

### Validation of Contractor HMA Testing Data

## in the Materials Acceptance Process

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by

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| Highway Administration  |                     |                           | runop or runon,      |                |
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|   |                     |                           |                      |                |
| 16. Abstract  |                     |                           |                      |                |
| This study conducted an analysis  | of the SCDOT H      | MA specification. A l     | Research Steer       | ing            |
| Committee comprised of SCDOT  | , FHWA, and Inc     | lustry representatives    | provided overs       | ight of the    |
| process. The research process included a literature review, a brief survey to which 42 highway          |                     |                           |                      |                |
| agencies replied, in-person interviews with a few selected agencies, and extensive statistical analyses |                     |                           |                      |                |
| of test data supplied by SCDOT.   |                     |                           |                      |                |
|   |                     |                           |                      |                |
| Analyses were conducted to determine appropriate standard deviation values to represent the             |                     |                           |                      |                |
| variability of each of the acceptance characteristics used by SCDOT. A total of 1,260 density test      |                     |                           |                      |                |
| results were provided from 22 different projects. A total of 1,775 asphalt content (AC) tests and       |                     |                           |                      |                |
| 1,343 air voids (AV) and VMA to   | ests were provide   | d from 30 different pr    | ojects.              |                |
| In addition SCDOT verification  | test results were o | btained from 10 proje     | ects and were a      | nalyzed and    |
| compared with their correspondit  | g contractor acce   | ptance tests. The proje   | vious and curre      | nt SCDOT       |
| verification procedures were evaluated and issues concerning each were presented and discussed          |                     |                           |                      |                |
| vermeation procedures were evaluated and issues concerning each were presented and discussed.           |                     |                           |                      |                |
| Ranges for the appropriate values   | to use for the wi   | thin-lot standard devia   | ations for Dens      | ity, AC, AV,   |
| and VMA were also developed. The analysis of verification tests results resulted in new verification    |                     |                           |                      |                |
| testing procedures that were recommended for consideration by SCDOT.                                    |                     |                           |                      |                |
|   |                     |                           |                      |                |
| 17. Koy Wordo   |                     | 19 Distribution Statement |                      |                |
| Specification Limits PWI Speci  | fications Risks     |                           |                      |                |
| Varification Tasting $F$ tast $t$ tast $\Omega^{\Lambda}$   |                     |                           |                      |                |
| Specifications  | , <b>Y</b> A        |                           |                      |                |
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|  | SI* (MODERN METRIC) CONVERSION FACTORS                               |  |  |  |  |   |  |   |  |
|--|--|--|--|--|--|---|--|---|--|
| APPROXIMATE CONVERSIONS TO SI UNITS  |  | APPROXIMATE CONVERSIONS FROM SI UNITS    |  |  |  |   |  |   |  |
| Symbol   | When You Know  | Multiply By                              | To Find  | <u>Symbol</u>  | Symbol   | When You Know   | <u>Multiply By</u>                         | <u>To Find</u>  | Symbol   |
|  |  | LENGTH                                   | I  |  |  |   | LENGTH                                     |   |  |
| in<br>ft<br>yd<br>mi   | inches<br>feet<br>yards<br>miles                                     | 25.4<br>0.305<br>0.914<br>1.61           | millimeters<br>meters<br>meters<br>kilometers  | mm<br>m<br>m<br>km   | mm<br>m<br>m<br>km   | millimeters<br>meters<br>meters<br>kilometers   | 0.039<br>3.28<br>1.09<br>0.621             | inches<br>feet<br>yards<br>miles                                      | in<br>ft<br>yd<br>mi   |
|  |  | AREA                                     |  |  |  |   | AREA                                       |   |  |
| in <sup>2</sup><br>ft <sup>2</sup><br>yd <sup>2</sup><br>ac<br>mi <sup>2</sup> | square inches<br>square feet<br>square yard<br>acres<br>square miles | 645.2<br>0.093<br>0.836<br>0.405<br>2.59 | square<br>millimeters<br>square meters<br>square meters<br>hectares<br>square kilometers | mm <sup>2</sup><br>m <sup>2</sup><br>m <sup>2</sup><br>ha<br>km <sup>2</sup> | mm <sup>2</sup><br>m <sup>2</sup><br>m <sup>2</sup><br>ha<br>km <sup>2</sup> | square millimeters<br>square meters<br>square meters<br>hectares<br>square kilometers | 0.0016<br>10.764<br>1.195<br>2.47<br>0.386 | square inches<br>square feet<br>square yards<br>acres<br>square miles | in <sup>2</sup><br>ft <sup>2</sup><br>yd <sup>2</sup><br>ac<br>mi <sup>2</sup> |
|  |  | VOLUME                                   | E  |  |  |   | VOLUME                                     |   |  |
| fl oz<br>gal<br>ft <sup>3</sup><br>yd <sup>3</sup>                             | fluid ounces<br>gallons<br>cubic feet<br>cubic yards                 | 29.57<br>3.785<br>0.028<br>0.765         | milliliters<br>liters<br>cubic meters<br>cubic meters                                    | mL<br>L<br>m <sup>3</sup><br>m <sup>3</sup>                                  | mL<br>L<br>m <sup>3</sup><br>m <sup>3</sup>                                  | milliliters<br>liters<br>cubic meters<br>cubic meters                                 | 0.034<br>0.264<br>35.314<br>1.307          | fluid ounces<br>gallons<br>cubic feet<br>cubic yards                  | fl oz<br>gal<br>ft <sup>3</sup><br>yd <sup>3</sup>                             |
| NOTE. VOIUI  | nes greater than 1000 L sha  |  |  |  |  |   | MASS                                       |   |  |
| oz<br>Ib<br>T  | ounces<br>pounds<br>short tons (2000 lb)                             | 28.35<br>0.454<br>0.907                  | grams<br>kilograms<br>megagrams<br>(or "metric ton")                                     | g<br>kg<br>Mg<br>(or "t")  | g<br>kg<br>Mg<br>(or "t")  | grams<br>kilograms<br>megagrams<br>(or "metric ton")                                  | 0.035<br>2.202<br>1.103                    | ounces<br>pounds<br>short tons (2000 lb)                              | oz<br>Ib<br>T  |
| 0-   | TEMPERA  | TURE (exact degre                        | es)  | 0.5  | TEMPERATURE (exact degrees)  |   |  |   |  |
| ۴  | Fahrenheit   | 5 (F-32)/9<br>or (F-32)/1.8              | Celsius  | °С   | °C   | Celsius   | 1.8C+32                                    | Fahrenheit  | F  |
|  |  | ILLUMINATIO.                             | N  |  |  |   | ILLUMINATION                               |   |  |
| fc<br>fl   | foot-candles<br>foot-Lamberts  | 10.76 lux<br>3.426 cano                  | dela/m <sup>2</sup>  | lx<br>cd/m <sup>2</sup>  | lx<br>cd/m²  | lux<br>candela/m²   | 0.0929<br>0.2919                           | foot-candles<br>foot-Lamberts   | fc<br>fl   |
| FORCE and PRESSURE or STRESS   |  |  |  | FORCE and  | PRESSURE or STRESS   |   |  |   |  |
| lbf<br>lbf/in <sup>2</sup>   | poundforce<br>poundforce per<br>square inch                          | 4.45 newt<br>6.89 kilop                  | tons<br>pascals  | N<br>kPa   | N<br>kPa   | newtons<br>kilopascals  | 0.225<br>0.145                             | poundforce<br>poundforce per<br>square inch                           | lbf<br>lbf/in <sup>2</sup>   |

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#### **CHAPTER 1 — INTRODUCTION**

#### Background

In the late 1980's, industry and the Federal Highway Administration (FHWA) encouraged states to move away from method specifications towards statistically based specifications and greater contractor quality control (QC) and Acceptance. After conducting initial research in this area, in the mid 1990's the SCDOT began implementing its first contractor QC/Acceptance program. This move was bolstered by the 1997 performance audit that recommended that the SCDOT "Implement a contractor self-certification program."

At that time, hot mixed asphalt (HMA) acceptance had utilized contractor QC/Acceptance data for nearly 10 years and a recent FHWA Quality Assurance (QA) Stewardship Review indicated that changes were needed to the current QC/Acceptance and Independent Assurance (IA) process associated with this program. The Stewardship review concluded that the SCDOT allowable differences in HMA test data were two to three times the current practice in other states and that the IA tolerances were in a similar need of analyzing and updating.

Because SCDOT inspectors no longer performed extensive routine HMA testing, the limited testing they performed must be used to accept or reject the contractor's test data and, consequently, the material it represents. The SCDOT needed to re-evaluate its current HMA QC/Acceptance and IA programs to ensure proper Department oversight and validation of the contractor's HMA testing data in accordance with Title 23, Code of Federal Regulations, Part 637 (*23 CFR 637*). (<u>1</u>)

A great deal of time and effort was devoted to the development of the SCDOT HMA QA Specification. The initial specification was developed over a five-year period with significant input from a joint SCDOT/Contractor/FHWA specification development committee ( $\underline{2}$ ). The HMA QA Specification was subsequently reevaluated ( $\underline{3}$ ) to establish how well the specification was working in the field and to uncover any problems that users of the specification had encountered. As part of this evaluation, based on statistical evaluation of project data, some modifications were made to the initial specification limits.

Since the re-analysis was completed, FHWA had issued Technical Advisory T 6120.3 (T 6120.3) ( $\underline{4}$ ) that provides more detailed and specific "guidance and recommendations for the use and validation of contractor's test results for acceptance, the use of quality measures, and the identification of contractor and department risks." There had also been significant discussion among professionals concerning the risks associated with validation procedures that may not be sufficient for the purposes intended in 23 CFR 637 or T 6120.3. See, for example, *Burati et al* 2004 ( $\underline{5}$ ) and *Burati and* Lin 2006 ( $\underline{6}$ ).

It was important, therefore, to once again conduct a formal and complete analysis of the SCDOT HMA specification in light of the information that had become available since it was last analyzed.

#### Objectives

The objectives of this study were:

- To examine the current SCDOT HMA QA specification, which includes QC, Acceptance and IA testing.
- To provide the SCDOT with technical assistance necessary to review and analyze project test data.
- To survey and interview officials in other state transportation departments (STDs) to obtain details of their existing validation and IA procedures.
- To make a detailed comparison of existing HMA QC, Acceptance, and IA specification requirements with recent FHWA technical recommendations on the use of contractor data for materials control and acceptance.
- To review the current allowable differences for HMA test validation and HMA IA test comparisons.
- To re-analyze the details of the current SCDOT HMA PWL analysis procedures along with the corresponding pay factors.
- To determine through analysis whether or not it is necessary to revise the tolerances that are currently used for comparing IA test results for the SCDOT IA program.
- To develop new procedures for validating contractor HMA test data that comply with the regulatory requirements of Title 23 Code of Federal Regulations, Part 637 (23CFR637).
- To develop an implementation plan for any specification changes that are recommended.
- To develop, if recommended by the FHWA QA Stewardship Review Team, guidelines for pilot projects to allow for more in-depth evaluation of proposed specification revisions and increased HMA data collection.

#### Methodology

The major items that needed to be accomplished to achieve the project objectives are discussed in each of the following sections. These major work tasks include:

- Establish a Research Steering Committee.
- Conduct a review of the existing literature.
- Survey other state departments of transportation (STDs) regarding their procedures.
- If needed, conduct interviews with selected STDs.
- Analyze test result data from SCDOT projects.
- Assist SCDOT, as needed, with revising the existing specification.
- If necessary, recommend implementation procedures for the new specification.

**Research Steering Committee.** The first step that was taken was to establish a Research Steering Committee (the Committee). Since all parties of the construction process, i.e., SCDOT, FHWA, and the construction industry, would be impacted by changes in the QC, Acceptance, and IA procedures, it was decided that individuals from all three of these groups would serve on the Committee. The Committee was charged to oversee the project on behalf of the SCDOT. The principal investigator (PI) served as the facilitator during meetings at which the Committee guided the PI in establishing the final tasks and timeline to meet the project objectives. These meetings were held in Columbia to minimize travel costs for team members. The members of the Committee are shown in Table 1.1.

| Name                   | Position                        | Organization       |
|------------------------|---------------------------------|--------------------|
| Merrill Zwanka (Chair) | State Materials Engineer        | SCDOT              |
| Milton Fletcher        | Materials and Research Engineer | SCDOT              |
| Chad Hawkins           | Quality Assurance Engineer      | SCDOT              |
| John McCarter          | DCE, District 4                 | SCDOT              |
| Danny Shealy           | Director of Construction        | SCDOT              |
| David Law              | Pavement and Materials Engineer | FHWA               |
| David Herndon          | Executive Director              | SCAPA              |
| James Horton           | QC Manager                      | Weaver Constr.     |
| Jim Burati             | Principal Investigator          | Clemson University |

#### Table 1.1. Research Steering Committee Team Members

**Literature Review.** A literature review was conducted to identify reports and publications that address various aspects of the use of contractor tests for acceptance as well as any procedures for validating contractor tests. First, a computer search using the facilities of the Clemson University Cooper Library was conducted. In particular, Transportation Research Records were searched for papers relating to the areas of research. A search of FHWA's website was also conducted. In addition, the FHWA National Highway Specifications website was studied and the HMA specifications were downloaded for all states identified as using contractor tests for acceptance purposes. The results of the literature review were summarized and presented to the Committee.

**Survey of STDs.** In addition to the literature review, a brief survey instrument was developed and sent by SCDOT to all state materials engineers by means of the Materials Engineer LISTSERVE. The survey instrument was also sent to FHWA's Federal Lands Highways division. This survey briefly explained the purpose for the study, and asked each STD to provide a copy of its current HMA specification as well as how it developed any comparison limits that it uses for validation or IA tests. The survey requested the name and contact information of an individual who could provide further information regarding the development and implementation of the state's verification procedures, and also asked if the STD was willing to participate in an in-person interview with members of the research team. The specifications that were provided were reviewed and summarized and presented to the Committee.

**Interviews with Selected STDs.** To obtain more in-depth information, it was planned that inperson interviews be conducted with a few selected STDs that use contractor test results in the acceptance decision. After the PI presented the summary of the survey responses, the PI and the Committee were to jointly select STDs to contact to set up in-person interviews. The STDs that agreed to participate were then to be interviewed by one or more members of the research team.

Before the interview, each STD was provided a list of questions that the Committee wanted to have answered. The interviews were then summarized and presented to the Committee.

**Analyze Project Test Data**. Statistical analyses were conducted on project test results data supplied by the SCDOT. It was planned that the test result data would be supplied in the form of Excel (XLS or XLSX) files or comma separated variables (CSV) files. In fact, much of the data was provided as paper copies of SCDOT test reports. This necessitated that the data be input manually into Excel spreadsheet files that could then be imported for subsequent analyses by Minitab statistical software. This required a significant amount of time for data entry and checking to ensure that data entry errors were eliminated, or at least kept to a very low number.

The variability data from the projects, in terms of standard deviations, were compared with current specification limits to determine if the limits are still appropriate. The risks to both the contractor and the SCDOT could then be evaluated and used in the evaluation of the existing limits.

The project test results were also analyzed with respect to the current SCDOT validation and IA procedures, including the appropriateness of the existing comparison limits. These limits were also compared with those of other STDs that were identified during the survey. Statistical analyses included determination of the power of the existing comparison limits to identify differences between contractor and STD tests for various sample sizes. A risk analysis considered the ability of differing comparison limits to detect actual differences as well as the corresponding likelihoods of incorrectly identifying differences that do not actually exist. The comparison limits studied in the analyses spanned the range identified from the STD specifications that were reviewed for the project.

**Revising the Existing Specification**. The initial plan was for the Committee, based on all of the information provided, including survey, interview, and statistical and risk analyses results, to determine whether or not revisions to the limits and procedures of the existing HMA QA specification were necessary. If it was the consensus of the Committee that revisions were needed, the research team would provide any necessary information to assist the Committee in determining what revisions to make. The PI was to serve as facilitator for all meetings that were necessary for the Committee to reach a consensus on the required revisions.

The original plan was changed after the project began. Based on the FHWA stewardship review, SCDOT decided that it needed to have a new verification procedure to use on projects to be let in the 2008 construction season. So, the SCDOT developed new validation procedures before any survey, interview, or data analyses results were available. The proposed new procedures were reviewed by the PI. The PI also met with industry representatives to discuss their concerns over the new draft procedures that SCDOT had developed. The new procedures were discussed at a meeting of the Committee on March 11, 2008, and then SCDOT finalized the procedures that were implemented on an interim basis, pending the findings and recommendations of the current research project.

**Implementation Procedures**. As noted in the previous section, new validation procedures have already been implemented on an interim basis. Therefore, it should be relatively easy for the Committee to decide if, and how, it will implement any of the recommendations that resulted from this research project.

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#### **CHAPTER 2 — LITERATURE REVIEW**

#### Background

The purpose of this literature review is to identify publications that address contractor tests for acceptance as well as any procedures used for validating contractor tests. There has been an evolutionary process in the way asphalt paving projects are constructed and how quality is measured. In many STD programs today, the contractor has the responsibility for process control (quality control or QC) and Acceptance Testing, and the STD does a moderate amount of verification testing. As contractor tests for acceptance are becoming used more in the asphalt paving industry, questions are being raised about their legitimacy.

In the early days of formal highway construction the responsibilities were distributed in such a way that the STD had more control over the work. The STD controlled the production, production rates, and process control of mainline paving. The contractor essentially supplied the financing, the labor, and the equipment needed to complete the project. This scenario, where the product quality is the responsibility of the STD, is the result of the method type specification which was in use at the time. The *TRB Glossary of Highway Quality Assurance Terms* defines method-type specifications as "specifications that require the contractor to use specified materials in definite proportions and specific types of equipment and methods to place the material." Method type specifications generally force the agency to accept the final product regardless of actual quality (<u>7</u>).

#### **Evolution of Quality Assurance Specifications**

OA specifications emerged as the industry recognized the need for contractors to have more control over their own processes. There was a fundamental transition where contractors performed QC testing, and the STD performed the Acceptance Testing. This approach is typical in QA specifications, where the functions of QC and Acceptance are clearly separated. This division is an integral part of QA. QA specifications reflect a mix of specifying both methods and end result testing. They specify methods for processes that do not have good or practical end result tests. For example, the segregation of aggregate is something that is difficult to measure in place. Prescriptive methods are written to help minimize aggregate segregation because there is not a good end result test to measure it. QA specifications also demonstrate a shift towards end result specifications. End result specifications, as defined by the TRB Glossary, are "specifications that require the contractor to take the entire responsibility for supplying a product or an item of construction. The STD's responsibility is either to accept or reject the final product or to apply a pay adjustment commensurate with the degree of compliance with the specifications" (7). Contractors have the opportunity to use other methods of compaction, scheduling techniques, and new technologies to get the desired result faster and more cost effectively.

This situation where the contractor is responsible for the quality, but the STD performs the Acceptance Testing, is still being used in STDs today. Potential reasons for this are there may not have been a need to reduce agency employment, or the agency does not believe that it is appropriate to give the contractor responsibility for Acceptance Testing. Currently, the majority of STDs are using contractor tests for acceptance (<u>8</u>). During the 1990's many STDs experienced a decline in resources that meant staff cuts. QC and Acceptance Testing were

observed to be an easy and practical area to place more responsibility on the contractor and to reduce work load on STD testing personnel. To do this, a methodology for verification testing is needed to ensure the STD is getting the quality it desires.

STDs that have opted to make this transition to using contractor acceptance tests have developed and integrated verification procedures into their specifications. The process of developing the methodology requires the specification developer to make assumptions to later be verified or refined. For instance, verification plans require sampling and testing procedures that inherently exhibit risks to both the STD and the contractor. These risks may not be fully evaluated before implementation. The need to make assumptions shows that QA specifications are evolutionary in nature.

#### 23 CFR 637 B

FHWA issued *Title 23 Code of Federal Regulations Part 637 Subpart B* (23 CFR 637 B) to mandate certain basic characteristics of a QA plan. It has also created a standard for STDs to meet which subsequently keeps them aligned with other STD's QA programs. *Technical Advisory T 6120.3* (<u>4</u>), issued by FHWA in August of 2004, further explains these points by providing insight and recommendations. Some key topics addressed in these documents include:

- Independent Assurance (IA).
- Split vs. Independent samples.
- Requirements for qualified testing facilities and technicians.
- Dispute Resolution.

**Independent Assurance.** 23 CFR 637 B requires that a QA program have an IA program to assure the STD that their testing equipment and the contractor's testing equipment are calibrated properly, and that the sampling and testing personnel are performing to standard. The IA program shall evaluate all testing procedures involved in the QA program on a periodic basis. IA complements the QA program by verifying procedure integrity. When assessing the testing equipment and procedures, split samples are used rather than independent samples. This is further discussed in the following section.

**Split vs. Independent Samples.** 23 CFR 637 B requires that all samples used for QC and verification sampling and testing shall be random independent samples. This means that a contractor cannot take samples, split them, and have the STD run a verification test on one of the split samples. However, this does not mean that split samples can never be used in verification testing. Figure 2.1 shows different scenarios of how samples can be taken and which samples can be used in the verification procedure.



Figure 2.1. Verification and IA Testing Utilizing Split Samples (after <u>4</u>)

Figure 2.1 demonstrates how IA and verification testing can be done efficiently. It shows that as long as the samples are organized appropriately both IA and verification testing can be accomplished by sharing data. A sample from each lot or sublot is split and an IA test can be performed on one of the split samples. These IA tests can be used as verification tests provided the corresponding split samples are removed from the contractor test results. This assures that the verification tests are independent from the acceptance tests in the verification procedure. If the contractor's acceptance tests are verified, then all of his samples are used for the acceptance decision, where the payment factor is calculated. Otherwise, the STD will use a dispute resolution process to investigate the reason for the verification failure, or use their samples to determine the payment factor.

The STD needs to have samples independent of the contractor's samples to capture the variability of the materials, process, sampling, and testing, all of which must be integrated into the verification limits. If only split samples are used, the STD captures only the contractor's testing variability, which does not fulfill the purpose of verification testing. However, the split samples can be used for the IA program.

**Qualified Testing Facilities and Technicians.** 23 CFR 637 B requires that all sampling and testing to be used in the acceptance decision or in the IA program shall be executed by qualified sampling and testing personnel, and that testing can occur only in qualified laboratories. It is left up to the STD to determine how to qualify a technician or laboratory. The laboratories must, at a minimum, include provisions for checking test equipment and the laboratory shall keep records of calibration checks. Each STD's central laboratory must be accredited by the AASHTO Accreditation Program or an equivalent accreditation program. (1)

**Dispute Resolution.** To ensure checks and balances are in place in verification procedures, 23 CFR 637 B mandates that a dispute resolution process be in place for STDs who choose to use results from contractor testing in the acceptance program. "The dispute resolution system shall address the resolution of discrepancies occurring between the verification sampling and testing and the quality control sampling and testing" (1). By formalizing a dispute resolution system it should provide means for minimizing adversarial relationships and claims. Three primary scenarios for dispute resolution should be developed and integrated into a QA plan (9):

- Disputes where contractor and STD test for same property with different procedures.
- Disputes where contractor and STD data do not compare.
- Disputes where no test data are applicable (e.g., segregation, workmanship, and manufactured products defects).

#### QC vs. Acceptance Testing

23 CFR 637 B states that results of "QC sampling and testing results may be used as part of the acceptance decision...(1)" The fact that an integral part of QA specifications is the separation of QC and Acceptance Testing, as discussed earlier, may seem to contradict this previous statement. 23 CFR 637 B is inconsistent in the terms used in the regulation, as it can be easily misconstrued that QC tests should be used in the acceptance decision. A misconception is that all contractor tests are QC tests and all STD tests are acceptance tests. Contractor tests performed separately and independently from QC, i.e., acceptance tests, are used in the acceptance decision once they are verified by the STD. *Burati and Hughes* believe that QC and acceptance functions should be separated regardless of who performs the acceptance testing (<u>10</u>).

Acceptance tests are typically inappropriate for QC and vice versa. The intent with an acceptance test is to measure the in place quality and make a payment decision based on the result. Conversely, the intent of a QC test is to monitor the production process to ensure that unacceptable material is not integrated into the project. "For an acceptance test to be statistically valid, the sample to be tested must be obtained in a random or stratified manner" (<u>11</u>). If the contractor discovers a suspicious QC test result, it may choose to retest the material. Both tests must be reported, but the second sample cannot be considered random. Again this highlights the importance of separating QC and acceptance testing to ensure a valid verification procedure.

#### **Verification Methods**

23 CFR 637 B does not say how data should be verified, but T 6120.3 explains the different methods and makes a recommendation. This recommended validation procedure for comparing contractor and STD data is the use of the statistically based *F*-tests and *t*-tests. Brief descriptions of different verification methods are discussed below:

**One-to-One Comparison.** The easiest verification method is a one-to-one comparison. This approach determines the results from the contractor test and the STD test done on a split sample, and compares the difference to some allowable limit. The difference two-sigma (D2S) limit is commonly used for comparing two split samples. D2S limits can be found in many AASHTO and ASTM test procedures (<u>12</u>). The limits are established by testing manufactured 'identical' samples by multiple labs. These limits may be too tight for actual conditions, so other ways to establish limits may be used. It is important to remember that if split samples are compared, the only variability under consideration is testing. For example, if the difference in test results is less than the comparison limit, then the testing procedure under consideration is a "pass." This procedure is inherently the least powerful method because the sample size is one, which makes it difficult to detect real differences unless the test results are far apart (<u>12</u>).

**Paired t-test.** The paired *t*-test is a useful procedure for comparing sets of STD and contractor split sample test results. This test can be done on an accumulated amount of one-to-one comparisons of split samples from the contractor and STD. The test checks to see if the differences *within* pairs are significantly different from zero. This method is more powerful than a one-to-one comparison such as using D2S limits because the sample size is greater than one.

**F-test and t-test.** The *F*-test is used to compare the variability and *t*-test is used to compare the means of the verification and acceptance test data. First, the variabilities are tested with the *F*-test (see equation 2.1). If the variabilities are statistically significantly different, then it indicates that the samples are not likely from the same population. Next, the means are tested with the *t*-test. There are two different equations for finding the test statistic for the *t*-test (see equation 2.2 and 2.3). If the variabilities were not significantly different, then the pooled variance (see equation 2.4) is used to find the test statistic for the *t*-test. If the variabilities were significantly different, the two sample variances are used to compute the test statistic (see equation 2.2).

$$F = \frac{s_1^2}{s_2^2}$$
(2.1)

$$t = \frac{\overline{X}_1 - \overline{X}_2}{\sqrt{\frac{s_1^2}{n_1} + \frac{s_2^2}{n_2}}}$$
(2.2)

$$t = \frac{\overline{X}_{1} - \overline{X}_{2}}{s_{p}\sqrt{\frac{1}{n_{1}} + \frac{1}{n_{2}}}}$$
(2.3)

$$s_{p} = \sqrt{\frac{(n_{1}-1)s_{1}^{2} + (n_{2}-1)s_{2}^{2}}{n_{1}+n_{2}-2}}$$
(2.4)

One reason that the *F*-test and *t*-test approach is more powerful is because not only does it compare the means of two data sets, it also considers the variability. If only one measure is used to compare data sets, the risk of concluding the data are the same when they actually are not is increased. Also, with increased sample sizes associated with *F*-tests and *t*-tests, the risks to both the STD and contractor are reduced. Similarly, when paired *t*-tests are used in IA, there is an increased sample size that reduces the probability of an error. (4, 11)

When using the statistical approach for validating data, a critically important decision about the level of risks to the STD and the contractor must be made before data analysis begins. An alpha value ( $\alpha$ ), or level of significance, is the probability of making a Type I error, or determining that the data are significantly different when they are not. Typically, alpha values range from 0.01 to 0.10, with 0.05 being the most common. The contractor would like to lower the probability of a Type 1 error so an alpha value of 0.01 would be most beneficial to the contractor. The beta value ( $\beta$ ) is the probability of making a Type II error, or accepting that the data are similar when they are not. This can be identified as the STD's risk. Since  $\beta$  is inversely related to the level of significance ( $\alpha$ ) and directly related to the sample sizes, a balance of acceptable risks needs to be determined by the STD (<u>12</u>).

#### Industry Acceptance

A common opinion of some STDs and research papers is that contractors should not conduct tests for acceptance because of the apparent conflict of interest. (13, 14, 15, 16) *Mahboub*, *Hancher and Wang* (13) conducted a survey of all STDs and some large contractors. A frequent comment from STDs was that they have a general lack of trust in the contractor-performed test data.

Exhibit 2.1 shows the questions used in a survey by *Parker and Turochy* (<u>17</u>) and Table 2.1 summarizes the survey responses. The survey was sent to 500 NICET certified asphalt technicians and 21 technicians in a course sponsored by the Florida DOT. The responses to these surveys indicate the perception that contractor acceptance testing is like the "fox guarding the henhouse," or giving the contractor control over its payment. This perception is human nature and should be addressed within the STD. *Killingsworth and Hughes* state that, due to human nature, STD personnel must make a psychological adjustment to accept the fact that contractor test results will be used to establish the pay factor (<u>11</u>).

- **1.** My employer is
  - □ a state department of transportation
  - $\Box$  a contractor,
  - $\Box$  a consultant, or
  - $\Box$  other
- **2.** I am involved in sampling and testing to control the production and placement of construction materials and/or the acceptance of these materials. Acceptance may be pass/fail or involve adjustments to bid process.
  - $\Box$  Yes continue

 $\square \ No-stop$ 

- **3.** Have you ever felt pressure to produce test results, or to retest, to give more favorable control or acceptance outcomes?
  - $\Box$  Yes continue
  - $\square \ No-stop$
- **4.** Was the pressure you felt to produce test results that would give more favorable outcomes
  - $\hfill\square$  Self-induced you just felt you should, or
  - $\hfill\square$  Due to specific reasons/instructions/comments from supervisors?
- **5.** How easy/difficult would it be to manipulate test results to achieve more favorable outcomes?

Easy Difficult 1 2 3 4 5

- **6.** Please rank, from 1 (most effective) to 5 (least effective), the following techniques for preventing manipulation of test results.
  - a. sampling and testing of split samples for comparison \_\_\_\_\_
  - b. sampling and testing of independent samples for comparison \_\_\_\_\_
  - c. occasional observation of sampling and testing procedures \_\_\_\_\_
  - d. use contractor-performed tests for process control and state DOT-performed tests only for acceptance \_\_\_\_\_
  - e. periodic (weekly or monthly) audit and comparison of contractor and state DOT test results by an independent organization \_\_\_\_\_

#### Exhibit 2.1. Asphalt Technician Survey Questions (17)

| Quest<br>No.    | ion 1<br>(%)            | ζuest<br>γ/ν (γ    | tion 2<br>^ / N %) | Quest<br>Y/N (Y    | ion 3<br>/ N %)     | Quest                  | ion 4*  | Ques<br>(Ave | tion 5<br>rage) | Quest<br>(Method                          | tion 6<br>  – Rank)                              |  |
|-----------------|-------------------------|--------------------|--------------------|--------------------|---------------------|------------------------|---|--------------|-----------------|---|--|--|
| ы               | NICET                   | FDOT               | NICET              | FDOT               | NICET               | FDOT                   | NICET   | FDOT         | NICET           | FDOT                                      | NICET  |  |
| ultants<br>[1%) | Consultants<br>95 (66%) | 1/1<br>50/50%      | 90 / 5<br>95 / 5%  | 0 / 1<br>0 / 100%  | 61 / 30<br>67 / 33% | I                      | A 33 (54%)<br>B 11 (18%)<br>C 8 (13%)<br>D 7 (11%)<br>E 1 ( 2%)<br>F 1 ( 2%)  | 1.00         | 1.28            | a - 1<br>b - 2<br>c - 3<br>d - 5<br>e - 4 | a - 1<br>b - 2<br>c 2<br>e - 5<br>f - 5<br>f - 5 |  |
| actors<br>14%)  | Contractors<br>17 (12%) | 8 / 0<br>100 / 0%  | 15 / 2<br>88 / 12% | 3 / 5<br>38 /62%   | 10 / 5<br>67 / 33%  | A 0(0%)<br>B 3(100%)   | A 6(60%)<br>B 3(30%)<br>C 1(10%)  | 3.12         | 1.37            | a - 2<br>b - 1<br>c - 4<br>d - 5<br>e - 3 | a - 2<br>b - 1<br>c - 4<br>d - 5<br>e - 3        |  |
| ЮТ<br>39%)      | DOT<br>7 (5%)           | 7 / 0<br>100 / 0%  | 6 / 1<br>86 / 14%  | 1/6<br>14/86%      | 2 / 4<br>33 / 67%   | A 1 (100%)<br>B 0 (0%) | A 1 (50%)<br>B 1 (50%)  | 1.50         | 1.26            | a – 2<br>b – 3<br>c – 4<br>d – 1<br>e – 5 | a – 1<br>b – 5<br>c – 2<br>d – 4<br>e – 3        |  |
| .her<br>(6%)    | Other<br>24 (17%)       | 0 / 1<br>0 / 100%  | 23 / 1<br>96 / 4%  | I                  | 15 / 8<br>65 / 35%  | 1                      | A 5 (33%)<br>B 3 (20%)<br>C 2 (13%)<br>D 4 (27%)<br>F 1 (7%)                  | I            | 1.24            | I   | a - 1<br>b - 2<br>c - 3<br>d - 5<br>e - 4        |  |
| 4II<br>100%)    | All<br>143 (100%)       | 16 / 2<br>89 / 11% | 134 /94<br>94 / 6% | 4 / 12<br>25 / 75% | 88 / 47<br>65 / 35% | A 1 (25%)<br>B 3 (75%) | A 45 (54%)<br>B 18 (21%)<br>C 11 (12%)<br>D 11 (12%)<br>E 1 (12%)<br>F 2 (2%) | 2.33         | 1.27            | a – 1<br>b – 2<br>c – 4<br>d – 3<br>e – 5 | a - 1<br>b - 2<br>c - 3<br>d - 5<br>e - 4        |  |
| Superviso       | or B: Self C            | : Supervisor an    | d Self D: Con      | tractor E: Cli     | ents E: No Ro       | esponse                |   |              |                 |   | 4  |  |

Table 2.1. Summary of Responses to the Asphalt Technician Survey Questions (<u>17</u>)

There are a number of advantages and disadvantages discussed in the literature. By having contractors do their own acceptance testing it encourages a more careful testing process, where more attention is placed on maintaining sample integrity and the testing procedures themselves (<u>11</u>). Contractors certainly should place more attention on their sampling and testing procedures knowing that the test results will be used in the payment decision. If a contractor's test results are not verified and the STD uses its own data to determine payment, the risk of coming to an incorrect decision is increased due to the resulting smaller sample size. This poses a great financial threat to the contractor because it could ultimately be paid for less than the actual quality or even be required to remove and replace. Another advantage is the advanced knowledge the contractor gains by doing its own acceptance tests. A pay factor can be projected assuming the data are verified and the contractor can anticipate the pay factors associated with each lot (<u>11</u>).

A debatable advantage is the reduced inspection staff required at the STD as a result of contractors performing acceptance tests. Depending on the level of risk associated with the number of verification samples the STD tests, there may or may not be a significant reduction in staff by having contractors conduct acceptance tests (<u>11</u>).

The primary disadvantage of using contractor tests for acceptance that was expressed in research papers examining the adequacy of contractor tests is the fact that the contractor and STD data do not consistently compare. Frazier and Turochy (<u>16</u>) found that in six states considered, there was a consistent trend of significant differences in contractor and state data with a 1% level of significance. They also found that the contractor means and variances tended to be more favorable values. These data are compiled with similar data from other papers and discussed in the next section.

#### Analysis of Contractor Acceptance Test Data

Large data sets for Georgia, North Carolina, Florida, Alabama, Kentucky, Kansas, California, and New Mexico have been compiled and analyzed in various research papers to see if contractor and STD test data are coming from the same populations (<u>13</u>, <u>14</u>, <u>15</u>, <u>16</u>, <u>17</u>). The data provided in Table 2.2 are a result of compiling all available data for each STD and corresponding contractor tests. Descriptions of the verification procedures and available data for the states analyzed are provided in the following sections.

**Florida (FDOT):** FDOT conducts verification testing and independent sample verification testing (ISVT) on asphalt content and 9 gradation sieves. The verification testing is performed on split samples, and a one-to-one comparison is used to determine if contractor acceptance tests are used in the pay factor computation. For material density the contractor takes 5 cores per 500-ton sublot and FDOT will test 5 cores in a lot. FDOT then uses one-to-one comparisons to verify the core density. The ISVT results are compared with specification tolerances, and production may be stopped if the ISVT shows that the mix is out of tolerance. For ISVT, 2 tests are done for every 12,000 tons, or 6 lots. A total of 98 projects from the 2003 and 2004 construction season were analyzed.

**Georgia (GDOT):** *t*-tests are performed on 8 gradation sieves and asphalt content, although only 4 sieves are used for pay adjustment. GDOT randomly takes 2 samples for every 5

contractor samples. GDOT takes 1 split sample for every 10 contractor samples for IA. Data from the 2003 construction season were used for analysis.

**Alabama (ALDOT):** Acceptance tests included asphalt content, air voids, and density. However, only asphalt content and air voids were analyzed in the study. The acceptance procedure comprised of computing the average absolute deviation from the JMF target and was modified during implementation. Data used for analysis included 80 mix designs from 1990 to 1992 during the implementation of the Alabama Highway Department's QA specifications.

**North Carolina (NCDOT):** The NCDOT performs 2 types of testing: QA (split samples) and verification (independent samples). Density and the following mix properties are tested: asphalt content, air voids, VMA,  $\%G_{mm}$  @ N<sub>i</sub>, VFA, and 7 gradation sieves. QA testing is done at a rate of 1 NCDOT test per every 10 contractor tests and the results are compared with precision limits. Verification testing is performed at a rate of 5%, or 1 out of every 20 contractor tests. When a QA comparison is not within precision limits the engineer investigates the source of the error and pay adjustments are applied as a last resort. A total of 735 mix designs from the 2004 construction season were analyzed.

**California (Caltrans):** QA procedures include both density and mix properties, although only mix properties were provided for analysis. The mix properties tested are asphalt content and 6 gradation sieves. Caltrans performs verification testing at a rate of 10% with independent samples. A lot is an entire project's production and a sublot is 500 tons.

