

Montana Department of Transportation (MDT)
Performance Prediction Models



Performance Prediction Models

PROJECT HWY-30604 DT
September 6, 2007

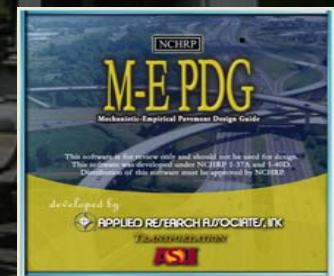
Fugro Consultants, Inc.
Applied Research Associates, Inc.



Presentation Outline



1. Introduction & Overview of Project
2. Ancillary Studies
3. Determination of MEPDG Inputs
4. Database
5. Verification & Calibration of MEPDG for Use in Montana
6. Summary & Concluding Comments





Objective



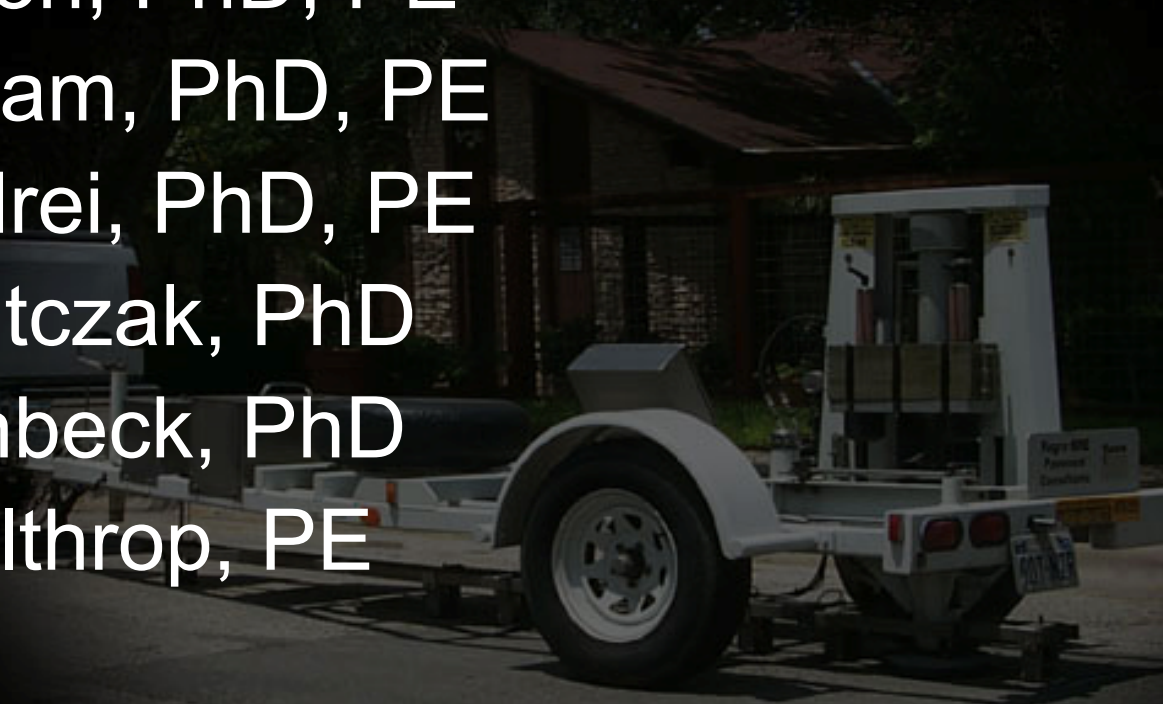
- ✦ To calibrate & streamline a design procedure based on HMA distress prediction models using mechanistic-empirical principles in Montana
- ✦ To verify and calibrate the distress prediction models or transfer functions included in the MEPDG for use in Montana



Project Team



- ✦ Harold L. Von Quintus, PE
- ✦ Brian Killingsworth, PE
- ✦ Amy Simpson, PhD, PE
- ✦ Weng-On Tam, PhD, PE
- ✦ Dragos Andrei, PhD, PE
- ✦ Matthew Witczak, PhD
- ✦ Mark Hallenbeck, PhD
- ✦ James Moulthrop, PE





Phases for MEPDG Implementation



**Phase I -
Planning**



**Phase II -
Initial Data
Collection & Analyses**



**Phase III -
Annual Data
Collection, Analyses,
& Calibration**



Road Map for Implementation



Phase I

1. Distress Prediction Models.

2. Typical Design Features, Materials, Construction Procedures

3. Experimental Design Factorial

4. Monitoring & Test Plans

Phase II

5. Initial Data Collection & QC

6. Data Analysis & Calibration

Phase III

5. Annual Data Collection

7. Data QC & Updates to Calibration Function



Dual Purpose Experimental Factorial



1. Local
Calibration

2. Confirmation of
Default Values

✦ Identify test
sections to cover
typical design
features

- Design inputs & features
- Materials
- Construction



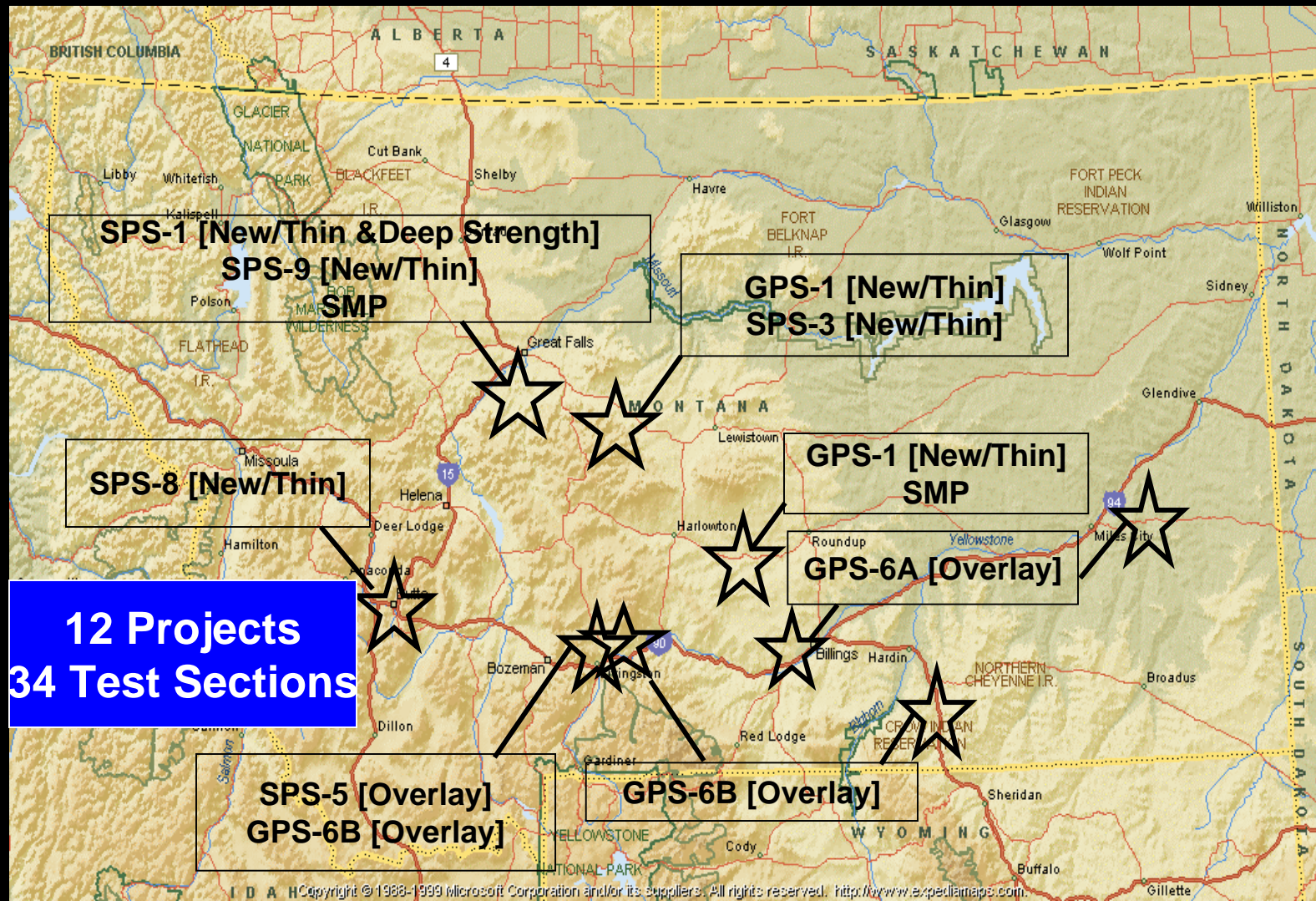
Experimental Factorial



Climate/Region		Western			Eastern		
Mix Designation		B	D	SP	B	D	SP
Conventional HMA Pavement	Type A Base	1	2	3	4	5	6
	Type B Base						
	ATPB (<i>SPS-1</i>)	13	14	15	16	17	18
Deep-Strength Pavement		7	8	9	10	11	12
Semi-Rigid Pavement		19	20	21	22	23	24
Reconstruct.; In-Place Recycle	Semi-Rigid						
	Granular	25	26	27	28	29	30
HMA Overlay	HMA	37	38	39	40	41	42
	Mill-Overlay						
	Semi-Rigid	31	32	33	34	35	36

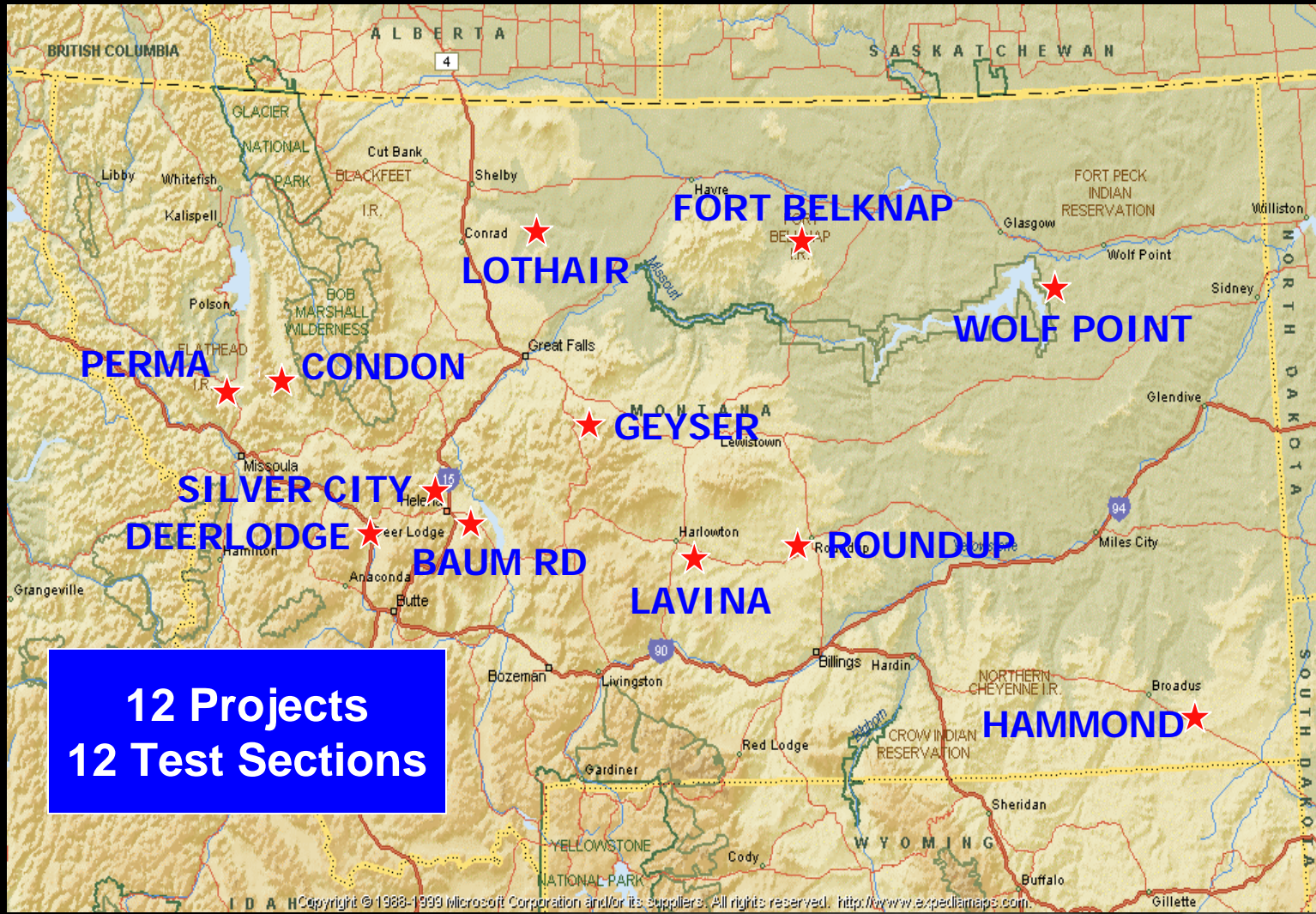


Test Sections: LTPP – Montana





Test Sections: Non-LTPP – Montana





Test Sections: LTPP – Surrounding States



State, Experiment (No. of Sites)

- ✦ ID, GPS-1 (7), GPS-6 (1)
- ✦ ND, GPS-2 (1)
- ✦ SD, SPS-8 (2)
- ✦ WY, GPS-1 (1), GPS-2 (6), GPS-6 (3)
- ✦ AB, SPS-5 (9), GPS-1 (3), GPS-2 (1) SPS-9 (3)
- ✦ SK, GPS-1 (1), GPS-6 (6)

**33 Projects
44 Test Sections**



Total Projects



✦ Total Number of Projects and Test Sections available:

- 57 Projects
- 90 Test Sections

✦ Total Number of Projects and Test Sections Used in the Study:

- 40 Projects
- 52 Test Sections





Lab & Field Investigations: Non-LTPP Sites



- ☑ **Materials Recovery & Laboratory Testing**
 - **HMA**
 - **CTB**
 - **Unbound Materials & Soils**
- ☑ **FWD Testing**
- ☑ **Traffic from MDT Database**
- ☑ **Profile**
- ☑ **Distress Surveys**





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Ancillary Studies



- ✦ Test sections located in Montana versus those located in adjacent States:
 - Performance comparisons
 - HMA volumetric properties
 - Traffic volumes
- ✦ Distribution of Weather Stations
- ✦ Deflection basin comparisons between LTPP FWD and Montana's FWD
- ✦ Profile comparisons between LTPP profilometer & Montana's profilometer



Performance Comparisons: Montana Vs. Adjacent States



Distress, Average	Montana Sections	Adjacent State
Rutting, in.	0.29	0.50
Transverse Cracking, ft./mi.	479	2026
Semi-Rigid; Fatigue Cracking	None	55%
Longitudinal Cracking, ft./mi.	965	1576
Raveling	None	30%

Result: Systematic difference in performance between Montana sections & those in adjacent States



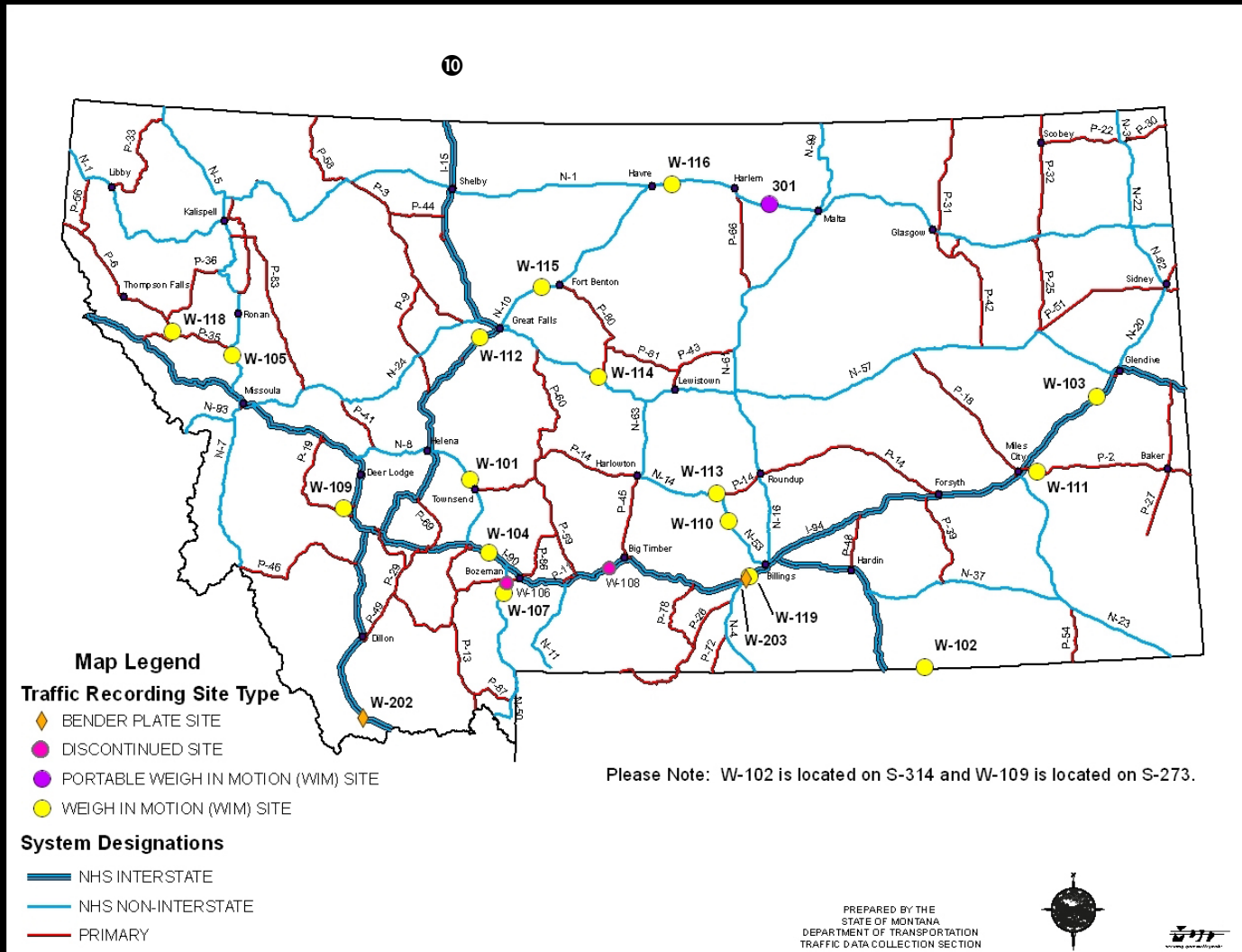
HMA Volumetric Properties: Montana Vs. Adjacent States



- ✦ Air voids of the HMA mixtures were generally lower from the cores recovered from the Montana sections than from the test sections located in adjacent States
- ✦ No significant systematic difference in total asphalt content by weight.
- ✦ Effects of Pavement Preservation Activities?

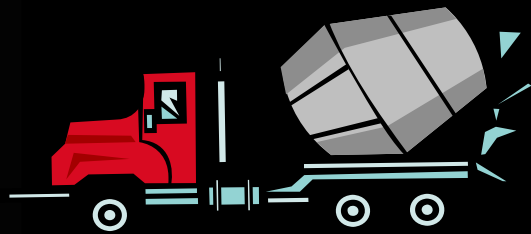
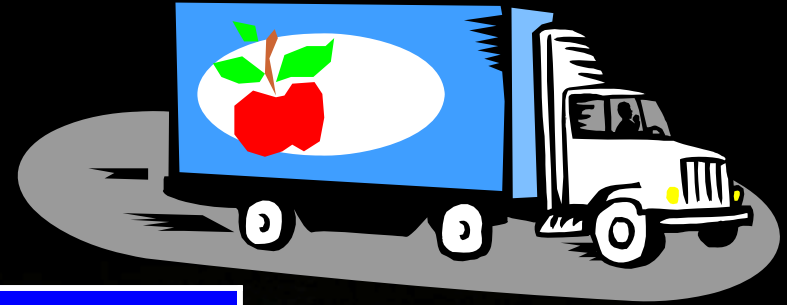
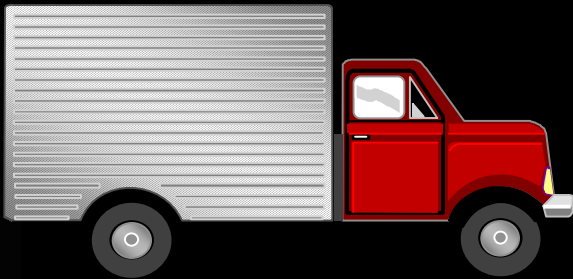


Traffic WIM Sites

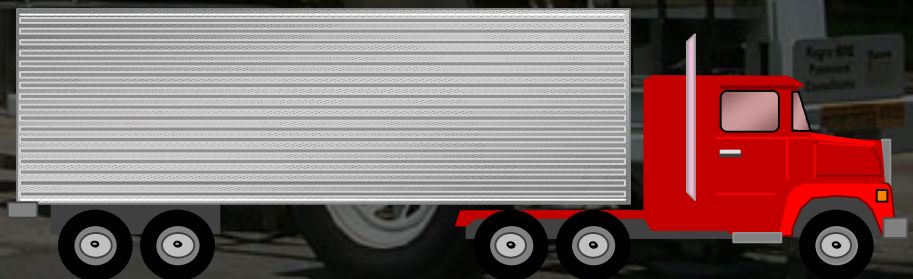
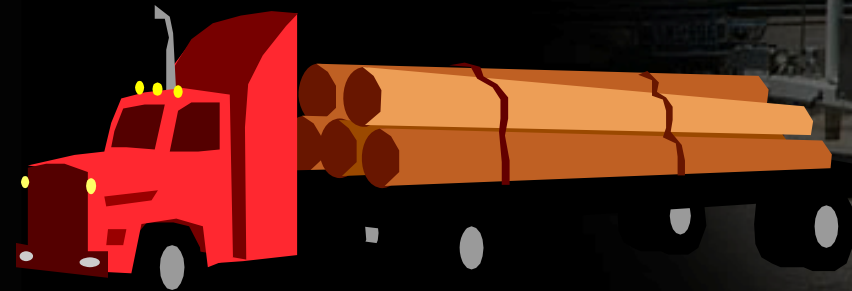




Traffic

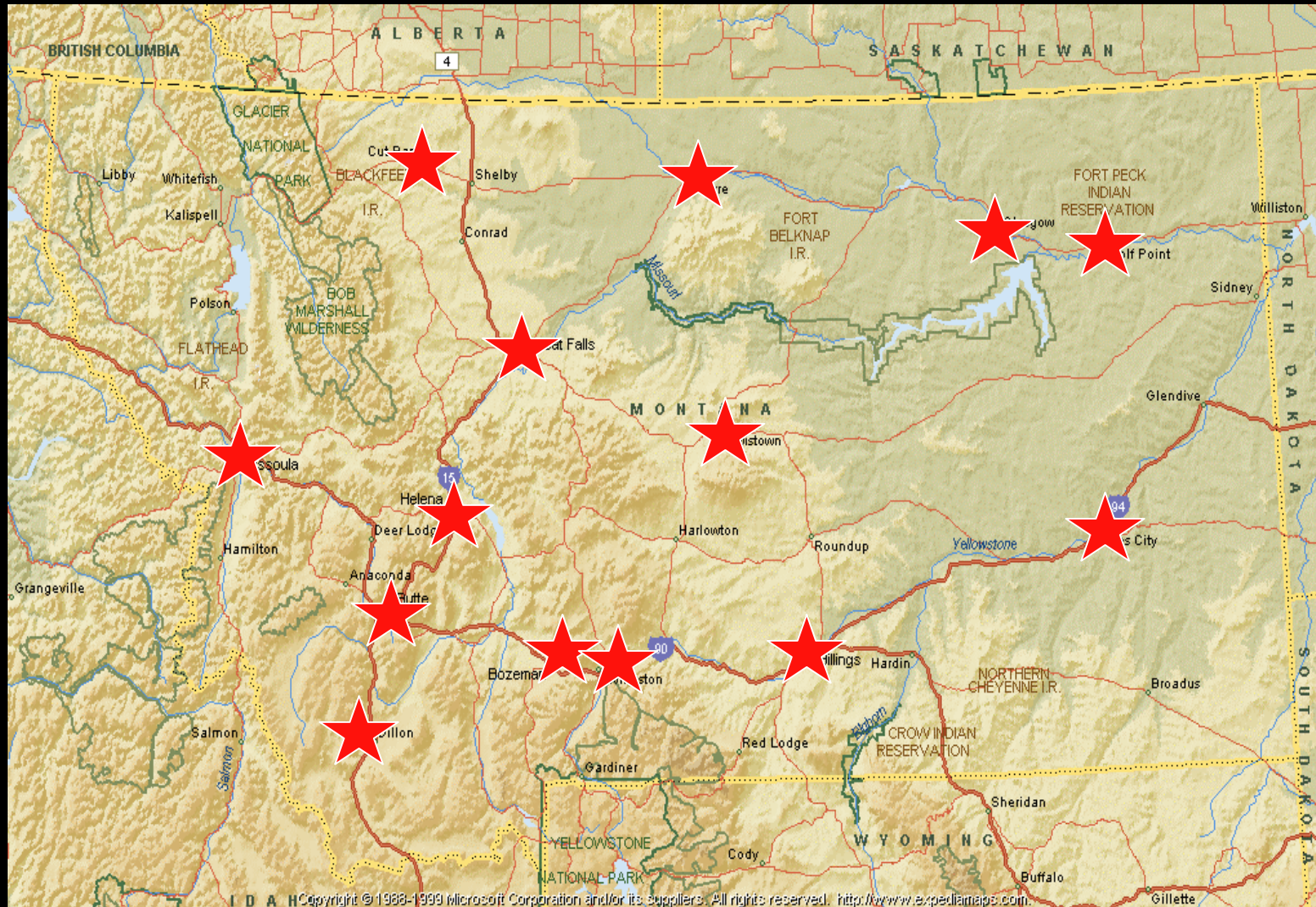


No significant systematic difference in truck volumes and distributions between Montana & adjacent States



