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| 16. Abstract Test method Tex-113-E prepares laboratory aggregate base test specimens with an impact hammer compactor. These specimens are used for compaction characteristics and design tests. Although the historical Tex-113-E required a certain amount of compaction energy, no method to validate attainment of that energy existed until Texas Department of Transportation (TxDOT) Project 0-5135 developed the Soil Compactor Analyzer (SCA). The SCA measures the kinetic energy applied by each drop of the impact hammer. In this project, the SCA system was modified to control the compactor, where the SCA starts the machine and then turns off the compactor when the prescribed amount of energy is attained. This project then evaluated how changing the machine operational parameters, such as hammer weight, drop height, and number of blows per lift, impacted test results. In this evaluation, the SCA was used in all cases to control the compactor, so the prescribed amount of total energy was always applied regardless of machine operational parameters. The results showed that while using the current TxDOT-approved SCA to control total energy per lift between 740 and 765 ft-lbf, the number of blows per lift may vary between 45 and 60 with no impact on test results. Finally, this project conducted an interlaboratory study to develop precision statistics of Tex-113-E compaction. This study showed that the SCA enables excellent precision of total compaction energy. Total compaction energy should be repeatable and reproducible within about 27 ft-lbf, or approximately 1 percent of the specification value. Compacted dry density should be repeatable within about 2.5 pounds per cubic foot (pcf) and reproducible within about 3.3 pcf. | | | | | |
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**IMPLEMENTATION OF THE SOIL COMPACTOR ANALYZER
INTO TEST METHOD TEX-113-E: TECHNICAL REPORT**

by

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Report 5-5135-01-1
Project 5-5135-01
Project Title: Implementation of the Soil Compactor Analyzer
for Tex-113-E

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The contents of this report reflect the views of the authors, who are responsible for the facts and the accuracy of the data presented herein. The contents do not necessarily reflect the official view or policies of the Federal Highway Administration (FHWA) or the Texas Department of Transportation (TxDOT). This report does not constitute a standard, specification, or regulation. The researcher in charge was Stephen Sebesta.

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EXECUTIVE SUMMARY

In Test Method Tex-113-E, the Texas Department of Transportation (TxDOT) employs an impact hammer method of sample compaction for laboratory preparation of road base materials for testing. Although the historical Tex-113-E required a certain amount of compaction energy, no method to validate attainment of that energy existed until TxDOT Project 0-5135 developed the Soil Compactor Analyzer (SCA). The SCA measures the kinetic energy applied by each drop of the impact hammer. In this implementation project, the research team modified the SCA to not only measure the compaction energy, but also to control the automatic tamper and stop the machine upon attainment of the prescribed energy per lift. Fifteen SCA units with machine control capability were delivered to TxDOT in this implementation project. Additionally, the 12 SCA units delivered to TxDOT in prior Project 0-5135 were retrofitted with machine control capability in this implementation project, yielding 27 SCA systems in TxDOT with machine control capability.

As TxDOT prepared to officially implement the SCA into Test Method Tex-113-E, the researchers also investigated the influence of changing machine operational parameters on test results while using the SCA to maintain the prescribed amount of energy per lift. Machine operational parameters include the hammer weight, drop height, and number of drops per lift. Varying the hammer weight and drop height will result in different energies per drop, which results in a different number of drops per lift to attain the prescribed energy. In this project, parameters were varied to perform test series with average energies per drop between approximately 12.5 and 16.7 ft-lbf, which resulted in a range of 45 to 60 drops per lift. Tests investigated included the moisture-density relationship; the dielectric constant and seismic modulus, both at the time of molding and after Tex-117-E Part II conditioning; the unconfined compressive strength (UCS) per Tex-117-E Part II; and the moisture content after compressive strength testing. The results showed that while using the current TxDOT-approved SCA to control total energy per lift between 740 and 765 ft-lbf, the number of blows per lift may vary between 45 and 60 with no impact on test results.

As a final stage in this project, an interlaboratory study was conducted to develop precision statistics for Tex-113-E compaction. This study showed that the SCA enables excellent precision of total compaction energy. Total compaction energy should be repeatable and reproducible within about 27 ft-lbf, or approximately 1 percent of the specification value. Compacted dry density should be repeatable within about 2.5 pounds per cubic foot (pcf) and reproducible within about 3.3 pcf.

CHAPTER 1. EVALUATION OF IMPACT HAMMER ADJUSTMENTS ON MEASURED MATERIAL PROPERTIES

INTRODUCTION

With TxDOT’s recent inclusion of the SCA in Tex-113-E, labs can now control and obtain the required amount of total energy applied to each lift during compaction of flexible base test specimens. The current Tex 113-E requires 750 ft-lbf per lift to be reached within 50 ± 5 blows of a 10 ± 0.02 lb hammer. To investigate these tolerances, researchers at the Texas Transportation Institute (TTI) employed a Grade 2 flexible base and systematically varied the automatic tamper’s drop height and weight to yield blows per lift during sample fabrication ranging from 45 to 60 while still maintaining a total energy per lift of approximately 750 ft-lbf. Test series with three different target numbers of blows per lift were conducted. The results showed that while using the current TxDOT-approved SCA to control total energy per lift between 740 and 765 ft-lbf, the number of blows per lift may vary between 45 and 60 with no impact on test results. Tests investigated included the moisture-density relationship from Tex-113-E; the dielectric constant and seismic modulus, both at the time of molding and after Tex-117-E Part II conditioning; the UCS per Tex-117-E Part II; and the moisture content after compressive strength testing.

Kinetic energy during compaction with the automatic tamper used in Tex-113-E is most effectively increased by obtaining increases in the impact velocity. With the tampers used in TxDOT, this is best accomplished through decreasing friction losses as much as possible and increasing the drop height. If additional adjustment is necessary to obtain the prescribed total energy per lift within 45 and 60 blows, adding weight to the hammer is the next step to take.

SUMMARY OF EXPERIMENT

Table 1.1 presents the experiment used to investigate energy tolerances and drop height adjustments. In essence, the experiment was designed to use varying hammer drop heights and hammer weights to obtain the different target energies per blow. These different energies per blow in turn result in the different levels of target number of blows per lift while maintaining the total sample compaction energy requirement of 750 ft-lbf per lift.

Table 1.1. Experimental Design to Investigate Impact of Number of Drops per Lift on Test Results.

| Target Average Impact Energy per Blow (ft-lbf) | Target Number of Drops per Lift | Tests Performed in Triplicate for Each Target Level |
|--|---------------------------------|---|
| 12.5 | 60 | <ul style="list-style-type: none"> • Tex-113-E moisture-density relationship. • Compressive strength at 0 psi lateral pressure (Tex-117-E Part II). • Dielectric constant at molding and immediately before breaking. • Seismic modulus at molding and immediately before breaking. • Moisture content after breaking. |
| 15.0 | 50 | |
| 16.7 | 45 | |

MATERIAL USED IN TESTING

For these tests, researchers used a Grade 2 base from the Vulcan Groesbeck pit. Appendix A presents the TxDOT test report from the material used.

PRESENTATION OF RESULTS

Appendix B presents the results from the specimens tested. In summary, the results revealed that when the target compaction energy was controlled by the current TxDOT-approved SCA and achieved within 45 to 60 drops per lift:

- No statistical difference existed in the maximum dry density or optimum water content.
- No statistical difference existed in the dielectric constant at time of molding or after Tex 117-E Part II conditioning.
- No statistical difference existed in the seismic modulus at the time of molding or after Tex 117-E Part II conditioning.
- No statistical difference existed in the unconfined compressive strength after Tex-117-E Part II conditioning.
- The moisture content after breaking was less with specimens compacted at average energies of 16.7 ft-lbf per drop (i.e., samples only requiring 45 blows to reach the target energy per lift). Although statistically significant, in terms of performance this difference is insignificant since the mean strengths did not differ among the treatments.

SUMMARY OF MACHINE PARAMETERS USED

Table 1.2 summarizes the machine parameters and average effort applied for each treatment. The research team tested a total of 45 specimens (15 for each treatment). The desired range of blows per lift and average energy per blow were obtained while maintaining efforts within the range implied in TxDOT’s allowable tolerances on sample height. The average drop height of

18.6 inches when targeting 16.7 ft-lbf per blow was obtained by maximizing the distance between the engager and the releaser body on the automatic tamper (i.e., with this particular tamper, that drop height was the maximum drop height attainable).

Table 1.2. Summary of Machine Parameters for Treatments Investigated.

| Target Energy per Blow (ft-lbf) | Hammer weight used (lb) | AVG # blows per lift | AVG Drop Ht (in.) | AVG Energy per blow (ft-lbf) | AVG Total Energy per Lift (ft-lbf) | AVG Effort (ft-lbf/in ³) |
|---------------------------------|-------------------------|----------------------|-------------------|------------------------------|------------------------------------|--------------------------------------|
| 12.5 | 10.31 | 61 | 16.2 | 12.4 | 750.7 | 13.3 |
| 15 | 11.04 | 52 | 18 | 14.6 | 751.3 | 13.6 |
| 16.7 | 12.21 | 45 | 18.6 | 16.8 | 759.2 | 13.2 |

RESULTS FROM MOISTURE DENSITY RELATIONSHIP

Figures 1.1–1.3 illustrate the moisture-density relationships measured in triplicate for the three target energies per blow. Table 1.2 showed these target energies per blow were 12.5, 15, and 16.7 ft-lbf while maintaining total compaction energy of 750 ft-lbf per lift. Since each moisture-density curve requires 4 samples, a total of 36 samples were required to generate these data. Appendix B presents the entirety of each sample’s results in the column labeled “113-E Moisture-Density Samples.”

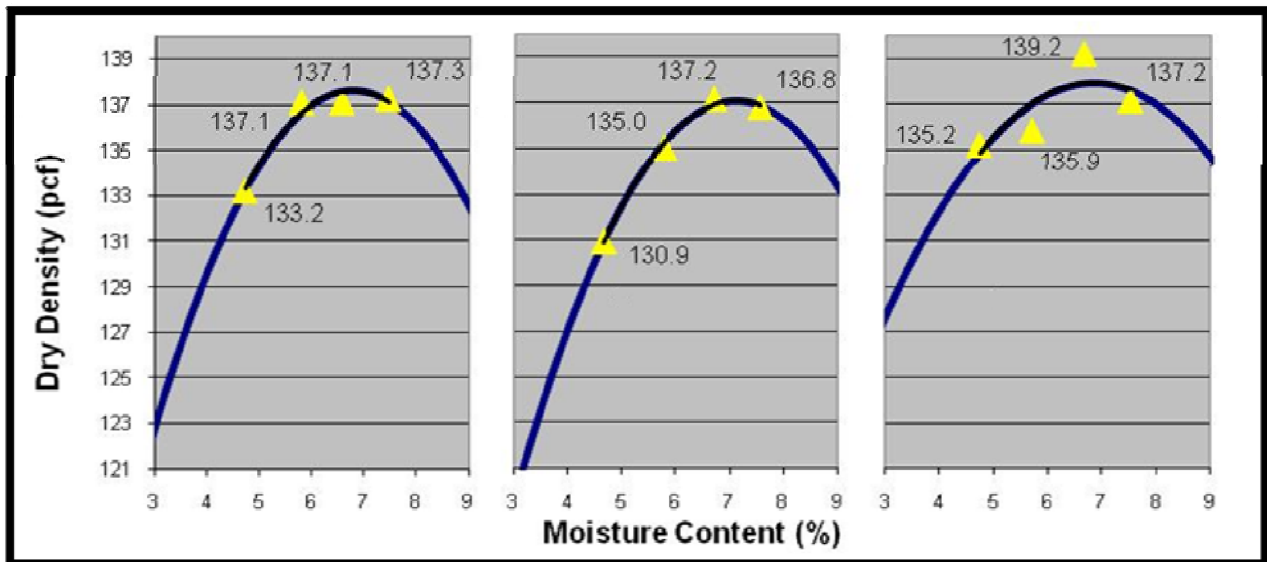


Figure 1.1. Triplicate Moisture-Density Curves for Samples Molded at Energies per Blow of 12.5 ft-lbf and Total Energy per Lift of 750 ft-lbf.

Left to right: Replicate 1, 2, and 3

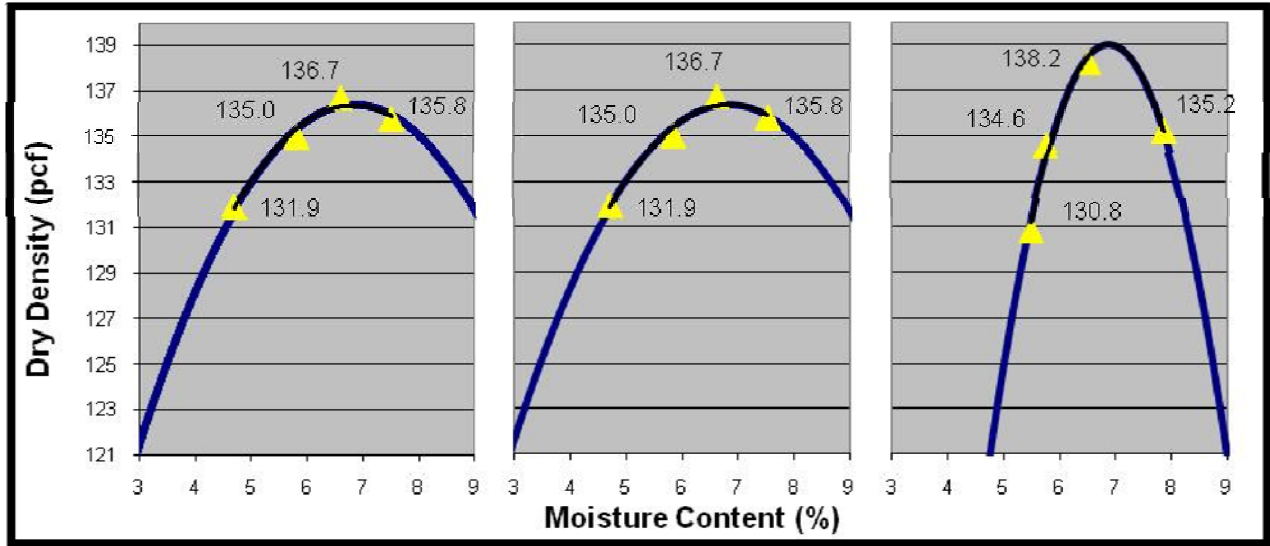


Figure 1.2. Triplicate Moisture-Density Curves for Samples Molded at Energies per Blow of 15 ft-lbf and Total Energy per Lift of 750 ft-lbf.
Left to right: Replicate 1, 2, and 3

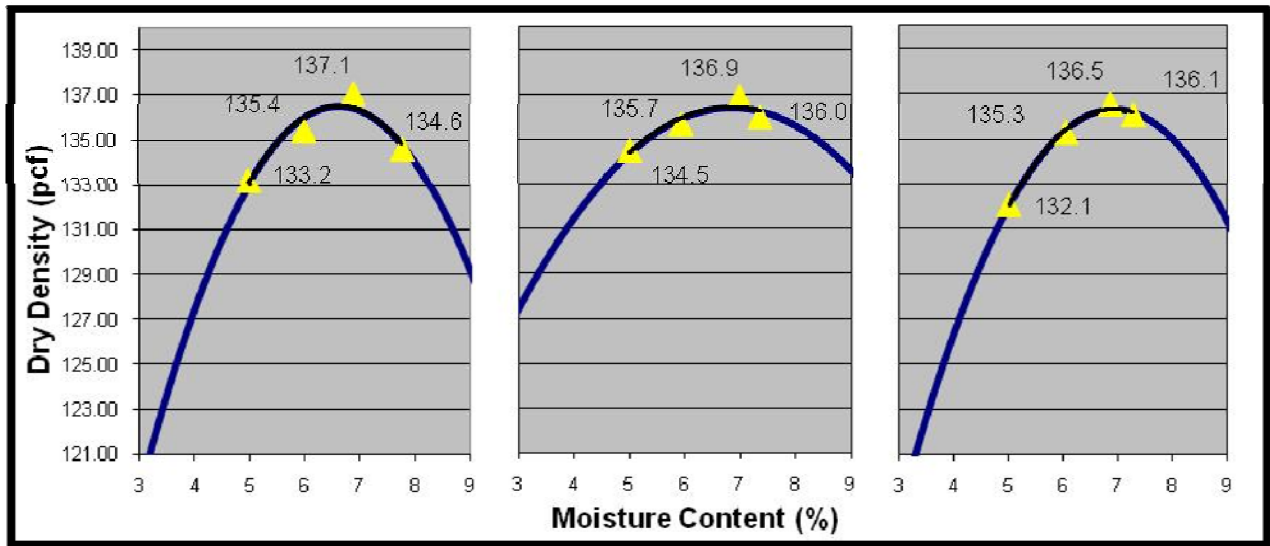


Figure 1.3. Triplicate Moisture-Density Curves for Samples Molded at Energies per Blow of 16.7 ft-lbf and Total Energy per Lift of 750 ft-lbf.
Left to right: Replicate 1, 2, and 3

Each replicate in Figures 1.1–1.3 generated optimum moisture content (OMC) and maximum dry density output using TxDOT’s approved Tex-113-E spreadsheet. Table 1.3 summarizes these OMC and maximum dry density results from each replicate. The data suggest, and statistical tests confirm, that no significant difference in the average maximum dry density or optimum water content existed among the treatments. So long as the SCA was used to control the compaction energy at 750 ft-lbf per lift, the optimum moisture and max density were statistically equivalent regardless of whether the average energy per blow was 12.5, 15, or 16.7 ft-lbf.