Analysis was performed on data from 149 projects between 1996 and 2005.

**Kansas (KSDOT):** Theoretical MSG, AV, and mat density are analyzed. Asphalt content and gradation tests are performed by the contractor and KSDOT but only for process control. Density is most commonly tested by nuclear gages but cores may also be used. Contractors take 4 verification tests per lot and KSDOT takes 1 test per lot. Means are compared with *t*-tests and if contractor data are verified they are used in the acceptance decision. A lot is 3000 tons and is split up into 4 sublots of 750 tons each. A total of 49 projects from the 2003 construction season were analyzed.

It appears from the summary data in Table 2.2 that there is a tendency for the variabilities between the STD and the contractor data to be significantly different. There is no distinct pattern, although out of the 15 STD and Contractor comparisons, 14 (93%) of the variabilities are significantly different. Only 4 out of the 15 average differences (27%) show evidence of a significant difference.

| Source     | п      | α    | Avg.<br>Diff. | Sig.<br>Diff.? | σ     | Sig.<br>Diff.? |
|------------|--------|------|---------------|----------------|-------|----------------|
|            |        | Asp  | halt Conten   | t              |       |                |
| AL         | N/A    | 0.05 | -0.045        | no             | 0.272 | yes            |
| Contractor | N/A    | 0.05 | -0.036        |                | 0.230 |                |
| KY         | 3,082  | 0.05 | -0.007        | no             | 0.210 | yes            |
| Contractor | 3,082  | 0.05 | -0.007        |                | 0.152 |                |
| GA         | 2,487  | 0.01 | 0.004         | no             | 0.253 | yes            |
| Contractor | 14,061 | 0.01 | 0.005         |                | 0.200 |                |
| FL         | 526    | 0.01 | 0.016         | no             | 0.290 | yes            |
| Contractor | 2,307  | 0.01 | -0.012        |                | 0.249 |                |
| NC         | 814    | 0.01 | -0.021        | no             | 0.286 | yes            |
| Contractor | 14,396 | 0.01 | -0.003        |                | 0.243 |                |
| СА         | 1,405  | 0.01 | 0.036         | yes            | 0.295 | yes            |
| Contractor | 9,258  | 0.01 | -0.003        |                | 0.205 |                |
|            |        | 1    | Air Voids     |                |       |                |
| AL         | N/A    | 0.05 | -0.357        | yes            | 1.025 | yes            |
| Contractor | N/A    | 0.05 | -0.281        |                | 0.863 |                |
| KY         | 1,827  | 0.05 | 4.063         | no             | 0.978 | yes            |
| Contractor | 1,818  | 0.05 | 4.086         |                | 0.853 |                |
| FL         | 469    | 0.01 | -0.285        | no             | 1.144 | yes            |
| Contractor | 2,063  | 0.01 | -0.248        |                | 0.841 |                |
| NC         | 817    | 0.01 | -0.161        | no             | 1.039 | yes            |
| Contractor | 14,225 | 0.01 | -0.097        |                | 0.751 |                |
| KA         | 393    | 0.01 | 0.322         | no             | 0.802 | yes            |
| Contractor | 1,494  | 0.01 | 0.262         |                | 0.564 |                |
|            |        |      | VMA           |                |       |                |
| КҮ         | 422    | 0.05 | 1.225         | no             | 1.037 | no             |
| Contractor | 422    | 0.05 | 1.267         |                | 0.940 |                |
| FL         | 469    | 0.01 | -0.508        | no             | 1.011 | yes            |
| Contractor | 2,095  | 0.01 | -0.490        |                | 0.858 |                |
| NC         | 808    | 0.01 | 1.217         | yes            | 1.459 | yes            |
| Contractor | 14,225 | 0.01 | 1.507         |                | 1.343 |                |
|            |        |      | Density       |                |       |                |
| AL         | N/A    | 0.05 | -1.245        | yes            | 1.470 | yes            |
| Contractor | N/A    | 0.05 | -0.997        |                | 1.175 |                |

Table 2.2. Summary of STD and contractor comparisons (after 17, 18)

#### Conclusion

From the publications identified in this literature search, it is apparent that there is no industrywide consensus on the adequacy of using contractor tests for acceptance. The number of STDs with statistical data analysis over a large number of projects found during the literature review is limited to GA, NC, FL, AL, KY, KS, CA, and NM.

These publications look at data from a statewide, multi-project standpoint down to a single project with 6 or more test results for analysis. Consistent results are not typical as there is no distinguishable pattern of data coming from the same or different populations.

There are a number of potential reasons that significant differences arise in contractor and STD performed tests. With knowledge of these potential reasons the STD can make an effort to minimize its chance of affecting the validation procedure. Some of these reasons are provided below in no particular order:

- The number of specimens tested by contractor and state agency technicians.
- The time between sampling and testing of specimens often found between contractors and state agencies (13).
- Differences in procedures.
- Failure to follow prescribed procedures.
- Incorrectly calibrated testing equipment.

#### CHAPTER 3 — SURVEY RESULTS

#### Background

This chapter summarizes and discusses the responses to a survey sent out by SCDOT in December of 2007. The survey was developed by SCDOT and then reviewed by the PI. Its purpose was to gain knowledge about whether other states use contractor test results for acceptance as well as to identify other aspects of their acceptance and verification processes. The surveys were sent out to the Materials Engineer of each agency as well as the Federal Lands Highway Divisions. The survey questions are shown in Exhibit 3.1.

- **1.** Does your agency use Contractor test results for acceptance of hot-mix asphalt (HMA)?
- **2.** If your answer to 1 was no, did you consider using Contractor tests results for acceptance? If so, why did you decide against it?

NOTE: If you don't use Contractor's test results for acceptance you have finished the survey. If you use Contractor's tests results for acceptance, please complete the remaining portion of the survey.

- **3.** Why did you decide to use Contractor test results for acceptance?
- 4. What HMA properties do the Contractors sample and test for acceptance?
- **5.** Does your agency have a HMA verification program that is separate from your Independent Assurance sampling and testing program?
- 6. Are the verification tests the same as the acceptance tests?
- **7.** What are your sampling locations and frequencies of acceptance and verification sampling and testing?
- **8.** If you use mix volumetrics for acceptance and verification, do you re-heat the verification samples from ambient room to the proper compaction temperature before testing?
- **9.** What procedure do you use to compare acceptance test results with your verification test results?

#### **Exhibit 3.1 Survey Questions**

In addition to the information gained from the survey responses from the State Highway Agencies (SHAs), the technical specifications for the participating SHAs were also assembled. Some of the SHAs responding included an attachment of their specifications to the survey, while others were gathered using the SHA's website. These specifications were used to provide more detailed information on the individual SHA's testing procedures.

#### **Survey Summary**

A total of 42 agencies, including 40 states, the FHWA Western Federal Lands Highway Division (WFLHD), and the province of Ontario, Canada (ONT), responded to the survey. This section breaks down the responses on a question-by-question basis. The responding agencies, along with whether or not they use Contractor tests for acceptance, are shown on the map in Figure 3.1.



#### Figure 3.1. Agencies Responding to the Survey and whether They Use Contractor Tests

**Question 1.** *Does your agency use Contractor test results for acceptance of hot-mix asphalt (HMA)?* 

A total of 28 agencies responded that they use contractor tests results for HMA acceptance, while 14 agencies responded that they did not. The responses of the agencies were divided as shown in Table 3.1.

| Use? | No. | Agency   |
|------|-----|--|
| Yes  | 28  | AL, AR, CA, CT, FL, GA, ID, IL, IA, KS, KY, MD, MS, MO, NE, NY, NC, ND, NM, OH, ONT, OK, SC, SD, UT, VA, WFLHD, WY |
| No   | 14  | AK, AZ, CO, DE, LA, ME, MI, MT, NV, NH, NJ, RI, TN, WA   |

# **Question 2.** If your answer to 1 was no, did you consider using Contractor tests results for acceptance? If so, why did you decide against it?

This question was just for the agencies that indicated that they do not use contractor tests for acceptance. This question was used to determine the reason the agency has chosen not to use contractor test results for acceptance. This question provides insight into some of the perceived problems that can be associated with using contractor tests for acceptance.

The most common answer for this question was that agencies believed that there was a conflict of interest with the contractor doing the acceptance testing. For example, if there is a test that does not meet the specifications then the contractor has a conflict of interest in whether or not to report the correct numbers, which may result in a lower pay factor or the material having to be replaced, or to manipulate the numbers to be in compliance with the specification. This was the reason that AZ, NH, RI, TN, and WA gave for not using contractor tests for acceptance. MI's response said that at one time they used contractor tests for acceptance, but the program was ended as a result of a fraud investigation by the FHWA. CO said they had problems with a pilot program and that was their reason for not using contractor tests for acceptance. ME said there was no advantage of using contractor tests for acceptance, but do not at this time.

#### Question 3. Why did you decide to use Contractor test results for acceptance?

This question was designed to gather information on why agencies have decided to use contractor test results for acceptance. The most common response was that the contractor takes better care of the testing when their tests are used for acceptance. There were 11 agencies that said this played a role in their decision to use contractor tests for acceptance. The next most common response was that there was a shortage in agency personnel to perform all of the tests themselves. IL's response was that allowing the contractor to perform the acceptance tests allowed for higher testing frequency and quicker turnaround on results as compared to the agency doing the testing themselves. By having quicker turnaround on the results they felt as though the contractor was better able to adjust the mix to stay within the specification limits. NM said that they had achieved improvements in HMA quality by using a statistically based acceptance decision with an incentive/disincentive program. One agency also cited a cost savings as the reason for switching to contractor tests for acceptance.

#### Question 4. What HMA properties do the Contractors sample and test for acceptance?

This question was asked to see which properties each agency requires the contractor to test for acceptance. There are five properties that are used by a large number of agencies, with a larger number of properties that are used by a smaller number of agencies. The five properties that are most commonly used are: laboratory air voids, gradation, roadway density, asphalt cement content, and voids in mineral aggregate (VMA). The less common tests that are used include: dust to asphalt ratio, voids filled with asphalt (VFA), smoothness, G<sub>mm</sub>, G<sub>se</sub>, N<sub>ini</sub>, N<sub>max</sub>, film thickness, maximum specific gravity, fractured face count, and moisture content. Table 3.2 shows a summary of the number of agencies that use each of these tests. Table 3.3 shows a breakdown of the agencies that use each of the more common tests.

#### Table 3.2. Characteristics for which Contractor Tests Are Used for Acceptance

| Property  | Number of Agencies |
|---|--------------------|
| Laboratory Air Voids  | 23                 |
| Gradation   | 21                 |
| Roadway Density   | 18                 |
| Liquid AC Content   | 18                 |
| VMA   | 16                 |
| Dust/Asphalt Ratio  | 5                  |
| VFA   | 4                  |
| Ride Smoothness   | 3                  |
| G <sub>mm</sub> , G <sub>se</sub> , N <sub>ini</sub> , N <sub>max</sub> , Film Thickness,<br>Max Spec Gravity, Fractured Face Count,<br>Moisture Content, Hydrated Lime | 1                  |

| Agency         | Laboratory<br>Air Voids | Gradation | Roadway<br>Density | Asphalt<br>Content | VMA |
|----------------|-------------------------|-----------|--------------------|--------------------|-----|
| Alabama        | Х                       | Х         | Х                  | Х                  | Х   |
| Arkansas       | Х                       |           | Х                  | Х                  | Х   |
| California     |                         | Х         |                    | Х                  |     |
| Connecticut    | Х                       | Х         |                    | Х                  | Х   |
| Florida        | Х                       | Х         | Х                  | Х                  |     |
| Georgia        |                         | Х         |                    | Х                  |     |
| Idaho          | Х                       |           |                    |                    | Х   |
| Illinois       | Х                       | Х         | Х                  | Х                  | Х   |
| Iowa           | Х                       | Х         |                    |                    |     |
| Kansas         | Х                       |           | Х                  |                    |     |
| Kentucky       | Х                       |           |                    | Х                  | Х   |
| Maryland       | Х                       | Х         | Х                  | Х                  |     |
| Mississippi    | Х                       | Х         |                    | Х                  | Х   |
| Missouri       | Х                       |           | Х                  | Х                  | Х   |
| Nebraska       | Х                       |           | Х                  |                    | Х   |
| New Mexico     | Х                       | Х         | Х                  |                    | Х   |
| New York       | Х                       |           |                    |                    |     |
| North Carolina | Х                       | Х         | Х                  | Х                  | Х   |
| North Dakota   | Х                       | Х         | Х                  |                    |     |
| Ohio           |                         | Х         |                    | Х                  |     |
| Ontario        | Х                       | Х         | Х                  | Х                  | Х   |
| Oklahoma       | Х                       | Х         | Х                  | Х                  |     |
| South Carolina | Х                       | Х         | Х                  | Х                  | Х   |
| South Dakota   | Х                       | Х         |                    |                    | Х   |
| Utah           | Х                       | Х         | Х                  | Х                  | Х   |
| Virginia       |                         | Х         | Х                  | Х                  |     |
| WFLHD          | Х                       | Х         | Х                  | Х                  | Х   |
| Wyoming        |                         | Х         | Х                  |                    |     |
| TOTAL          | 23                      | 21        | 18                 | 18                 | 16  |

# Table 3.3. Characteristics for which Each Agency Uses Contractor Tests for Acceptance

**Question 5.** Does your agency have a HMA verification program that is separate from your Independent Assurance sampling and testing program?

A total of 29 agencies responded that they have separate programs for verification and independent assurance testing, while there were 13 that responded saying they did not. The responses of the agencies were divided as shown in Table 3.4.

| Table 3.4. | <b>Responses Regarding Agencies that Use Separate Verification and I</b> | Α |
|------------|--|---|
|            | Programs   |   |

| Use? | No. | Agency   |
|------|-----|--|
| Yes  | 29  | AL, AR, CA, CO, CT, FL, GA, ID, IL, IA, KS, KY, MD, MS, MO, NE, NY, NM, NC, ND, OH, ONT, OK, SC, SD, UT, VA, WFLHD, WY |
| No   | 13  | AK, AZ, DE, LA, ME, MI, MT, NH, NV, NJ, TN, WA, RI   |

**Question 6.** Are the verification tests the same as the acceptance tests?

This question was designed to find out if the agencies used the same tests for verification that the contractors perform for acceptance. There were 25 agencies that use the same tests, with 17 not using the same tests. The responses of the agencies were divided as shown in Table 3.5.

#### Table 3.5. Responses Regarding Agencies that Use the Same Verification and Acceptance Tests

| Use? | No. | Agency   |
|------|-----|--|
| Yes  | 25  | AL, AR, CO, CT, FL, GA, ID, IL, IA, KS, KY, MD, NE, NY, NC, ND, OH, ONT, OK, SC, SD, UT, VA, WFLHD, WY |
| No   | 17  | AK, AZ, CA, DE, LA, ME, MI, MS, MO, MT, NV, NH, NJ, NM, RI, TN, WA                                     |

**Question 7.** What are your sampling locations and frequencies of acceptance and verification sampling and testing?

Question 7 was asked to acquire data on how much testing the agencies do, and also how the data are collected. Each agency has its own set of tests it uses for acceptance, and each agency has a different frequency to take their tests. Each responding agency's frequency is shown in Table 3.6.
| Agency | Test Frequency  |
|--------|---|
| AL     | Core every 3000 feet; other tests every 700 tons.   |
| AR     | Acceptance every 750 tons, verification every 3000 tons.  |
| CA     | Aggregate is sampled from belt or bin. HMA binder content is sampled behind paver.  |
| со     | Location determined by the contractor. Samples were taken from windrow prior to pick-up device. Binder and Density: 1 / 500 tons;<br>Air Voids and VMA: 1 / 1,000 tons.   |
| СТ     | Samples are taken at the plant at a rate of 1 / 500 tons.   |
| FL     | Acceptance tests are done at 1 / 1000 tons, split sample verification samples of 1 in 4 are tested. Independent plant taken at 1 / 4000 tons for binder content, gradation, and air voids.  |
| GA     | 1 / 1000 or 1 / 500 tons–contractor's choice for acceptance.<br>Verification 1 / 4000 tons.   |
| ID     | Acceptance every 750 tons, verification twice per shift.  |
| IL     | From the truck at the HMA plant once in the morning and once in the afternoon.  |
| IA     | Samples taken from behind the paver at 4 locations, 4 / day. DOT takes 1 random test per day for verification.  |
| KS     | Random locations for air voids and density.   |
| кү     | Samples taken from truck at the HMA plant, one per 1 / 1000 tons. DOT verifies at 1 / 4000 tons.  |
| MD     | 1 / 1000 tons, and 5 cores taken for QC, 5 for SHA lab.   |
| MS     | Taken from the truck at the plant based on daily tonnage.   |
| мо     | 1 / 1000 ton sublot.  |
| NE     | Sample taken behind paver 1 / 750 tons, every sample split, used for QC, and one random for verification.   |
| NM     | 1 / 1000 tons for acceptance, 1/3000 tons for verification.   |
| NC     | 1 / 750 tons, and 10% used for verification.  |
| ND     | 4 tests to the contractor's first 10, then 10% afterwards.  |
| SC     | Acceptance of HMA mixture (Binder, AV, VMA) every 500 tons by contractor –<br>Split samples obtained at a minimum of 10%. Random verification samples<br>taken at least 1 per lot. Roadway cores taken by contractor every 1500 feet<br>for Intermediate and every 2000 feet for Surface. |
| SD     | 1 / 5000 tons for verification.   |
| UT     | Behind paver 5 / day.   |
| VA     | 1 / 500 tons for contractor tests and 1 / 2000 tons for verification.   |
| WFLHD  | 1 / 750 tons behind the paver before compaction.  |
| WY     | Aggregate 1 / 1000 tons, cores 1 / 250 tons, volumetrics 1 / 5000 tons.   |

**Question 8.** If you use mix volumetrics for acceptance and verification, do you re-heat the verification samples from ambient room to the proper compaction temperature before testing?

Question 8 takes into consideration only those agencies that use volumetrics for acceptance and verification testing. This is the reason there are only 28 agencies of the 42 in the survey that have a response to this question. The responses of the agencies were divided as shown in Table 3.7.

| Use? | No. | Agency   |
|------|-----|--|
| Yes  | 24  | AR, CA, CO, CT, FL, ID, IL, IA, KS, MD, MS, MO, NE, NM, NY, NC, ND, ONT, OK, SC, UT, VA, WFLHD, WY |
| No   | 4   | AL, GA, KY, OH, SD   |

| Table 3.7. Responses | <b>Regarding State</b> | es that Re-Heat | Samples before | e Testing |
|----------------------|------------------------|-----------------|----------------|-----------|
|----------------------|------------------------|-----------------|----------------|-----------|

**Question 9.** What procedure do you use to compare acceptance test results with your verification test results?

Verification testing is used to ensure the acceptance tests are accurate. Each agency has its own way of comparing the acceptance test results with its verification tests. There were 9 agencies that used some sort of statistical analysis using *F*-tests and *t*-tests to verify the acceptance tests. These agencies include: CO, ID, KS, MD, NM, SD, UT, VA and WFLHD. Kansas currently uses an Excel spreadsheet to perform its *F*-tests and *t*-tests. They use a significance level (alpha value) of 0.01. However, they are considering changing that to 0.025 or 0.05 at the request of FHWA.

Many agencies use some variety of tolerance tables to compare their verification results to the contractor's test results. FL, GA, MS, NY, NC, VA, ND, WY, AR, NE, and KY all use some version of tolerance tables to verify acceptance tests. Some of these agencies' tolerances are displayed in Table 3.8. MO considers the tests verified if the acceptance tests and the verification tests are within two standard deviations of the lot average for acceptance tests. IL does not have a formal procedure for comparing the tests results, but starts an investigation if the tests do not match. IA does a one-to-one comparison for verification and acceptance tests and multiple sample bias.

The tolerances in the table represent the differences between the contractor and agency tests that would cause a test not to be acceptable or would cause a stoppage of production. Other differences may trigger a pay reduction but still allow the material to remain in place.

| State  | Density | Air<br>Voids | AC<br>Content                             | Gradation<br>5/8" or<br>3/8"         | Gradation<br>No. 200                 | VMA  | Bulk<br>Specific<br>Gravity | Max.<br>Specific<br>Gravity |
|--|---------|--------------|---|--------------------------------------|--------------------------------------|------|-----------------------------|-----------------------------|
| AR   | 2.0%    | 1.0%         | 0.30%                                     |                                      |                                      | 1.0% |                             |                             |
| FL   |         |              | 0.55%                                     | 5.5%                                 | 1.5%                                 |      | 0.016                       | 0.022                       |
| GA   |         |              | 0.50%                                     | 4.0%                                 | 2.0%                                 |      |                             |                             |
| MS   |         |              | 0.40%                                     | 6.0%                                 | 2.0%                                 |      | 0.030                       | 0.020                       |
| NE   |         | 0.5%         | 0.50%                                     | 5.0%                                 |                                      | 0.5% |                             |                             |
| NY   |         |              |   | 5.0%                                 |                                      |      | 0.200                       | 0.011                       |
| NC   | 2.0%    |              | 0.50%                                     | 5.0%                                 | 2.0%                                 | 1.0% | 0.030                       | 0.020                       |
| ND   |         |              |   | 7.0%                                 | 2.5%                                 |      | 0.040                       | 0.035                       |
| VA<br>1 test<br>2 tests<br>3 tests<br>4 tests<br>8 tests |         |              | 0.60%<br>0.43%<br>0.33%<br>0.30%<br>0.21% | 8.0%<br>5.7%<br>4.4%<br>4.0%<br>2.8% | 2.0%<br>1.4%<br>1.1%<br>1.0%<br>0.7% |      |                             |                             |

Table 3.8. Tolerances Used to Compare Acceptance and Verification Tests

# Conclusion

This summary condenses all of the data that were gathered from the survey responses and the specification search. This summary is designed to give an overview of what agencies are doing with regard to using contractor tests for acceptance of asphalt pavements. While each agency has its own procedures, trends can be seen in the responses.

A majority of the responding agencies (28 of 42, or 67%) in some way incorporate contractor test results into the acceptance decision. Only 9 of these 28 agencies use F-tests and t-tests when comparing contractor acceptance tests with the agency's verification tests.

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# CHAPTER 4 — INTERVIEW RESULTS

## Background

This chapter summarizes and discusses the results of in-person interviews that were conducted with STDs. The intent of the interviews was to obtain more in-depth information from STDs that use contractor test results in the acceptance decision. Before each interview, the STD was provided a list of questions that the Committee wanted to have answered.

### Interviews

After obtaining approval from the Committee chair, it was decided that the initial interviews would be conducted with the neighboring states of Georgia and North Carolina since many SC contractors also work in these states. This also allowed the researchers to determine the effectiveness of the in-person interviews while keeping travel costs to a minimum. GDOT was interviewed on August 29, 2008 and NC was interviewed on September 15, 2008. Summaries of the results of these interviews are presented in Exhibits 4.1 and 4.2, respectively.

# Change to the Interview Process

The researchers experienced difficulties in contacting states that were willing to meet for interviews and in finding mutually agreeable dates for interviews. As a result, based on the initial in-person interviews, and in an effort to make scheduling easier, at the March 12, 2009 meeting of the Committee the researchers proposed that future interviews be conducted as telephone interviews. The Committee agreed to this change in the interview process. The researchers scheduled a telephone interview with the Tennessee DOT (TDOT). The results of this interview are presented in Exhibit 4.3.

Due to the long amount of time that it took to find a time that the three TDOT interviewees could participate in a conference call, and based on the information that had been obtained from the three interviews that were conducted, it was decided that additional "formal" interviews would not be the most efficient method for gathering information. Rather, the graduate research assistant contacted individual STDs on a one-to-one basis to seek additional information and clarifications as needed.

## Conclusion

Due to the increasing workloads experienced by STDs, it was very difficult and time consuming to set up formal interviews. The interviews that were conducted did not yield significantly more information than could be obtained from the surveys and from the specifications and procedures manuals of the various STDs. It was therefore concluded that eliminating the formal interviews in favor of telephone calls and emails to solicit additional information on an as needed basis was a better approach than continuing with formal STD interviews.

#### Summary of Interview Questions: Georgia DOT, August 29, 2008

#### Why did you decide to use contractor tests for acceptance?

FHWA encouraged it, and it saves staffing requirements for the DOT.

#### Have there been any complications using the contractor tests for acceptance?

When the DOT people were not present there was a problem with getting lime into some of the mixes. Since lime is not an acceptance material it was not caught in the IA testing.

# How did you come up with the allowable differences between the department and contractor acceptance tests?

#### Was there any research done to come up with these numbers?

They are not sure; they have been trying to figure it out. They are considering a research project to revisit them.

#### Is there any statistical backing for these numbers?

Not sure.

#### Have you considered using statistical comparison (F- or t-tests) for quality assurance?

They are reviewing using F- and t-tests for quality assurance. The problem is they are not getting enough information for statistical comparison. They have enough information from the contractor side, but only having 2 QA tests per week is not enough for a statistical comparison. This results in about a 1 to 10 ratio of DOT to contractor tests.

# Has using contractor tests for acceptance been able to maintain the same level of quality of the pavements?

See above referenced comments about the lime not in mix. It is also hard to tell about the quality since the pavements have yet to make it to their expected design life.

#### Why did you choose the HMA properties that you have for quality assurance testing?

They feel like gradation and AC Content are the most important aspects to the QA of HMA. These are used for the payment decision. The 3/8" sieve, No.4, and No. 8 sieves are also used for surface courses.

Other tests are used for QC and can shut down the plant, but are not used in the payment decision.

#### How did you decide on the acceptance characteristics?

Because they have always used these characteristics, i.e., "if it ain't broke don't fix it." They also perform field verifications of the mix design during construction.

#### Other Information:

They use both ignition oven and extraction for AC content. This has caused problems because there are differences in the results obtained by the two methods, and the individual apparatus.

They have 2 levels: (1) testing twice per week to take samples and (2) "inspectors" that rotate around the state and visit plants and constructions sites.

#### Exhibit 4.1. Summary of In-Person Interview with Georgia DOT

#### Summary of Interview Questions: North Carolina DOT, September 15, 2008

#### Why did you decide to use contractor tests for acceptance?

Began QC/QA in Mid 90's. It was mostly about manpower issues.

#### Have there been any complications using the contractor tests for acceptance?

They have seen good contractors who take more care in the product, realizing the way to make profit is not by trying to stay on the edge of acceptable limits but by having a better product. The contractors understand more about their product now that they do the testing. They had some fraud issues, which resulted in some technician certifications being revoked.

# How did you come up with the allowable differences between the department and contractor acceptance tests?

These were based off recommendations from their consultant (not D2S Limits) and some are tighter than D2S. They are reworking most of these to get them more in line with AASHTO/ASTM D2S limits.

On independent samples they have used the same allowable limits for years. For 2008 they are going to evaluate these limits.

They were doing a minimum of 10% split and 5% independent verification testing and switched after their stewardship review. They now do 10% independent verification testing and 5% split.

They have a referee system with splits for QC, QA, and 1 held by QA for referee check by central lab if needed.

#### Was there any research done to come up with these numbers?

Not sure.

#### Is there any statistical backing for these numbers?

Not that they are aware of.

#### Have you considered using statistical comparison (F- or t-tests) for quality assurance?

Yes, but they have limitations on capturing enough data for F- and t-tests. They do not have a way to separate QC/QA data from data input into the system to be used for F- and t-tests. They are thinking about adding a new part to the in-house developed software to separate out data and allow for F- and t-tests.

# Has using contractor tests for acceptance been able to maintain the same level of quality of the pavements?

When letting volume was higher and greater amounts of outside help were hired it was down some because of how fast paced things were going. Overall, it is about the same, but the last few years it seems as though some of the attention to detail has been lost. Starting in 2005 they started to evaluate individual technicians as well.

*(continued)* 

#### Exhibit 4.2. Summary of In-Person Interview with North Carolina DOT

# Have there been any problems with allowing contractors to use cores or nuclear density tests for density? Was there any discussion on the accuracy difference between using cores versus using nuclear density gauges?

Nuclear density is correlated to a percentage of control strip density, on which cores have been taken and tested. Core jobs use 5 random tests per lot as does nuclear testing, but nuclear testing takes 2 readings per spot to reduce some of the variability. East of Raleigh mostly utilizes nuclear control. West of Raleigh does not want to use nuclear control.

#### **Other Information:**

Use 250 ton lots sampled from truck at plant.

AC content (ignition oven) and Gradation (#8 and #200) are used for payment.

They use bulk specific gravity, Rice gravity, and check volumetrics as a percentage of MTD. Run recommended Superpave gyrations going toward Table 9-9 levels.

Verification Samples (independent samples taken randomly by DOT forces): they are based on what they call Retest Limits. If the verification sample and the most recent QC sample from the same lot are outside of the Retest Limits, an investigation is initiated.

Pay Factors: These are based on a straight-line drop from 100% down to 50%. Anything < 50% is Remove and Replace.

#### Exhibit 4.2. Summary of In-Person Interview with North Carolina DOT (continued)

| Summary of Interview Questions: Tennessee DOT   |
|---|
| Why did you decide against using contractor tests for acceptance?   |
| They have always had a strong asphalt interest. They have been fortunate to have their own people be able to do the testing.  |
| Are there any drawbacks to the department having to do all of the testing itself?   |
| Personnel is now a tremendous problem.  |
| Have you considered the possible cost savings by being able to reduce in house testing?   |
| They would rather do what they can themselves than to use contractor tests for acceptance.<br>Nobody really wants to switch. They now use certified producers for Liquid AC and it has cut<br>down on their testing. They still pull assurance tests though.  |
| What HMA properties do you test for acceptance, and why did you choose those properties?  |
| Pay factor sieves: 3/8", #4, #8, #16, #30, #50, #100, #200. Pay tables single or double test. Use absolute average deviation (keep contractor from compensating up or down). The majority of tests are taken from the truck. For AC content the majority use vacuum method, but ignition oven is also accepted. Their tests are done in the contractors' labs so it depends on which equipment the contractor has. Sublots 1< 500 tons, 2: 500–1000 tons, 3: 1500–3000 tons, 4: 3000–4500 tons. |
| For Density they use Nuclear Gauges for time purposes. This allows for instant feedback (contractor can keep rolling). Density tested 1 test/sublot.  |
| Is the contractor required to do any Quality Control testing? If so, what QC tests are required and what are the frequencies of these tests?  |
| They recommend tests for QC. They usually recommend the same frequencies that TDOT uses. Contractor Quality plans are submitted in the pre-construction meeting.  |

# Exhibit 4.3. Summary of Telephone Interview with Tennessee DOT

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# CHAPTER 5 — ANALYSIS OF ACCEPTANCE TEST RESULTS

# Background

This chapter discusses the analyses that were conducted to determine appropriate standard deviation values to represent the variability of each of the acceptance characteristics used by SCDOT. These include asphalt content, air voids, and VMA of plant samples, as well as core densities from the in-place pavement. These variabilities are necessary to evaluate the appropriateness of the existing specification limits. They can also be used when evaluating the risks of various comparison and verification procedures.

# Data Obtained for Analysis

Test result data from SCDOT projects were obtained from SCDOT. The data were divided into two categories:

- Density acceptance test results.
- Plant acceptance test results, including AC, AV, and VMA.

All of the density acceptance test data that were provided are included in Appendix A. A total of 1,260 density test results were provided. In all, density data were provided from 22 different projects, with some projects having multiple HMA mixes involved.

All of the plant acceptance test data that were provided are included in Appendix A. A total of 1,775 asphalt content tests were provided from 30 different projects, with some projects having multiple HMA mixes involved. Since no voids testing was done on Base course mixes, open graded friction course (OGFC) mixes, or Surface E mixes, there were only 1,343 air voids and VMA tests provided.

Each project is identified with a unique number, ranging from P01 to P36. Each of these numbered projects corresponds with a unique SCDOT project file number. Each job mix formula (JMF) is identified with a unique number, ranging from J01 to J83.

# Data Analyses

A number of different analyses were conducted on the test result data that were obtained from SCDOT. Some of the analyses conducted included analysis of variance (ANOVA) to determine if differences in means existed among the various subsets of the data. These subsets included comparing individual lots within a project, individual projects within a mix type, individual mix types within a course, and courses against one another. *F*-tests, Bartlett's tests, and Levene's tests were conducted to make similar comparisons among the variances.

The analyses were conducted separately on the density and plant test data. The density data also had to be divided into two different subsets. This was due to the fact that that there is no formal target value for density, and that there are different specification limits for Interstate and multi-lift paving (Interstate) than for all other paving (Other). Since there was no target value there was no common reference point to which to compare the density results. So, the density analyses were conducted treating the Interstate and Other as different populations.

Unlike density, the plant test data had specific target values. It was not possible to compare directly the actual test results since each project and each mix design had its own set of target values. It was possible, however, to normalize the data by considering the asphalt content (AC), air voids (AV), and VMA values as differences from their target values. This made it possible to make comparisons among the various lots, mix designs, projects, mix types, and courses that could not be done on the actual test values.

Since they were treated differently, the results of the analyses on the density and plant tests are presented in separate chapters. One of the most important goals of the analyses was to determine appropriate standard deviation values to represent the variability for density, AC, AV, and VMA. Before presenting the results of the data analyses it is important to present some general principles associated with selecting these typical project variabilities.

## Selecting a "Typical" Variability

The first question to be answered in the analyses was "What variability will be used for the typical variability on which to base the specification limits?"

**Determining the Project Variability.** The first, and perhaps most important, issue is to develop a value for project variability that is consistent with the way in which a lot is defined under the acceptance plan. Since the SCDOT specification is based on lot-by-lot acceptance, the variability that is used to evaluate the specification limits must be that which is appropriate for a typical lot. To determine this, the individual standard deviation values for each lot must be calculated and then these lot standard deviations are "averaged" in some way to get a typical "within-lot" standard deviation for the process.

This within-lot population standard deviation can be estimated by a function of the *average* sample standard deviation. This is obtained by averaging the individual standard deviations calculated from each of the lots on the project, with each lot having some size, n. There is, unfortunately, a slight problem involved when working with the usual estimator of  $\sigma$ .

If  $\sigma^2$  is the unknown variance of a probability distribution, then the *sample* variance is an unbiased estimator of  $\sigma^2$  (see equation 5.1).

$$s^{2} = \frac{\sum_{i=1}^{n} \left(X_{i} - \overline{X}\right)^{2}}{n-1}$$
(5.1)

Where

 $s^2$ 

= the sample variance,

 $X_i$  = the individual data values in the sample,

 $\overline{X}$  = the sample mean,

n = the number of data values in each sample.

However, *s*, the sample standard deviation which is the square root of the variance, is *not* an unbiased estimator of  $\sigma$ . If the underlying distribution is normal, then *s* actually estimates  $c_4 \sigma$ , where  $c_4$  is a constant that depends on the sample size *n*. This constant is tabulated in many text books on statistical quality control and may be calculated using equation 5.2.

$$c_{4} = \sqrt{\frac{2}{n-1}} \frac{\left(\frac{n}{2} - 1\right)!}{\left(\frac{n-1}{2} - 1\right)!}$$
(5.2)

To compute this we need a *non-integer factorial*, which is defined for n/2 as shown in equation 5.3.

$$\left(\frac{n}{2}\right)! = \left(\frac{n}{2}\right)\left(\frac{n}{2} - 1\right)\left(\frac{n}{2} - 2\right)\cdots\left(\frac{1}{2}\right)\sqrt{\pi}$$
(5.3)

Since it depends only on *n*, values of  $c_4$  are readily available in tables. Table 5.1 shows  $c_4$  values for various values of *n*.

So the *mean* or expected value of the sample standard deviation is  $\overline{s} = c_4 \sigma$ . In other words, the population standard deviation,  $\sigma$ , is estimated by  $\overline{s}/c_4$ . For equal sample sizes, equation 5.4 is used to calculate  $\overline{s}$ . In the equation, k = the number of sample standard deviations used (i.e., the number of lots) to calculate  $\overline{s}$ .

$$\overline{s} = \frac{s_1 + s_2 + \dots + s_k}{k}.$$
(5.4)

The estimated population standard deviation,  $\hat{\sigma}$ , is then calculated using equation 5.5 with the single  $c_4$  value for the equal sample size.

$$\hat{\sigma} = \frac{\overline{s}}{c_4} \tag{5.5}$$

If the sample sizes are not equal, then compute  $\hat{\sigma}$  with equation 5.6 using the  $c_4$  values for the appropriate sample sizes. In the equation, k = the number of sample standard deviations used (i.e., the number of lots) to calculate  $\overline{s}$ .

$$\hat{\sigma} = \frac{\frac{s_1}{c_{4_1}} + \frac{s_2}{c_{4_2}} + \dots + \frac{s_k}{c_{4_k}}}{k}$$
(5.6)

| Table 5.1. $c_4$ ractors for various bample bizes, r | Table | 5.1. <i>c</i> ₄ | <b>Factors for</b> | Various | Sample | Sizes, | n |
|--|-------|-----------------|--------------------|---------|--------|--------|---|
|--|-------|-----------------|--------------------|---------|--------|--------|---|

| Sample<br>Size, <i>n</i> | <i>c</i> <sub>4</sub> |
|--------------------------|-----------------------|
| 2                        | 0.7979                |
| 3                        | 0.8862                |
| 4                        | 0.9213                |
| 5                        | 0.9400                |
| 6                        | 0.9515                |
| 7                        | 0.9594                |
| 8                        | 0.9650                |
| 9                        | 0.9693                |
| 10                       | 0.9727                |
| 11                       | 0.9754                |
| 12                       | 0.9776                |
| 13                       | 0.9794                |
| 14                       | 0.9810                |
| 15                       | 0.9823                |
| 16                       | 0.9835                |
| 17                       | 0.9845                |
| 18                       | 0.9854                |
| 19                       | 0.9862                |
| 20                       | 0.9869                |
| 21                       | 0.9876                |
| 22                       | 0.9882                |
| 23                       | 0.9887                |
| 24                       | 0.9892                |
| 25                       | 0.9896                |
| Over 25                  | *                     |

\* (4n-4)/(4n-3)

**Target Miss.** The typical standard deviation value that is selected serves as a measure of variability within the process for a typical contractor on a typical project. This standard deviation will be used to help decide upon specification limits for the acceptance plan. Another factor that needs to be considered in addition to this within–process variability is the capability of contractors to center their processes on the target value. This may be an even more difficult task than deciding on a typical within–process standard deviation.

