         100.00         5.10         9.67           MR         100.00         0.72         115.98         100.00         0.58         133.61         100.00         5.73         11.28           HR         100.00         0.73         135.90         100.00         0.65         159.49         100.00         6.06         11.90           PM         500.00         0.52         116.51         500.00         0.53         90.24         500.00         0.44         69.52           Longitudinal Cracking         LR         500.00         0.67         146.86         500.00         0.54         104.52         500.00         0.51         81.25           HR         500.00         0.71         153.66         500.00         0.59         146.45         500.00	DIOCK CLACKING	MR	100.00	4.46	142.20	100.00	2.58	48.74	100.00	8.80	108.82
PM         100.00         0.58         101.42         100.00         0.49         96.93         100.00         4.24         8.20           Alligator Cracking         LR         100.00         0.62         104.61         100.00         0.53         113.11         100.00         5.10         9.67           MR         100.00         0.72         115.98         100.00         0.58         133.61         100.00         5.73         11.28           HR         100.00         0.72         115.98         100.00         0.65         159.49         100.00         6.06         11.90           Longitudinal Cracking         PM         500.00         0.52         116.51         500.00         0.53         90.24         500.00         0.44         69.52           LR         500.00         0.60         133.63         500.00         0.54         104.52         500.00         0.51         81.25           MR         500.00         0.67         146.86         500.00         0.59         146.45         500.00         0.51         81.25           HR         500.00         0.71         153.66         500.00         0.59         146.45         500.00         0.58         84.37		HR	100.00	4.98	146.76	100.00	3.14	58.32	100.00	10.10	125.49
Alligator Cracking         LR         100.00         0.62         104.61         100.00         0.53         113.11         100.00         5.10         9.67           MR         100.00         0.72         115.98         100.00         0.58         133.61         100.00         5.73         11.28           HR         100.00         0.73         135.90         100.00         0.65         159.49         100.00         6.06         11.90           Longitudinal Cracking         PM         500.00         0.52         116.51         500.00         0.53         90.24         500.00         0.44         69.52           Longitudinal Cracking         LR         500.00         0.67         146.86         500.00         0.56         123.32         500.00         0.51         81.25           MR         500.00         0.67         146.86         500.00         0.59         146.45         500.00         0.51         81.25           HR         500.00         0.71         153.66         500.00         0.59         146.45         500.00         0.58         84.37           PM         20.00         0.71         95.12         20.00         0.49         68.47         20.00		PM	100.00	0.58	101.42	100.00	0.49	96.93	100.00	4.24	8.20
Cracking         MR         100.00         0.72         115.98         100.00         0.58         133.61         100.00         5.73         11.28           HR         100.00         0.73         135.90         100.00         0.65         159.49         100.00         6.06         11.90           Longitudinal Cracking         PM         500.00         0.52         116.51         500.00         0.53         90.24         500.00         0.44         69.52           Longitudinal Cracking         LR         500.00         0.67         146.86         500.00         0.54         104.52         500.00         0.51         81.25           MR         500.00         0.67         146.86         500.00         0.59         146.45         500.00         0.51         81.25           HR         500.00         0.71         153.66         500.00         0.59         146.45         500.00         0.58         84.37           PM         20.00         0.71         95.12         20.00         0.49         68.47         20.00         0.88         20.33           Transverse Cracking         LR         20.00         1.11         109.50         20.00         0.54         68.87	Alligator	LR	100.00	0.62	104.61	100.00	0.53	113.11	100.00	5.10	9.67
HR         100.00         0.73         135.90         100.00         0.65         159.49         100.00         6.06         11.90           Longitudinal Cracking         PM         500.00         0.52         116.51         500.00         0.53         90.24         500.00         0.44         69.52           Longitudinal Cracking         LR         500.00         0.60         133.63         500.00         0.54         104.52         500.00         0.50         71.55           MR         500.00         0.67         146.86         500.00         0.56         123.32         500.00         0.51         81.25           HR         500.00         0.71         153.66         500.00         0.59         146.45         500.00         0.58         84.37           PM         20.00         0.71         95.12         20.00         0.49         68.47         20.00         0.88         20.33           Transverse Cracking         LR         20.00         1.11         109.50         20.00         0.54         68.87         20.00         0.92         21.07	Cracking	MR	100.00	0.72	115.98	100.00	0.58	133.61	100.00	5.73	11.28
PM         500.00         0.52         116.51         500.00         0.53         90.24         500.00         0.44         69.52           Longitudinal Cracking         LR         500.00         0.60         133.63         500.00         0.54         104.52         500.00         0.50         71.55           MR         500.00         0.67         146.86         500.00         0.56         123.32         500.00         0.51         81.25           HR         500.00         0.71         153.66         500.00         0.59         146.45         500.00         0.58         84.37           PM         20.00         0.71         95.12         20.00         0.49         68.47         20.00         0.88         20.33           Transverse Cracking         LR         20.00         1.11         109.50         20.00         0.54         68.87         20.00         0.92         21.07		HR	100.00	0.73	135.90	100.00	0.65	159.49	100.00	6.06	11.90
Longitudinal Cracking         LR         500.00         0.60         133.63         500.00         0.54         104.52         500.00         0.50         71.55           MR         500.00         0.67         146.86         500.00         0.56         123.32         500.00         0.51         81.25           HR         500.00         0.71         153.66         500.00         0.59         146.45         500.00         0.58         84.37           PM         20.00         0.71         95.12         20.00         0.49         68.47         20.00         0.88         20.33           Transverse Cracking         LR         20.00         1.11         109.50         20.00         0.54         68.87         20.00         0.92         21.07		PM	500.00	0.52	116.51	500.00	0.53	90.24	500.00	0.44	69.52
Cracking         MR         500.00         0.67         146.86         500.00         0.56         123.32         500.00         0.51         81.25           HR         500.00         0.71         153.66         500.00         0.59         146.45         500.00         0.58         84.37           PM         20.00         0.71         95.12         20.00         0.49         68.47         20.00         0.88         20.33           Transverse Cracking         LR         20.00         1.11         109.50         20.00         0.54         68.87         20.00         0.92         21.07	Longitudinal	LR	500.00	0.60	133.63	500.00	0.54	104.52	500.00	0.50	71.55
HR         500.00         0.71         153.66         500.00         0.59         146.45         500.00         0.58         84.37           PM         20.00         0.71         95.12         20.00         0.49         68.47         20.00         0.88         20.33           Transverse Cracking         LR         20.00         1.11         109.50         20.00         0.54         68.87         20.00         0.92         21.07	Cracking	MR	500.00	0.67	146.86	500.00	0.56	123.32	500.00	0.51	81.25
PM         20.00         0.71         95.12         20.00         0.49         68.47         20.00         0.88         20.33           Transverse Cracking         LR         20.00         1.11         109.50         20.00         0.54         68.87         20.00         0.92         21.07		HR	500.00	0.71	153.66	500.00	0.59	146.45	500.00	0.58	84.37
Transverse         LR         20.00         1.11         109.50         20.00         0.54         68.87         20.00         0.92         21.07           Cracking         LR         LR <td></td> <td>PM</td> <td>20.00</td> <td>0.71</td> <td>95.12</td> <td>20.00</td> <td>0.49</td> <td>68.47</td> <td>20.00</td> <td>0.88</td> <td>20.33</td>		PM	20.00	0.71	95.12	20.00	0.49	68.47	20.00	0.88	20.33
Cracking	Transverse	LR	20.00	1.11	109.50	20.00	0.54	68.87	20.00	0.92	21.07
MR 20.00 1.52 125.33 20.00 0.55 77.01 20.00 0.99 22.61	Cracking	MR	20.00	1.52	125.33	20.00	0.55	77.01	20.00	0.99	22.61
HR 20.00 1.95 143.04 20.00 0.61 78.23 20.00 1.09 25.68		HR	20.00	1.95	143.04	20.00	0.61	78.23	20.00	1.09	25.68
PM 100.00 0.38 101.23 100.00 0.64 49.65 100.00 0.52 87.67		PM	100.00	0.38	101.23	100.00	0.64	49.65	100.00	0.52	87.67
LR 100.00 0.41 105.68 100.00 0.65 53.60 100.00 0.52 100.95	Patching	LR	100.00	0.41	105.68	100.00	0.65	53.60	100.00	0.52	100.95
MR 100.00 0.48 119.25 100.00 0.65 57.65 100.00 0.53 115.41		MR	100.00	0.48	119.25	100.00	0.65	57.65	100.00	0.53	115.41
HR 100.00 0.50 119.67 100.00 0.78 61.64 100.00 0.54 131.59		HR	100.00	0.50	119.67	100.00	0.78	61.64	100.00	0.54	131.59
PM 100.00 2.27 8.69 100.00 2.09 9.74 100.00 3.68 8.45		PM	100.00	2 27	8 69	100.00	2.09	9 74	100.00	3.68	8 45
I.R         100.00         2.27         0.05         100.00         2.05         5.74         100.00         5.08         0.45           I.R         100.00         4.46         10.48         100.00         2.41         10.16         100.00         6.47         11.14		IR	100.00	4.46	10.48	100.00	2.05	10.16	100.00	6.47	11 1/
Ride Score         LK         100.00 $4.96$ 10.00 $2.41$ 10.10         100.00 $0.47$ 11.14           MP         100.00         4.96         14.69         100.00         2.47         14.06         100.00         8.82         12.02	Ride Score	MD	100.00	4.96	14.60	100.00	2.41	14.06	100.00	Q 02	12.02
INIX         100.00         4.70         14.07         100.00         2.47         14.90         100.00         8.65         12.95           HR         100.00         42.52         18.71         100.00         44.12         19.52         100.00         47.08         18.53		HR	100.00	42 52	14.09	100.00	2.47 44.12	19.50	100.00	47.08	12.95