Table 1.3. Tex-113-E Moisture-Density Results with Varying Energies per Blow.

| Replicate | 12.5 ft-lbf per blow | | | 15 ft-lbf per blow | | | 16.7 ft-lbf per blow | | |
|-----------|----------------------|---------|--------------------------------------|--------------------|---------|--------------------------------------|----------------------|---------|--------------------------------------|
| | Max Density (pcf) | OMC (%) | AVG Total Energy per Sample (ft-lbf) | Max Density (pcf) | OMC (%) | AVG Total Energy per Sample (ft-lbf) | Max Density (pcf) | OMC (%) | AVG Total Energy per Sample (ft-lbf) |
| 1 | 137.6 | 6.8 | 3002 | 138.7 | 7 | 3000 | 136.5 | 6.6 | 3034 |
| 2 | 137.1 | 7.1 | 2997 | 136.4 | 6.8 | 2991 | 136.5 | 6.8 | 3036 |
| 3 | 138 | 6.8 | 3025 | 139 | 6.9 | 3023 | 136.3 | 6.9 | 3036 |
| AVG | 137.6 | 6.9 | 3008.0 | 138.0 | 6.9 | 3004.7 | 136.4 | 6.8 | 3035.3 |

RESULTS FROM DIELECTRIC, MODULUS, AND STRENGTH TESTS

To evaluate the potential impact of the different energy treatments on the dielectric, modulus, and strength tests, specimens were made at each treatment level while targeting the appropriate average maximum density and optimum water content from Table 1.3. The dielectric and modulus tests were performed on the same specimens used for strength testing. Table 1.4 presents the machine parameters from these tests; the results are the average of three replicates per target energy level. Appendix B presents the entirety of each sample’s results in the column labeled “Test Samples at 113-E Optimum.”

Table 1.4. Machine Parameters for Dielectric, Modulus, and Strength Specimens.

| Target Energy per Blow (ft-lbf) | Hammer weight (lb) | AVG # blows per lift | AVG Drop Ht (in.) | AVG Energy per blow (ft-lbf) | Avg Effort (ft-lbf/in ³) |
|---------------------------------|--------------------|----------------------|-------------------|------------------------------|--------------------------------------|
| 12.5 | 10.31 | 59 | 17.2 | 12.8 | 13.4 |
| 15 | 11.04 | 52 | 18.2 | 14.6 | 13.45 |
| 16.7 | 12.21 | 45 | 18.6 | 16.9 | 13.45 |

Figure 1.4 illustrates, and statistical tests confirm, that no difference in mean sample dry density or compaction effort existed among the specimens compacted at the different energies per blow for the dielectric, modulus, and strength testing experiments. This is important since varying efforts could potentially impact density, which in turn could impact modulus and strength.

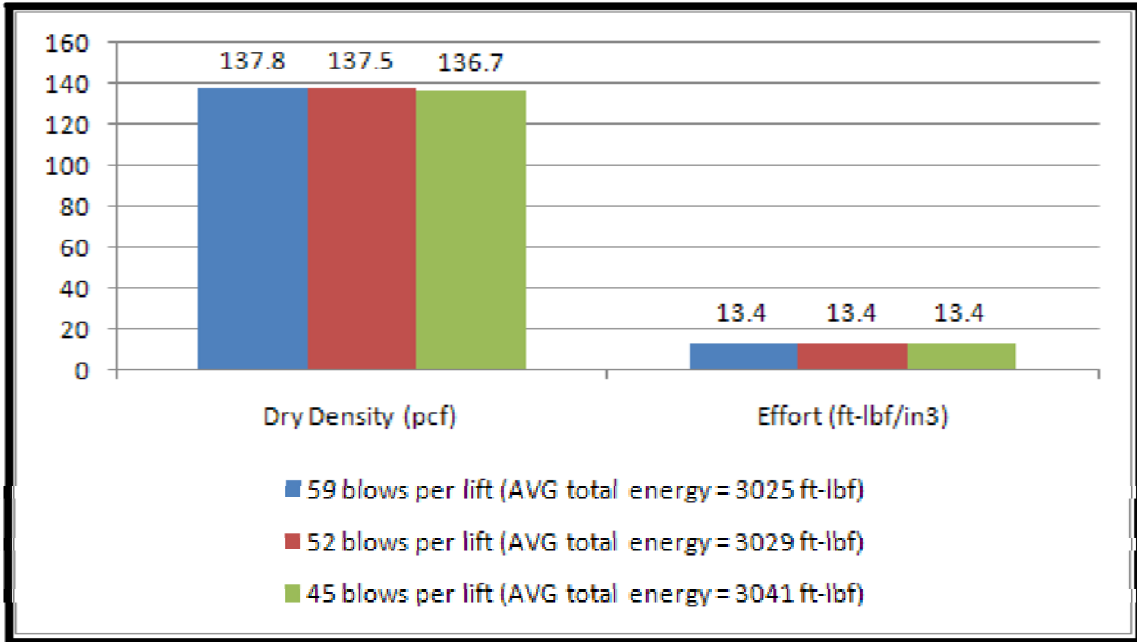


Figure 1.4. No Difference in Dry Density or Effort Observed among Samples from Different Energies per Blow.

Note: Each result is the average of three specimens. No significant difference exists among means.

Figures 1.5 through 1.8 illustrate that no statistically significant differences existed among the means for dielectric, seismic modulus, or compressive strength at 0 psi lateral pressure per Tex-17-E Part II. Figure 1.8 presents the moisture content results after breaking, which showed specimens prepared with 45 blows per lift had average water content 0.2 percentage points lower than the other treatments. This observation was deemed unimportant from a performance standpoint, since no differences in modulus or strength were observed.

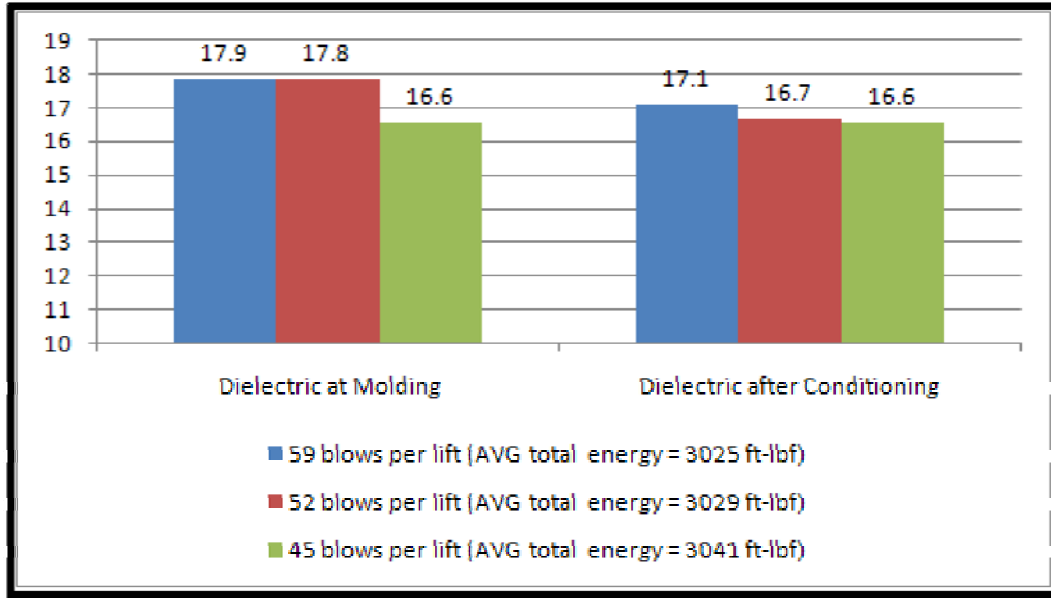


Figure 1.5. Summary of Results from Dielectric Testing.

Note: Each result is the average of three specimens. No significant difference exists among means.

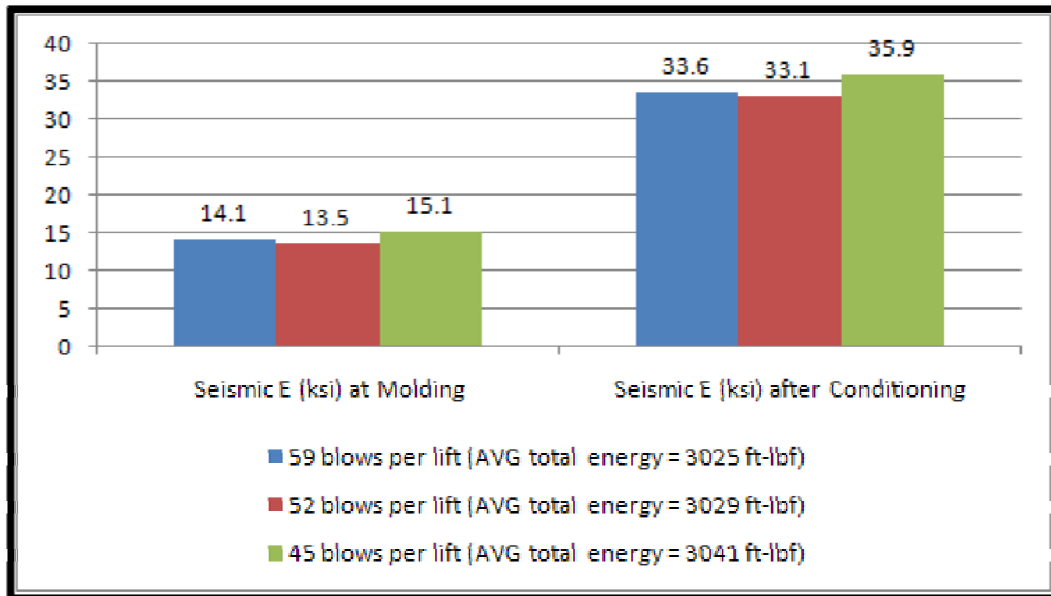


Figure 1.6. Summary of Results from Modulus Testing.

Note: Each result is the average of three specimens. No significant difference exists among means.

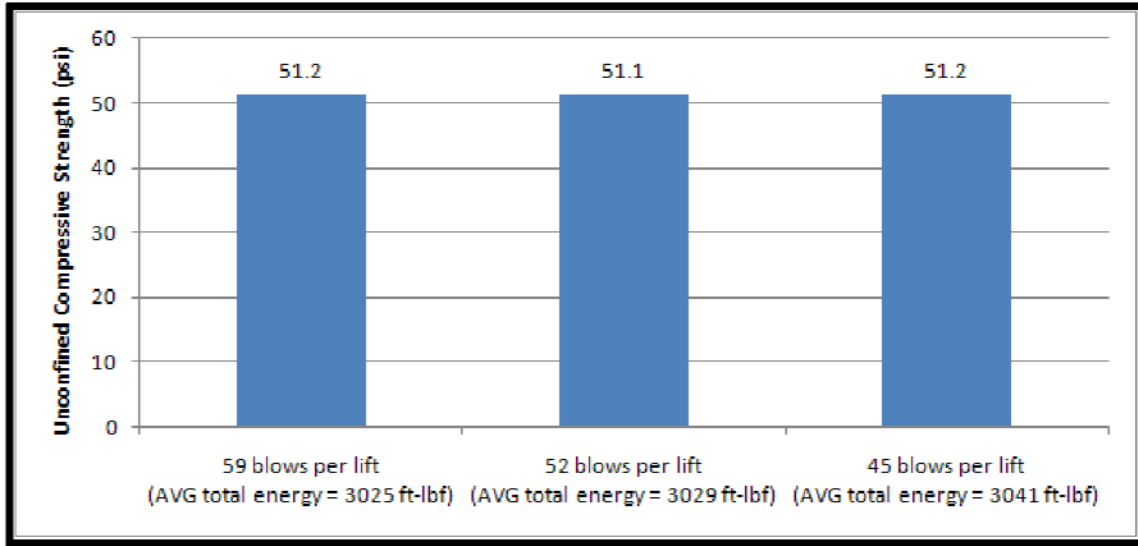


Figure 1.7. Summary of Results from Unconfined Strength Testing after Tex-117-E Part II.
Note: Each result is the average of three specimens. No significant difference exists among means.

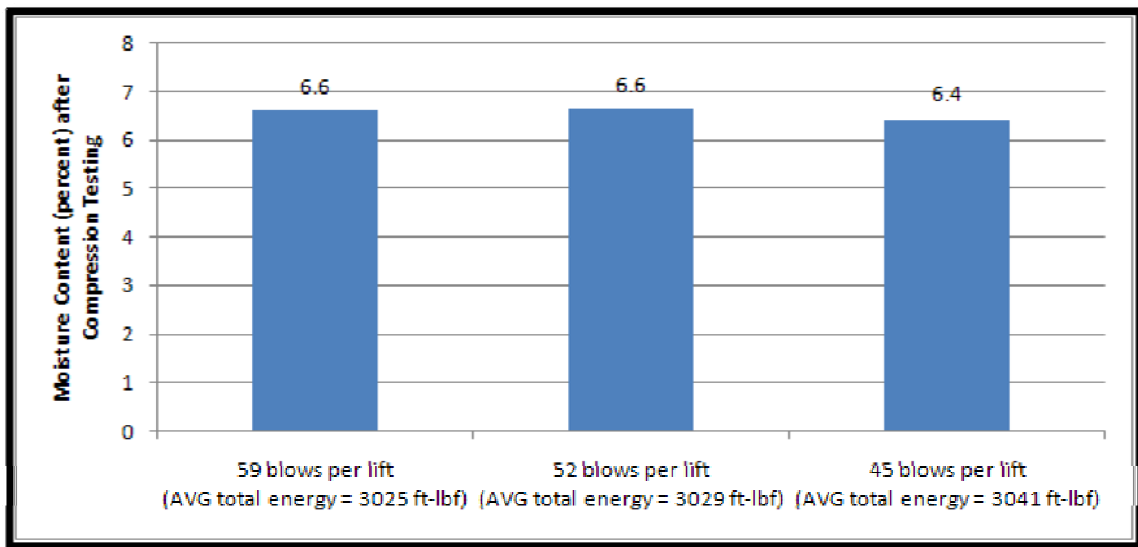


Figure 1.8. Summary of Moisture Contents after Strength Testing.
Note: Each result is the average of three specimens. Mean water content after conditioning from specimens with 45 blows per lift was lower than other treatments.

CONCLUSIONS

The data show the range of blows per lift in Tex-113-E can vary from at least 45 to 60 as long as the total energy per lift is controlled by the SCA to average approximately 750 ft-lbf. In the experiment conducted to determine this finding, the total energy per lift was always between 740 and 765 ft-lbf. When achieving this energy per lift with no less than 45 and no more than 60 blows, no differences in important test results, such as maximum dry density, optimum water content, dielectric constant, seismic modulus, or unconfined compressive strength, existed.

CHAPTER 2. PRECISION OF TEX-113-E COMPACTION WITH THE SCA

SUMMARY

With the implementation of the SCA into Test Method Tex-113-E, TxDOT desired to determine if the precision of the test method improved. To facilitate answering this question, an interlaboratory study was conducted to develop precision statistics for both the applied total compaction energy and effort, and for important measured sample properties including moisture content and specimen dry density. The end of this chapter presents precision statements for each of these parameters. The results show excellent precision of total compaction energy when the SCA is used to control the compactor. Total compaction energy should be repeatable and reproducible within 30 ft-lbf, or approximately 1 percent of the specification value. Compacted dry density should be repeatable within 2 to 3 pounds per cubic foot and reproducible within 3 to 4 pcf.

METHOD FOR INTERLABORATORY STUDY

To develop precision statistics for Tex-113-E compaction, TTI researchers followed American Society for Testing and Materials (ASTM) E691-09. With the help of TxDOT, the participation of six laboratories was obtained. Next, three materials were selected for use in the experiment. These are the minimum participatory and testing requirements for conducting an interlaboratory study (ILS) per E691-09.

To gather the necessary data, the research team recombined samples from each of the materials and delivered three samples of each material to each participating lab. The laboratories then:

- Molded the samples at the provided optimum moisture content.
- Dried the samples and determined sample compacted dry density.
- Reported the compaction energy and density results to TTI.

MATERIALS USED IN ILS

In conjunction with the TxDOT project director, two limestones and one sandstone base were selected for use in the interlaboratory study. Table 2.1 summarizes the key properties of the materials reconstituted for distribution to the participating laboratories.

Table 2.1. Summary of Materials Used in Interlaboratory Study.

| | | Groesbeck | Spicewood | Oklahoma |
|--|-------|------------------|------------------|-----------------|
| Dry Screen Gradation Cumulative Percent Retained | 1 3/4 | 2.5 | 0.0 | 0.0 |
| | 1 1/4 | 14.7 | 4.7 | 1.0 |
| | 7/8 | 29.2 | 15.9 | 11.6 |
| | 5/8 | 41.0 | 26.9 | 28.9 |
| | 3/8 | 54.7 | 42.1 | 44.1 |
| | #4 | 66.8 | 59.3 | 61.5 |
| | #40 | 89.3 | 95.3 | 81.5 |
| Plasticity Index | | 2* | 7 | 6 |
| Wet Ball Mill Value | | 40 | 24 | 36 |
| Percent Soil Binder Increase | | 16 | 6 | 10 |
| Molding Moisture (Tex-113-E Optimum) | | 6.9 | 5.4 | 7.6 |

*Calculated from linear shrinkage.

RESULTS FROM INTERLABORATORY STUDY

Appendix C presents reported data by testing laboratory. The following sections present the worksheets and consistency evaluation for the parameters evaluated. These parameters included:

- Total compaction energy.
- Total compaction effort.
- Sample dry density.

In this ILS, with the number of labs and number of replicates, the critical value of the between-lab consistency statistic h was 1.92, and the critical value of the within-lab consistency statistic k was 1.98. Data generating consistency statistics exceeding these values were investigated for possible sources of error.

Calculation and Display of Statistics—Total Compaction Energy

Tables 2.2–2.4 present each lab’s data and the ILS worksheet for the measured total compaction energy. Figures 2.1 and 2.2 present the between-lab consistency statistic, h , and the within-lab consistency statistic, k , for these data. No problematic patterns were observed in the consistency statistics, and no consistency statistic exceeded the critical value.