AC, AV, and VMA all have target values about which two-sided specification limits are established. The typical process standard deviation can be used to establish these specification limits. The STD, however, must decide whether or not a typical contractor can be expected to always be able to center its process exactly on the target value. If the STD believes this to be possible, then the typical process standard deviation that was developed from the individual project values can be used when setting the specification limits. If, on the other hand, the STD believes that a typical contractor's process mean may vary somewhat about the target value, then it will be necessary to consider this fact when developing specification limits.

What is being considered here is not the case where a contractor, for whatever reason, chooses to intentionally center its process at some point other than the target value. If a contractor chooses to do this, then the contractor must bear any potential acceptance risks associated with its decision. On the other hand, failure to consider that current technology may not be adequate to allow the contractor to always hit the target with all of its processes places a risk on the contractor.

The ideal way to address the issue of "target miss," is to determine how variable the actual process means are about the target value. This variability regarding where the process will be centered, call it "process center variability," can then be combined with the previously determined typical within–process variability to obtain the correct standard deviation value for use in establishing specification limits.

The "process center variability" and the "within–process variability" can be combined simply by adding their associated variances, NOT their standard deviations. This assumes that the amount of process variability is independent of where the process is centered; an assumption that seems reasonable, particularly as long as the target miss is not very large. Note that it is NOT correct to add the two standard deviations. The two variances must be added to get a combined variance. The square root of this combined variance can then be used as an estimate of the standard deviation value.

It is difficult to answer this "target miss" question from project data because the STD never knows with certainty where the contractor intended to center its process. A contractor with particularly low variability could, for a number of reasons, choose to center its process at a point other than the target value and still plan to meet the specification requirements based on its low variability. It will also not be possible to determine from project data whether or not the contractor's process mean was constant throughout the project or whether for any of a number of reasons it was changed during the course of the project. Any "target miss" analysis will therefore require some assumptions.

If the agency assumes that there is a constant process throughout a project, then the mean value of all of the individual lot means on the project can be used as an estimate of where the process was centered for the project. The agency could then obtain a large number of project "target misses" and analyze these to determine the variability associated with missing the target value. One potential problem with this approach is that the project data that were obtained do not have a large number of lots for many of the projects. This, therefore, makes it difficult to obtain a good estimate of where the process was centered.

If the STD does not believe that the contractor's process is constant throughout the life of a project, as would typically be the case when the agency has decided to use lot–by–lot acceptance, then there is no way to know how much of the lot–to–lot variation in sample means is from the natural variation of the sampling process and how much is due to misses, changes, or adjustments in the contractor's target mean during the project.

One possibility might be to calculate a standard deviation based on combining all of the project data into one data set. While this is not recommended as the best way to establish a typical within–process standard deviation to use with lot–by–lot acceptance, this approach will

provide a larger standard deviation value that includes the lot-to-lot variation among the individual lot means. A decision to use this approach assumes that any "target miss" variation within the project will be accounted for when all the test results are combined. The various project standard deviations could then be used to arrive at a typical process standard deviation that attempts to include both the "within-process" and the possible "target miss" variability.

**Determining the Typical Process Variability.** Once the project variability data are available, a decision must be made regarding what variability to use as the "typical" process variability. This typical variability can then be used to establish specification limits. There is no single "correct" way to decide upon the typical variability to use.

Suppose that an STD has collected data from a number of past projects that it considered acceptable. The STD could decide to select the smallest project standard deviation as the "typical" process standard deviation value (measure of process variability) since this value is "capable" of being achieved. On the other hand, the STD could select the largest value since this value was obtained on a project that the STD had apparently considered acceptable. It is probably not appropriate to select either the best (smallest) variability or the worst (largest) variability as the "typical" variability. An STD cannot reduce variability by simply specifying it, particularly if it has been shown that contractors, in general, have not been able consistently to meet that variability value. It is probably also not a good practice to base acceptance plan decisions on the worst contractor results.

Therefore, the STD would probably wish to select the typical process variability value based on consideration of all the past project data rather than just a single best or worst project. The STD might order the standard deviation values from smallest to largest and then subjectively decide what value to select as the typical process variability. This decision might be based on selecting a value that was attained on two-thirds, or three-fourths of the projects. This is a judgment decision, and many defensible subjective choices are possible.

# CHAPTER 6 — RESULTS OF DENSITY ACCEPTANCE TEST ANALYSES

### Background

This chapter summarizes and discusses the results of analyses to determine appropriate standard deviation values to represent the variability for density. This variability is necessary to evaluate the appropriateness of the existing specification limits. It can also be used when evaluating the risks of various comparison and verification procedures.

## **Data Obtained for Analysis**

All of the density acceptance test data that were provided are included in Appendix A. A total of 1,260 density test results were provided. In all, density data were provided from 22 different projects, with some projects having multiple HMA mixes involved. The numbers of density tests for the various projects and JMF mix designs are presented in Tables 6.1-6.4.

In the tables, each project is identified with a unique number, ranging from P01 to P36. Each of these numbered projects corresponds with a unique SCDOT project file number. Each job mix formula (JMF) is identified with a unique number, ranging from J01 to J83.

The density data had to be divided into two different subsets. This was due to the facts that that there is no formal target value for density and that there were different specification limits for multi-lane and Interstate highways (Interstate) than for non-multi-lane and non-Interstate highways (Other). Since there was no target value there was no common reference point to which to compare the density results. So, the density analyses were conducted treating Interstate projects and Other projects as different populations.

| Mix Type       | Project | JMF | Lots in<br>JMF | Tests in<br>JMF | Lots on<br>Project | Tests on<br>Project |
|----------------|---------|-----|----------------|-----------------|--------------------|---------------------|
| Intermediate B | P01     | J23 | 2              | 8               | 2                  | 8                   |
|                | P03     | J04 | 5              | 30              | 5                  | 30                  |
|                | P36     | J09 | 5              | 21              | 5                  | 21                  |
| Total          |         |     | 12             | 59              | 12                 | 59                  |

| Mix Type   | Project | JMF | Lots in<br>JMF | Tests in<br>JMF | Lots on<br>Project | Tests on<br>Project |
|------------|---------|-----|----------------|-----------------|--------------------|---------------------|
| Surface 1  | P06     | J26 | 1              | 14              | 1                  | 14                  |
| Surface 1D | P06     | J24 | 5              | 25              | 5                  | 25                  |
| Surface 1P | P04     | J14 | 5              | 36              | 5                  | 36                  |
| Surface IK | P08     | J11 | 1              | 8               | 1                  | 8                   |
|            | P27     | J55 | 4              | 24              | 11                 | 57                  |
| Surface B  | P27     | J70 | 7              | 33              | 11                 | 57                  |
| Surface B  | P30     | J65 | 2              | 8               | 2                  | 8                   |
|            | P31     | J71 | 2              | 8               | 2                  | 8                   |
|            | P13     | J03 | 1              | 9               | 1                  | 9                   |
|            | P14     | J16 | 6              | 38              | 6                  | 38                  |
|            | P15     | J44 | 5              | 18              | 5                  | 18                  |
|            | P16     | J20 | 3              | 12              | 3                  | 12                  |
| Surface C  | P18     | J48 | 3              | 18              | 3                  | 18                  |
|            | P20     | J50 | 7              | 67              | 7                  | 67                  |
|            | P24     | J56 | 7              | 56              | 7                  | 56                  |
|            | P26     | J59 | 8              | 55              | 8                  | 55                  |
|            | P28     | J39 | 4              | 28              | 4                  | 28                  |
| Total      |         |     | 71             | 457             | 71                 | 457                 |

Table 6.2. Summary of Density Data for Surface Course on Other Projects

#### Table 6.3. Summary of Density Data for Intermediate Course on Interstate Projects

| Mix Type       | Project | JMF | Lots in<br>JMF | Tests in<br>JMF | Lots on<br>Project | Tests on<br>Project |
|----------------|---------|-----|----------------|-----------------|--------------------|---------------------|
| Binder 1       | P01     | J02 | 4              | 22              | 4                  | 22                  |
| Intermediate B | P01     | J10 | 7              | 30              | 7                  | 30                  |
|                | P23     | J33 | 4              | 16              | 4                  | 16                  |
|                | P32     | J76 | 13             | 105             | 13                 | 105                 |
|                | P33     | J73 | 8              | 56              | 8                  | 56                  |
| Total          |         |     | 36             | 229             | 36                 | 229                 |

| Міх Туре   | Project     | JMF | Lots in<br>JMF | Tests in<br>JMF | Lots on<br>Project | Tests on<br>Project |  |
|------------|-------------|-----|----------------|-----------------|--------------------|---------------------|--|
| Surface 1C | P01         | J07 | 4              | 22              | 4                  | 22                  |  |
|            | P26         | J62 | 9              | 42              | 25                 | 122                 |  |
|            | F20         | J69 | 16             | 81              | 25                 | 125                 |  |
| Surface A  | <b>D</b> 32 | J74 | 1              | 6               | 26                 | 172                 |  |
| Surface A  | F JZ        | J79 | 25             | 166             | 20                 |                     |  |
|            | P33         | J77 | 6              | 40              | 6                  | 40                  |  |
|            | P34         | J62 | 4              | 25              | 4                  | 25                  |  |
|            | P01         | J07 | 5              | 20              | 5                  | 20                  |  |
| Surface B  | P03         | J15 | 5              | 25              | 5                  | 25                  |  |
| Surface B  | P23         | J63 | 6              | 18              | 6                  | 18                  |  |
|            | P32         | J72 | 8              | 70              | 8                  | 70                  |  |
| Total      |             |     | 89             | 515             | 89                 | 515                 |  |

# Density Test Data Analyses

As noted above, the density tests were divided into two different subsets since the Interstate and Other projects had different specification limits. The Interstate projects had lower and upper specification limits of 92.2 and 96.0, respectively. Other projects had the same upper limit, but had a lower limit of 91.2. The specifications listed target values of 94.0 for Interstate and 93.0 for Other paving.

However, since these "target" values are not in the centers of their respective specification limits, there is no real benefit to the contractor to attempt to hit these targets with its process. The contractor maximizes it chances of meeting the PWL requirement by aiming for the center of the specification limits. This allows for the largest standard deviation that can be obtained while still meeting the specification requirements for full payment. So, even though the specification lists "target" values, in reality the "real" target values become the midpoint between the lower and upper specification limits. Therefore, these target values were not considered when performing analyses on the density test results.

**Interstate vs. Other Paving.** To determine if the difference in specification limits led to differences in the densities achieved on projects, the mean and variance of the Interstate projects were compared statistically with those for the Other projects. These comparisons were made separately for Intermediate and Surface mixes. Table 6.5 presents the results of these comparisons.

# Table 6.5. Summary of Density Comparisons between Interstate and Other Paving for Intermediate and Surface Mixes

| Course       | Paving<br>Type | No. of<br>Projects | No. of<br>Tests | Mean  | P-value* | St Dev | P-value* |
|--------------|----------------|--------------------|-----------------|-------|----------|--------|----------|
|              | Other          | 3                  | 59              | 93.39 | 0 105    | 1.420  | 0.094    |
| Intermediate | Interstate     | 4                  | 229             | 93.15 | 0.195    | 1.204  |          |
| Surface      | Other          | 15                 | 457             | 92.02 | 0.000    | 1.695  | 0.000    |
|              | Interstate     | 7                  | 515             | 92.97 | 0.000    | 1.131  |          |

\* Values in bold are statistically significantly different at the  $\alpha = 0.05$  level.

The results in Table 6.5 show that the density Surface course results definitely had a higher mean and lower standard deviation for Interstate paving than for Other paving. For Intermediate course, the differences were not significant at the 0.05 level.

Table 6.6 shows the same mean and standard deviation values as in Table 6.5, but compares differences between Intermediate and Surface courses within Interstate paving and Other paving. For both Interstate and Other paving, the Intermediate course had higher mean values than the Surface course. However, the standard deviations were not significantly different at the 0.05 level for either type of paving.

| Table 6.6. Summary of Density Comparisons between Intermediate and Surface Mixes |
|--|
| for Interstate and Other Paving Projects   |

| Paving<br>Type | Course       | No. of<br>Projects | No. of<br>Tests | Mean  | P-value* | St Dev | P-value* |
|----------------|--------------|--------------------|-----------------|-------|----------|--------|----------|
| Interatora     | Intermediate | 4                  | 229             | 93.15 | 0.042    | 1.204  | 0.256    |
| Interstate     | Surface      | 7                  | 515             | 92.97 | 0.043    | 1.131  |          |
| Other          | Intermediate | 3                  | 59              | 93.39 | 0.000    | 1.420  | 0.096    |
|                | Surface      | 15                 | 457             | 92.02 | 0.000    | 1.695  |          |

\* Values in bold are statistically significantly different at the  $\alpha = 0.05$  level.

**Comparing Mix Types within Course.** Table 6.6 shows that it was not possible to declare a difference in variability between Intermediate and Surface course mixes. This supports an argument that there is not a need to have wider or narrower specification tolerances for the two courses. The next question to consider is whether it is appropriate to use the same specification tolerances for all Intermediate course mixes and for all Surface course mixes. When establishing the allowable tolerances it is the standard deviation that is most important. There were only two types of Intermediate course, Binder 1 and Intermediate B, for which data were provided. Since 266 out of 288 data values were Intermediate B, no comparison was made for Intermediate course.

Table 6.7 shows the results of comparisons among the density variabilities for the different types of Surface course mixes. The results show that the standard deviation values are definitely not the same for all Surface mix types. However, there are so few projects and total tests available for some of the mix types that it is difficult to consider these results conclusive.

**Caveat.** None of the standard deviation values shown in Tables 6.5-6.7 are the appropriate standard deviation to use to represent the process standard deviation for density. These calculations were done simply for exploratory purposes. Aggregating the data as in these tables is not appropriate for establishing specification limits since the specification limits are based on lot-by-lot acceptance, or at least on acceptance of a project.

**Typical Variability Values for Density.** As noted above, since the SCDOT specification is based on lot-by-lot acceptance, the variability that is used to evaluate the specification limits must be that which is appropriate for a typical lot. To determine this, the individual standard deviation values for each lot were calculated and then these lot standard deviations were averaged to get the "within-lot" standard deviation for each project. This was done by using the square root of equation 6.1 to calculate the standard deviation for each lot and then using equation 6.6 to calculate the unbiased estimate for the lot population standard deviation. This calculation process is illustrated in Exhibit 6.1 for one of the projects for which data were obtained.

| Mix<br>Type | No. of<br>Projects | No. of<br>Tests | St Dev | P-value* |
|-------------|--------------------|-----------------|--------|----------|
| Surface 1   | 1                  | 14              | 1.159  |          |
| Surface 1C  | 1                  | 22              | 0.792  |          |
| Surface 1D  | 1                  | 25              | 1.733  |          |
| Surface 1R  | 2                  | 44              | 1.339  | 0000     |
| Surface A   | 4                  | 360             | 1.222  |          |
| Surface B   | 7                  | 206             | 1.029  |          |
| Surface C   | 9                  | 301             | 1.438  |          |

Table 6.7. Summary of Density Variability Comparisons among Surface Mixes

\* Values in bold are statistically significantly different at the  $\alpha = 0.05$  level.



# Exhibit 6.1. Example of Calculating Unbiased Std Dev for Project P27, JMF J55

The data in Exhibit 6.1 are for Surface B using JMF J55 on project P27. There were 4 lots with differing sample sizes of 5, 6, and 7. The mean and standard deviation (calculated using equation 6.1) are shown for each lot. Then, each lot standard deviation is divided by the  $c_4$  factor corresponding to the lot sample size to get the unbiased estimate. Finally, the four unbiased lot standard deviations are averaged to arrive at the within-lot standard deviation for the project. As noted above, this within-lot standard deviation does not take into consideration any target miss variability that may be present.

To provide the option to consider using the total project as the payment lot, the total project standard deviation was also calculated for each project. This was done by using the square root of equation 6.1 to calculate a single standard deviation that combines all of the test results on the project. As noted above, this "project" standard deviation could also be used as one way of trying to incorporate any target miss variability that might be present in the contractor's process.

Appendix B includes calculations similar to those in Exhibit 6.1 for each project for which density data were obtained. These calculations were used to arrive at the project standard deviations that were used to establish the typical process variability for density.

**Projects with Multiple JMFs.** Before compiling all of the within-lot and project variabilities, a decision had to be made regarding how to deal with projects on which more than one JMF was used for the same mix type and course. Should each JMF be treated as a separate project, or should the multiple JMF results be combined together as one project? To help make this decision, the projects with multiple JMFs were examined. Table 6.8 shows the projects (extracted from Tables 6.1-6.4) that had multiple JMFs for the same mix type.

| Міх Туре  | Project | JMF | Lots in<br>JMF | Tests in<br>JMF | Lots on<br>Project | Tests on<br>Project |
|-----------|---------|-----|----------------|-----------------|--------------------|---------------------|
| Surface A | DOG     | J62 | 9              | 42              | 25                 | 123                 |
|           | F20     | J69 | 16             | 81              | 25                 |                     |
|           | P32     | J74 | 1              | 6               | 26                 | 172                 |
|           |         | J79 | 25             | 166             | 20                 |                     |
| Surface B | P27     | J55 | 4              | 24              | 11                 | 57                  |
|           |         | J70 | 7              | 33              |                    | 57                  |

Table 6.8. Projects with More than One JMF for the Same Mix Type

For each of the projects in Table 6.8 comparisons were made between the means and variances of the two JMFs on the project. The results of these comparisons are shown in Table 6.9.

Table 6.9. Summary of Density Comparisons for Projects with Multiple JMFs

| Project     | JMF | No. of<br>Lots | No. of<br>Tests | Mean  | P-value* | St Dev | P-value* |
|-------------|-----|----------------|-----------------|-------|----------|--------|----------|
| D26         | J62 | 9              | 42              | 92.85 | 0.026    | 1.358  | 0.362    |
| P20         | J69 | 16             | 81              | 93.39 | 0.020    | 1.206  |          |
| <b>D</b> 22 | J74 | 1              | 6               | 93.20 | 0.075    | 1.348  | 0.149    |
| P32         | J79 | 25             | 166             | 92.77 | 0.275    | 0.838  |          |
| P27         | J55 | 4              | 24              | 92.29 | 0.000    | 0.667  | 0.034    |
|             | J70 | 7              | 33              | 92.95 | 0.009    | 1.028  |          |

\* Values in bold are statistically significantly different at the  $\alpha = 0.05$  level.

Since the primary goal was to determine the within-lot standard deviation, the fact that the means are different for two of the projects is not a particular issue. For project P27, however, the different standard deviation values will lead to an averaged result that may not represent either value. Also, in the project data a new lot was established in nearly every case that the JMF changed. This would argue in favor of treating the JMFs as separate projects when determining the within-lot standard deviations.

However, if a total project is being used as the payment lot, then the data from the two JMFs would be combined when calculating the standard deviation to use for payment determination. This would argue in favor of combining the separate JMFs into a single project. For consistency in presentation and in comparing results, it was decided to treat the separate JMFs as separate projects when calculating standard deviations and when presenting the results.

# **Determining the Typical Process Variability for Density**

Table 6.10 shows the standard deviation results for density for all projects for which data were obtained. The projects are sorted by mix type. The "Lot" standard deviation is the average of the unbiased standard deviation estimates for each lot on the project. The "Project" standard deviation is the standard deviation of all the individual test results for the total project. The table also shows the total number of lots and tests for each project, the mean for all tests on the project, and the mean of the individual project lot means.

**Intermediate vs. Surface Course.** One thing to consider from the results in Table 6.10 was whether to treat the Intermediate course results separate from the Surface course results or to combine them. By observation, the standard deviation values for the Intermediate course projects are in the same range as those for the Surface course projects. Also, the Two-Sample Mann-Whitney hypothesis test was used to compare the medians of the Means of Lot Means results for the Intermediate and Surface results. The same test was used to compare the medians of the Lot Standard Deviations. The Mann-Whitney test does not require the data to come from normally distributed populations. It assumes that the populations of interest have the same shape and that the populations are independent. In both cases the Intermediate and Surface results were not significantly different at the 0.05 level of significance. It was therefore decided to combine the two sets of data for further evaluations.

**Interstate vs. Other Paving Projects.** Another thing to consider was whether the Interstate and Other projects should be treated separately or combined when deciding upon the process standard deviation. To investigate this, Table 6.11 shows the same standard deviation results from Table 6.10, but sorted into Interstate and Other projects. By observation, the average Lot mean appears to be higher and the average Lot standard deviation appears to be smaller for the Interstate paving projects. It would appear that there is better compaction control on Interstate paving projects than on Other paving projects. The fact that the means are different does not affect the selection of the process standard deviation.

| Nun     | nber   | Total Nu | umber of | Mean of * |           | Std Dev | /iation** | Mix      |
|---------|--------|----------|----------|-----------|-----------|---------|-----------|----------|
| Project | JMF    | Lots     | Tests    | All Tests | Lot Means | Project | Lot       | Туре     |
| P01     | J02    | 4        | 22       | 93.94     | 93.56     | 0.908   | 0.848     | Binder 1 |
| P01     | J10    | 7        | 30       | 92.90     | 92.85     | 0.599   | 0.515     | Inter B  |
| P23     | J33    | 4        | 16       | 91.64     | 91.63     | 1.374   | 1.649     | Inter B  |
| P32     | J76    | 13       | 105      | 93.27     | 93.27     | 1.072   | 1.059     | Inter B  |
| P33     | J73    | 8        | 56       | 93.18     | 93.17     | 1.377   | 1.459     | Inter B  |
| P01     | J23    | 2        | 8        | 93.75     | 93.77     | 1.160   | 1.403     | Interm B |
| P03     | J04    | 5        | 30       | 93.73     | 93.59     | 1.388   | 1.053     | Interm B |
| P36     | J09    | 5        | 21       | 92.76     | 92.83     | 1.439   | 1.524     | Interm B |
| Total/A | verage | 48       | 288      | 93.15     | 93.08     | 1.164   | 1.189     |          |
|         |        |          |          |           |           |         |           |          |
| P01     | J07    | 4        | 22       | 93.26     | 93.24     | 0.801   | 0.543     | Surf 1C  |
| P06     | J26    | 1        | 14       | 90.05     | 90.05     | 1.181   | 1.181     | Surf 1C  |
| P06     | J24    | 5        | 25       | 91.47     | 91.69     | 1.751   | 0.995     | Surf 1D  |
| P04     | J14    | 5        | 36       | 89.77     | 89.80     | 1.312   | 1.262     | Surf 1R  |
| P08     | J11    | 1        | 8        | 88.65     | 88.65     | 1.203   | 1.203     | Surf 1R  |
| P26     | J62    | 9        | 42       | 92.85     | 92.84     | 1.366   | 1.052     | Surf A   |
| P26     | J69    | 16       | 81       | 93.39     | 93.40     | 1.210   | 1.126     | Surf A   |
| P32     | J79    | 24       | 166      | 92.77     | 92.77     | 0.943   | 0.868     | Surf A   |
| P32     | J74    | 1        | 6        | 93.20     | 93.20     | 1.417   | 1.417     | Surf A   |
| P33     | J77    | 6        | 40       | 92.67     | 92.72     | 1.486   | 1.161     | Surf A   |
| P34     | J62    | 4        | 25       | 92.74     | 93.01     | 1.820   | 1.500     | Surf A   |
| P01     | J07    | 5        | 20       | 92.73     | 92.77     | 0.591   | 0.546     | Surf B   |
| P03     | J15    | 5        | 25       | 93.23     | 93.41     | 1.272   | 0.957     | Surf B   |
| P23     | J63    | 6        | 18       | 93.11     | 93.11     | 0.584   | 0.607     | Surf B   |
| P27     | J55    | 4        | 24       | 92.29     | 92.30     | 0.674   | 0.632     | Surf B   |
| P27     | J70    | 7        | 33       | 92.95     | 92.92     | 1.036   | 1.091     | Surf B   |
| P30     | J65    | 2        | 8        | 93.74     | 93.80     | 2.486   | 1.989     | Surf B   |
| P31     | J71    | 2        | 8        | 94.12     | 94.15     | 0.517   | 0.616     | Surf B   |
| P32     | J72    | 8        | 70       | 93.07     | 93.06     | 0.861   | 0.854     | Surf B   |
| P13     | J03    | 1        | 9        | 92.01     | 92.01     | 1.567   | 1.567     | Surf C   |
| P14     | J16    | 6        | 38       | 92.46     | 92.55     | 1.313   | 1.179     | Surf C   |
| P15     | J44    | 5        | 18       | 92.68     | 92.68     | 1.465   | 1.584     | Surf C   |
| P16     | J20    | 3        | 12       | 91.58     | 91.58     | 1.087   | 1.063     | Surf C   |
| P18     | J48    | 3        | 18       | 91.55     | 91.65     | 1.824   | 2.042     | Surf C   |
| P20     | J50    | 7        | 67       | 92.38     | 92.42     | 0.938   | 0.945     | Surf C   |
| P24     | J56    | 7        | 56       | 93.12     | 93.20     | 1.078   | 1.001     | Surf C   |
| P26     | J59    | 7        | 55       | 91.03     | 91.22     | 1.343   | 1.170     | Surf C   |
| P28     | J39    | 4        | 28       | 93.26     | 93.28     | 1.298   | 1.242     | Surf C   |
| Total/A | verage | 158      | 972      | 92.36     | 92.41     | 1.229   | 1.121     |          |

Table 6.10. Summary of Density Test Results for Each Project

\* All Tests: the mean of all individual test results on the project Lot Means: the mean of all the individual lot means on the project

\*\* **Project:** the unbiased standard deviation estimate of all individual test results on the project **Lot:** the average of the unbiased standard deviation estimates for all lots on the project

To further investigate the potential difference in standard deviations, the Two-Sample Mann-Whitney hypothesis test was used to compare the medians of the Lot Standard Deviations results for the Interstate and Other projects. The results were not significantly different at the 0.10 level of significance. The SCDOT will need to decide whether this is sufficient evidence to warrant using different process standard deviations for Interstate and Other projects. For this report, both cases were considered.

The case of combining the Interstate and Other projects was considered first. Table 6.12 shows the same standard deviation results from Table 6.10, but with the projects combined and sorted from the smallest to largest Lot (i.e., within-lot) standard deviations. The projects are listed in increasing order of the Lot standard deviation to facilitate selecting a typical process standard deviation. The table also shows the total number of lots and tests for all density projects, the averages for both the Project standard deviation values and for the Lot standard deviation values.

SCDOT can use Table 6.12 to assist in selecting the "typical" variability to use to establish specification limits. As noted in the discussion above, there is no single "correct" way to establish this value. A subjective decision must be made regarding the standard deviation to select. The percentile values shown in the table should assist in making the decision. To get a "picture" of the results in Table 6.12, Figure 6.1 shows the empirical cumulative distribution function (CDF) for the Lot standard deviation values.

As the reference lines show, there appears to be a natural break point at around a standard deviation of 1.26, which corresponds to approximately the  $72^{nd}$  percentile. This would seem to be a logical choice for the process standard deviation if only one will be selected for both Interstate and Other paving projects.

The case of treating the Interstate and Other paving projects separately can now be considered. Table 6.13 shows the standard deviation results from Table 6.10 that are for the Interstate paving projects. The projects are sorted from the smallest to largest Lot (i.e., within-lot) standard deviations. The table also shows the total number of lots and tests for all density projects, the averages for both the Project standard deviation values and for the Lot standard deviation values, and percentiles based on ranked order for both the Project and Lot standard deviation values. Figure 6.2 shows the empirical CDF for the Lot standard deviation values.

As the reference lines show, there appears to be a natural break point at around a standard deviation of 1.16, which corresponds to approximately the 75<sup>th</sup> percentile. This would seem to be a logical choice for the process standard deviation for Interstate paving projects if they are treated separately from Other paving projects.

| Nun       | nber    | Total Nu | umber of | Mea       | Mean of * |         | viation* | Paving     |
|-----------|---------|----------|----------|-----------|-----------|---------|----------|------------|
| Project   | JMF     | Lots     | Tests    | All Tests | Lot Means | Project | Lot      | Туре       |
| P01       | J02     | 4        | 22       | 93.94     | 93.56     | 0.908   | 0.848    | Interstate |
| P01       | J07     | 4        | 22       | 93.26     | 93.24     | 0.801   | 0.543    | Interstate |
| P01       | J07     | 5        | 20       | 92.73     | 92.77     | 0.591   | 0.546    | Interstate |
| P01       | J10     | 7        | 30       | 92.90     | 92.85     | 0.599   | 0.515    | Interstate |
| P03       | J15     | 5        | 25       | 93.23     | 93.41     | 1.272   | 0.957    | Interstate |
| P23       | J33     | 4        | 16       | 91.64     | 91.63     | 1.374   | 1.649    | Interstate |
| P23       | J63     | 6        | 18       | 93.11     | 93.11     | 0.584   | 0.607    | Interstate |
| P26       | J62     | 9        | 42       | 92.85     | 92.84     | 1.366   | 1.052    | Interstate |
| P26       | J69     | 16       | 81       | 93.39     | 93.40     | 1.210   | 1.126    | Interstate |
| P32       | J72     | 8        | 70       | 93.07     | 93.06     | 0.861   | 0.854    | Interstate |
| P32       | J74     | 1        | 6        | 93.20     | 93.20     | 1.417   | 1.417    | Interstate |
| P32       | J76     | 13       | 105      | 93.27     | 93.27     | 1.072   | 1.059    | Interstate |
| P32       | J79     | 24       | 166      | 92.77     | 92.77     | 0.943   | 0.868    | Interstate |
| P33       | J73     | 8        | 56       | 93.18     | 93.17     | 1.377   | 1.459    | Interstate |
| P33       | J77     | 6        | 40       | 92.67     | 92.72     | 1.486   | 1.161    | Interstate |
| P34       | J62     | 4        | 25       | 92.74     | 93.01     | 1.820   | 1.500    | Interstate |
| Total / A | Average | 124      | 744      | 93.00     | 93.00     | 1.105   | 1.010    | Interstate |
|           |         |          |          |           |           |         |          |            |
| P01       | J23     | 2        | 8        | 93.75     | 93.77     | 1.160   | 1.403    | Other      |
| P03       | J04     | 5        | 30       | 93.73     | 93.59     | 1.388   | 1.053    | Other      |
| P04       | J14     | 5        | 36       | 89.77     | 89.80     | 1.312   | 1.262    | Other      |
| P06       | J24     | 5        | 25       | 91.47     | 91.69     | 1.751   | 0.995    | Other      |
| P06       | J26     | 1        | 14       | 90.05     | 90.05     | 1.181   | 1.181    | Other      |
| P08       | J11     | 1        | 8        | 88.65     | 88.65     | 1.203   | 1.203    | Other      |
| P13       | J03     | 1        | 9        | 92.01     | 92.01     | 1.567   | 1.567    | Other      |
| P14       | J16     | 6        | 38       | 92.46     | 92.55     | 1.313   | 1.179    | Other      |
| P15       | J44     | 5        | 18       | 92.68     | 92.68     | 1.465   | 1.584    | Other      |
| P16       | J20     | 3        | 12       | 91.58     | 91.58     | 1.087   | 1.063    | Other      |
| P18       | J48     | 3        | 18       | 91.55     | 91.65     | 1.824   | 2.042    | Other      |
| P20       | J50     | 7        | 67       | 92.38     | 92.42     | 0.938   | 0.945    | Other      |
| P24       | J56     | 7        | 56       | 93.12     | 93.20     | 1.078   | 1.001    | Other      |
| P26       | J59     | 7        | 55       | 91.03     | 91.22     | 1.343   | 1.170    | Other      |
| P27       | J55     | 4        | 24       | 92.29     | 92.30     | 0.674   | 0.632    | Other      |
| P27       | J70     | 7        | 33       | 92.95     | 92.92     | 1.036   | 1.091    | Other      |
| P28       | J39     | 4        | 28       | 93.26     | 93.28     | 1.298   | 1.242    | Other      |
| P30       | J65     | 2        | 8        | 93.74     | 93.80     | 2.486   | 1.989    | Other      |
| P31       | J71     | 2        | 8        | 94.12     | 94.15     | 0.517   | 0.616    | Other      |
| P36       | J09     | 5        | 21       | 92.76     | 92.83     | 1.439   | 1.524    | Other      |
| Total / A | Average | 82       | 516      | 92.17     | 92.21     | 1.303   | 1.237    | Other      |

Table 6.11. Summary of Density Test Results for Each Project Sorted by Paving Type

\* All Tests: the mean of all individual test results on the project Lot Means: the mean of all the individual lot means on the project

\*\* **Project:** the unbiased standard deviation estimate of all individual test results on the project **Lot:** the average of the unbiased standard deviation estimates for all lots on the project

| Num     | nber | Total Nu | mber of | Mea       | Mean of * |         | Std Deviation* |          |
|---------|------|----------|---------|-----------|-----------|---------|----------------|----------|
| Project | JMF  | Lots     | Tests   | All Tests | Lot Means | Project | Lot            | Туре     |
| P01     | J10  | 7        | 30      | 92.90     | 92.85     | 0.599   | 0.515          | Inter B  |
| P01     | J07  | 4        | 22      | 93.26     | 93.24     | 0.801   | 0.543          | Surf 1C  |
| P01     | J07  | 5        | 20      | 92.73     | 92.77     | 0.591   | 0.546          | Surf B   |
| P23     | J63  | 6        | 18      | 93.11     | 93.11     | 0.584   | 0.607          | Surf B   |
| P31     | J71  | 2        | 8       | 94.12     | 94.15     | 0.517   | 0.616          | Surf B   |
| P27     | J55  | 4        | 24      | 92.29     | 92.30     | 0.674   | 0.632          | Surf B   |
| P01     | J02  | 4        | 22      | 93.94     | 93.56     | 0.908   | 0.848          | Binder 1 |
| P32     | J72  | 8        | 70      | 93.07     | 93.06     | 0.861   | 0.854          | Surf B   |
| P32     | J79  | 24       | 166     | 92.77     | 92.77     | 0.943   | 0.868          | Surf A   |
| P20     | J50  | 7        | 67      | 92.38     | 92.42     | 0.938   | 0.945          | Surf C   |
| P03     | J15  | 5        | 25      | 93.23     | 93.41     | 1.272   | 0.957          | Surf B   |
| P06     | J24  | 5        | 25      | 91.47     | 91.69     | 1.751   | 0.995          | Surf 1D  |
| P24     | J56  | 7        | 56      | 93.12     | 93.20     | 1.078   | 1.001          | Surf C   |
| P26     | J62  | 9        | 42      | 92.85     | 92.84     | 1.366   | 1.052          | Surf A   |
| P03     | J04  | 5        | 30      | 93.73     | 93.59     | 1.388   | 1.053          | Interm B |
| P32     | J76  | 13       | 105     | 93.27     | 93.27     | 1.072   | 1.059          | Inter B  |
| P16     | J20  | 3        | 12      | 91.58     | 91.58     | 1.087   | 1.063          | Surf C   |
| P27     | J70  | 7        | 33      | 92.95     | 92.92     | 1.036   | 1.091          | Surf B   |
| P26     | J69  | 16       | 81      | 93.39     | 93.40     | 1.210   | 1.126          | Surf A   |
| P33     | J77  | 6        | 40      | 92.67     | 92.72     | 1.486   | 1.161          | Surf A   |
| P26     | J59  | 7        | 55      | 91.03     | 91.22     | 1.343   | 1.170          | Surf C   |
| P14     | J16  | 6        | 38      | 92.46     | 92.55     | 1.313   | 1.179          | Surf C   |
| P06     | J26  | 1        | 14      | 90.05     | 90.05     | 1.181   | 1.181          | Surf 1C  |
| P08     | J11  | 1        | 8       | 88.65     | 88.65     | 1.203   | 1.203          | Surf 1R  |
| P28     | J39  | 4        | 28      | 93.26     | 93.28     | 1.298   | 1.242          | Surf C   |
| P04     | J14  | 5        | 36      | 89.77     | 89.80     | 1.312   | 1.262          | Surf 1R  |
| P01     | J23  | 2        | 8       | 93.75     | 93.77     | 1.160   | 1.403          | Interm B |
| P32     | J74  | 1        | 6       | 93.20     | 93.20     | 1.417   | 1.417          | Surf A   |
| P33     | J73  | 8        | 56      | 93.18     | 93.17     | 1.377   | 1.459          | Inter B  |
| P34     | J62  | 4        | 25      | 92.74     | 93.01     | 1.820   | 1.500          | Surf A   |
| P36     | J09  | 5        | 21      | 92.76     | 92.83     | 1.439   | 1.524          | Interm B |
| P13     | J03  | 1        | 9       | 92.01     | 92.01     | 1.567   | 1.567          | Surf C   |
| P15     | J44  | 5        | 18      | 92.68     | 92.68     | 1.465   | 1.584          | Surf C   |
| P23     | J33  | 4        | 16      | 91.64     | 91.63     | 1.374   | 1.649          | Inter B  |
| P30     | J65  | 2        | 8       | 93.74     | 93.80     | 2.486   | 1.989          | Surf B   |
| P18     | J48  | 3        | 18      | 91.55     | 91.65     | 1.824   | 2.042          | Surf C   |
| Total/  | Mean | 206      | 1260    | 92.54     | 92.56     | 1.215   | 1.136          |          |
|         |      |          |         |           | 50%       | 1.241   | 1.109          |          |
|         |      |          |         |           | 60%       | 1.313   | 1.179          |          |
|         |      |          |         |           | 70%       | 1.375   | 1.252          |          |
|         |      |          |         |           | 80%       | 1.439   | 1.459          |          |
|         |      |          |         |           | 90%       | 1.659   | 1.576          |          |

Table 6.12. Summary of Density Test Results for Each Project

- \* All Tests: the mean of all individual test results on the project Lot Means: the mean of all the individual lot means on the project
- \*\* **Project:** the unbiased standard deviation estimate of all individual test results on the project **Lot:** the average of the unbiased standard deviation estimates for all lots on the project



Figure 6.1. Empirical CDF for the Lot Standard Deviations for All Projects

| Number    |         | Total Number of |       | Mean of * |           | Std Deviation* |       |
|-----------|---------|-----------------|-------|-----------|-----------|----------------|-------|
| Project   | JMF     | Lots            | Tests | All Tests | Lot Means | Project        | Lot   |
| P01       | J10     | 7               | 30    | 92.9      | 92.85     | 0.599          | 0.515 |
| P01       | J07     | 4               | 22    | 93.26     | 93.24     | 0.801          | 0.543 |
| P01       | J07     | 5               | 20    | 92.73     | 92.77     | 0.591          | 0.546 |
| P23       | J63     | 6               | 18    | 93.11     | 93.11     | 0.584          | 0.607 |
| P01       | J02     | 4               | 22    | 93.94     | 93.56     | 0.908          | 0.848 |
| P32       | J72     | 8               | 70    | 93.07     | 93.06     | 0.861          | 0.854 |
| P32       | J79     | 24              | 166   | 92.77     | 92.77     | 0.943          | 0.868 |
| P03       | J15     | 5               | 25    | 93.23     | 93.41     | 1.272          | 0.957 |
| P26       | J62     | 9               | 42    | 92.85     | 92.84     | 1.366          | 1.052 |
| P32       | J76     | 13              | 105   | 93.27     | 93.27     | 1.072          | 1.059 |
| P26       | J69     | 16              | 81    | 93.39     | 93.40     | 1.210          | 1.126 |
| P33       | J77     | 6               | 40    | 92.67     | 92.72     | 1.486          | 1.161 |
| P32       | J74     | 1               | 6     | 93.20     | 93.20     | 1.417          | 1.417 |
| P33       | J73     | 8               | 56    | 93.18     | 93.17     | 1.377          | 1.459 |
| P34       | J62     | 4               | 25    | 92.74     | 93.01     | 1.820          | 1.500 |
| P23       | J33     | 4               | 16    | 91.64     | 91.63     | 1.374          | 1.649 |
| Total / A | Average | 124             | 744   | 93.00     | 93.00     | 1.105          | 1.010 |
|           |         |                 |       |           | 50%       | 1.141          | 1.005 |
|           |         |                 |       |           | 60%       | 1.272          | 1.059 |
|           |         |                 |       |           | 70%       | 1.370          | 1.144 |
|           |         |                 |       |           | 80%       | 1.377          | 1.417 |
|           |         |                 |       |           | 90%       | 1.452          | 1.480 |

\* see Table 6.10 for explanations for these terms.