Calibrated model coefficients for Zone 1-pavement family A

		Low Traffic		М	edium Trat	ffic	High Traffic			
Distress Type	Treatment Type	α	β	Α	α	β	Α	α	β	Α
	PM	100.00	0.39	90.81	100.00	0.73	51.56	100.00	0.30	99.51
Shallow	LR	100.00	0.41	106.60	100.00	0.74	56.02	100.00	0.33	103.93
Rutting	MR	100.00	0.43	127.73	100.00	0.75	60.38	100.00	0.38	115.99
	HR	100.00	0.46	130.80	100.00	0.76	64.74	100.00	0.39	137.75
	PM	100.00	0.60	101.99	100.00	0.73	82.60	100.00	0.51	101.42
Deep	LR	100.00	0.67	121.58	100.00	0.86	91.14	100.00	0.58	120.33
Rutting	MR	100.00	0.78	124.74	100.00	0.98	96.09	100.00	0.68	122.26
	HR	100.00	0.94	131.24	100.00	1.08	97.65	100.00	0.83	127.33
	PM	20.00	0.42	118.33	20.00	0.68	97.50	20.00	0.57	109.25
Failures	LR	20.00	0.62	129.27	20.00	0.72	98.24	20.00	1.18	126.57
1 anures	MR	20.00	0.66	153.80	20.00	0.79	102.39	20.00	1.71	144.27
	HR	20.00	0.89	167.58	20.00	0.90	110.55	20.00	2.12	160.90
	PM	100.00	0.63	118.81	100.00	3.89	50.61	100.00	7.79	25.39
Block	LR	100.00	0.80	133.78	100.00	4.21	55.19	100.00	9.31	26.85
Cracking	MR	100.00	0.90	140.54	100.00	4.58	59.86	100.00	9.62	29.82
	HR	100.00	1.18	165.32	100.00	4.99	65.57	100.00	10.32	34.55
	PM	100.00	0.46	74.29	100.00	0.54	53.38	100.00	3.34	9.15
Alligator	LR	100.00	0.53	78.08	100.00	0.56	58.71	100.00	3.64	9.28
Cracking	MR	100.00	0.57	93.06	100.00	0.59	66.42	100.00	4.03	9.49
	HR	100.00	0.57	104.61	100.00	0.63	75.32	100.00	4.56	9.71
	PM	500.00	0.57	25.48	500.00	0.49	67.22	500.00	0.54	72.19
Longitudinal	LR	500.00	0.62	27.71	500.00	0.58	78.01	500.00	0.61	74.44
Cracking	MR	500.00	0.71	33.43	500.00	0.74	80.44	500.00	0.64	85.46
	HR	500.00	0.73	34.89	500.00	0.74	87.33	500.00	0.75	91.01
	PM	20.00	1.58	6.58	20.00	0.29	107.15	20.00	6.98	6.29
Transverse	LR	20.00	1.81	7.59	20.00	0.32	116.81	20.00	7.87	6.95
Cracking	MR	20.00	1.92	8.34	20.00	0.33	118.06	20.00	8.78	7.89
	HR	20.00	2.25	9.50	20.00	0.38	133.00	20.00	9.69	9.66
Patching	PM	100.00	0.36	55.57	100.00	0.59	77.35	100.00	1.08	10.30
	LR	100.00	0.38	63.16	100.00	0.68	82.08	100.00	1.27	11.72
	MR	100.00	0.41	74.20	100.00	0.75	82.76	100.00	1.46	13.35
	HR	100.00	0.47	75.09	100.00	0.78	95.87	100.00	1.62	14.48
	PM	100.00	5.28	7.46	100.00	3.50	8.67	100.00	2.25	6.96
Ride Score	LR	100.00	5.67	9.56	100.00	6.24	11.13	100.00	2.53	7.39
	MR	100.00	6.31	14.94	100.00	7.89	12.05	100.00	3.02	7.77
	HR	100.00	17.19	19.80	100.00	42.69	17.67	100.00	3.23	8.28

### Calibrated model coefficients for Zone 1-pavement family B

		I	Low Traffi	с	Medium Traffic			High Traffic		
Distress Type	Treatment Type	α	β	Α	α	β	Α	α	β	Α
	PM	100.00	0.30	111.93						
Shallow	LR	100.00	0.35	125.82						
Rutting	MR	100.00	0.38	134.17						
	HR	100.00	0.39	134.69						
	PM	100.00	0.51	97.89						
Deep	LR	100.00	0.54	99.55						
Rutting	MR	100.00	0.61	106.95						
	HR	100.00	0.71	119.97						
	PM	20.00	0.60	85.56						
Failures	LR	20.00	0.72	96.57						
1 anares	MR	20.00	0.85	107.31						
	HR	20.00	0.99	116.75						
	PM	100.00	5.51	112.31			,	nts)		
Block Cracking	LR	100.00	6.28	113.75			;	ticie.		
	MR	100.00	7.34	119.19			ء ۲			
	HR	100.00	8.79	127.92			ļ	HIC (		
	PM	100.00	0.76	48.31			E			
Alligator	LR	100.00	0.91	50.79				MO		
Cracking	MR	100.00	1.07	52.81				Jse I		
	HR	100.00	1.23	53.91			e e e e e e e e e e e e e e e e e e e	ta ( <b>1</b>		
	PM	500.00	0.64	84.90				t Da		
Longitudinal	LR	500.00	0.77	94.96				cien		
Cracking	MR	500.00	0.90	104.07			ę			
	HR	500.00	1.03	111.74			,	Ï		
	PM	20.00	9.15	58.53						
Transverse	LR	20.00	10.19	60.41						
Cracking	MR	20.00	10.63	69.24						
	HR	20.00	12.48	74.90						
	PM	100.00	0.41	69.14						
Patching	LR	100.00	0.46	70.51						
5	MR	100.00	0.47	80.20						
	HR	100.00	0.54	83.32						
	PM	100.00	2.16	9.14						
Ride Score	LR	100.00	5.50	11.60						
	MR	100.00	8.52	13.89						
	HR	100.00	10.13	19.47						

### Calibrated model coefficients for Zone 1-pavement family C

		Low Traffic			Medium Traffic			High Traffic		
Distress Type	Treatment Type	α	β	Α	α	β	Α	α	β	Α
	РМ	100.00	0.42	110.20	100.00	0.50	91.77	100.00	0.52	71.62
Shallow	LR	100.00	0.47	121.74	100.00	0.52	107.61	100.00	0.58	74.26
Rutting	MR	100.00	0.50	125.66	100.00	0.55	129.57	100.00	0.61	85.16
	HR	100.00	0.59	145.28	100.00	0.59	132.43	100.00	0.71	90.54
	РМ	100.00	0.62	85.47	100.00	0.70	76.20	100.00	0.89	44.97
Deep Rutting	LR	100.00	0.75	95.17	100.00	0.83	83.33	100.00	1.05	46.10
Deep Rutting	MR	100.00	0.89	104.45	100.00	0.88	89.09	100.00	1.18	54.08
	HR	100.00	1.03	112.31	100.00	1.53	93.10	100.00	1.28	61.40
	PM	20.00	0.87	21.95	20.00	0.55	111.45	20.00	0.78	69.14
Failures	LR	20.00	0.91	23.32	20.00	0.63	122.81	20.00	0.86	82.97
T anares	MR	20.00	1.00	25.56	20.00	0.66	126.71	20.00	1.02	90.45
	HR	20.00	1.12	29.47	20.00	0.78	145.99	20.00	1.10	105.81
	РМ	100.00	0.57	97.50	100.00	0.54	89.19	100.00	0.88	85.46
Block	LR	100.00	0.60	113.66	100.00	0.55	102.78	100.00	1.04	94.11
Cracking	MR	100.00	0.64	131.51	100.00	0.57	119.77	100.00	1.20	101.08
	HR	100.00	0.66	151.23	100.00	0.58	139.97	100.00	1.34	105.18
	РМ	100.00	0.49	68.28	100.00	0.54	35.51	100.00	0.95	19.85
Alligator	LR	100.00	0.55	68.53	100.00	0.62	42.29	100.00	0.99	20.93
Cracking	MR	100.00	0.56	76.35	100.00	0.66	46.25	100.00	1.05	22.33
	HR	100.00	0.62	76.19	100.00	0.78	47.48	100.00	1.13	23.74
	PM	500.00	0.65	41.91	500.00	0.39	75.34	500.00	0.47	115.36
Longitudinal	LR	500.00	0.76	42.71	500.00	0.45	79.93	500.00	0.54	131.06
Cracking	MR	500.00	0.85	50.70	500.00	0.50	80.72	500.00	0.60	142.35
	HR	500.00	0.91	57.23	500.00	0.52	93.19	500.00	0.63	146.90
	PM	20.00	0.66	50.51	20.00	0.51	68.85	20.00	0.63	60.35
Transverse	LR	20.00	0.67	54.85	20.00	1.21	81.97	20.00	0.67	65.17
Cracking	MR	20.00	0.67	59.12	20.00	1.38	86.76	20.00	0.69	69.94
	HR	20.00	0.68	63.36	20.00	1.95	98.37	20.00	0.69	74.61
	PM	100.00	0.58	54.80	100.00	0.42	110.20	100.00	0.60	67.13
Datahina	LR	100.00	0.61	61.13	100.00	0.47	121.74	100.00	0.66	79.75
T atening	MR	100.00	0.64	69.17	100.00	0.50	125.66	100.00	0.79	86.73
	HR	100.00	0.70	80.26	100.00	0.59	145.28	100.00	0.85	101.63
	РМ	100.00	5.35	7.53	100.00	42.24	6.19	100.00	25.01	6.36
Ride Score	LR	100.00	5.78	11.51	100.00	43.80	8.47	100.00	34.52	8.65
	MR	100.00	7.94	13.56	100.00	49.03	11.94	100.00	37.72	10.67
	HR	100.00	42.65	17.26	100.00	49.50	13.86	100.00	45.51	18.06