Table 2.2. ILS Worksheet for Total Compaction Energy (ft-lbf)—Groesbeck.

| Lab | Sample | | | \bar{x} | s | d | h | k |
|----------------------------------|----------|---------|---------------|-----------|-------|-------|-------|------|
| | 1 | 2 | 3 | | | | | |
| 1 | 3023.16 | 3032.44 | * | 3027.80 | 6.56 | 3.04 | 0.48 | 0.63 |
| 2 | 3017.43 | 3034.27 | 2995.33 | 3015.68 | 19.53 | -9.08 | -1.44 | 1.88 |
| 3 | 3031.28 | 3031.61 | 3037.05 | 3033.31 | 3.24 | 8.56 | 1.36 | 0.31 |
| 4 | 3014.39 | 3022.75 | 3022.8 | 3019.98 | 4.84 | -4.78 | -0.76 | 0.47 |
| 5 | 3034.335 | 3021.4 | * | 3027.87 | 9.15 | 3.11 | 0.49 | 0.88 |
| 6 | 3035.69 | 3019.35 | 3016.66 | 3023.90 | 10.30 | -0.86 | -0.14 | 0.99 |
| *not tested due to sample damage | | | \bar{x} | 3024.76 | | | | |
| | | | $s_{\bar{x}}$ | 6.30 | | | | |
| | | | s_r | 10.39 | | | | |
| | | | $(s_r)^*$ | 10.57 | | | | |

Table 2.3. ILS Worksheet for Total Compaction Energy (ft-lbf)—Spicewood.

| Lab | Sample | | | \bar{x} | s | d | h | k |
|--------------------------------------|---------|---------|---------------|-----------|-------|-------|-------|------|
| | 1 | 2 | 3 | | | | | |
| 1 | 3028.21 | 3019.16 | 3045.63 | 3031.00 | 13.45 | 6.54 | 1.30 | 1.50 |
| 2 | 3025.36 | 3032.06 | 3016.49 | 3024.64 | 7.81 | 0.17 | 0.03 | 0.87 |
| 3 | 3033.85 | 3022.51 | * | 3028.18 | 8.02 | 3.72 | 0.74 | 0.89 |
| 4 | 3006.88 | 3024.14 | 3022.59 | 3017.87 | 9.55 | -6.59 | -1.31 | 1.06 |
| 5 | 3022.79 | 3010.16 | 3025.29 | 3019.41 | 8.11 | -5.05 | -1.00 | 0.90 |
| 6 | 3023.57 | 3022.59 | 3030.88 | 3025.68 | 4.53 | 1.22 | 0.24 | 0.50 |
| *Not tested due to sample prep error | | | \bar{x} | 3024.463 | | | | |
| | | | $s_{\bar{x}}$ | 5.040589 | | | | |
| | | | s_r | 8.979374 | | | | |
| | | | $(s_r)^*$ | 8.897208 | | | | |

Table 2.4. ILS Worksheet for Total Compaction Energy (ft-lbf)—Oklahoma.

| Lab | Sample | | | \bar{x} | s | d | h | k |
|-----|---------|---------|---------|-----------------|----------|-------|-------|------|
| | 1 | 2 | 3 | | | | | |
| 1 | 3026.96 | 3020.14 | 3011.80 | 3019.63 | 7.59 | -6.91 | -1.13 | 0.82 |
| 2 | 3034.71 | 3038.00 | 3030.67 | 3034.46 | 3.67 | 7.91 | 1.29 | 0.40 |
| 3 | 3029.24 | 3038.46 | 3031.31 | 3033.00 | 4.84 | 6.46 | 1.06 | 0.52 |
| 4 | 3025.74 | 3015.02 | 3027.91 | 3022.89 | 6.90 | -3.66 | -0.60 | 0.74 |
| 5 | 3031.00 | 3015.45 | 3019.37 | 3021.94 | 8.09 | -4.61 | -0.75 | 0.87 |
| 6 | 3025.58 | 3010.71 | 3045.75 | 3027.35 | 17.59 | 0.80 | 0.13 | 1.89 |
| | | | | $\bar{\bar{x}}$ | 3026.546 | | | |
| | | | | \bar{s} | 6.121048 | | | |
| | | | | s_r | 9.281308 | | | |
| | | | | $(s_r)^*$ | 9.741442 | | | |

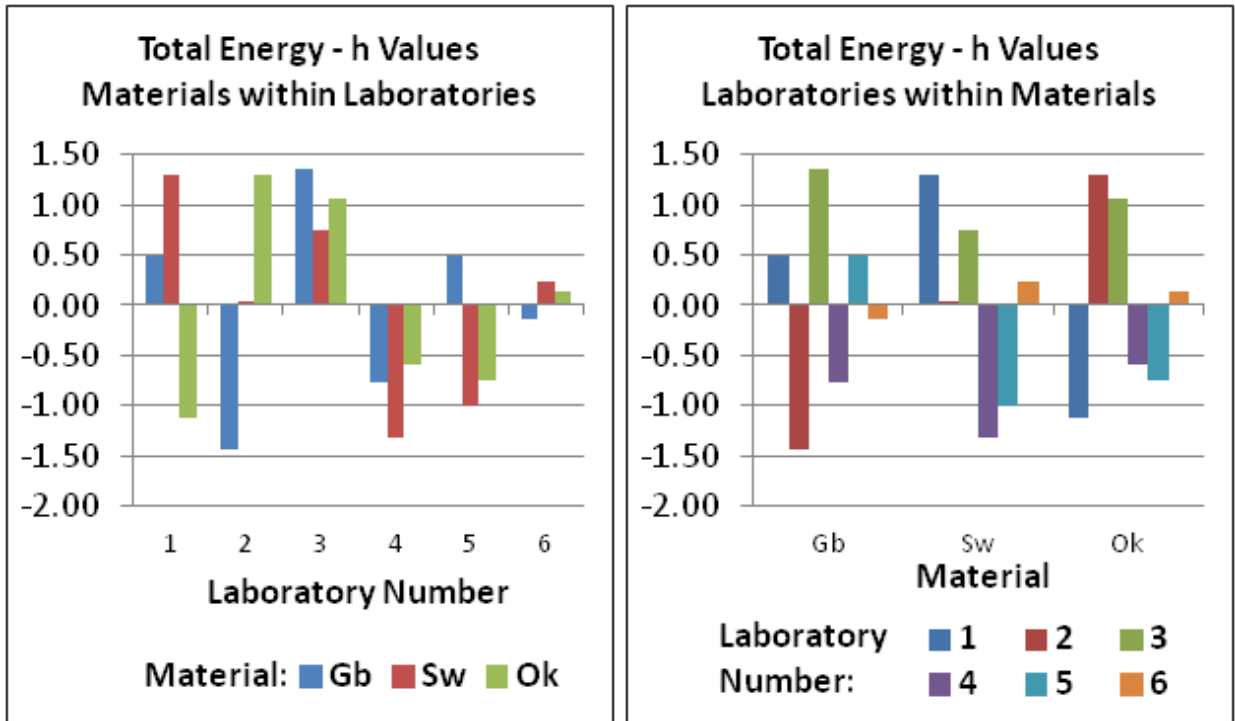


Figure 2.1. Between-Lab Consistency Statistics for Total Compaction Energy.

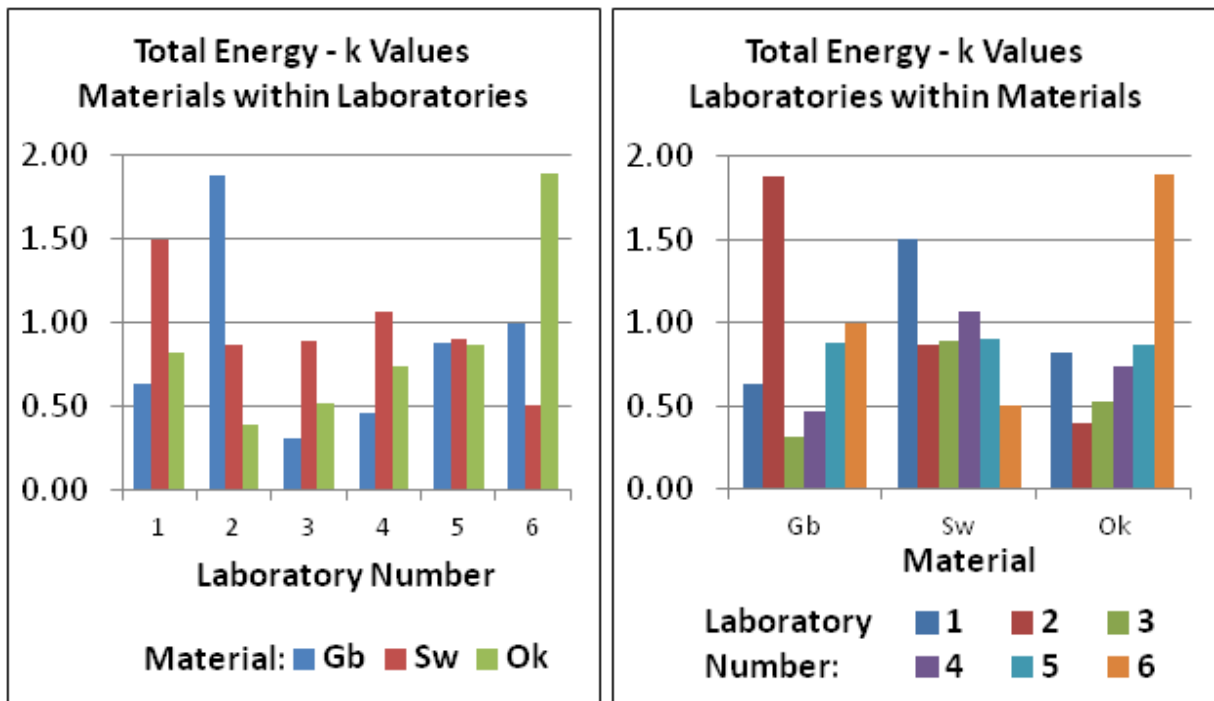


Figure 2.2. Within-Lab Consistency Statistics for Total Compaction Energy.

Calculation and Display of Statistics—Total Compaction Effort

Tables 2.5–2.7 present each lab’s data and the ILS worksheet for the measured total compaction effort. Figures 2.3 and 2.4 present the between-lab consistency statistic, h , and the within-lab consistency statistic, k , for these data. No problematic patterns were observed in the consistency statistics, and no consistency statistic exceeded the critical value.

Table 2.5. ILS Worksheet for Total Compaction Effort (ft-lbf/in³)—Groesbeck.

| Lab | Sample ft-lbf/in ³ | | | \bar{x}_{bar} | s | d | h | k |
|----------------------------------|-------------------------------|-------|---------------------------|------------------------|------|-------|-------|------|
| | 1 | 2 | 3 | | | | | |
| 1 | 13.27 | 13.36 | * | 13.32 | 0.06 | 0.11 | 0.90 | 0.57 |
| 2 | 13.17 | 13.20 | 12.97 | 13.11 | 0.13 | -0.09 | -0.71 | 1.18 |
| 3 | 13.02 | 13.07 | 12.96 | 13.02 | 0.06 | -0.19 | -1.49 | 0.55 |
| 4 | 13.28 | 13.39 | 13.38 | 13.35 | 0.06 | 0.15 | 1.18 | 0.57 |
| 5 | 13.22 | 13.16 | * | 13.19 | 0.04 | -0.02 | -0.12 | 0.38 |
| 6 | 13.26 | 13.02 | 13.42 | 13.23 | 0.20 | 0.03 | 0.24 | 1.87 |
| *not tested due to sample damage | | | \bar{x}_{barbar} | 13.203 | | | | |
| | | | s_{xbar} | 0.1252 | | | | |
| | | | s_r | 0.1067 | | | | |
| | | | $(s_r)^*$ | 0.1526 | | | | |

Table 2.6. ILS Worksheet for Total Compaction Effort (ft-lbf/in³)—Spicewood.

| Lab | Sample | | | \bar{x}_{bar} | s | d | h | k |
|--------------------------------------|--------|-------|--------------------|-----------------|------|-------|-------|------|
| | 1 | 2 | 3 | | | | | |
| 1 | 13.57 | 13.57 | 13.64 | 13.59 | 0.04 | 0.06 | 0.48 | 0.30 |
| 2 | 13.73 | 13.41 | 13.60 | 13.58 | 0.16 | 0.05 | 0.36 | 1.25 |
| 3 | 13.46 | 13.41 | * | 13.44 | 0.04 | -0.09 | -0.73 | 0.31 |
| 4 | 13.75 | 13.77 | 13.67 | 13.73 | 0.05 | 0.20 | 1.57 | 0.41 |
| 5 | 13.66 | 13.46 | 13.29 | 13.47 | 0.19 | -0.06 | -0.49 | 1.43 |
| 6 | 13.37 | 13.20 | 13.57 | 13.38 | 0.19 | -0.15 | -1.19 | 1.43 |
| *Not tested due to sample prep error | | | \bar{x}_{barbar} | 13.53099 | | | | |
| | | | S_{xbar} | 0.129047 | | | | |
| | | | S_r | 0.129985 | | | | |
| | | | $(S_r)^*$ | 0.167084 | | | | |

Table 2.7. ILS Worksheet for Total Compaction Effort (ft-lbf/in³)—Oklahoma.

| Lab | Sample | | | \bar{x}_{bar} | s | d | h | k |
|-----|--------|-------|--------------------|-----------------|------|-------|-------|------|
| | 1 | 2 | 3 | | | | | |
| 1 | 13.42 | 13.01 | 13.54 | 13.32 | 0.28 | -0.06 | -0.25 | 1.82 |
| 2 | 13.52 | 13.54 | 13.53 | 13.53 | 0.01 | 0.15 | 0.67 | 0.09 |
| 3 | 13.23 | 13.23 | 13.25 | 13.24 | 0.01 | -0.14 | -0.64 | 0.04 |
| 4 | 13.83 | 13.77 | 13.69 | 13.76 | 0.07 | 0.38 | 1.72 | 0.45 |
| 5 | 13.09 | 13.27 | 13.27 | 13.21 | 0.11 | -0.17 | -0.77 | 0.69 |
| 6 | 13.05 | 13.15 | 13.47 | 13.22 | 0.22 | -0.16 | -0.72 | 1.41 |
| | | | \bar{x}_{barbar} | 13.3808 | | | | |
| | | | S_{xbar} | 0.22271 | | | | |
| | | | S_r | 0.15388 | | | | |
| | | | $(S_r)^*$ | 0.25571 | | | | |

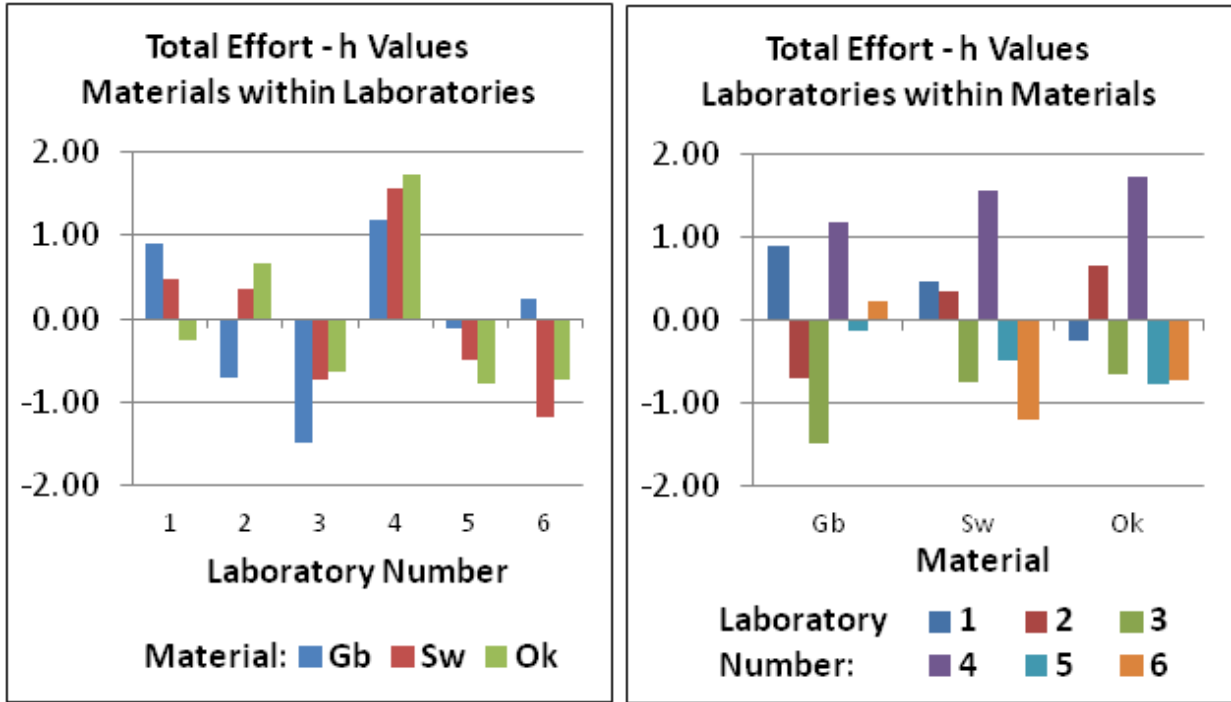


Figure 2.3. Between-Lab Consistency Statistics for Total Compaction Effort.

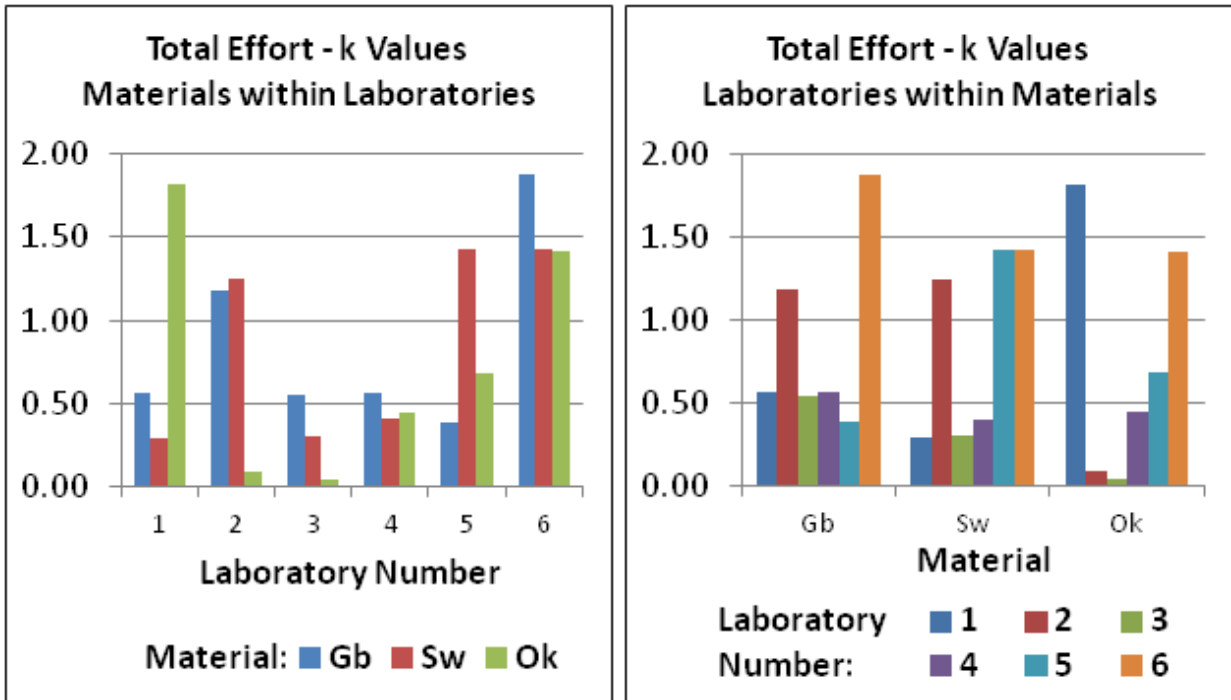


Figure 2.4. Within-Lab Consistency Statistics for Total Compaction Effort.