Figure 6.2. Empirical CDF for the Lot Standard Deviations for Interstate Projects

Table 6.14 shows the standard deviation results from Table 6.10 that are for the Other paving projects. Figure 6.3 shows the empirical CDF for the Lot standard deviation values.

As the reference lines show, there may be a natural break point at around a standard deviation of 1.20, which corresponds to approximately the 75<sup>th</sup> percentile. Although, the 80<sup>th</sup> percentile, with a standard deviation of 1.26, is another possible choice. Therefore, somewhere in the range 1.20 to 1.26 would seem to be a logical choice for the process standard deviation for Interstate paving projects if they are treated separately from Other paving projects.

The results from Figures 6.1-6.3 show that possible choices for within-lot process standard deviation are 1.16 for Interstate paving projects, 1.20 to 1.26 for Other paving projects, and 1.25 if Interstate and Other projects are combined and treated as one data set. SCDOT will need to reach its own decision regarding whether or not to separate Interstate and Other paving projects, and then decide what typical standard deviation or deviations to use. For the remaining calculations in this report, a value of 1.20 will be used as the standard deviation to represent both Interstate and Other paving projects.

This value, as well as some of the various standard deviation values in Table 6.12, may seem high if compared with values that may have been calculated on some past projects. This is at least partially due to the fact that the values in the table have been adjusted for bias, whereas the lot standard deviation values do not need to be adjusted for bias when calculating PWL. The average lot standard deviation that would be expected in the field would depend upon the sample size and can be calculated using equation 6.5. For example, if the typical lot size were n = 5, which corresponds to a  $c_4$  value of 0.9400 (see Table 5.1), then the selected Lot standard deviation of 1.20 would correspond to an average sample standard deviation of  $1.20 \times 0.9400 = 1.128$ . Different corresponding values would be expected for different sample sizes.

| Number    |         | Total Number of |       | Mean of * |             | Std Deviation* |       |
|-----------|---------|-----------------|-------|-----------|-------------|----------------|-------|
| Project   | JMF     | Lots            | Tests | All Tests | Lot Means   | Project        | Lot   |
| P31       | J71     | 2               | 8     | 94.12     | 94.15       | 0.517          | 0.616 |
| P27       | J55     | 4               | 24    | 92.29     | 92.30       | 0.674          | 0.632 |
| P20       | J50     | 7               | 67    | 92.38     | 92.42       | 0.938          | 0.945 |
| P06       | J24     | 5               | 25    | 91.47     | 91.69       | 1.751          | 0.995 |
| P24       | J56     | 7               | 56    | 93.12     | 93.20       | 1.078          | 1.001 |
| P03       | J04     | 5               | 30    | 93.73     | 93.59       | 1.388          | 1.053 |
| P16       | J20     | 3               | 12    | 91.58     | 91.58       | 1.087          | 1.063 |
| P27       | J70     | 7               | 33    | 92.95     | 92.92       | 1.036          | 1.091 |
| P26       | J59     | 7               | 55    | 91.03     | 91.22       | 1.343          | 1.170 |
| P14       | J16     | 6               | 38    | 92.46     | 92.55       | 1.313          | 1.179 |
| P06       | J26     | 1               | 14    | 90.05     | 90.05       | 1.181          | 1.181 |
| P08       | J11     | 1               | 8     | 88.65     | 88.65       | 1.203          | 1.203 |
| P28       | J39     | 4               | 28    | 93.26     | 93.28       | 1.298          | 1.242 |
| P04       | J14     | 5               | 36    | 89.77     | 89.80       | 1.312          | 1.262 |
| P01       | J23     | 2               | 8     | 93.75     | 93.77       | 1.160          | 1.403 |
| P36       | J09     | 5               | 21    | 92.76     | 92.83       | 1.439          | 1.524 |
| P13       | J03     | 1               | 9     | 92.01     | 92.01       | 1.567          | 1.567 |
| P15       | J44     | 5               | 18    | 92.68     | 92.68       | 1.465          | 1.584 |
| P30       | J65     | 2               | 8     | 93.74     | 93.80       | 2.486          | 1.989 |
| P18       | J48     | 3               | 18    | 91.55     | 91.65       | 1.824          | 2.042 |
| Total / / | Average | 82              | 516   | 92.17     | 92.21       | 1.303          | 1.237 |
|           |         |                 |       |           | <b>50%</b>  | 1.305          | 1.090 |
|           |         |                 |       |           | <b>60</b> % | 1.325          | 1.174 |
|           |         |                 |       |           | 70%         | 1.403          | 1.188 |
|           |         |                 |       |           | 80%         | 1.485          | 1.290 |
|           |         |                 |       |           | 90%         | 1.758          | 1.569 |

#### Table 6.14. Summary of Density Test Results for Other Paving Projects

\* see Table 6.10 for explanations for these terms.



Figure 6.3. Empirical CDF for the Lot Standard Deviations for Other Projects

**PWL Values for the Density Projects.** One potential point of concern with the values in Table 6.12 was the relatively low value for the average densities on the various projects. These individual project average values ranged from a low of 88.65 to a high of 94.12, and the average for all projects was around 92.4. The specification "target" values for density were 94.0 for Interstate paving and 93.0 for Other paving. To further investigate how well the projects for which data were obtained met the specification requirements, lot PWL values were calculated. For each project, the PWL value for each lot was calculated and the average PWL for all lots on the project was also calculated. The average PWL values for each project are shown in Table 6.15 for Interstate paving projects and Table 6.16 for Other paving projects. Appendix C includes the PWL values for each individual lot on each project.

As shown in Table 6.15, the average lot PWL estimates for the Interstate paving projects vary from 37.76 to 99.52. Of concern is the fact that 11 of the 16 projects had average PWL values less than 90, which is the minimum value to receive 100 percent payment. The average PWL values in Table 6.16 for Other paving projects vary from 0.16 to 100, and 12 of the 20 projects had PWL values less than 90. Furthermore, 3 of the projects had PWL values less than 20, which is the value that triggers the remove and replace provision.

| Project         | JMF<br>Number | No. of | Average | Average | Avg Lot | Mix Type |
|-----------------|---------------|--------|---------|---------|---------|----------|
|                 | Inumber       |        |         |         |         | Dindor 1 |
| P01             | J02           | 4      | 93.56   | 0.810   | 98.50   | Binder 1 |
| P01             | J10           | 7      | 92.85   | 0.478   | 96.42   | Interm B |
| P23             | J33           | 4      | 91.63   | 1.502   | 37.76   | Interm B |
| P32             | J76           | 13     | 93.27   | 1.009   | 83.58   | Interm B |
| P33             | J73           | 8      | 93.17   | 1.394   | 72.47   | Interm B |
| Total / A       | Average       | 36     | 93.01   | 1.030   | 77.75   | Interm   |
|                 |               |        |         |         |         |          |
| P01             | J07           | 4      | 93.24   | 0.515   | 96.47   | Surf 1C  |
| P26             | J62           | 9      | 92.84   | 0.987   | 73.49   | Surf A   |
| P26             | J69           | 16     | 93.40   | 1.057   | 83.86   | Surf A   |
| P32             | J74           | 1      | 93.20   | 1.348   | 76.06   | Surf A   |
| P32             | J79           | 24     | 92.77   | 0.826   | 75.01   | Surf A   |
| P33             | J77           | 6      | 92.72   | 1.109   | 66.63   | Surf A   |
| P34             | J62           | 4      | 93.01   | 1.426   | 70.43   | Surf A   |
| P01             | J07           | 5      | 92.77   | 0.4942  | 90.83   | Surf B   |
| P03             | J15           | 5      | 93.41   | 0.892   | 85.06   | Surf B   |
| P23             | J63           | 6      | 93.11   | 0.538   | 99.52   | Surf B   |
| P32             | J72           | 8      | 93.06   | 0.821   | 83.05   | Surf B   |
| Total / Average |               | 88     | 93.01   | 0.888   | 81.06   | Surface  |
|                 |               |        |         |         |         |          |
| Total / A       | Average       | 124    | 93.01   | 0.928   | 80.57   | All      |

#### Table 6.15. Summary of Density Lot PWL Values for Each Interstate Paving Project

#### Summary

Analyses were conducted on project test results for Density. The primary goal of these analyses was to determine a value to use to represent the typical variability for Density. This is a subjective decision that ultimately must be made by SCDOT. Some potential values were identified during the analyses, and these are used as examples for additional evaluations in subsequent chapters.

The range of values that SCDOT might consider for the typical Density standard used to evaluate existing specification limits includes 1.16% to 1.26%.

**Important Note of Caution:** As noted in Chapter 5, a STD may choose to establish the typical standard deviation value to use based on "data from a number of past projects that it considered acceptable." Considering that nearly two-thirds of the projects from which density data were obtained had average project PWL values less than the AQL of 90 PWL, SCDOT must decide whether or not it wishes to establish the typical project standard deviation based on these data.

If SCDOT believes that these projects represent the state-of-the-art regarding the process capability of a typical contractor, then SCDOT will need to re-evaluate their target density value and their density specification limits. If SCDOT believes that these projects do not represent what a typical contractor is capable of providing, then additional data from other representative projects will need to be obtained for analysis.

# CHAPTER 7 — ANALYSIS OF PLANT ACCEPTANCE TEST RESULTS

## Background

This chapter summarizes and discusses the results of analyses to determine appropriate standard deviation values to represent the variability of each of the plant acceptance characteristics used by SCDOT. These include asphalt content, air voids, and VMA. These variabilities are necessary to evaluate the appropriateness of the existing specification limits.

# **Data Obtained for Analysis**

All of the plant acceptance test data that were provided are included in Appendix A. A total of 1,775 asphalt content tests were provided from 30 different projects, with some projects having multiple HMA mixes involved. Since no voids testing was done on Base course mixes, open graded friction course (OGFC) mixes, or Surface E mixes, there were only 1,341 air voids and VMA tests provided. The numbers of tests for the various projects and JMF mix designs are presented in Tables 7.1-7.5.

In the tables, each project is identified with a unique number, ranging from P01 to P36. Each of these numbered projects corresponds with a unique SCDOT project file number. Each job mix formula (JMF) is identified with a unique number, ranging from J01 to J83.

| Mix Type | Project    | JMF | Lots in<br>JMF | Tests in<br>JMF | Lots on<br>Project | Tests on<br>Project |
|----------|------------|-----|----------------|-----------------|--------------------|---------------------|
| AABC 1   | P01        | J01 | 8              | 22              | 11                 | 31                  |
|          | 101        | J06 | 3              | 9               |                    |                     |
|          | P01        | J18 | 33             | 82              | 46                 | 109                 |
|          | FUI        | J21 | 15             | 27              |                    |                     |
| Base A   | P02<br>P26 | J17 | 6              | 17              | 19                 | 47                  |
| Dase A   |            | J28 | 13             | 30              |                    |                     |
|          |            | J45 | 4              | 12              | 4                  | 12                  |
|          | P27        | J66 | 11             | 11              | 11                 | 11                  |
| Base B   | P28        | J47 | 10             | 14              | 10                 | 14                  |
| Base C   | P24        | J57 | 6              | 12              | 6                  | 12                  |
| Total    |            |     | 109            | 236             | 107                | 236                 |

#### Table 7.1. Summary of Asphalt Content Data for Base Course

| Mix Type       | Project     | JMF | Lots in<br>JMF | Tests in<br>JMF | Lots on<br>Project | Tests on<br>Project |
|----------------|-------------|-----|----------------|-----------------|--------------------|---------------------|
| Bindor 1       | P01         | J02 | 4              | 12              | 4                  | 12                  |
| Dinder i       | P04         | J08 | 11             | 21              | 11                 | 21                  |
|                | <b>D</b> 01 | J10 | 18             | 39              | 24                 | 51                  |
|                | FUI         | J23 | 6              | 12              |                    |                     |
|                | P02         | J04 | 14             | 30              | 30                 | 64                  |
| Intermediate B | F UZ        | J09 | 18             | 34              | 32                 | 04                  |
|                | P27         | J60 | 15             | 15              | 15                 | 15                  |
|                | P32         | J76 | 12             | 43              | 12                 | 43                  |
|                | P33         | J73 | 8              | 25              | 8                  | 25                  |
|                | P05         | J27 | 8              | 15              | 8                  | 15                  |
|                | P10         | J31 | 41             | 77              | 61                 | 114                 |
|                |             | J37 | 12             | 22              |                    |                     |
|                |             | J82 | 8              | 15              |                    |                     |
| Intermediate C | P17         | J22 | 6              | 11              | 6                  | 11                  |
|                | P21         | J34 | 3              | 8               | 3                  | 8                   |
|                | P24         | J51 | 15             | 23              | 15                 | 23                  |
|                | P25         | J29 | 7              | 12              | 7                  | 12                  |
|                | P27         | J53 | 16             | 19              | 16                 | 19                  |
|                | P28         | J42 | 13             | 15              | 13                 | 15                  |
| Total          |             |     | 235            | 448             | 235                | 448                 |

# Table 7.2. Summary of Asphalt Content Data for Intermediate Course

| Mix Type   | Project     | JMF        | Lots in | Tests in | Lots on | Tests on |
|------------|-------------|------------|---------|----------|---------|----------|
|            | Doc         | 100        | JIVIF   | JIVIF    | FIOJECI | FIOJECI  |
| OGFC       | P26<br>P33  | J68<br>178 | 4       | 13       | 4       | 13       |
| Surface 1C | P01         | 107        | 5       | 16       | 5       | 16       |
| Surface 1D |             | J07        | 5       | 10       | 5       | 10       |
| Surface 1D | P06         | J24        | 5       | 10       | 5<br>5  | 15       |
| Surface 1R | P04         | J14        | 5       | 17       | 5       | 17       |
| Surface 3  | P07         | J30        | 19      | 40       | 19      | 40       |
| Surface 4  | P10         | J12        | 13      | 19       | 13      | 19       |
|            | P26         | J62        | 9       | 31       | 27      | 84       |
| Surface A  | <b>D</b> 22 | 170        | 10      | 06       | 24      | 06       |
| Surface A  | P33         | 177        | 6       | 30       | 6       | 30       |
|            | P34         | 162        | 7       | 22       | 7       | 22       |
|            | P01         | 107        | 1       | 14       | 1       | 14       |
|            | P01         | J07        | 4       | 14       | 4       | 14       |
|            | F UZ        | J 15       | 5       | 10       | 0       | 10       |
| Surface B  | P27         | 171        | 0<br>0  | 10<br>27 | 14      | 42       |
|            | P30         | J65        | 4       | 8        | 4       | 8        |
|            | P32         | J72        | 8       | 34       | 8       | 34       |
|            | P01         | .119       | 14      | 18       | 14      | 18       |
|            | 101         | .105       | 6       | 8        |         | 10       |
|            | P02         | J13        | 14      | 18       | 20      | 26       |
|            | P11         | J41        | 4       | 10       | 4       | 10       |
|            | P12         | J38        | 6       | 14       | 6       | 14       |
|            | P13         | J03        | 8       | 16       | 16      |          |
|            |             | J43        | 8       | 19       |         | 35       |
|            | P14         | J16        | 13      | 32       | 13      | 32       |
|            | P16         | J20        | 3       | 9        | 3       | 9        |
| Surface C  | P18         | J48        | 7       | 12       | 7       | 12       |
| Surface C  | P20         | J50        | 17      | 46       | 17      | 46       |
|            | P21         | J39        | 6       | 15       | 6       | 15       |
|            | P24         | J56        | 18      | 40       | 24      | 50       |
|            |             | J67        | 6       | 10       | 24      | 50       |
|            | P26         | J58        | 12      | 13       | 12      | 13       |
|            | P28         | J39        | 9       | 24       | 9       | 24       |
|            | P29         | J59        | 9       | 26       | 9       | 26       |
|            | P34         | J81        | 7       | 13       | 7       | 13       |
|            | P35         | J32        | 6       | 14       | 22      | 50       |
|            | 1.00        | J38        | 16      | 36       |         |          |
|            | P09         | J35        | 3       | 9        | 6       | 17       |
| Surface CM |             | J83        | 3       | 8        | 5       | .,       |
|            | P27         | J61        | 9       | 9        | 9       | 9        |
|            | P05         | J25        | 8       | 8        | 8       | 8        |
|            | P19         | J49        | 7       | 20       | 7       | 20       |
| Surface D  | P22         | J54        | 3       | 12       | 3       | 12       |
|            | P24         | J64        | 7       | 13       | 7       | 13       |
|            | P25         | J36        | 6       | 10       | 6       | 10       |
|            | P05         | J40        | 5       | 9        | 5       | 9        |
|            | P26         | J52        | 30      | 58       | 30      | 58       |
| Surface E  | P32         | J46        | 31      | 41       | 31      | 41       |
|            | P33         | J75        | 10      | 10       | 10      | 10       |
|            | P34         | J80        | 6       | 12       | 6       | 12       |
| Total      |             |            | 472     | 1091     | 472     | 1091     |

 Table 7.3. Summary of Asphalt Content Data for Surface Course

| Mix Type       | Project | JMF | Lots in<br>JMF | Tests in<br>JMF | Lots on<br>Project | Tests on<br>Project |
|----------------|---------|-----|----------------|-----------------|--------------------|---------------------|
| Bindor 1       | P01     | J02 | 4              | 8               | 4                  | 8                   |
| Dinder i       | P04     | J08 | 5              | 10              | 5                  | 10                  |
|                | P01     | J10 | 18             | 39              | 24                 | 51                  |
|                | FUI     | J23 | 6              | 12              |                    |                     |
|                | D02     | J04 | 14             | 30              | 32                 | 64                  |
| Intermediate B | F UZ    | J09 | 18             | 34              |                    |                     |
|                | P27     | J60 | 15             | 15              | 15                 | 15                  |
|                | P32     | J76 | 12             | 43              | 12                 | 43                  |
|                | P33     | J73 | 8              | 25              | 8                  | 25                  |
|                | P05     | J27 | 8              | 15              | 8                  | 15                  |
|                | P10     | J31 | 41             | 77              | 61                 | 114                 |
|                |         | J37 | 12             | 22              |                    |                     |
|                |         | J82 | 8              | 15              |                    |                     |
| Intermediate C | P17     | J22 | 6              | 11              | 6                  | 11                  |
|                | P21     | J34 | 3              | 8               | 3                  | 8                   |
|                | P25     | J29 | 7              | 12              | 7                  | 12                  |
|                | P27     | J53 | 14             | 15              | 14                 | 15                  |
|                | P28     | J42 | 13             | 15              | 13                 | 15                  |
| Total          |         |     | 212            | 406             | 212                | 406                 |

# Table 7.4. Summary of Air Voids and VMA Data for Intermediate Course
| Mix Type    | Project | JMF  | Lots in<br>JMF | Tests in<br>JMF | Lots on<br>Project | Tests on<br>Project |
|-------------|---------|------|----------------|-----------------|--------------------|---------------------|
| Surface 1C  | P01     | J07  | 5              | 16              | 5                  | 16                  |
| Surface 1D  | P06     | J24  | 5              | 15              | 5                  | 15                  |
| Surface 1R  | P04     | J14  | 5              | 17              | 5                  | 17                  |
| Surface 3   | P07     | J30  | 19             | 40              | 19                 | 40                  |
| Surface 4   | P10     | J12  | 13             | 19              | 13                 | 19                  |
|             |         | J62  | 9              | 31              |                    |                     |
|             | P26     | J69  | 18             | 53              | 27                 | 84                  |
| Surface A   | P32     | J79  | 24             | 96              | 24                 | 96                  |
|             | P33     | J77  | 6              | 22              | 6                  | 22                  |
|             | P34     | J62  | 7              | 28              | 7                  | 28                  |
|             | P01     | J07  | 4              | 14              | 4                  | 14                  |
|             | P02     | J15  | 6              | 18              | 6                  | 18                  |
| Curría da D | D07     | J55  | 5              | 15              | 4.4                | 40                  |
| Surface B   | P27     | J71  | 9              | 27              | 14                 | 42                  |
|             | P30     | J65  | 4              | 8               | 4                  | 8                   |
|             | P32     | J72  | 8              | 34              | 8                  | 34                  |
|             | P01     | J19  | 14             | 18              | 14                 | 18                  |
|             | D02     | J05  | 6              | 8               | 20                 | 26                  |
|             | FUZ     | J13  | 14             | 18              | 20                 | 20                  |
|             | P11     | J41  | 4              | 10              | 4                  | 10                  |
|             | P12     | J38  | 6              | 14              | 6                  | 14                  |
|             | P13     | J03  | 8              | 16              | 16                 | 35                  |
|             |         | J43  | 8              | 19              | 10                 | 00                  |
|             | P14     | J16  | 13             | 32              | 13                 | 32                  |
|             | P16     | J20  | 3              | 9               | 3                  | 9                   |
| Surface C   | P18     | J48  | 7              | 12              | 7                  | 12                  |
|             | P20     | J50  | 17             | 46              | 17                 | 46                  |
|             | P21     | J39  | 6              | 15              | 6                  | 15                  |
|             | P24     | J56  | 18             | 40              | 24                 | 50                  |
|             | D26     | 159  | 12             | 10              | 12                 | 12                  |
|             | P28     | 130  | 9              | 24              | 9                  | 24                  |
|             | P29     | .159 | 9              | 26              | 9                  | 24                  |
|             | P34     | J81  | 7              | 13              | 7                  | 13                  |
|             |         | J32  | 6              | 14              |                    |                     |
|             | P35     | J38  | 16             | 36              | 24                 | 50                  |
|             | Dea     | J35  | 3              | 9               |                    | · -                 |
| Surface CM  | P09     | J83  | 3              | 8               | 6                  | 17                  |
|             | P27     | J61  | 9              | 9               | 9                  | 9                   |
|             | P05     | J25  | 8              | 8               | 8                  | 8                   |
|             | P19     | J49  | 7              | 20              | 7                  | 20                  |
| Surface D   | P22     | J54  | 3              | 12              | 3                  | 12                  |
|             | P24     | J64  | 7              | 13              | 7                  | 13                  |
|             | P25     | J36  | 6              | 10              | 6                  | 10                  |
| Total       |         |      | 382            | 935             | 384                | 935                 |

 Table 7.5. Summary of Air Voids and VMA Data for Surface Course

### Plant Test Data Analyses

Unlike density, the plant test data had specific target values. It was not possible to compare directly the actual test results since each project and each mix design had its own set of target values. It was possible, however, to normalize the data by considering the asphalt content (AC), air voids (AV), and VMA values as differences from their target values. This made it possible to make comparisons among the various lots, mix designs, projects, mix types, and courses that could not be done on the actual test values.

## **Asphalt Content**

**Comparing Courses.** The specifications for AC had one set of allowable tolerances for "mainline paving." Unlike density, the AC tolerances did not differ between Interstate and Other paving projects. There were, however, different tolerances for Base, Intermediate, and Surface courses. These tolerances were 0.36 for Surface course, 0.43 for Intermediate course, and 0.50 for Base course. To evaluate whether or not different tolerances were warranted for different courses, the variances of the three courses were compared statistically using Bartlett's test and Levene's test. Bartlett's test assumes that the data are from normal distributions, whereas Levene's test applies for any continuous distribution. Table 7.6 shows the results of the comparisons.

| Course       | No. of<br>Tests | St Dev | P-value*<br>Bartlett's | P-value*<br>Levene's |  |
|--------------|-----------------|--------|------------------------|----------------------|--|
| Base         | 236             | 0.2500 |                        |                      |  |
| Intermediate | 448             | 0.2372 | 0.011                  | 0.000                |  |
| Surface      | 1091            | 0.1960 |                        |                      |  |

### Table 7.6. Summary of AC Comparisons among Courses

\* Values in bold are statistically significantly different at the  $\alpha = 0.05$  level.

The results in Table 7.6 show that, with a P-value of 0.011 for Bartlett's test and 0.000 for Levene's test, there is essentially no chance that the variabilities are the same for the three courses. To further investigate the variabilities, Figure 7.1 shows the standard deviation along with its 95% confidence interval for each course. Since the confidence interval for Surface course does not overlap at all with those for Base and Intermediate courses, it is apparent that the AC for Surface course has less variability than for Intermediate and Base courses. While the standard deviation for Intermediate Course is less than that for Base course, due to the overlap of the confidence intervals, it cannot be concluded that the Base course standard deviation is larger than the standard deviation for Intermediate course.



Figure 7.1. Comparison of AC Standard Deviations for Each Course

**Comparing Mix Types within Course.** The next question to consider is whether it is appropriate to use the same specification tolerances for all mix types within a given course. When establishing the allowable tolerances it is the standard deviation that is most important.

**Base Course Mixes.** Table 7.7 shows the results of comparisons among the AC variabilities for the different types of Base course mixes. The results are mixed, with Bartlett's test, with a P-value of 0.013, showing the variances different, and Levene's test showing them not different at the 0.10 significance level.

Table 7.7. Summary of AC Comparisons of Base Course Mix Types

| Mix Type | No. of<br>Tests | St Dev | P-value*<br>Bartlett's | P-value*<br>Levene's |
|----------|-----------------|--------|------------------------|----------------------|
| AABC 1   | 31              | 0.2206 |                        |                      |
| Base A   | 179             | 0.2602 | 0.012                  | 0.100                |
| Base B   | 14              | 0.2361 | 0.013                  |                      |
| Base C   | 12              | 0.1085 |                        |                      |

\* Values in bold are statistically significantly different at the  $\alpha = 0.05$  level.

From Table 7.7, it is apparent that if the variabilities are different it is most likely due to the low value for the Base C mix. All of the other values are more than twice as large as the Base C value.

To further investigate the variabilities, Figure 7.2 shows the standard deviation along with its 95% confidence interval for each Base course mix type. The large sample size for the Base A mix is apparent in its narrow confidence interval. The small Base C standard deviation is apparent, but due to the small sample size its confidence interval overlaps two of the other confidence intervals.



Figure 7.2. Comparison of AC Standard Deviations for Each Base Course Mix Type

To investigate further, Base C was eliminated and the variabilities of the other three mixes were compared. The results are shown in Table 7.8. Without Base C, there is strong evidence to consider the standard deviations to be the same for Base course mixes.

Table 7.8. Summary of AC Comparisons of Base Course Mix Types without Base C Mix

| Міх Туре | No. of<br>Tests | St Dev | P-value*<br>Bartlett's | P-value*<br>Levene's |  |
|----------|-----------------|--------|------------------------|----------------------|--|
| AABC 1   | 31              | 0.2206 |                        |                      |  |
| Base A   | 179             | 0.2602 | 0.495                  | 0.699                |  |
| Base B   | 14              | 0.2361 |                        |                      |  |

\* Values in bold are statistically significantly different at the  $\alpha = 0.05$  level.

**Intermediate Course Mixes.** Table 7.9 shows the results of comparisons among the AC variabilities for the different types of Intermediate course mixes. The results, with Bartlett's test having a P-value of 0.425 and Levene's test having a P-value of 0.582, show no evidence that the standard deviations are different for the different mix types. Figure 7.3 shows the

standard deviation along with its 95% confidence interval for each Intermediate course mix type.

| Mix Type       | No. of<br>Tests | St Dev | P-value*<br>Bartlett's | P-value*<br>Levene's |
|----------------|-----------------|--------|------------------------|----------------------|
| Binder 1       | 33              | 0.2598 |                        |                      |
| Intermediate B | 198             | 0.2337 | 0.425                  | 0.582                |
| Intermediate C | 217             | 0.2216 |                        |                      |

 Table 7.9. Summary of AC Comparisons of Intermediate Course Mix Types

\* Values in bold are statistically significantly different at the  $\alpha = 0.05$  level.



# Figure 7.3 Comparison of AC Standard Deviations for Each Intermediate Course Mix Type

**Surface Course Mixes.** Table 7.10 shows the results of comparisons among the AC variabilities for the different types of Surface course mixes. The results show clearly that the standard deviations are not equal for all 12 mix types. Figure 7.4 shows the standard deviation along with its 95% confidence interval for each Surface course mix type. It is apparent that the OGFC mix is markedly larger than any of the other mixes. The Surface 4 mix also seems to be above the range of the other values. If these two projects are eliminated the Bartlett's P-value is still 0.000, but Levene's P-value rises to 0.111.

| Міх Туре   | No. of<br>Tests | St Dev | P-value*<br>Bartlett's | P-value*<br>Levene's |
|------------|-----------------|--------|------------------------|----------------------|
| OGFC       | 26              | 0.3872 |                        |                      |
| Surface 1C | 16              | 0.1773 |                        |                      |
| Surface 1D | 15              | 0.1701 |                        |                      |
| Surface 1R | 17              | 0.1907 |                        |                      |
| Surface 3  | 40              | 0.1454 |                        |                      |
| Surface 4  | 19              | 0.2743 | 0.000                  | 0.000                |
| Surface A  | 230             | 0.1925 | 0.000                  | 0.000                |
| Surface B  | 116             | 0.1758 |                        |                      |
| Surface C  | 393             | 0.2182 |                        |                      |
| Surface CM | 26              | 0.1482 |                        |                      |
| Surface D  | 63              | 0.2027 |                        |                      |
| Surface E  | 130             | 0.1586 |                        |                      |

Table 7.10. Summary of AC Comparisons of Surface Course Mix Types



Figure 7.4 Comparison of AC Standard Deviations for Each Surface Course Mix Type

**Caveat.** None of the standard deviation values shown in Tables 7.6-7.10 are the appropriate standard deviation to use to represent the process standard deviation for AC. These calculations were done simply for exploratory purposes. Aggregating the data as is done in these tables is not appropriate for establishing specification limits since the specification limits are based on lot-by-lot acceptance, or at least on acceptance of a project.

**Typical Variability Values for AC.** As noted above, since the SCDOT specification is based on lot-by-lot acceptance, the AC variability that is used to evaluate the specification limits must be that which is appropriate for a typical lot. To determine this, the individual standard deviation values for each lot were calculated and then these lot standard deviations were averaged to get the "within-lot" standard deviation for each project. This was done using the procedure that is described for density in Chapter 6. As noted in Chapter 6, this within-lot standard deviation does not take into consideration any target miss variability that may be present.

To provide the option to consider using the total project as the payment lot, the total project AC standard deviation was also calculated for each project. As noted above, this "project" standard deviation could also be used as one way of trying to incorporate any target miss variability that might be present in the contractor's process.

Appendix B includes the necessary calculations for each project for which AC data were obtained. These calculations were used to arrive at the project standard deviations that were used to establish the typical process variability for AC.

**Projects with Multiple JMFs.** Before compiling all of the within-lot and project variabilities, a decision had to be made regarding how to deal with projects on which more than one JMF was used for the same mix type and course. Should each JMF be treated as a separate project, or should the multiple JMF results be combined together as one project? To help make this decision, the projects with multiple JMFs were examined. Table 7.11 shows the projects (extracted from Tables 7.1-7.5) that had multiple JMFs for the same mix type.

None of the multi-mix design projects showed a difference in variability for the Base course and Intermediate course. Two of the seven Surface course projects showed significantly different variabilities. So, in a total of 11 out of 13 projects no difference was detected between the multiple mix designs on the project. Also, in the project data a new lot was established in nearly every case that the JMF changed. This would argue in favor of treating the JMFs as separate projects when determining the within-lot standard deviations.

However, if a total project is being used as the payment lot, then the data from the multiple JMFs would be combined when calculating the standard deviation to use for payment determination. This would argue in favor of combining the separate JMFs into a single project. For consistency in presentation and in comparing results, it was decided to treat the separate JMFs as separate projects when calculating standard deviations and when presenting the results.

| Project     | JMF | No. of<br>Lots | No. of<br>Tests | St Dev | F-Test<br>P-value* |  |  |  |  |
|-------------|-----|----------------|-----------------|--------|--------------------|--|--|--|--|
| Base Course |     |                |                 |        |                    |  |  |  |  |
| <b>D</b> 01 | J01 | 8              | 22              | 0.229  | 0.840              |  |  |  |  |
| PUT         | J06 | 3              | 9               | 0.210  | 0.040              |  |  |  |  |
| D01         | J18 | 33             | 82              | 0.243  | 0.010              |  |  |  |  |
| FUI         | J21 | 15             | 27              | 0.255  | 0.919              |  |  |  |  |
| P02         | J17 | 6              | 17              | 0.294  | 0 389              |  |  |  |  |
| F 02        | J28 | 13             | 30              | 0.245  | 0.369              |  |  |  |  |
|             |     | Intermedia     | ate Course      |        |                    |  |  |  |  |
| 504         | J10 | 18             | 39              | 0.200  | 0.050              |  |  |  |  |
| P01         | J23 | 6              | 12              | 0.304  | 0.056              |  |  |  |  |
| Dee         | J04 | 14             | 30              | 0.224  | 0.04.4             |  |  |  |  |
| P02         | J09 | 18             | 34              | 0.246  | 0.614              |  |  |  |  |
|             | J31 | 41             | 77              | 0.257  |                    |  |  |  |  |
| P10         | J37 | 12             | 22              | 0.204  | 0.238**            |  |  |  |  |
|             | J82 | 8              | 15              | 0.193  |                    |  |  |  |  |
|             |     | Surface        | Course          |        |                    |  |  |  |  |
|             | J62 | 9              | 31              | 0.178  |                    |  |  |  |  |
| P26         | J69 | 18             | 53              | 0.194  | 0.610              |  |  |  |  |
|             | J55 | 5              | 15              | 0.191  |                    |  |  |  |  |
| P27         | J71 | 9              | 27              | 0.161  | 0.427              |  |  |  |  |
| Baa         | J05 | 6              | 8               | 0.145  | 0.070              |  |  |  |  |
| P02         | J13 | 14             | 18              | 0.291  | 0.070              |  |  |  |  |
| <b>D</b> 40 | J03 | 8              | 16              | 0.269  | 0.005              |  |  |  |  |
| P13         | J43 | 8              | 19              | 0.153  | 0.025              |  |  |  |  |
| D24         | J56 | 18             | 40              | 0.249  | 0.000              |  |  |  |  |
| P24         | J67 | 6              | 10              | 0.595  | 0.000              |  |  |  |  |
| Dor         | J32 | 6              | 14              | 0.148  | 0.007              |  |  |  |  |
| P35         | J38 | 16             | 36              | 0.124  | 0.387              |  |  |  |  |
| DOO         | J35 | 3              | 9               | 0.144  | 0.472              |  |  |  |  |
| P09         | J83 | 3              | 8               | 0.189  | 0.473              |  |  |  |  |

Table 7.11. Projects with More than One JMF for the Same Mix Type for AC

- \* Values in bold are statistically significantly different at the  $\alpha = 0.05$  level.
- **\*\*** Bartlett's Test

**Determining the Typical Process Variability for AC.** Table 7.12 shows the standard deviation results for AC for all projects for which data were obtained. The projects are sorted by mix type. The "Lot" standard deviation is the average of the unbiased standard deviation estimates for each lot on the project. The "Project" standard deviation is the standard deviation of all the individual test results for the total project. The table also shows the total number of lots and tests for each project, the mean for all tests on the project, and the mean of the individual project lot means. Note that some projects do not have an average Lot standard deviation. This is due to the fact that there was only one AC test for each lot on the project. With only one test it is not possible to calculate a standard deviation for the lot.

One thing to consider from the results in Table 7.12 is whether to treat the Base course results, the Intermediate course results, and the Surface course results as separate from one another or to combine them. By observation, the standard deviation values for the three courses are in the same general range. Also, the Two-Sample Mann-Whitney hypothesis test was used to make all pair-wise comparisons of the medians of the Means of Lot Means results for each course. The same test was used to make pair-wise comparisons of the medians of the Lot Standard Deviations. The Mann-Whitney test does not require the data to come from normally distributed populations. It assumes that the populations of interest have the same shape and that the populations are independent. The results of the Mann-Whitney tests are shown in Table 7.13.