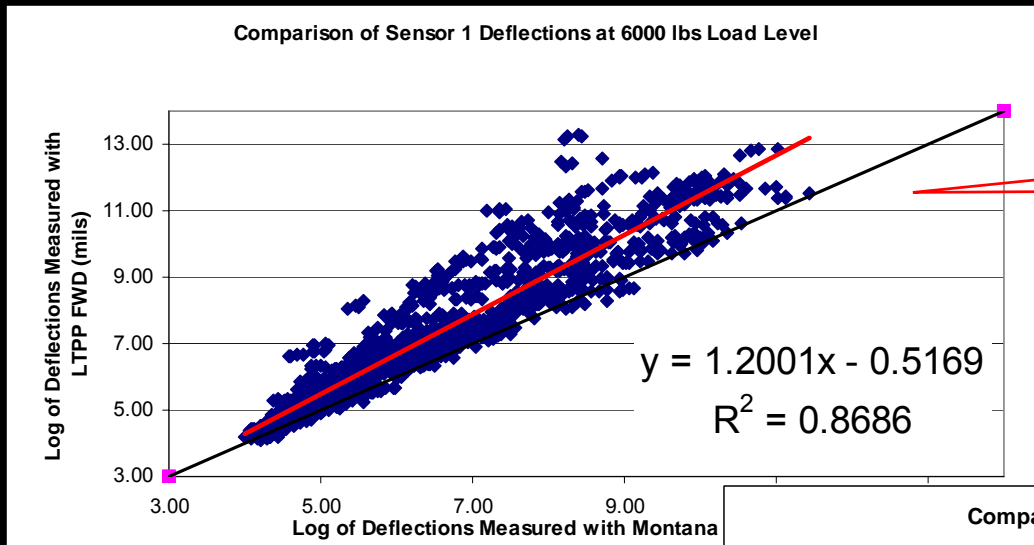


Weather Stations



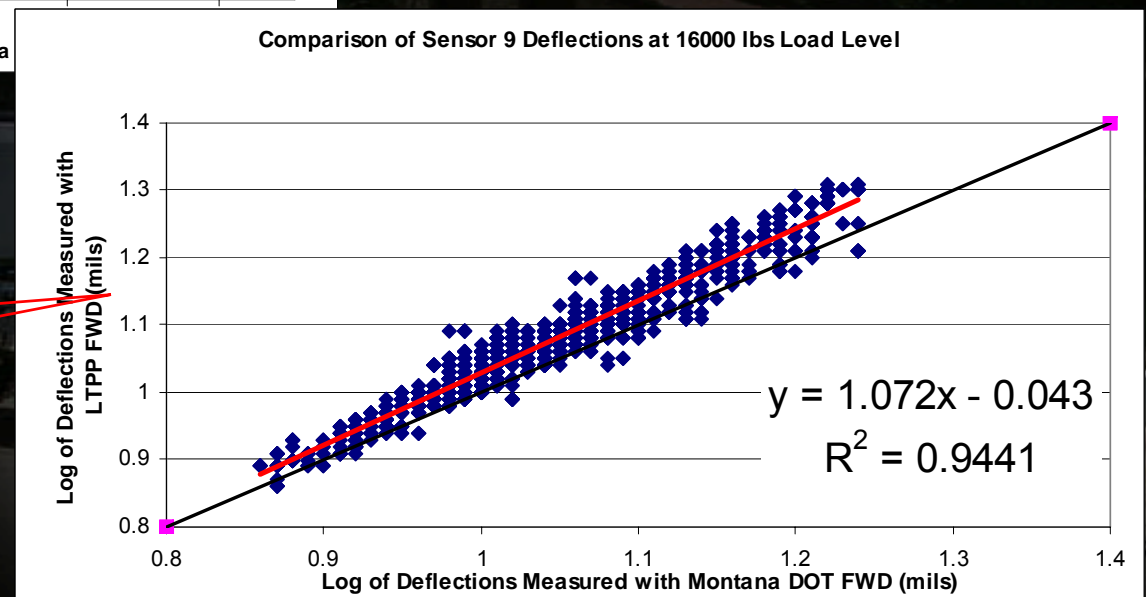


FWD Comparison Study: Deflections



Sensor #1

Sensor #9

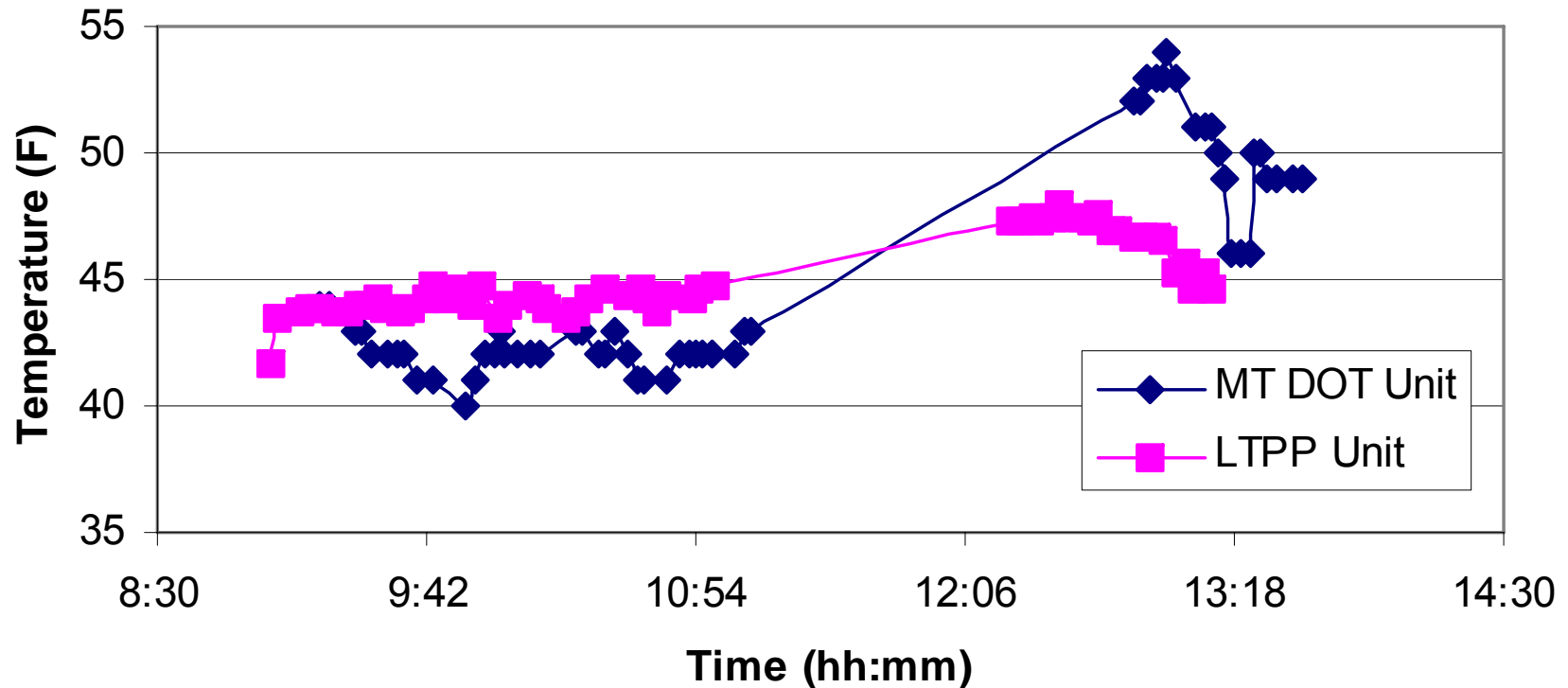




FWD Comparison Study: Temperature Readings

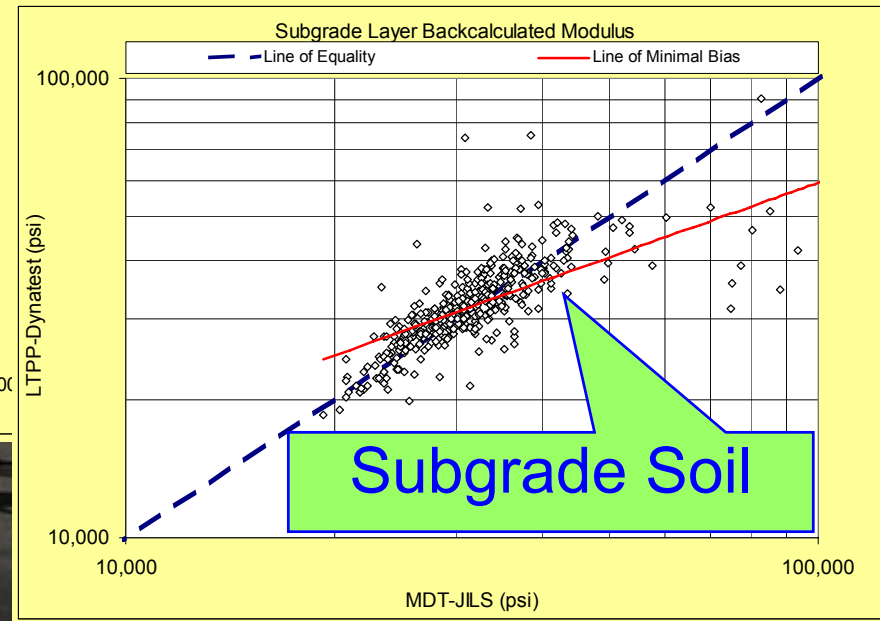
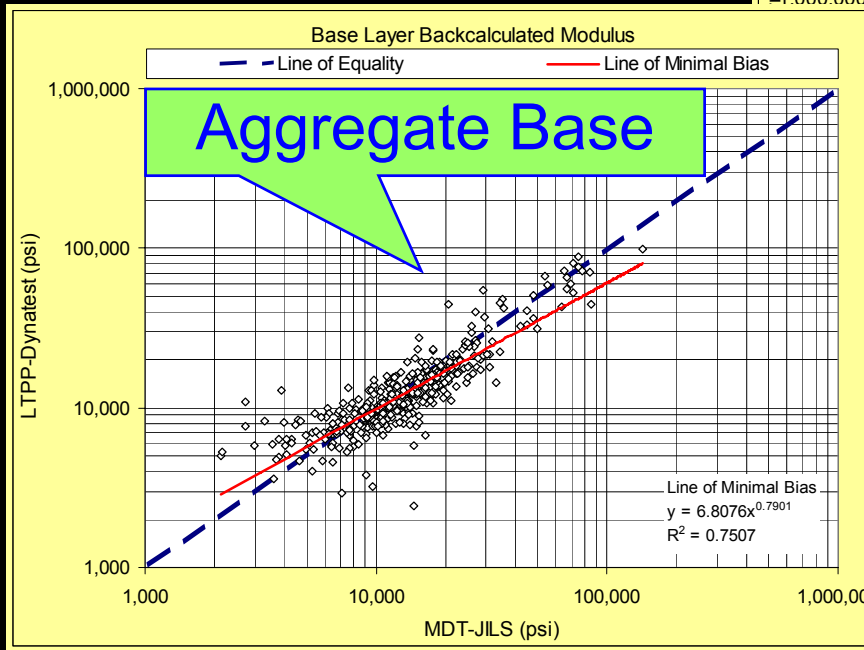
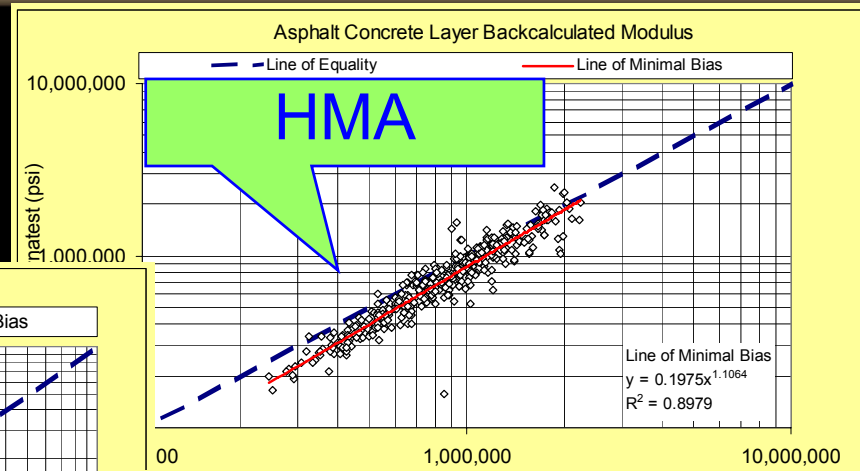


Comparison of Temperature Measurements Obtained by 2
Different FWDs on 05/11/04





FWD Comparison Study: Modulus





FWD Comparison Study: Results



- ✦ The LTPP equipment consistently measured higher deflections when compared to the MDT equipment.
- ✦ The difference between the two devices decreased further from the loading plate.
- ✦ Back-calculated elastic layer modulus values:
 - Subgrade and aggregate base layers – no significant difference.
 - HMA layers – elastic modulus values from LTPP measured basins are consistently lower than those from the Montana measured basins.



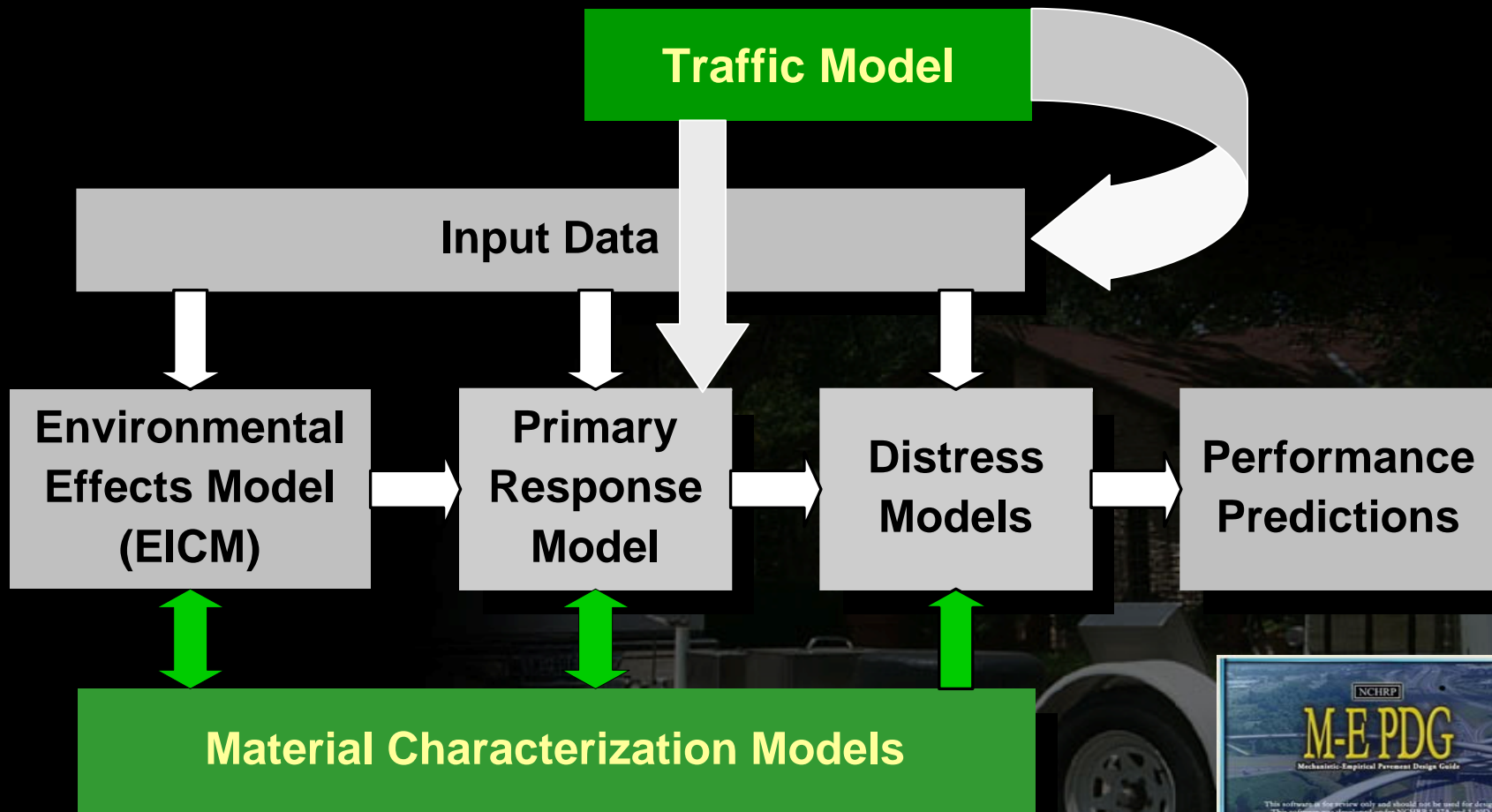
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MEPDG Design Process





Traffic: Volume Distribution Factors



Roadway Description	Applicable TTC Group
Interstate Highways & Primary Arterials, Heavier Volume Roadways	TTC-11
Primary & Secondary Arterials, Moderate Volume Roadways	TTC-5
Secondary Arterials, Lower Volume Roadways	TTC-8
Local Routes with Low Truck Volumes	TTC-15



Traffic: Seasonal Distribution Factors



Month	Single Units	Combination Trucks	Multi-Trailer Trucks
Jan.	0.84	0.91	0.99
Feb.	0.79	0.92	0.89
Mar.	0.76	0.94	0.88
April	0.86	0.99	0.99
May	1.10	1.06	1.03
June	1.30	1.09	0.96
July	1.43	1.02	0.92
Aug.	1.39	1.06	1.11
Sept.	1.14	1.00	1.09
Oct.	1.06	1.15	1.12
Nov.	0.87	1.00	1.00
Dec.	0.76	0.84	0.87



Traffic: Axle Load Distribution Factors

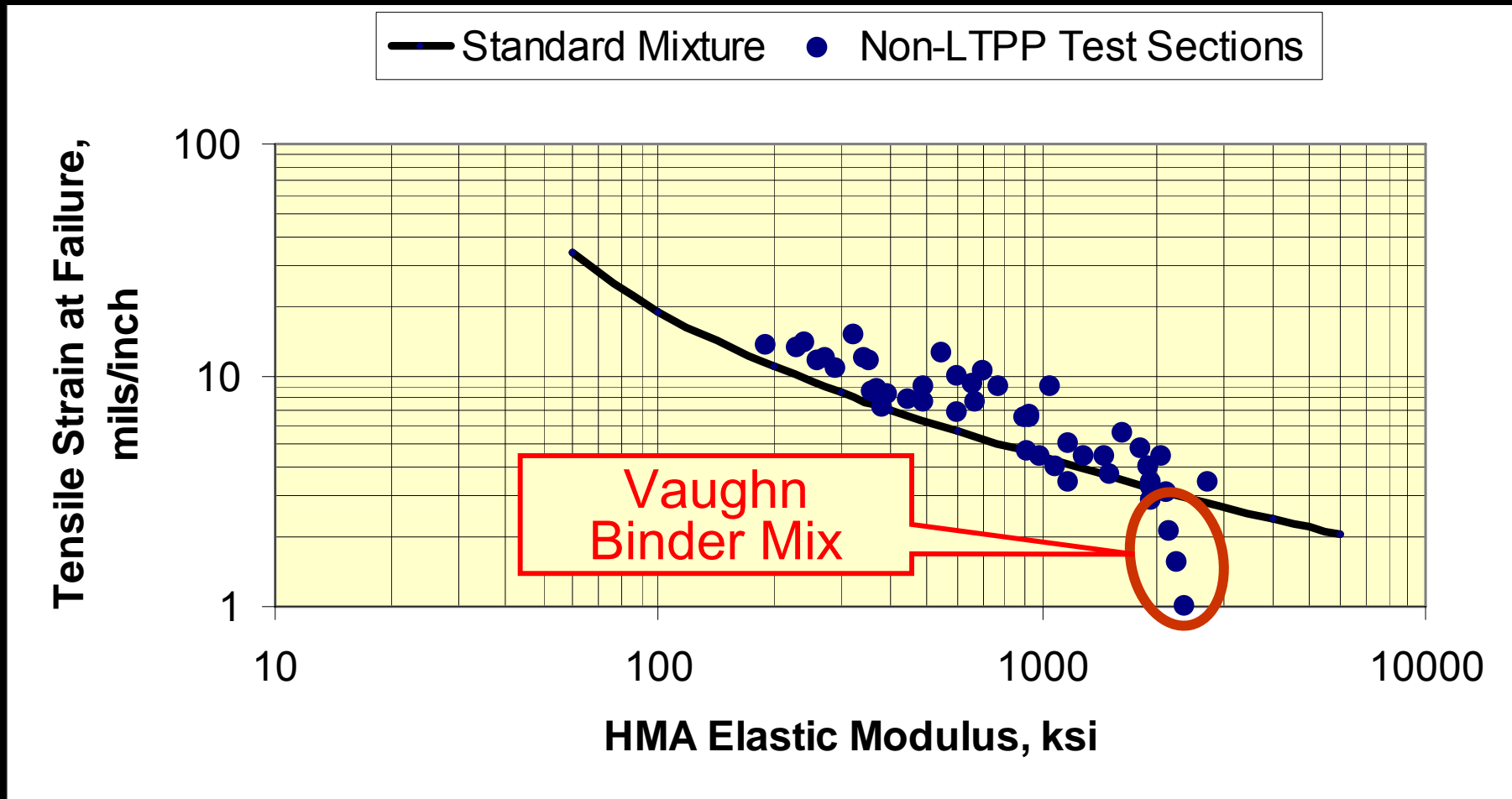


1. Primarily Loaded Trucks
2. Bimodal Loaded Condition – Heavy Distribution
3. Bimodal Loaded Condition – Even Distribution
4. Lightly Loaded Trucks