Calculation and Display of Statistics—Sample Dry Density

Tables 2.8–2.10 present each lab’s data and the ILS worksheet for molded sample dry density. Figures 2.5 and 2.6 present the between-lab consistency statistic, h , and the within-lab consistency statistic, k , for these data. While no problematic patterns were observed in the consistency statistics, the k within-lab consistency statistic for lab 6 exceeded the critical value. The data were examined, and no procedural or tabulation errors were discovered, so the data were retained for use in the tabulation of the precision statistics.

Table 2.8. ILS Worksheet for Dry Density (pcf)—Groesbeck.

| Lab | Sample | | | \bar{x}_{bar} | s | d | h | k |
|----------------------------------|--------|--------|---------------------------|------------------------|------|-------|-------|------|
| | 1 | 2 | 3 | | | | | |
| 1 | 137.00 | 136.30 | * | 136.65 | 0.49 | 0.79 | 1.21 | 0.50 |
| 2 | 136.90 | 136.90 | 136.00 | 136.60 | 0.52 | 0.74 | 1.13 | 0.52 |
| 3 | 135.60 | 135.50 | 134.10 | 135.07 | 0.84 | -0.80 | -1.22 | 0.84 |
| 4 | 135.30 | 135.60 | 135.20 | 135.37 | 0.21 | -0.50 | -0.76 | 0.21 |
| 5 | 135.59 | 135.60 | * | 135.60 | 0.01 | -0.27 | -0.41 | 0.01 |
| 6 | 135.81 | 133.78 | 138.12 | 135.90 | 2.17 | 0.04 | 0.06 | 2.18 |
| *not tested due to sample damage | | | \bar{x}_{barbar} | 135.864 | | | | |
| | | | S_{xbar} | 0.65061 | | | | |
| | | | S_r | 0.99809 | | | | |
| | | | $(S_r)^*$ | 1.0428 | | | | |

Table 2.9. ILS Worksheet for Dry Density (pcf)—Spicewood.

| Lab # | Sample | | | \bar{x}_{bar} | s | d | h | k |
|--------------------------------------|--------|--------|---------------------------|------------------------|------|-------|-------|------|
| | 1 | 2 | 3 | | | | | |
| 1 | 149.50 | 149.70 | 149.20 | 149.47 | 0.25 | 0.92 | 0.70 | 0.39 |
| 2 | 150.10 | 150.50 | 149.90 | 150.17 | 0.31 | 1.62 | 1.24 | 0.47 |
| 3 | 149.00 | 148.70 | * | 148.85 | 0.21 | 0.30 | 0.23 | 0.33 |
| 4 | 149.00 | 148.50 | 147.50 | 148.33 | 0.76 | -0.22 | -0.17 | 1.19 |
| 5 | 148.90 | 148.20 | 147.20 | 148.10 | 0.85 | -0.45 | -0.35 | 1.33 |
| 6 | 146.38 | 145.40 | 147.37 | 146.38 | 0.99 | -2.17 | -1.66 | 1.53 |
| *Not tested due to sample prep error | | | \bar{x}_{barbar} | 148.55 | | | | |
| | | | S_{xbar} | 1.302903 | | | | |
| | | | S_r | 0.643588 | | | | |
| | | | $(S_r)^*$ | 1.404882 | | | | |

Table 2.10. ILS Worksheet for Dry Density (pcf)—Oklahoma.

| Lab | Sample | | | \bar{x} | s | d | h | k |
|-----|--------|--------|--------|-----------------|--------|-------|-------|------|
| | 1 | 2 | 3 | | | | | |
| 1 | 136.10 | 136.20 | 136.20 | 136.17 | 0.06 | 0.06 | 0.09 | 0.06 |
| 2 | 136.30 | 136.40 | 135.00 | 135.90 | 0.78 | -0.21 | -0.30 | 0.82 |
| 3 | 135.50 | 136.20 | 136.70 | 136.13 | 0.60 | 0.03 | 0.04 | 0.63 |
| 4 | 137.30 | 138.00 | 136.80 | 137.37 | 0.60 | 1.26 | 1.84 | 0.63 |
| 5 | 133.70 | 136.70 | 136.70 | 135.70 | 1.73 | -0.41 | -0.59 | 1.81 |
| 6 | 134.14 | 135.99 | 135.99 | 135.37 | 1.07 | -0.73 | -1.07 | 1.12 |
| | | | | $\bar{\bar{x}}$ | 136.11 | | | |
| | | | | \bar{s} | 0.6838 | | | |
| | | | | s_r | 0.9558 | | | |
| | | | | $(s_r)^*$ | 1.0376 | | | |

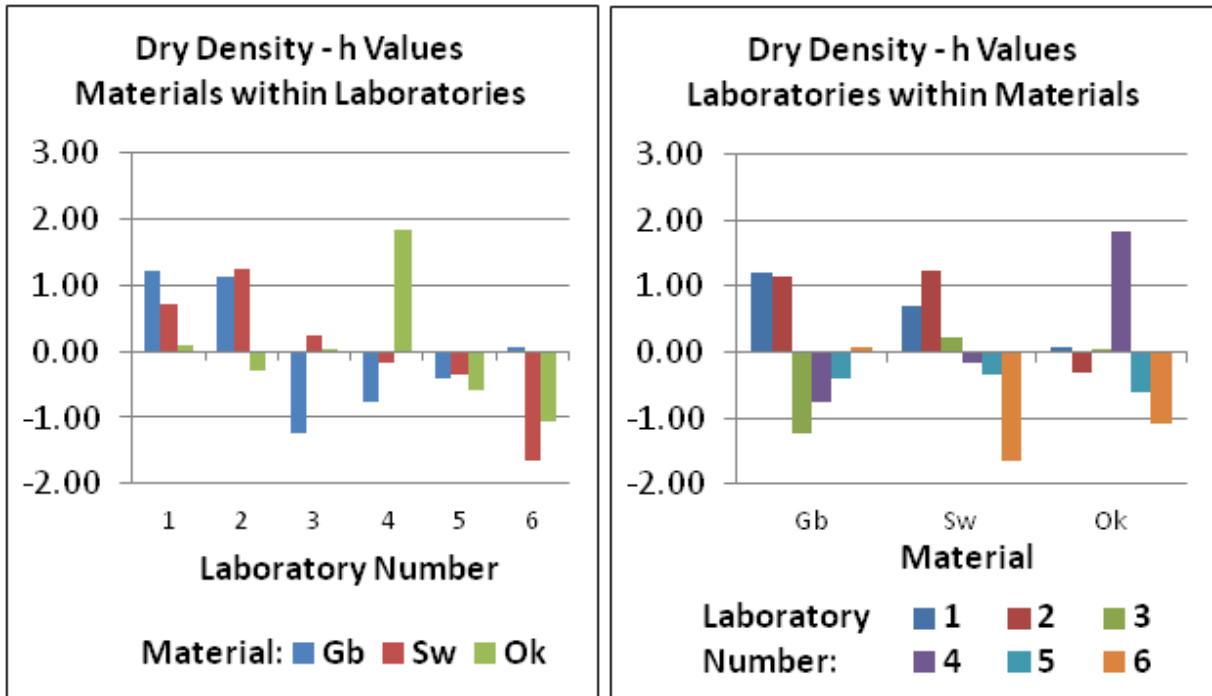


Figure 2.5. Between-Lab Consistency Statistics for Dry Density.

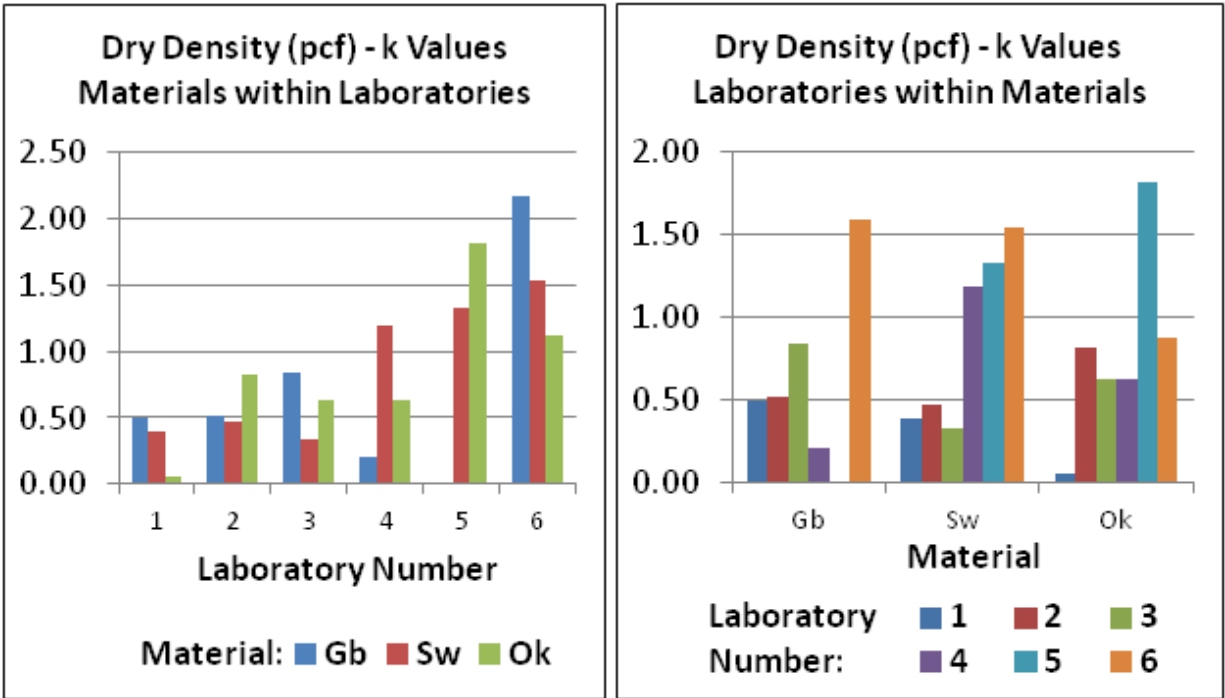


Figure 2.6. Within-Lab Consistency Statistics for Dry Density.

PRESENTATION OF PRECISION STATISTICS

Based upon the ILS worksheets in Tables 2.2–2.10, the precision statistics for total compaction energy, total compaction effort, and sample dry density are presented in Tables 2.11 through 2.13. The results suggest:

- Total compaction energy applied in Tex-113-E with the SCA exhibits excellent precision. The specification total compaction energy is 3000 ft-lbf. Both the repeatability and reproducibility limit are around 30 ft-lbf, or about 1 percent of the specification value.
- Total compaction effort exhibits good precision, with repeatability and reproducibility limits typically between 0.3 and 0.5 ft-lbf/in³, or approximately 5 percent of the specification value.
- Density should be repeatable within 2 to 3 pcf and reproducible within 3 to 4 pcf.

Table 2.11. Precision Statistics for Total Compaction Energy (ft-lbf) in Tex-113-E.

| Material | X bar | S _{xbar} | S _r | S _R | r | R |
|-----------|--------|-------------------|----------------|----------------|-------|-------|
| Groesbeck | 3024.8 | 6.30 | 10.39 | 10.57 | 29.10 | 29.58 |
| Spicewood | 3024.5 | 5.04 | 8.98 | 8.89 | 25.14 | 25.14 |
| Oklahoma | 3026.6 | 6.12 | 9.28 | 9.74 | 25.98 | 27.23 |

Table 2.12. Precision Statistics for Total Compaction Effort (ft-lbf/in³) in Tex-113-E.

| Material | X bar | S_{xbar} | Sr | S_R | r | R |
|------------------|--------------|-------------------------|-----------|----------------------|----------|----------|
| Groesbeck | 13.20 | 0.125 | 0.107 | 0.153 | 0.299 | 0.427 |
| Spicewood | 13.53 | 0.129 | 0.130 | 0.167 | 0.364 | 0.468 |
| Oklahoma | 13.38 | 0.223 | 0.154 | 0.256 | 0.431 | 0.716 |

Table 2.13. Precision Statistics for Sample Dry Density (pcf) after Tex-117-E Part II.

| Material | X bar | S_{xbar} | Sr | S_R | r | R |
|------------------|--------------|-------------------------|-----------|----------------------|----------|----------|
| Groesbeck | 135.9 | 0.65 | 1.00 | 1.04 | 2.79 | 2.91 |
| Spicewood | 148.6 | 1.30 | 0.64 | 1.40 | 1.80 | 3.93 |
| Oklahoma | 136.1 | 0.68 | 0.96 | 1.04 | 2.68 | 2.90 |

While ASTM E 691 does not call for pooling data from different materials to determine globally-applicable precision estimates, for purposes of provided a single numeric precision estimate to TxDOT the research team determined the pooled repeatability and reproducibility standard deviations. These pooled standard deviations allow for estimating a single repeatability and reproducibility limit as Table 2.14 presents.

Table 2.14. Precision Estimates from Pooled Data.

| | Energy (ft-lbf) | Effort (ft-lbf/in³) | Dry Density (pcf) |
|------------------------------|------------------------|---------------------------------------|--------------------------|
| Repeatability Limit | 26.80 | 0.368 | 2.46 |
| Reproducibility Limit | 27.32 | 0.552 | 3.29 |

CONCLUSIONS

The SCA addresses equipment variability during the sample fabrication process, and this interlaboratory study demonstrated that the SCA provides excellent precision in the application of compaction energy during that process. With the implementation of the SCA, TxDOT should generally expect the total compaction energy among samples to differ by no more than 27 ft-lbf. Additionally, the compacted dry density of samples constructed with Tex-113-E compaction should generally be repeatable within about 2.5 pcf and reproducible within about 3.3 pcf.

CHAPTER 3. CONCLUSIONS AND RECOMMENDATIONS

CONCLUSIONS AND RECOMMENDATIONS ON MACHINE OPERATIONAL TOLERANCES

Many factors in the stages of sample fabrication, conditioning, and testing can impact the precision of strength results in Tex-117-E Part II. Since this test method is a specification requirement in Item 247, achieving the most homogenous compaction is in the best interest of producers, contractors, and the state. This project focused on homogenizing the application of compaction energy during the sample fabrication process. The impact of varying hammer weights and drop heights, while the Soil Compactor Analyzer controlled compaction to apply between 740 to 760 ft-lbf total energy per lift, was evaluated with a particular focus on:

- Moisture-density relationship.
- Molded specimen dry density when molded at Tex-113-E optimum.
- Specimen dielectric constant immediately after molding and after Tex-117-E Part II conditioning.
- Seismic modulus immediately after molding and after Tex-117-E Part II conditioning.
- Unconfined compressive strength after Tex-117-E Part II.
- Percent moisture after Tex-117-E Part II.

The results showed that while using the current TxDOT-approved SCA to control total energy per lift between 740 and 765 ft-lbf, the number of blows per lift may vary between 45 and 60 with no impact on important test results. TxDOT should require the prescribed amount of energy to be obtained within this number of blows per lift.

CONCLUSIONS AND RECOMMENDATIONS FROM INTERLABORATORY STUDY

As a final stage in this project, an interlaboratory study was conducted to develop precision statistics for total compaction energy, total compaction effort, and specimen dry density when molded at Tex-113-E optimum. These results showed that the SCA enables excellent precision of total compaction energy and good precision of total compaction effort. TxDOT should generally expect the total compaction energy among samples constructed with Tex-113-E to differ by no more than 27 ft-lbf and incorporate that precision information into the test procedure.

The dry density of replicate samples constructed at optimum water content within a single lab should generally not vary by more than 2 to 3 pcf, with 2.5 pcf representing the pooled repeatability limit. The dry density of replicate samples compacted at different labs should generally not vary by more than 3 to 4 pcf, with 3.3 pcf representing the pooled reproducibility limit. The precision statement for dry density should be added to the Tex-113-E test procedure.