The medians of the Lot Means for Intermediate and Surface courses are different at the 0.041 significance level. The medians of the Lot Std Devs show more evidence of differing between courses, with the Base and Surface courses different at the 0.015 level and the Intermediate and Surface courses different at the 0.056 level. The results support the use of different AC specification limits for different courses.

| Num         | nber      | Total Nu | umber of   | Mea        | n of *    | Std Dev | viation** |  |  |
|-------------|-----------|----------|------------|------------|-----------|---------|-----------|--|--|
| Project     | JMF       | Lots     | Tests      | All Tests  | Lot Means | Project | Lot       |  |  |
| Base Course |           |          |            |            |           |         |           |  |  |
| P01         | J01       | 8        | 22         | 0.0673     | 0.0398    | 0.2318  | 0.1933    |  |  |
| P01         | J06       | 3        | 9          | 0.0978     | 0.0942    | 0.2163  | 0.2512    |  |  |
| P01         | J18       | 33       | 82         | -0.0480    | -0.0564   | 0.2435  | 0.2237    |  |  |
| P01         | J21       | 15       | 27         | 0.1085     | 0.1324    | 0.2574  | 0.3360    |  |  |
| P02         | J17       | 6        | 17         | -0.0147    | 0.0022    | 0.2983  | 0.3225    |  |  |
| P02         | J28       | 13       | 30         | 0.0383     | 0.0404    | 0.2475  | 0.1832    |  |  |
| P24         | J57       | 6        | 12         | 0.1375     | 0.1375    | 0.1110  | 0.0517    |  |  |
| P26         | J45       | 4        | 12         | 0.0620     | 0.0423    | 0.3723  | 0.3406    |  |  |
| P27         | J66       | 11       | 11         | 0.0455     | 0.0455    | 0.2035  | —         |  |  |
| P28         | J47       | 10       | 14         | -0.0250    | -0.0385   | 0.2407  | 0.2193    |  |  |
| Total/A     | verage    | 109      | 236        | 0.0469     | 0.0439    | 0.2422  | 0.2357    |  |  |
|             |           |          | Intermedia | ate Course | e         |         |           |  |  |
| P01         | J02       | 4        | 12         | 0.1217     | 0.1150    | 0.1734  | 0.1915    |  |  |
| P01         | J10       | 18       | 39         | 0.0036     | 0.0162    | 0.2016  | 0.1559    |  |  |
| P01         | J23       | 6        | 12         | 0.1050     | 0.0936    | 0.3111  | 0.4165    |  |  |
| P02         | J04       | 14       | 30         | 0.1290     | 0.1815    | 0.2260  | 0.2131    |  |  |
| P02         | J09       | 18       | 34         | 0.0218     | 0.1190    | 0.2479  | 0.2058    |  |  |
| P04         | J08       | 11       | 21         | 0.1800     | 0.1959    | 0.3053  | 0.2916    |  |  |
| P05         | J27       | 8        | 15         | -0.1187    | -0.1200   | 0.1290  | 0.1494    |  |  |
| P10         | J31       | 41       | 77         | 0.0129     | 0.0222    | 0.2583  | 0.2984    |  |  |
| P10         | J37       | 12       | 22         | 0.0250     | 0.0396    | 0.2067  | 0.1764    |  |  |
| P10         | J82       | 8        | 15         | -0.0313    | -0.0238   | 0.1963  | 0.1291    |  |  |
| P17         | J22       | 6        | 11         | 0.0036     | -0.0175   | 0.2648  | 0.2322    |  |  |
| P21         | J34       | 3        | 8          | 0.1025     | 0.0467    | 0.1861  | 0.1294    |  |  |
| P24         | J51       | 15       | 23         | 0.0287     | 0.0457    | 0.1627  | 0.1806    |  |  |
| P25         | J29       | 7        | 12         | -0.1567    | -0.1614   | 0.2091  | 0.2127    |  |  |
| P27         | J53       | 16       | 19         | -0.0000    | 0.0134    | 0.2079  | 0.1566    |  |  |
| P27         | J60       | 15       | 15         | 0.2613     | 0.2613    | 0.2445  | _         |  |  |
| P28         | J42       | 13       | 15         | 0.0847     | 0.0877    | 0.1950  | 0.1241    |  |  |
| P32         | J76       | 12       | 43         | 0.0935     | 0.0920    | 0.2078  | 0.1813    |  |  |
| P33         | J73       | 8        | 25         | 0.0520     | 0.0783    | 0.2283  | 0.2585    |  |  |
| Total/A     | verage    | 235      | 448        | 0.0483     | 0.0571    | 0.2190  | 0.2057    |  |  |
|             | Continued |          |            |            |           |         |           |  |  |

## Table 7.12. Summary of AC Test Results for Each Project

\* All Tests: the mean of all individual test results on the project Lot Means: the mean of all the individual lot means on the project

\*\* **Project:** the unbiased standard deviation estimate of all individual test results on the project **Lot:** the average of the unbiased standard deviation estimates for all lots on the project

| Num     | nber      | Total Nu | Imber of | Mean of * |           | Std Deviation** |        |  |
|---------|-----------|----------|----------|-----------|-----------|-----------------|--------|--|
| Project | JMF       | Lots     | Tests    | All Tests | Lot Means | Project         | Lot    |  |
|         |           |          | Surface  | Course    |           |                 |        |  |
| P01     | J07       | 9        | 30       | -0.0243   | -0.0212   | 0.1808          | 0.1811 |  |
| P01     | J19       | 14       | 18       | 0.0828    | 0.1007    | 0.1435          | 0.1462 |  |
| P02     | J05       | 6        | 8        | -0.0050   | -0.0117   | 0.1506          | 0.0798 |  |
| P02     | J13       | 14       | 18       | -0.0572   | -0.0318   | 0.2949          | 0.1130 |  |
| P02     | J15       | 6        | 18       | -0.0122   | 0.0501    | 0.2058          | 0.1750 |  |
| P04     | J14       | 5        | 17       | 0.0618    | 0.0575    | 0.1937          | 0.2051 |  |
| P05     | J25       | 8        | 8        | -0.1313   | -0.1313   | 0.1884          | _      |  |
| P05     | J40       | 5        | 9        | -0.1344   | -0.1180   | 0.1756          | 0.1726 |  |
| P06     | J24       | 5        | 15       | 0.0647    | 0.0647    | 0.1732          | 0.1438 |  |
| P07     | J30       | 19       | 40       | -0.0940   | -0.0971   | 0.1463          | 0.1034 |  |
| P09     | J35       | 3        | 9        | -0.0178   | -0.0178   | 0.1492          | 0.1349 |  |
| P09     | J83       | 3        | 8        | -0.0413   | -0.0333   | 0.1954          | 0.1891 |  |
| P10     | J12       | 13       | 19       | -0.0374   | -0.0373   | 0.2781          | 0.2083 |  |
| P11     | J41       | 4        | 10       | 0.0710    | 0.0721    | 0.1731          | 0.1190 |  |
| P12     | J38       | 6        | 14       | 0.0536    | 0.0676    | 0.1820          | 0.1592 |  |
| P13     | J03       | 8        | 16       | -0.0100   | -0.0458   | 0.2735          | 0.3268 |  |
| P13     | J43       | 8        | 19       | -0.0011   | -0.0020   | 0.1554          | 0.1305 |  |
| P14     | J16       | 13       | 32       | -0.1769   | -0.1827   | 0.2113          | 0.1937 |  |
| P16     | J20       | 3        | 9        | -0.1811   | -0.1811   | 0.2351          | 0.2103 |  |
| P18     | J48       | 7        | 12       | 0.1117    | 0.1164    | 0.2138          | 0.1701 |  |
| P19     | J49       | 7        | 20       | -0.0775   | -0.0788   | 0.2602          | 0.2105 |  |
| P20     | J50       | 17       | 46       | 0.0202    | 0.0484    | 0.1923          | 0.1648 |  |
| P21     | J39       | 6        | 15       | 0.0007    | -0.0026   | 0.1283          | 0.1078 |  |
| P22     | J54       | 3        | 12       | 0.0467    | 0.0647    | 0.0845          | 0.0609 |  |
| P24     | J56       | 18       | 40       | 0.0000    | 0.0759    | 0.2507          | 0.2161 |  |
| P24     | J64       | 7        | 13       | 0.1431    | 0.1443    | 0.0574          | 0.0473 |  |
| P24     | J67       | 6        | 10       | 0.0590    | 0.1667    | 0.6117          | 0.0682 |  |
| P25     | J36       | 6        | 10       | 0.0570    | 0.0458    | 0.2081          | 0.2906 |  |
| P26     | J52       | 30       | 58       | -0.0621   | -0.0525   | 0.1452          | 0.1211 |  |
| P26     | J58       | 12       | 13       | -0.0031   | 0.0050    | 0.1707          | 0.2481 |  |
| P26     | J62       | 9        | 31       | 0.0145    | 0.0082    | 0.1791          | 0.1741 |  |
| P26     | J68       | 4        | 13       | -0.0970   | -0.0879   | 0.4339          | 0.4153 |  |
| P26     | J69       | 18       | 53       | 0.0029    | -0.0201   | 0.1949          | 0.1531 |  |
| P27     | J55       | 5        | 15       | 0.1287    | 0.1287    | 0.1947          | 0.2122 |  |
| P27     | J61       | 9        | 9        | -0.0589   | -0.0589   | 0.1290          | —      |  |
| P27     | J71       | 9        | 27       | 0.0559    | 0.0597    | 0.1621          | 0.1882 |  |
| P28     | J39       | 9        | 24       | 0.0429    | 0.0149    | 0.1542          | 0.1486 |  |
| P29     | J59       | 9        | 26       | -0.0458   | -0.0494   | 0.1427          | 0.1296 |  |
| P30     | J65       | 4        | 8        | -0.0100   | 0.0000    | 0.0905          | 0.1000 |  |
| P32     | J46       | 31       | 41       | -0.0220   | -0.0157   | 0.1792          | 0.1736 |  |
| P32     | J72       | 8        | 34       | 0.0706    | 0.0773    | 0.1740          | 0.1819 |  |
| P32     | J79       | 24       | 96       | 0.1139    | 0.1106    | 0.1622          | 0.1253 |  |
| P33     | J75       | 10       | 10       | -0.0150   | -0.0150   | 0.1885          | —      |  |
|         | Continued |          |          |           |           |                 |        |  |

## Table 7.12. Summary of AC Test Results for Each Project (continued)

| Num     | nber   | Total Nu | Total Number of Mean of * Std Devi |           | Mean of * |         | /iation** |
|---------|--------|----------|------------------------------------|-----------|-----------|---------|-----------|
| Project | JMF    | Lots     | Tests                              | All Tests | Lot Means | Project | Lot       |
| P33     | J77    | 6        | 22                                 | 0.0973    | 0.0988    | 0.2472  | 0.2295    |
| P33     | J78    | 4        | 13                                 | 0.0492    | 0.0419    | 0.3541  | 0.3556    |
| P34     | J62    | 7        | 28                                 | -0.0232   | -0.0225   | 0.2043  | 0.1496    |
| P34     | J80    | 7        | 12                                 | -0.0058   | -0.0286   | 0.1030  | 0.0806    |
| P34     | J81    | 7        | 13                                 | 0.0923    | 0.0971    | 0.2117  | 0.2600    |
| P35     | J32    | 6        | 14                                 | -0.0507   | -0.0294   | 0.1513  | 0.1347    |
| P35     | J38    | 16       | 36                                 | 0.0536    | 0.0495    | 0.1249  | 0.1171    |
| Total/A | verage | 472      | 1091                               | 0.0020    | 0.0079    | 0.1962  | 0.1708    |

Table 7.12. Summary of AC Test Results for Each Project (continued)

\* All Tests: the mean of all individual test results on the project Lot Means: the mean of all the individual lot means on the project

\*\* **Project:** the unbiased standard deviation estimate of all individual test results on the project **Lot:** the average of the unbiased standard deviation estimates for all lots on the project

| Course       | No. of<br>Lots | Median of Lot<br>Means | P-Value* | No. of<br>Lots | Median of<br>Lot Std Devs | P-Value* |
|--------------|----------------|------------------------|----------|----------------|---------------------------|----------|
| Base         | 10             | 0.0413                 | 0.697    | 9              | 0.2237                    | 0.143    |
| Intermediate | 19             | 0.0467                 |          | 18             | 0.1864                    |          |
|              |                |                        |          |                |                           |          |
| Base         | 10             | 0.0413                 | 0.317    | 9              | 0.2237                    | 0.015    |
| Surface      | 50             | -0.0010                |          | 47             | 0.1648                    |          |
|              |                |                        |          |                |                           |          |
| Intermediate | 19             | 0.0467                 | 0.041    | 18             | 0.1864                    | 0.056    |
| Surface      | 50             | -0.0010                |          | 47             | 0.1648                    |          |
|              |                |                        |          |                |                           |          |

\* Values in bold are statistically significantly different at the  $\alpha = 0.05$  level.

**Base Course.** Table 7.14 shows Lot standard deviation results for Base course (from Table 7.12), but with the projects sorted from the smallest to largest Lot (i.e., within-lot) standard deviations. The projects are listed in increasing order of the Lot standard deviation to facilitate selecting a typical process standard deviation. The table also shows the total number of lots and tests for all AC projects, the averages for both the Project standard deviation values and for the Lot standard deviation values, and percentiles based on ranked order for both the Project and Lot standard deviation values.

SCDOT can use Table 7.14 to assist in selecting the "typical" variability to use to establish specification limits. As noted in the discussion above, there is no single "correct" way to establish this value. A subjective decision must be made regarding the standard deviation to select. The percentile values shown in the table should assist in making the decision. To get a "picture" of the results in Table 7.14, Figure 7.5 shows the empirical cumulative distribution function (CDF) for the Lot standard deviation values.

As the reference lines show, there appears to be a natural break point at around a standard deviation of 0.25, which corresponds to approximately the  $67^{th}$  percentile on the CDF plot. This would seem to be a logical choice for the process standard deviation. However, note that due to the large gap between values, the  $70^{th}$  percentile (see Table 7.14), at 0.294, is quite a bit larger than 0.25. This difference is due to the relatively small number of projects and the relatively large gap between standard deviation values of 0.2512 and 0.3225. Somewhere in the range 0.25 to 0.295 would seem to be a logical choice for the process standard deviation.

| Num               | nber | Total Nu | mber of | Mea       | n of *    | Std Deviation* |        |
|-------------------|------|----------|---------|-----------|-----------|----------------|--------|
| Project           | JMF  | Lots     | Tests   | All Tests | Lot Means | Project        | Lot    |
| P27               | J66  | 11       | 11      | 0.0455    | 0.0455    | 0.2035         | —      |
| P24               | J57  | 6        | 12      | 0.1375    | 0.1375    | 0.1110         | 0.0517 |
| P02               | J28  | 13       | 30      | 0.0383    | 0.0404    | 0.2475         | 0.1832 |
| P01               | J01  | 8        | 22      | 0.0673    | 0.0398    | 0.2318         | 0.1933 |
| P28               | J47  | 10       | 14      | -0.0250   | -0.0385   | 0.2407         | 0.2193 |
| P01               | J18  | 33       | 82      | -0.0480   | -0.0564   | 0.2435         | 0.2237 |
| P01               | J06  | 3        | 9       | 0.0978    | 0.0942    | 0.2163         | 0.2512 |
| P02               | J17  | 6        | 17      | -0.0147   | 0.0022    | 0.2983         | 0.3225 |
| P01               | J21  | 15       | 27      | 0.1085    | 0.1324    | 0.2574         | 0.3360 |
| P26               | J45  | 4        | 12      | 0.0620    | 0.0423    | 0.3723         | 0.3406 |
| Total/Ave<br>rage |      | 109      | 236     | 0.0469    | 0.0439    | 0.2422         | 0.2357 |
|                   |      |          |         |           | 50%       | 0.2421         | 0.2237 |
|                   |      |          |         |           | 60%       | 0.2451         | 0.2457 |
|                   |      |          |         |           | 70%       | 0.2505         | 0.2940 |
|                   |      |          |         |           | 80%       | 0.2656         | 0.3279 |
|                   |      |          |         |           | 90%       | 0.3057         | 0.3369 |

 Table 7.14. Summary of AC Test Results for Each Base Course Project

\* All Tests: the mean of all individual test results on the project Lot Means: the mean of all the individual lot means on the project

\*\* **Project:** the unbiased standard deviation estimate of all individual test results on the project **Lot:** the average of the unbiased standard deviation estimates for all lots on the project



Figure 7.5. CDF for the Lot Standard Deviations for AC for Base Course Projects

**Intermediate Course.** Table 7.15 shows Lot standard deviation results for Intermediate course (from Table 7.12), but with the projects sorted from the smallest to largest Lot (i.e., within-lot) standard deviations. The projects are listed in increasing order of the Lot standard deviation to facilitate selecting a typical process standard deviation. The table also shows the total number of lots and tests for all AC projects, the averages for both the Project standard deviation values and for the Lot standard deviation values, and percentiles based on ranked order for both the Project and Lot standard deviation values.

SCDOT can use Table 7.15 to assist in selecting the "typical" variability to use to establish specification limits. As noted in the discussion above, there is no single "correct" way to establish this value. A subjective decision must be made regarding the standard deviation to select. The percentile values shown in the table should assist in making the decision. To get a "picture" of the results in Table 7.15, Figure 7.6 shows the empirical cumulative distribution function (CDF) for the Lot standard deviation values.

There is not as obvious a natural break point as in Figure 7.5, but the reference lines shown represent the 70<sup>th</sup>, 75<sup>th</sup>, and 80<sup>th</sup> percentiles and the corresponding standard deviations between 0.21 and 0.26. Given the CDF, somewhere in this range would seem to be a logical choice for the process standard deviation.

| Number  |           | Total Nu | umber of | Mea       | n of *    | Std Dev | viation* |
|---------|-----------|----------|----------|-----------|-----------|---------|----------|
| Project | JMF       | Lots     | Tests    | All Tests | Lot Means | Project | Lot      |
| P27     | J60       | 15       | 15       | 0.2613    | 0.2613    | 0.2445  |          |
| P28     | J42       | 13       | 15       | 0.0847    | 0.0877    | 0.1950  | 0.1241   |
| P10     | J82       | 8        | 15       | -0.0313   | -0.0238   | 0.1963  | 0.1291   |
| P21     | J34       | 3        | 8        | 0.1025    | 0.0467    | 0.1861  | 0.1294   |
| P05     | J27       | 8        | 15       | -0.1187   | -0.1200   | 0.1290  | 0.1494   |
| P01     | J10       | 18       | 39       | 0.0036    | 0.0162    | 0.2016  | 0.1559   |
| P27     | J53       | 16       | 19       | -0.0000   | 0.0134    | 0.2079  | 0.1566   |
| P10     | J37       | 12       | 22       | 0.0250    | 0.0396    | 0.2067  | 0.1764   |
| P24     | J51       | 15       | 23       | 0.0287    | 0.0457    | 0.1627  | 0.1806   |
| P32     | J76       | 12       | 43       | 0.0935    | 0.0920    | 0.2078  | 0.1813   |
| P01     | J02       | 4        | 12       | 0.1217    | 0.1150    | 0.1734  | 0.1915   |
| P02     | J09       | 18       | 34       | 0.0218    | 0.1190    | 0.2479  | 0.2058   |
| P25     | J29       | 7        | 12       | -0.1567   | -0.1614   | 0.2091  | 0.2127   |
| P02     | J04       | 14       | 30       | 0.1290    | 0.1815    | 0.2260  | 0.2131   |
| P17     | J22       | 6        | 11       | 0.0036    | -0.0175   | 0.2648  | 0.2322   |
| P33     | J73       | 8        | 25       | 0.0520    | 0.0783    | 0.2283  | 0.2585   |
| P04     | J08       | 11       | 21       | 0.1800    | 0.1959    | 0.3053  | 0.2916   |
| P10     | J31       | 41       | 77       | 0.0129    | 0.0222    | 0.2583  | 0.2984   |
| P01     | J23       | 6        | 12       | 0.1050    | 0.0936    | 0.3111  | 0.4165   |
| Tota    | I/Average | 235      | 448      | 0.0483    | 0.0571    | 0.2190  | 0.2057   |
|         |           |          |          |           | 50%       | 0.2079  | 0.1864   |
|         |           |          |          |           | 60%       | 0.2226  | 0.2072   |
|         |           |          |          |           | 70%       | 0.2380  | 0.2131   |
|         |           |          |          |           | 80%       | 0.2521  | 0.2480   |
|         |           |          |          |           | 90%       | 0.2729  | 0.2936   |

### Table 7.15. Summary of AC Test Results for Each Intermediate Course Project

\* All Tests: the mean of all individual test results on the project Lot Means: the mean of all the individual lot means on the project

\*\* **Project:** the unbiased standard deviation estimate of all individual test results on the project **Lot:** the average of the unbiased standard deviation estimates for all lots on the project



Figure 7.6. CDF for the Lot Standard Deviations for AC for Intermediate Course Projects

**Surface Course.** Table 7.16 shows Lot standard deviation results for Surface course (from Table 7.12), but with the projects sorted from the smallest to largest Lot (i.e., within-lot) standard deviations. The projects are listed in increasing order of the Lot standard deviation to facilitate selecting a typical process standard deviation. The table also shows the total number of lots and tests for all AC projects, the averages for both the Project standard deviation values and for the Lot standard deviation values, and percentiles based on ranked order for both the Project and Lot standard deviation values.

SCDOT can use Table 7.16 to assist in selecting the "typical" variability to use to establish specification limits. As noted in the discussion above, there is no single "correct" way to establish this value. A subjective decision must be made regarding the standard deviation to select. The percentile values shown in the table should assist in making the decision. To get a "picture" of the results in Table 7.16, Figure 7.7 shows the empirical cumulative distribution function (CDF) for the Lot standard deviation values.

There is more than one potential break point in Figure 7.7. The reference lines shown represent approximately the 72<sup>nd</sup> and 85<sup>th</sup> percentiles and the corresponding standard deviations of 0.194 and 0.216, respectively. From Table 7.16, the 80<sup>th</sup> percentile with a standard deviation of 0.21 would be another possibility. SCDOT will need to make a subjective decision regarding the typical standard deviation to use to represent Surface course paving. Given the CDF, somewhere between 0.195 and 0.215 would seem to be a logical choice for the process standard deviation.

| Num       | Number Total Number of |      | mber of | Mean of * |           | Std Deviation* |        |  |
|-----------|------------------------|------|---------|-----------|-----------|----------------|--------|--|
| Project   | JMF                    | Lots | Tests   | All Tests | Lot Means | Project        | Lot    |  |
| P05       | J25                    | 8    | 8       | -0.1313   | -0.1313   | 0.1884         | —      |  |
| P27       | J61                    | 9    | 9       | -0.0589   | -0.0589   | 0.1290         | —      |  |
| P33       | J75                    | 10   | 10      | -0.0150   | -0.0150   | 0.1885         | _      |  |
| P24       | J64                    | 7    | 13      | 0.1431    | 0.1443    | 0.0574         | 0.0473 |  |
| P22       | J54                    | 3    | 12      | 0.0467    | 0.0647    | 0.0845         | 0.0609 |  |
| P24       | J67                    | 6    | 10      | 0.0590    | 0.1667    | 0.6117         | 0.0682 |  |
| P02       | J05                    | 6    | 8       | -0.0050   | -0.0117   | 0.1506         | 0.0798 |  |
| P34       | J80                    | 7    | 12      | -0.0058   | -0.0286   | 0.1030         | 0.0806 |  |
| P30       | J65                    | 4    | 8       | -0.0100   | 0.0000    | 0.0905         | 0.1000 |  |
| P07       | J30                    | 19   | 40      | -0.0940   | -0.0971   | 0.1463         | 0.1034 |  |
| P21       | J39                    | 6    | 15      | 0.0007    | -0.0026   | 0.1283         | 0.1078 |  |
| P02       | J13                    | 14   | 18      | -0.0572   | -0.0318   | 0.2949         | 0.1130 |  |
| P35       | J38                    | 16   | 36      | 0.0536    | 0.0495    | 0.1249         | 0.1171 |  |
| P11       | J41                    | 4    | 10      | 0.0710    | 0.0721    | 0.1731         | 0.1190 |  |
| P26       | J52                    | 30   | 58      | -0.0621   | -0.0525   | 0.1452         | 0.1211 |  |
| P32       | J79                    | 24   | 96      | 0.1139    | 0.1106    | 0.1622         | 0.1253 |  |
| P29       | J59                    | 9    | 26      | -0.0458   | -0.0494   | 0.1427         | 0.1296 |  |
| P13       | J43                    | 8    | 19      | -0.0011   | -0.0020   | 0.1554         | 0.1305 |  |
| P35       | J32                    | 6    | 14      | -0.0507   | -0.0294   | 0.1513         | 0.1347 |  |
| P09       | J35                    | 3    | 9       | -0.0178   | -0.0178   | 0.1492         | 0.1349 |  |
| P06       | J24                    | 5    | 15      | 0.0647    | 0.0647    | 0.1732         | 0.1438 |  |
| P01       | J19                    | 14   | 18      | 0.0828    | 0.1007    | 0.1435         | 0.1462 |  |
| P28       | J39                    | 9    | 24      | 0.0429    | 0.0149    | 0.1542         | 0.1486 |  |
| P34       | J62                    | 7    | 28      | -0.0232   | -0.0225   | 0.2043         | 0.1496 |  |
| P26       | J69                    | 18   | 53      | 0.0029    | -0.0201   | 0.1949         | 0.1531 |  |
| P12       | J38                    | 6    | 14      | 0.0536    | 0.0676    | 0.1820         | 0.1592 |  |
| P20       | J50                    | 17   | 46      | 0.0202    | 0.0484    | 0.1923         | 0.1648 |  |
| P18       | J48                    | 7    | 12      | 0.1117    | 0.1164    | 0.2138         | 0.1701 |  |
| P05       | J40                    | 5    | 9       | -0.1344   | -0.1180   | 0.1756         | 0.1726 |  |
| P32       | J46                    | 31   | 41      | -0.0220   | -0.0157   | 0.1792         | 0.1736 |  |
| P26       | J62                    | 9    | 31      | 0.0145    | 0.0082    | 0.1791         | 0.1741 |  |
| P02       | J15                    | 6    | 18      | -0.0122   | 0.0501    | 0.2058         | 0.1750 |  |
| P01       | J07                    | 9    | 30      | -0.0243   | -0.0212   | 0.1808         | 0.1811 |  |
| P32       | J72                    | 8    | 34      | 0.0706    | 0.0773    | 0.1740         | 0.1819 |  |
| P27       | J71                    | 9    | 27      | 0.0559    | 0.0597    | 0.1621         | 0.1882 |  |
| P09       | J83                    | 3    | 8       | -0.0413   | -0,0333   | 0.1954         | 0,1891 |  |
| P14       | J16                    | 13   | 32      | -0.1769   | -0.1827   | 0.2113         | 0.1937 |  |
| P04       | J14                    | 5    | 17      | 0.0618    | 0.0575    | 0.1937         | 0.2051 |  |
| P10       | J12                    | 13   | 19      | -0.0374   | -0.0373   | 0.2781         | 0.2083 |  |
| P16       | J20                    | 3    | .0      | -0.1811   | -0.1811   | 0.2351         | 0.2103 |  |
| P19       | J49                    | 7    | 20      | -0.0775   | -0.0788   | 0.2602         | 0.2105 |  |
| P27       | J55                    | 5    | 15      | 0.1287    | 0.1287    | 0.1947         | 0.2122 |  |
|           |                        | v    |         |           | 511207    | 0.1017         | 012122 |  |
| Continued |                        |      |         |           |           |                |        |  |

| Table 7.16. Summary of AC Test Results for Each Surface Course Pro | ject |
|--|------|
|--|------|

| Num               | ber | Total Nu | umber of | of Mean of * |           | Std Dev | viation* |
|-------------------|-----|----------|----------|--------------|-----------|---------|----------|
| Project           | JMF | Lots     | Tests    | All Tests    | Lot Means | Project | Lot      |
| P24               | J56 | 18       | 40       | 0.0000       | 0.0759    | 0.2507  | 0.2161   |
| P33               | J77 | 6        | 22       | 0.0973       | 0.0988    | 0.2472  | 0.2295   |
| P26               | J58 | 12       | 13       | -0.0031      | 0.0050    | 0.1707  | 0.2481   |
| P34               | J81 | 7        | 13       | 0.0923       | 0.0971    | 0.2117  | 0.2600   |
| P25               | J36 | 6        | 10       | 0.0570       | 0.0458    | 0.2081  | 0.2906   |
| P13               | J03 | 8        | 16       | -0.0100      | -0.0458   | 0.2735  | 0.3268   |
| P33               | J78 | 4        | 13       | 0.0492       | 0.0419    | 0.3541  | 0.3556   |
| P26               | J68 | 4        | 13       | -0.0970      | -0.0879   | 0.4339  | 0.4153   |
| Total/Ave<br>rage |     | 472      | 1091     | 0.0020       | 0.0079    | 0.1962  | 0.1708   |
|                   |     |          |          |              | 50%       | 0.1800  | 0.1648   |
|                   |     |          |          |              | 60%       | 0.1929  | 0.1746   |
|                   |     |          |          |              | 70%       | 0.2048  | 0.1900   |
|                   |     |          |          |              | 80%       | 0.2181  | 0.2105   |
|                   |     |          |          |              | 90%       | 0.2740  | 0.2529   |

Table 7.16. Summary of AC Test Results for Each Surface Course Project (continued)

\* All Tests: the mean of all individual test results on the project Lot Means: the mean of all the individual lot means on the project

\*\* **Project:** the unbiased standard deviation estimate of all individual test results on the project **Lot:** the average of the unbiased standard deviation estimates for all lots on the project





**PWL Values for the AC Projects.** The AC projects did not exhibit the same concern that was found with the Density projects where many of the projects had relatively low average PWL values. A different problem with the AC projects was that many of the projects did not have sufficient sample sizes to calculate a PWL value for the lots. There must be at least 3 test results for a lot to be able to estimate the PWL value for the lot. Rather than to combine lots, which is what would have been done in the field to determine the PWL to use for determining the payment factor, lots that had at least 3 tests were evaluated to determine their estimated PWL values.

For Base course, only 6 of 42 lots had PWL values less than the 90 that was required for full payment. For Intermediate course, only 8 of 42 lots had PWL values less than the 90. The Surface course requirements were a little more difficult to meet, with 39 of 207 lots having PWL values less than 90. For Base course, 1 of 7 projects had average PWL values less than 90. For Surface course, 10 of 37 projects had average PWL values less than 90. For Surface course, 10 of 37 projects had average PWL values less than 90. For Surface course, 10 of 37 projects had average PWL values less than 90. For Surface course, 10 of 37 projects had average PWL values less than 90. For Surface course, 10 of 37 projects had average PWL values less than 90. For Surface course, 10 of 37 projects had average PWL values less than 90. For Surface course, 10 of 37 projects had average PWL values less than 90. For Surface course, 10 of 37 projects had average PWL values less than 90. For Surface course, 10 of 37 projects had average PWL values less than 90. For Surface course, 10 of 37 projects had average PWL values less than 90. For Surface course, 10 of 37 projects had average PWL values less than 90. For Surface course, 10 of 37 projects had average PWL values less than 90. For Surface course, 10 of 37 projects had average PWL values less than 90. For Surface course, 10 of 37 projects had average PWL values less than 90. For Surface course, 10 of 37 projects had average PWL values less than 90. For Surface course, 10 of 37 projects had average PWL values less than 90. For Surface course, 10 of 37 projects had average PWL values less than 90. For Surface course, 10 of 37 projects had average PWL values less than 90. For Surface course, 10 of 37 projects had average PWL values less than 90. For Surface course, 10 of 37 projects had average PWL values less than 90. For Surface course, 10 of 37 projects had average PWL values less than 90. For Surface course, 10 of 37 projects had average PWL values less than 90. For Surface course, 10 of

## Air Voids

**Comparing Courses.** The specifications for AV had one set of allowable tolerances, 1.15%, for Intermediate, and Surface courses. AV values were not determined for Base course mixes. To evaluate whether or not different tolerances might be warranted for Intermediate and Surface courses, the variances of the two courses were compared statistically using the *F*-test and Levene's test. The *F*-test assumes that the data are from normal distributions, whereas Levene's test applies for any continuous distribution. Table 7.17 shows the results of the comparison.

| Table 7.17 | . Summary of AV | / Comparisons | among Courses |
|------------|-----------------|---------------|---------------|
|------------|-----------------|---------------|---------------|

| Course       | No. of<br>Tests | St Dev | P-value*<br><i>F</i> -test | P-value*<br>Levene's |  |
|--------------|-----------------|--------|----------------------------|----------------------|--|
| Intermediate | 406             | 0.5907 | 0.025                      | 0 1 1 1              |  |
| Surface      | 935             | 0.6464 | 0.035                      | 0.141                |  |

\* Values in bold are statistically significantly different at the  $\alpha = 0.05$  level.

The results in Table 7.17 show that the *F*-test, with a P-value of 0.035, concludes that the variabilities for Intermediate and Surface courses are likely not the same. Levene's test, with a P-value of 0.141, would not conclude that the variabilities should be considered different. To further investigate the variabilities, Figure 7.8 shows the standard deviation along with its 95% confidence interval for each course. While the standard deviation result for Surface course is outside the upper confidence limit for the Intermediate course standard deviation, there is still quite a bit of overlap between the two confidence intervals. Therefore, there is some evidence to conclude that the AV variability is less for Intermediate course than it is for Surface course. There is also contradictory evidence to support using the same variability to represent both

courses. While the decision must be made by SCDOT, for this report, it has been assumed that it is reasonable to treat the two courses as having similar variabilities.



# Figure 7.8. Comparison of AV Standard Deviations for Intermediate and Surface Courses

**Comparing Mix Types within Course.** The next question to consider is whether it is appropriate to use the same specification tolerances for all mix types within a given course. When establishing the allowable tolerances it is the standard deviation that is most important.

**Intermediate Course Mixes.** Table 7.18 shows the results of comparisons among the AV variabilities for the different types of Intermediate course mixes. The results, with Bartlett's test having a P-value of 0.693 and Levene's test having a P-value of 0.554, show no evidence that the standard deviations are different for the different mix types. Figure 7.9 shows the standard deviation along with its 95% confidence interval for each Intermediate course mix type.

 Table 7.18. Summary of AV Comparisons of Intermediate Course Mix Types

| Міх Туре       | No. of<br>Tests | St Dev | P-value*<br>Bartlett's | P-value*<br>Levene's |
|----------------|-----------------|--------|------------------------|----------------------|
| Binder 1       | 18              | 0.5291 |                        |                      |
| Intermediate B | 198             | 0.5344 | 0.693                  | 0.554                |
| Intermediate C | 190             | 0.5673 |                        |                      |

\* Values in bold are statistically significantly different at the  $\alpha = 0.05$  level.



Figure 7.9 Comparison of AC Standard Deviations for Each Intermediate Course Mix Type

**Surface Course Mixes.** Table 7.19 shows the results of comparisons among the AV variabilities for the different types of Surface course mixes. The results show clearly that the standard deviations are not equal for all 10 mix types. Figure 7.10 shows the standard deviation along with its 95% confidence interval for each Surface course mix type.

| Міх Туре   | No. of<br>Tests | St Dev | P-value*<br>Bartlett's | P-value*<br>Levene's |  |  |  |
|------------|-----------------|--------|------------------------|----------------------|--|--|--|
| Surface 1C | 16              | 0.5805 |                        |                      |  |  |  |
| Surface 1D | 15              | 0.4212 |                        |                      |  |  |  |
| Surface 1R | 17              | 0.5145 |                        |                      |  |  |  |
| Surface 3  | 40              | 0.5004 |                        |                      |  |  |  |
| Surface 4  | 19              | 0.6232 | 0.011                  | 0.012                |  |  |  |
| Surface A  | 230             | 0.6231 | 0.011                  | 0.012                |  |  |  |
| Surface B  | 116             | 0.5145 |                        |                      |  |  |  |
| Surface C  | 393             | 0.6720 |                        |                      |  |  |  |
| Surface CM | 26              | 0.5952 |                        |                      |  |  |  |
| Surface D  | 63              | 0.6986 |                        |                      |  |  |  |

Table 7.19. Summary of AV Comparisons of Surface Course Mix Types

\* Values in bold are statistically significantly different at the  $\alpha = 0.05$  level.



Figure 7.10 Comparison of AC Standard Deviations for Each Surface Course Mix Type

It must be noted that the above analysis can be thought of as a quick simplification. For example, many of the mix types with the smaller standard deviations also had the smallest number of data points. With a limited number of projects there is likely to be less variability when the data are combined than there would be when many projects were combined. In fact, the Surface 1C, 1D, 1R, 3, and 4 mixes each appeared on only one project. The effect of combining several projects in the other Surface mix types will be addressed when the individual average Lot standard deviation and average project standard deviations are analyzed.

**Caveat.** None of the standard deviation values shown in Tables 7.17-7.19 are the appropriate standard deviation to use to represent the process standard deviation for AV. These calculations were done simply for exploratory purposes. Aggregating the data as in these tables is not appropriate for establishing specification limits since the specification limits are based on lot-by-lot acceptance, or at least on acceptance of a project.

**Typical Variability Values for AV.** As noted above, since the SCDOT specification is based on lot-by-lot acceptance, the AV variability that is used to evaluate the specification limits must be that which is appropriate for a typical lot. To determine this, the individual standard deviation values for each lot were calculated and then these lot standard deviations were averaged to get the "within-lot" standard deviation for each project. This was done using the procedure that is described for density in Chapter 6. As noted in Chapter 6, this within-lot standard deviation does not take into consideration any target miss variability that may be present.

To provide the option to consider using the total project as the payment lot, the total project AV standard deviation was also calculated for each project. As noted above, this "project" standard deviation could also be used as one way of trying to incorporate any target miss variability that might be present in the contractor's process.

Appendix B includes the necessary calculations for each project for which AV data were obtained. These calculations were used to arrive at the project standard deviations that were used to establish the typical process variability for AV.

**Projects with Multiple JMFs.** Before compiling all of the within-lot and project variabilities, a decision had to be made regarding how to deal with projects on which more than one JMF was used for the same mix type and course. Should each JMF be treated as a separate project, or should the multiple JMF results be combined together as one project? To help make this decision, the projects with multiple JMFs were examined. Table 7.20 shows the projects (extracted from Tables 7.1-7.5) that had multiple JMFs for the same mix type.

Only 1 out of 10 multi-mix design projects showed a difference in variability. Also, in the project data a new lot was established in nearly every case that the JMF changed. This would argue in favor of treating the JMFs as separate projects when determining the within-lot standard deviations.