### Calibrated model coefficients for Zone 2-pavement family A
			Low Traffi	c	Me	edium Tra	ffic	High Traffic			
Distress Type	Treatment Type	α	β	Α	α	β	Α	α	β	Α	
	PM	100.00	0.49	93.49	100.00	0.74	46.21				
Shallow	LR	100.00	0.51	110.67	100.00	1.01	53.71				
Rutting	MR	100.00	0.55	112.98	100.00	1.09	57.91				
	HR	100.00	0.61	118.76	100.00	1.40	68.24				
	PM	100.00	0.82	55.66	100.00	0.59	118.61				
Deen Putting	LR	100.00	0.84	61.69	100.00	0.69	137.57				
Deep Rutting	MR	100.00	0.88	69.12	100.00	0.78	153.66				
	HR	100.00	0.94	78.38	100.00	0.85	164.70				
	PM	20.00	2.87	10.68	20.00	1.22	19.56				
Failures	LR	20.00	3.20	11.67	20.00	1.25	20.57				
Failules	MR	20.00	3.75	13.25	20.00	1.29	21.63				
	HR	20.00	3.86	15.73	20.00	1.33	22.69		<b>S</b> )		
	PM	100.00	4.58	37.62	100.00	4.64	34.94		ient		
Block	LR	100.00	5.44	44.08	100.00	5.43	39.55		α β Insufficient Data (use Medium Traffic Coefficients)		
Cracking	MR	100.00	5.88	46.13	100.00	5.69	40.32		c Co		
	HR	100.00	6.93	52.43	100.00	6.41	43.43		affic		
	PM	100.00	0.74	53.56	100.00	0.73	39.14		n Tr		
Alligator	LR	100.00	0.76	59.13	100.00	0.83	46.76		diun		
Cracking	MR	100.00	0.79	65.12	100.00	0.90	52.78		Me		
	HR	100.00	0.82	72.21	100.00	0.92	56.47		α     β       A   Insufficient Data (use Medium Traffic Coefficients)		
	PM	500.00	0.28	111.35	500.00	0.37	A       α       β         46.21       53.71         53.71       57.91         68.24       118.61         137.57       153.66         164.70       19.56         20.57       21.63         22.69       34.94         39.55       40.32         43.43       39.14         46.76       52.78         56.47       86.61         99.37       113.92         131.58       16.22         16.46       16.62         17.79       94.44         111.07       111.41         114.06       7.72         11.60       13.65         17.39       9				
Longitudinal	LR	500.00	0.32	124.55	500.00	0.37	99.37		β Insufficient Data (use Medium Traffic Coefficients)		
Cracking	MR	500.00	0.34	132.67	500.00	0.38	113.92				
	HR	500.00	0.35	159.94	500.00	0.39	1.29       21.63         1.33       22.69         4.64       34.94         5.43       39.55         5.69       40.32         6.41       43.43         0.73       39.14         0.83       46.76         0.90       52.78         0.92       56.47         0.37       86.61         0.37       99.37         0.38       113.92         0.39       131.58         0.79       16.22         0.81       16.46         0.84       16.62				
	PM	20.00	1.08	22.90	20.00	0.79	16.22		-		
Transverse	LR	20.00	1.14	24.49	20.00	0.81	16.46				
Cracking	MR	20.00	1.23	0.74       33.30       100.00       0.73       39.14         0.76       59.13       100.00       0.83       46.76         0.79       65.12       100.00       0.90       52.78         0.82       72.21       100.00       0.92       56.47         0.28       111.35       500.00       0.37       86.61         0.32       124.55       500.00       0.37       99.37         0.34       132.67       500.00       0.39       131.58         1.08       22.90       20.00       0.81       16.46         1.23       26.20       20.00       0.89       17.79         0.34       102.28       100.00       0.79       94.44							
	HR	20.00	1.36	28.91	20.00	00       0.90       52.78         00       0.92       56.47         00       0.37       86.61         00       0.37       99.37         00       0.38       113.92         00       0.39       131.58         00       0.79       16.22         00       0.84       16.46         00       0.84       16.62         00       0.71       94.44         00       0.74       111.07					
-	PM	100.00	0.28         111.35         500.00         0.37         86.61           0.32         124.55         500.00         0.37         99.37           0.34         132.67         500.00         0.38         113.92           0.35         159.94         500.00         0.39         131.58           1.08         22.90         20.00         0.79         16.22           1.14         24.49         20.00         0.81         16.46           1.23         26.20         20.00         0.89         17.79           0.34         102.28         100.00         0.71         94.44           0.37         107.66         100.00         0.78         111.41           0.43         123.83         100.00         0.78         111.41           0.46         127.92         100.00         0.85         114.06								
Patching	LR	100.00	0.37	107.66	100.00	0.74	111.07		Insufficient Data (use Medium Traffic Coefficients)		
1 atening	MR	100.00	0.43	123.83	100.00	0.78	111.41		Insufficient Data (use Medium Traffic Coefficients)		
	HR	100.00	0.46	127.92	100.00	0.85	114.06				
	РМ	100.00	18.25	6.38	100.00	6.32	7.72		α β Insufficient Data (use Medium Traffic Coefficients)		
Ride Score	LR	100.00	20.03	7.52	100.00	6.81	11.60		High Traf		
itide Score	MR	100.00	21.16	9.67	100.00	9.02	13.65				
	HR	100.00	21.82	13.26	100.00	43.72	17.39				

#### Calibrated model coefficients for Zone 2-pavement family B

		1	Low Traffi	c	М	edium Tra	ffic	E	ligh Traf	fic
Distress Type	Treatment Type	α	β	A	α	β	Α	α	β	А
	PM	100.00	0.58	49.93	100.00	0.46	96.74			
Shallow	LR	100.00	0.59	53.87	100.00	0.49	98.00			
Rutting	MR	100.00	0.60	58.23	100.00	0.54	104.16			
	HR	100.00	0.60	62.57	100.00	0.63	115.82			
	PM	100.00	0.60	90.24	100.00	0.65	103.52			
Deep	LR	100.00	0.60	101.52	100.00	0.71	108.86			
Rutting	MR	100.00	0.80	112.77	100.00	0.82	122.33			
	HR	100.00	1.01	123.06	100.00	0.86	145.53			
	PM	20.00	0.78	100.18	20.00	4.36	90.05			
Failures	LR	20.00	0.84	101.50	20.00	4.70	104.11			
Failures	MR	20.00	0.93	108.45	20.00	5.11	121.38			
	HR	20.00	1.08	120.54	20.00	5.59	141.92		<b>s</b> )	
	PM	100.00	3.17	42.00	100.00	9.87	33.50		ient	
Block	LR	100.00	3.38	44.69	100.00	11.39	34.21		effic	
Cracking	MR	100.00	3.61	48.17	100.00	12.65	39.69		Co	
	HR	100.00	3.87	51.67	100.00	13.49	44.76		affic	
	РМ	100.00	0.62	65.51	100.00	0.47	92.92		Ľ.	
Alligator	LR	100.00	0.67	77.95	100.00	0.49	110.43		lium	
Cracking	MR	100.00	0.79	82.99	100.00	0.52	111.54		Mee	
	HR	100.00	0.83	94.98	100.00	0.58	116.91		(use	
	PM	500.00	0.48	117.56	500.00	0.48	105.14		ata	
Longitudinal	LR	500.00	0.56	136.53	500.00	0.53	112.14		nt D	
Cracking	MR	500.00	0.63	152.26	500.00	0.63	129.81		licie	
	HR	500.00	0.68	162.75	500.00	0.69	137.24		suff	
	PM	20.00	0.84	49.84	20.00	0.77	111.83		<b>P</b>	
Transverse	LR	20.00	0.84	53.07	20.00	0.86	122.68			
Cracking	MR	20.00	1.00	55.46	20.00	0.90	124.05			
	HR	20.00	1.16	56.55	20.00	1.03	138.96			
	PM	100.00	1.16	28.63	100.00	0.37	101.70			
Datching	LR	100.00	1.25	31.85	100.00	0.44	120.93			
1 atening	MR	100.00	1.41	36.46	100.00	0.54	122.24			
	HR	100.00	1.67	36.09	100.00	0.68	125.78			
	Iransverse     LR       Cracking     MR       HR     HR       Patching     LR       MR     HR       PM     LR       PM     LR	100.00	8.04	6.50	100.00	6.66	5.91			
Ride Score	LR	100.00	8.27	7.80	100.00	8.00	8.73			
Riue Scole	MR	100.00	8.43	10.35	100.00	11.71	11.19			
	HR	100.00	11.11	12.49	100.00	29.15	19.68			