MEPDG defaults used because of drifts noted in 2000-2001 data

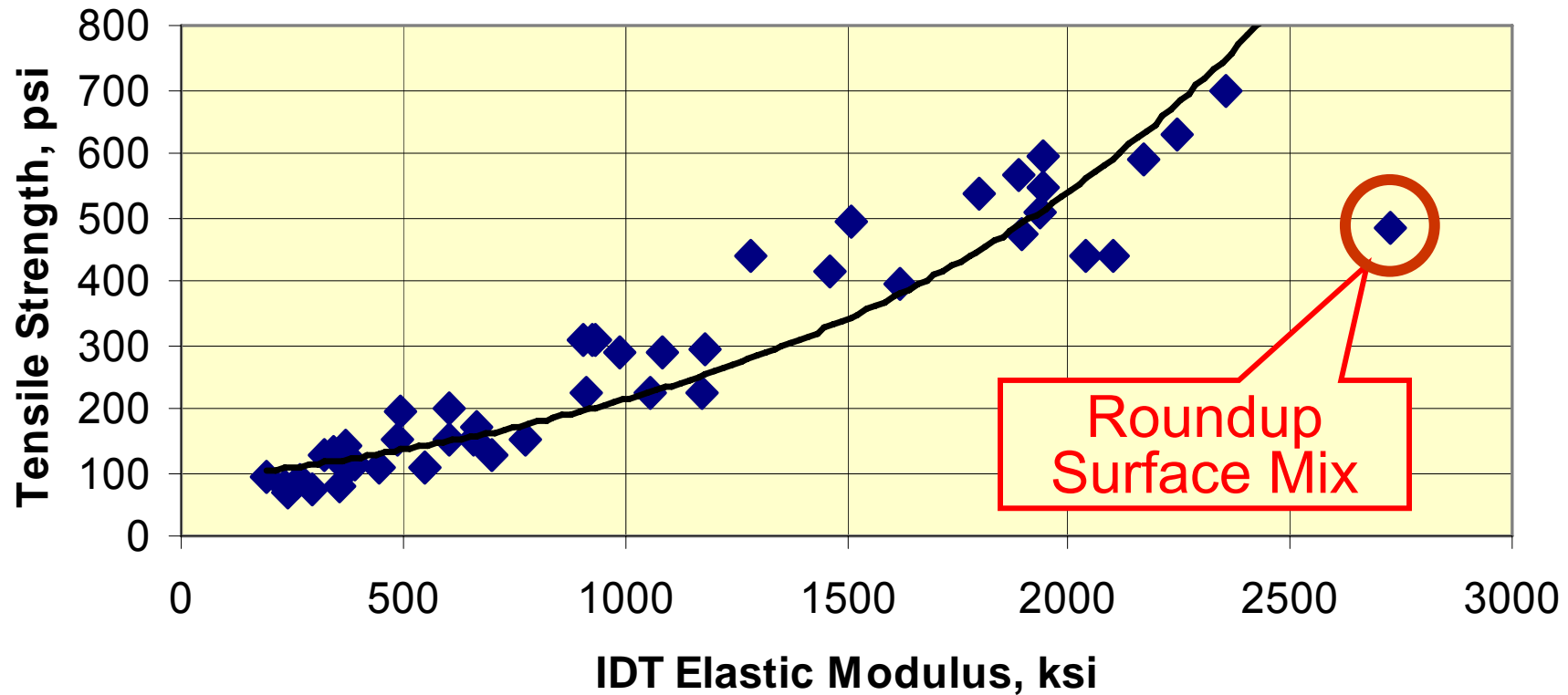


HMA Characterization



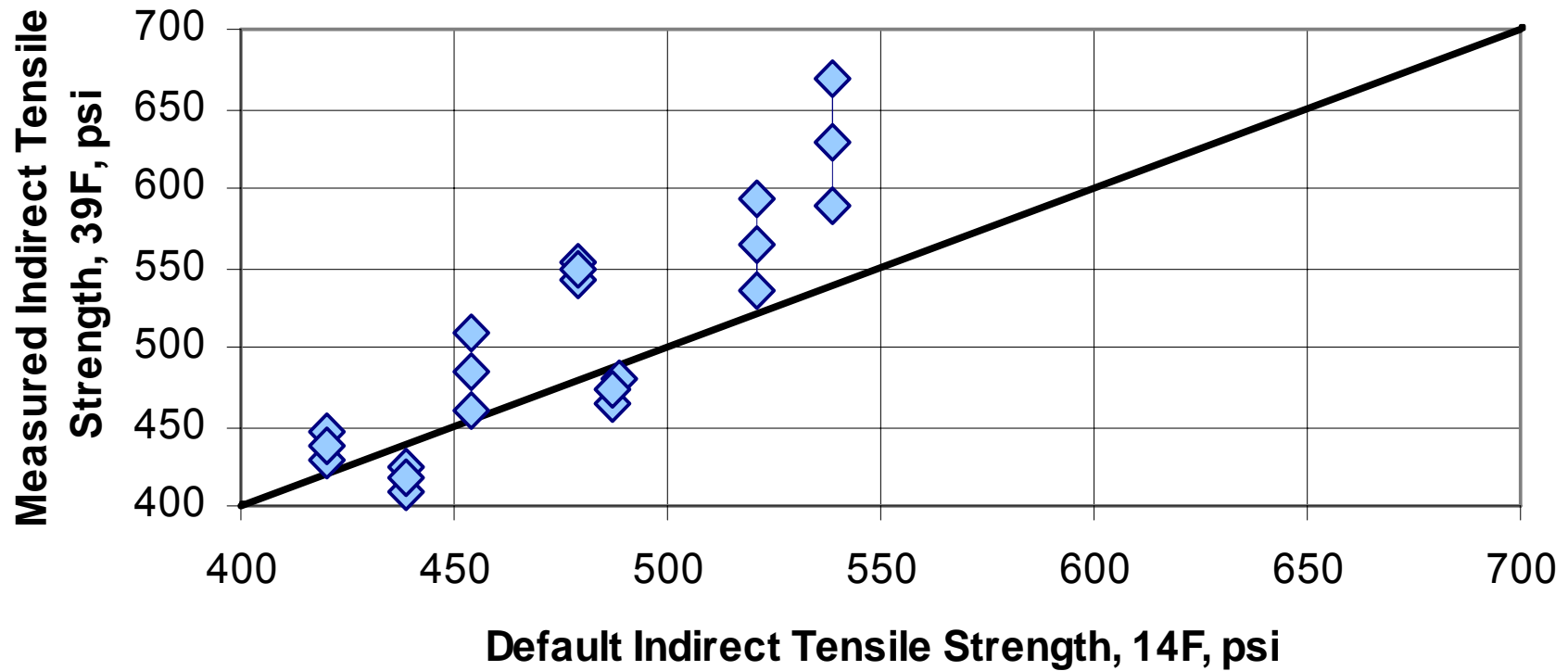


HMA Characterization



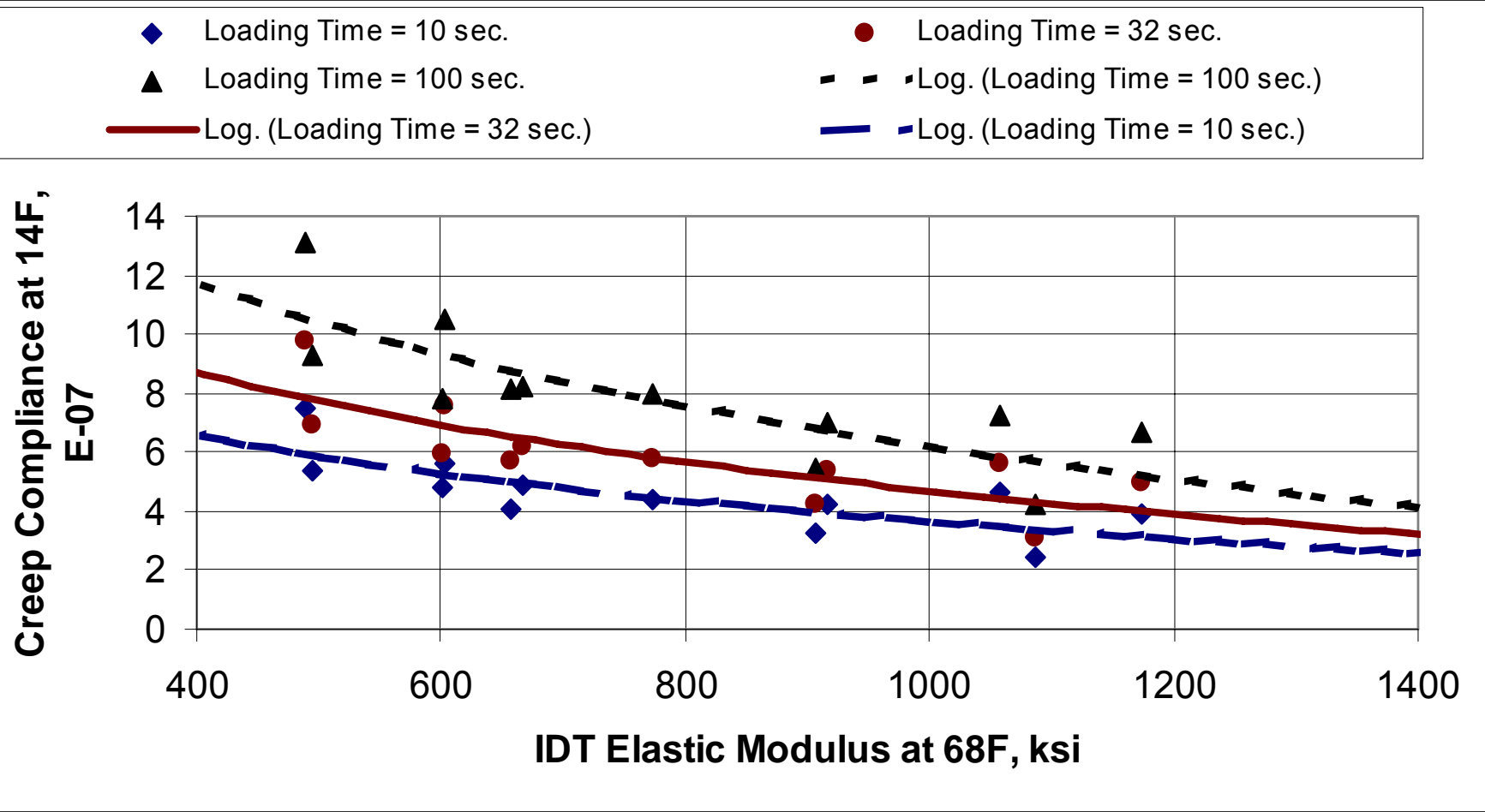


IDT Strength





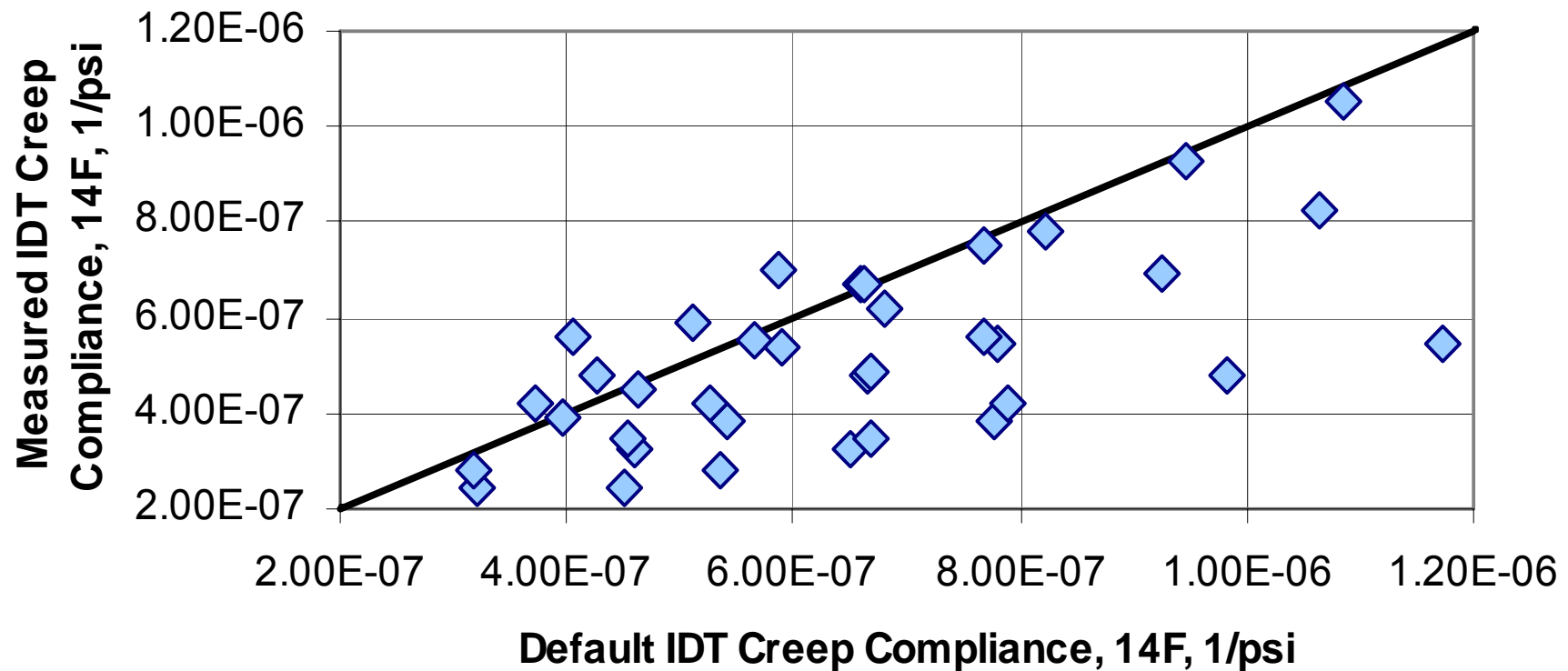
IDT Creep Compliance



Default values versus laboratory measured values

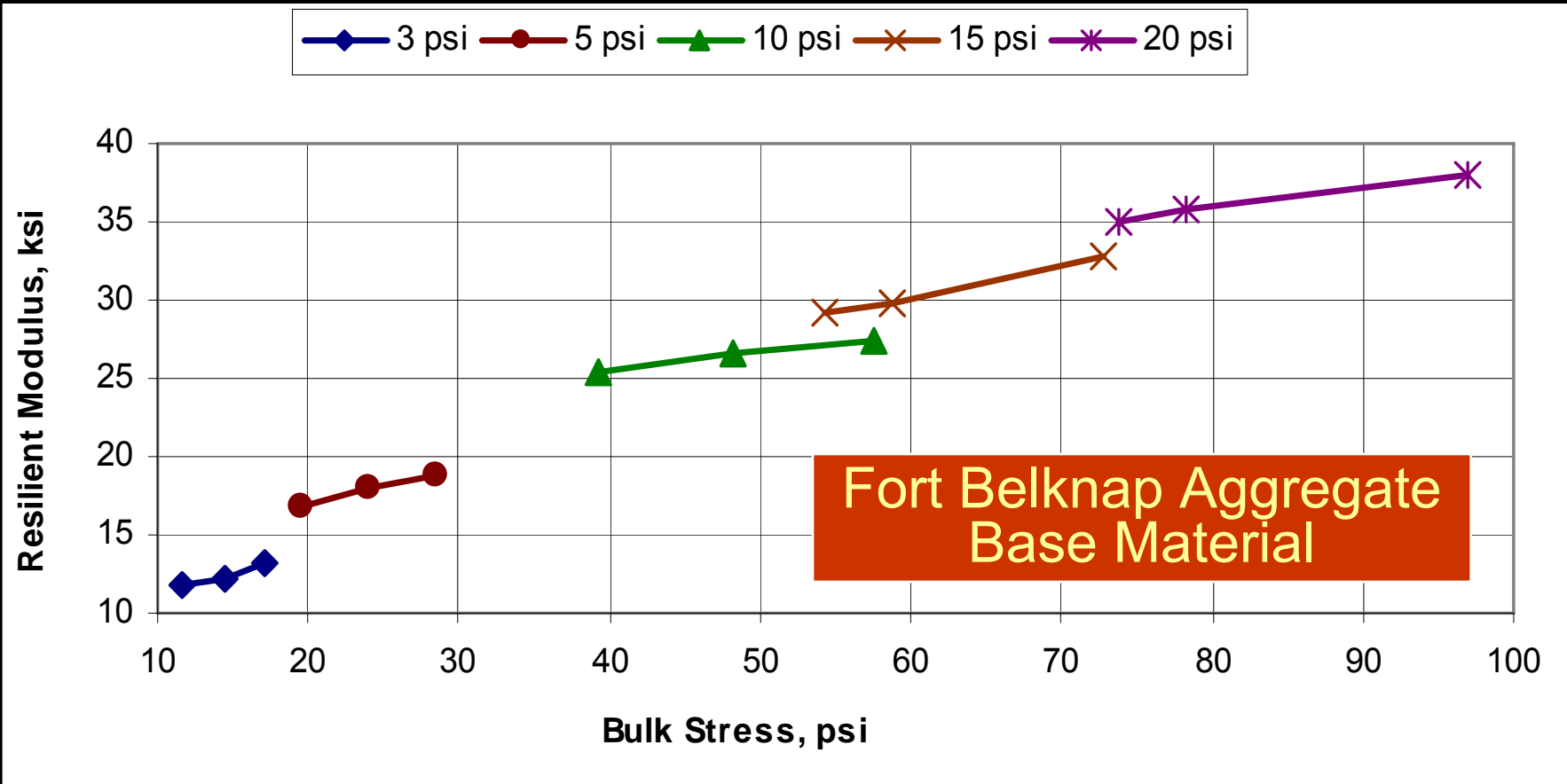


IDT Creep Compliance





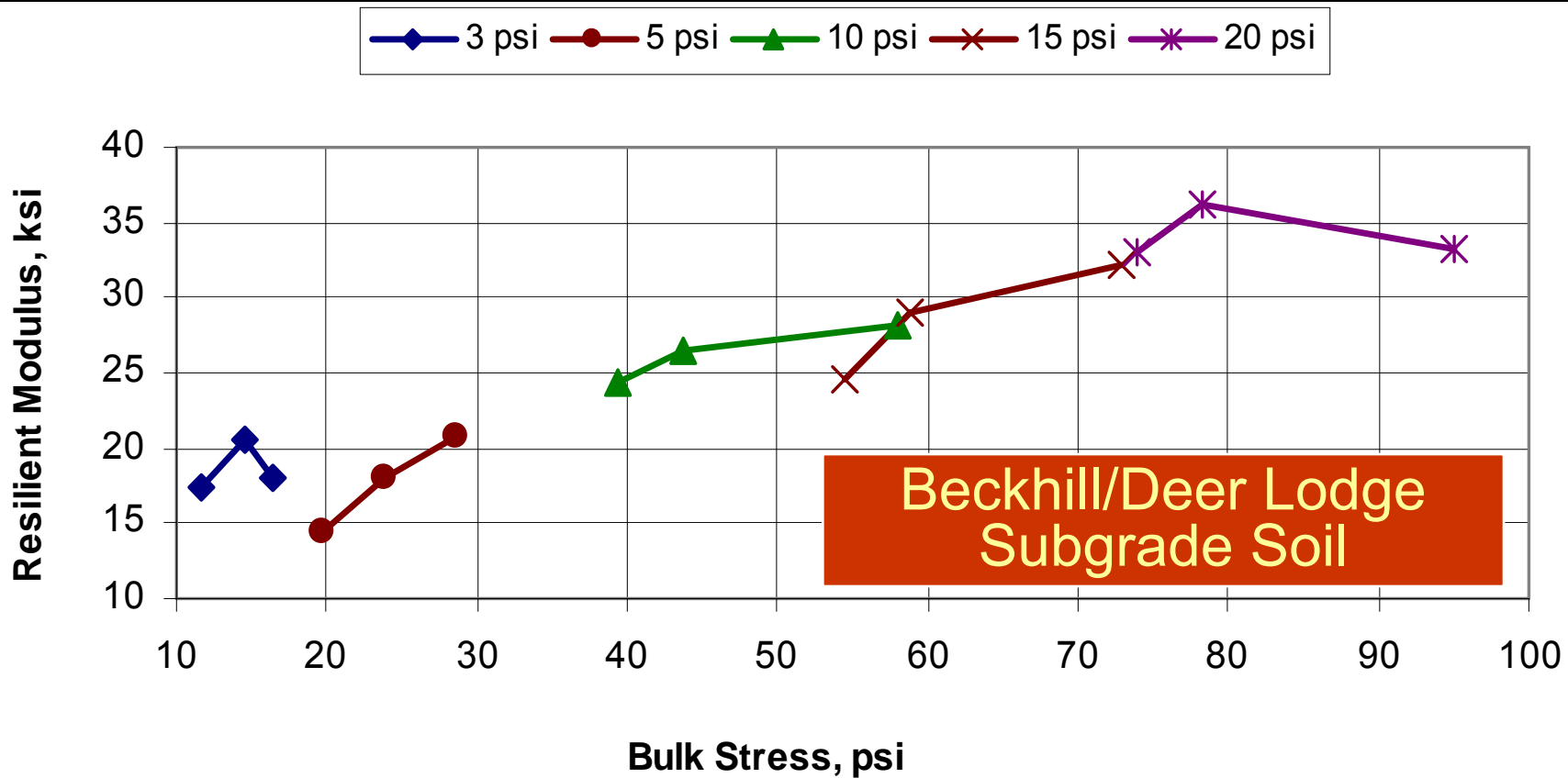
Resilient Modulus of Unbound Materials & Soils



Default values versus laboratory measured values



Resilient Modulus of Unbound Materials & Soils





Conversion Factors for Backcalculated Modulus Values



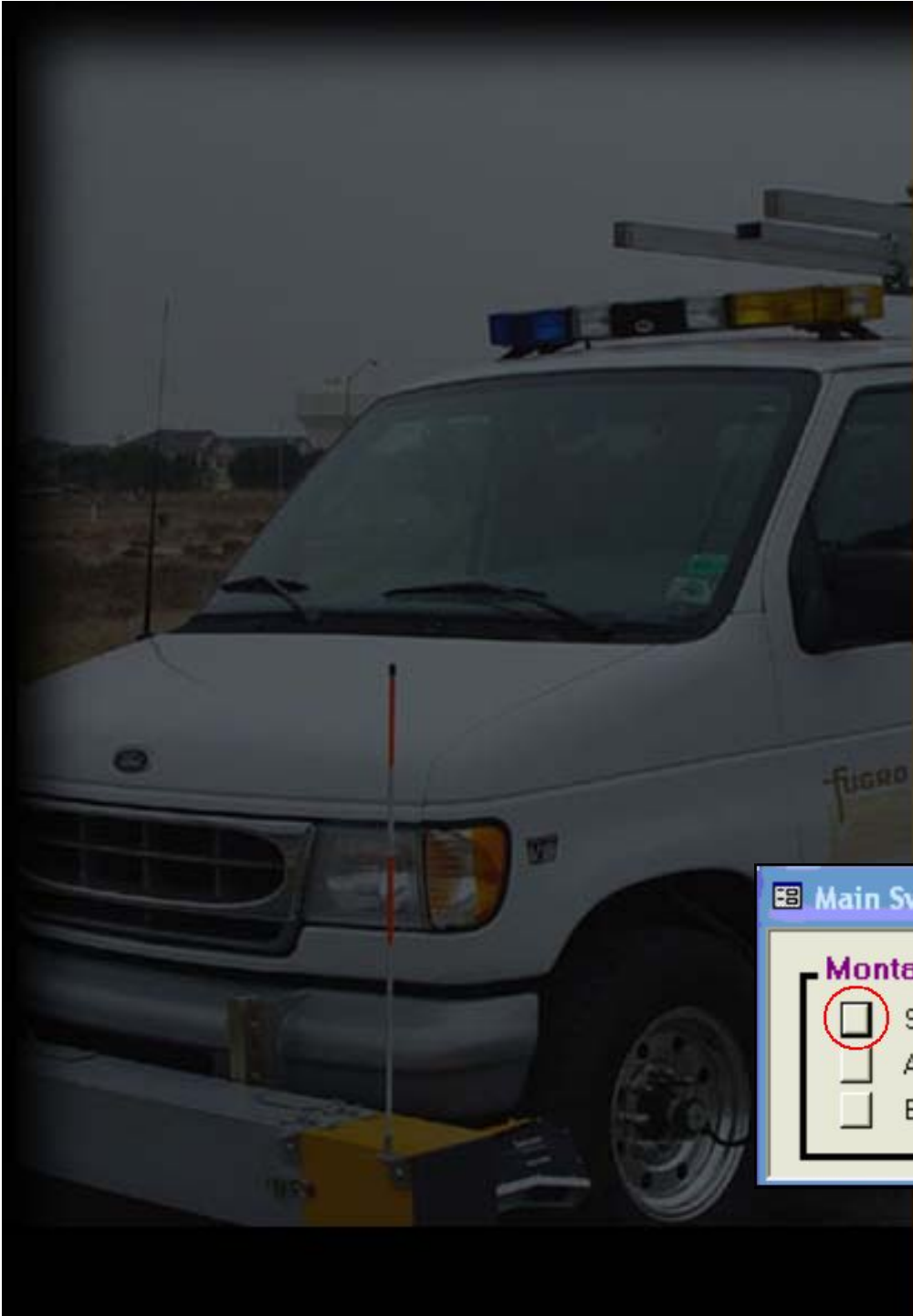
Layer & Material Type	Layer Description	Adjustment Factor
Subgrade Soil/Foundation	Soil Under a CAM without granular base	1.00
	Soil under a CAM with a granular base	0.50
	Soil under flexible pavement with a granular base	0.50
Aggregate Base Layers	Granular base under a CAM layer	0.75
	Granular base under an HMA surface or base	0.60
CAM Layers	Cement treated aggregate	1.50
HMA Layers	Temperature = 41F	0.90
	Temperature = 77F	0.60
	Temperature = 104F	0.50



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Database

Main Switchboard

Montana DOT

- Section Detail
- Append Tables
- Exit Application



Calibration/Validation Database



- ✦ Incorporates pavement related data from 93 LTPP sections (MT, adjacent States, and Provinces)
- ✦ 13 Non-LTPP sections
- ✦ Database is relational-linked





Pavement Data Includes



- ✦ Section identification and layer data
- ✦ Pavement materials data
- ✦ Traffic data
- ✦ Performance data