However, if a total project is being used as the payment lot, then the data from the multiple JMFs would be combined when calculating the standard deviation to use for payment determination. This would argue in favor of combining the separate JMFs into a single project. For consistency in presentation and in comparing results, it was decided to treat the separate JMFs as separate projects when calculating standard deviations and when presenting the results.

| Project             | JMF | No. of<br>Lots | No. of<br>Tests | St Dev | <i>F</i> -Test<br>P-value* |  |  |  |  |  |
|---------------------|-----|----------------|-----------------|--------|----------------------------|--|--|--|--|--|
| Intermediate Course |     |                |                 |        |                            |  |  |  |  |  |
| D01                 | J10 | 18             | 39              | 0.4843 | 0.007                      |  |  |  |  |  |
| PUI                 | J23 | 6              | 12              | 0.3473 | 0.237                      |  |  |  |  |  |
| D02                 | J04 | 14             | 30              | 0.5750 | 0.471                      |  |  |  |  |  |
| P02                 | J09 | 18             | 34              | 0.5053 | 0.471                      |  |  |  |  |  |
|                     | J31 | 41             | 77              | 0.5658 |                            |  |  |  |  |  |
| P10                 | J37 | 12             | 22              | 0.3924 | 0.005**                    |  |  |  |  |  |
|                     | J82 | 8              | 15              | 0.2876 |                            |  |  |  |  |  |
|                     |     | Surface        | Course          |        |                            |  |  |  |  |  |
| DOG                 | J62 | 9              | 31              | 0.5947 | 0.044                      |  |  |  |  |  |
| P20                 | J69 | 18             | 53              | 0.6044 | 0.944                      |  |  |  |  |  |
| D27                 | J55 | 5              | 15              | 0.4386 | 0.612                      |  |  |  |  |  |
| FZI                 | J71 | 9              | 27              | 0.5013 | 0.012                      |  |  |  |  |  |
| <b>P</b> 02         | J05 | 6              | 8               | 0.4277 | 0.611                      |  |  |  |  |  |
| F UZ                | J13 | 14             | 18              | 0.5225 | 0.011                      |  |  |  |  |  |
| D13                 | J03 | 8              | 16              | 0.7029 | 0.486                      |  |  |  |  |  |
| FIS                 | J43 | 8              | 19              | 0.8416 | 0.400                      |  |  |  |  |  |
| P24                 | J56 | 18             | 40              | 0.8204 | 0.664                      |  |  |  |  |  |
| F 24                | J67 | 6              | 10              | 0.7071 | 0.004                      |  |  |  |  |  |
| P35                 | J32 | 6              | 14              | 0.5270 | 0 1 2 9                    |  |  |  |  |  |
| 1 35                | J38 | 16             | 36              | 0.3817 | 0.123                      |  |  |  |  |  |
| PNQ                 | J35 | 3              | 9               | 0.4907 | 0.627                      |  |  |  |  |  |
| P09                 | J83 | 3              | 8               | 0.5858 | 0.021                      |  |  |  |  |  |

Table 7.20. Projects with More than One JMF for the Same Mix Type for AV

**\*\*** Bartlett's Test

**Determining the Typical Process Variability for AV.** Table 7.21 shows the standard deviation results for AV for all projects for which data were obtained. The projects are sorted by mix type. The "Lot" standard deviation is the average of the unbiased standard deviation estimates for each lot on the project. The "Project" standard deviation is the standard deviation of all the individual test results for the total project. The table also shows the total number of lots and tests for each project, the mean for all tests on the project, and the mean of the individual project lot means. Note that some projects do not have an average Lot standard deviation. This is due to the fact that there was only one AV test for each lot on the project. With only one test it is not possible to calculate a standard deviation for the lot.

One thing to consider from the results in Table 7.21 is whether to treat the Intermediate course results and the Surface course results as separate from one another or to combine them. By observation, the standard deviation values for the two courses are in the same general range. The Two-Sample Mann-Whitney hypothesis test was used to compare the medians of the Means of Lot Means results for each course. The same test was used to compare the medians of the Lot Standard Deviations. The Mann-Whitney test does not require the data to come from

normally distributed populations. It assumes that the populations of interest have the same shape and that the populations are independent. The results of the Mann-Whitney tests are shown in Table 7.22.

The medians of the Lot Means for Intermediate and Surface courses, with a P-value of 0.7339, are not different from one another. Similarly, with a P-value of 0.1827, the medians of the Lot Std Devs, cannot be declared significantly different. This supports the use of one set of tolerances for both Intermediate and Surface course mixes.

Table 7.23 shows Lot standard deviation results for the combined Intermediate and Surface course projects (from Table 7.21), but with the projects sorted from the smallest to largest Lot (i.e., within-lot) standard deviations. The projects are listed in increasing order of the Lot standard deviation to facilitate selecting a typical process standard deviation. The table also shows the total number of lots and tests for all AV projects, the averages for both the Project standard deviation values and for the Lot standard deviation values, and percentiles based on ranked order for both the Project and Lot standard deviation values.

SCDOT can use Table 7.23 to assist in selecting the "typical" variability to use to establish specification limits. As noted in the discussion above, there is no single "correct" way to establish this value. A subjective decision must be made regarding the standard deviation to select. The percentile values shown in the table should assist in making the decision. To get a "picture" of the results in Table 7.23, Figure 7.11 shows the empirical cumulative distribution function (CDF) for the combined Lot standard deviation values.

As the reference lines show, there appears to be a natural break point at around a standard deviation of 0.525, which corresponds to approximately the 75<sup>th</sup> percentile on the CDF plot. This would seem to be a logical choice for the process standard deviation. However, note that the slope of the CDF begins to flatten noticeably around the 89<sup>th</sup> percentile, which corresponds to a standard deviation of about 0.59. Somewhere within the range of these two values would be a reasonable choice for the typical process standard deviation for AV.

| Num     | ber       | Total Nu | umber of   | Mea        | n of *    | Std Dev | viation** |  |  |
|---------|-----------|----------|------------|------------|-----------|---------|-----------|--|--|
| Project | JMF       | Lots     | Tests      | All Tests  | Lot Means | Project | Lot       |  |  |
|         |           |          | Intermedia | ate Course | 9         |         |           |  |  |
| P01     | J02       | 4        | 8          | -0.301     | -0.2750   | 0.5772  | 0.4763    |  |  |
| P01     | J10       | 18       | 39         | -0.3559    | -0.4066   | 0.4875  | 0.3224    |  |  |
| P01     | J23       | 6        | 12         | -0.328     | -0.3075   | 0.3550  | 0.3523    |  |  |
| P02     | J04       | 14       | 30         | -0.1630    | -0.0838   | 0.5799  | 0.2696    |  |  |
| P02     | J09       | 18       | 34         | -0.0912    | -0.0825   | 0.5091  | 0.4415    |  |  |
| P04     | J08       | 5        | 10         | 0.1330     | 0.1330    | 0.4534  | 0.5619    |  |  |
| P05     | J27       | 8        | 15         | 0.2327     | 0.2256    | 0.3932  | 0.2823    |  |  |
| P10     | J31       | 41       | 77         | 0.1560     | 0.1524    | 0.5677  | 0.4411    |  |  |
| P10     | J37       | 12       | 22         | 0.5327     | 0.5371    | 0.3971  | 0.2207    |  |  |
| P10     | J82       | 8        | 15         | 0.7847     | 0.7869    | 0.2928  | 0.2216    |  |  |
| P17     | J22       | 6        | 11         | -0.4240    | -0.3875   | 0.5813  | 0.6717    |  |  |
| P21     | J34       | 3        | 8          | -0.0100    | 0.0833    | 0.3834  | 0.3477    |  |  |
| P25     | J29       | 7        | 12         | 0.6360     | 0.5929    | 0.5074  | 0.2375    |  |  |
| P27     | J53       | 14       | 15         | -0.1810    | -0.1811   | 0.4510  | 0.0443    |  |  |
| P27     | J60       | 15       | 15         | 0.0080     | 0.0080    | 0.6414  | -         |  |  |
| P28     | J42       | 13       | 15         | -0.0290    | -0.0092   | 0.4540  | 0.5938    |  |  |
| P32     | J76       | 12       | 43         | -0.6007    | -0.5974   | 0.3272  | 0.3108    |  |  |
| P33     | J73       | 8        | 25         | 0.1260     | 0.0860    | 0.5295  | 0.4808    |  |  |
| Total/A | verage    | 212      | 406        | 0.0070     | 0.0153    | 0.4716  | 0.3692    |  |  |
|         |           |          | Surface    | Course     |           |         |           |  |  |
| P01     | J07       | 9        | 30         | 0.3303     | 0.3323    | 0.5090  | 0.3991    |  |  |
| P01     | J19       | 14       | 18         | -0.4180    | -0.3925   | 0.5957  | 0.5251    |  |  |
| P02     | J05       | 6        | 8          | 0.331      | 0.3942    | 0.4435  | 0.3944    |  |  |
| P02     | J13       | 14       | 18         | 0.457      | 0.3721    | 0.5307  | 0.2880    |  |  |
| P02     | J15       | 6        | 18         | 0.532      | 0.2926    | 0.5602  | 0.3942    |  |  |
| P04     | J14       | 5        | 17         | 0.244      | 0.2433    | 0.5231  | 0.3691    |  |  |
| P05     | J25       | 8        | 8          | 0.011      | 0.0113    | 0.5534  | —         |  |  |
| P06     | J24       | 5        | 15         | -0.391     | -0.3907   | 0.4286  | 0.4613    |  |  |
| P07     | J30       | 19       | 40         | 0.0193     | 0.0884    | 0.5036  | 0.5144    |  |  |
| P09     | J35       | 3        | 9          | 0.293      | 0.2933    | 0.5066  | 0.3475    |  |  |
| P09     | J83       | 3        | 8          | -0.310     | -0.3633   | 0.6073  | 0.4908    |  |  |
| P10     | J12       | 13       | 19         | 0.415      | 0.3935    | 0.6317  | 0.5627    |  |  |
| P11     | J41       | 4        | 10         | 0.106      | 0.0977    | 0.4256  | 0.3034    |  |  |
| P12     | J38       | 6        | 14         | -0.643     | -0.7899   | 0.7625  | 0.5774    |  |  |
| P13     | J03       | 8        | 16         | -0.212     | -0.0487   | 0.7148  | 0.5782    |  |  |
| P13     | J43       | 8        | 19         | 0.067      | 0.1515    | 0.8538  | 0.7440    |  |  |
| P14     | J16       | 13       | 32         | -0.447     | -0.3851   | 0.7389  | 0.5168    |  |  |
| P16     | J20       | 3        | 9          | 0.164      | 0.1644    | 0.7841  | 0.7990    |  |  |
| P18     | J48       | 7        | 12         | -0.442     | -0.4002   | 0.8357  | 0.2787    |  |  |
| P19     | J49       | 7        | 20         | -0.514     | -0.4204   | 0.5826  | 0.5758    |  |  |
|         | Continued |          |            |            |           |         |           |  |  |

## Table 7.21. Summary of AV Test Results for Each Project

| Num     | nber   | Total Nu | umber of   | Mea                   | n of *    | Std Dev | viation** |
|---------|--------|----------|------------|-----------------------|-----------|---------|-----------|
| Project | JMF    | Lots     | Tests      | All Tests             | Lot Means | Project | Lot       |
|         |        |          | Surface Co | ourse ( <i>cont</i> ) | )         |         |           |
| P20     | J50    | 17       | 46         | -0.2567               | -0.3337   | 0.5495  | 0.4515    |
| P21     | J39    | 6        | 15         | -0.8340               | -0.7936   | 0.1504  | 0.1451    |
| P22     | J54    | 3        | 12         | 0.112                 | 0.2432    | 0.8910  | 0.8222    |
| P24     | J56    | 18       | 40         | -0.263                | -0.1499   | 0.8253  | 0.6368    |
| P24     | J64    | 7        | 13         | -0.6423               | -0.5964   | 0.2932  | 0.1935    |
| P24     | J67    | 6        | 10         | -0.192                | -0.1569   | 0.7268  | 0.5045    |
| P25     | J36    | 6        | 10         | 0.375                 | 0.4125    | 0.6240  | 0.6116    |
| P26     | J58    | 12       | 13         | 0.281                 | 0.1821    | 0.6810  | 0.2038    |
| P26     | J62    | 9        | 31         | 0.335                 | 0.3689    | 0.6000  | 0.4910    |
| P26     | J69    | 18       | 53         | 0.1649                | 0.2549    | 0.6703  | 0.4460    |
| P27     | J55    | 5        | 15         | 0.133                 | 0.1333    | 0.4469  | 0.4258    |
| P27     | J61    | 9        | 9          | -0.364                | -0.3644   | 0.5365  | -         |
| P27     | J71    | 9        | 27         | 0.2059                | 0.2039    | 0.5061  | 0.5727    |
| P28     | J39    | 9        | 24         | -0.5963               | -0.5436   | 0.2858  | 0.2291    |
| P29     | J59    | 9        | 26         | -0.0069               | -0.0072   | 0.2840  | 0.2487    |
| P30     | J65    | 4        | 8          | 0.5100                | 0.4867    | 0.2434  | 0.2316    |
| P32     | J72    | 8        | 34         | -0.0374               | -0.0719   | 0.5010  | 0.2384    |
| P32     | J79    | 24       | 96         | -0.2536               | -0.2436   | 0.4877  | 0.4356    |
| P33     | J77    | 6        | 22         | 0.462                 | 0.4626    | 0.6375  | 0.4186    |
| P34     | J62    | 7        | 28         | 0.152                 | 0.1174    | 0.6853  | 0.5621    |
| P34     | J81    | 7        | 13         | 0.075                 | 0.0907    | 0.5851  | 0.3057    |
| P35     | J32    | 6        | 14         | 0.399                 | 0.3861    | 0.5372  | 0.4463    |
| P35     | J38    | 16       | 36         | 0.0358                | 0.0815    | 0.3844  | 0.2381    |
| Total/A | verage | 382      | 935        | -0.0143               | -0.0045   | 0.5633  | 0.4385    |

Table 7.21. Summary of AV Test Results for Each Project (continued)

\* All Tests: the mean of all individual test results on the project Lot Means: the mean of all the individual lot means on the project

\*\* **Project:** the unbiased standard deviation estimate of all individual test results on the project **Lot:** the average of the unbiased standard deviation estimates for all lots on the project

 Table 7.22. Results of Mann-Whitney Tests on the AV Lot Means and Lot Std Devs

| Course       | No. of Lots | Median of Lot<br>Means | ledian of Lot<br>Means P-Value* |        | P-Value* |
|--------------|-------------|------------------------|---------------------------------|--------|----------|
| Intermediate | 18          | -0.0006                | 0 7220                          | 0.3477 | 0 1927   |
| Surface      | 43          | 0.0907                 | 0.7559                          | 0.4460 | 0.1027   |

\* Values in bold are statistically significantly different at the  $\alpha = 0.05$  level.

| Num       | nber | Total Nu | umber of | Mean of * |           | Std De  | Std Deviation* |         |
|-----------|------|----------|----------|-----------|-----------|---------|----------------|---------|
| Project   | JMF  | Lots     | Tests    | All Tests | Lot Means | Project | Lot            | Course  |
| P27       | J60  | 15       | 15       | 0.0080    | 0.0080    | 0.6414  | —              | Interm  |
| P05       | J25  | 8        | 8        | 0.011     | 0.0113    | 0.5534  | _              | Surface |
| P27       | J61  | 9        | 9        | -0.364    | -0.3644   | 0.5365  | —              | Surface |
| P27       | J53  | 14       | 15       | -0.1810   | -0.1811   | 0.4510  | 0.0443         | Interm  |
| P21       | J39  | 6        | 15       | -0.8340   | -0.7936   | 0.1504  | 0.1451         | Surface |
| P24       | J64  | 7        | 13       | -0.6423   | -0.5964   | 0.2932  | 0.1935         | Surface |
| P26       | J58  | 12       | 13       | 0.281     | 0.1821    | 0.6810  | 0.2038         | Surface |
| P10       | J37  | 12       | 22       | 0.5327    | 0.5371    | 0.3971  | 0.2207         | Interm  |
| P10       | J82  | 8        | 15       | 0.7847    | 0.7869    | 0.2928  | 0.2216         | Interm  |
| P28       | J39  | 9        | 24       | -0.5963   | -0.5436   | 0.2858  | 0.2291         | Surface |
| P30       | J65  | 4        | 8        | 0.5100    | 0.4867    | 0.2434  | 0.2316         | Surface |
| P25       | J29  | 7        | 12       | 0.6360    | 0.5929    | 0.5074  | 0.2375         | Interm  |
| P35       | J38  | 16       | 36       | 0.0358    | 0.0815    | 0.3844  | 0.2381         | Surface |
| P32       | J72  | 8        | 34       | -0.0374   | -0.0719   | 0.5010  | 0.2384         | Surface |
| P29       | J59  | 9        | 26       | -0.0069   | -0.0072   | 0.2840  | 0.2487         | Surface |
| P02       | J04  | 14       | 30       | -0.1630   | -0.0838   | 0.5799  | 0.2696         | Interm  |
| P18       | J48  | 7        | 12       | -0.442    | -0.4002   | 0.8357  | 0.2787         | Surface |
| P05       | J27  | 8        | 15       | 0.2327    | 0.2256    | 0.3932  | 0.2823         | Interm  |
| P02       | J13  | 14       | 18       | 0.457     | 0.3721    | 0.5307  | 0.2880         | Surface |
| P11       | J41  | 4        | 10       | 0.106     | 0.0977    | 0.4256  | 0.3034         | Surface |
| P34       | J81  | 7        | 13       | 0.075     | 0.0907    | 0.5851  | 0.3057         | Surface |
| P32       | J76  | 12       | 43       | -0.6007   | -0.5974   | 0.3272  | 0.3108         | Interm  |
| P01       | J10  | 18       | 39       | -0.3559   | -0.4066   | 0.4875  | 0.3224         | Interm  |
| P09       | J35  | 3        | 9        | 0.293     | 0.2933    | 0.5066  | 0.3475         | Surface |
| P21       | J34  | 3        | 8        | -0.0100   | 0.0833    | 0.3834  | 0.3477         | Interm  |
| P01       | J23  | 6        | 12       | -0.328    | -0.3075   | 0.3550  | 0.3523         | Interm  |
| P04       | J14  | 5        | 17       | 0.244     | 0.2433    | 0.5231  | 0.3691         | Surface |
| P02       | J15  | 6        | 18       | 0.532     | 0.2926    | 0.5602  | 0.3942         | Surface |
| P02       | J05  | 6        | 8        | 0.331     | 0.3942    | 0.4435  | 0.3944         | Surface |
| P01       | J07  | 9        | 30       | 0.3303    | 0.3323    | 0.5090  | 0.3991         | Surface |
| P33       | J77  | 6        | 22       | 0.462     | 0.4626    | 0.6375  | 0.4186         | Surface |
| P27       | J55  | 5        | 15       | 0.133     | 0.1333    | 0.4469  | 0.4258         | Surface |
| P32       | J79  | 24       | 96       | -0.2536   | -0.2436   | 0.4877  | 0.4356         | Surface |
| P10       | J31  | 41       | 77       | 0.1560    | 0.1524    | 0.5677  | 0.4411         | Interm  |
| P02       | J09  | 18       | 34       | -0.0912   | -0.0825   | 0.5091  | 0.4415         | Interm  |
| P26       | J69  | 18       | 53       | 0.1649    | 0.2549    | 0.6703  | 0.4460         | Surface |
| P35       | J32  | 6        | 14       | 0.399     | 0.3861    | 0.5372  | 0.4463         | Surface |
| P20       | J50  | 17       | 46       | -0.2567   | -0.3337   | 0.5495  | 0.4515         | Surface |
| P06       | J24  | 5        | 15       | -0.391    | -0.3907   | 0.4286  | 0.4613         | Surface |
| P01       | J02  | 4        | 8        | -0.301    | -0.2750   | 0.5772  | 0.4763         | Interm  |
| P33       | J73  | 8        | 25       | 0.1260    | 0.0860    | 0.5295  | 0.4808         | Interm  |
| Continued |      |          |          |           |           |         |                |         |

## Table 7.23. Summary of AV Test Results for Combined Intermediate and Surface Projects

| Num     | nber   | Total Nu | mber of | Mea       | n of *    | Std Deviation* |         |         |
|---------|--------|----------|---------|-----------|-----------|----------------|---------|---------|
| Project | JMF    | Lots     | Tests   | All Tests | Lot Means | Project        | Lot     | Course  |
| P09     | J83    | 3        | 8       | -0.310    | -0.3633   | 0.6073         | 0.4908  | Surface |
| P26     | J62    | 9        | 31      | 0.335     | 0.3689    | 0.6000         | 0.4910  | Surface |
| P24     | J67    | 6        | 10      | -0.192    | -0.1569   | 0.7268         | 0.5045  | Surface |
| P07     | J30    | 19       | 40      | 0.0193    | 0.0884    | 0.5036         | 0.5144  | Surface |
| P14     | J16    | 13       | 32      | -0.447    | -0.3851   | 0.7389         | 0.5168  | Surface |
| P01     | J19    | 14       | 18      | -0.4180   | -0.3925   | 0.5957         | 0.5251  | Surface |
| P04     | J08    | 5        | 10      | 0.1330    | 0.1330    | 0.4534         | 0.5619  | Interm  |
| P34     | J62    | 7        | 28      | 0.152     | 0.1174    | 0.6853         | 0.5621  | Surface |
| P10     | J12    | 13       | 19      | 0.415     | 0.3935    | 0.6317         | 0.5627  | Surface |
| P27     | J71    | 9        | 27      | 0.2059    | 0.2039    | 0.5061         | 0.5727  | Surface |
| P19     | J49    | 7        | 20      | -0.514    | -0.4204   | 0.5826         | 0.5758  | Surface |
| P12     | J38    | 6        | 14      | -0.643    | -0.7899   | 0.7625         | 0.5774  | Surface |
| P13     | J03    | 8        | 16      | -0.212    | -0.0487   | 0.7148         | 0.5782  | Surface |
| P28     | J42    | 13       | 15      | -0.0290   | -0.0092   | 0.4540         | 0.5938  | Interm  |
| P25     | J36    | 6        | 10      | 0.375     | 0.4125    | 0.6240         | 0.6116  | Surface |
| P24     | J56    | 18       | 40      | -0.263    | -0.1499   | 0.8253         | 0.6368  | Surface |
| P17     | J22    | 6        | 11      | -0.4240   | -0.3875   | 0.5813         | 0.6717  | Interm  |
| P13     | J43    | 8        | 19      | 0.067     | 0.1515    | 0.8538         | 0.7440  | Surface |
| P16     | J20    | 3        | 9       | 0.164     | 0.1644    | 0.7841         | 0.7990  | Surface |
| P22     | J54    | 3        | 12      | 0.112     | 0.2432    | 0.8910         | 0.8222  | Surface |
| Total/A | verage | 594      | 1341    | -0.008    | 0.0013    | 0.5363         | 0.4182  |         |
|         |        |          |         |           | 50%       | 0.5307         | 0.43070 |         |
|         |        |          |         |           | 60%       | 0.5677         | 0.45346 |         |
|         |        |          |         |           | 70%       | 0.5957         | 0.50315 |         |
|         |        |          |         |           | 80%       | 0.6414         | 0.56246 |         |
|         |        |          |         |           | 90%       | 0.7389         | 0.59914 |         |

#### Table 7.23. Summary of AV Test Results for Combined Intermediate and Surface Projects (*continued*)

\* All Tests: the mean of all individual test results on the project Lot Means: the mean of all the individual lot means on the project

\*\* **Project:** the unbiased standard deviation estimate of all individual test results on the project **Lot:** the average of the unbiased standard deviation estimates for all lots on the project



Figure 7.11. CDF for AV for Lot Standard Deviations for Intermediate and Surface Projects

**PWL Values for the AV Projects.** The AV projects did not exhibit the same concern that was found with the Density projects where many of the projects had relatively low average PWL values. A different problem with the AV projects was that many of the projects did not have sufficient sample sizes to calculate a PWL value for the lots. There must be at least 3 test results for a lot to be able to estimate the PWL value for the lot. Rather than to combine lots, which is what would have been done in the field to determine the PWL to use for determining the payment factor, lots that had at least 3 tests were evaluated to determine their estimated PWL values. This resulted in PWL calculations for 207 lots.

Of the 207 lots, 32 had PWL values less than 90, which would result in some form of price reduction. Only 6 of the projects had average lot PWL values less than 90, and 2 of those had average lot PWL values greater than 89.5.

### VMA

**Comparing Courses.** The specifications for VMA had one set of allowable tolerances, 1.15%, for Intermediate and Surface courses. VMA values were not determined for Base course mixes. To evaluate whether or not different tolerances might be warranted for Intermediate and Surface courses, the variances of the two courses were compared statistically using the *F*-test and Levene's test. The *F*-test assumes that the data are from normal distributions, whereas Levene's test applies for any continuous distribution. Table 7.24 shows the results of the comparison.

| Course       | No. of<br>Tests | St Dev | P-value*<br><i>F</i> -test | P-value*<br>Levene's |
|--------------|-----------------|--------|----------------------------|----------------------|
| Intermediate | 406             | 0.5974 | 0 1 9 2                    | 0.249                |
| Surface      | 935             | 0.5654 | 0.165                      | 0.240                |

Table 7.24. Summary of VMA Comparisons among Courses

The results in Table 7.24 show that neither the *F*-test, with a P-value of 0.035, nor Levene's test, with a P-value of 0.141, would conclude that the variabilities should be considered different. To further investigate the variabilities, Figure 7.12 shows the standard deviation along with its 95% confidence interval for each course. There is quite a bit of overlap between the two confidence intervals. Therefore, it is reasonable to conclude that the two courses can be treated having similar variabilities.



Figure 7.12. Comparison of VMA Standard Deviations for Intermediate and Surface Courses

**Comparing Mix Types within Course.** The next question to consider is whether it is appropriate to use the same specification tolerances for all mix types within a given course. When establishing the allowable tolerances it is the standard deviation that is most important.

**Intermediate Course Mixes.** Table 7.25 shows the results of comparisons among the VMA variabilities for the different types of Intermediate course mixes. The results, with Bartlett's test having a P-value of 0.216 and Levene's test having a P-value of 0.153, show no evidence that the standard deviations are different for the different mix types. Figure 7.13 shows the standard deviation along with its 95% confidence interval for each Intermediate course mix type.

| Mix Type       | No. of<br>Tests | St Dev | P-value*<br>Bartlett's | P-value*<br>Levene's |
|----------------|-----------------|--------|------------------------|----------------------|
| Binder 1       | 18              | 0.7076 |                        |                      |
| Intermediate B | 198             | 0.5565 | 0.216                  | 0.153                |
| Intermediate C | 190             | 0.6123 |                        |                      |

Table 7.25. Summary of VMA Comparisons of Intermediate Course Mix Types



### Figure 7.13. Comparison of VMA Standard Deviations for Each Intermediate Mix Type

**Surface Course Mixes.** Table 7.26 shows the results of comparisons among the VMA variabilities for the different types of Surface course mixes. The results show clearly that the standard deviations are not equal for all 10 mix types. Figure 7.14 shows the standard deviation along with its 95% confidence interval for each Surface course mix type.

| Міх Туре   | No. of<br>Tests | St Dev | P-value*<br>Bartlett's | P-value*<br>Levene's |  |  |
|------------|-----------------|--------|------------------------|----------------------|--|--|
| Surface 1C | 16              | 0.4013 |                        |                      |  |  |
| Surface 1D | 15              | 0.5012 |                        | 0.002                |  |  |
| Surface 1R | 17              | 0.5099 |                        |                      |  |  |
| Surface 3  | 40              | 0.4565 |                        |                      |  |  |
| Surface 4  | 19              | 0.6871 | 0.000                  |                      |  |  |
| Surface A  | 230             | 0.5162 | 0.000                  | 0.002                |  |  |
| Surface B  | 116             | 0.4550 |                        |                      |  |  |
| Surface C  | 393             | 0.5482 |                        |                      |  |  |
| Surface CM | 26              | 0.5549 |                        |                      |  |  |
| Surface D  | 63              | 0.7526 |                        |                      |  |  |

Table 7.26. Summary of VMA Comparisons of Surface Course Mix Types



Figure 7.14 Comparison of VMA Standard Deviations for Each Surface Course Mix Type

It must be noted that the above analysis can be thought of as a quick simplification. The effect of combining several projects in the varioius Surface mix types will be addressed when the individual average Lot standard deviation and average project standard deviations are analyzed.

**Caveat.** None of the standard deviation values shown in Tables 7.24-7.26 are the appropriate standard deviation to use to represent the process standard deviation for VMA. These calculations were done simply for exploratory purposes. Aggregating the data as in these tables is not appropriate for establishing specification limits since the specification limits are based on lot-by-lot acceptance, or at least on acceptance of a project.

**Typical Variability Values for VMA.** As noted above, since the SCDOT specification is based on lot-by-lot acceptance, the VMA variability that is used to evaluate the specification limits must be that which is appropriate for a typical lot. To determine this, the individual standard deviation values for each lot were calculated and then these lot standard deviations were averaged to get the "within-lot" standard deviation for each project. This was done using the procedure that is described for density in Chapter 6. As noted in Chapter 6, this within-lot standard deviation does not take into consideration any target miss variability that may be present.

To provide the option to consider using the total project as the payment lot, the total project VMA standard deviation was also calculated for each project. As noted above, this "project" standard deviation could also be used as one way of trying to incorporate any target miss variability that might be present in the contractor's process.

Appendix B includes the necessary calculations for each project for which VMA data were obtained. These calculations were used to arrive at the project standard deviations that were used to establish the typical process variability for VMA.

**Projects with Multiple JMFs.** Before compiling all of the within-lot and project variabilities, a decision had to me made regarding how to deal with projects on which more than one JMF was used for the same mix type and course. Should each JMF be treated as a separate project, or should the multiple JMF results be combined together as one project? To help make this decision, the projects with multiple JMFs were examined. Table 7.27 shows the projects (extracted from Tables 7.4-7.5) that had multiple JMFs for the same mix type.

None of the multi-mix design projects showed a difference in variability. Also, in the project data a new lot was established in nearly every case that the JMF changed. This would argue in favor of treating the JMFs as separate projects when determining the within-lot standard deviations.

However, if a total project is being used as the payment lot, then the data from the multiple JMFs would be combined when calculating the standard deviation to use for payment determination. This would argue in favor of combining the separate JMFs into a single project. For consistency in presentation and in comparing results, it was decided to treat the separate JMFs as separate projects when calculating standard deviations and when presenting the results.

**Determining the Typical Process Variability for VMA.** Table 7.28 shows the standard deviation results for VMA for all projects for which data were obtained. The projects are sorted by mix type. The "Lot" standard deviation is the average of the unbiased standard deviation estimates for each lot on the project. The "Project" standard deviation is the standard deviation

of all the individual test results for the total project. The table also shows the total number of lots and tests for each project, the mean for all tests on the project, and the mean of the individual project lot means. Note that some projects do not have an average Lot standard deviation. This is due to the fact that there was only one VMA test for each lot on the project. With only one test it is not possible to calculate a standard deviation for the lot.

| Project             | JMF            | No. of<br>Lots | No. of<br>Tests | No. of<br>Tests St Dev |         |  |  |  |
|---------------------|----------------|----------------|-----------------|------------------------|---------|--|--|--|
| Intermediate Course |                |                |                 |                        |         |  |  |  |
| D01                 | J10            | 18             | 39              | 0.4694                 | 0.959   |  |  |  |
| FUI                 | J23            | 6              | 12              | 0.4798                 | 0.656   |  |  |  |
| P02                 | J04            | 14             | 30              | 0.5831                 | 0.644   |  |  |  |
| F UZ                | J09            | 18             | 34              | 0.6351                 | 0.044   |  |  |  |
|                     | J31            | 41             | 77              | 0.6384                 |         |  |  |  |
| P10                 | J37            | 12             | 22              | 0.7139                 | 0.696** |  |  |  |
|                     | J82            | 8              | 15              | 0.5838                 |         |  |  |  |
|                     | Surface Course |                |                 |                        |         |  |  |  |
| DOC                 | J62            | 9              | 31              | 0.4305                 | 0.713   |  |  |  |
| F20                 | J69            | 18             | 53              | 0.4596                 |         |  |  |  |
| <b>D</b> 27         | J55            | 5              | 15              | 0.3453                 | 0.401   |  |  |  |
| Γ21                 | J71            | 9              | 27              | 0.4127                 | 0.491   |  |  |  |
| P02                 | J05            | 6              | 8               | 0.3108                 | 0.077   |  |  |  |
| F UZ                | J13            | 14             | 18              | 0.6103                 | 0.077   |  |  |  |
| D13                 | J03            | 8              | 16              | 0.4195                 | 0.210   |  |  |  |
| FIJ                 | J43            | 8              | 19              | 0.5765                 | 0.219   |  |  |  |
| P24                 | J56            | 18             | 40              | 0.5181                 | 0.632   |  |  |  |
| 1 24                | J67            | 6              | 10              | 0.4409                 | 0.032   |  |  |  |
| P35                 | J32            | 6              | 14              | 0.4541                 | 0 1 1 8 |  |  |  |
| F 30                | J38            | 16             | 36              | 0.3257                 | 0.110   |  |  |  |
| POQ                 | J35            | 3              | 9               | 0.4315                 | 0 /83   |  |  |  |
| F 03                | J83            | 3              | 8               | 0.5592                 | 0.405   |  |  |  |

Table 7.27. Projects with More than One JMF for the Same Mix Type for VMA

- \* Values in bold are statistically significantly different at the  $\alpha = 0.05$  level.
- \*\* Bartlett's Test

One thing to consider from the results in Table 7.28 is whether to treat the Intermediate course results and the Surface course results as separate from one another or to combine them. By observation, the standard deviation values for the two courses are in the same general range. The Two-Sample Mann-Whitney hypothesis test was used to compare the medians of the Means of Lot Means results for each course. The same test was used to compare the medians of the Lot Standard Deviations. The Mann-Whitney test does not require the data to come from normally distributed populations. It assumes that the populations of interest have the same shape and that the populations are independent. The results of the Mann-Whitney tests are shown in Table 7.29.