### Calibrated model coefficients for Zone 2-pavement family C

		L	ow Traff	ic	Me	dium Tra	offic	Н	ligh Traff	ïc
Distress Type	Treatment Type	α	β	Α	α	β	Α	α	β	Α
	PM	100.00	0.60	38.00	100.00	0.72	49.36	100.00	0.39	93.20
Shallow	LR	100.00	0.69	45.74	100.00	0.72	52.28	100.00	0.41	111.05
Rutting	MR	100.00	0.75	51.83	100.00	0.86	54.69	100.00	0.45	113.92
	HR	100.00	0.76	55.28	100.00	1.01	57.32	100.00	0.50	121.25
	PM	100.00	0.60	38.00	100.00	0.66	93.30	100.00	1.47	19.47
Deep	LR	100.00	0.69	45.74	100.00	0.68	109.59	100.00	1.50	19.24
Rutting	MR	100.00	0.75	51.83	100.00	0.72	131.53	100.00	1.50	22.99
	HR	100.00	0.76	55.28	100.00	0.78	134.19	100.00	1.79	27.66
	PM	20.00	0.95	45.35	20.00	0.68	87.47	20.00	9.56	100.94
Failures	LR	20.00	1.11	46.06	20.00	0.69	98.27	20.00	10.69	110.36
Tanuics	MR	20.00	1.25	53.97	20.00	0.82	110.18	20.00	11.17	112.24
	HR	20.00	1.35	61.19	20.00	0.97	122.22	20.00	13.09	128.18
	PM	100.00	0.91	52.14	100.00	6.17	57.67	100.00	7.31	14.32
Block	LR	100.00	0.92	55.67	100.00	6.34	69.79	100.00	8.45	14.39
Cracking	MR	100.00	0.92	59.56	100.00	7.18	77.09	100.00	9.86	14.54
	HR	100.00	1.10	63.36	100.00	7.46	77.46	100.00	11.59	15.69
	PM	100.00	0.60	94.44	100.00	0.50	95.69	100.00	0.70	73.43
Alligator	LR	100.00	0.63	111.68	100.00	0.53	96.07	100.00	0.79	75.55
Cracking	MR	100.00	0.67	113.84	100.00	0.58	100.16	100.00	0.83	87.17
	HR	100.00	0.74	119.43	100.00	0.66	108.68	100.00	0.96	92.43
	PM	500.00	0.39	84.13	500.00	0.44	57.29	500.00	0.30	70.76
Longitudinal	LR	500.00	0.47	94.78	500.00	0.46	64.57	500.00	0.33	74.03
Cracking	MR	500.00	0.56	106.02	500.00	0.51	76.98	500.00	0.34	86.91
	HR	500.00	0.66	117.05	500.00	0.58	79.33	500.00	0.40	95.59
	PM	20.00	0.41	84.04	20.00	0.55	33.12	20.00	0.32	113.93
Transverse	LR	20.00	0.49	94.64	20.00	0.62	38.69	20.00	0.37	129.94
Cracking	MR	20.00	0.58	105.72	20.00	0.64	42.05	20.00	0.41	141.41
	HR	20.00	0.68	116.56	20.00	0.74	49.59	20.00	0.43	146.17
	PM	100.00	0.55	93.11	100.00	0.59	60.92	100.00	0.58	97.59
Patching	LR	100.00	0.59	96.04	100.00	0.63	70.20	100.00	0.62	98.90
i utoning	MR	100.00	1.12	106.52	100.00	0.71	70.67	100.00	0.69	104.70
	HR	100.00	2.26	126.90	100.00	0.84	75.60	100.00	0.79	116.03
	PM	100.00	3.78	8.73	100.00	13.47	8.01	100.00	3.15	9.42
Ride Score	LR	100.00	6.97	10.94	100.00	14.48	9.55	100.00	3.19	11.60
	MR	100.00	7.55	15.56	100.00	21.45	12.59	100.00	5.76	13.75
	HR	100.00	28.32	17.37	100.00	41.38	15.02	100.00	33.18	17.38

#### Calibrated model coefficients for Zone 3-pavement family A

		L	ow Traff	ic	Me	dium Tra	ffic	Н	igh Traff	ic
Distress Type	Treatment Type	α	β	Α	α	β	Α	α	β	Α
	PM	100.00	0.56	49.36	100.00	0.57	76.78	100.00	0.51	87.86
Shallow	LR	100.00	0.57	52.75	100.00	0.65	81.89	100.00	0.52	101.12
Rutting	MR	100.00	0.57	57.01	100.00	0.72	82.44	100.00	0.52	115.75
	HR	100.00	0.57	60.89	100.00	0.74	93.67	100.00	0.53	133.15
	PM	100.00	0.56	49.36	100.00	0.76	76.78	100.00	0.92	51.94
Deep	LR	100.00	0.57	52.75	100.00	0.87	81.03	100.00	0.92	55.58
Rutting	MR	100.00	0.57	57.01	100.00	0.93	95.61	100.00	1.11	59.38
	HR	100.00	0.57	60.89	100.00	0.93	106.60	100.00	1.32	62.07
	PM	20.00	0.78	83.75	20.00	0.65	84.70	20.00	0.71	80.98
Failures	LR	20.00	0.92	92.56	20.00	0.78	94.81	20.00	0.86	88.21
Failures	MR	20.00	1.06	99.13	20.00	0.90	103.75	20.00	1.67	92.33
	HR	20.00	1.17	101.83	20.00	1.03	111.23	20.00	2.42	92.55
	PM	100.00	5.92	91.20	100.00	6.49	47.84	100.00	2.83	93.88
Block	LR	100.00	6.00	95.02	100.00	6.87	54.13	100.00	3.25	98.62
Cracking	MR	100.00	6.64	108.23	100.00	7.75	63.40	100.00	3.40	113.26
	HR	100.00	6.66	111.74	100.00	9.23	64.24	100.00	3.87	117.22
	PM	100.00	0.58	84.99	100.00	0.51	104.29	100.00	0.65	97.12
Alligator	LR	100.00	0.69	95.36	100.00	0.56	110.31	100.00	0.69	97.17
Cracking	MR	100.00	0.81	104.94	100.00	0.66	126.22	100.00	0.75	101.11
	HR	100.00	0.94	114.17	100.00	0.71	130.35	100.00	0.86	109.48
	PM	500.00	0.31	72.86	500.00	0.39	91.01	500.00	0.47	54.04
Longitudinal	LR	500.00	0.35	77.01	500.00	0.40	106.77	500.00	0.49	60.22
Cracking	MR	500.00	0.38	91.16	500.00	0.42	107.08	500.00	0.52	68.45
	HR	500.00	0.39	102.18	500.00	0.46	109.77	500.00	0.57	79.80
	PM	20.00	0.79	8.48	20.00	0.31	66.46	20.00	1.50	20.04
Transverse	LR	20.00	1.04	9.98	20.00	0.34	66.58	20.00	1.53	20.29
Cracking	MR	20.00	1.28	11.90	20.00	0.35	74.21	20.00	1.65	20.07
	HR	20.00	1.50	13.83	20.00	0.39	74.97	20.00	1.76	21.27
	PM	100.00	2.55	9.44	100.00	0.81	65.89	100.00	0.51	69.04
Patching	LR	100.00	2.86	9.78	100.00	0.88	77.37	100.00	0.57	70.04
T utening	MR	100.00	3.41	11.48	100.00	1.01	80.31	100.00	0.58	78.29
	HR	100.00	3.62	11.18	100.00	1.04	89.06	100.00	0.65	79.75
	PM	100.00	21.50	6.55	100.00	3.93	8.73	100.00	1.74	9.72
Ride Score	LR	100.00	22.72	8.10	100.00	7.12	10.94	100.00	1.98	10.10
Rue Score	MR	100.00	25.27	9.90	100.00	7.69	11.38	100.00	4.40	14.70
	HR	100.00	29.49	14.21	100.00	42.48	17.31	100.00	40.79	19.14