**APPENDIX A: TEST REPORT FROM FLEX BASE USED IN IMPACT
HAMMER ADJUSTMENTS**



TEXAS DEPARTMENT OF TRANSPORTATION

BAR LINEAR SHRINKAGE
TEX-107-E

Refresh Workbook

File Version: 08/26/09 23:36:38

| | | | |
|------------------|-------------|--------------------|-------------|
| SAMPLE ID: | | SAMPLED DATE: | 03/04/2010 |
| TEST NUMBER: | 10-074 | LETTING DATE: | |
| SAMPLE STATUS: | | CONTROLLING CSJ: | 0456-03-015 |
| COUNTY: | FREESTONE | SPEC YEAR: | 2004 |
| SAMPLED BY: | BA | SPEC ITEM: | 247 |
| SAMPLE LOCATION: | STKPL#01-10 | SPECIAL PROVISION: | |
| MATERIAL CODE: | | MIX TYPE / GRADE: | 2 |
| MATERIAL NAME: | | | |
| PRODUCER: | VULCAN | | |
| AREA ENGINEER: | | PROJECT MANAGER: | |
| COURSE/LIFT: | | STATION: | |
| | | DIST. FROM CL: | |

Bar Linear Shrinkage - Tex-107-E

| Unit | Initial Length (percent) | Final Length (percent) | Linear Shrinkage |
|---------|--------------------------|------------------------|------------------|
| percent | 100 | 99 | 1.0 |

Calculate Plasticity Index from Bar Linear Shrinkage? Yes

Plasticity Index Calculated from Linear Shrinkage: 1.8

Remarks:

ROUNDS UP TO A 2.0 PI

| | | |
|------------------|------------------|-----------------------------|
| Test Method: | Tested By: | Tested Date: |
| TX107 | TERRY GREEN | 03/18/10 |
| Test Stamp Code: | Omit Test: | Completed Date: Revised By: |
| | | |
| Locked By: | TxDOT: | District: Area: |
| | | |
| Authorized By: | Authorized Date: | |
| | | |



TEXAS DEPARTMENT OF TRANSPORTATION

PARTICLE SIZE ANALYSIS
Tex-110-E

Refresh Workbook

File Version: 10/06/09 11:04:06

| | | | |
|------------------|-------------|--------------------|-------------|
| SAMPLE ID: | | SAMPLED DATE: | 03/04/2010 |
| TEST NUMBER: | 10-074 | LETTING DATE: | |
| SAMPLE STATUS: | | CONTROLLING CS.J: | 0456-03-015 |
| COUNTY: | FREESTONE | SPEC YEAR: | 2004 |
| SAMPLED BY: | BA | SPEC ITEM: | 247 |
| SAMPLE LOCATION: | STKPL#01-10 | SPECIAL PROVISION: | |
| MATERIAL CODE: | | GRADE: | 2 |
| MATERIAL NAME: | | | |
| PRODUCER: | VULCAN | | |
| AREA ENGINEER: | | PROJECT MANAGER: | |
| COURSE/LIFT: | | STATION: | |
| | | DIST. FROM CL: | |

Particle Size Analysis - Tex-110-E

| Sieve Size | Cumulative | Individual Weight Retained | Cumulative Percent Retained | Lower Spec Limit % | Upper Spec Limit % | Within Master Grading |
|------------|--------------------------------|----------------------------|-----------------------------|--------------------|--------------------|-----------------------|
| | Cumulative Weight Retained (g) | | | | | |
| 2-1/2" | 0 | 0 | 0.0 | 0 | 0 | Yes |
| 1-3/4" | 0 | 0 | 0.0 | 0 | 10 | Yes |
| No. 4 | 3233.8 | 3233.8 | 64.7 | 45 | 75 | Yes |
| No. 40 | 3780.8 | 547 | 75.6 | 60 | 85 | Yes |
| | | | | | | |
| | | | | | | |
| Total: | 5000.00 | | | | | |

Remarks:

| |
|--|
| |
|--|

| | | |
|------------------|------------------|-----------------|
| Test Method: | Tested By: | Tested Date: |
| TX110 | TERRY GREEN | 03/16/10 |
| Test Stamp Code: | Omit Test: | Completed Date: |
| | | |
| Reviewed By: | | |
| Locked By: | TxDOT: | District: |
| | | |
| Area: | | |
| Authorized By: | Authorized Date: | |
| | | |

**APPENDIX B: RESULTS FROM SPECIMENS TESTED FOR IMPACT
HAMMER ADJUSTMENTS**

Table B.1. Results from Samples Targeting 12.5 ft-lbf per Blow.

| | | Sample ID | 113-E Moisture-Density Samples | | | | | | | | | | | | Test samples at 113-E Optimum | | |
|--|--|--------------------------------|--------------------------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------------|-------------------------------|-----------|---------|
| | | | Group 4 | | | | Group 5 | | | | Group 6 | | | | 1 | 2 | 3 |
| | | | 1 | 2 | 3 | 4 | 1 | 2 | 3 | 4 | 1 | 2 | 3 | 4 | 1 | 2 | 3 |
| Data after Tex-117-E part II Conditioning | Molding Data | Hammer Weight | 10.089 | 10.089 | 10.089 | 10.089 | 10.089 | 10.089 | 10.089 | 10.089 | 10.089 | 10.089 | 10.089 | 10.089 | 10.31 | 10.31 | 10.31 |
| | | AVG drop ht (in) | 15.28 | 15.03 | 16.25 | 16.88 | 16.60 | 14.84 | 15.92 | 14.21 | 16.37 | 15.45 | 16.23 | 16.43 | 16.43 | 17.32 | 17.49 |
| | | Lift 1 # drops | 60 | 60 | 61 | 61 | 60* | 61 | 62 | 62 | 65 | 62 | 62 | 64 | 58 | 59 | 60 |
| | | Total Energy (ft-lbf) | 746.63 | 750.35 | 742.85 | 744.74 | 745.95 | 750.5 | 748.7 | 749.01 | 747.85 | 751.34 | 751.1 | 751.1 | 751.41 | 759.32 | 756.35 |
| | | AVG drop ht (in) | | 15.63 | 16.07 | 16.1 | 16.91 | 15.23 | | 14.86 | 16.31 | 16.17 | 16.56 | 16.72 | 17.35 | 17.49 | 16.79 |
| | | Lift 2 # drops | 65* | 62 | 61 | 61 | 60 | 63 | 60* | 57 | 64 | 57 | 62 | 61 | 58 | 58 | 60 |
| | | Total Energy (ft-lbf) | | 749.7 | 749.93 | 752.97 | 745.66 | 756.18 | | 750.07 | 751.81 | 747.76 | 754.87 | 747.25 | 757.39 | 750.8 | 757.82 |
| | | AVG drop ht (in) | 16.74 | 14.45 | 14.05 | 14.22 | 16.38 | 16.22 | 16.37 | 16.76 | 16.67 | | 14.65 | 15.95 | 17.3 | 17.49 | 17.5 |
| | | Lift 3 # drops | 61 | 61 | 62 | 54 | 60 | 62 | 60 | 63 | 63 | 65* | 63 | 62 | 58 | 58 | 58 |
| | | Total Energy (ft-lbf) | 745.1 | 743.3 | 752.81 | 748.58 | 745.75 | 754.72 | 746.41 | 761.82 | 743.06 | | 751.54 | 751.19 | 754.76 | 762.43 | 757.61 |
| | | AVG drop ht (in) | 15.15 | 16.25 | 16.6 | 14.07 | 16.15 | 16.67 | 16.99 | 17.17 | 15.39 | | 14.79 | | 17.5 | 17.49 | 16.91 |
| | | Lift 4 # drops | 61 | 60 | 60 | 64 | 61 | 58 | 61 | 61 | 63 | 65* | 62 | 60* | 58 | 58 | 58 |
| | | Total Energy (ft-lbf) | 743.8 | 743.58 | 744.97 | 748.91 | 747.69 | 750.49 | 753.91 | 750.8 | 748.17 | | 750.92 | | 753.41 | 761.36 | 752.93 |
| | | Total Energy Measured (ft-lbf) | 2235.53 | 2986.93 | 2990.56 | 2995.2 | 2239.1 | 3007.34 | 2250.82 | 3011.39 | 2992.05 | 1495.61 | 3008.67 | 2249.54 | 3016.97 | 3033.91 | 3024.72 |
| | Sample Ht (in) | 8.2 | 8 | 8 | 8 | 8.4 | 8.1 | 8 | 8 | 8 | 8.1 | 7.9 | 7.8 | 7.9 | 8.05 | 8 | |
| | Sample Volume (ft³) | 0.134172 | 0.1309 | 0.1309 | 0.1309 | 0.137445 | 0.132536 | 0.1309 | 0.1309 | 0.1309 | 0.132536 | 0.129263 | 0.127627 | 0.1292634 | 0.1317178 | 0.1308997 | |
| | Effort Measured [(ft-lbf/ft³)] | 16661.65 | 22818.46 | 22846.2 | 22881.64 | 16290.92 | 22690.75 | 17105 | 23005.32 | 22857.58 | 11284.56 | 23275.67 | 17625.67 | 23330.699 | 23033.406 | 23107.159 | |
| | Molded water content (%) | 5 | 6 | 7 | 8 | 5 | 6 | 7 | 8 | 5 | 6 | 7 | 8 | 6.9 | 6.9 | 6.9 | |
| | Sample dry density (pcf) | 133.2 | 137.1 | 137.1 | 137.26 | 130.93 | 135.02 | 137.17 | 136.8 | 135.22 | 135.85 | 139.2 | 137.17 | 139.21 | 136.7 | 137.63 | |
| | Max dry density (pcf) | | 137.6 | | | | 137.1 | | | | 138 | | | | Not Applicable | | |
| Optimum Water Content (%) | | 6.8 | | | | 7.1 | | | | 6.8 | | | | Not Applicable | | | |
| Dielectric at Molding | Reading 1 | 12.2 | 17.1 | 16.3 | 17 | 13 | 16.3 | 18.9 | 21.9 | 13.9 | 17.2 | 17.9 | 18.1 | 19.2 | 18.8 | 16 | |
| | Reading 2 | 12.9 | 16.7 | 17.5 | 19.6 | 15.1 | 16.3 | 17 | 16.7 | 13.7 | 11 | 18.2 | 19.7 | 18.9 | 17.6 | 16 | |
| | Reading 3 | 13.6 | 15.6 | 19.1 | 20.9 | 14.7 | 14 | 19.9 | 18.5 | 13.9 | 12.7 | 17.7 | 19.5 | 17.9 | 17.4 | 17.9 | |
| | Reading 4 | 13 | 16.6 | 17.9 | 21.2 | 14.7 | 17.2 | 19 | 20 | 12 | 16.9 | 18.6 | 17.2 | 18.4 | 19.2 | 16 | |
| | Reading 5 | 14.1 | 15.8 | 17.1 | 22 | 14.7 | 17.7 | 17.1 | 19.2 | 11.8 | 14.7 | 19.2 | 17.3 | 19.9 | 17.4 | 17.5 | |
| AVG Dielectric at Molding | 13.16 | 16.36 | 17.58 | 20.14 | 14.44 | 16.3 | 18.38 | 19.26 | 13.06 | 15.1 | 18.32 | 18.36 | 18.86 | 18.08 | 16.68 | | |
| Seismic E at Molding | Reading 1 | 9 | 26.7 | 22.6 | 9.2 | 53.1 | 47.3 | 9.2 | 15.2 | 14.7 | 22.4 | 9.2 | 9 | 9.3 | 15 | 22.7 | |
| | Reading 2 | 24.2 | 22.4 | 13.5 | 10.6 | 38.7 | 31.2 | 7.9 | 7.9 | 10.2 | 22.4 | 7.9 | 5.5 | 8 | 15 | 16.9 | |
| | Reading 3 | 19.5 | 17.3 | 11.9 | 10.1 | 32.7 | 36.2 | 7.5 | 10.1 | 8.9 | 28.2 | 6.7 | 7.1 | 9.3 | 11 | 16.3 | |
| AVG Seismic E at Molding | 17.56667 | 22.13333 | 16 | 9.966667 | 41.5 | 38.23333 | 8.2 | 11.06667 | 11.26667 | 24.33333 | 7.933333 | 7.3 | 8.866667 | 14.666667 | 18.633333 | | |
| Seismic E Values | Water content (%) after conditioning | 4.73 | 5.82 | 6.59 | 7.48 | 4.67 | 5.78 | 6.7 | 7.56 | 4.72 | 5.69 | 6.65 | 7.5 | 6.5 | 6.61 | 6.62 | |
| | Reading 1 | 12.4 | 15.6 | 17.4 | 16.7 | 13.1 | 15.5 | 18.4 | 15.1 | 12.7 | 16.4 | 18.1 | 17.4 | 18 | 17 | 16 | |
| | Reading 2 | 11.2 | 15.5 | 14 | 16.8 | 11.4 | 16 | 17.5 | 14.6 | 11.3 | 12.5 | 16.2 | 18.5 | 17.3 | 18.6 | 16.2 | |
| | Reading 3 | 11.9 | 15 | 15.5 | 19.7 | 9.8 | 13 | 17.2 | 18.4 | 12.2 | 13.2 | 16.4 | 18.5 | 18.1 | 16.1 | 15.4 | |
| | Reading 4 | 12.4 | 15.9 | 16.5 | 16.6 | 13.8 | 16.7 | 18.3 | 16.9 | 11.9 | 13.9 | 19.9 | 13.8 | 18.8 | 16.7 | 17.5 | |
| | Reading 5 | 12.7 | 14.3 | 16.4 | 17.9 | 13.3 | 17.8 | 17.7 | 19.9 | 11.6 | 15 | 17.5 | 17 | 18.6 | 15.2 | 16.5 | |
| | AVG Dielectric after conditioning | 12.12 | 15.26 | 15.96 | 17.54 | 12.28 | 15.8 | 17.82 | 16.98 | 11.94 | 14.2 | 17.62 | 17.04 | 18.16 | 16.72 | 16.32 | |
| | Reading 1 | 59.2 | 47.4 | 60.5 | 9.2 | 41.5 | 47.3 | 15.1 | 22.7 | 18.1 | 67 | 36.7 | 26.4 | 26.9 | 31.2 | 41.8 | |
| | Reading 2 | 38.4 | 36.3 | 42 | 29.4 | 36.1 | 44.4 | 15.1 | 20.7 | 18.1 | 53.6 | 24.8 | 16.6 | 24.7 | 31.2 | 39.1 | |
| | Reading 3 | 41.1 | 36.3 | 36.5 | 21.4 | 36.1 | 43.4 | 16.3 | 17.6 | 18.1 | 51.5 | 21.3 | 18.4 | 24 | 45.4 | 38.2 | |
| | AVG Seismic E after conditioning | 46.23333 | 40 | 46.33333 | 20 | 37.9 | 45.03333 | 15.5 | 20.33333 | 18.1 | 57.36667 | 27.6 | 20.46667 | 25.2 | 35.03333 | 39.7 | |
| | Unconfined Compressive Strength (psi) | 42.1 | 56.1 | 51.1 | 35.1 | 55.3 | 55.1 | 41.0 | 21.8 | 44.1 | 83.8 | 55.9 | 26.6 | 42.6 | 61.1 | 46.7 | |
| | Water content (%) after compression test | 4.73 | 5.82 | 6.59 | 7.48 | 4.67 | 5.78 | 6.7 | 7.56 | 4.72 | 5.69 | 6.65 | 7.5 | 6.5 | 6.61 | 6.62 | |
| *Drop count estimated due to SCA software lockup | | | | | | | | | | | | | | | | | |

Table B.2. Results from Samples Targeting 15 ft-lbf per Blow.