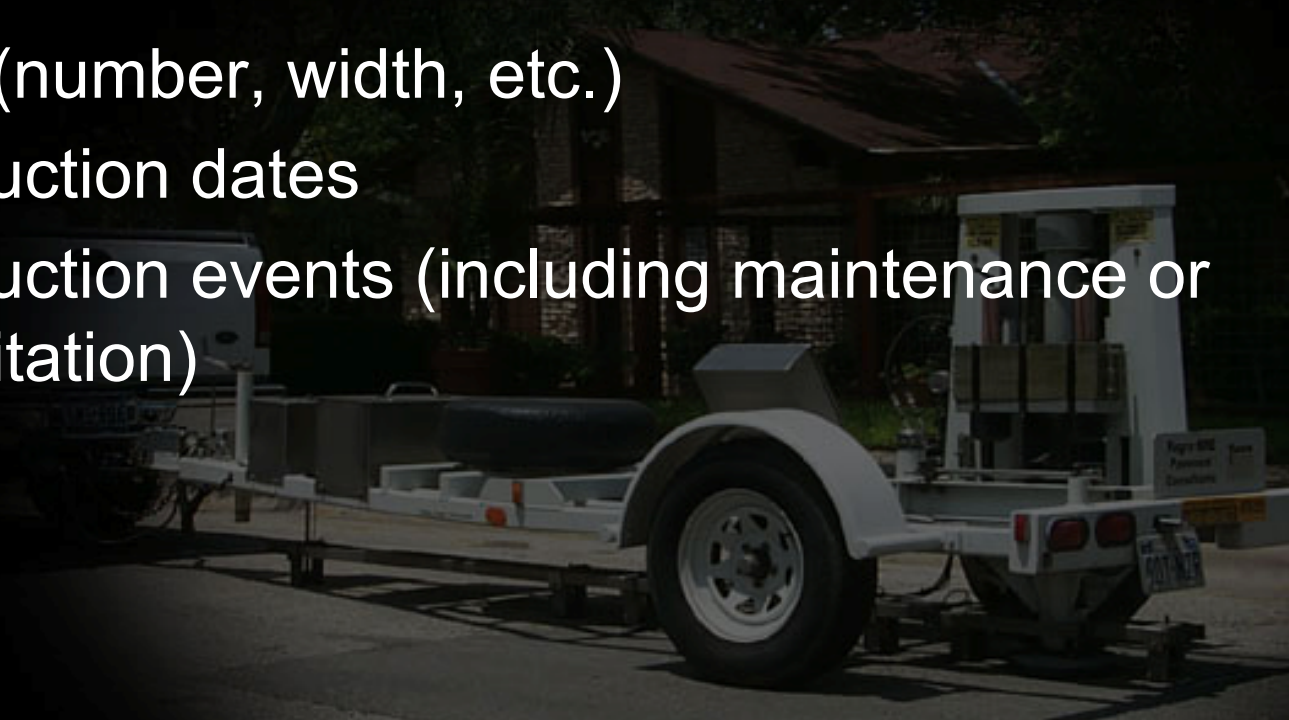




Section Information



- ✦ Contains details regarding test sections such as:
 - Location
 - Lanes (number, width, etc.)
 - Construction dates
 - Construction events (including maintenance or rehabilitation)





Pavement Materials Data



✦ Includes test information for:

- HMA materials (aggregate, binder)
- Unbound materials (base, subbase, and subgrade)
- Depth to water table





Pavement Performance Data



- ✦ Deflection
 - Raw deflection data
 - Backcalculated layer moduli
- ✦ Longitudinal profile data
- ✦ Distress data (cracking)
- ✦ Rutting data





Traffic Data



- ✦ Equivalent Single Axle Loading (ESAL)
- ✦ Axle load spectra (Automated Vehicle Classification and Weigh-in-Motion)

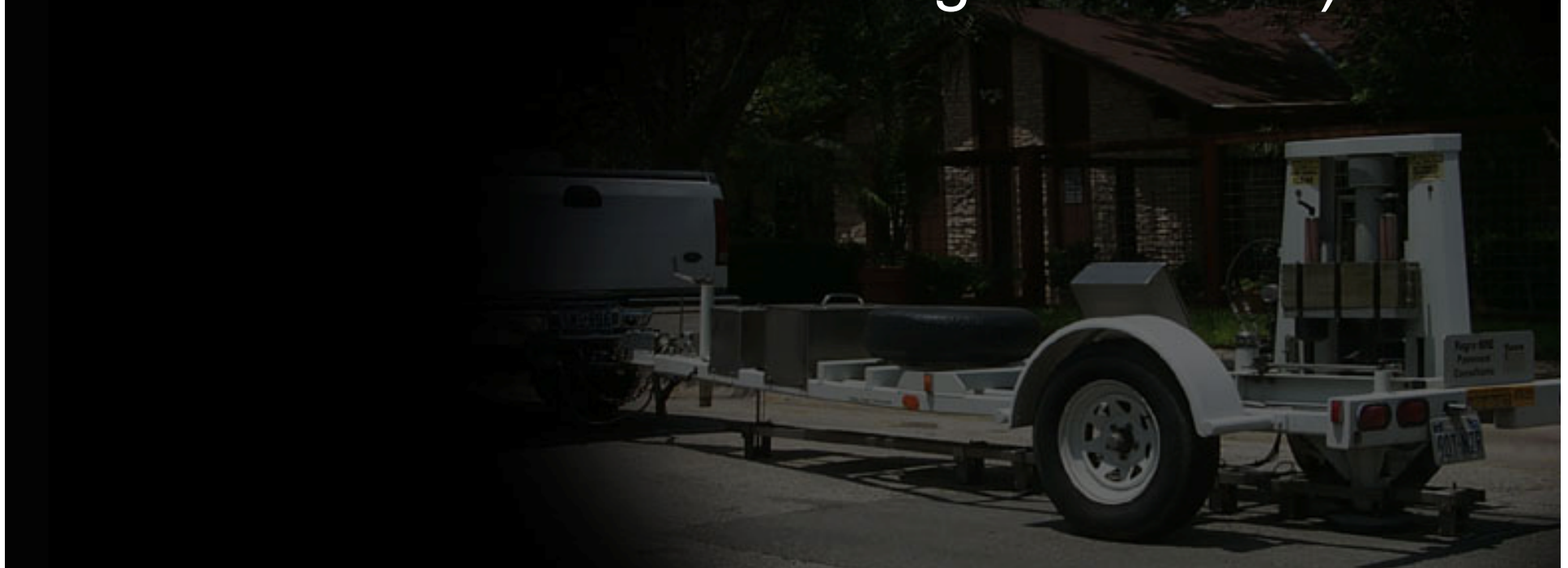




Table Structure/ Database Schema



- ✦ Details contained in Appendix B and D of Volume II of Final Report
- ✦ Examples follow:



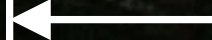


Section Information



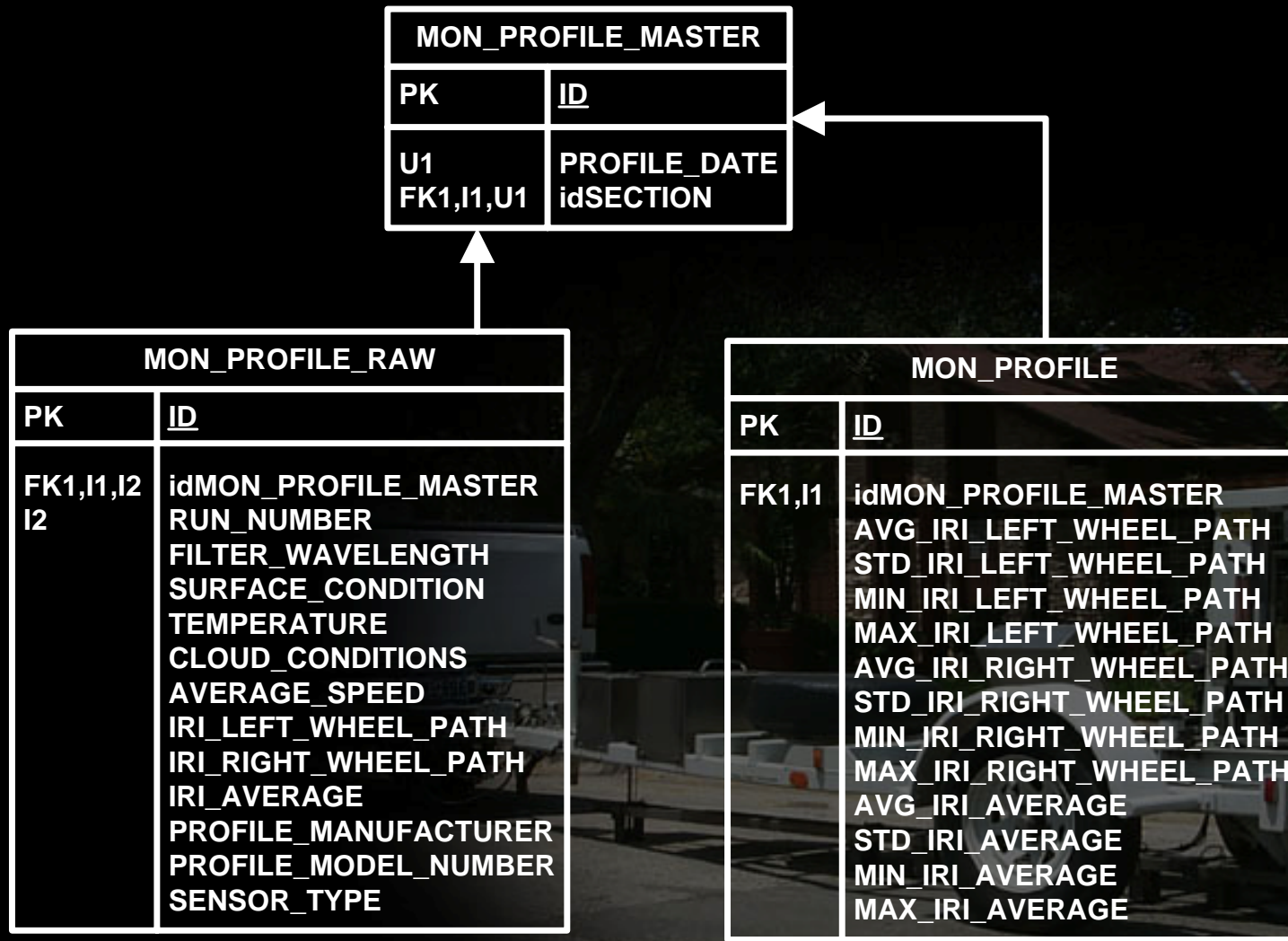
SECTION	
PK	ID
U1	STATE_CODE
U1	SHRP_ID
	HIGHWAY
	DIRECTION_OF_TRAVEL
	TOT_LANES
	LANE_NUMBER
	FUNC_CLASS
	TRAFFIC_OPEN_DATE
	COUNTY
	LATITUDE
	LONGITUDE
	ELEVATION
	LOCATION_INFO
	LANE_WIDTH
	SHOULDER_TYPE
	SHOULDER_WIDTH
	ACCESS_CONTROL
	MEDIAN
	DESCRIPTION

SECTION_EVENTS	
PK	ID
FK1,I1,U1	idSECTION
U1	CONSTRUCTION_NO
	EXP_NO
	TERMINAL_SI
	STRUCTURAL_NO
	PAVE_TYPE
	RIGID_DEPTH_ESAL
	CN_ASSIGN_DATE
	CN_CHANGE_REASON
	DATE_EARTHWORK



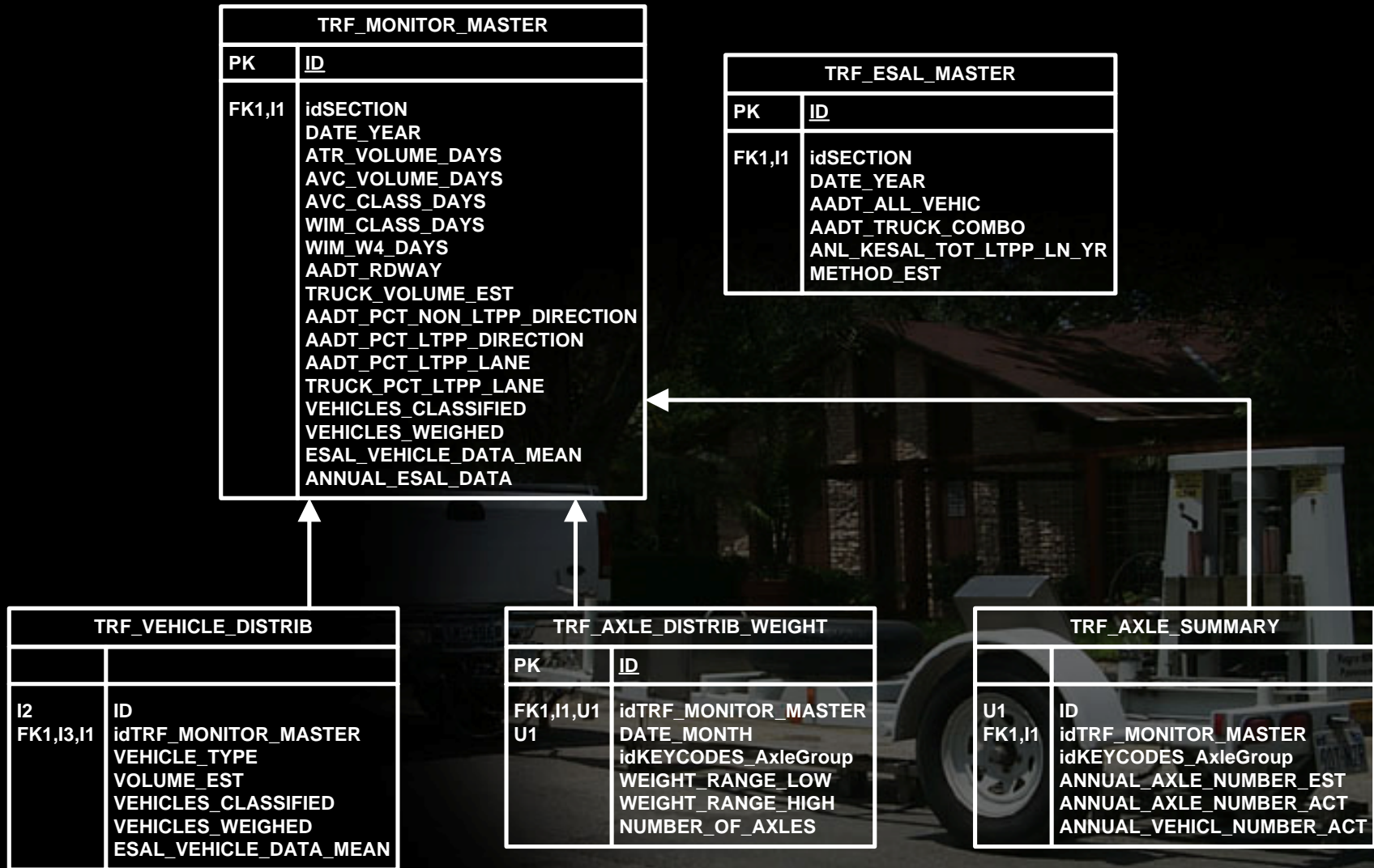


Profile





Traffic





Rutting



MON_RUT_MASTER	
PK	ID
FK1,11	idSECTION TEST_DATE STATION WIRELINE_RUT_LEFT_WHEELPATH WIRELINE_RUT_RIGHT_WHEELPATH HMA_RUT_LWP HMA_RUT_RWP BASE_RUT_LWP BASE_RUT_RWP SUBGRADE_RUT_LWP SUBGRADE_RUT_RWP

MON_RUT_RAW	
PK	ID
FK1,11	idMON_RUT_MASTER STATION DEPTH

MON_RUT_RAW_DISTANCE	
PK	ID
FK1,11	idMON_RUT_RAW DISTANCE DEPTH_RUT

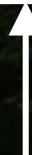


Distress



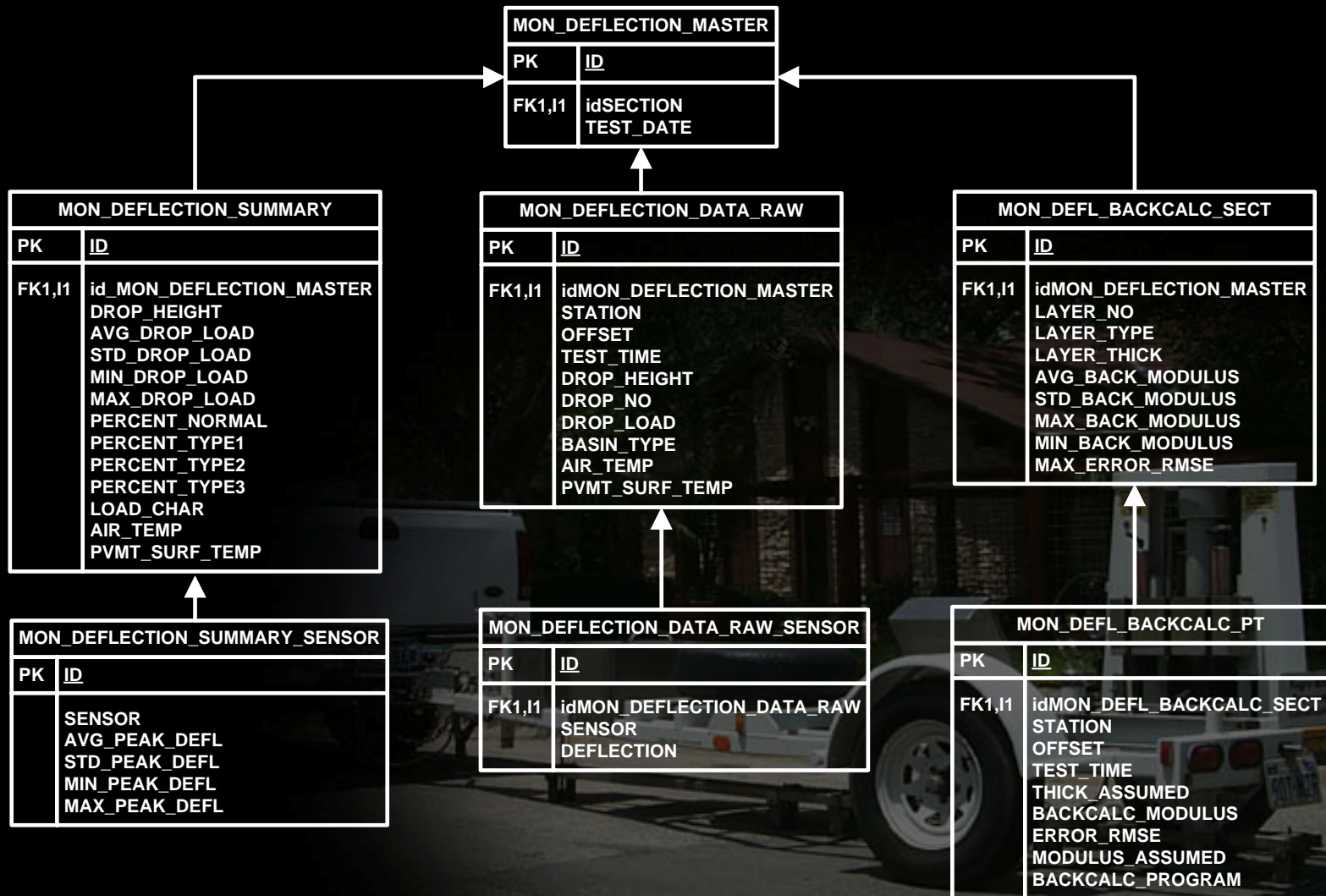
MON_DISTRESS_MASTER	
PK	<u>ID</u>
FK1,1	idSECTION SURVEY_DATE PERCENT_FATIGUE CRACK_ORIGIN THERMAL_CRACK AVG_WIRELINE_RUT_DEPTH STD_WIRELINE_RUT_DEPTH STUDED_TIRE_WEAR OTHER

MON_DISTRESS_RAW	
PK	<u>ID</u>
FK1,1	idMON_DISTRESS_MASTER idKEYCODES_Distress idKEYCODES_Severity Value
I2	Number idKEYCODES_Unit idKEYCODES_Wheelpath idKEYCODES_Sealed idKEYCODES_Reflective





Deflection





Populating the Database- LTPP Data



1. Use the current LTPP data release to update the database with the latest information for LTPP sections
2. A set of queries has been created to add new data and delete existing data for LTPP sections (detailed instructions are provided in Volume II of the Final Report)



Populating the Database- LTPP Data



3. Store the LTPP data tables from the new release and re-establish links to these tables with the MDT calibration/validation database
4. Use queries to delete old data and update the MDT calibration/validation database with the latest data in the most recent LTPP data release



Populating the Database- Non-LTPP Data



- ✦ Accomplished manually using forms and tables
- ✦ Detailed instructions in Volume II of Final Report





Populating the Database- Non-LTPP Data



- ◆ Populate the data tables in the following order:

Sections



Section Events



Master



Data



Presentation Outline



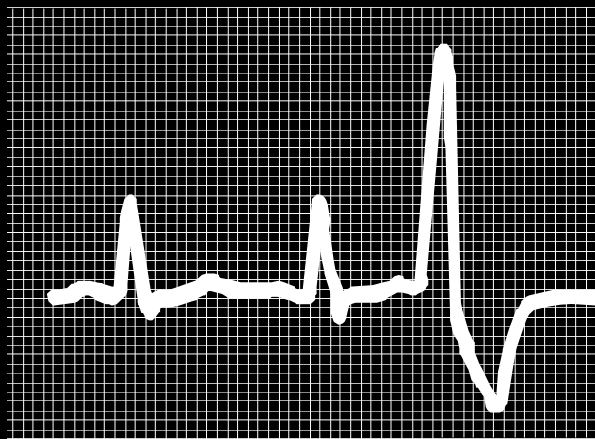
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Calibration of Distress Transfer Functions