The medians of the Lot Means for Intermediate and Surface courses, with a P-value of 0.3077, are not different from one another. Similarly, with a P-value of 0.1665, the medians of the Lot Std Devs, cannot be declared significantly different. This supports the use of one set of tolerances for both Intermediate and Surface course mixes.

| Num       | nber   | Total Nu | Imber of   | Mean of *  |           | Std Deviation** |        |
|-----------|--------|----------|------------|------------|-----------|-----------------|--------|
| Project   | JMF    | Lots     | Tests      | All Tests  | Lot Means | Project         | Lot    |
|           |        | l        | Intermedia | ate Course | ;         |                 |        |
| P01       | J02    | 4        | 8          | 0.021      | -0.0346   | 0.5575          | 0.7095 |
| P01       | J10    | 18       | 39         | -0.2841    | -0.3032   | 0.4725          | 0.3657 |
| P01       | J23    | 6        | 12         | -0.025     | -0.0232   | 0.4910          | 0.6908 |
| P02       | J04    | 14       | 30         | 0.218      | 0.4242    | 0.5880          | 0.3765 |
| P02       | J09    | 18       | 34         | 0.040      | 0.0211    | 0.6398          | 0.5249 |
| P04       | J08    | 5        | 10         | 0.607      | 0.6070    | 0.7628          | 0.9022 |
| P05       | J27    | 8        | 15         | 0.051      | 0.0413    | 0.4265          | 0.4077 |
| P10       | J31    | 41       | 77         | 0.2103     | 0.2279    | 0.6405          | 0.5970 |
| P10       | J37    | 12       | 22         | 0.402      | 0.4317    | 0.7225          | 0.5353 |
| P10       | J82    | 8        | 15         | 0.651      | 0.6731    | 0.5945          | 0.3279 |
| P17       | J22    | 6        | 11         | -0.468     | -0.4875   | 0.5188          | 0.6221 |
| P21       | J34    | 3        | 8          | 0.2300     | 0.1942    | 0.1737          | 0.1290 |
| P25       | J29    | 7        | 12         | 0.438      | 0.3879    | 0.4818          | 0.4023 |
| P27       | J53    | 14       | 15         | 0.035      | 0.0300    | 0.4632          | 0.4786 |
| P27       | J60    | 15       | 15         | 0.611      | 0.6107    | 0.5202          | _      |
| P28       | J42    | 13       | 15         | 0.169      | 0.1958    | 0.5161          | 0.5716 |
| P32       | J76    | 12       | 43         | -0.0809    | -0.0884   | 0.4439          | 0.4136 |
| P33       | J73    | 8        | 25         | 0.1468     | 0.1714    | 0.4241          | 0.2938 |
| Total/A   | verage | 212      | 406        | 0.1651     | 0.1711    | 0.5243          | 0.4911 |
|           |        |          | Surface    | Course     |           |                 |        |
| P01       | J07    | 9        | 30         | 0.2430     | 0.2536    | 0.4805          | 0.4326 |
| P01       | J19    | 14       | 18         | -0.036     | 0.0307    | 0.6343          | 0.4564 |
| P02       | J05    | 6        | 8          | 0.353      | 0.3975    | 0.3223          | 0.2083 |
| P02       | J13    | 14       | 18         | 0.233      | 0.2046    | 0.6190          | 0.3567 |
| P02       | J15    | 6        | 18         | 0.404      | 0.3438    | 0.5998          | 0.4860 |
| P04       | J14    | 5        | 17         | 0.356      | 0.3465    | 0.5180          | 0.5125 |
| P05       | J25    | 8        | 8          | -0.221     | -0.2213   | 0.7627          | _      |
| P06       | J24    | 5        | 15         | -0.210     | -0.2100   | 0.5100          | 0.5491 |
| P07       | J30    | 19       | 40         | -0.0288    | 0.0262    | 0.4594          | 0.4234 |
| P09       | J35    | 3        | 9          | 0.230      | 0.2300    | 0.4447          | 0.3995 |
| P09       | J83    | 3        | 8          | -0.331     | -0.3622   | 0.5793          | 0.6334 |
| P10       | J12    | 13       | 19         | 0.249      | 0.2435    | 0.6966          | 0.3057 |
| P11       | J41    | 4        | 10         | 0.3030     | 0.2931    | 0.2468          | 0.3680 |
| P12       | J38    | 6        | 14         | -0.454     | -0.5500   | 0.6565          | 0.6036 |
| P13       | J03    | 8        | 16         | -0.089     | -0.0267   | 0.4260          | 0.3149 |
| P13       | J43    | 8        | 19         | 0.155      | 0.2220    | 0.5851          | 0.5881 |
| Continued |        |          |            |            |           |                 |        |

### Table 7.28. Summary of VMA Test Results for Each Project
| Nun     | nber                           | Total Nu | umber of | Mea       | n of *    | Std Dev | viation** |  |  |
|---------|--------------------------------|----------|----------|-----------|-----------|---------|-----------|--|--|
| Project | JMF                            | Lots     | Tests    | All Tests | Lot Means | Project | Lot       |  |  |
|         | Surface Course ( <i>cont</i> ) |          |          |           |           |         |           |  |  |
| P14     | J16                            | 13       | 32       | -0.7066   | -0.6616   | 0.5427  | 0.4245    |  |  |
| P16     | J20                            | 3        | 9        | -0.234    | -0.2344   | 0.4529  | 0.4793    |  |  |
| P18     | J48                            | 7        | 12       | -0.057    | -0.0107   | 0.6577  | 0.3949    |  |  |
| P19     | J49                            | 7        | 20       | -0.590    | -0.5126   | 0.5948  | 0.4926    |  |  |
| P20     | J50                            | 17       | 46       | -0.2063   | -0.2124   | 0.4182  | 0.3178    |  |  |
| P21     | J39                            | 6        | 15       | -0.7020   | -0.6738   | 0.2255  | 0.1744    |  |  |
| P22     | J54                            | 3        | 12       | 0.217     | 0.3628    | 0.7651  | 0.7207    |  |  |
| P24     | J56                            | 18       | 40       | -0.2148   | -0.1542   | 0.5214  | 0.3821    |  |  |
| P24     | J64                            | 7        | 13       | -0.2123   | -0.1971   | 0.2673  | 0.1920    |  |  |
| P24     | J67                            | 6        | 10       | -0.354    | -0.3350   | 0.4534  | 0.5878    |  |  |
| P25     | J36                            | 6        | 10       | 0.700     | 0.7069    | 0.7762  | 0.8118    |  |  |
| P26     | J58                            | 12       | 13       | 0.288     | 0.2204    | 0.5575  | 0.6824    |  |  |
| P26     | J62                            | 9        | 31       | 0.3458    | 0.3665    | 0.4341  | 0.3949    |  |  |
| P26     | J69                            | 18       | 53       | 0.1757    | 0.2076    | 0.4618  | 0.2928    |  |  |
| P27     | J55                            | 5        | 15       | 0.4627    | 0.4627    | 0.3515  | 0.3754    |  |  |
| P27     | J61                            | 9        | 9        | -0.286    | -0.2856   | 0.5550  | _         |  |  |
| P27     | J71                            | 9        | 27       | 0.3057    | 0.3144    | 0.3086  | 0.5121    |  |  |
| P28     | J39                            | 9        | 24       | -0.4029   | -0.4229   | 0.2105  | 0.1827    |  |  |
| P29     | J59                            | 9        | 26       | -0.0165   | -0.0273   | 0.3254  | 0.2577    |  |  |
| P30     | J65                            | 4        | 8        | 0.4800    | 0.4800    | 0.1793  | 0.2270    |  |  |
| P32     | J72                            | 8        | 34       | 0.1409    | 0.1268    | 0.4499  | 0.3933    |  |  |
| P32     | J79                            | 24       | 96       | 0.0493    | 0.0514    | 0.5533  | 0.4482    |  |  |
| P33     | J77                            | 6        | 22       | 0.126     | 0.1761    | 0.6578  | 0.4098    |  |  |
| P34     | J62                            | 7        | 28       | 0.0946    | 0.0602    | 0.4099  | 0.3731    |  |  |
| P34     | J81                            | 7        | 13       | 0.469     | 0.3186    | 0.4789  | 0.5110    |  |  |
| P35     | J32                            | 6        | 14       | 0.233     | 0.2633    | 0.4628  | 0.3182    |  |  |
| P35     | J38                            | 16       | 36       | 0.1622    | 0.1899    | 0.3280  | 0.3607    |  |  |
| Total/A | verage                         | 382      | 935      | 0.0331    | 0.0419    | 0.4870  | 0.4233    |  |  |

#### Table 7.28. Summary of VMA Test Results for Each Project (continued)

\* All Tests: the mean of all individual test results on the project Lot Means: the mean of all the individual lot means on the project

\*\* **Project:** the unbiased standard deviation estimate of all individual test results on the project **Lot:** the average of the unbiased standard deviation estimates for all lots on the project

| Table 7.29. Results of Mann-Whitney | Tests on the VMA Lot Means and Lot Std Devs |
|-------------------------------------|---|
|-------------------------------------|---|

| Course       | No. of<br>Lots | Median of Lot<br>Means | P-Value* | No. of<br>Lots | Median of<br>Lot Std Devs | P-Value* |
|--------------|----------------|------------------------|----------|----------------|---------------------------|----------|
| Intermediate | 18             | 0.1828                 | 0 2077   | 17             | 0.4786                    | 0 1665   |
| Surface      | 43             | 0.1268                 | 0.3077   | 41             | 0.3995                    | 0.1005   |

\* Values in bold are statistically significantly different at the  $\alpha = 0.05$  level.

Table 7.30 shows Lot standard deviation results for the combined Intermediate and Surface course projects (from Table 7.28), but with the projects sorted from the smallest to largest Lot (i.e., within-lot) standard deviations. The projects are listed in increasing order of the Lot standard deviation to facilitate selecting a typical process standard deviation. The table also shows the total number of lots and tests for all VMA projects, the averages for both the Project standard deviation values and for the Lot standard deviation values, and percentiles based on ranked order for both the Project and Lot standard deviation values.

SCDOT can use Table 7.30 to assist in selecting the "typical" variability to use to establish specification limits. As noted in the discussion above, there is no single "correct" way to establish this value. A subjective decision must be made regarding the standard deviation to select. The percentile values shown in the table should assist in making the decision. To get a "picture" of the results in Table 7.30, Figure 7.15 shows the empirical cumulative distribution function (CDF) for the combined Lot standard deviation values.

As the reference lines show, there is not an obvious natural break point on the plot until approximately the 90<sup>th</sup> percentile, which corresponds to a standard deviation of about 0.63. Another possible choice might be at around a standard deviation of 0.55, which corresponds to approximately the 77<sup>th</sup> percentile on the CDF plot. Somewhere within the range of these two values would be a reasonable choice for the typical process standard deviation for VMA.

| Num     | nber      | Total Nu | Imber of | Mea       | Mean of * |         | Std Deviation* |         |
|---------|-----------|----------|----------|-----------|-----------|---------|----------------|---------|
| Project | JMF       | Lots     | Tests    | All Tests | Lot Means | Project | Lot            | Course  |
| P27     | J60       | 15       | 15       | 0.611     | 0.6107    | 0.5202  | _              | Interm  |
| P05     | J25       | 8        | 8        | -0.221    | -0.2213   | 0.7627  | _              | Surface |
| P27     | J61       | 9        | 9        | -0.286    | -0.2856   | 0.5550  | _              | Surface |
| P21     | J34       | 3        | 8        | 0.2300    | 0.1942    | 0.1737  | 0.1290         | Interm  |
| P21     | J39       | 6        | 15       | -0.7020   | -0.6738   | 0.2255  | 0.1744         | Surface |
| P28     | J39       | 9        | 24       | -0.4029   | -0.4229   | 0.2105  | 0.1827         | Surface |
| P24     | J64       | 7        | 13       | -0.2123   | -0.1971   | 0.2673  | 0.1920         | Surface |
| P02     | J05       | 6        | 8        | 0.353     | 0.3975    | 0.3223  | 0.2083         | Surface |
| P30     | J65       | 4        | 8        | 0.4800    | 0.4800    | 0.1793  | 0.2270         | Surface |
| P29     | J59       | 9        | 26       | -0.0165   | -0.0273   | 0.3254  | 0.2577         | Surface |
| P26     | J69       | 18       | 53       | 0.1757    | 0.2076    | 0.4618  | 0.2928         | Surface |
| P33     | J73       | 8        | 25       | 0.1468    | 0.1714    | 0.4241  | 0.2938         | Interm  |
| P10     | J12       | 13       | 19       | 0.249     | 0.2435    | 0.6966  | 0.3057         | Surface |
| P13     | J03       | 8        | 16       | -0.089    | -0.0267   | 0.4260  | 0.3149         | Surface |
| P20     | J50       | 17       | 46       | -0.2063   | -0.2124   | 0.4182  | 0.3178         | Surface |
| P35     | J32       | 6        | 14       | 0.233     | 0.2633    | 0.4628  | 0.3182         | Surface |
| P10     | J82       | 8        | 15       | 0.651     | 0.6731    | 0.5945  | 0.3279         | Interm  |
| P02     | J13       | 14       | 18       | 0.233     | 0.2046    | 0.6190  | 0.3567         | Surface |
| P35     | J38       | 16       | 36       | 0.1622    | 0.1899    | 0.3280  | 0.3607         | Surface |
| P01     | J10       | 18       | 39       | -0.2841   | -0.3032   | 0.4725  | 0.3657         | Interm  |
| P11     | J41       | 4        | 10       | 0.3030    | 0.2931    | 0.2468  | 0.3680         | Surface |
| P34     | J62       | 7        | 28       | 0.0946    | 0.0602    | 0.4099  | 0.3731         | Surface |
| P27     | J55       | 5        | 15       | 0.4627    | 0.4627    | 0.3515  | 0.3754         | Surface |
| P02     | J04       | 14       | 30       | 0.218     | 0.4242    | 0.5880  | 0.3765         | Interm  |
| P24     | J56       | 18       | 40       | -0.2148   | -0.1542   | 0.5214  | 0.3821         | Surface |
| P32     | J72       | 8        | 34       | 0.1409    | 0.1268    | 0.4499  | 0.3933         | Surface |
| P18     | J48       | 7        | 12       | -0.057    | -0.0107   | 0.6577  | 0.3949         | Surface |
| P26     | J62       | 9        | 31       | 0.3458    | 0.3665    | 0.4341  | 0.3949         | Surface |
| P09     | J35       | 3        | 9        | 0.230     | 0.2300    | 0.4447  | 0.3995         | Surface |
| P25     | J29       | 7        | 12       | 0.438     | 0.3879    | 0.4818  | 0.4023         | Interm  |
| P05     | J27       | 8        | 15       | 0.051     | 0.0413    | 0.4265  | 0.4077         | Interm  |
| P33     | J77       | 6        | 22       | 0.126     | 0.1761    | 0.6578  | 0.4098         | Surface |
| P32     | J76       | 12       | 43       | -0.0809   | -0.0884   | 0.4439  | 0.4136         | Interm  |
| P07     | J30       | 19       | 40       | -0.0288   | 0.0262    | 0.4594  | 0.4234         | Surface |
| P14     | J16       | 13       | 32       | -0.7066   | -0.6616   | 0.5427  | 0.4245         | Surface |
| P01     | J07       | 9        | 30       | 0.2430    | 0.2536    | 0.4805  | 0.4326         | Surface |
| P32     | J79       | 24       | 96       | 0.0493    | 0.0514    | 0.5533  | 0.4482         | Surface |
| P01     | J19       | 14       | 18       | -0.036    | 0.0307    | 0.6343  | 0.4564         | Surface |
| P27     | J53       | 14       | 15       | 0.035     | 0.0300    | 0.4632  | 0.4786         | Interm  |
| P16     | J20       | 3        | 9        | -0.234    | -0.2344   | 0.4529  | 0.4793         | Surface |
|         | Continued |          |          |           |           |         |                |         |

# Table 7.30. Summary of VMA Test Results for Combined Intermediate and Surface Projects

| Num               | ber | Total Nu | umber of | Mea       | n of *    | Std Deviation* |        |         |
|-------------------|-----|----------|----------|-----------|-----------|----------------|--------|---------|
| Project           | JMF | Lots     | Tests    | All Tests | Lot Means | Project        | Lot    | Course  |
| P02               | J15 | 6        | 18       | 0.404     | 0.3438    | 0.5998         | 0.4860 | Surface |
| P19               | J49 | 7        | 20       | -0.590    | -0.5126   | 0.5948         | 0.4926 | Surface |
| P34               | J81 | 7        | 13       | 0.469     | 0.3186    | 0.4789         | 0.5110 | Surface |
| P27               | J71 | 9        | 27       | 0.3057    | 0.3144    | 0.3086         | 0.5121 | Surface |
| P04               | J14 | 5        | 17       | 0.356     | 0.3465    | 0.5180         | 0.5125 | Surface |
| P02               | J09 | 18       | 34       | 0.040     | 0.0211    | 0.6398         | 0.5249 | Interm  |
| P10               | J37 | 12       | 22       | 0.402     | 0.4317    | 0.7225         | 0.5353 | Interm  |
| P06               | J24 | 5        | 15       | -0.210    | -0.2100   | 0.5100         | 0.5491 | Surface |
| P28               | J42 | 13       | 15       | 0.169     | 0.1958    | 0.5161         | 0.5716 | Interm  |
| P24               | J67 | 6        | 10       | -0.354    | -0.3350   | 0.4534         | 0.5878 | Surface |
| P13               | J43 | 8        | 19       | 0.155     | 0.2220    | 0.5851         | 0.5881 | Surface |
| P10               | J31 | 41       | 77       | 0.2103    | 0.2279    | 0.6405         | 0.5970 | Interm  |
| P12               | J38 | 6        | 14       | -0.454    | -0.5500   | 0.6565         | 0.6036 | Surface |
| P17               | J22 | 6        | 11       | -0.468    | -0.4875   | 0.5188         | 0.6221 | Interm  |
| P09               | J83 | 3        | 8        | -0.331    | -0.3622   | 0.5793         | 0.6334 | Surface |
| P26               | J58 | 12       | 13       | 0.288     | 0.2204    | 0.5575         | 0.6824 | Surface |
| P01               | J23 | 6        | 12       | -0.025    | -0.0232   | 0.4910         | 0.6908 | Interm  |
| P01               | J02 | 4        | 8        | 0.021     | -0.0346   | 0.5575         | 0.7095 | Interm  |
| P22               | J54 | 3        | 12       | 0.217     | 0.3628    | 0.7651         | 0.7207 | Surface |
| P25               | J36 | 6        | 10       | 0.700     | 0.7069    | 0.7762         | 0.8118 | Surface |
| P04               | J08 | 5        | 10       | 0.607     | 0.6070    | 0.7628         | 0.9022 | Interm  |
| Total/Ave<br>rage |     | 594      | 1341     | 0.0721    | 0.0800    | 0.4980         | 0.4432 |         |
|                   |     |          |          |           | 50%       | 0.4910         | 0.4117 |         |
|                   |     |          |          |           | 60%       | 0.5214         | 0.4608 |         |
|                   |     |          |          |           | 70%       | 0.5793         | 0.5120 |         |
|                   |     |          |          |           | 80%       | 0.6190         | 0.5813 |         |
|                   |     |          |          |           | 90%       | 0.6578         | 0.6481 |         |

## Table 7.30. Summary of VMA Test Results for Combined Intermediate and Surface Projects (*continued*)

\* All Tests: the mean of all individual test results on the project Lot Means: the mean of all the individual lot means on the project

\*\* **Project:** the unbiased standard deviation estimate of all individual test results on the project **Lot:** the average of the unbiased standard deviation estimates for all lots on the project



Figure 7.15. CDF for AV for Lot Standard Deviations for Intermediate and Surface Projects

**PWL Values for the VMA Projects.** The VMA projects did not exhibit the same concern that was found with the Density projects where many of the projects had relatively low average PWL values. A different problem with the VMA projects was that many of the projects did not have sufficient sample sizes to calculate a PWL value for the lots. There must be at least 3 test results for a lot to be able to estimate the PWL value for the lot. Rather than to combine lots, which is what would have been done in the field to determine the PWL to use for determining the payment factor, lots that had at least 3 tests were evaluated to determine their estimated PWL values. This resulted in PWL calculations for 207 lots.

Of the 207 lots, 19 had PWL values less than 90, which would result in some form of price reduction. Only 4 of the projects had average lot PWL values less than 90, and one of those had an average lot PWL value 89.92.

# Summary

Analyses were conducted on project test results for Asphalt Content, Air Voids, and VMA. The primary goal of these analyses was to determine values to use to represent the typical variability for each of these characteristics. This is a subjective decision that ultimately must be made by SCDOT. Some potential values were identified during the analyses, and these are used as examples for additional evaluations in subsequent chapters.

The values for typical standard deviations that SCDOT might consider to represent the typical within-lot variability used to evaluate existing specification limits include:

| Base Course:         | 0.25% - 0.295%  |
|----------------------|---|
| Intermediate Course: | 0.21% - 0.26%   |
| Surface Course:      | 0.195% - 0.215%   |
|                      | Base Course:<br>Intermediate Course:<br>Surface Course: |

**Air Voids:** 0.525% - 0.59%

**VMA:** 0.55% – 0.63%

**Important Note:** The above values consider only the "within-lot" process standard deviation for each of the characteristics. If SCDOT would also like to consider some form of "target-miss" variability, then the appropriate standard deviations should likely be larger than those shown above. This issue is discussed in the next chapter that deals with payment considerations.

# **CHAPTER 8 — PAYMENT CONSIDERATIONS**

# Background

In Chapter 6 a range of within-lot standard deviation values was calculated for Density. In Chapter 7, similar within-lot standard deviation ranges were developed for asphalt content (AC), air voids (AV), and VMA. In this chapter, the potential variability of the population mean about the target value is considered in addition to the within-lot standard deviation values to develop an overall process standard deviation for each of the acceptance characteristics. These standard deviation values are compared with the current SCDOT specification limits to investigate whether or not these limits are still appropriate.

# Variability of the Process Mean

The typical within-lot standard deviation serves as a measure of variability within the process for a typical contractor on a typical project. This standard deviation can be used to help decide upon specification limits for the acceptance characteristic. However, as discussed in Chapter 5, another factor that may need to be considered in addition to the within–lot variability is the capability of contractors to center their processes on the target value.

AC, AV, and VMA all have target values about which two-sided specification limits are established. The typical within-lot standard deviation can be used to establish these specification limits. The STD, however, must decide whether or not a typical contractor can be expected to always be able to center its process exactly on the target value. If the STD believes this to be possible, then the typical process standard deviation that was developed from the individual project values can be used when setting the specification limits. If, on the other hand, the STD believes that a typical contractor's process mean may vary about the target value, then it may be necessary to consider this fact when developing specification limits.

One approach would be to combine the "process center" variability and the "within–lot" variability by adding their associated variances, not their standard deviations. This assumes that the amount of process variability is independent of where the process is centered; an assumption that seems reasonable, particularly as long as the target miss is not very large.

If the STD does not believe that the contractor's process is constant throughout the life of a project, as would typically be the case when the agency has decided to use lot-by-lot acceptance, then there is no way to know how much of the lot-to-lot variation in sample means is from the natural variation of the sampling process and how much is due to misses, changes, or adjustments in the contractor's target mean during the project.

Therefore, a second approach might be to calculate a standard deviation based on combining all of the project data into one data set. While this is not a good way to establish a typical within–lot standard deviation, this approach will provide a larger standard deviation value that includes the lot–to–lot variation among the individual lot means. A decision to use this approach assumes that any "process center" variation within the project will be accounted for when all the test results are combined. The various project standard deviations could then be used to arrive at a typical process standard deviation that attempts to include both the "within–lot" and the possible "process center" variability.

# Density

As noted in Chapter 6, since the "target" values for Density are not in the centers of their respective specification limits, there is no real benefit to the contractor to attempt to hit these targets with its process. The contractor maximizes it chances of meeting the PWL requirement by aiming for the center of the specification limits. This allows for the largest standard deviation that can be obtained while still meeting the specification requirements for full payment. So, even though the specification lists "target" values, these target values were not considered when performing analyses on the density test results.

**Selecting the Project Variability.** With no "process target" variability available, if SCDOT thought it necessary to account for variability of the contractor's process mean, the best option would be to use the standard deviation for all tests on a given project.

<u>Interstate Paving Projects</u>. Table 8.1 shows the Density results for the Interstate paving projects. The table shows the average and standard deviation for all the average project lot means, as well as percentiles based on ranked order for both the Project and Lot standard deviation values. Also, Figure 8.1 shows the empirical CDF for the Project standard deviation values.

As the reference lines show, there is somewhat of a natural break at around the 65<sup>th</sup> percentile. Actually, at around 1.38, there is very little difference between the 65<sup>th</sup> and 80<sup>th</sup> percentiles.

In Chapter 6, the within-lot standard deviation was shown to be around 1.16 for Interstate projects. SCDOT will need to decide whether to use the within-lot or project standard deviation when establishing its specification limits for Density.

| Nun       | nber    | Mea       | n of *    | Std Deviation* |       |  |
|-----------|---------|-----------|-----------|----------------|-------|--|
| Project   | JMF     | All Tests | Lot Means | Project        | Lot   |  |
| P01       | J10     | 92.90     | 92.85     | 0.599          | 0.515 |  |
| P01       | J07     | 93.26     | 93.24     | 0.801          | 0.543 |  |
| P01       | J07     | 92.73     | 92.77     | 0.591          | 0.546 |  |
| P23       | J63     | 93.11     | 93.11     | 0.584          | 0.607 |  |
| P01       | J02     | 93.94     | 93.56     | 0.908          | 0.848 |  |
| P32       | J72     | 93.07     | 93.06     | 0.861          | 0.854 |  |
| P32       | J79     | 92.77     | 92.77     | 0.943          | 0.868 |  |
| P03       | J15     | 93.23     | 93.41     | 1.272          | 0.957 |  |
| P26       | J62     | 92.85     | 92.84     | 1.366          | 1.052 |  |
| P32       | J76     | 93.27     | 93.27     | 1.072          | 1.059 |  |
| P26       | J69     | 93.39     | 93.40     | 1.210          | 1.126 |  |
| P33       | J77     | 92.67     | 92.72     | 1.486          | 1.161 |  |
| P32       | J74     | 93.20     | 93.20     | 1.417          | 1.417 |  |
| P33       | J73     | 93.18     | 93.17     | 1.377          | 1.459 |  |
| P34       | J62     | 92.74     | 93.01     | 1.820          | 1.500 |  |
| P23       | J33     | 91.64     | 91.63     | 1.374          | 1.649 |  |
| Total / / | Average | Mean      | 93.00     | 1.105          | 1.010 |  |
|           |         | St Dev    | 0.445     |                |       |  |
|           |         |           | 50%       | 1.141          | 1.005 |  |
|           |         |           | 60%       | 1.272          | 1.059 |  |
|           |         |           | 70%       | 1.370          | 1.144 |  |
|           |         |           | 80%       | 1.377          | 1.417 |  |
|           |         |           | 90%       | 1.452          | 1.480 |  |

 Table 8.1. Summary of Density Test Results for Interstate Paving Projects

- \* All Tests: the mean of all individual test results on the project Lot Means: the mean of all the individual lot means on the project
- \*\* **Project:** the unbiased standard deviation estimate of all individual test results on the project **Lot:** the average of the unbiased standard deviation estimates for all lots on the project



Figure 8.1. CDF for the Project Standard Deviations for Density for Interstate Projects

<u>Other Paving Projects</u>. Table 8.2 shows the Density results for the Other paving projects. The table shows the average and standard deviation for all the average project lot means, as well as percentiles based on ranked order for both the Project and Lot standard deviation values.

The first thing that is apparent in the table is the large standard deviation value of 1.436 for the lot means for the projects. This reflects the high degree of variability among the different projects regarding the contractors' abilities to meet the target Density in the specification requirements. Indeed, this standard deviation was in general greater than the within-lot standard deviation values for the various projects. This indicates that regardless the standard deviation, many contractors had difficulty meeting the density requirements.

Figure 8.2 shows the empirical CDF for the Project standard deviation values. As the reference lines show, there is a natural break at around the 80<sup>th</sup> percentile, with a corresponding standard deviation value of about 1.47.

In Chapter 6, the within-lot standard deviation was shown to be around 1.20 to 1.26 for Other projects. SCDOT will need to decide whether to use the within-lot or project standard deviation when establishing its specification limits for Density.

| Number    |         | Mea       | n of *    | Std De  | viation* |
|-----------|---------|-----------|-----------|---------|----------|
| Project   | JMF     | All Tests | Lot Means | Project | Lot      |
| P31       | J71     | 94.12     | 94.15     | 0.517   | 0.616    |
| P27       | J55     | 92.29     | 92.30     | 0.674   | 0.632    |
| P20       | J50     | 92.38     | 92.42     | 0.938   | 0.945    |
| P06       | J24     | 91.47     | 91.69     | 1.751   | 0.995    |
| P24       | J56     | 93.12     | 93.20     | 1.078   | 1.001    |
| P03       | J04     | 93.73     | 93.59     | 1.388   | 1.053    |
| P16       | J20     | 91.58     | 91.58     | 1.087   | 1.063    |
| P27       | J70     | 92.95     | 92.92     | 1.036   | 1.091    |
| P26       | J59     | 91.03     | 91.22     | 1.343   | 1.170    |
| P14       | J16     | 92.46     | 92.55     | 1.313   | 1.179    |
| P06       | J26     | 90.05     | 90.05     | 1.181   | 1.181    |
| P08       | J11     | 88.65     | 88.65     | 1.203   | 1.203    |
| P28       | J39     | 93.26     | 93.28     | 1.298   | 1.242    |
| P04       | J14     | 89.77     | 89.80     | 1.312   | 1.262    |
| P01       | J23     | 93.75     | 93.77     | 1.160   | 1.403    |
| P36       | J09     | 92.76     | 92.83     | 1.439   | 1.524    |
| P13       | J03     | 92.01     | 92.01     | 1.567   | 1.567    |
| P15       | J44     | 92.68     | 92.68     | 1.465   | 1.584    |
| P30       | J65     | 93.74     | 93.80     | 2.486   | 1.989    |
| P18       | J48     | 91.55     | 91.65     | 1.824   | 2.042    |
| Total / A | Average | Mean      | 92.21     | 1.303   | 1.237    |
|           |         | St Dev    | 1.436     |         |          |
|           |         |           | 50%       | 1.305   | 1.090    |
|           |         |           | 60%       | 1.325   | 1.174    |
|           |         |           | 70%       | 1.403   | 1.188    |
|           |         |           | 80%       | 1.485   | 1.290    |
|           |         |           | 90%       | 1.758   | 1.569    |

Table 8.2. Summary of Density Test Results for Other Paving Projects

- \* All Tests: the mean of all individual test results on the project Lot Means: the mean of all the individual lot means on the project
- \*\* **Project:** the unbiased standard deviation estimate of all individual test results on the project **Lot:** the average of the unbiased standard deviation estimates for all lots on the project



Figure 8.2. CDF for the Project Standard Deviations for Density for Other Projects

**Density Specification Limits.** As noted in Chapter 6, for Interstate paving projects the lower and upper specification limits for density were 92.2 and 96.0, respectively. The limits for Other paving projects were 91.2 and 96.0. For the projects on which data were obtained, the target values for density were 94.0 for Interstate paving projects and 93.0 for Other paving projects. The current SCDOT specification requirements, effective May 2010, have the same specification limits, but now call for a target value of 94.0 for both "Interstate and US Primary Routes" and for "All Other Paving."

The typical process standard deviation that was used to develop the current Density specification limits was 1.09 (3). This value was used to determine the lower specification limits of 92.2 and 91.2. Note that each of these limits is 1.80 below the target value. This value was determined when SCDOT chose to set the limit such that 5% of the acceptable quality level (AQL) population would be below the limit. For any normal distribution, the point that is 1.645 standard deviation units below the mean will have 5% of the population below it. The specification limit therefore needed to be  $1.645 \times 1.09 = 1.80$  from the target value.

Next, it was necessary to consider how the standard deviation values compare with the existing SCDOT specification limits. Using a standard deviation value of 1.20, which is within the 1.16 to 1.26 range identified in Chapter 6, the acceptable quality level (AQL) is therefore a population with a mean of 94.0 and a standard deviation of 1.20. Note that the situation would be worse if one of the higher Project standard deviations, 1.38 or 1.47, were used. Using a population mean of 94.0, standard deviation of 1.20, and the specification limits, the AQL can be calculated in terms of PWL. Figure 8.3 shows a plot of the AQL population.

The AQL population also can be defined in terms of PWL by calculating the area under the normal curve between the lower and upper specification limits. Figure 8.4 shows the AQL population along with the specification limits for Interstate paving projects. The area within the specification limits, i.e., the PWL, can be calculated using a spreadsheet or statistical software program, or by using equation 8.1 and 8.2 to calculate the *Z*-values to use with a table of the standard normal distribution.

$$Z_L = \frac{\mu - L}{\sigma} \tag{8.1}$$

$$Z_U = \frac{U - \mu}{\sigma} \tag{8.2}$$

Where:

- $Z_L = Z$ -value corresponding to the lower specification limit.
  - L = Lower specification limit.
  - $Z_U$  = Z-value corresponding to the upper specification limit.
  - U = Upper specification limit.
  - $\overline{X}$  = Population mean.
  - $\sigma$  = Population standard deviation.



Figure 8.3. Plot of the AQL Population for Density



Figure 8.4. AQL Population for Density in Terms of PWL on Interstate Paving Projects

The PWL for the AQL population was calculated as 88.54. This is less than the PWL of 90 that is required for the contractor to receive 100 percent payment for the material placed.

Since the specified target value of 94.0 is not in the center of the specification region, it might be possible to increase the PWL value by centering the process at the center of the specification range, i.e., at 94.1. However, this raises the PWL only to 88.67, which is still below the 90 PWL requirement for full payment.

Therefore, SCDOT is faced with several options:

- **1.** Decide that a standard deviation value of approximately 1.20 is appropriate and use the current specification limits. This has the effect of requiring the contractor to provide better than AQL quality to average 100 percent payment in the long run. To do this, the contractor would need to produce a population with standard deviation less than 1.20.
- **2.** Decide that a standard deviation value of 1.20 was appropriate and modify the current specification limits so that the AQL population will have 90 percent within the revised limits.

It is relatively simple to calculate the new limits if the mean is at the center of the specification region. For example, if the target mean remains at 94.0, then with a standard deviation of 1.20, it can be calculated that the specification limits would need to be 92.03 and 95.97 to have exactly 90 PWL. These would likely be rounded to 92 and 96.

If SCDOT wishes to keep the lower specification limit at 92.2, then the mid-point for a symmetric specification region would correspond to the population mean that has 5% below the lower specification limit of 92.2. So, the population would need to have a mean that is  $1.645 \times 1.20 = 1.974$  units above the lower specification limit, or a value of 94.174.

The upper specification limit would then be 1.974 units above the mean, or a value of 96.148.

**3.** Decide that a standard deviation less than 1.20 was appropriate and use the current specification limits and target value. Using a trial-and-error process with Excel, it easily can be determined that selecting a standard deviation value of 1.15 (which is very near the value of 1.16 that was originally identified above for Interstate paving) will yield exactly 90.00 for the PWL of the AQL population.

The second and third options seem to be the better choice. Although, the first option really turns out to be the same as the third option. The third option merely quantifies the decrease in standard deviation that is alluded to in option 1. Since the selection of the appropriate process standard deviation is subjective, option 3 is the easiest to implement since it does not require any modification to the current specification limits or target value. While this is the easiest option, the analyses of the project data indicate that the contractors may have a difficult time consistently providing the necessary process standard deviation.

A possible standard deviation value that was calculated in Chapter 6 to use with Other paving projects was 1.20. Due to the fact the lower specification limit is 91.2 rather than 92.2, the AQL population for Other paving projects will be 94.24 PWL (see Figure 8.5). So, the current specification limits and target value for Other paving should not present a particular problem to meet with respect to variability. However, Table 8.2 shows that for the projects in this study there was quite a bit of difficulty in achieving the 93.0 target value that was in place at the time of the projects.



Figure 8.5. AQL Population for Density in Terms of PWL on Other Paving Projects

If a higher standard deviation in the range from 1.38 or 1.47, as calculated above, were selected as the typical standard deviation, then the situation would be much worse. For example, Figure 8.6 shows the AQL population if the current SCDOT specification limits for Interstate projects were used and the typical standard deviation was selected as 1.40. This results in an AQL of 82.4 in terms of PWL. This is quite far from the PWL of 90 that is required for full payment.



# Figure 8.6. AQL Population for Density in Terms of PWL on Interstate Paving Projects with Standard Deviation = 1.40

**Note of Caution:** As noted in Chapter 5, a STD may choose to establish the typical standard deviation value to use based on "data from a number of past projects that it considered acceptable." Considering that nearly two-thirds of the projects from which density data were obtained had average project PWL values less than 90 PWL, SCDOT must decide whether or not it wishes to establish the typical project standard deviation based on these data.

If SCDOT believes that these projects represent the state-of-the-art regarding the process capability of a typical contractor, then SCDOT may need to re-evaluate their target density value and their density specification limits. If SCDOT believes that these projects do not represent what a typical contractor is capable of providing, then additional data from other representative projects will need to be obtained for analysis.

# **Asphalt Content**

As noted in Chapter 7, the AC test data had specific target values. It was not possible to compare directly the actual test results since each project and each mix design had its own set of target values. It was possible, however, to normalize the data by considering the AC as differences from their target values. This made it possible to make comparisons among the various lots, mix designs, projects, mix types, and courses that could not be done on the actual test values.

**Selecting the Project Variability.** With a target value, if SCDOT thought it necessary, it could combine any potential "process target" variability with the selected "within-lot" variability to determine the overall typical process variability for AC. One approach to do this would be to add the "process center" variance and the "within–lot" variance. Another approach, as discussed above, would be to use the "Project" standard deviation values to select the typical process standard deviation.

<u>Base Course</u>. Table 8.3 shows the AC results for Base course mixes. The table shows the average and standard deviation for the average project Lot means, as well as percentiles based on ranked order for both the Project and Lot standard deviation values.

| Number  |        | Mea       | n of *    | Std Deviation* |        |  |
|---------|--------|-----------|-----------|----------------|--------|--|
| Project | JMF    | All Tests | Lot Means | Project        | Lot    |  |
| P27     | J66    | 0.0455    | 0.0455    | 0.2035         | _      |  |
| P24     | J57    | 0.1375    | 0.1375    | 0.1110         | 0.0517 |  |
| P02     | J28    | 0.0383    | 0.0404    | 0.2475         | 0.1832 |  |
| P01     | J01    | 0.0673    | 0.0398    | 0.2318         | 0.1933 |  |
| P28     | J47    | -0.0250   | -0.0385   | 0.2407         | 0.2193 |  |
| P01     | J18    | -0.0480   | -0.0564   | 0.2435         | 0.2237 |  |
| P01     | J06    | 0.0978    | 0.0942    | 0.2163         | 0.2512 |  |
| P02     | J17    | -0.0147   | 0.0022    | 0.2983         | 0.3225 |  |
| P01     | J21    | 0.1085    | 0.1324    | 0.2574         | 0.3360 |  |
| P26     | J45    | 0.0620    | 0.0423    | 0.3723         | 0.3406 |  |
| Total/A | verage | Mean      | 0.0439    | 0.2422         | 0.2357 |  |
|         |        | Std Dev   | 0.0648    |                |        |  |
|         |        |           | 50%       | 0.2421         | 0.2237 |  |
|         |        |           | 60%       | 0.2451         | 0.2457 |  |
|         |        |           | 70%       | 0.2505         | 0.2940 |  |
|         |        |           | 80%       | 0.2656         | 0.3279 |  |
|         |        |           | 90%       | 0.3057         | 0.3369 |  |

 Table 8.3. Summary of AC Test Results for Each Base Course Project

- \* All Tests: the mean of all individual test results on the project Lot Means: the mean of all the individual lot means on the project
- \*\* **Project:** the unbiased standard deviation estimate of all individual test results on the project **Lot:** the average of the unbiased standard deviation estimates for all lots on the project

In Chapter 7, the typical Base course within-lot standard deviation was found to be in the 0.25 to 0.295 range. For illustration, a value of 0.27 is used. In Table 8.3, the standard deviation of the project Lot means, 0.0648, might be used as an estimate for the process target standard deviation. Equation 8.3 can be used to combine these into a single typical process standard deviation.

$$\sqrt{(0.27)^2 + (0.0648)^2} = 0.278 \approx 0.28$$
 (8.3)

Using the lower and upper limits of the within-lot standard deviation results in limits of 0.258 to 0.302, or approximately 0.26 to 0.30.

Figure 8.7 shows the empirical CDF for the Project standard deviation values in Table 8.3. As the reference lines show, an obvious choice appears at the 80<sup>th</sup> percentile and a Project standard deviation of approximately 0.26, which is a little less than the one calculated using the within-lot and process target variabilities.