| | | 113-E Moisture-Density Samples | | | | | | | | | | | | | | | | |
|---|--|--------------------------------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------------|-------------------------------|-----------|-----------|--------|
| | | Sample ID | Group 1 | | | | Group 2 | | | | Group 3 | | | | Test samples at 113-E Optimum | | | |
| | | | 1 | 2 | 3 | 4 | 1 | 2 | 3 | 4 | 1 | 2 | 3 | 4 | 1 | 2 | 3 | |
| Molding Data | | Hammer Weight | 11.041 | 11.041 | 11.041 | 11.041 | 11.041 | 11.041 | 11.041 | 11.041 | 11.041 | 11.041 | 11.041 | 11.041 | 11.041 | 11.041 | 11.041 | 11.041 |
| | | AVG drop ht (in) | 17.83 | 17.05 | 16.96 | 17.57 | 18.41 | | 17.79 | 17.8 | 18.41 | 18.41 | 18.41 | 18.41 | 17.49 | 18.23 | 18.22 | 18.24 |
| | Lift 1 | # drops | 58 | 52 | 53 | 54 | 49 | 55* | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 52 | 52 | 52 |
| | | Total Energy (ft-lbf) | 746.66 | 744.36 | 749.77 | 746.09 | 745.1 | | 753.95 | 742.51 | 755.72 | 753.37 | 750.39 | 757.81 | 758.53 | 752.24 | 759.26 | |
| | | AVG drop ht (in) | 17.49 | 17.55 | 17.6 | | 18.16 | | 17.37 | 18.4 | | 17.79 | 18.17 | 17.27 | 18.23 | 18.23 | 18.22 | |
| | Lift 2 | # drops | 56 | 48 | 49 | 60* | 49 | | 50 | 50 | 50* | 50 | 50 | 50 | 50 | 52 | 52 | 52 |
| | | Total Energy (ft-lbf) | 748.19 | 750.8 | 751.38 | | 744 | | 750.21 | 747.13 | | 743.68 | 755.01 | 750.49 | 764.72 | 750.61 | 758.71 | |
| | | AVG drop ht (in) | 17.79 | 18.3 | 17.83 | 18.31 | 18.39 | | 18.16 | 17.98 | 17.38 | 17.84 | 18.39 | 17.21 | 18.22 | 18.22 | 18.22 | |
| | Lift 3 | # drops | 55 | 50 | 56 | 64 | 49 | | 50 | 50 | 52 | 51 | 50 | 50 | 52 | 52 | 52 | 52 |
| | | Total Energy (ft-lbf) | 744.31 | 748.01 | 753.05 | 752.3 | 747.32 | | 752.18 | 744.99 | 756.73 | 756.88 | 751.74 | 743.69 | 760.68 | 757.89 | 752.5 | |
| | | AVG drop ht (in) | 17.51 | 18.31 | 18.35 | 18.33 | 17.66 | | 17.96 | 17.5 | 18.42 | 17.47 | | 17.83 | 18.22 | 18.23 | 18.21 | |
| | Lift 4 | # drops | 55 | 51 | 54 | 58 | 50 | | 50 | 50 | 50 | 50 | 55* | 51 | 52 | 52 | 52 | 52 |
| | | Total Energy (ft-lbf) | 749.03 | 749.11 | 751.75 | 750.93 | 749.47 | | 752.08 | 743.75 | 744.71 | 748.7 | | 754.47 | 755.15 | 755.7 | 761.66 | |
| | | AVG drop ht (in) | 17.51 | 18.31 | 18.35 | 18.33 | 17.66 | | 17.96 | 17.5 | 18.42 | 17.47 | | 17.83 | 18.22 | 18.23 | 18.21 | |
| | | Total Energy Measured (ft-lbf) | 2988.19 | 2992.28 | 3005.95 | 2249.32 | 2985.89 | 0 | 3008.42 | 2978.38 | 2257.16 | 3002.63 | 2257.14 | 3006.46 | 3039.08 | 3016.44 | 3032.13 | |
| | | Sample Ht (in) | 7.9 | 7.8 | 7.8 | 7.6 | 7.6 | 7.8 | 8 | 8.2 | 8 | 8 | 7.8 | 7.9 | 8 | 8 | 7.9 | |
| | | Sample Volume (ft^3) | 0.129263 | 0.127627 | 0.127627 | 0.124355 | 0.124355 | 0.127627 | 0.1309 | 0.134172 | 0.1309 | 0.1309 | 0.127627 | 0.129263 | 0.1308997 | 0.1308997 | 0.1292634 | |
| | | Effort Measured [(ft-lbf/ft^3)] | 23117.05 | 23445.47 | 23552.58 | 18087.94 | 24011.07 | 0 | 22982.64 | 22198.19 | 17243.43 | 22938.4 | 17685.41 | 23258.39 | 23216.861 | 23043.904 | 23456.979 | |
| | | Molded water content (%) | 5 | 6 | 7 | 8 | 5 | 6 | 7 | 8 | 5 | 6 | 7 | 8 | 6.9 | 6.9 | 6.9 | |
| | | Sample dry density (pcf) | 132.61 | 136.91 | 138.93 | 138.31 | 131.93 | 131.99 | 136.71 | 135.78 | 130.82 | 131.58 | 138.21 | 135.21 | 137.38 | 137.38 | 137.81 | |
| | Max dry density (pcf) | 138.7 | | | | 136.4 | | | | 139 | | | | Not Applicable | | | | |
| | Optimum Water Content (%) | 7 | | | | 6.8 | | | | 6.9 | | | | Not Applicable | | | | |
| Dielectric at Molding | Reading 1 | 13 | 17.9 | 10.2 | 21 | 16 | 17.5 | 12.6 | 14.1 | 15.6 | 15.1 | 15.8 | 6.5 | 16.4 | 17.5 | 18.3 | | |
| | Reading 2 | 13.2 | 12.7 | 19.7 | 20 | 19 | 18.3 | 12.7 | 12.9 | 20.4 | 17.3 | 15.7 | 9.9 | 16.2 | 19 | 16.8 | | |
| | Reading 3 | 13.8 | 11.1 | 19.3 | 20.4 | 18.5 | 17.9 | 16.1 | 12.9 | 19.7 | 15.2 | 17.1 | 9.6 | 19.2 | 19 | 18.9 | | |
| | Reading 4 | 12.3 | 16.9 | 19 | 21.4 | 18.2 | 16.8 | 15 | 13 | 18.7 | 15.8 | 15.7 | 12.1 | 16.7 | 16.5 | 19.9 | | |
| | Reading 5 | 12.5 | 14.2 | 20.2 | 20.1 | 17.5 | 17.2 | 14.6 | 12.2 | 19.2 | 14.9 | 13.3 | 9.5 | 17.7 | 17.5 | 18 | | |
| | AVG Dielectric at Molding | 12.96 | 14.56 | 19.48 | 20.58 | 17.86 | 17.54 | 14.2 | 13.02 | 18.72 | 44.1 | 15.52 | 9.52 | 17.24 | 17.9 | 18.38 | | |
| Seismic E at Molding | Reading 1 | 91 | 30.9 | 30.4 | 6.1 | 4.2 | 21.5 | 15.1 | 4.8 | 45.1 | 26.2 | 9 | 6.6 | 6.7 | 22.6 | 11.9 | | |
| | Reading 2 | 96 | 31.7 | 24.4 | 7.2 | 8.2 | 19.6 | 16.8 | 3.9 | 32.1 | 24 | 10.3 | 7.8 | 12 | 16.9 | 13.4 | | |
| | Reading 3 | 88.3 | 32.5 | 25.8 | 7.1 | 6.7 | 20.3 | 16.2 | 4.2 | 31.3 | 23.4 | 9.9 | 7.4 | 11 | 16.3 | 10.9 | | |
| | AVG Seismic E at Molding | 91.76667 | 31.7 | 26.86667 | 6.8 | 6.366667 | 20.46667 | 16.03333 | 4.3 | 36.16667 | 24.53333 | 9.733333 | 7.266667 | 9.9 | 18.6 | 12.066667 | | |
| Data after Tex-117-E part II Conditioning | Seismic E Values Dielectric Values | Water content (%) after conditioning | 4.37 | 5.71 | 6.66 | 7.63 | 4.72 | 5.84 | 6.6 | 7.53 | 5.49 | 5.76 | 6.52 | 7.86 | 6.66 | 6.67 | 6.6 | |
| | | Reading 1 | 12.3 | 14.2 | 17.7 | 20 | 12.7 | 14.7 | 16 | 17 | 13.7 | 13.3 | 15.3 | 15.1 | 16 | 17.1 | 18.2 | |
| | | Reading 2 | 11.5 | 16 | 16.7 | 17.5 | 6.3 | 15.5 | 17.3 | 17.2 | 12.5 | 13.8 | 17.3 | 18 | 16.8 | 16.9 | 14.4 | |
| | | Reading 3 | 11.1 | 11.4 | 18.3 | 15.9 | 9.2 | 15.9 | 15 | 21 | 11.8 | 15.5 | 16.8 | 17.5 | 17.2 | 17.9 | 17.2 | |
| | | Reading 4 | 11.7 | 9.2 | 16.7 | 16.3 | 9.7 | 14.7 | 14.9 | 17.5 | 13.5 | 13.8 | 16.2 | 18 | 14 | 15.4 | 18 | |
| | | Reading 5 | 12 | 10.9 | 16.9 | 16.6 | 9.7 | 11.3 | 12 | 17.5 | 12.7 | 14.4 | 16.7 | 17.5 | 17 | 16.8 | 16.9 | |
| | | AVG Dielectric after conditioning | 11.72 | 12.34 | 17.26 | 17.26 | 9.52 | 14.42 | 15.04 | 18.04 | 12.84 | 14.16 | 16.46 | 17.22 | 16.2 | 16.82 | 16.94 | |
| | Seismic E Values | Reading 1 | 49 | 42.8 | 61.2 | 14.3 | 6 | 40 | 41.9 | 15.5 | 34.6 | 52.5 | 35.9 | 14.9 | 36.7 | 36.7 | 22.4 | |
| | | Reading 2 | 47 | 47.5 | 59 | 16 | 9.4 | 40 | 41.9 | 19.1 | 34.6 | 49.5 | 26.4 | 13.3 | 31.6 | 39.4 | 31.3 | |
| | | Reading 3 | 45.8 | 49.2 | 55.3 | 18.1 | 10.7 | 36.6 | 34.8 | 16.7 | 41.5 | 48.5 | 31 | 13.8 | 30 | 40.3 | 29.7 | |
| AVG Seismic E after conditioning | | 47.26667 | 46.5 | 58.5 | 16.13333 | 8.7 | 38.86667 | 39.53333 | 17.1 | 36.9 | 50.16667 | 31.1 | 14 | 32.766667 | 38.8 | 27.8 | | |
| | Unconfined Compressive Strength (psi) | 60.0 | 56.7 | 39.4 | 31.0 | 24.8 | 41.3 | 43.5 | 26.0 | 55.4 | 57.9 | 47.3 | 28.9 | 50.8 | 46.5 | 56.0 | | |
| | Water content (%) after compression test | 4.37 | 5.71 | 6.66 | 7.63 | 4.72 | 5.84 | 6.6 | 7.53 | 5.49 | 5.76 | 6.52 | 7.86 | 6.66 | 6.67 | 6.6 | | |
| | *Drop count estimated due to SCA software lockup | | | | | | | | | | | | | | | | | |

Table B.3. Results from Samples Targeting 16.7 ft-lbf per Blow.

| | | Sample ID | 113-E Moisture-Density Samples | | | | | | | | | | | | Test samples at 113-E Optimum | | | | | |
|--|--------------------------------------|---------------------------------|--------------------------------|----------|----------|---------------------|----------|----------|----------|-------------------------------------|----------|----------|----------------|----------------|-------------------------------|-----------|-----------|-----------|-----------|---------|
| | | | Group 7 | | | | Group 8 | | | | Group 9 | | | | 1 | 2 | 3 | | | |
| | | | 1 | 2 | 3 | 4 | 1 | 2 | 3 | 4 | 1 | 2 | 3 | 4 | 1 | 2 | 3 | | | |
| Data after Test-113-E part II Conditioning | Molding Data | Hammer Weight | 12.20675 | 12.20675 | 12.20675 | 12.20675 | 12.20675 | 12.20675 | 12.20675 | 12.20675 | 12.20675 | 12.20675 | 12.20675 | 12.20675 | 12.20675 | 12.20675 | 12.20675 | 12.20675 | | |
| | | AVG drop ht (in) | 18.73 | 18.72 | 18.69 | 18.73 | 18.7 | 18.72 | 18.71 | 18.73 | 18.75 | 18.72 | 18.68 | 18.75 | 18.77 | 18.76 | 18.76 | 18.76 | | |
| | | Lift 1 | # drops | 44 | 45 | 45 | 45 | 45 | 45 | 45 | 46 | 46 | 45 | 45 | 46 | 45 | 45 | 45 | 45 | |
| | | Total Energy (ft-lbf) | 751.54 | 762 | 760.84 | 754.61 | 753.67 | 761.05 | 757.27 | 765.63 | 765.25 | 753.36 | 765.71 | 766.23 | 765.37 | 762.78 | 760.97 | 760.97 | 760.97 | |
| | | AVG drop ht (in) | 18.73 | 18.7 | 18.53 | 18.73 | 18.67 | 18.5 | 18.74 | 18.69 | 18.71 | 18.72 | 18.52 | 18.74 | 18.05 | 18.51 | 18.74 | 18.74 | 18.74 | |
| | | Lift 2 | # drops | 45 | 45 | 44 | 45 | 45 | 45 | 45 | 45 | 45 | 45 | 45 | 45 | 37 | 45 | 45 | 45 | |
| | | Total Energy (ft-lbf) | 767.12 | 761.93 | 751.13 | 755.39 | 756.86 | 752.79 | 766.18 | 759.5 | 755.51 | 757.46 | 762.09 | 758 | 763.69 | 754.59 | 761.99 | 761.99 | 761.99 | |
| | | AVG drop ht (in) | 18.05 | 18.34 | 18.72 | 18.72 | 18.36 | 18.7 | 18.73 | 18.68 | 18.73 | 18.71 | 18.69 | 18.75 | 18.75 | 18.32 | 18.73 | 18.73 | 18.73 | |
| | | Lift 3 | # drops | 45 | 46 | 45 | 45 | 46 | 46 | 45 | 45 | 45 | 46 | 46 | 46 | 46 | 45 | 46 | 45 | 46 |
| | | Total Energy (ft-lbf) | 751.72 | 770.15 | 758.1 | 752.97 | 764.08 | 764.16 | 752.81 | 755.23 | 751.36 | 763.37 | 751.52 | 755.54 | 755.17 | 750.2 | 763.7 | 763.7 | 763.7 | |
| | | AVG drop ht (in) | 18.74 | 18.69 | 18.71 | 18.72 | 18.06 | 18.68 | 18.66 | 18.49 | 18.72 | 18.75 | 18.69 | 18.74 | 18.75 | 18.69 | 18.75 | 18.69 | 18.75 | 18.75 |
| | | Lift 4 | # drops | 45 | 45 | 45 | 46 | 44 | 46 | 45 | 45 | 46 | 46 | 46 | 45 | 46 | 45 | 46 | 45 | 45 |
| | | Total Energy (ft-lbf) | 760.94 | 759.22 | 756.57 | 768.77 | 753.32 | 765.49 | 750.38 | 765.6 | 753.84 | 763.37 | 764.85 | 756.46 | 760.36 | 762.07 | 757.43 | 757.43 | 757.43 | 757.43 |
| | | Total Energy Measured (ft-lbf) | 3031.32 | 3053.3 | 3026.64 | 3026.74 | 3027.93 | 3043.49 | 3026.64 | 3045.96 | 3025.96 | 3037.56 | 3044.17 | 3036.23 | 3050.59 | 3029.64 | 3044.09 | 3044.09 | 3044.09 | 3044.09 |
| | Sample Ht (in) | 8.25 | 8.1 | 8.05 | 8.1 | 8.1 | 8.1 | 8.05 | 7.95 | 8.25 | 8.2 | 8.05 | 8 | 8.1 | 8 | 7.9 | 7.9 | 7.9 | 7.9 | |
| | Sample Volume (ft^3) | 0.13499 | 0.132536 | 0.131718 | 0.132536 | 0.132536 | 0.132536 | 0.131718 | 0.130082 | 0.13499 | 0.134172 | 0.131718 | 0.1309 | 0.1325359 | 0.1308997 | 0.1292684 | 0.1292684 | 0.1292684 | 0.1292684 | |
| | Effort Measured [(ft-lbf/ft^3)] | 22455.83 | 23037.52 | 22978.21 | 22837.13 | 22846.1 | 22963.51 | 22978.21 | 23415.77 | 22416.13 | 22639.27 | 23111.3 | 23195.09 | 23017.077 | 23144.745 | 23549.503 | 23549.503 | 23549.503 | 23549.503 | |
| | Molded water content (%) | 5 | 6 | 7 | 8 | 5 | 6 | 7 | 8 | 5 | 6 | 7 | 8 | 6.8 | 6.8 | 6.8 | 6.8 | 6.8 | 6.8 | |
| | Sample dry density (pcf) | 133.21 | 135.43 | 137.08 | 134.62 | 134.49 | 135.69 | 136.92 | 136.01 | 132.08 | 135.28 | 136.52 | 136.06 | 136.09 | 136.37 | 137.63 | 137.63 | 137.63 | 137.63 | |
| | Max dry density (pcf) | 135.5 | | | | 136.5 | | | | 136.3 | | | | Not Applicable | | | | | | |
| Optimum Water Content (%) | 6.6 | | | | 6.8 | | | | 6.9 | | | | Not Applicable | | | | | | | |
| Dielectric at Molding | Reading 1 | | | | | | | | 18.4 | | | | | 17.4 | 16.8 | 17.9 | 18.8 | | | |
| | Reading 2 | | | | | | | | 19.6 | | | | | 20.9 | 14.6 | 18 | 18.5 | | | |
| | Reading 3 | No percometer available 9/16/10 | | | | | | | 20.7 | No percometer available | | | | 22.9 | 18.1 | 16.7 | 17.7 | | | |
| | Reading 4 | | | | | | | | 21.2 | | | | | 21.9 | 17.3 | 18.5 | 19.8 | | | |
| | Reading 5 | | | | | | | | 22.7 | | | | | 16 | 16.3 | 18.7 | 18.7 | | | |
| | AVG Dielectric at Molding | | | | | | | | 20.52 | | | | | 20.775 | 16.56 | 17.48 | 18.7 | | | |
| Seismic E at Molding | Reading 1 | 36.1 | 36.4 | 15.2 | 6.8 | 14.8 | 47.6 | 15.2 | 6.8 | 46.8 | 15 | 12 | 6.8 | 18.7 | 9.1 | 22.2 | 22.2 | 22.2 | | |
| | Reading 2 | 28.8 | 36.4 | 13.5 | 5.7 | 10.3 | 44.7 | 9.2 | 7.9 | 43.9 | 11.9 | 6.8 | 15.2 | 18.7 | 10.4 | 13.3 | 13.3 | 13.3 | | |
| | Reading 3 | 28 | 38.2 | 14.1 | 4.7 | 11.7 | 34.7 | 9.2 | 8.3 | 46.8 | 11.9 | 6.8 | 11 | 15.2 | 16.1 | 11.8 | 11.8 | 11.8 | | |
| | AVG Seismic E at Molding | 30.96667 | 37 | 14.26667 | 5.733333 | 12.26667 | 42.33333 | 11.2 | 7.666667 | 45.83333 | 12.93333 | 8.533333 | 11 | 17.53333 | 11.866667 | 15.766667 | 15.766667 | 15.766667 | | |
| Seismic E Values Dielectric Values | Water content (%) after conditioning | 5 | 6.01 | 6.88 | 7.78 | 5 | 5.93 | 6.98 | 7.35 | 5.01 | 6.04 | 6.85 | 7.27 | 6.48 | 6.38 | 6.45 | 6.45 | 6.45 | | |
| | Reading 1 | 12.8 | 14.3 | 18.3 | 20.2 | 12.8 | 14.2 | 15.9 | 19.9 | 13 | 15.6 | 17.8 | 15.8 | 16.9 | 17.7 | 18 | 18 | 18 | | |
| | Reading 2 | 13.3 | 13.6 | 16.8 | 17.9 | 12.1 | 12.5 | 13 | 20.1 | 13 | 13.5 | 14.2 | 18.8 | 16.6 | 16.8 | 18.1 | 18.1 | 18.1 | | |
| | Reading 3 | 11.9 | 14.4 | 17 | 19.1 | 12 | 12.1 | 16.9 | 19.1 | 13.3 | 12.9 | 12.9 | 17.4 | 14.9 | 16 | 17.6 | 17.6 | 17.6 | | |
| | Reading 4 | 10.9 | 13.5 | 15.1 | 18.4 | 11.6 | 11.3 | 13.3 | 17.5 | 11.5 | 12.3 | 13.5 | 20.1 | 13.5 | 15.9 | 16.7 | 16.7 | 16.7 | | |
| | Reading 5 | 12.3 | 14.6 | 16.7 | 18.3 | 11.6 | 13.5 | 17.3 | 20 | 12.9 | 14.6 | 16.9 | 19 | 16.5 | 16 | 17.1 | 17.1 | 17.1 | | |
| | AVG Dielectric after conditioning | 12.24 | 14.08 | 16.78 | 18.78 | 12.02 | 12.72 | 15.28 | 19.32 | 12.74 | 13.78 | 15.06 | 18.22 | 15.68 | 16.48 | 17.5 | 17.5 | 17.5 | | |
| | Reading 1 | skip due to cryness | 46.9 | 53.3 | 17.3 | skip due to cryness | 48.9 | 36.4 | 18.8 | cannot report in weighing - no test | 26 | 49.6 | 22.7 | 33.5 | 26.4 | 36.4 | 36.4 | 36.4 | 36.4 | |
| | Reading 2 | | 46.9 | 34.5 | 15.5 | | 48.9 | 36.4 | 24.8 | | 26 | 49.6 | 31.7 | 34.5 | 26.4 | 30.4 | 30.4 | 30.4 | 30.4 | |
| | Reading 3 | | 47.9 | 30.7 | 13.5 | | 49.9 | 43 | 25.5 | | 26 | 55.1 | 30.1 | 34.5 | 25 | 55.8 | 55.8 | 55.8 | 55.8 | |
| AVG Seismic E after conditioning | | 47.23333 | 39.5 | 15.43333 | | 49.23333 | 38.6 | 23.03333 | | 26 | 51.43333 | 28.16667 | 34.166667 | 25.933333 | 47.533333 | 47.533333 | 47.533333 | | | |
| Unconfined Compressive Strength (psi) | 32.3 | 77.5 | 48.7 | 37.7 | 65.9 | 81.6 | 49.6 | 26.8 | 38.5 | 41.5 | 46.4 | 26.4 | 40.9 | 58.9 | 53.7 | 53.7 | 53.7 | 53.7 | | |
| Water content (%) after compression test | 5 | 6.01 | 6.88 | 7.78 | 5 | 5.93 | 6.98 | 7.35 | 5.01 | 6.04 | 6.85 | 7.27 | 6.48 | 6.38 | 6.45 | 6.45 | 6.45 | 6.45 | | |