Pavement Response



- Stresses
- Strains
- Deflections



Distress

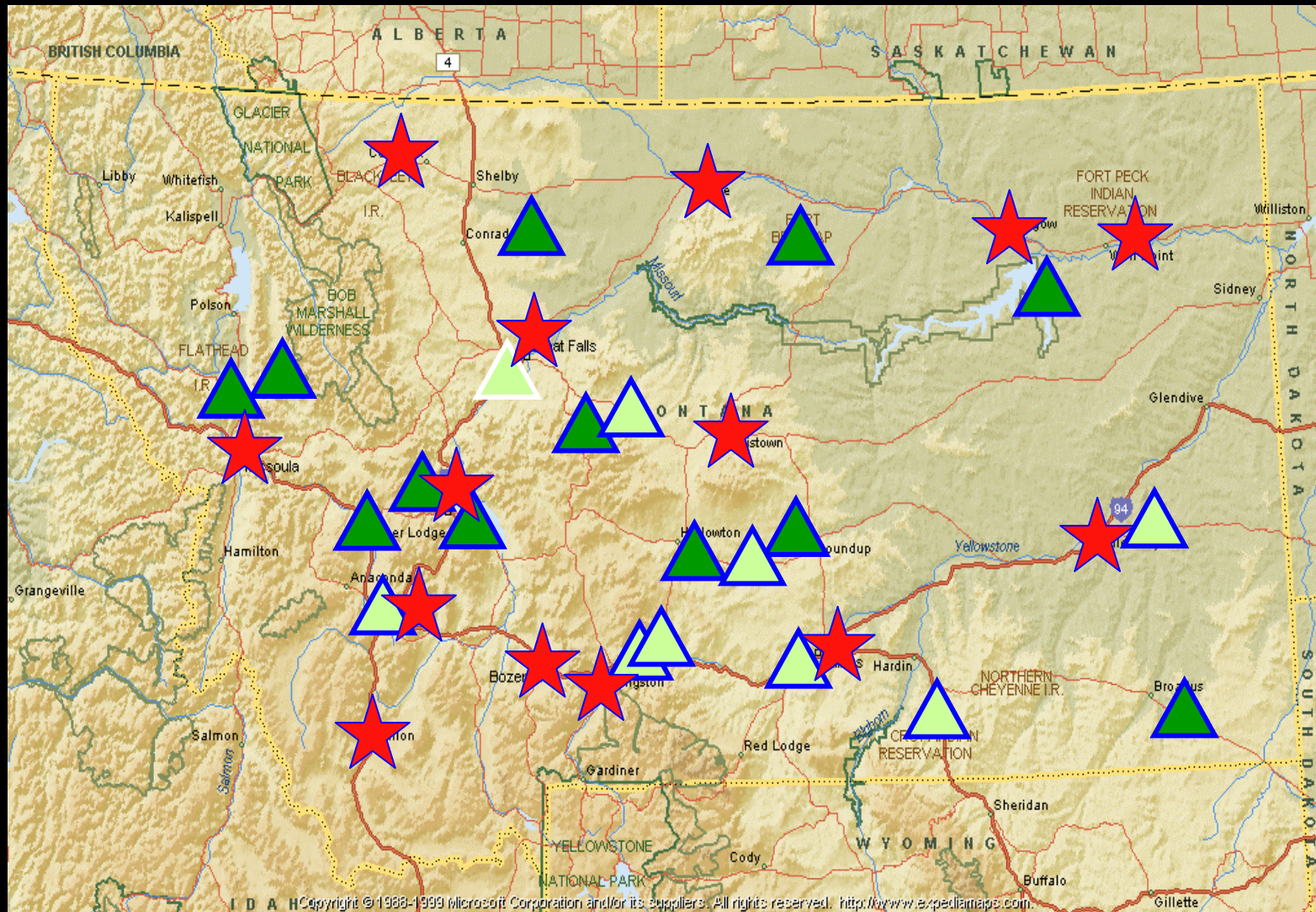


Calibration is a key

- Fatigue Cracks
- Rut Depths
- Transverse Cracks



▲ Test Sections ★ Weather Stations



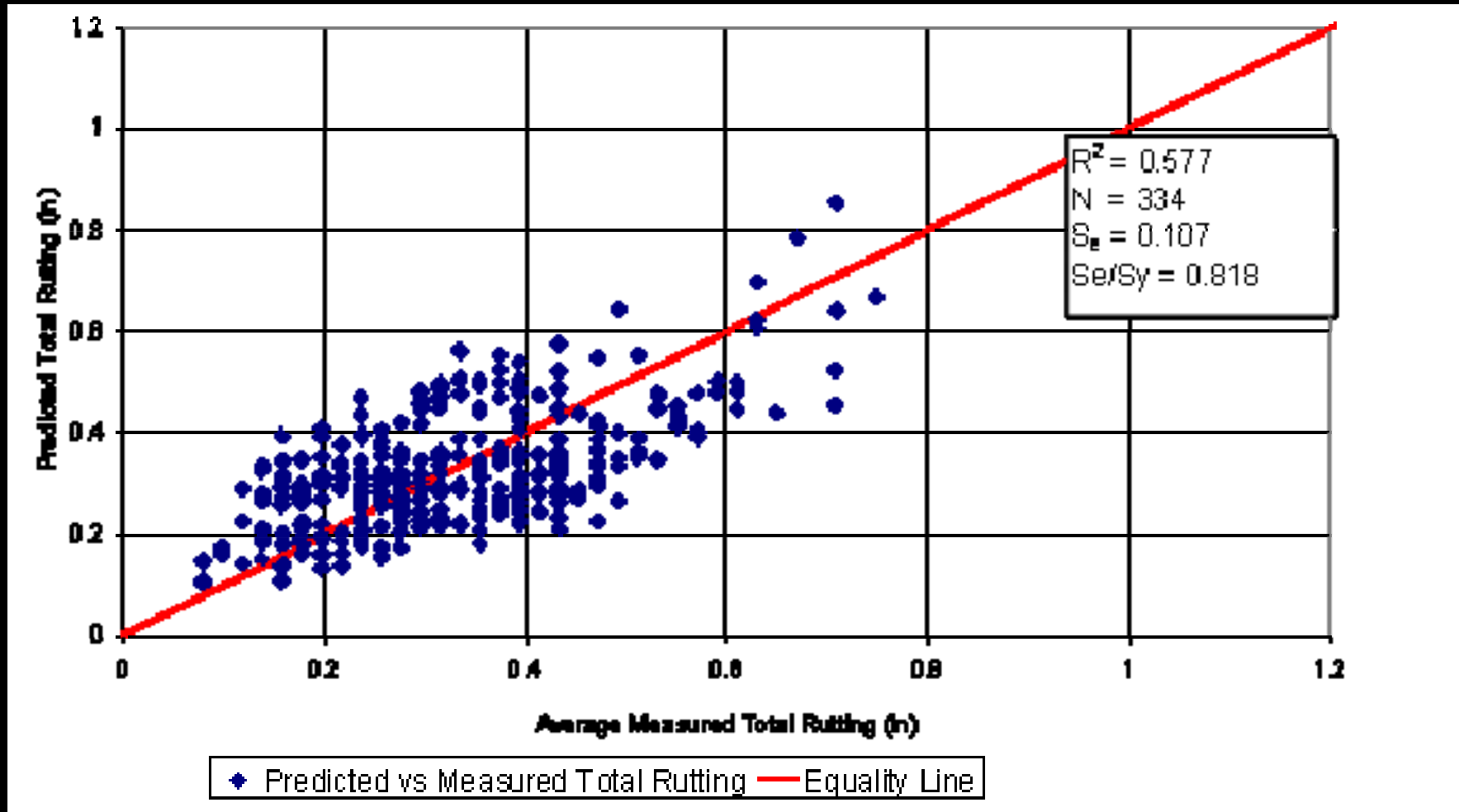


Rut Depth Prediction Model

- ◆ Unbound Layers
- ◆ HMA Layers

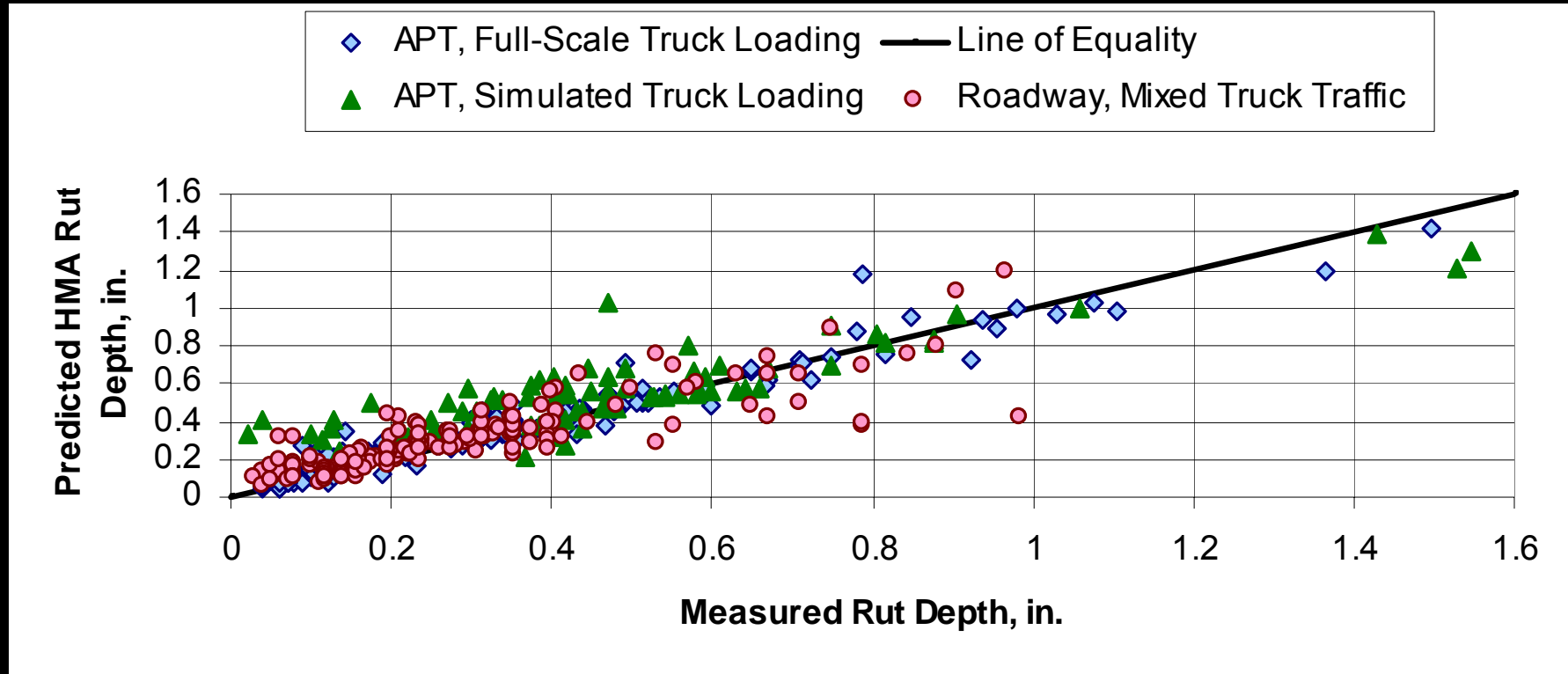


Total Rutting: NCHRP 1-40D





HMA Rutting: NCHRP 1-40B



# of Points	Bias	RMSE	S_e/S_y	R^2
418	0.0303	0.1170	0.439	0.837



Tools Menu, Drop-Down Box



The screenshot shows the 'Untitled - Mechanistic Empirical Pavement Design Guide' application window. The 'Tools' menu is open, displaying options such as 'Options', 'Expert Mode', 'Set Default Mode', 'Calibration Settings', 'Special Axle Configuration', 'Import TrafLoad', 'Additional Programs', 'Batch File', and 'Update Calibration Settings'. A sub-menu is open under 'Calibration Settings', listing 'Flexible - New', 'Flexible - Rehab', 'Rigid - New', 'Rigid - Restore', 'Rigid - Bonded', and 'Rigid - Unbonded'. The main window content features a large graphic with the text 'M-E PDG Mechanistic-Empirical Pavement Design Guide'. Below the graphic, a disclaimer states: 'This software is for review only and should not be used for design. This software was developed under NCHRP 1-37A and 1-40D. Distribution of this software must be approved by NCHRP.' The software is credited to 'APPLIED RESEARCH ASSOCIATES, INC TRANSPORTATION ASU'. At the bottom of the window, it indicates 'Version 1.000' and 'Last Build: April 8, 2007'. The Windows taskbar at the bottom shows the start button and several open applications, including 'FINAL_Fug...', 'Presentatio...', 'DRAFT_Mo...', 'Montana Pr...', 'Slides_Mod...', 'VOLUME_I...', and 'Untitled - M...'. The system clock shows '4:31 AM'.



Rutting, Unbound Layers



Distress Model Calibration Settings - Flexible New

AC Fatigue | AC Rutting | Thermal Fracture | CSM Fatigue | **Subgrade Rutting** | AC Cracking | CSM Cracking | IRI

$$\delta_a(N) = \beta_{s_1} \epsilon_v h \left(\frac{\epsilon_o}{\epsilon_\gamma} \right) e^{-\left(\frac{p}{N} \right)^\beta}$$

δ_a = permanent deformation for the layer
 N = number of repetitions
 ϵ_v = average vertical strain (in/in)
 h = thickness of the layer (in)
 ϵ_o, β, ρ = material properties
 ϵ_γ = resilient strain (in/in)

Special Analysis
 National Calibration
 State/Regional Calibration
 Typical Agency Values

0.20

Granular: k1: 2.03 Bs1: 1

Fine-grain: k1: 1.35 Bs1: 1

Standard Deviation (BASERUT): 0.1477*POWER(BASERUT,0.6711)+0.001

Standard Deviation (SUBRUT): 0.1235*POWER(SUBRUT,0.5012)+0.001

0.20

Rutting in Unbound Layers & Subgrade

OK Cancel



HMA Rutting



Distress Model Calibration Settings - Flexible New

AC Fatigue | **AC Rutting** | Thermal Fracture | CSM Fatigue | Subgrade Rutting | AC Cracking | CSM Cracking | IRI

$$\frac{\epsilon_p}{\epsilon_r} = k_z \beta_{r1} 10^{k_1 T} k_2 N^{k_3}$$

$$k_z = (C_1 + C_2 * depth) * 0.328196^{depth}$$

$$C_1 = -0.1039 * H_{ac}^2 + 2.4868 * H_{ac} - 17.342$$

$$C_2 = 0.0172 * H_{ac}^2 - 1.7331 * H_{ac} + 27.428$$

Where:
Hac = total AC thickness (in)

HMA Rutting

NCHRP 1-37A

- Special Analysis
- Nationally Calibration
- State/Regional Calibration
- Typical Agency Values**

K1: -3.35412 Br1:

K2: 1.5606 Br2:

K3: 0.4791 Br3:

Standard Deviation: 0.247
 Standard Deviation (Rutting (RUT)): 0.247 * POWER(RUT, 0.8026) + 0.001

OK Cancel

Based on Volumetric Properties



Calibration Refinement

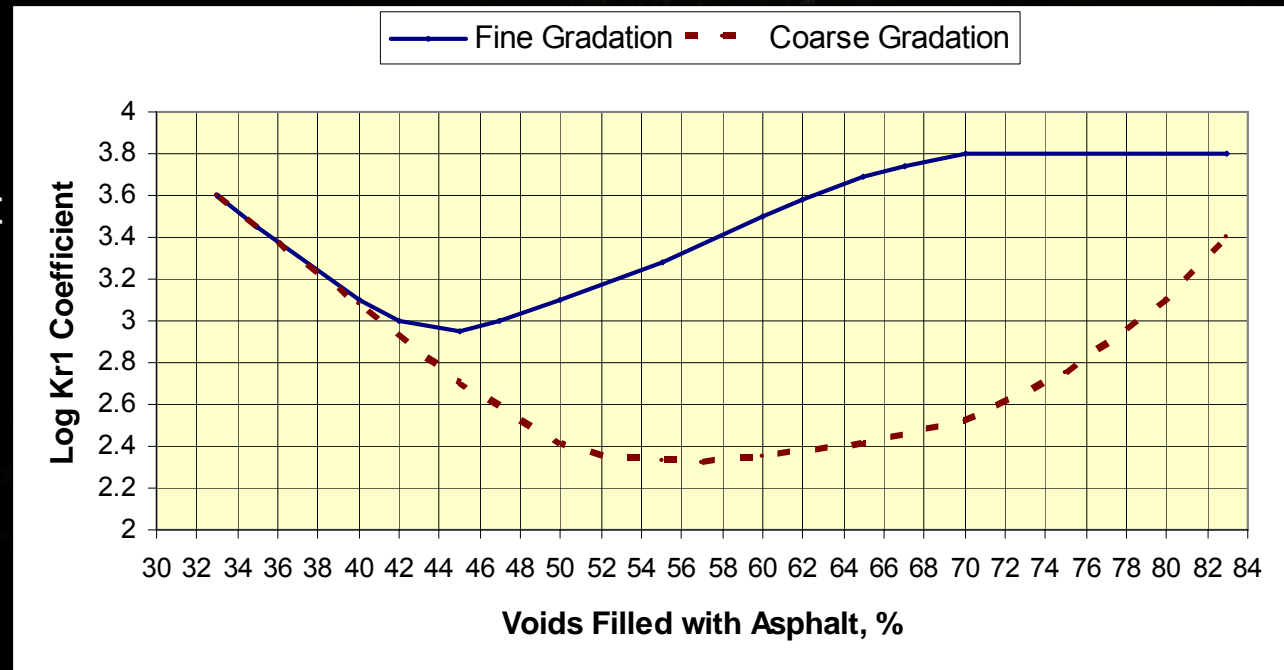


Determine the k_{r1} coefficient

$$k_{r1} = \text{Log} \left[0.0015093 (K_{r1}) (V_a)^{0.5213} (V_{be})^{1.0057} \right] - 3.4488$$

V_a = Air Voids, %

V_{be} = Effective asphalt content by volume, %





Calibration Refinement



Determine the k_{r2} , temperature exponent

$$k_{r2} = 1.5606 \left(\frac{V_a}{V_{a(Design)}} \right)^{0.25} \left(\frac{P_b}{P_{b(Design)}} \right)^{1.25} (F_{Index}) (C_{Index})$$

$V_{a(Design)}$

= Design air void level to determine asphalt content, %

P_b

= Asphalt content by weight, %

$P_{b(Design)}$

= Design asphalt content by weight, %

F_{Index}

= Fine aggregate angularity index

C_{Index}

= Coarse aggregate angularity index



Calibration Refinement



F_{Index}		
Gradation; Restricted Zone	Fine Aggregate Angularity	
	<45	>45
Dense, External	1.00	0.90
Dense, Through	1.05	1.00

C_{Index}					
Gradation	Percent Crushed with Two Faces				
	0	25	50	75	100
Well-Graded	1.1	1.05	1.0	1.0	0.9
Gap-Graded	1.2	1.1	1.05	1.0	0.9



Calibration Refinement



Determine the k_{r3} , number of load applications exponent

$$k_{r3} = 0.4791(K_{r3}) \left(\frac{P_b}{P_{b(Design)}} \right)$$

Gradation	G-Index	K_{r3}
Fine-Graded	<20	0.40
Coarse-Graded	20 to 40	0.70
Coarse-Graded	>40	0.80



Gradation Index



$$GI = \sum_{i=\#3/8}^{\#50} \left| P_i - P_{i(0.45)} \right|$$

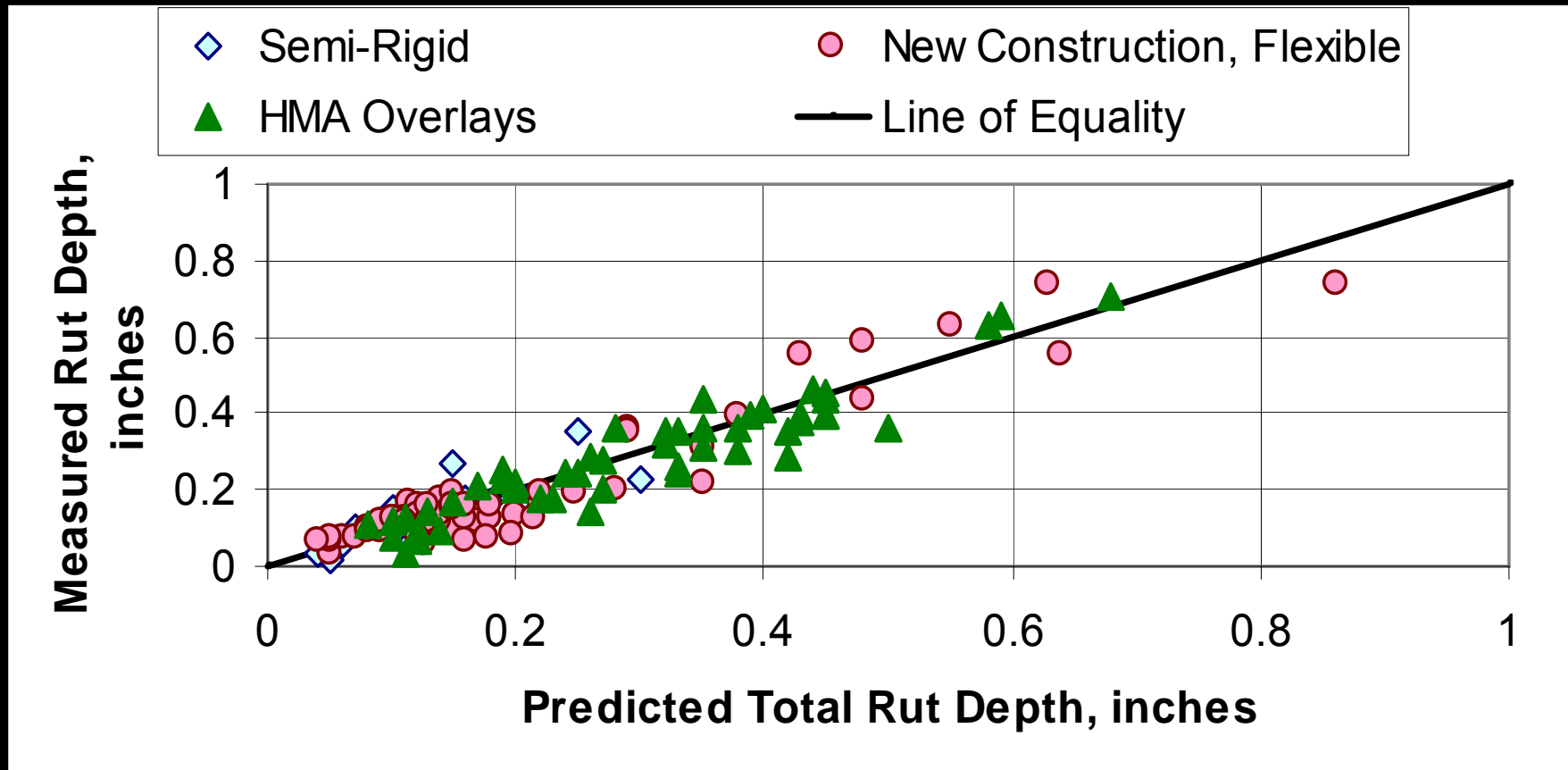
GI = Gradation Index

P_i = Percent passing sieve size i , %

$P_{i(0.45)}$ = Percent passing sieve size i for the FHWA 0.45 maximum density line

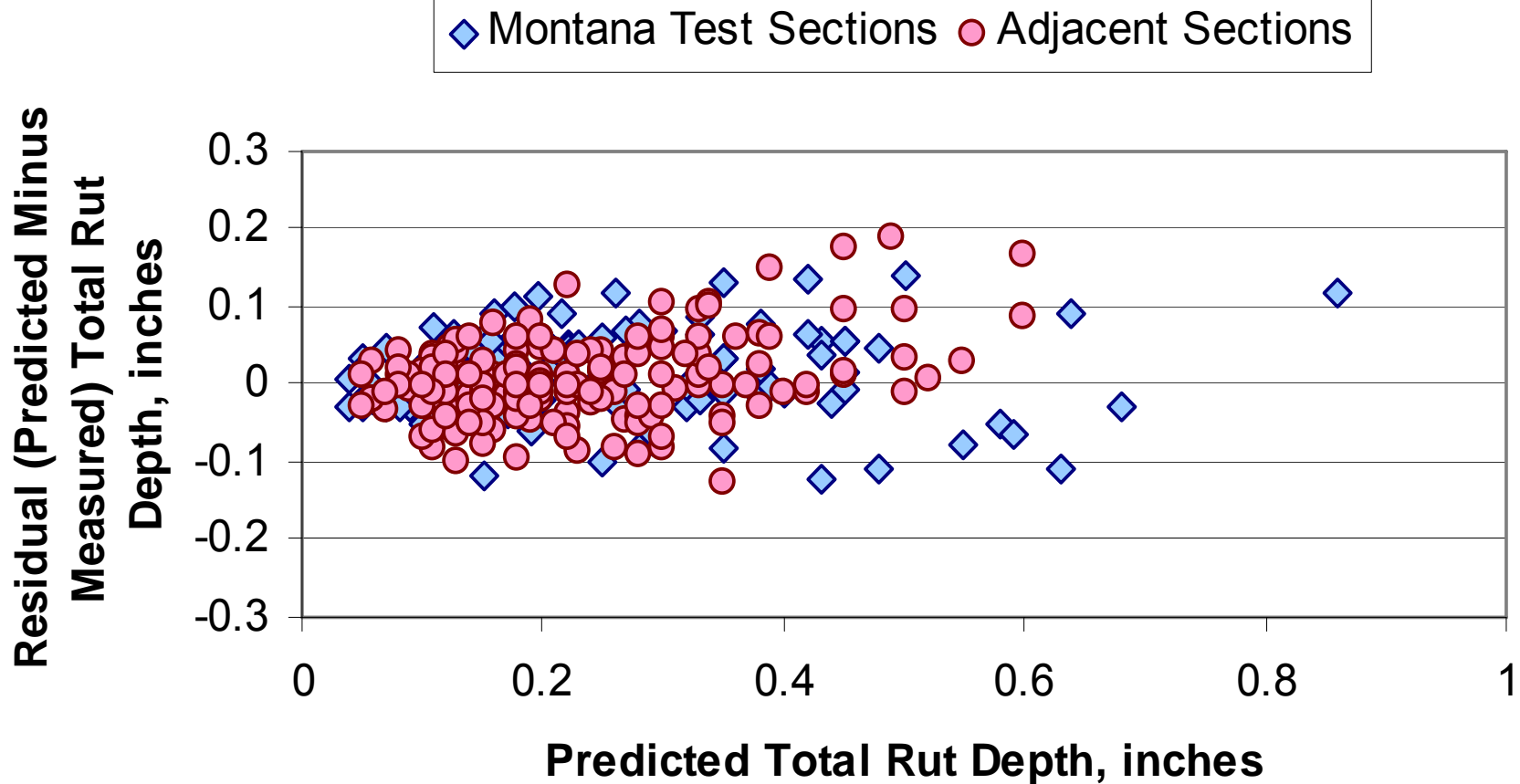


Total Rutting





Total Rutting





MDT Calibration Project: Total Rutting



Type of Pavement		No. of Points	Bias, in.	Standard Error, in.	RMSE, in.	S_e/S_y
MT Sites	New Construction, Flexible Pavts	67	0.0069	0.0536	0.1098	0.342
	Semi-Rigid Pavts	18	-0.0103	0.0457	0.0789	0.662
	HMA Overlays of Flexible Pavts	50	0.0126	0.0520	0.0937	0.359
All Sites	New Construction, Flexible Pavts	72	0.0108	0.0539	0.0988	0.418
	Semi-Rigid Pavts	32	-0.0023	0.0472	0.0833	0.384
	HMA Overlays, All Type Pavts	75	0.0058	0.0494	0.0941	0.4927