#### Calibrated model coefficients for Zone 3-pavement family B

		L	ow Traff	ic	Me	dium Tra	offic	Н	ligh Traf	fic
Distress Type	Treatment Type	α	β	Α	α	β	Α	α	β	Α
	PM	100.00	0.47	92.92	100.00	0.42	116.22			
Shallow	LR	100.00	0.49	110.43	100.00	0.49	133.09			
Rutting	MR	100.00	0.52	111.54	100.00	0.55	147.01			
	HR	100.00	0.58	116.91	100.00	0.59	155.54			
	PM	100.00	0.60	89.57	100.00	0.97	40.67			
Deep	LR	100.00	0.61	103.70	100.00	1.11	48.60			
Rutting	MR	100.00	0.63	120.53	100.00	1.19	54.91			
	HR	100.00	0.64	140.51	100.00	1.20	57.54		ts)	
	PM	20.00	0.65	90.72	20.00	1.47	23.67		en	
Failuras	LR	20.00	0.67	105.15	20.00	1.52	25.05		ici	
Failures	MR	20.00	0.69	122.36	20.00	1.60	26.29		<b>F</b>	
	HR	20.00	0.71	142.82	20.00	1.69	27.52		, e	
	PM	100.00	2.55	35.71	100.00	0.60	91.96		<u> </u>	
Block	LR	100.00	2.69	38.13	100.00	0.62	107.20		H	
Cracking	MR	100.00	2.87	40.74	100.00	0.65	126.58		La	
-	HR	100.00	3.08	44.03	100.00	0.69	127.51		E	
	PM	100.00	0.58	84.99	100.00	0.49	87.29			
Alligator	LR	100.00	0.69	95.36	100.00	0.49	99.18		liu	
Cracking	MR	100.00	0.81	104.94	100.00	0.50	113.35		le	
	HR	100.00	0.94	114.17	100.00	0.50	129.52			
	PM	500.00	0.59	60.92	500.00	0.36	61.59		ISE	
Longitudinal	LR	500.00	0.63	70.20	500.00	0.39	72.32			
Cracking	MR	500.00	0.71	70.67	500.00	0.45	75.19		ata	
	HR	500.00	0.84	75.60	500.00	0.46	83.94		Ä	
	PM	20.00	0.53	83.84	20.00	0.36	99.89		nt	
Transverse	LR	20.00	0.63	93.93	20.00	0.39	103.99		cie	
Cracking	MR	20.00	0.73	103.18	20.00	0.45	116.06		ĮĮ.	
-	HR	20.00	0.84	111.02	20.00	0.46	137.82		Sul	
	PM	100.00	0.51	104.29	100.00	0.37	86.61		<b>I</b>	
Datahing	LR	100.00	0.56	110.31	100.00	0.37	99.37			
Patching	MR	100.00	0.66	126.22	100.00	0.38	113.92			
	HR	100.00	0.71	130.35	100.00	0.39	131.58			
	PM	100.00	2.31	9.63	100.00	5.34	8.81			
Dida Carro	LR	100.00	5.06	11.95	100.00	6.57	11.40			
Kide Score	MR	100.00	8.36	15.96	100.00	7.23	14.65			
	HR	100.00	26.41	17.46	100.00	7.79	18.30			

#### Calibrated model coefficients for Zone 3-pavement family C

		1	Low Traffi	c	M	edium Tra	ffic	I	<u>ligh Traffi</u>	c
Distress Type	Treatment Type	α	β	Α	α	β	Α	α	β	А
	PM	100.00	0.43	95.69	100.00	0.47	92.92	100.00	0.55	94.44
Shallow	LR	100.00	0.46	96.07	100.00	0.49	110.43	100.00	0.58	111.97
Rutting	MR	100.00	0.51	100.16	100.00	0.52	111.54	100.00	0.62	114.49
	HR	100.00	0.59	108.68	100.00	0.58	116.91	100.00	0.69	120.47
	PM	100.00	0.57	116.22	100.00	0.86	54.62	100.00	0.88	60.35
Deen Rutting	LR	100.00	0.74	126.95	100.00	0.88	60.15	100.00	0.92	65.17
Deep Rutting	MR	100.00	0.78	151.64	100.00	0.91	66.05	100.00	0.94	69.94
	HR	100.00	0.98	166.84	100.00	0.94	73.03	100.00	0.94	74.61
	РМ	20.00	0.63	90.15	20.00	0.77	60.53	20.00	4.54	102.37
Failures	LR	20.00	0.64	103.93	20.00	0.81	69.42	20.00	5.11	102.51
Fanales	MR	20.00	0.66	120.95	20.00	0.90	81.88	20.00	5.94	107.28
	HR	20.00	0.68	141.16	20.00	1.03	84.21	20.00	7.12	115.03
	РМ	100.00	3.46	19.85	100.00	1.32	22.04	100.00	6.71	93.11
Block	LR	100.00	3.94	21.92	100.00	1.37	22.78	100.00	8.00	93.95
Cracking	MR	100.00	3.98	25.31	100.00	1.43	24.21	100.00	8.38	100.35
	HR	100.00	4.29	25.89	100.00	1.51	25.45	100.00	9.26	112.37
	PM	100.00	0.61	56.90	100.00	0.58	50.13	100.00	1.20	17.56
Alligator	LR	100.00	0.64	63.85	100.00	0.58	53.97	100.00	1.22	18.31
Cracking	MR	100.00	0.69	74.32	100.00	0.59	58.41	100.00	1.23	18.18
	HR	100.00	0.77	88.47	100.00	0.60	62.86	100.00	1.33	18.05
	PM	500.00	0.47	70.47	500.00	0.33	93.68	500.00	0.47	86.52
Longitudinal	LR	500.00	0.53	71.91	500.00	0.34	112.74	500.00	0.47	98.81
Cracking	MR	500.00	0.55	81.85	500.00	0.38	117.63	500.00	0.47	112.61
	HR	500.00	0.63	86.34	500.00	0.43	128.00	500.00	0.47	128.33
	PM	20.00	1.37	20.99	20.00	0.79	34.85	20.00	1.20	27.59
Transverse	LR	20.00	1.41	21.59	20.00	0.85	41.99	20.00	1.28	30.55
Cracking	MR	20.00	1.45	22.62	20.00	1.43	47.89	20.00	1.43	34.93
	HR	20.00	1.49	23.81	20.00	1.89	52.75	20.00	1.66	41.19
	PM	100.00	0.34	61.02	100.00	0.35	78.21	100.00	0.53	61.40
Patching	LR	100.00	0.36	71.17	100.00	0.41	85.05	100.00	0.57	70.64
T atoming	MR	100.00	0.42	73.91	100.00	0.46	89.16	100.00	0.64	72.63
	HR	100.00	0.43	82.53	100.00	0.51	89.88	100.00	0.77	79.45
	РМ	100.00	11.03	6.69	100.00	18.25	6.38	100.00	29.23	7.89
Ride Score	LR	100.00	13.81	9.89	100.00	20.03	7.52	100.00	32.47	9.78
	MR	100.00	20.72	12.29	100.00	21.16	9.67	100.00	36.73	10.63
	HR	100.00	34.06	19.63	100.00	21.82	13.26	100.00	49.18	12.48

#### Calibrated model coefficients for Zone 4-pavement family A

_			Low Traffi	с	М	edium Tra	ffic	I	ligh Traf	fic
Distress Type	Treatment Type	α	β	Α	α	β	Α	α	β	Α
	PM	100.00	0.36	96.83	100.00	0.42	97.79			
Shallow	LR	100.00	0.38	98.63	100.00	0.45	100.03			
Rutting	MR	100.00	0.43	106.47	100.00	0.50	107.93			
	HR	100.00	0.51	119.87	100.00	0.60	123.21			
	PM	100.00	0.60	101.99	100.00	0.66	79.17			
Deen Rutting	LR	100.00	0.65	105.86	100.00	0.83	87.75			
Deep Rutting	MR	100.00	0.75	117.40	100.00	0.94	96.08			
	HR	100.00	0.77	137.53	100.00	0.98	102.67			
	PM	20.00	9.95	99.32	20.00	1.11	23.48			
Failures	LR	20.00	10.88	104.94	20.00	1.17	24.55			
Failures	MR	20.00	12.95	121.25	20.00	1.26	27.30			
	HR	20.00	14.05	127.01	20.00	1.40	30.05		<b>(s</b>	
	PM	100.00	9.31	97.21	100.00	0.71	46.78		ient	
Block	LR	100.00	10.33	104.85	100.00	0.84	49.16		effic	
Cracking	MR	100.00	10.64	105.51	100.00	0.98	50.18		c Co	
	HR	100.00	12.27	119.35	100.00	1.12	59.95		affic	
	PM	100.00	0.65	47.36	100.00	0.58	49.93		n Tr	
Alligator	LR	100.00	0.93	54.93	100.00	0.59	53.87		diun	
Cracking	MR	100.00	1.03	59.34	100.00	0.60	58.23		Me	
	HR	100.00	1.38	69.90	100.00	0.60	62.57		(use	
	PM	500.00	0.46	45.45	500.00	0.29	107.15		ata	
Longitudinal	LR	500.00	0.55	47.42	500.00	0.32	116.81		nt D	
Cracking	MR	500.00	0.65	48.67	500.00	0.33	118.06		α β Insufficient Data (use Medium Traffic Coefficients)	
	HR	500.00	0.75	50.03	α         β         A         α         β         A           100.00         0.42         97.79         100.03         100.00         0.45         100.03           100.00         0.50         107.93         100.00         0.66         79.17           100.00         0.66         79.17         100.00         0.83         87.75           100.00         0.94         96.08         102.67         20.00         1.11         23.48           20.00         1.26         27.30         20.00         1.40         30.05           100.00         0.84         49.16         100.00         0.58         49.93           100.00         0.59         53.87         100.00         0.54         49.93           100.00         0.60         58.23         100.00         0.32         116.81           500.00         0.32         116.81         500.00         0.33         118.06           500.00         0.33         118.06         50.06         20.00         1.05         98.42           100.00         0.54         80.58         20.00         0.75         96.06           20.00         0.503         11.84         100.00         <					
	PM	20.00	0.44	114.98	20.00	0.42	70.47		7	
Transverse	LR	20.00	0.50	130.98	20.00	0.54	80.58			
Cracking	MR	20.00	0.56	142.26	1111       11111       11111       11111					
	HR	20.00	0.59	146.80	20.00	1.05	98.42	23.48         24.55         27.30         30.05         46.78         49.16         50.18         59.95         49.93         53.87         58.23         62.57         107.15         116.81         118.06         133.00         70.47         80.58         96.06         98.42         10.30         11.84         13.58         15.99         9.07         10.19         14.33         19.86		
	PM	100.00	0.34	89.86	100.00	0.88	10.30			
Patching	LR	100.00	0.35	105.32	100.00	1.05	11.84		Insufficient Data (use Medium Traffic Coefficients)	
1 defining	MR	100.00	0.36	125.24	100.00	1.23	13.58			
	HR	100.00	0.39	126.92	100.00	1.40	15.99			
	PM	100.00	8.42	5.65	100.00	3.51	9.07	Insufficient Data (use Medium Traffic Coefficients)		
Ride Score	LR	100.00	10.24	8.51	100.00	3.90	10.19		High Traf	
	MR	100.00	12.87	13.97	100.00	5.03	14.33			
	HR	100.00	21.53	18.04	100.00	14.56	19.86			