APPENDIX C: INDIVIDUAL LAB RESULTS FROM ILS

Table C.1. ILS Results from Laboratory 1.

| Triaxial Test Data Sheet | | | | | | | | | |
|---|---------|---------|-----------|---------|---------|---------|---------|---------|---------|
| Specimen Data | | | | | | | | | |
| Specimen Number: | GB-1 | GB-2 | GB-3 | SW-1 | SW-2 | SW-3 | OK-1 | OK-2 | OK-3 |
| Cell No.: | | | | | | | | | |
| Wet Mass Spec. & Mold, (lb): | 38.649 | 38.505 | No Sample | 39.638 | 39.637 | 39.638 | 38.390 | 38.960 | 38.161 |
| Wet Mass Specimen, (lb): | 19.361 | 19.218 | | 20.351 | 20.350 | 20.351 | 19.102 | 19.672 | 18.874 |
| Initial Height of Specimen, in.: | 8.056 | 8.029 | | 7.890 | 7.871 | 7.899 | 7.976 | 8.211 | 7.865 |
| New Height of Specimen, in.: | 8.000 | 8.000 | | 8.000 | 8.000 | 8.000 | 8.000 | 8.000 | 8.000 |
| Average Diameter, in.: | 6.00 | 6.00 | | 6.00 | 6.00 | 6.00 | 6.00 | 6.00 | 6.00 |
| Circumference, in. (manual): | 19.100 | 19.100 | | 19.000 | 19.000 | 19.000 | 18.900 | 18.900 | 18.900 |
| Circumference, in. (auto): | 19.100 | 19.100 | | 19.000 | 19.000 | 19.000 | 18.900 | 18.900 | 18.900 |
| Area, in. ² : | 28.65 | 28.65 | | 28.50 | 28.50 | 28.50 | 28.35 | 28.35 | 28.35 |
| Avg. Cross Sectional Area, in. ² : | 29.84 | 29.56 | | 29.35 | 29.44 | 29.62 | 28.99 | 29.01 | 28.81 |
| Dry-Back Data | | | | | | | | | |
| Wet Mass of Pan & Specimen, (lb): | 22.271 | 22.401 | | 23.482 | 23.519 | 23.453 | 22.161 | 22.787 | 23.007 |
| Dry Mass of Pan & Specimen, (lb): | 21.031 | 21.138 | | 22.485 | 22.494 | 22.436 | 20.875 | 21.466 | 21.644 |
| Mass of Pan, (lb): | 3.210 | 3.239 | | 3.210 | 3.239 | 3.231 | 3.210 | 3.239 | 3.231 |
| Dry Mass of Material, (lb): | 17.821 | 17.899 | | 19.275 | 19.255 | 19.205 | 17.665 | 18.227 | 18.413 |
| Mass of Water, (lb): | 1.240 | 1.263 | | 0.997 | 1.025 | 1.017 | 1.286 | 1.321 | 1.363 |
| Moisture Content, (%): | 7.0 | 7.1 | | 5.2 | 5.3 | 5.3 | 7.3 | 7.2 | 7.4 |
| Wet Density, (pcf): | 146.5 | 145.9 | | 157.3 | 157.6 | 157.1 | 146.0 | 146.1 | 146.3 |
| Dry Density, (pcf): | 137.0 | 136.3 | | 149.5 | 149.7 | 149.2 | 136.1 | 136.2 | 136.2 |
| SCA Data | | | | | | | | | |
| Total Energy (lb-ft) Lift 1: | 759.620 | 759.710 | | 758.000 | 755.000 | 760.760 | 757.170 | 754.610 | 750.470 |
| Total Energy (lb-ft) Lift 2: | 759.640 | 752.220 | | 759.560 | 751.690 | 763.130 | 753.000 | 753.450 | 750.600 |
| Total Energy (lb-ft) Lift 3: | 751.140 | 758.860 | | 757.430 | 762.460 | 761.400 | 761.670 | 752.910 | 759.470 |
| Total Energy (lb-ft) Lift 4: | 752.760 | 761.650 | | 753.220 | 750.010 | 760.340 | 755.120 | 759.170 | 751.260 |
| Energy/Lift (lb-ft) Lift 1: | 13.330 | 12.880 | | 12.850 | 13.260 | 13.350 | 13.050 | 13.240 | 12.940 |
| Energy/Lift (lb-ft) Lift 2: | 13.330 | 12.970 | | 13.330 | 13.670 | 13.390 | 12.980 | 12.150 | 12.720 |
| Energy/Lift (lb-ft) Lift 3: | 13.180 | 13.080 | | 13.530 | 13.620 | 13.840 | 13.360 | 12.980 | 12.870 |
| Energy/Lift (lb-ft) Lift 4: | 13.210 | 13.360 | | 13.450 | 13.640 | 13.580 | 13.360 | 12.650 | 12.520 |
| Avg. Drop Ht. (lb-ft) Lift 1: | 18.300 | 15.990 | | 18.470 | 18.480 | 18.400 | 17.180 | 17.810 | 16.520 |
| Avg. Drop Ht. (lb-ft) Lift 2: | 17.550 | 18.290 | | 18.490 | 18.490 | 18.400 | 18.010 | 17.120 | 17.370 |
| Avg. Drop Ht. (lb-ft) Lift 3: | 17.960 | 18.000 | | 18.490 | 18.500 | 17.420 | 17.960 | 18.470 | 18.040 |
| Avg. Drop Ht. (lb-ft) Lift 4: | 17.260 | 18.490 | | 18.490 | 18.490 | 17.970 | 17.050 | 17.660 | 17.050 |
| No. of Blows (lb-ft) Lift 1: | 57.000 | 59.000 | | 59.000 | 57.000 | 57.000 | 58.000 | 57.000 | 58.000 |
| No. of Blows (lb-ft) Lift 2: | 57.000 | 58.000 | | 57.000 | 55.000 | 57.000 | 58.000 | 62.000 | 59.000 |
| No. of Blows (lb-ft) Lift 3: | 57.000 | 58.000 | | 56.000 | 56.000 | 55.000 | 57.000 | 58.000 | 59.000 |
| No. of Blows (lb-ft) Lift 4: | 57.000 | 57.000 | | 56.000 | 55.000 | 56.000 | 59.000 | 60.000 | 60.000 |

Table C.2. ILS Results from Laboratory 2.

| Triaxial Test Data Sheet | | | | | | | | | |
|--|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| Specimen Data | | | | | | | | | |
| Specimen Number: | GB-1 | GB-2 | GB-3 | OK-1 | OK-2 | OK-3 | SW-1 | SW-2 | SW-3 |
| Cell No.: | 57 | 60 | 72 | 94 | 103 | 105 | 34 | 36 | 56 |
| Wet Mass Spec. & Mold, (lb): | 37.840 | 37.874 | 37.880 | 37.553 | 37.548 | 37.330 | 38.646 | 39.213 | 38.745 |
| Wet Mass Specimen, (lb): | 19.454 | 19.488 | 19.494 | 19.167 | 19.162 | 18.944 | 20.260 | 20.827 | 20.359 |
| Initial Height of Specimen, in.: | 8.105 | 8.127 | 8.168 | 7.940 | 7.933 | 7.925 | 7.793 | 7.999 | 7.847 |
| New Height of Specimen, in.: | 8.105 | 8.127 | 8.198 | 7.940 | 7.933 | 7.925 | 7.793 | 7.999 | 7.847 |
| Average Diameter, in.: | 6.00 | 6.00 | 6.00 | 6.00 | 6.00 | 6.00 | 6.00 | 6.00 | 6.00 |
| Circumference, in. (manual): | | | | | | | | | |
| Circumference, in. (auto): | 18.850 | 18.850 | 18.850 | 18.850 | 18.850 | 18.850 | 18.850 | 18.850 | 18.850 |
| Area, in. ² : | 28.27 | 28.27 | 28.27 | 28.27 | 28.27 | 28.27 | 28.27 | 28.27 | 28.27 |
| Avg. Cross Sectional Area, in ² : | 28.99 | 28.90 | 29.00 | 28.72 | 28.81 | 28.84 | 28.87 | 28.96 | 29.09 |
| Dry-Back Data | | | | | | | | | |
| Wet Mass of Pan & Specimen, (lb) | 24.424 | 24.031 | 22.891 | 25.662 | 25.560 | 25.623 | 26.373 | 26.815 | 25.404 |
| Dry Mass of Pan & Specimen, (lb): | 23.297 | 22.936 | 21.749 | 24.328 | 24.231 | 24.287 | 25.415 | 25.851 | 24.454 |
| Mass of Pan, (lb): | 5.285 | 5.143 | 3.762 | 6.188 | 6.054 | 6.106 | 6.107 | 6.066 | 5.087 |
| Dry Mass of Material, (lb): | 18.012 | 17.794 | 17.987 | 18.140 | 18.177 | 18.182 | 19.308 | 19.785 | 19.368 |
| Mass of Water, (lb): | 1.127 | 1.095 | 1.143 | 1.334 | 1.330 | 1.336 | 0.969 | 0.964 | 0.950 |
| Moisture Content, (%): | 6.3 | 6.2 | 6.4 | 7.4 | 7.3 | 7.3 | 5.0 | 4.9 | 4.9 |
| Wet Density, (pcf): | 145.5 | 145.3 | 144.6 | 146.3 | 146.4 | 144.9 | 157.6 | 157.8 | 157.2 |
| Dry Density, (pcf): | 136.9 | 136.9 | 136.0 | 136.3 | 136.4 | 135.0 | 150.1 | 150.5 | 149.9 |
| SCA Data | | | | | | | | | |
| Total Energy (lb-ft) Lift 1: | 753.520 | 758.040 | 753.130 | 759.620 | 761.420 | 761.750 | 760.070 | 761.310 | 750.620 |
| Total Energy (lb-ft) Lift 2: | 750.540 | 758.930 | 761.340 | 752.770 | 757.180 | 751.160 | 757.690 | 756.300 | 758.760 |
| Total Energy (lb-ft) Lift 3: | 762.010 | 762.700 | 750.430 | 759.540 | 756.960 | 759.760 | 754.020 | 760.590 | 752.050 |
| Total Energy (lb-ft) Lift 4: | 751.360 | 754.600 | 750.460 | 762.780 | 762.440 | 758.000 | 753.580 | 753.860 | 755.060 |
| Energy/Lift (lb-ft) Lift 1: | 13.220 | 13.300 | 13.210 | 13.100 | 13.130 | 13.130 | 13.570 | 13.130 | 13.170 |
| Energy/Lift (lb-ft) Lift 2: | 13.170 | 13.080 | 13.130 | 12.950 | 13.050 | 12.950 | 13.060 | 13.040 | 13.080 |
| Energy/Lift (lb-ft) Lift 3: | 13.140 | 13.150 | 13.170 | 13.100 | 13.050 | 13.100 | 13.000 | 13.110 | 13.190 |
| Energy/Lift (lb-ft) Lift 4: | 13.180 | 13.240 | 13.170 | 13.150 | 13.150 | 13.070 | 13.220 | 13.230 | 13.250 |
| Avg. Drop Ht. (lb-ft) Lift 1: | 18.400 | 18.380 | 18.390 | 18.380 | 18.360 | 18.330 | 18.380 | 18.410 | 18.390 |
| Avg. Drop Ht. (lb-ft) Lift 2: | 18.400 | 18.410 | 18.380 | 18.390 | 18.390 | 18.310 | 18.360 | 18.380 | 18.360 |
| Avg. Drop Ht. (lb-ft) Lift 3: | 18.390 | 18.370 | 18.390 | 18.370 | 18.380 | 18.390 | 18.340 | 18.360 | 18.360 |
| Avg. Drop Ht. (lb-ft) Lift 4: | 18.390 | 18.400 | 18.400 | 18.400 | 18.390 | 18.380 | 18.390 | 18.380 | 18.390 |
| No. of Blows (lb-ft) Lift 1: | 57.000 | 57.000 | 57.000 | 58.000 | 58.000 | 58.000 | 56.000 | 58.000 | 57.000 |
| No. of Blows (lb-ft) Lift 2: | 57.000 | 58.000 | 58.000 | 58.000 | 58.000 | 58.000 | 58.000 | 58.000 | 58.000 |
| No. of Blows (lb-ft) Lift 3: | 58.000 | 58.000 | 57.000 | 58.000 | 58.000 | 58.000 | 58.000 | 58.000 | 57.000 |
| No. of Blows (lb-ft) Lift 4: | 57.000 | 57.000 | 57.000 | 58.000 | 58.000 | 58.000 | 57.000 | 57.000 | 57.000 |

Table C.3. ILS Results from Laboratory 3.

| Triaxial Test Data Sheet | | | | | | | | | |
|---|---------|---------|---------|---------|---------|---------|---------|---------|--------|
| Specimen Data | | | | | | | | | |
| Specimen Number: | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| Cell No.: | G-1 | G-2 | G-3 | O-5 | O-6 | O-7 | S-A | S-B | |
| Wet Mass Spec. & Mold, (lb): | 38.866 | 38.756 | 38.776 | 38.514 | 38.664 | 38.667 | 39.776 | 39.738 | |
| Wet Mass Specimen, (lb): | 19.549 | 19.439 | 19.459 | 19.197 | 19.347 | 19.350 | 20.459 | 20.421 | |
| Initial Height of Specimen, in.: | 8.235 | 8.202 | 8.291 | 8.096 | 8.120 | 8.094 | 7.969 | 7.973 | |
| New Height of Specimen, in.: | 8.235 | 8.202 | 8.291 | 8.096 | 8.120 | 8.094 | 7.969 | 7.973 | |
| Average Diameter, in.: | 6.00 | 6.00 | 6.00 | 6.00 | 6.00 | 6.00 | 6.00 | 6.00 | |
| Circumference, in. (manual): | | | | | | | | | |
| Circumference, in. (auto): | 18.850 | 18.850 | 18.850 | 18.850 | 18.850 | 18.850 | 18.850 | 18.850 | 18.850 |
| Area, in. ² : | 28.27 | 28.27 | 28.27 | 28.27 | 28.27 | 28.27 | 28.27 | 28.27 | |
| Avg. Cross Sectional Area, in. ² : | 28.96 | 28.99 | 28.78 | 28.78 | 28.69 | 29.05 | 28.84 | 28.72 | |
| Dry-Back Data | | | | | | | | | |
| Wet Mass of Pan & Specimen, (lb): | 25.650 | 25.222 | 25.543 | 24.474 | 25.445 | 24.999 | 25.349 | 26.396 | |
| Dry Mass of Pan & Specimen, (lb): | 24.421 | 24.011 | 24.321 | 23.278 | 24.247 | 23.807 | 24.371 | 25.427 | |
| Mass of Pan, (lb): | 6.141 | 5.833 | 6.116 | 5.409 | 6.246 | 5.793 | 4.939 | 6.031 | |
| Dry Mass of Material, (lb): | 18.280 | 18.178 | 18.205 | 17.869 | 18.001 | 18.014 | 19.432 | 19.396 | |
| Mass of Water, (lb): | 1.229 | 1.211 | 1.222 | 1.196 | 1.198 | 1.192 | 0.978 | 0.969 | |
| Moisture Content, (%): | 6.7 | 6.7 | 6.7 | 6.7 | 6.7 | 6.6 | 5.0 | 5.0 | |
| Wet Density, (pcf): | 144.7 | 144.5 | 143.1 | 144.6 | 145.3 | 145.8 | 156.5 | 156.2 | |
| Dry Density, (pcf): | 135.6 | 135.5 | 134.1 | 135.5 | 136.2 | 136.7 | 149.0 | 148.7 | |
| SCA Data | | | | | | | | | |
| Total Energy (lb-ft) Lift 1: | 751.500 | 763.990 | 761.530 | 759.200 | 757.720 | 760.230 | 762.180 | 759.710 | |
| Total Energy (lb-ft) Lift 2: | 760.510 | 750.180 | 761.340 | 758.000 | 762.650 | 758.990 | 764.060 | 757.220 | |
| Total Energy (lb-ft) Lift 3: | 758.790 | 761.270 | 760.340 | 760.150 | 761.030 | 759.100 | 754.840 | 753.520 | |
| Total Energy (lb-ft) Lift 4: | 760.480 | 756.170 | 753.840 | 751.890 | 757.060 | 752.990 | 752.770 | 752.060 | |
| Energy/Lift (lb-ft) Lift 1: | 14.180 | 14.150 | 14.100 | 14.060 | 14.030 | 14.080 | 13.860 | 14.070 | |
| Energy/Lift (lb-ft) Lift 2: | 18.080 | 14.150 | 14.100 | 14.040 | 14.120 | 14.060 | 13.890 | 14.020 | |
| Energy/Lift (lb-ft) Lift 3: | 18.050 | 14.100 | 14.080 | 14.080 | 14.090 | 14.060 | 13.980 | 13.950 | |
| Energy/Lift (lb-ft) Lift 4: | 18.080 | 14.000 | 13.960 | 13.920 | 14.020 | 13.940 | 13.940 | 13.930 | |
| Avg. Drop Ht. (lb-ft) Lift 1: | 18.530 | 18.530 | 18.510 | 18.520 | 18.540 | 18.530 | 18.490 | 18.530 | |
| Avg. Drop Ht. (lb-ft) Lift 2: | 18.520 | 18.510 | 18.520 | 18.510 | 18.540 | 18.540 | 18.490 | 18.510 | |
| Avg. Drop Ht. (lb-ft) Lift 3: | 18.520 | 18.520 | 18.520 | 18.520 | 18.530 | 18.530 | 18.510 | 18.510 | |
| Avg. Drop Ht. (lb-ft) Lift 4: | 18.510 | 18.500 | 18.500 | 18.520 | 18.510 | 18.500 | 18.510 | 18.510 | |
| No. of Blows (lb-ft) Lift 1: | 53.000 | 54.000 | 54.000 | 54.000 | 54.000 | 54.000 | 55.000 | 54.000 | |
| No. of Blows (lb-ft) Lift 2: | 54.000 | 53.000 | 54.000 | 54.000 | 54.000 | 54.000 | 55.000 | 54.000 | |
| No. of Blows (lb-ft) Lift 3: | 54.000 | 54.000 | 54.000 | 54.000 | 54.000 | 54.000 | 54.000 | 54.000 | |
| No. of Blows (lb-ft) Lift 4: | 54.000 | 54.000 | 54.000 | 54.000 | 54.000 | 54.000 | 54.000 | 54.000 | |