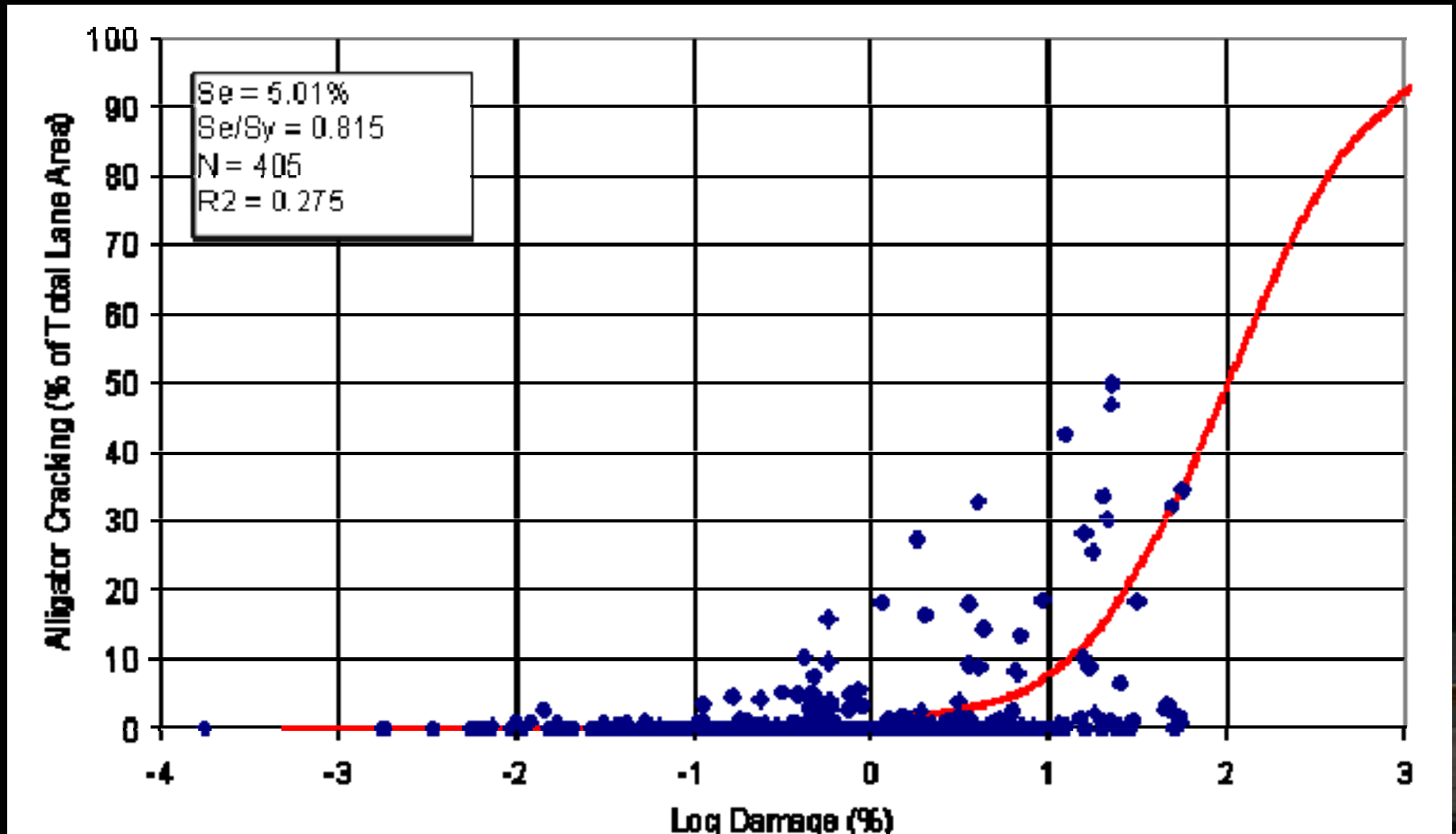


Load Related Cracking Model

- ◆ Surface Initiated Cracks - LCWP
- ◆ Bottom Initiated Cracks – Area Cracking

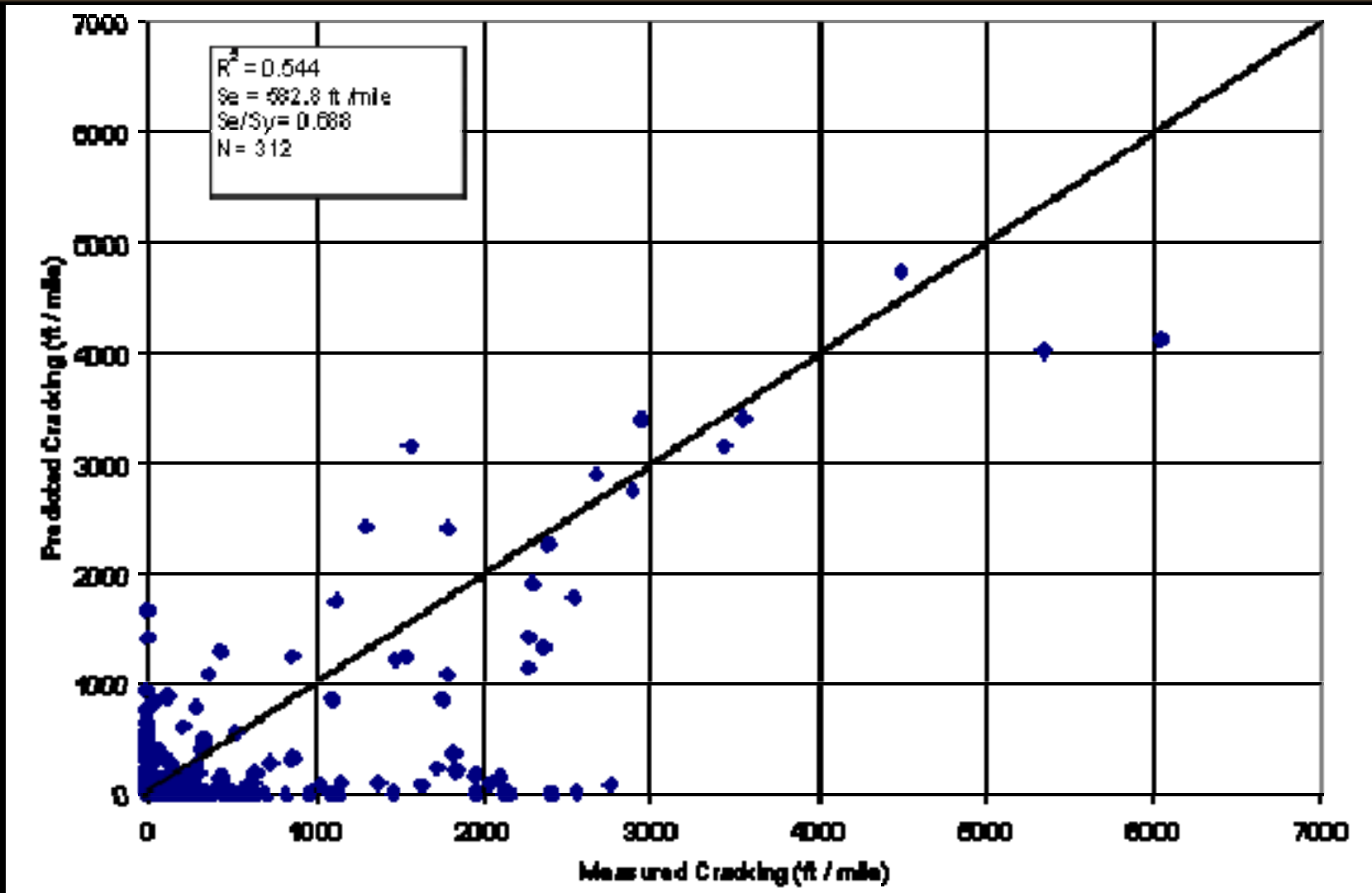


Alligator Cracking – HMA: NCHRP 1-40D



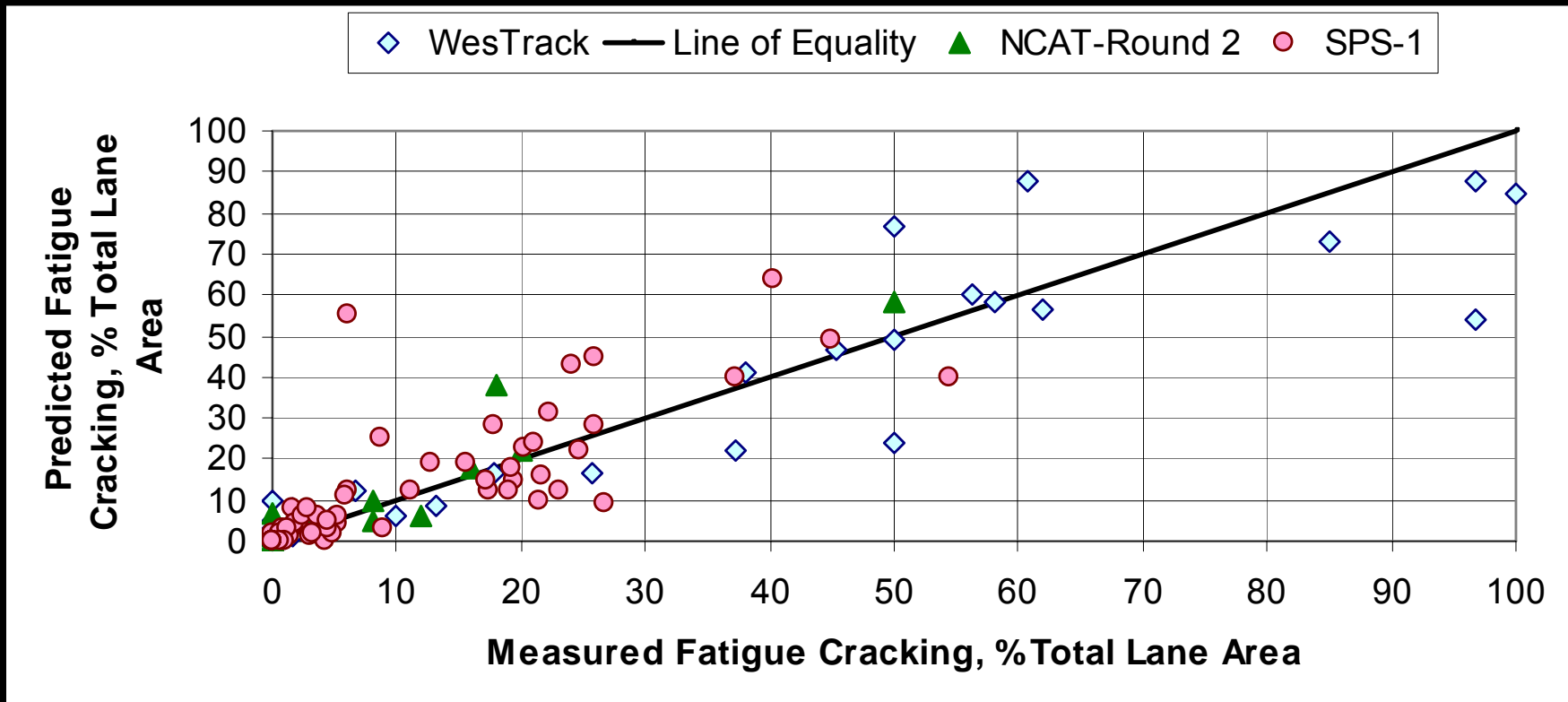


Longitudinal Cracking – HMA: NCHRP 1-40D





Alligator Cracking – HMA: NCHRP 1-40B



Bias	RMSE	S_e/S_y	R^2
-0.616	7.84	0.409	0.841



Fatigue Cracking



Distress Model Calibration Settings - Flexible New

AC Fatigue | AC Rutting | Thermal Fracture | CSM Fatigue | Subgrade Rutting | AC Cracking | CSM Cracking | IRI

$$N_f = 0.00432 * C * \beta \left(\frac{1}{S_t} \right)^{k_1} \left(\frac{1}{E} \right)^{k_2}$$
$$C = 10^{M}$$
$$M = 4.84 \left(\frac{V_o}{V_a + V_o} - 0.69 \right)$$

Special Analysis
 National Calibration
 State/Regional Calibration
 Typical Agency Values

k1: 0.007566 Bf1:
k2: 3.9492 Bf2:
k3: 1.281 Bf3:

Endurance limit for calculation of HMA Fatigue Damage

OK Cancel

Based on Volumetric Properties

Fatigue Cracking



Fatigue Cracking



Distress Model Calibration Settings - Flexible New

AC Fatigue | AC Rutting | Thermal Fracture | CSM Fatigue | Subgrade Rutting | AC Cracking | CSM Cracking | IRI

AC Top Down Cracking

$$FC_{top} = \left(\frac{C_4}{1 + e^{(C_1 - C_2 * \log_{10}(Damage))}} \right) * 10.56$$

C1 (top)

C2 (top)

C3 (top)

C4 (top)

Standard Deviation (TOP):

AC Bottom Up Cracking

$$F.C. = \left(\frac{6000}{1 + e^{(C'_1 * C'_2 - C'_2 * \log_{10}(D * 100))}} \right) * \left(\frac{1}{60} \right)$$
$$C'_2 = -2.40874 - 39.748 * (1 + h_{ac})^{-2.856}$$
$$C'_1 = -2 * C'_2$$

C1 (bottom)

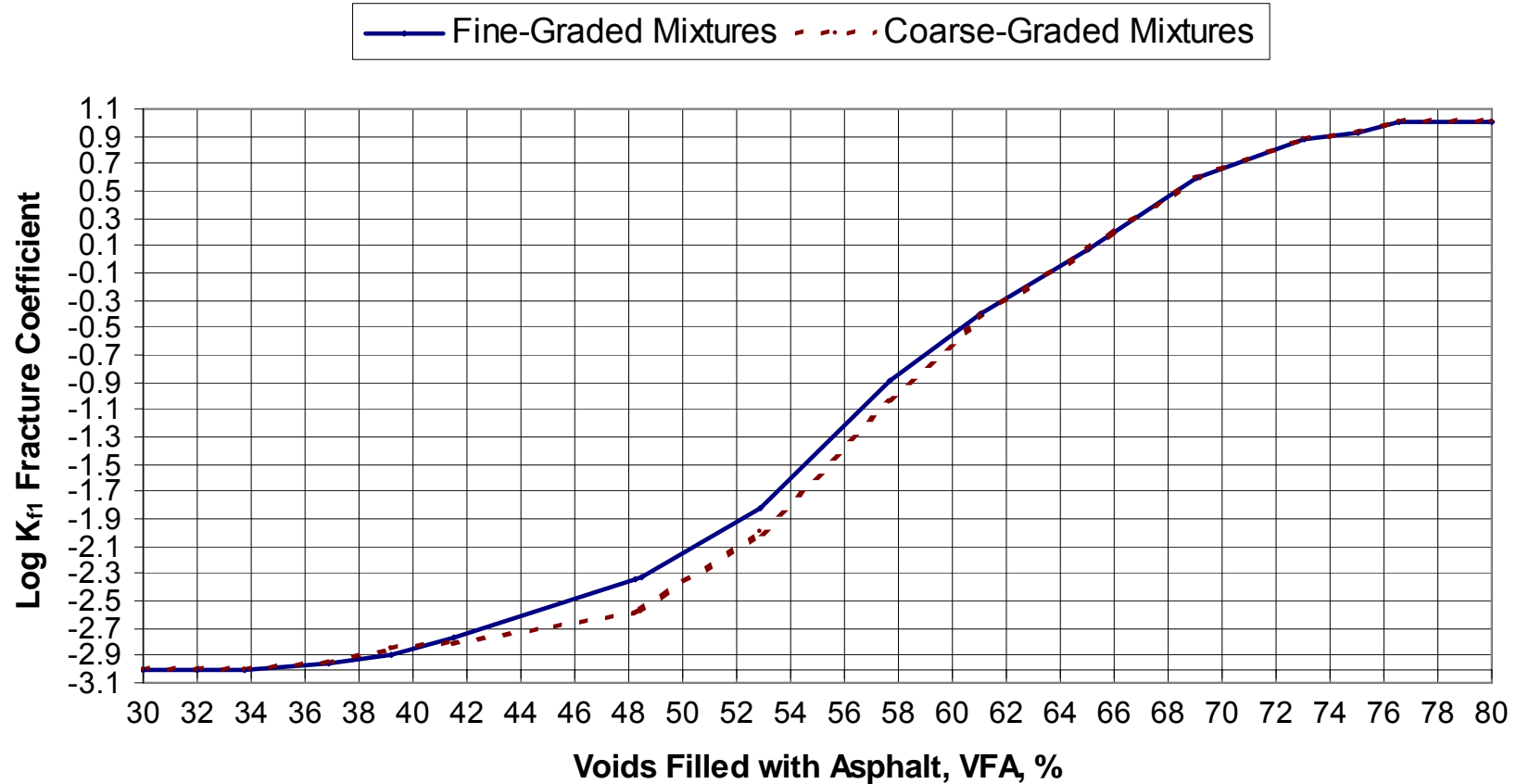
C2 (bottom)

C4 (bottom)

Standard Deviation (BOTTOM):