#### Calibrated model coefficients for Zone 4-pavement family B

_		I	Low Traffi	с	M	edium Tra	ffic	E	ligh Traf	fic
Distress Type	Treatment Type	α	β	Α	α	β	Α	α	β	А
	PM	100.00	0.42	97.79	100.00	0.39	56.14			
Shallow	LR	100.00	0.45	100.03	100.00	0.41	63.30			
Rutting	MR	100.00	0.50	107.93	100.00	0.44	74.46			
	HR	100.00	0.60	123.21	100.00	0.51	75.50			
	PM	100.00	0.68	97.50	100.00	0.49	116.13			
Deep	LR	100.00	0.72	98.24	100.00	0.56	132.55			
Rutting	MR	100.00	0.79	102.39	100.00	0.63	145.77			
	HR	100.00	0.90	110.55	100.00	0.67	152.57			
	PM	20.00	0.59	70.95	20.00	0.42	100.84			
Failures	LR	20.00	0.67	72.62	20.00	0.83	113.32			
Failures	MR	20.00	0.68	82.87	20.00	1.00	122.16			
	HR	20.00	0.78	86.41	20.00	2.16	126.34		<b>S</b> )	
	PM	100.00	3.39	84.04	100.00	0.33	114.03		ient	
Block	LR	100.00	3.65	96.43	100.00	0.50	120.85		effic	
Cracking	MR	100.00	3.96	110.73	100.00	0.81	136.54		C	
	HR	100.00	4.34	129.03	100.00	0.90	163.92		affic	
	PM	100.00	0.65	55.86	100.00	0.28	111.35		Ŀ	
Alligator	LR	100.00	0.68	62.31	100.00	0.32	124.55		lim	
Cracking	MR	100.00	0.72	70.46	100.00	0.34	132.67		Me	
	HR	100.00	0.79	81.70	100.00	0.35	159.94		(use	
	PM	500.00	0.48	82.69	500.00	0.29	72.09		ata	
Longitudinal	LR	500.00	0.57	92.51	500.00	0.33	75.44		nt D	
Cracking	MR	500.00	0.66	101.42	500.00	0.36	88.61		icie	
	HR	500.00	0.75	107.54	500.00	0.36	99.25		ling	
	PM	20.00	5.71	16.32	20.00	1.76	23.96			
Transverse	LR	20.00	5.89	18.04	20.00	1.81	24.66			
Cracking	MR	20.00	6.75	19.05	20.00	1.85	25.50			
	HR	20.00	7.18	22.38	20.00	1.87	26.34			
	PM	100.00	0.39	71.42	100.00	0.32	40.19			
Datching	LR	100.00	0.46	76.60	100.00	0.37	41.03			
1 atoming	MR	100.00	1.05	80.33	100.00	0.42	48.60			
	HR	100.00	1.62	80.71	100.00	0.47	56.73			
	PM	100.00	15.22	7.08	100.00	11.03	6.69			
Ride Score	LR	100.00	18.40	9.57	100.00	13.81	9.89			
Rue Scole	MR	100.00	19.49	11.02	100.00	20.72	12.29			
	HR	100.00	33.49	19.17	100.00	34.06	19.63			

#### Calibrated model coefficients for Zone 4-pavement family C

## APPENDIX C CALIBRATED CRCP PERFORMANCE MODEL COEFFICIENTS

Zana	CDCD Distance	Re	-Calibrate	d Performan	ce Curve Coeffi	cients
Zone	CKCP Distress	α	β	ρ	R <sup>2</sup> -Median	R <sup>2</sup> -Quartile
	Spalled Cracks	15.729	2.323	13.602	0.766	0.181
Zona 1	Punchouts	44.211	20.854	17.801	1.000	0.787
Zone i	ACP Patches	9.8	45.3479	16.74	0.97253	0.2763
	PCC Patches	5.268	13.707	14.232	0.891	0.460
	Spalled Cracks	99.866	0.929	44.017	0.734	0.451
Zana 2	Punchouts	3.246	17.9479	14.72	0.95652	0.4215
Zone 2	ACP Patches	71.58	19.818	17.93	1	1
	PCC Patches	585.746	1.207	58.058	0.943	0.468
	Spalled Cracks	4.166	94.121	9.182	0.860	0.597
Zana 2	Punchouts	7.436	30.341	17.15	1	0.992
Zone 5	ACP Patches	1.8E-13	0.65692	1.21	-	0.0011
	PCC Patches	7.338	4.957	13.884	0.870	0.567
	Spalled Cracks	2.200	79.276	9.223	0.964	0.275
Zona 1	Punchouts	-	-	-	-	-
Zone 4	ACP Patches	-	-	-	-	-
	PCC Patches	56.507	1.278	29.925	0.961	0.663

#### Table J-1. Re-Calibration of CRCP Performance Curves for Zones.

# Table J-2. Re-Calibration of CRCP Performance Curves for Zones with Constrained Parameters.

Zana	CDCD Distances	Re	-Calibrate	d Performan	ce Curve Coeffic	cients
Zone	CKCP Distress	α	β	ρ	R <sup>2</sup> -Median	R <sup>2</sup> -Quartile
	Spalled Cracks	3.000	230.000	9.088	0.664	0.258
Zona 1	Punchouts	1.000	225.000	16.161	1.000	0.787
Zone i	ACP Patches	1.000	250.000	14.214	0.397	0.375
	PCC Patches	3.000	31.930	13.648	0.844	0.466
	Spalled Cracks	5.000	8.994	9.463	0.778	0.429
Zana 2	Punchouts	1.000	162.997	14.150	0.926	0.338
Zone 2	ACP Patches	1.000	250.000	16.132	1.000	1.000
	PCC Patches	2.000	163.899	12.187	0.712	0.395
	Spalled Cracks	2.000	200.000	9.084	0.860	0.599
7	Punchouts	1.000	250.000	16.145	1.000	0.992
Zone 5	ACP Patches	-	-	-	-	0.000
	PCC Patches	2.000	12.913	10.640	0.683	0.466
	Spalled Cracks	1.000	200.000	9.090	0.963	0.299
Zana 4	Punchouts	1.000	145.397	13.192	1.000	0.099
Zone 4	ACP Patches	-	-	-	-	-
	PCC Patches	3.000	11.805	9.691	0.760	0.484

APPENDIX D	CALIBRATED JCP PERFORMANCE MODELS COEFFICIENTS
------------	--

Please note that there were no JCP sections present in Zone 4 at the time of the analysis. If such pavements are constructed in Zone 4 in the future, the researchers recommend using the Zone 3 coefficients.