Table C.4. ILS Results from Laboratory 4.

| Triaxial Test Data Sheet | | | | | | | | | |
|--|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| Specimen Data | | | | | | | | | |
| Specimen Number: | GB-1 | GB-2 | GB-3 | SW-1 | SW-2 | SW-3 | OK-1 | OK-2 | OK-3 |
| Cell No.: | 4 | 5 | 6 | 7 | 8 | 9 | 1 | 2 | 3 |
| Wet Mass Spec. & Mold, (lb): | 29.382 | 29.347 | 29.273 | 30.250 | 30.274 | 30.262 | 28.995 | 29.122 | 29.113 |
| Wet Mass Specimen, (lb): | 19.421 | 19.386 | 19.312 | 20.289 | 20.313 | 20.301 | 19.034 | 19.161 | 19.152 |
| Initial Height of Specimen, in.: | 8.028 | 7.985 | 7.989 | 7.733 | 7.765 | 7.818 | 7.737 | 7.746 | 7.820 |
| New Height of Specimen, in.: | 8.028 | 7.985 | 7.989 | 7.733 | 7.765 | 7.818 | 7.737 | 7.746 | 7.820 |
| Average Diameter, in.: | 6.00 | 6.00 | 6.00 | 6.00 | 6.00 | 6.00 | 6.00 | 6.00 | 6.00 |
| Circumference, in. (manual): | | | | | | | | | |
| Circumference, in. (auto): | 18.850 | 18.850 | 18.850 | 18.850 | 18.850 | 18.850 | 18.850 | 18.850 | 18.850 |
| Area, in. ² : | 28.27 | 28.27 | 28.27 | 28.27 | 28.27 | 28.27 | 28.27 | 28.27 | 28.27 |
| Avg. Cross Sectional Area, in ² : | 28.65 | 28.68 | 28.66 | 28.60 | 28.69 | 28.64 | 28.71 | 28.69 | 28.66 |
| Dry-Back Data | | | | | | | | | |
| Wet Mass of Pan & Specimen, (lb) | 22.955 | 23.161 | 23.158 | 24.056 | 23.852 | 24.124 | 22.532 | 23.016 | 22.806 |
| Dry Mass of Pan & Specimen, (lb): | 21.778 | 21.970 | 21.993 | 23.125 | 22.912 | 23.200 | 21.342 | 21.819 | 21.635 |
| Mass of Pan, (lb): | 3.534 | 3.774 | 3.836 | 3.777 | 3.546 | 3.836 | 3.558 | 3.895 | 3.794 |
| Dry Mass of Material, (lb): | 18.244 | 18.196 | 18.157 | 19.348 | 19.366 | 19.364 | 17.784 | 17.924 | 17.841 |
| Mass of Water, (lb): | 1.177 | 1.191 | 1.165 | 0.931 | 0.940 | 0.924 | 1.190 | 1.197 | 1.171 |
| Moisture Content, (%): | 6.5 | 6.5 | 6.4 | 4.8 | 4.9 | 4.8 | 6.7 | 6.7 | 6.6 |
| Wet Density, (pcf): | 144.0 | 144.5 | 143.9 | 156.2 | 155.7 | 154.6 | 146.4 | 147.2 | 145.8 |
| Dry Density, (pcf): | 135.3 | 135.6 | 135.2 | 149.0 | 148.5 | 147.5 | 137.3 | 138.0 | 136.8 |
| SCA Data | | | | | | | | | |
| Total Energy (lb-ft) Lift 1: | 752.570 | 761.310 | 753.370 | 751.030 | 755.450 | 755.560 | 750.510 | 753.260 | 752.060 |
| Total Energy (lb-ft) Lift 2: | 754.140 | 758.790 | 758.700 | 750.480 | 756.570 | 755.040 | 751.130 | 758.880 | 762.160 |
| Total Energy (lb-ft) Lift 3: | 756.110 | 752.000 | 751.350 | 754.730 | 758.060 | 758.190 | 761.690 | 751.560 | 760.410 |
| Total Energy (lb-ft) Lift 4: | 751.570 | 750.650 | 759.380 | 750.640 | 754.060 | 753.800 | 762.410 | 751.320 | 753.280 |
| Energy/Lift (lb-ft) Lift 1: | 12.760 | 12.480 | 12.560 | 12.520 | 12.380 | 12.190 | 12.940 | 12.770 | 12.750 |
| Energy/Lift (lb-ft) Lift 2: | 12.570 | 12.440 | 12.440 | 12.510 | 12.200 | 11.980 | 12.950 | 12.650 | 12.490 |
| Energy/Lift (lb-ft) Lift 3: | 12.600 | 12.330 | 12.320 | 12.370 | 12.230 | 12.230 | 12.690 | 12.630 | 12.670 |
| Energy/Lift (lb-ft) Lift 4: | 12.530 | 12.310 | 12.050 | 12.110 | 12.160 | 11.970 | 12.500 | 12.320 | 12.350 |
| Avg. Drop Ht. (lb-ft) Lift 1: | 18.010 | 17.120 | 17.990 | 17.990 | 17.510 | 17.980 | 18.000 | 18.000 | 17.870 |
| Avg. Drop Ht. (lb-ft) Lift 2: | 17.980 | 17.170 | 17.330 | 17.490 | 17.080 | 17.320 | 17.510 | 17.280 | 17.620 |
| Avg. Drop Ht. (lb-ft) Lift 3: | 18.000 | 17.310 | 17.200 | 17.980 | 16.700 | 17.980 | 17.990 | 17.290 | 17.120 |
| Avg. Drop Ht. (lb-ft) Lift 4: | 17.510 | 18.000 | 17.250 | 17.390 | 17.610 | 16.790 | 18.000 | 18.000 | 18.000 |
| No. of Blows (lb-ft) Lift 1: | 59.000 | 61.000 | 60.000 | 60.000 | 61.000 | 62.000 | 58.000 | 59.000 | 59.000 |
| No. of Blows (lb-ft) Lift 2: | 60.000 | 61.000 | 61.000 | 60.000 | 62.000 | 63.000 | 58.000 | 60.000 | 61.000 |
| No. of Blows (lb-ft) Lift 3: | 60.000 | 61.000 | 61.000 | 61.000 | 62.000 | 62.000 | 60.000 | 60.000 | 60.000 |
| No. of Blows (lb-ft) Lift 4: | 60.000 | 61.000 | 63.000 | 62.000 | 62.000 | 63.000 | 61.000 | 61.000 | 61.000 |

Table C.5. ILS Results from Laboratory 5.

| Triaxial Test Data Sheet | | | | | | | | | |
|---|---------|---------|------|---------|---------|---------|---------|---------|---------|
| Specimen Data | | | | | | | | | |
| Specimen Number: | GB-1 | GB-2 | GB-3 | SW-1 | SW-2 | SW-3 | OK-1 | OK-2 | OK-3 |
| Cell No.: | 8 | 9 | | 8 | 9 | 28 | 8 | 9 | 28 |
| Wet Mass Spec. & Mold, (lb): | 38.678 | 38.694 | | 39.456 | 39.799 | 39.804 | 38.591 | 38.687 | 38.693 |
| Wet Mass Specimen, (lb): | 19.208 | 19.224 | | 19.986 | 20.329 | 20.334 | 19.121 | 19.217 | 19.223 |
| Initial Height of Specimen, in.: | 8.120 | 8.121 | | 7.827 | 7.991 | 8.052 | 8.192 | 8.035 | 8.050 |
| New Height of Specimen, in.: | 7.991 | 8.052 | | 7.827 | 7.991 | 8.052 | 8.192 | 8.035 | 8.050 |
| Average Diameter, in.: | 6.00 | 6.00 | | 6.00 | 6.00 | 6.00 | 6.00 | 6.00 | 6.00 |
| Circumference, in. (manual): | 18.850 | 18.850 | | 18.900 | 18.850 | 18.900 | 18.900 | 18.850 | 19.000 |
| Circumference, in. (auto): | 18.850 | 18.850 | | 18.900 | 18.850 | 18.900 | 18.900 | 18.850 | 19.000 |
| Area, in. ² : | 28.28 | 28.28 | | 28.35 | 28.28 | 28.35 | 28.35 | 28.28 | 28.50 |
| Avg. Cross Sectional Area, in. ² : | 28.95 | 28.84 | | 29.04 | 28.95 | 28.92 | 30.64 | 29.65 | 29.04 |
| Dry-Back Data | | | | | | | | | |
| Wet Mass of Pan & Specimen, (lb) | 22.932 | 22.953 | | 23.679 | 24.068 | 24.068 | 22.745 | 22.869 | 22.856 |
| Dry Mass of Pan & Specimen, (lb): | 21.782 | 21.791 | | 22.806 | 23.158 | 23.172 | 21.592 | 21.672 | 21.689 |
| Mass of Pan, (lb): | 3.763 | 3.765 | | 3.763 | 3.773 | 3.782 | 3.765 | 3.789 | 3.769 |
| Dry Mass of Material, (lb): | 18.019 | 18.026 | | 19.043 | 19.385 | 19.390 | 17.827 | 17.883 | 17.920 |
| Mass of Water, (lb): | 1.150 | 1.162 | | 0.873 | 0.910 | 0.896 | 1.153 | 1.197 | 1.167 |
| Moisture Content, (%): | 6.4 | 6.4 | | 4.6 | 4.7 | 4.6 | 6.5 | 6.7 | 6.5 |
| Wet Density, (pcf): | 144.2 | 144.3 | | 155.7 | 155.1 | 154.0 | 142.3 | 145.8 | 145.6 |
| Dry Density, (pcf): | 135.6 | 135.6 | | 148.9 | 148.2 | 147.2 | 133.7 | 136.7 | 136.7 |
| SCA Data | | | | | | | | | |
| Total Energy (lb-ft) Lift 1: | 759.190 | 753.740 | | 754.540 | 753.110 | 755.120 | 761.850 | 758.560 | 761.920 |
| Total Energy (lb-ft) Lift 2: | 751.150 | 753.610 | | 750.790 | 750.720 | 756.350 | 760.300 | 751.370 | 752.030 |
| Total Energy (lb-ft) Lift 3: | 763.600 | 754.370 | | | 753.690 | 756.040 | 753.100 | 751.000 | 755.270 |
| Total Energy (lb-ft) Lift 4: | 760.395 | 759.680 | | 761.760 | 752.640 | 757.780 | | 754.520 | 750.150 |
| Energy/Lift (lb-ft) Lift 1: | 13.319 | 13.460 | | 13.010 | 12.980 | 12.590 | 13.850 | 13.080 | 13.140 |
| Energy/Lift (lb-ft) Lift 2: | 13.180 | 13.460 | | 12.940 | 12.940 | 12.200 | 13.340 | 13.420 | 13.190 |
| Energy/Lift (lb-ft) Lift 3: | 13.640 | 13.720 | | | 12.990 | 11.120 | 13.210 | 13.180 | 12.380 |
| Energy/Lift (lb-ft) Lift 4: | 13.840 | 13.570 | | 13.360 | 12.760 | 8.880 | | 13.010 | 12.930 |
| Avg. Drop Ht. (lb-ft) Lift 1: | 17.450 | 18.410 | | 17.630 | 17.650 | 17.600 | 18.420 | 17.880 | 18.340 |
| Avg. Drop Ht. (lb-ft) Lift 2: | 17.690 | 18.390 | | 17.410 | 17.380 | 16.770 | 18.290 | 18.360 | 18.430 |
| Avg. Drop Ht. (lb-ft) Lift 3: | 18.210 | 18.430 | | | 18.200 | 15.190 | 18.070 | 18.380 | 18.190 |
| Avg. Drop Ht. (lb-ft) Lift 4: | 18.340 | 18.420 | | 17.800 | 16.970 | 13.290 | | 18.410 | 18.400 |
| No. of Blows (lb-ft) Lift 1: | 57.000 | 56.000 | | 58.000 | 58.000 | 60.000 | 55.000 | 58.000 | 58.000 |
| No. of Blows (lb-ft) Lift 2: | 57.000 | 56.000 | | 58.000 | 58.000 | 62.000 | 55.000 | 56.000 | 57.000 |
| No. of Blows (lb-ft) Lift 3: | 56.000 | 55.000 | | | 58.000 | 68.000 | 57.000 | 57.000 | 61.000 |
| No. of Blows (lb-ft) Lift 4: | 55.000 | 56.000 | | 57.000 | 59.000 | 78.000 | | 58.000 | 58.000 |

Table C.6. ILS Results from Laboratory 6.

| Triaxial Test Data Sheet | | | | | | | | | |
|--|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| Specimen Data | | | | | | | | | |
| Specimen Number: | GB-1 | GB-2 | GB-3 | SW-1 | SW-2 | SW-3 | OK-1 | OK-2 | OK-3 |
| Cell No.: | | | | | | | | | |
| Wet Mass Spec. & Mold, (lb): | 30.354 | 30.347 | 30.348 | 31.330 | 31.446 | 31.182 | 30.383 | 30.414 | 30.315 |
| Wet Mass Specimen, (lb): | 19.089 | 19.081 | 19.083 | 20.065 | 20.181 | 19.917 | 19.118 | 19.148 | 19.050 |
| Initial Height of Specimen, in.: | 8.100 | 8.200 | 7.950 | 8.000 | 8.100 | 7.900 | 8.200 | 8.100 | 8.050 |
| New Height of Specimen, in.: | 8.105 | 8.127 | 8.198 | 7.940 | 7.933 | 7.925 | 7.793 | 7.999 | 7.847 |
| Average Diameter, in.: | 6.00 | 6.00 | 6.00 | 6.00 | 6.00 | 6.00 | 6.00 | 6.00 | 6.00 |
| Circumference, in. (manual): | | | | | | | | | |
| Circumference, in. (auto): | 18.850 | 18.850 | 18.850 | 18.850 | 18.850 | 18.850 | 18.850 | 18.850 | 18.850 |
| Area, in. ² : | 28.27 | 28.27 | 28.27 | 28.27 | 28.27 | 28.27 | 28.27 | 28.27 | 28.27 |
| Avg. Cross Sectional Area, in ² : | 28.74 | 28.84 | 28.95 | 28.89 | 28.75 | 28.93 | 28.60 | 28.74 | 28.68 |
| Dry-Back Data | | | | | | | | | |
| Wet Mass of Pan & Specimen, (lb) | 20.199 | 20.359 | 19.940 | 20.737 | 20.979 | 21.288 | 20.343 | 20.405 | 20.065 |
| Dry Mass of Pan & Specimen, (lb): | 19.156 | 19.271 | 18.871 | 19.887 | 20.116 | 20.463 | 19.273 | 19.328 | 18.975 |
| Mass of Pan, (lb): | 1.177 | 1.321 | 0.947 | 0.888 | 0.864 | 1.321 | 1.373 | 1.384 | 1.113 |
| Dry Mass of Material, (lb): | 17.978 | 17.950 | 17.924 | 18.998 | 19.252 | 19.142 | 17.900 | 17.944 | 17.862 |
| Mass of Water, (lb): | 1.044 | 1.088 | 1.069 | 0.850 | 0.863 | 0.825 | 1.070 | 1.077 | 1.091 |
| Moisture Content, (%): | 5.8 | 6.1 | 6.0 | 4.5 | 4.5 | 4.3 | 6.0 | 6.0 | 6.1 |
| Wet Density, (pcf): | 143.7 | 141.9 | 146.4 | 152.9 | 151.9 | 153.7 | 142.2 | 144.1 | 144.3 |
| Dry Density, (pcf): | 135.8 | 133.8 | 138.1 | 146.4 | 145.4 | 147.4 | 134.1 | 136.0 | 136.0 |
| SCA Data | | | | | | | | | |
| Total Energy (lb-ft) Lift 1: | 762.500 | 754.070 | 753.410 | 751.030 | 762.150 | 760.810 | 756.550 | 753.500 | 769.770 |
| Total Energy (lb-ft) Lift 2: | 758.360 | 755.990 | 755.530 | 762.190 | 757.990 | 757.970 | 756.120 | 751.180 | 759.410 |
| Total Energy (lb-ft) Lift 3: | 754.720 | 756.920 | 753.890 | 756.880 | 751.720 | 757.080 | 756.830 | 752.770 | 758.170 |
| Total Energy (lb-ft) Lift 4: | 760.110 | 752.370 | 753.830 | 753.470 | 750.730 | 755.020 | 756.080 | 753.260 | 758.400 |
| Energy/Lift (lb-ft) Lift 1: | 12.924 | 12.568 | 12.557 | 12.517 | 12.918 | 12.895 | 12.823 | 12.771 | 13.272 |
| Energy/Lift (lb-ft) Lift 2: | 13.075 | 13.034 | 13.026 | 12.918 | 13.069 | 13.068 | 13.037 | 12.951 | 12.871 |
| Energy/Lift (lb-ft) Lift 3: | 13.012 | 12.829 | 13.226 | 13.050 | 13.188 | 13.053 | 13.049 | 12.979 | 13.072 |
| Energy/Lift (lb-ft) Lift 4: | 13.105 | 12.540 | 13.225 | 13.219 | 13.171 | 12.797 | 13.036 | 12.987 | 13.076 |
| Avg. Drop Ht. (lb-ft) Lift 1: | 17.880 | 18.290 | 18.310 | 18.320 | 18.290 | 18.070 | 18.130 | 18.110 | 18.230 |
| Avg. Drop Ht. (lb-ft) Lift 2: | 17.830 | 17.780 | 18.320 | 18.280 | 18.300 | 18.180 | 18.280 | 18.290 | 18.100 |
| Avg. Drop Ht. (lb-ft) Lift 3: | 18.240 | 18.090 | 18.310 | 18.260 | 18.290 | 18.130 | 18.280 | 18.270 | 18.280 |
| Avg. Drop Ht. (lb-ft) Lift 4: | 18.240 | 17.960 | 18.240 | 18.290 | 18.240 | 18.020 | 18.250 | 18.240 | 18.250 |
| No. of Blows (lb-ft) Lift 1: | 59 | 60 | 60 | 60 | 59 | 59 | 59 | 59 | 58 |
| No. of Blows (lb-ft) Lift 2: | 58 | 58 | 58 | 59 | 58 | 58 | 58 | 58 | 59 |
| No. of Blows (lb-ft) Lift 3: | 58 | 59 | 57 | 58 | 57 | 58 | 58 | 58 | 58 |
| No. of Blows (lb-ft) Lift 4: | 58 | 60 | 57 | 57 | 57 | 59 | 58 | 58 | 58 |