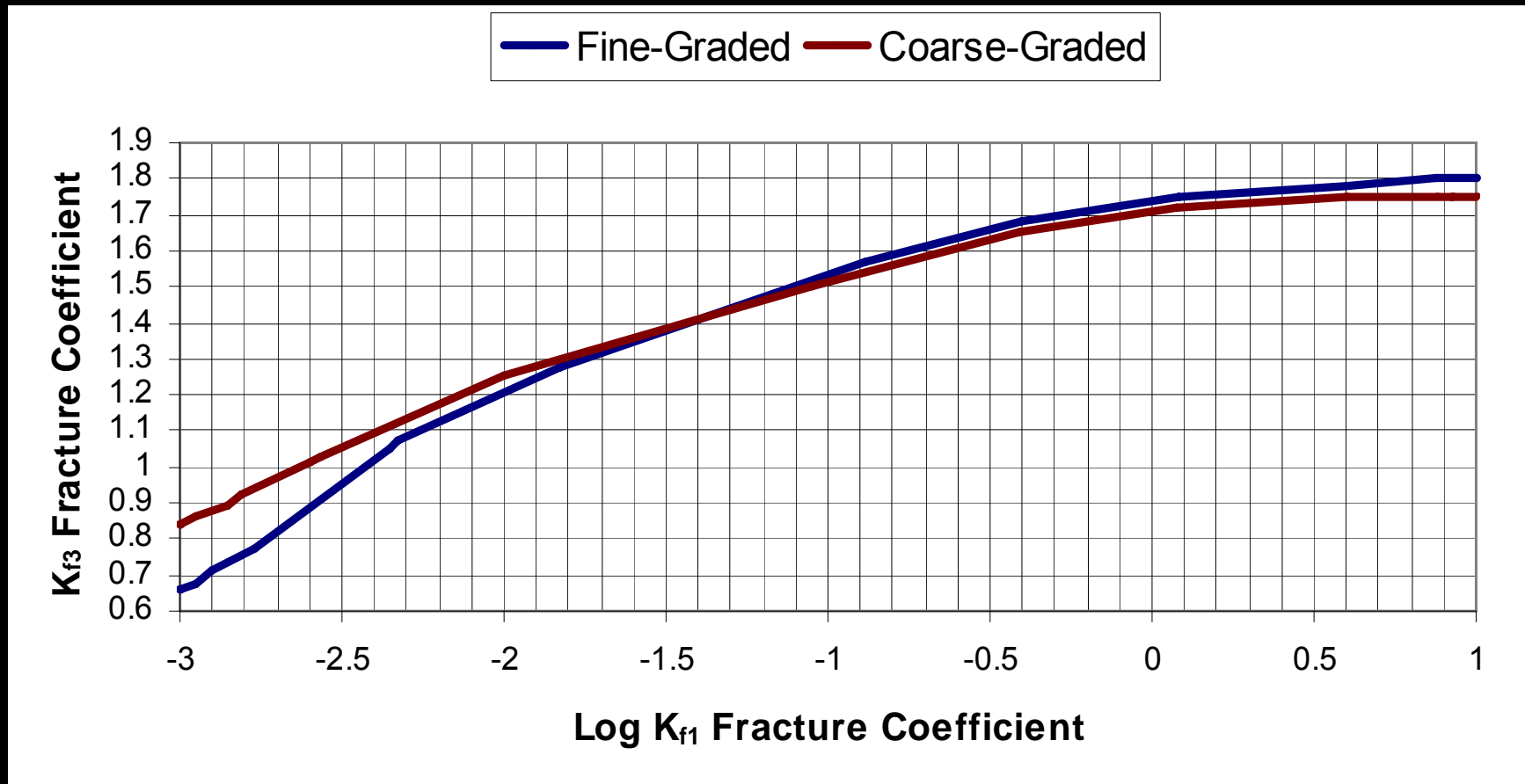


Fatigue Cracking – Mix Calibration Adjustment



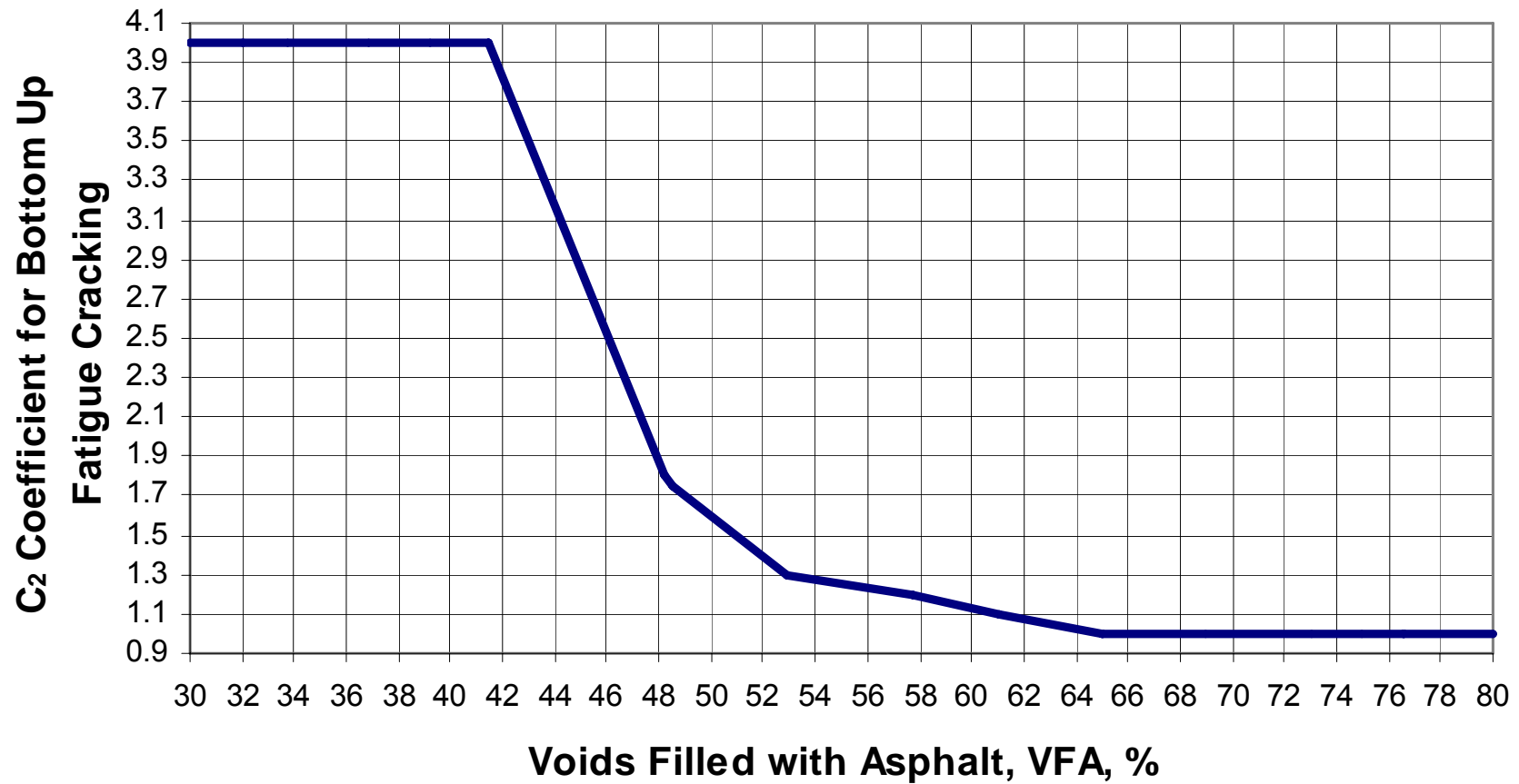


Fatigue Cracking – Mix Calibration Adjustment





Fatigue Cracking – Calibration Refinement Adjustments

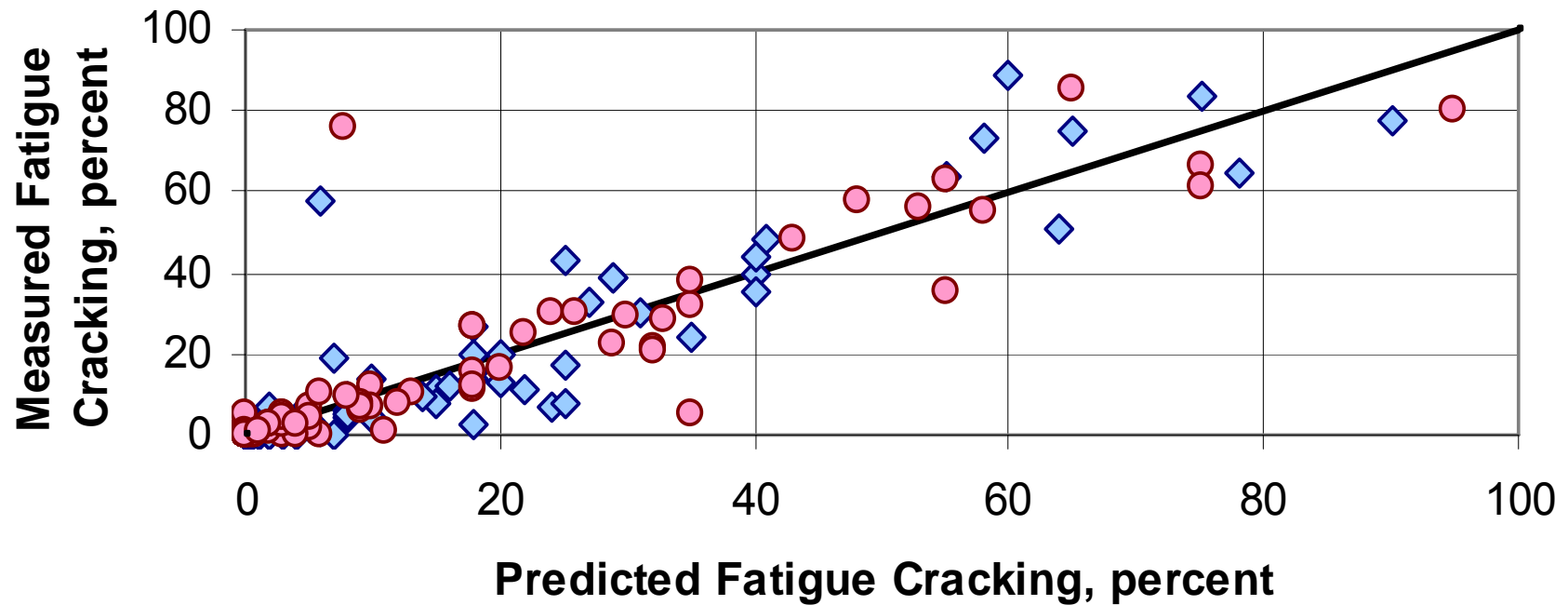




Fatigue Cracking

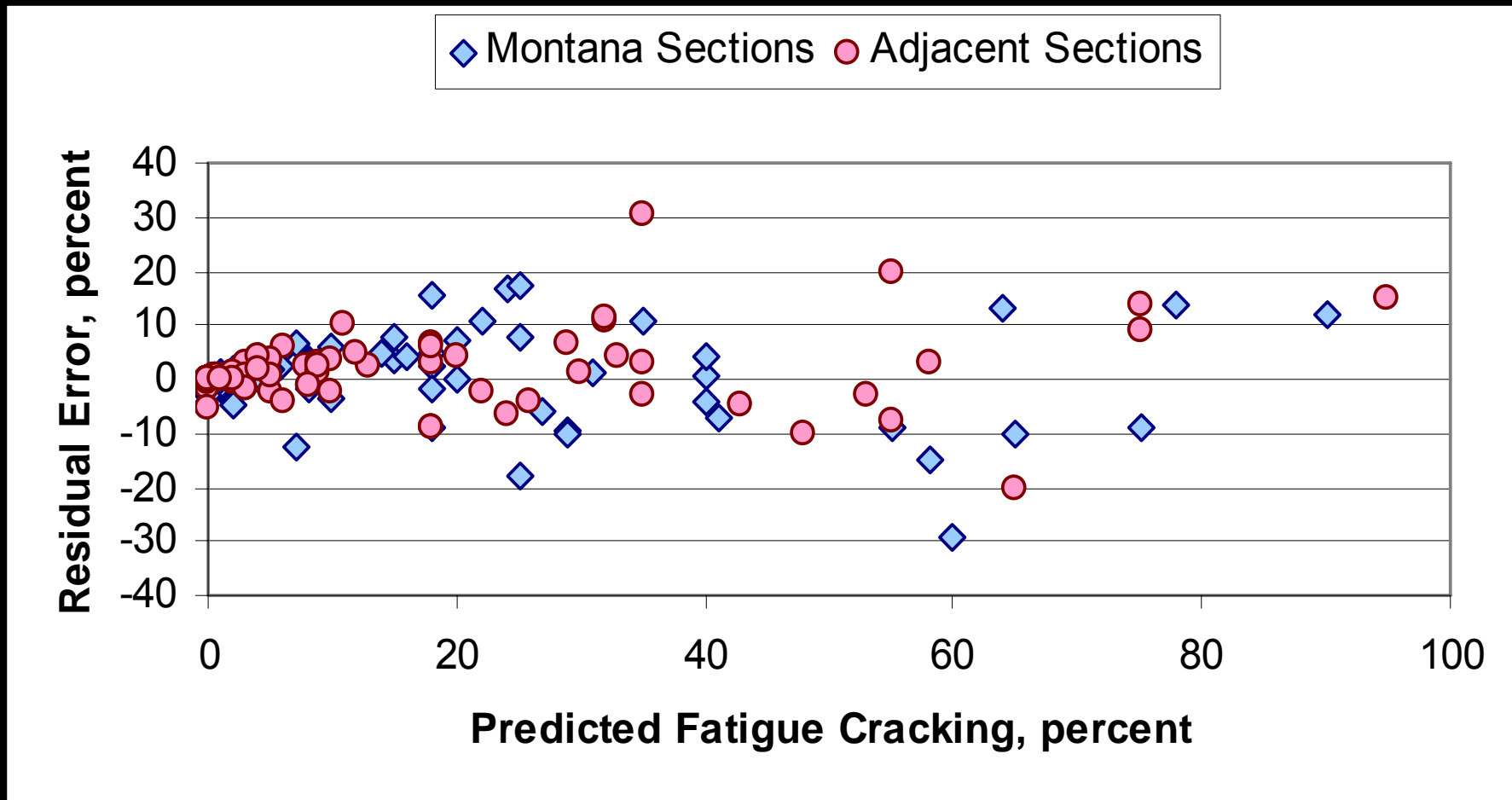


◆ Montana Sections ● Adjacent Sections — Line of Equality



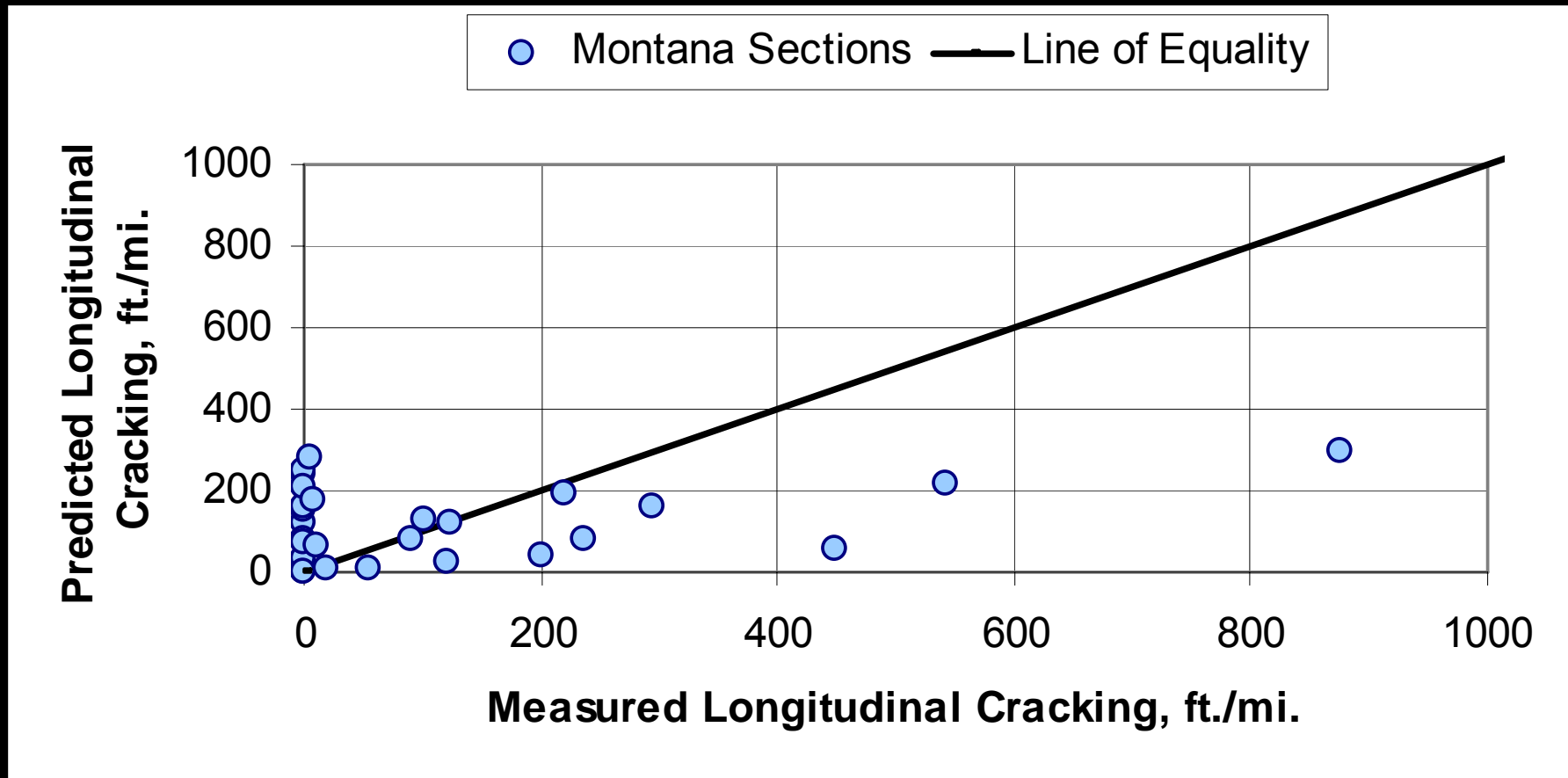


Fatigue Cracking





Longitudinal Cracking





Fatigue Cracking, Semi-Rigid



Distress Model Calibration Settings - Flexible New

AC Fatigue | AC Rutting | Thermal Fracture | **CSM Fatigue** | Subgrade Rutting | AC Cracking | CSM Cracking | IRI

$$N_f = 10^{\left(\frac{\beta_r \left(\frac{\sigma_s}{M_r} \right)}{M_r \beta_{cs}} \right)}$$

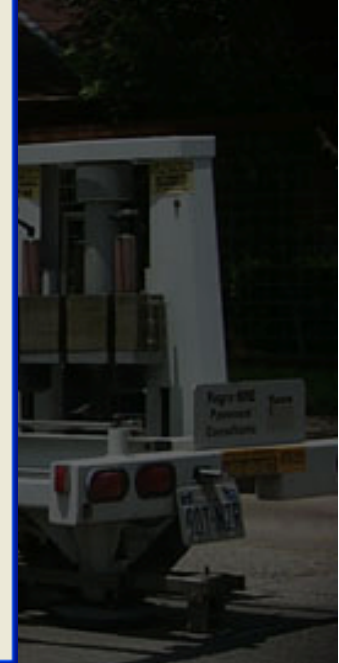
N_f = number of repetitions to fatigue cracking
 σ_s = Tensile stress (psi)
 M_r = modulus of rupture (psi)

Special Analysis
 National Calibration
 State/Regional Calibration
 Typical Agency Values

k1: Bc1:
k2: Bc2:

Factor Dependent on CAM Strength

Fatigue Cracking of Semi-Rigid Pavements





Semi-Rigid Pavements



Distress Model Calibration Settings - Flexible New

AC Fatigue | AC Rutting | Thermal Fracture | CSM Fatigue | Subgrade Rutting | AC Cracking | CSM Cracking | IRI

$$FC_{ctb} = C_1 + \frac{C_2}{1 + e^{C_3 - C_4(Damage)}}$$

C1 (CSM)

C2 (CSM)

C3 (CSM)

C4 (CSM)

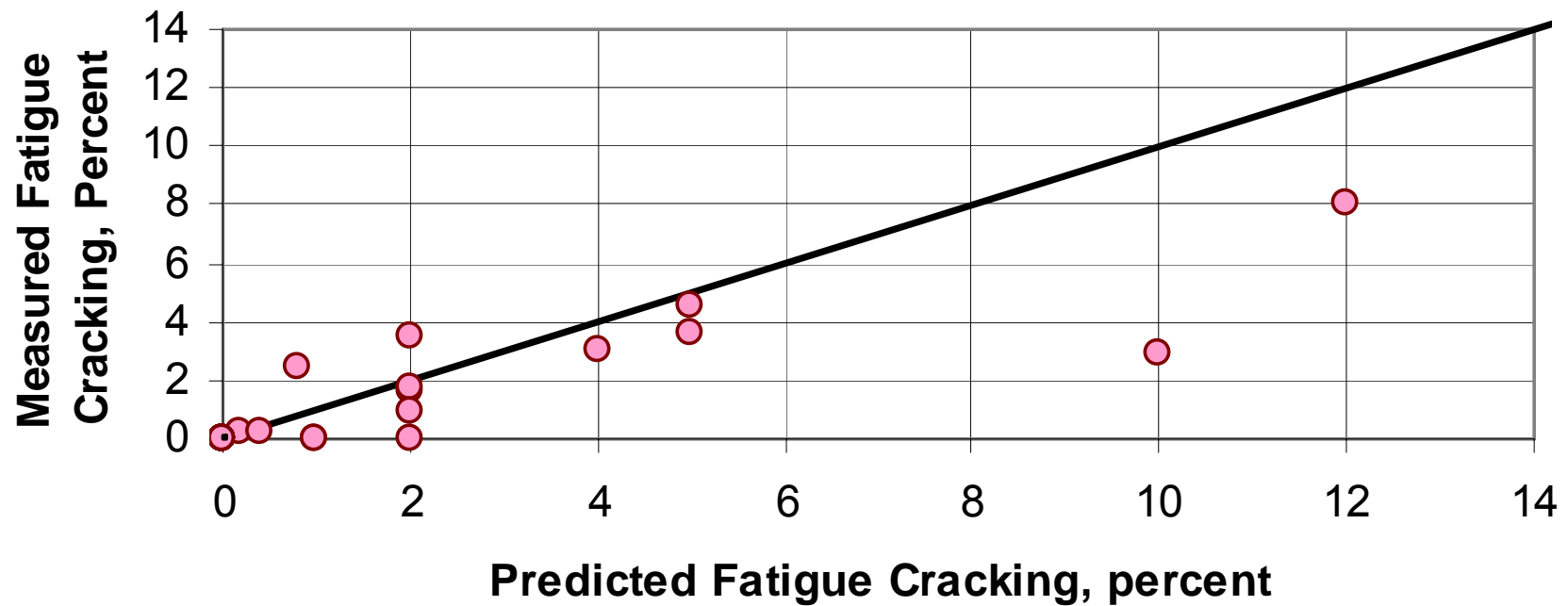
Standard Deviation (CTB):



Fatigue Cracking of Semi-Rigid

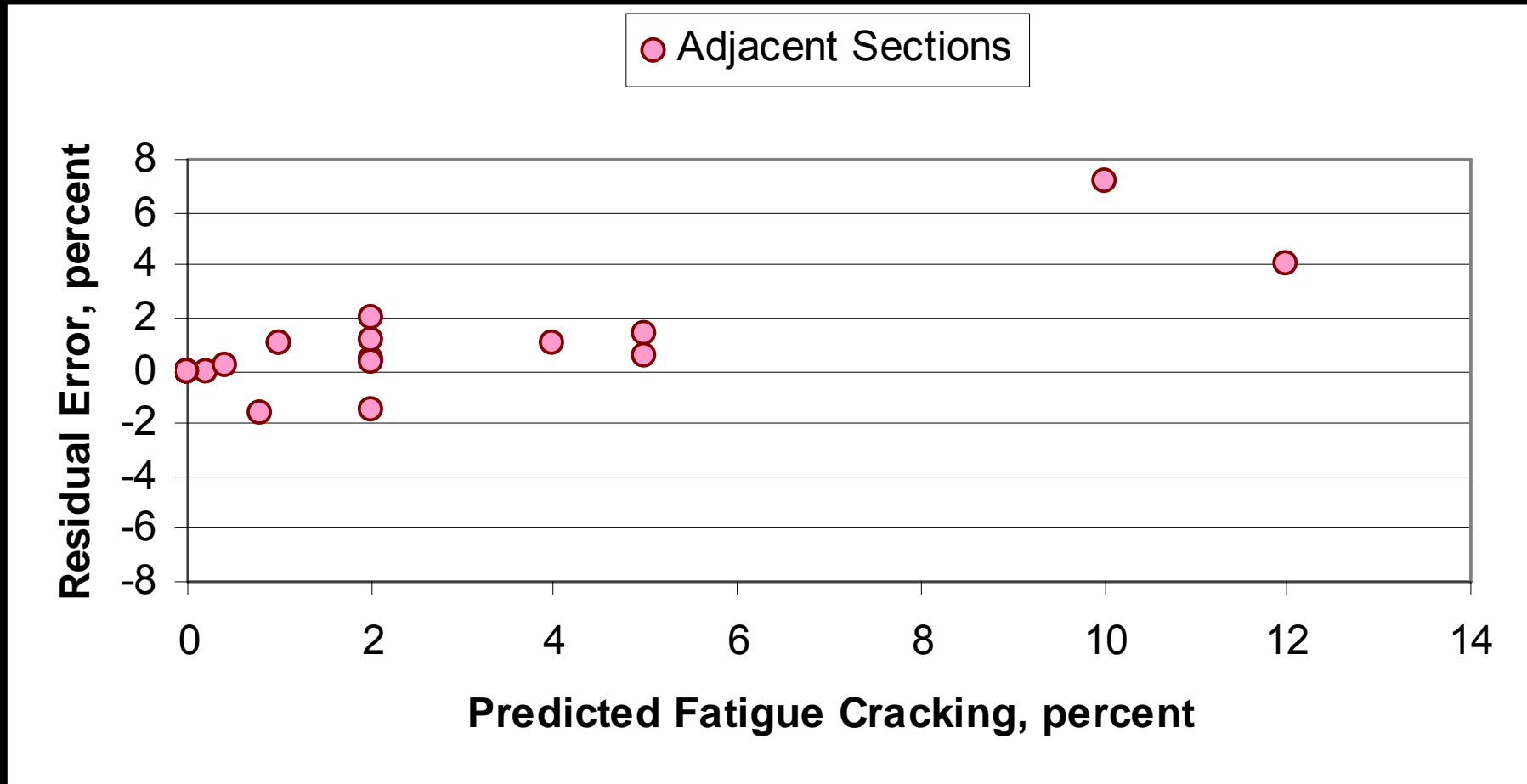


◆ Montana Sections ● Adjacent Sections — Line of Equality





Fatigue Cracking: Semi-Rigid

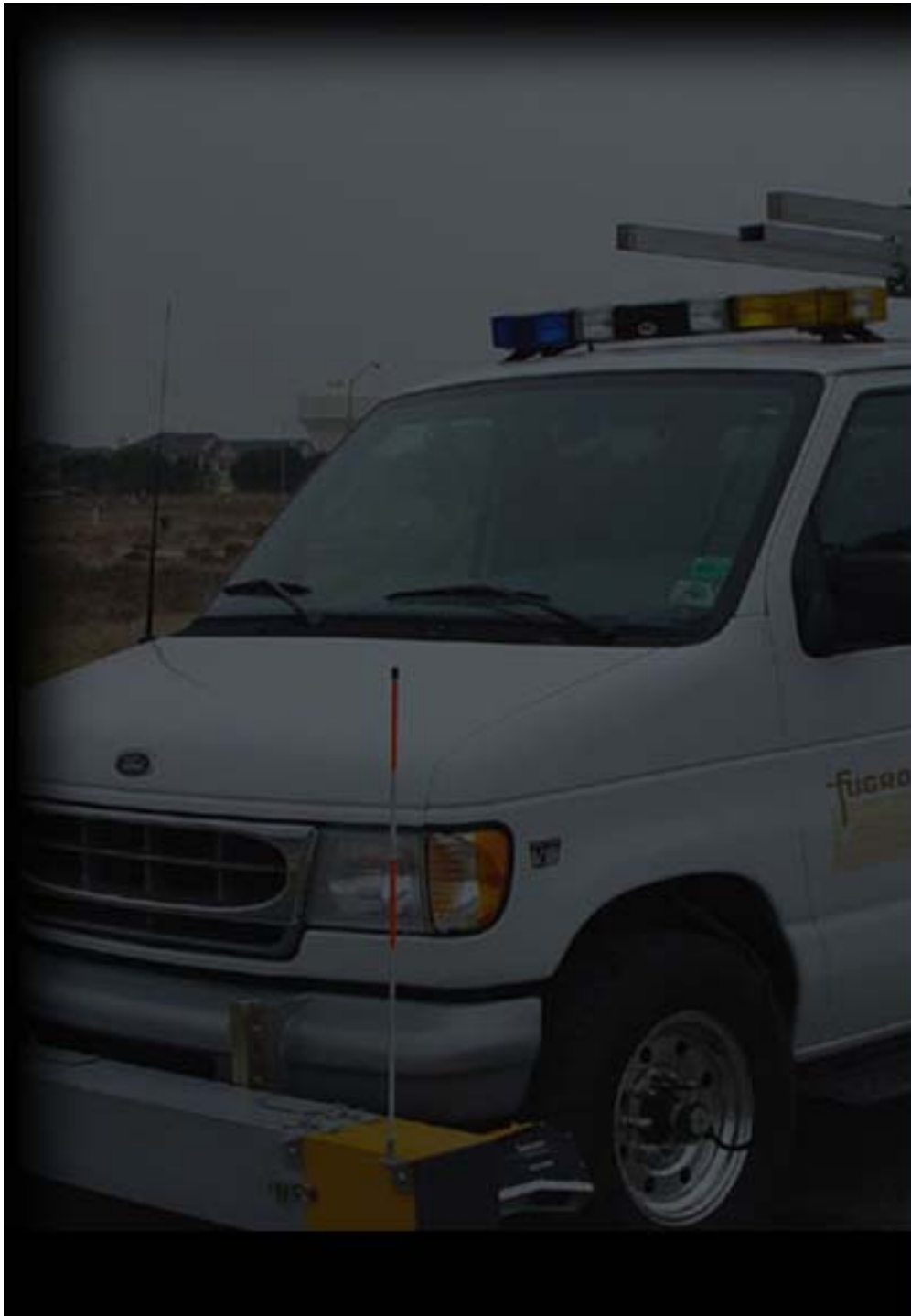




MDT Calibration Project – Alligator Cracking



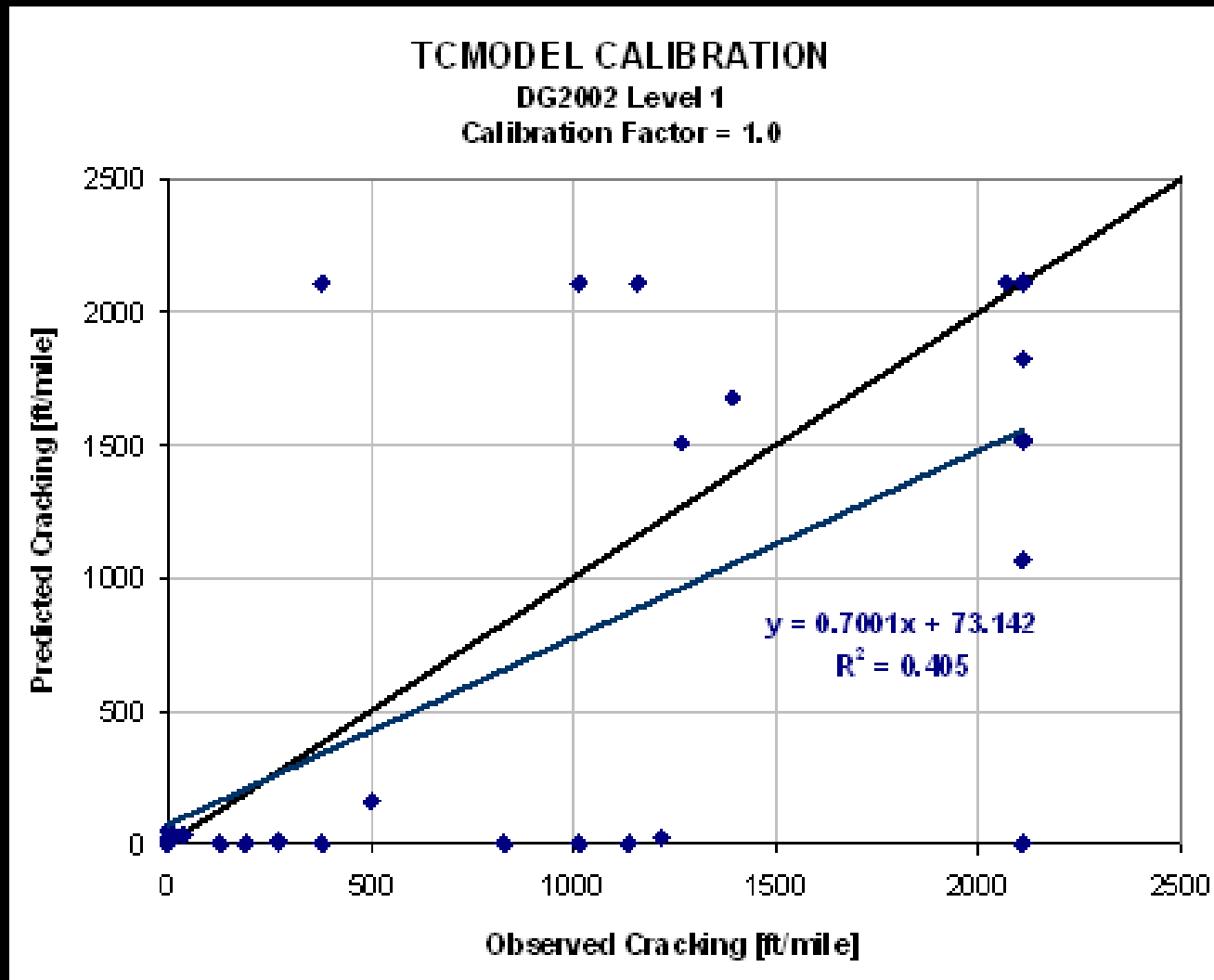
Type of Pavement		No. of Points	Bias in.	Standard Error, in.	RMSE in.	S_e/S_y
Montana Sites	New Construction; Flexible Pavts.	58	1.11	2.34	5.11	0.401
	Semi-Rigid	No alligator cracking measured!				
	HMA Overlays of Flexible Pavts.	50	-0.02	8.17	14.30	0.318
All Sites Combined	New Construction; Flexible Pavts.	76	0.15	2.45	4.67	0.315
	Semi-Rigid Pavts.	51	0.51	1.51	2.86	0.532
	HMA Overlays, All Type Pavts.	70	0.67	7.670	13.94	0.318



Transverse Cracking Prediction Model



Transverse Cracking – HMA: NCHRP 1-40D





Transverse/Thermal Cracking



Distress Model Calibration Settings - Flexible New

AC Fatigue | AC Rutting | **Thermal Fracture** | CSM Fatigue | Subgrade Rutting | AC Cracking | CSM Cracking | IRI

$$C_f = 400 * N\left(\frac{\log C / h_{ac}}{\sigma}\right)$$

$$\Delta C = (k * \beta t)^{n+1} * A * \Delta K^n$$

$$A = 10^{(4.389 - 2.52 * \log(E * \sigma_m * n))}$$

Cr = observed amount of thermal cracking (ft/500 ft)
 k = regression coefficient determined through field calibration
 N() = standard normal distribution evaluated at ()
 σ = standard deviation of the log of the depth of cracks in the pavements
 C = crack depth (in)
 h = thickness of asphalt layer (in)
 ΔC = Change in the crack depth due to a cooling cycle.
 ΔK = Change in the stress intensity factor due to a cooling cycle.
 A, n = Fracture parameters for the asphalt mixture.
 E = Mixture stiffness.
 σ_m = Undamaged mixture tensile strength.
 βt = Calibration parameter.