	2,3 2,3 2,3 FJC	PM PM PM Original	L M H Model	33 88.87 94.11 97.54 <b>37.02</b>	_	02 0.98 1.03 1.02 <b>5.21</b>	D2         0.98         1.03         1.02         5.21           5.2         8.99         7.66         5.98         7.95	D2         0.98         1.03         1.02         5.21           5.2         8.99         7.66         5.98         7.95           64         2818         2633         1566         7.95	D2         0.98         1.03         1.02         5.21           5.2         8.99         7.66         5.98         7.95           64         2818         2633         1566         7.95           5%         -9.7%         -9.0%         -18.9%         7.95	32     0.98     1.03     1.02     5.21       i.2     8.99     7.66     5.98     7.95       64     2818     2633     1566       8%     -9.7%     -9.0%     -18.9%	22         0.98         1.03         1.02         5.21           1.2         8.99         7.66         5.98         7.95           64         2818         2633         1566         7.95           5%         -9.7%         -9.0%         -18.9%         7.95           1         3         3         3         FL	22         0.98         1.03         1.02         5.21           1.2         8.99         7.66         5.98         7.95           64         2818         2633         1566         7.95           58         -9.7%         -9.0%         -18.9%         7.95           58         -9.7%         -9.0%         -18.9%         7.95           58         -9.7%         9.0%         -18.9%         7.95           59         -9.7%         9.0%         7.956         7.95           59         -9.7%         3.1566         7.95         7.95           59         -9.7%         3.1566         7.95         7.95           50         -9.7%         -9.0%         -18.9%         7.95           50         1         3         3         5           50         PM         PM         PM         Original	22         0.98         1.03         1.02         5.21           1.2         8.99         7.66         5.98         7.95           64         2818         2633         1566         7.95           1.5         -9.7%         -9.0%         -18.9%         7.95           1.5         -9.7%         -9.0%         -18.9%         7.95           1.5         -9.7%         9.0%         -18.9%         7.95           1.5         -9.7%         9.0%         -18.9%         7.95           1.5         -9.0%         -18.9%         -18.9%         1.0           1.5         -9.1%         -9.1%         -18.9%         1.0           1.5         -9.1%         -18.9%         -18.9%         1.0           1.5         -18.9%         -18.9%         -18.9%         1.0           1.5         -18.9%         -18.9%         -18.9%         -19.9%           1.5         -18.9%         -18.9%         -18.9%         -19.9%           1.5         -19.9%         -18.9%         -18.9%         -18.9%           1.5         -19.9%         -18.9%         -18.9%         -18.9%           1.5         -19.9% <t< th=""><th>22         0.98         1.03         1.02         5.21           6.2         8.99         7.66         5.98         7.95           6.4         2818         2633         1566         7.95           6.4         2818         2633         1566         7.95           6.4         2818         2633         1566         7.95           6.4         2818         2633         1566         7.95           6.9         -9.0%         -18.9%         7.95         7.95           7.9         -9.0%         -18.9%         7.95         7.95           7.9         -9.0%         -18.9%         7.95         7.95           7.9         -9.0%         -18.9%         7.95         7.95           7.9         -9.0%         -18.9%         7.96         7.95           7.9         -9.0%         -18.9%         7.97         7.95           9         -1         37.65         25         30         47.67</th><th>22         0.98         1.03         1.02         5.21           (12         8.99         7.66         5.98         7.95           64         2818         2633         1566         7.95           64         2818         2633         1566         7.95           64         2818         2633         1566         7.95           64         2818         2633         1566         7.95           64         29.0%         -18.9%         7.95         7.95           1         33         33         8         1           1         33         33         8         1           1         1         33         3         7           1         1         33         3         7           1         PM         I         PM         Model           MM,H         I,M,H         I,M         M         47.67           7         0.74         0.76         0.6         0.36</th><th>22         0.98         1.03         1.02         5.21           6.2         8.99         7.66         5.98         7.95           6.4         2818         2633         1566         7.95           6.4         2818         2633         1566         7.95           6.4         2818         2633         1566         7.95           6.4         2818         2633         1566         7.95           7.9         -9.0%         -18.9%         7.95         7.95           7.9         -9.0%         -18.9%         7.95         7.95           7.9         -9.0%         -18.9%         7.95         7.95           7.9         -9.0%         -18.9%         7.95         7.95           7.9         9.0         -18.9%         7.95         7.95           7.9         9.0         1.0         1.0         1.0         47.67           7.9         0.76         0.96         0.05         0.36         0.36           7.9         1.58         40.12         8         47.89         0.36</th><th>22         0.98         1.03         1.02         5.21           6.2         8.99         7.66         5.98         7.95           6.4         2818         2633         1566         7.95           6.4         2818         2633         1566         7.95           6.4         2818         2633         1566         7.95           6.4         2818         2633         1566         7.95           7.9         -9.7%         -9.0%         -18.9%         7.95           7.9         -9.7%         -9.0%         -18.9%         7.95           7.9         -9.7%         -9.0%         -18.9%         7.95           7.9         0.7         8.3         5         6           7.9         1.1         3         3         5         6           7.4         0.74         1.0         7         47.67           7.4         0.74         0.76         0.36         0.36           7.4         0.74         0.76         0.36         0.36           7.4         0.76         0.76         0.36         0.36           7.4         0.76         0.76         0.36         0.36</th></t<>	22         0.98         1.03         1.02         5.21           6.2         8.99         7.66         5.98         7.95           6.4         2818         2633         1566         7.95           6.4         2818         2633         1566         7.95           6.4         2818         2633         1566         7.95           6.4         2818         2633         1566         7.95           6.9         -9.0%         -18.9%         7.95         7.95           7.9         -9.0%         -18.9%         7.95         7.95           7.9         -9.0%         -18.9%         7.95         7.95           7.9         -9.0%         -18.9%         7.95         7.95           7.9         -9.0%         -18.9%         7.96         7.95           7.9         -9.0%         -18.9%         7.97         7.95           9         -1         37.65         25         30         47.67	22         0.98         1.03         1.02         5.21           (12         8.99         7.66         5.98         7.95           64         2818         2633         1566         7.95           64         2818         2633         1566         7.95           64         2818         2633         1566         7.95           64         2818         2633         1566         7.95           64         29.0%         -18.9%         7.95         7.95           1         33         33         8         1           1         33         33         8         1           1         1         33         3         7           1         1         33         3         7           1         PM         I         PM         Model           MM,H         I,M,H         I,M         M         47.67           7         0.74         0.76         0.6         0.36	22         0.98         1.03         1.02         5.21           6.2         8.99         7.66         5.98         7.95           6.4         2818         2633         1566         7.95           6.4         2818         2633         1566         7.95           6.4         2818         2633         1566         7.95           6.4         2818         2633         1566         7.95           7.9         -9.0%         -18.9%         7.95         7.95           7.9         -9.0%         -18.9%         7.95         7.95           7.9         -9.0%         -18.9%         7.95         7.95           7.9         -9.0%         -18.9%         7.95         7.95           7.9         9.0         -18.9%         7.95         7.95           7.9         9.0         1.0         1.0         1.0         47.67           7.9         0.76         0.96         0.05         0.36         0.36           7.9         1.58         40.12         8         47.89         0.36	22         0.98         1.03         1.02         5.21           6.2         8.99         7.66         5.98         7.95           6.4         2818         2633         1566         7.95           6.4         2818         2633         1566         7.95           6.4         2818         2633         1566         7.95           6.4         2818         2633         1566         7.95           7.9         -9.7%         -9.0%         -18.9%         7.95           7.9         -9.7%         -9.0%         -18.9%         7.95           7.9         -9.7%         -9.0%         -18.9%         7.95           7.9         0.7         8.3         5         6           7.9         1.1         3         3         5         6           7.4         0.74         1.0         7         47.67           7.4         0.74         0.76         0.36         0.36           7.4         0.74         0.76         0.36         0.36           7.4         0.76         0.76         0.36         0.36           7.4         0.76         0.76         0.36         0.36
1 2,3 2,3 PM PM PM PM	M M M M H	2 	2	96.33 88.87 94.11	1.02 0.98 1.03		6.2 8.99 7.66	6.2         8.99         7.66           364         2818         2633	6.2         8.99         7.66           364         2818         2633           -5.8%         -9.7%         -9.0%	6.28.997.6636428182633-5.8%-9.7%-9.0%	6.2         8.99         7.66           364         2818         2633           -5.8%         -9.7%         -9.0%           1         1         3	6.2     8.99     7.66       364     2818     2633       -5.8%     -9.7%     -9.0%       1     1     3       PM     PM     LR	6.2 8.99 7.66 364 2818 2633 -5.8% -9.7% -9.0% 1 1 3 PM PM LR L M,H L,M,H	6.28.997.6636428182633-5.8%-9.7%-9.0%-5.8%-9.7%-9.0%113PMPMLRLM,HL,M,H25.4641.737.65	6.28.997.6636428182633-5.8%-9.7%-9.0%-5.8%-9.7%-9.0%113PMPMIRPMPMIRLM,HI,M,H25.4641.737.650.740.740.36	6.28.997.6636428182633-5.8%-9.7%-9.0%-5.8%-9.7%-9.0%113PMPMLRPMPMLRPMPMLRLM,HL,M,HLM,H25.4641.70.740.740.361.951.5840.12	6.28.997.663642.8182633-5.8%-9.7%-9.0%-5.8%-9.7%-9.0%113PMPMLRPMPMLRPMPMLRPMPM25.4641.725.4641.737.650.740.740.361.951.5840.1217352466107
1 1 PM PM PM PM 93.5 96.33	РМ РМ М Н 93.5 96.33	М Н 93.5 96.33	93.5 96.33		1.03 1.02	7.2 6.2		2102 364	2102 364 -9.4% -5.8%	2102 364 -9.4% -5.8%	2102 364 -9.4% -5.8% 1 1	2102 364 -9.4% -5.8% 1 1 LR PM	2102 364 -9.4% -5.8% 1 1 LR PM H L	2102 364 -9.4% -5.8% 1 1 LR PM H L 9 25.46	2102 364 -9.4% -5.8% 1 1 1 1 1 R H H L 9 25.46 0.74 0.74	2102 364 -9.4% -5.8% 1 1 1 LR PM LR PM H L H L 0.74 0.74	2102     364       -9.4%     -5.8%       1     1       1     1       1     1       1     1       1     1       1     1       1     1       1     25.46       0.74     0.74       5.5     1.95       731     1735
2,3 1		LR PM	н	56 89	1.02 0.99		8 8.5	8 8.5 2214 1735	8 8.5 2214 1735 0.3% -5.2%	8 8.5 2214 1735 0.3% -5.2%	8 8.5 2214 1735 0.3% -5.2% 2 1	8 8.5 2214 1735 0.3% -5.2% 2 1 2 1 PM LR	8 8.5 2214 1735 0.3% -5.2% 2 1 2 1 PM LR H L,M	8.5 2214 1735 0.3% -5.2% 2 1 2 1 PM LR H L,M 89.98 8.47	8.5 8.5 2214 1735 0.3% -5.2% 2 1 2 1 R PM LR H L/M 89.98 8.47 0.51 0.71	8.5 2214 1735 0.3% -5.2% 2 1 2 1 PM LR H L,M H L,M 89.98 8.47 0.51 0.71 4.99 6	8.5 8.5 8.5 2214 1735 0.3% -5.2% 2.1 1735 0.3% -5.2% 2.1 2.2 1 2.2 1 2.2 1 2.2 2.2 1 2.2 2.2
	2,3 2	LR	Σ	50	1.02	L	č.ð	c.8 2127	2.8 2127 2 -15.0% -(	<ul> <li>c.8</li> <li>2127</li> <li>215.0%</li> <li>-15.0%</li> </ul>	<ul> <li>c.8</li> <li>2127</li> <li>215.0%</li> <li>-15.0%</li> <li>2</li> </ul>	2127 2 2127 2 -15.0% -( -15.0% -( PM F	8.5 2127 2 -15.0% -( -0 -0 -0 -0 -0 -0 -0 -0 -0 -0 -0 -0 -0	<ul> <li>8.5</li> <li>2127</li> <li>2127</li> <li>2</li> <li>PM</li> <li>F</li> <li>M</li> <li>34.78</li> <li>3</li> </ul>	2127 2 2127 2 -15.0% -6 PM F M 3 34.78 3 0.52	<ul> <li>8.5</li> <li>2127</li> <li>2127</li> <li>2</li> <li>-15.0%</li> <li>-6</li> <li>-15.0%</li> <li>-6</li> <li>-6</li> <li>-15.0%</li> <li>-6</li> <li>-15.0%</li> <li>-6</li> <li>-15.0%</li> <li>-6</li> <li>-15.0%</li> <li>-6</li> <li>-15.0%</li> <li>-15.0%</li></ul>	<ul> <li>8.5</li> <li>2127</li> <li>2127</li> <li>215.0%</li> <li>-(</li> <li>-15.0%</li> <li>-(</li> <li>-(</li> <li>-15.0%</li> <li>-(</li> <li>-(</li></ul>
	2,3	LR		45	1.02		10	10 2513	10 2513 -36.4%	10 2513 -36.4%	10 2513 -36.4% 2	10 2513 -36.4% 2 PM	10 2513 -36.4% 2 PM	10 2513 -36.4% PM L L	10 2513 -36.4% PM L L 33.32 0.51	10 2513 -36.4% PM L L L 33.32 0.51 7.21	10 2513 -36.4% PM L L L L 33.32 33.32 0.51 7.21 2818
	1	LR	т	56.3	1.02		7.7	7.7 731	7.7 731 -2.8%	7.7 731 -2.8%	7.7 731 -2.8%	7.7 731 -2.8% 2 LR	7.7 731 -2.8% 2 LR H	7.7 731 -2.8% 2 LR H 10.01	7.7 731 -2.8% 2 LR H H 10.01 0.7	7.7 731 -2.8% 2 LR H H 10.01 9.98	7.7 731 -2.8% -2.8% H H H 10.01 0.7 9.98 9.98
•	-	LR	Σ	51	1.02		7.9	7.9 1079	7.9 1079 -9.8%	7.9 1079 -9.8%	7.9 1079 -9.8% 2	7.9 1079 -9.8% 2 LR	7.9 1079 -9.8% 2 LR M	7.9 1079 -9.8% 2 LR M 9	7.9 1079 -9.8% 2 LR M 9 0.7	7.9 1079 -9.8% -9.8% LR M 9 0.7 11	7.9 1079 -9.8% 2 LR M 9 0.7 11 2127
	-	LR		48	1.02		10	10 1249	10 1249 -29.5%	10 1249 -29.5%	10 1249 -29.5% 2	10 1249 -29.5% 2 LR	10 1249 -29.5% 2 LR LR	10 1249 -29.5% 2 LR LR 8.09	10 1249 -29.5% 2 LR LR LR 8.09 8.09 0.705	10 1249 -29.5% 2 LR LR L R 8.09 0.705 12.91	10 1249 -29.5% 2 LR L R 8.09 8.09 0.705 12.91 2513
, c c t	С,2,1	HR	т	8.87	0.61	_	7.98	7.98 3269	7.98 3269 -56.2%	7.98 3269 -56.2%	7.98 3269 -56.2% 1,2,3	7.98 3269 -56.2% 1,2,3 HR	7.98 3269 -56.2% 1,2,3 HR H	7.98 3269 -56.2% 1,2,3 HR H 6.21	7.98 3269 -56.2% 1,2,3 HR H H 6.21 0.71	7.98 3269 -56.2% 1,2,3 HR H 6.21 0.71 12.11	7.98 3269 -56.2% -56.2% HR H H 6.21 0.71 0.71 12.11
	1,2,3	HR	Σ	6.32	0.58		8.79	8.79 2316	8.79 2316 -23.2%	8.79 2316 -23.2%	8.79 2316 -23.2% 1,2,3	8.79 2316 -23.2% 1,2,3 HR	8.79 2316 -23.2% 1,2,3 HR M	8.79 2316 -23.2% 1,2,3 HR M 4.34	8.79 2316 -23.2% 1,2,3 HR M 4.34 0.72	8.79 2316 -23.2% 1,2,3 HR M 4.34 0.72 15.03	8.79 2316 -23.2% -23.2% HR M M 4.34 4.34 0.72 0.72 15.03 2316
	1,2,3	HR		2.47	0.61		5.89	5.89 2234	5.89 2234 -33.6%	5.89 2234 -33.6%	5.89 2234 -33.6% 1,2,3	5.89 2234 -33.6% 1,2,3 HR	5.89 2234 -33.6% 1,2,3 HR L	5.89 2234 -33.6% 1,2,3 HR L L 7.02	5.89 2234 -33.6% 1,2,3 HR L L 7.02 0.71	5.89 2234 -33.6% 1,2,3 HR HR L C 7.02 0.71 49.78	5.89 2234 -33.6% 1,2,3 HR HR 1,2,3 HR 0.71 0.71 49.78 2234
	Zone	Treatment	Traffic level	8	ß		σ	ρ Observations	ρ Observations % Change in RMSE	ρ Observations % Change in RMSE Failures	P Observations % Change in RMSE Failures Zone	p Observations % Change in RMSE Failures Zone Treatment	p Observations % Change in RMSE Failures Zone Treatment Traffic level	ρ Observations % Change in RMSE Failures Zone Treatment Traffic level	ρ Observations % Change in RMSE Failures Zone Treatment Traffic level β	ρ Observations % Change in RMSE Failures Zone Treatment Traffic level β	ρ Observations % Change in RMSE Failures Zone Treatment Traffic level β Observations

Appendix D continued

										Ð	Original	Model	478.6	0.37	504.57		
	ΓC	Original	Model	34.47	0.52	240.75				ε	ΡM	M,H	463.14	0.49	497.89	65	-38.5%
	1&2	M	т	60.12	0.45	176.4	1970	-2.70%		m	ΡM	-	455.84	0.49	520.5	504	-7.9%
	1	PM	Σ	52.3	0.469	175.6	2102	-4.60%		œ	LR	L,M,H	450.3	0.49	595.1	107	-90.2%
	1	ΡM	-	40.3	0.485	185.43	1735	-1.70%		2	ΡM	н	21.77	0.32	25.89	1566	-25.2%
	2	PM	Σ	44	0.48	180	2633	-1.50%		2	PM	Σ	19.67	0.33	29.6	2633	-40.9%
	2	PM	_	40.97	0.487	187.3	2818	-1.10%		2	PM	_	15.15	0.33	30.34	2818	-54.9%
	3	LR&PM	т	50.15	0.47	178.65	121	-6.60%		7	PM	M,H	465	0.46	580	2466	-71.1%
	3	LR&PM	L,M	43.21	0.498	190.23	555	-5.60%		1	PM	-	460.74	0.46	600	1735	-82.0%
	1&2	LR	т	45.7	0.499	198.6	2945	-1.60%		2	LR	т	120.11	0.58	200	2214	-90.1%
	1	LR	Σ	39.56	0.5	204	1079	-1.20%		2	LR	Σ	130.45	0.58	220.5	2127	-88.4%
	1	LR	_	45	0.53	213	1249	-0.60%		2	LR		410	0.49	597.5	2513	-92.8%
	2	LR	Σ	35	0.51	222	2127	-0.20%		1	LR	т	450.18	0.47	594	731	-92.1%
	2	LR	_	40	0.53	232	2513	-0.10%		1	LR	Σ	430.25	0.49	570.11	1079	-91.7%
	1,2,3	HR	т	34.47	0.52	240.75	3269	0.00%		1	LR	_	384.5	0.49	596.1	1249	-93.7%
	1,2,3	HR	Σ	33	0.56	235	2316	0.10%		1,2,3	HR	M,H	403.4	0.5	595.1	5585	7.0%
	1,2,3	HR	_	23	0.6	238.4	2234	0.40%		1,2,3	HR	_	472.2	0.52	595.9	2234	1.8%
Longitudinal Cracks	Zone	Treatment	Traffic level	σ	ß	d	Observations	% Change in RMSE	Concrete Patches	Zone	Treatment	Traffic level	α	β	d	Observations	% Change in RMSE

Note: original model recommended for longitudinal cracks, heavy rehabilitation, heavy traffic (all zones).

Appendix D final page

		SS	Original	Model	80	1	30			
		1,2,3	PM	т	13.03	0.55	265.00	1,970	-97%	
		1,2,3	PM	L,M	13.08	0.61	235.00	9,817	-86%	
		1,2,3	LR	L,M,H	12.10	0.59	298.00	10,020	-99.7%	
)		1,2,3	HR	L,M,H	13.00	0.71	300.00	7,819	-98%	
•	Shattered Slabs	Zone	Treatment	Traffic level	α	β	ρ	Observations	% Change in RMSE	

NOTE: For the above tables, Low Traffic is defined as having a projected 20 year 18KESAL forecast below 1,000,000; Medium Traffic is between 1,000,000 and 10,000,000; and High Traffic is greater than or equal to 10,000,000.