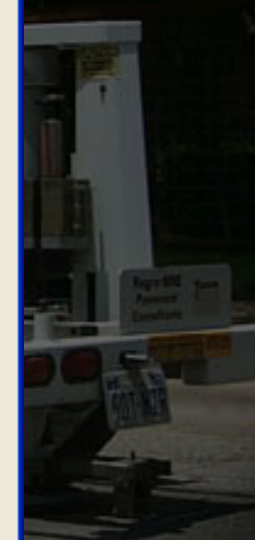
Special Analysis
 National Calibration
 State/Regional Calibration
 Typical Agency values

Level 1 K:	1.5	Bt1:	1	Std. Dev. (THERMAL):	0.1468 * THERMAL + 65.027
Level 2 K:	0.5	Bt2:	1	Std. Dev. (THERMAL):	0.2841 * THERMAL + 55.462
Level 3 K:	1.5	Bt3:	1	Std. Dev. (THERMAL):	0.3972 * THERMAL + 20.422

0.25

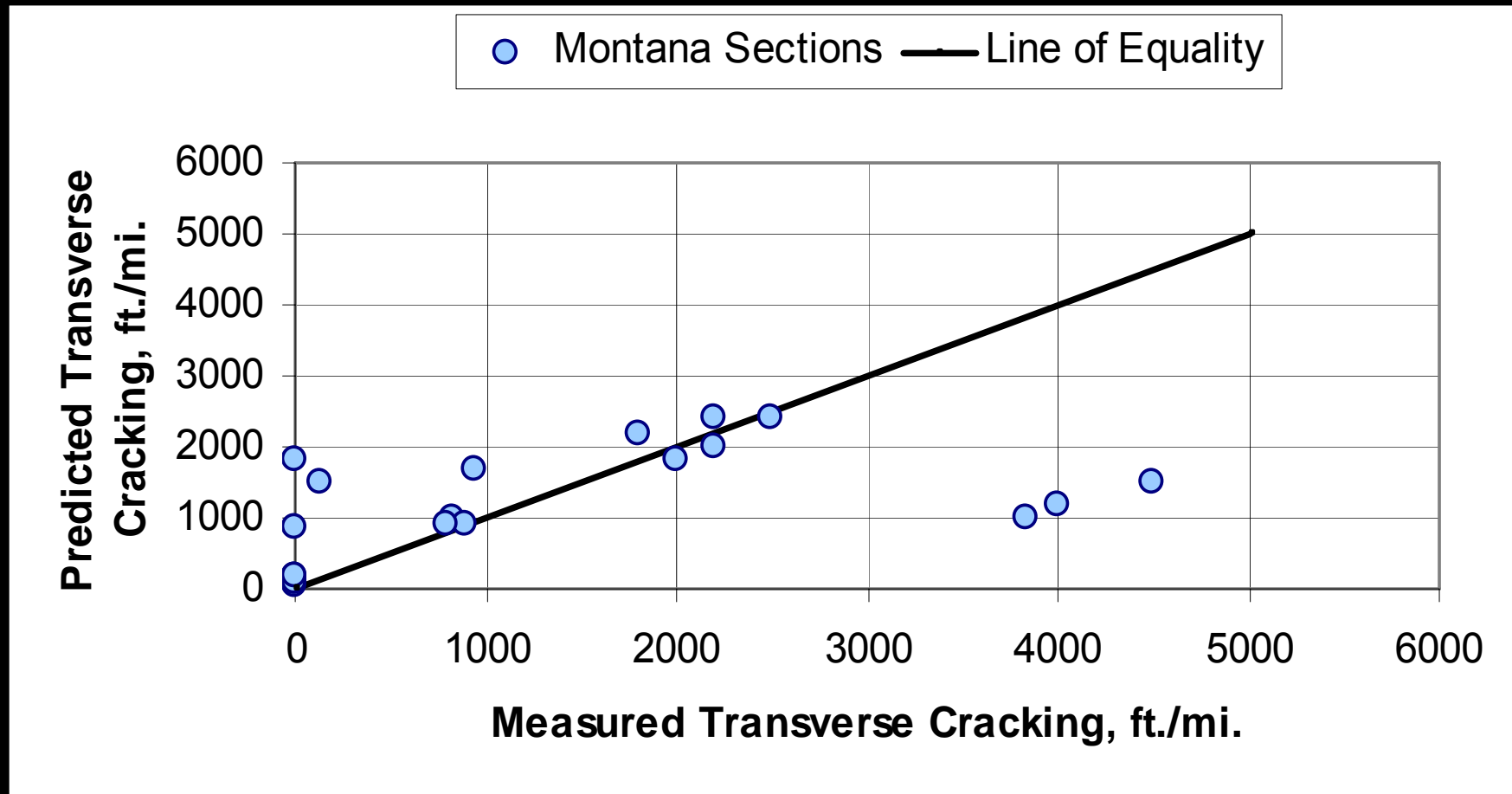
Transverse/Thermal Cracking

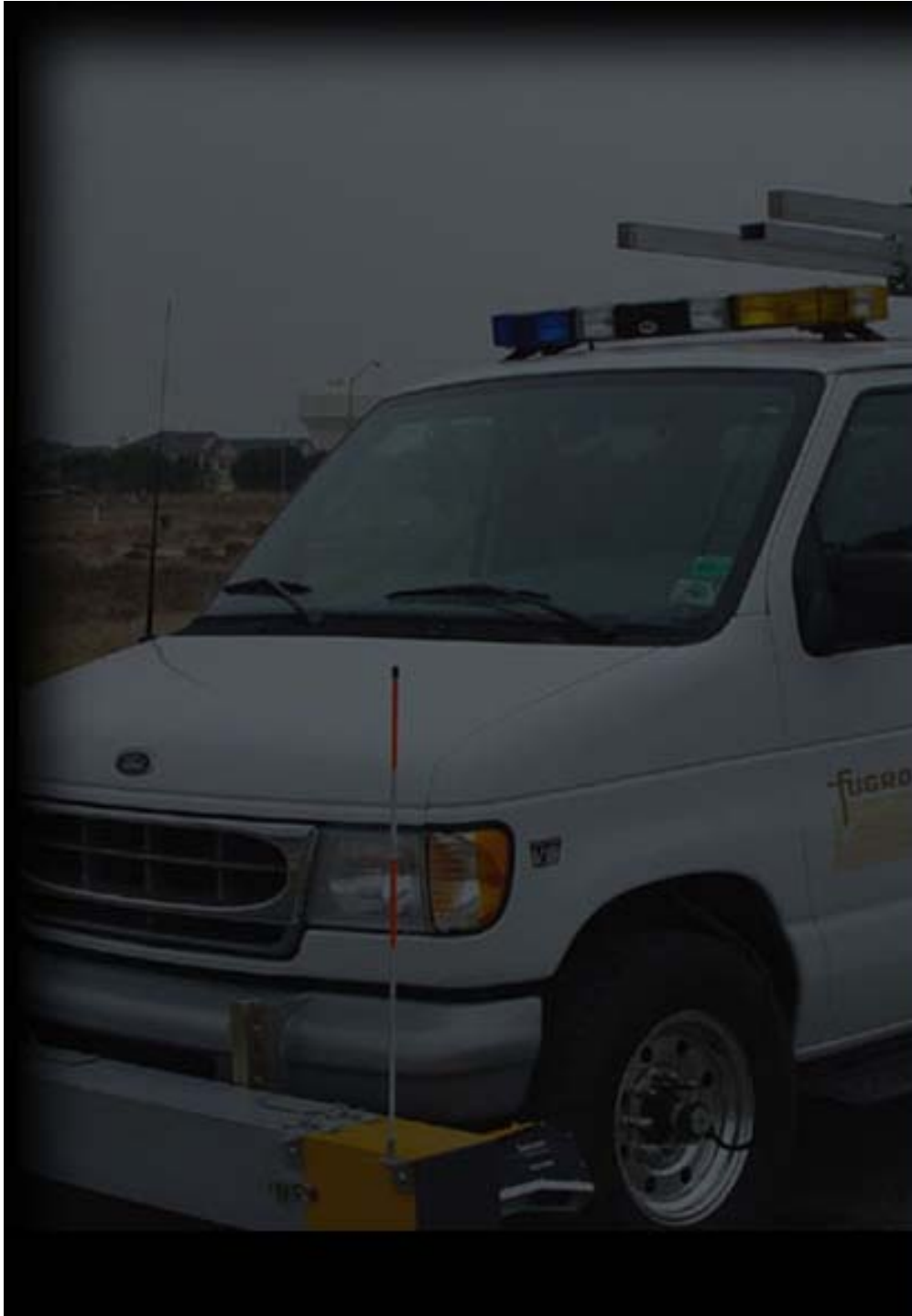
OK Cancel





Transverse Cracking

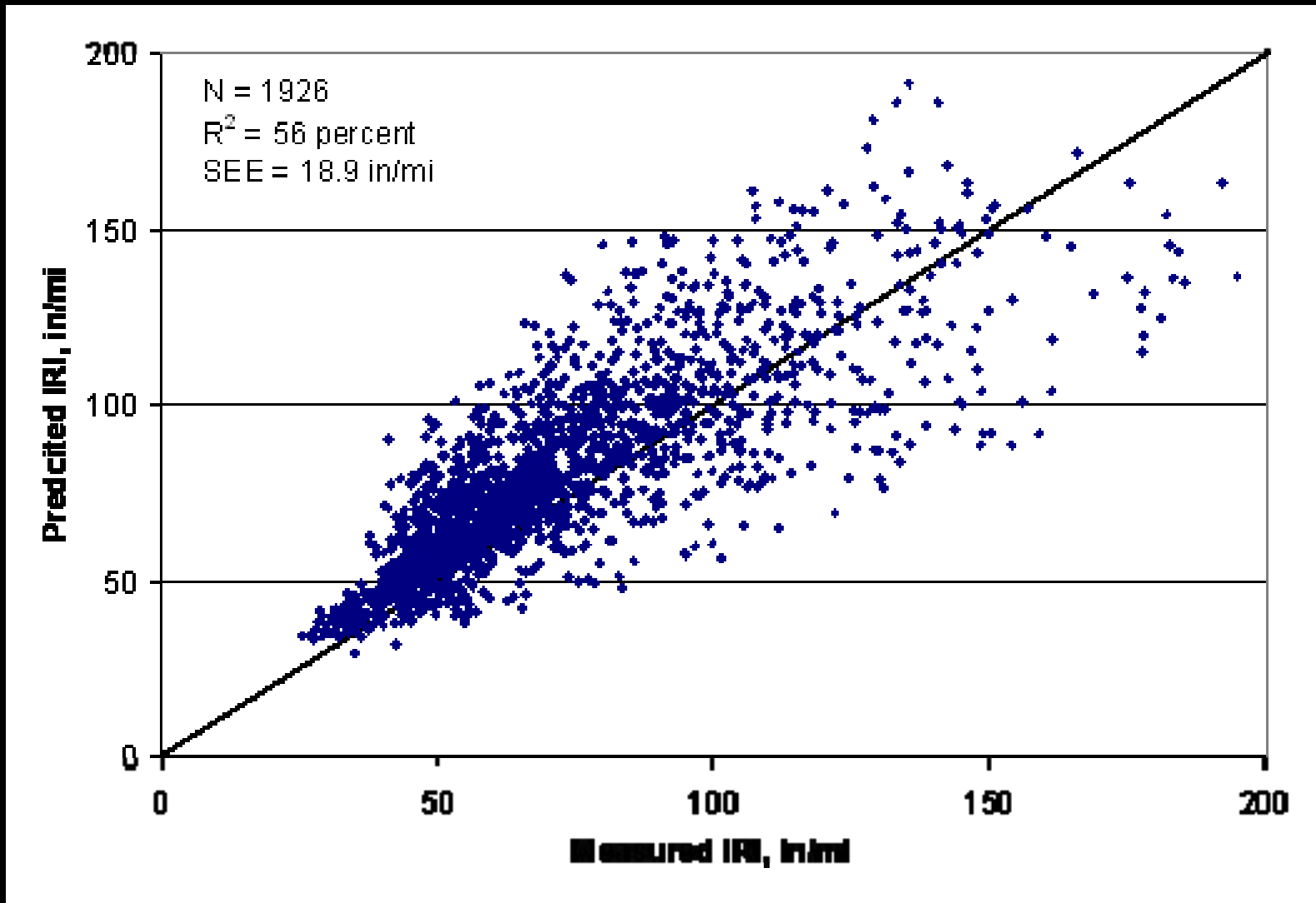




IRI / Smoothness Prediction Model

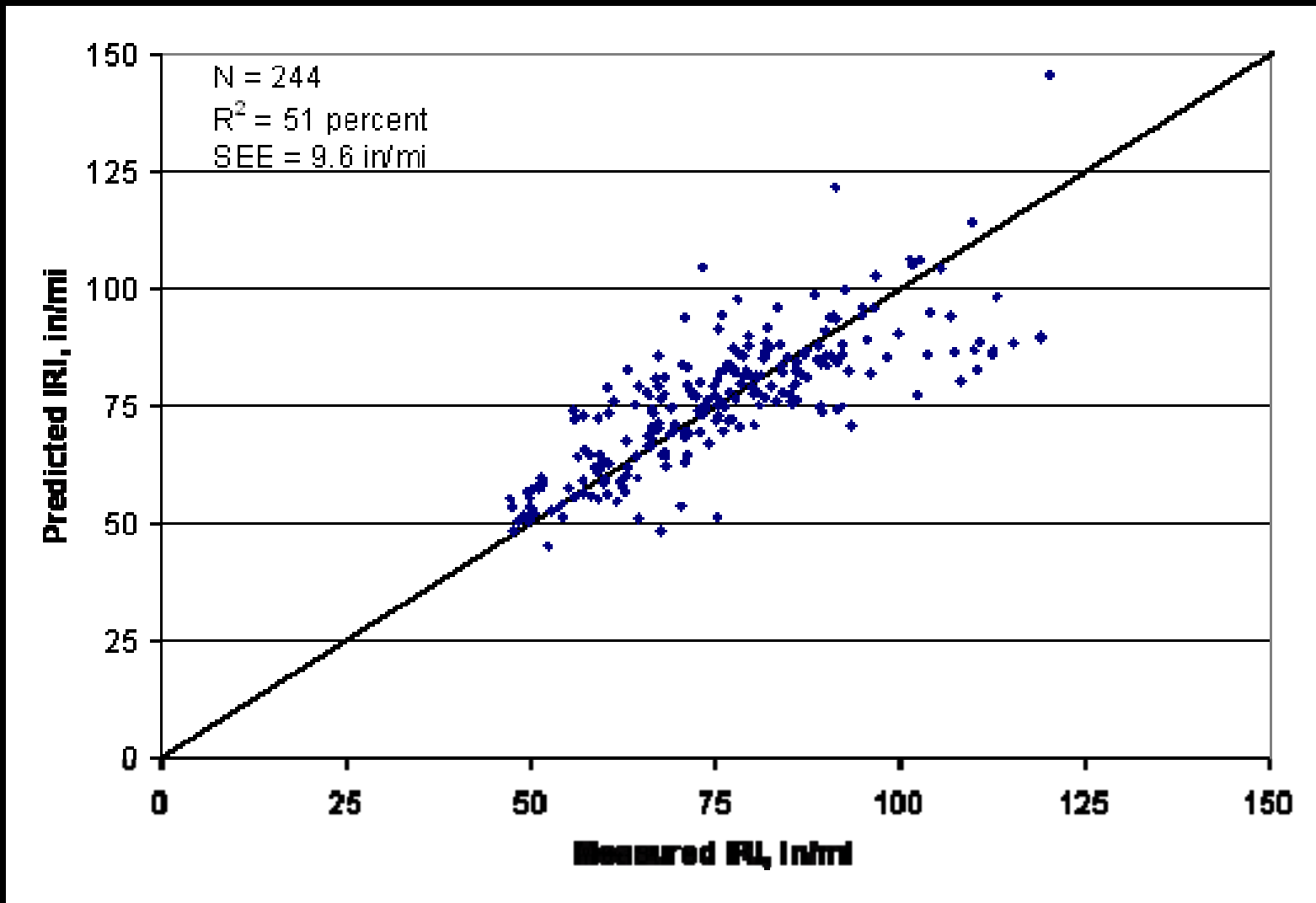


IRI / Smoothness – HMA / HMA





IRI / Smoothness – HMA / PCC





Smoothness/IRI



Distress Model Calibration Settings - Flexible New

AC Fatigue | AC Rutting | Thermal Fracture | CSM Fatigue | Subgrade Rutting | AC Cracking | CSM Cracking | **IRI**

IRI Flexible Pavements

- C1 - Rutting
- C2 - Fatigue Crack
- C3 - Transverse Crack
- C4 - Site Factors

C1 (HMA)	<input type="text" value="40"/>
C2 (HMA)	<input type="text" value="0.4"/>
C3 (HMA)	<input type="text" value="0.008"/>
C4 (HMA)	<input type="text" value="0.015"/>

IRI Flexible Over PCC

- C1 - Rutting
- C2 - Fatigue Crack
- C3 - Transverse Crack
- C4 - Site Factors

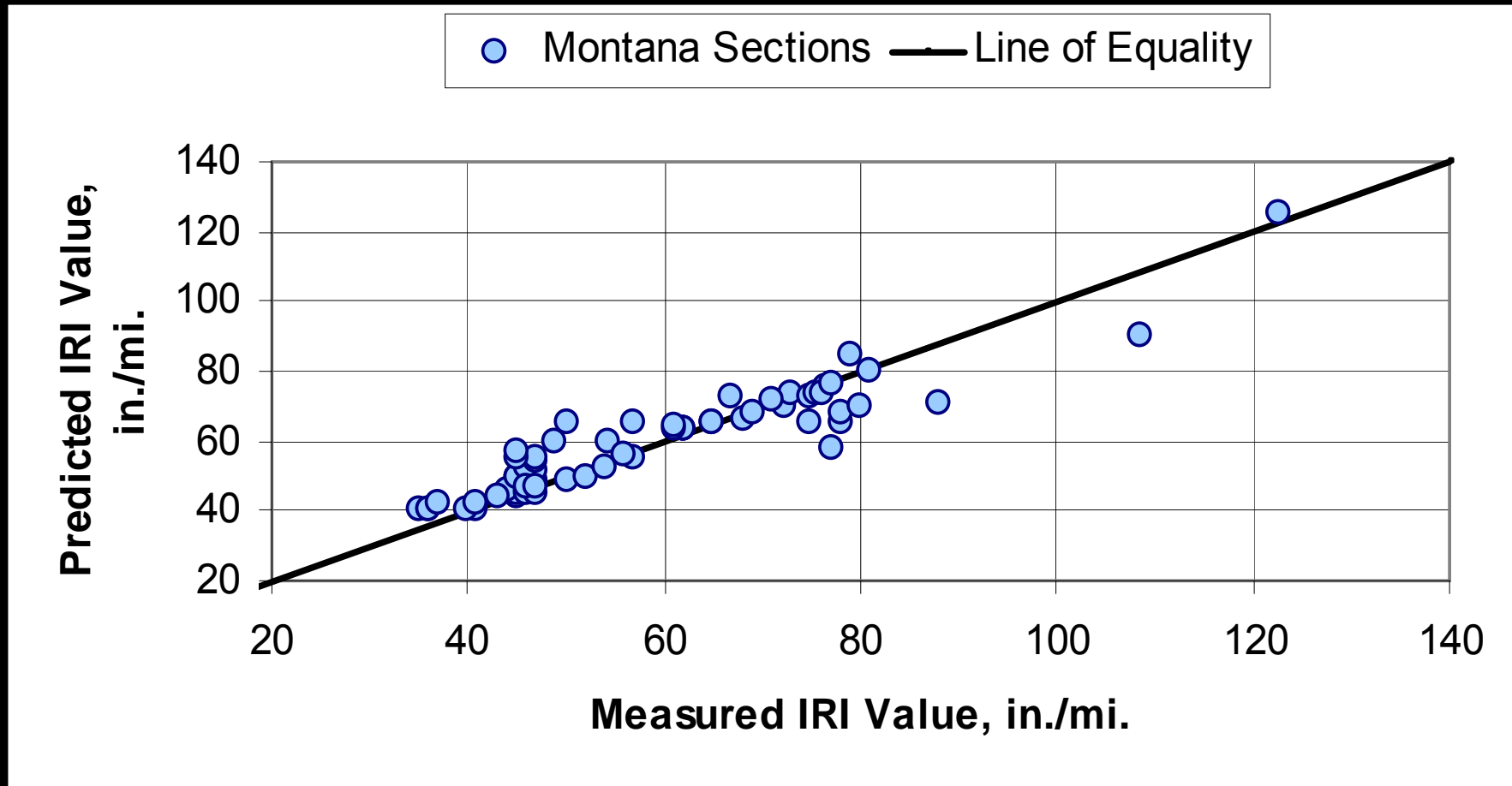
C1 (HMA/PCC)	<input type="text" value="40.8"/>
C2 (HMA/PCC)	<input type="text" value="0.575"/>
C3 (HMA/PCC)	<input type="text" value="0.0014"/>
C4 (HMA/PCC)	<input type="text" value="0.00825"/>

Smoothness or IRI

OK Cancel



IRI





Presentation Outline



1. Introduction & Overview of Project
2. Determination of MEPDG Inputs
3. Database
4. Verification & Calibration of MEPDG for Use in Montana
5. Summary & Concluding Comments



Conclusions & Recommendations



Inputs for MEPDG:

- ☑ HMA and other materials characterization
- ☑ Traffic characterization
- ☑ Climate





Conclusions & Recommendations



Performance Prediction Models:

- Rutting
- Fatigue Cracking
 - Alligator, area cracking
 - Longitudinal cracking
 - Fatigue, semi-rigid layers
- Thermal/transverse cracking
- Smoothness or IRI





Suggested Improvements



Material Properties & Characterization

- ✦ Polymer modified binders
- ✦ Fatigue properties of semi-rigid layers
- ✦ Full-depth reclamation layer properties

Performance Prediction Models

- ✦ Load related longitudinal cracking
- ✦ Rutting in unbound aggregate layers and soils of pavements with thin surface layers



Topics to be Quantified (not included within scope of work)



1. Benefit & effect of pavement preservation activities on reducing distress & extending a roadway's serviceable life.
2. Benefit of increased density: comparison of roadways with lower and higher air voids.
3. Determine reason for differences between LTPP & MDT FWDs.
4. Continue to measure IDT strength, modulus, strain at failure, & creep compliance on some mixes for use with the MEPDG.
5. Wear from use of studded tires believed to be minor on non-LTPP & other segments of roadways included within study.



Questions?





THANK YOU