Figure 8.7. CDF for the Project Standard Deviations for AC for Base Course

<u>Intermediate Course</u>. Table 8.4 shows the AC results for Intermediate course mixes. The table shows the average and standard deviation for the average project Lot means, as well as percentiles based on ranked order for both the Project and Lot standard deviation values.

| Number  |        | Mea       | n of *    | Std De  | viation* |
|---------|--------|-----------|-----------|---------|----------|
| Project | JMF    | All Tests | Lot Means | Project | Lot      |
| P27     | J60    | 0.2613    | 0.2613    | 0.2445  | _        |
| P28     | J42    | 0.0847    | 0.0877    | 0.1950  | 0.1241   |
| P10     | J82    | -0.0313   | -0.0238   | 0.1963  | 0.1291   |
| P21     | J34    | 0.1025    | 0.0467    | 0.1861  | 0.1294   |
| P05     | J27    | -0.1187   | -0.1200   | 0.1290  | 0.1494   |
| P01     | J10    | 0.0036    | 0.0162    | 0.2016  | 0.1559   |
| P27     | J53    | -0.0000   | 0.0134    | 0.2079  | 0.1566   |
| P10     | J37    | 0.0250    | 0.0396    | 0.2067  | 0.1764   |
| P24     | J51    | 0.0287    | 0.0457    | 0.1627  | 0.1806   |
| P32     | J76    | 0.0935    | 0.0920    | 0.2078  | 0.1813   |
| P01     | J02    | 0.1217    | 0.1150    | 0.1734  | 0.1915   |
| P02     | J09    | 0.0218    | 0.1190    | 0.2479  | 0.2058   |
| P25     | J29    | -0.1567   | -0.1614   | 0.2091  | 0.2127   |
| P02     | J04    | 0.1290    | 0.1815    | 0.2260  | 0.2131   |
| P17     | J22    | 0.0036    | -0.0175   | 0.2648  | 0.2322   |
| P33     | J73    | 0.0520    | 0.0783    | 0.2283  | 0.2585   |
| P04     | J08    | 0.1800    | 0.1959    | 0.3053  | 0.2916   |
| P10     | J31    | 0.0129    | 0.0222    | 0.2583  | 0.2984   |
| P01     | J23    | 0.1050    | 0.0936    | 0.3111  | 0.4165   |
| Total/A | verage | Mean      | 0.0571    | 0.2190  | 0.2057   |
|         |        | Std Dev   | 0.1011    |         |          |
|         |        |           | 50%       | 0.2079  | 0.1864   |
|         |        |           | 60%       | 0.2226  | 0.2072   |
|         |        |           | 70%       | 0.2380  | 0.2131   |
|         |        |           | 80%       | 0.2521  | 0.2480   |
|         |        |           | 90%       | 0.2729  | 0.2936   |

## Table 8.4. Summary of AC Test Results for Each Intermediate Course Project

- \* All Tests: the mean of all individual test results on the project Lot Means: the mean of all the individual lot means on the project
- \*\* **Project:** the unbiased standard deviation estimate of all individual test results on the project **Lot:** the average of the unbiased standard deviation estimates for all lots on the project

In Chapter 7, the typical Intermediate course within-lot standard deviation was found to be in the 0.21 to 0.26 range. For illustration, a value of 0.24 is used. In Table 8.4, the standard deviation of the project Lot means might be used as an estimate for the process target standard deviation. Equation 8.4 can be used to combine these into a single typical process standard deviation.

$$\sqrt{(0.24)^2 + (0.1011)^2} = 0.260$$
 (8.4)

Using the lower and upper limits of the within-lot standard deviation results in limits of 0.233 to 0.279, or approximately 0.23 to 0.28.

Figure 8.8 shows the empirical CDF for the Project standard deviation values in Table 8.4. As the reference lines show, an obvious choice appears at approximately the 80<sup>th</sup> percentile and a Project standard deviation of about 0.25, which is consistent with the one calculated using the within-lot and process target variabilities.



Figure 8.8. CDF for the Project Standard Deviations for AC for Intermediate Course

<u>Surface Course</u>. Table 8.5 shows the AC results for Surface course mixes. The table shows the average and standard deviation for the average project Lot means, as well as percentiles based on ranked order for both the Project and Lot standard deviation values.

In Chapter 7, the typical Surface course within-lot standard deviation was found to be in the 0.195 to 0.215 range. For illustration, a value of 0.205 is used. In Table 8.5, the standard deviation of the project Lot means might be used as an estimate for the process target standard deviation. Equation 8.6 can be used to combine these into a single typical process standard deviation.

$$\sqrt{(0.205)^2 + (0.0788)^2} = 0.220$$
 (8.6)

Using the lower and upper limits of the within-lot standard deviation results in limits of 0.210 to 0.229, or approximately 0.21 to 0.23.

Figure 8.9 shows the empirical CDF for the Project standard deviation values in Table 8.5. As the reference lines show, an obvious choice appears at approximately the 80<sup>th</sup> percentile and a Project standard deviation of 0.21, which is consistent with the one calculated using the within-lot and process target variabilities.

| Num     | Number Mean of * |           | Std De    | viation* |        |  |  |
|---------|------------------|-----------|-----------|----------|--------|--|--|
| Project | JMF              | All Tests | Lot Means | Project  | Lot    |  |  |
| P05     | J25              | -0.1313   | -0.1313   | 0.1884   | —      |  |  |
| P27     | J61              | -0.0589   | -0.0589   | 0.1290   | —      |  |  |
| P33     | J75              | -0.0150   | -0.0150   | 0.1885   | —      |  |  |
| P24     | J64              | 0.1431    | 0.1443    | 0.0574   | 0.0473 |  |  |
| P22     | J54              | 0.0467    | 0.0647    | 0.0845   | 0.0609 |  |  |
| P24     | J67              | 0.0590    | 0.1667    | 0.6117   | 0.0682 |  |  |
| P02     | J05              | -0.0050   | -0.0117   | 0.1506   | 0.0798 |  |  |
| P34     | J80              | -0.0058   | -0.0286   | 0.1030   | 0.0806 |  |  |
| P30     | J65              | -0.0100   | 0.0000    | 0.0905   | 0.1000 |  |  |
| P07     | J30              | -0.0940   | -0.0971   | 0.1463   | 0.1034 |  |  |
| P21     | J39              | 0.0007    | -0.0026   | 0.1283   | 0.1078 |  |  |
| P02     | J13              | -0.0572   | -0.0318   | 0.2949   | 0.1130 |  |  |
| P35     | J38              | 0.0536    | 0.0495    | 0.1249   | 0.1171 |  |  |
| P11     | J41              | 0.0710    | 0.0721    | 0.1731   | 0.1190 |  |  |
| P26     | J52              | -0.0621   | -0.0525   | 0.1452   | 0.1211 |  |  |
| P32     | J79              | 0.1139    | 0.1106    | 0.1622   | 0.1253 |  |  |
| P29     | J59              | -0.0458   | -0.0494   | 0.1427   | 0.1296 |  |  |
| P13     | J43              | -0.0011   | -0.0020   | 0.1554   | 0.1305 |  |  |
| P35     | J32              | -0.0507   | -0.0294   | 0.1513   | 0.1347 |  |  |
| P09     | J35              | -0.0178   | -0.0178   | 0.1492   | 0.1349 |  |  |
| P06     | J24              | 0.0647    | 0.0647    | 0.1732   | 0.1438 |  |  |
| P01     | J19              | 0.0828    | 0.1007    | 0.1435   | 0.1462 |  |  |
| P28     | J39              | 0.0429    | 0.0149    | 0.1542   | 0.1486 |  |  |
| P34     | J62              | -0.0232   | -0.0225   | 0.2043   | 0.1496 |  |  |
| P26     | J69              | 0.0029    | -0.0201   | 0.1949   | 0.1531 |  |  |
| P12     | J38              | 0.0536    | 0.0676    | 0.1820   | 0.1592 |  |  |
| P20     | J50              | 0.0202    | 0.0484    | 0.1923   | 0.1648 |  |  |
| P18     | J48              | 0.1117    | 0.1164    | 0.2138   | 0.1701 |  |  |
| P05     | J40              | -0.1344   | -0.1180   | 0.1756   | 0.1726 |  |  |
| P32     | J46              | -0.0220   | -0.0157   | 0.1792   | 0.1736 |  |  |
| P26     | J62              | 0.0145    | 0.0082    | 0.1791   | 0.1741 |  |  |
| P02     | J15              | -0.0122   | 0.0501    | 0.2058   | 0.1750 |  |  |
| P01     | J07              | -0.0243   | -0.0212   | 0.1808   | 0.1811 |  |  |
| P32     | J72              | 0.0706    | 0.0773    | 0.1740   | 0.1819 |  |  |
| P27     | J71              | 0.0559    | 0.0597    | 0.1621   | 0.1882 |  |  |
| P09     | J83              | -0.0413   | -0.0333   | 0.1954   | 0.1891 |  |  |
| P14     | J16              | -0.1769   | -0.1827   | 0.2113   | 0.1937 |  |  |
| P04     | J14              | 0.0618    | 0.0575    | 0.1937   | 0.2051 |  |  |
| P10     | J12              | -0.0374   | -0.0373   | 0.2781   | 0.2083 |  |  |
| P16     | J20              | -0.1811   | -0.1811   | 0.2351   | 0.2103 |  |  |
| P19     | J49              | -0.0775   | -0.0788   | 0.2602   | 0.2105 |  |  |
|         | Continued        |           |           |          |        |  |  |

# Table 8.5. Summary of AC Test Results for Each Surface Course Project

| Number  |        | Mea       | n of *    | Std Deviation* |        |
|---------|--------|-----------|-----------|----------------|--------|
| Project | JMF    | All Tests | Lot Means | Project        | Lot    |
| P27     | J55    | 0.1287    | 0.1287    | 0.1947         | 0.2122 |
| P24     | J56    | 0.0000    | 0.0759    | 0.2507         | 0.2161 |
| P33     | J77    | 0.0973    | 0.0988    | 0.2472         | 0.2295 |
| P26     | J58    | -0.0031   | 0.0050    | 0.1707         | 0.2481 |
| P34     | J81    | 0.0923    | 0.0971    | 0.2117         | 0.2600 |
| P25     | J36    | 0.0570    | 0.0458    | 0.2081         | 0.2906 |
| P13     | J03    | -0.0100   | -0.0458   | 0.2735         | 0.3268 |
| P33     | J78    | 0.0492    | 0.0419    | 0.3541         | 0.3556 |
| P26     | J68    | -0.0970   | -0.0879   | 0.4339         | 0.4153 |
| Total/A | verage | Mean      | 0.0079    | 0.1962         | 0.1708 |
|         |        | Std Dev   | 0.0078    |                |        |
|         |        |           | 50%       | 0.1800         | 0.1648 |
|         |        |           | 60%       | 0.1929         | 0.1746 |
|         |        |           | 70%       | 0.2048         | 0.1900 |
|         |        |           | 80%       | 0.2181         | 0.2105 |
|         |        |           | 90%       | 0.2740         | 0.2529 |

#### Table 8.5. Summary of AC Test Results for Each Surface Course Project (continued)

- \* All Tests: the mean of all individual test results on the project Lot Means: the mean of all the individual lot means on the project
- \*\* **Project:** the unbiased standard deviation estimate of all individual test results on the project **Lot:** the average of the unbiased standard deviation estimates for all lots on the project





**Asphalt Content Specification Limits.** As noted in Chapter 7, different allowable tolerances (specification limits) currently apply to Base, Intermediate, and Surface courses. For each course, tolerances were developed by multiplying 1.645 times the typical process standard deviation for the course. The typical process standard deviations that SCDOT used were 0.30 for Base course, 0.26 for Intermediate course, and 0.22 for Surface course (<u>3</u>). These calculations resulted in tolerances of  $1.645 \times 0.3 = 0.50$  for Base,  $1.645 \times 0.26 = 0.43$  for Intermediate, and  $1.645 \times 0.22 = 0.36$  for Surface.

The current standard deviations can be compared with those in the previous sections that were calculated from the data collected for this report. Table 8.6 shows such a comparison.

| Course       | Std Dev Assumed<br>in Current<br>Specification | From Combined<br>Within-Lot & Target<br>Std Dev | From Total Project<br>Std Dev<br>80 <sup>th</sup> Percentile |
|--------------|--|---|--|
| Base         | 0.30   | 0.26-0.30                                       | 0.26   |
| Intermediate | 0.26   | 0.23-0.28                                       | 0.25   |
| Surface      | 0.22   | 0.21-0.23                                       | 0.21   |

# Table 8.6. Comparison of Current SCDOT Standard Deviations with Those from the NewProject Data

In Table 8.6 there are no obvious inconsistencies among the currently assumed standard deviation values and those calculated based on the project data for the current research. Based on these values, the SCDOT may consider tightening slightly the Base AC tolerances. However, based on the limited number of projects for which Base course data were provided, a change at this time may not be warranted. There is no compelling evidence that indicates that a change is warranted for either the Intermediate or Surface tolerances.

# Air Voids

As noted in Chapter 7, the AV test data had specific target values. It was not possible to compare directly the actual test results since each project and each mix design had its own set of target values. It was possible, however, to normalize the data by considering the AV as differences from their target values. This made it possible to make comparisons among the various lots, mix designs, projects, mix types, and courses that could not be done on the actual test values.

**Selecting the Project Variability.** With a target value, if SCDOT thought it necessary, it could combine any potential "process target" variability with the selected "within-lot" variability to determine the overall typical process variability for AV. One approach to do this would be to add the "process center" variance and the "within–lot" variance. Another approach, as discussed above, would be to use the "Project" standard deviation values to select the typical process standard deviation.

Table 8.7 shows the AV results. The table shows the average and standard deviation for the average project Lot means, as well as percentiles based on ranked order for both the Project and Lot standard deviation values.

In Chapter 7, the typical within-lot standard deviation was found to be in the 0.525 to 0.59 range. For illustration, a value of 0.56 is used. In Table 8.7, the standard deviation of the project Lot means, 0.3524, might be used as an estimate for the process target standard deviation. Equation 8.7 can be used to combine these into a single typical process standard deviation.

$$\sqrt{(0.56)^2 + (0.3524)^2} = 0.662 \approx 0.66$$
(8.7)

Using the lower and upper limits of the within-lot standard deviation results in limits of 0.632 to 0.687, or approximately 0.63 to 0.69.

Figure 8.10 shows the empirical CDF for the Project standard deviation values in Table 8.7. There is not an obvious natural break point, although as the reference lines show, likely choices include a Project standard deviation of 0.64 at the 80<sup>th</sup> percentile or 0.685 at the 85<sup>th</sup> percentile. This is approximately the same range as the one calculated using the within-lot and process target variabilities.

Table 8.7. Summary of AV Test Results

| Num       | Number Mean of * |           | Std Deviation* |         |        |
|-----------|------------------|-----------|----------------|---------|--------|
| Project   | JMF              | All Tests | Lot Means      | Project | Lot    |
| P27       | J60              | 0.0080    | 0.0080         | 0.6414  | —      |
| P05       | J25              | 0.011     | 0.0113         | 0.5534  | —      |
| P27       | J61              | -0.364    | -0.3644        | 0.5365  | —      |
| P27       | J53              | -0.1810   | -0.1811        | 0.4510  | 0.0443 |
| P21       | J39              | -0.8340   | -0.7936        | 0.1504  | 0.1451 |
| P24       | J64              | -0.6423   | -0.5964        | 0.2932  | 0.1935 |
| P26       | J58              | 0.281     | 0.1821         | 0.6810  | 0.2038 |
| P10       | J37              | 0.5327    | 0.5371         | 0.3971  | 0.2207 |
| P10       | J82              | 0.7847    | 0.7869         | 0.2928  | 0.2216 |
| P28       | J39              | -0.5963   | -0.5436        | 0.2858  | 0.2291 |
| P30       | J65              | 0.5100    | 0.4867         | 0.2434  | 0.2316 |
| P25       | J29              | 0.6360    | 0.5929         | 0.5074  | 0.2375 |
| P35       | J38              | 0.0358    | 0.0815         | 0.3844  | 0.2381 |
| P32       | J72              | -0.0374   | -0.0719        | 0.5010  | 0.2384 |
| P29       | J59              | -0.0069   | -0.0072        | 0.2840  | 0.2487 |
| P02       | J04              | -0.1630   | -0.0838        | 0.5799  | 0.2696 |
| P18       | J48              | -0.442    | -0.4002        | 0.8357  | 0.2787 |
| P05       | J27              | 0.2327    | 0.2256         | 0.3932  | 0.2823 |
| P02       | J13              | 0.457     | 0.3721         | 0.5307  | 0.2880 |
| P11       | J41              | 0.106     | 0.0977         | 0.4256  | 0.3034 |
| P34       | J81              | 0.075     | 0.0907         | 0.5851  | 0.3057 |
| P32       | J76              | -0.6007   | -0.5974        | 0.3272  | 0.3108 |
| P01       | J10              | -0.3559   | -0.4066        | 0.4875  | 0.3224 |
| P09       | J35              | 0.293     | 0.2933         | 0.5066  | 0.3475 |
| P21       | J34              | -0.0100   | 0.0833         | 0.3834  | 0.3477 |
| P01       | J23              | -0.328    | -0.3075        | 0.3550  | 0.3523 |
| P04       | J14              | 0.244     | 0.2433         | 0.5231  | 0.3691 |
| P02       | J15              | 0.532     | 0.2926         | 0.5602  | 0.3942 |
| P02       | J05              | 0.331     | 0.3942         | 0.4435  | 0.3944 |
| P01       | J07              | 0.3303    | 0.3323         | 0.5090  | 0.3991 |
| P33       | J77              | 0.462     | 0.4626         | 0.6375  | 0.4186 |
| P27       | J55              | 0.133     | 0.1333         | 0.4469  | 0.4258 |
| P32       | J79              | -0.2536   | -0.2436        | 0.4877  | 0.4356 |
| P10       | J31              | 0.1560    | 0.1524         | 0.5677  | 0.4411 |
| P02       | J09              | -0.0912   | -0.0825        | 0.5091  | 0.4415 |
| P26       | J69              | 0.1649    | 0.2549         | 0.6703  | 0.4460 |
| P35       | J32              | 0.399     | 0.3861         | 0.5372  | 0.4463 |
| P20       | J50              | -0.2567   | -0.3337        | 0.5495  | 0.4515 |
| P06       | J24              | -0.391    | -0.3907        | 0.4286  | 0.4613 |
| P01       | J02              | -0.301    | -0.2750        | 0.5772  | 0.4763 |
| P33       | J73              | 0.1260    | 0.0860         | 0.5295  | 0.4808 |
| Continued |                  |           |                |         |        |

| Number  |        | Mean of * |           | Std Deviation* |         |
|---------|--------|-----------|-----------|----------------|---------|
| Project | JMF    | All Tests | Lot Means | Project        | Lot     |
| P09     | J83    | -0.310    | -0.3633   | 0.6073         | 0.4908  |
| P26     | J62    | 0.335     | 0.3689    | 0.6000         | 0.4910  |
| P24     | J67    | -0.192    | -0.1569   | 0.7268         | 0.5045  |
| P07     | J30    | 0.0193    | 0.0884    | 0.5036         | 0.5144  |
| P14     | J16    | -0.447    | -0.3851   | 0.7389         | 0.5168  |
| P01     | J19    | -0.4180   | -0.3925   | 0.5957         | 0.5251  |
| P04     | J08    | 0.1330    | 0.1330    | 0.4534         | 0.5619  |
| P34     | J62    | 0.152     | 0.1174    | 0.6853         | 0.5621  |
| P10     | J12    | 0.415     | 0.3935    | 0.6317         | 0.5627  |
| P27     | J71    | 0.2059    | 0.2039    | 0.5061         | 0.5727  |
| P19     | J49    | -0.514    | -0.4204   | 0.5826         | 0.5758  |
| P12     | J38    | -0.643    | -0.7899   | 0.7625         | 0.5774  |
| P13     | J03    | -0.212    | -0.0487   | 0.7148         | 0.5782  |
| P28     | J42    | -0.0290   | -0.0092   | 0.4540         | 0.5938  |
| P25     | J36    | 0.375     | 0.4125    | 0.6240         | 0.6116  |
| P24     | J56    | -0.263    | -0.1499   | 0.8253         | 0.6368  |
| P17     | J22    | -0.4240   | -0.3875   | 0.5813         | 0.6717  |
| P13     | J43    | 0.067     | 0.1515    | 0.8538         | 0.7440  |
| P16     | J20    | 0.164     | 0.1644    | 0.7841         | 0.7990  |
| P22     | J54    | 0.112     | 0.2432    | 0.8910         | 0.8222  |
| Total/A | verage | Mean      | 0.0013    | 0.5363         | 0.4182  |
|         |        | Std Dev   | 0.3524    |                |         |
|         |        |           | 50%       | 0.5307         | 0.43070 |
|         |        |           | 60%       | 0.5677         | 0.45346 |
|         |        |           | 70%       | 0.5957         | 0.50315 |
|         |        |           | 80%       | 0.6414         | 0.56246 |
|         |        |           | 90%       | 0.7389         | 0.59914 |

## Table 8.7. Summary of AV Test Results (continued)

- \* All Tests: the mean of all individual test results on the project Lot Means: the mean of all the individual lot means on the project
- \*\* **Project:** the unbiased standard deviation estimate of all individual test results on the project **Lot:** the average of the unbiased standard deviation estimates for all lots on the project



Figure 8.10. CDF for the Project Standard Deviations for AV

Air Voids Specification Limits. The current specification tolerances for AV were developed by multiplying 1.645 times the typical process standard deviation. The typical process standard deviation that SCDOT used was 0.70 (3). This calculation resulted in the current tolerances of  $1.645 \times 0.7 = 1.15$ .

The currently assumed standard deviation value is consistent with the ranges calculated based on the project data for the current research. Based on these values, the SCDOT may consider tightening slightly the AV tolerances, however, the results do not provide compelling evidence that a change is warranted.

# VMA

As noted in Chapter 7, the VMA test data had specific target values. It was not possible to compare directly the actual test results since each project and each mix design had its own set of target values. It was possible, however, to normalize the data by considering the VMA as differences from their target values. This made it possible to make comparisons among the various lots, mix designs, projects, mix types, and courses that could not be done on the actual test values.

**Selecting the Project Variability.** With a target value, if SCDOT thought it necessary, it could combine any potential "process target" variability with the selected "within-lot" variability to determine the overall typical process variability for VMA. One approach to do this would be to add the "process center" variance and the "within–lot" variance. Another

approach, as discussed above, would be to use the "Project" standard deviation values to select the typical process standard deviation.

Table 8.8 shows the VMA results. The table shows the average and standard deviation for the average project Lot means, as well as percentiles based on ranked order for both the Project and Lot standard deviation values.

In Chapter 7, the typical within-lot standard deviation was found to be in the 0.55 to 0.63 range. For illustration, a value of 0.59 is used. In Table 8.8, the standard deviation of the project Lot means, 0.3279, might be used as an estimate for the process target standard deviation. Equation 8.8 can be used to combine these into a single typical process standard deviation.

$$\sqrt{(0.59)^2 + (0.3279)^2} = 0.675$$
(8.8)

Using the lower and upper limits of the within-lot standard deviation results in limits of 0.64 to 0.71.

Figure 8.11 shows the empirical CDF for the Project standard deviation values in Table 8.8. There appears to be a natural break point at a Project standard deviation of approximately 0.66 at the 90<sup>th</sup> percentile. This is within the range calculated using the within-lot and process target variabilities.

**VMA Specification Limits.** The current specification tolerances for VMA were developed by multiplying 1.645 times the typical process standard deviation. The typical process standard deviation that SCDOT used was 0.70 (<u>3</u>). This calculation resulted in the current tolerances of  $1.645 \times 0.7 = 1.15$ .

The currently assumed standard deviation value is consistent with the ranges calculated based on the project data for the current research. Based on these values, the results do not provide compelling evidence that a change is warranted.

| Table 8.8. Summa | ry of VMA | <b>Test Results</b> |
|------------------|-----------|---------------------|
|------------------|-----------|---------------------|

| Num     | nber Mean |           | an of * Std Deviat |         | viation* |
|---------|-----------|-----------|--------------------|---------|----------|
| Project | JMF       | All Tests | Lot Means          | Project | Lot      |
| P27     | J60       | 0.611     | 0.6107             | 0.5202  |          |
| P05     | J25       | -0.221    | -0.2213            | 0.7627  | _        |
| P27     | J61       | -0.286    | -0.2856            | 0.5550  | _        |
| P21     | J34       | 0.2300    | 0.1942             | 0.1737  | 0.1290   |
| P21     | J39       | -0.7020   | -0.6738            | 0.2255  | 0.1744   |
| P28     | J39       | -0.4029   | -0.4229            | 0.2105  | 0.1827   |
| P24     | J64       | -0.2123   | -0.1971            | 0.2673  | 0.1920   |
| P02     | J05       | 0.353     | 0.3975             | 0.3223  | 0.2083   |
| P30     | J65       | 0.4800    | 0.4800             | 0.1793  | 0.2270   |
| P29     | J59       | -0.0165   | -0.0273            | 0.3254  | 0.2577   |
| P26     | J69       | 0.1757    | 0.2076             | 0.4618  | 0.2928   |
| P33     | J73       | 0.1468    | 0.1714             | 0.4241  | 0.2938   |
| P10     | J12       | 0.249     | 0.2435             | 0.6966  | 0.3057   |
| P13     | J03       | -0.089    | -0.0267            | 0.4260  | 0.3149   |
| P20     | J50       | -0.2063   | -0.2124            | 0.4182  | 0.3178   |
| P35     | J32       | 0.233     | 0.2633             | 0.4628  | 0.3182   |
| P10     | J82       | 0.651     | 0.6731             | 0.5945  | 0.3279   |
| P02     | J13       | 0.233     | 0.2046             | 0.6190  | 0.3567   |
| P35     | J38       | 0.1622    | 0.1899             | 0.3280  | 0.3607   |
| P01     | J10       | -0.2841   | -0.3032            | 0.4725  | 0.3657   |
| P11     | J41       | 0.3030    | 0.2931             | 0.2468  | 0.3680   |
| P34     | J62       | 0.0946    | 0.0602             | 0.4099  | 0.3731   |
| P27     | J55       | 0.4627    | 0.4627             | 0.3515  | 0.3754   |
| P02     | J04       | 0.218     | 0.4242             | 0.5880  | 0.3765   |
| P24     | J56       | -0.2148   | -0.1542            | 0.5214  | 0.3821   |
| P32     | J72       | 0.1409    | 0.1268             | 0.4499  | 0.3933   |
| P18     | J48       | -0.057    | -0.0107            | 0.6577  | 0.3949   |
| P26     | J62       | 0.3458    | 0.3665             | 0.4341  | 0.3949   |
| P09     | J35       | 0.230     | 0.2300             | 0.4447  | 0.3995   |
| P25     | J29       | 0.438     | 0.3879             | 0.4818  | 0.4023   |
| P05     | J27       | 0.051     | 0.0413             | 0.4265  | 0.4077   |
| P33     | J77       | 0.126     | 0.1761             | 0.6578  | 0.4098   |
| P32     | J76       | -0.0809   | -0.0884            | 0.4439  | 0.4136   |
| P07     | J30       | -0.0288   | 0.0262             | 0.4594  | 0.4234   |
| P14     | J16       | -0.7066   | -0.6616            | 0.5427  | 0.4245   |
| P01     | J07       | 0.2430    | 0.2536             | 0.4805  | 0.4326   |
| P32     | J79       | 0.0493    | 0.0514             | 0.5533  | 0.4482   |
| P01     | J19       | -0.036    | 0.0307             | 0.6343  | 0.4564   |
| P27     | J53       | 0.035     | 0.0300             | 0.4632  | 0.4786   |
| P16     | J20       | -0.234    | -0.2344            | 0.4529  | 0.4793   |

| Number  |        | Mean of * |           | Std Deviation* |        |
|---------|--------|-----------|-----------|----------------|--------|
| Project | JMF    | All Tests | Lot Means | Project        | Lot    |
| P02     | J15    | 0.404     | 0.3438    | 0.5998         | 0.4860 |
| P19     | J49    | -0.590    | -0.5126   | 0.5948         | 0.4926 |
| P34     | J81    | 0.469     | 0.3186    | 0.4789         | 0.5110 |
| P27     | J71    | 0.3057    | 0.3144    | 0.3086         | 0.5121 |
| P04     | J14    | 0.356     | 0.3465    | 0.5180         | 0.5125 |
| P02     | J09    | 0.040     | 0.0211    | 0.6398         | 0.5249 |
| P10     | J37    | 0.402     | 0.4317    | 0.7225         | 0.5353 |
| P06     | J24    | -0.210    | -0.2100   | 0.5100         | 0.5491 |
| P28     | J42    | 0.169     | 0.1958    | 0.5161         | 0.5716 |
| P24     | J67    | -0.354    | -0.3350   | 0.4534         | 0.5878 |
| P13     | J43    | 0.155     | 0.2220    | 0.5851         | 0.5881 |
| P10     | J31    | 0.2103    | 0.2279    | 0.6405         | 0.5970 |
| P12     | J38    | -0.454    | -0.5500   | 0.6565         | 0.6036 |
| P17     | J22    | -0.468    | -0.4875   | 0.5188         | 0.6221 |
| P09     | J83    | -0.331    | -0.3622   | 0.5793         | 0.6334 |
| P26     | J58    | 0.288     | 0.2204    | 0.5575         | 0.6824 |
| P01     | J23    | -0.025    | -0.0232   | 0.4910         | 0.6908 |
| P01     | J02    | 0.021     | -0.0346   | 0.5575         | 0.7095 |
| P22     | J54    | 0.217     | 0.3628    | 0.7651         | 0.7207 |
| P25     | J36    | 0.700     | 0.7069    | 0.7762         | 0.8118 |
| P04     | J08    | 0.607     | 0.6070    | 0.7628         | 0.9022 |
| Total/A | verage | Mean      | 0.0800    | 0.4980         | 0.4432 |
|         |        | Std Dev   | 0.3279    |                |        |
|         |        |           | 50%       | 0.4910         | 0.4117 |
|         |        |           | 60%       | 0.5214         | 0.4608 |
|         |        |           | 70%       | 0.5793         | 0.5120 |
|         |        |           | 80%       | 0.6190         | 0.5813 |
|         |        |           | 90%       | 0.6578         | 0.6481 |

Table 8.8. Summary of VMA Test Results (continued)

- \* All Tests: the mean of all individual test results on the project Lot Means: the mean of all the individual lot means on the project
- \*\* **Project:** the unbiased standard deviation estimate of all individual test results on the project **Lot:** the average of the unbiased standard deviation estimates for all lots on the project



Figure 8.10. CDF for the Project Standard Deviations for VMA

# Payment Considerations

SCDOT uses equation 8.9 along with the estimated PWL value for the lot to determine the payment factor for each quality characteristic, i.e., Density, AC, AV, and VMA.

$$PF = 55 + 0.5(TPWL)$$
(8.9)

Where: PF = Percent pay factor for each quality characteristic. TPWL = Total estimated percent within limits.

Once the individual payment factors have been calculated, the payment factor for the lot is determined from the composite payment equation in equation 8.10.

$$LPF = 0.30(PF_{AC}) + 0.25(PF_{AV}) + 0.10(PF_{VMA}) + 0.35(PF_{Den})$$
(8.10)

Where:LPF= Percent pay factor for the lot. $PF_{AC}$ = Percent pay factor for asphalt content. $PF_{AV}$ = Percent pay factor for air voids. $PF_{VMA}$ = Percent pay factor for VMA. $PF_{Den}$ = Percent pay factor for density

**Correlated Characteristics.** Equation 8.10 implicitly assumes that the quality characteristics are statistically independent of one another. The test data were analyzed to investigate any possible correlations among the acceptance quality characteristics. Since there is a one-to-one correspondence among each AC, AV, and VMA test it was possible to calculate linear correlation coefficients for the 3 pairwise combinations of AC-AV, AC-VMA, and AV-VMA.

However, since the lots for AC, AV, and VMA were based on tonnage at the plant, whereas the lots for density were based on paving lane length, there was no direct comparison possible between individual density and plant tests. There was, however, a direct correspondence between the plant test means and the density test means for each lot on a project. While field conditions in addition to the materials will affect the density obtained in the field, nevertheless the Density, AC, AV, and VMA means for each lot were analyzed to identify whether or not correlation was present.

Since there may be different levels or lack of correlation for different courses, mix types, job mix formulas, etc., each project was treated individually when calculating the correlation coefficients. Table 8.9 shows the correlation coefficient for the individual plant test values for each Intermediate course project for which AC, AV, and VMA results were all available. Table 8.10 shows similar information for Surface course projects. To obtain better estimates for the correlation coefficients, projects with fewer than 10 sets of plant tests were not included in the analyses.

| Braiget No  |          | No. of | Linear Correlation Coefficient |         |         |
|-------------|----------|--------|--------------------------------|---------|---------|
| Project No. | JINF NO. | Tests  | AC-AV*                         | AC-VMA* | AV-VMA* |
| P01         | J10      | 39     | -0.437                         | 0.570   | 0.487   |
| P01         | J23      | 12     | -0.791                         | 0.920   | -0.491  |
| P02         | J04      | 30     | -0.429                         | 0.508   | 0.558   |
| P02         | J09      | 34     | -0.237                         | 0.706   | 0.517   |
| P04         | J08      | 21     | -0.301                         | 0.877   | 0.194   |
| P10         | J31      | 77     | -0.369                         | 0.603   | 0.518   |
| P10         | J37      | 22     | -0.313                         | 0.723   | 0.170   |
| P10         | J82      | 15     | 0.348                          | 0.902   | 0.711   |
| P17         | J22      | 11     | -0.604                         | 0.530   | 0.354   |
| P25         | J29      | 12     | -0.485                         | 0.508   | 0.500   |
| P27         | J53      | 19     | -0.450                         | 0.591   | 0.452   |
| P27         | J60      | 15     | -0.584                         | 0.413   | 0.497   |
| P28         | J42      | 15     | -0.312                         | 0.623   | 0.545   |
| P32         | J76      | 43     | -0.271                         | 0.752   | 0.271   |
| P33         | J73      | 25     | -0.654                         | 0.494   | 0.334   |
| Total / A   | Average  | 390    | -0.393                         | 0.648   | 0.374   |

| Table 8.9. Summary of Correlation Coefficients for Individual Tests for AC, AV, | and |
|---|-----|
| VMA for Intermediate Course Projects  |     |

\* Values in **Bold** are significantly different from 0 at the 0.05 significance level. Values in *Italics* are significantly different from 0 at the 0.10 significance level.

The results in Table 8.9 show that AC and AV are negatively correlated, whereas AC and VMA as well as AV and VMA are positively correlated. For the AC-AV correlations, 14 of 15 projects showed negative correlation coefficients, with 7 of the values significantly different than 0 at the 0.05 level of significance and another 2 values significantly different than 0 at the 0.10 level. For the AC-VMA correlations, all 15 projects showed positive correlation coefficients, with 12 of the values significantly different than 0 at the 0.05 level of significantly different than 0 at the 0.05 level of significantly different than 0 at the 0.05 level of significantly different than 0 at the 0.05 level of significantly different than 0 at the 0.05 level of significance

and another 2 values significantly different than 0 at the 0.10 level. For the AV-VMA correlations, 14 of 15 projects showed positive correlation coefficients, with 6 of the values significantly different than 0 at the 0.05 level of significance and another 4 values significantly different than 0 at the 0.10 level.

Similar trends are shown in Table 8.10. For the AC-AV correlations, 33 of 37 projects showed negative correlation coefficients, with 19 of the values significantly different than 0 at the 0.05 level of significance and another 4 values significantly different than 0 at the 0.10 level. For the AC-VMA correlations, 34 of 37 projects showed positive correlation coefficients, with 18 of the values significantly different than 0 at the 0.10 level. For the values significantly different than 0 at the 0.10 level. Significantly different than 0 at the 0.10 level. For the AV-VMA correlations, 36 of 37 projects showed positive correlation coefficients, with 30 of the values significantly different than 0 at the 0.05 level of significantly different than 0 at the 0.05 level of significantly different than 0 at the 0.05 level of significantly different than 0 at the 0.05 level of significantly different than 0 at the 0.05 level of significantly different than 0 at the 0.05 level of significantly different than 0 at the 0.05 level of significantly different than 0 at the 0.05 level of significantly different than 0 at the 0.05 level of significantly different than 0 at the 0.05 level of significantly different than 0 at the 0.05 level of significantly different than 0 at the 0.05 level of significantly different than 0 at the 0.05 level of significantly different than 0 at the 0.05 level of significantly different than 0 at the 0.05 level of significance.

Table 8.11 shows the correlation coefficient for the plant test lot means and the density test lot means for each project. Since the plant test correlations are considered in Tables 8.9 and 8.10, Table 8.11 includes only the Density correlation coefficient for each of the three plant test characteristics. Specifically, the Density-AC, Density-AV, and Density-VMA correlations are presented in Table 8.11.

The values in Table 8.11 are not nearly as consistent as those in Tables 8.9 and 8.10. For example, for Intermediate course both the Density-AC and Density-VMA comparisons have 2 positive and 2 negative correlation coefficients and the Density-AV comparison has 1 negative and 3 positive coefficients. Only 1 of the 12 correlation coefficients is different than 0 at the 0.05 significance level, and another 2 are different than 0 at the 0.10 significance level.

The results are more consistent for the Surface course comparisons. For the Density-AC correlation coefficients, 11 of 17 projects showed Negative correlation coefficients, with 7 of the values significantly different than 0 at the 0.05 level of significance. All of the coefficients that were significantly different than 0 were positive. For the Density-AV correlation coefficients, 11 of 17 projects showed negative correlation coefficients, with 2 of the values significantly different than 0 at the 0.05 level of significance and another 2 values significantly different than 0 at the 0.05 level of significance and another 2 values significantly different than 0 at the 0.05 level of significantly different than 0 were negative. For the Density-VMA correlation coefficients, 8 projects showed negative correlation coefficients. None of the values were significantly different than 0 at the 0.05 level of significance. Two of the values were significantly different than 0 at the 0.10 level, but one of these was negative and the other was positive.

| Brainat No. IME No. |           | No. of | Linear Correlation Coefficient |         |         |
|---------------------|-----------|--------|--------------------------------|---------|---------|
| Project No.         | JIVIF NO. | Tests  | AC-AV*                         | AC-VMA* | AV-VMA* |
| P01                 | J07       | 30     | -0.383                         | 0.495   | 0.612   |
| P01                 | J19       | 18     | 0.111                          | 0.603   | 0.857   |
| P02                 | J13       | 18     | -0.409                         | 0.725   | 0.323   |
| P02                 | J15       | 18     | -0.236                         | 0.607   | 0.627   |
| P04                 | J14       | 17     | -0.415                         | 0.433   | 0.623   |
| P05                 | J25       | 23     | 0.128                          | 0.650   | 0.833   |
| P06                 | J24       | 15     | -0.098                         | 0.642   | 0.612   |
| P07                 | J30       | 40     | -0.270                         | 0.430   | 0.751   |
| P10                 | J12       | 19     | -0.304                         | 0.612   | 0.560   |
| P11                 | J41       | 10     | -0.796                         | 0.415   | 0.210   |
| P12                 | J38       | 14     | -0.387                         | 0.210   | 0.819   |
| P13                 | J03       | 16     | -0.715                         | 0.325   | 0.426   |
| P13                 | J43       | 19     | -0.651                         | -0.251  | 0.897   |
| P14                 | J16       | 32     | -0.580                         | 0.141   | 0.723   |
| P18                 | J48       | 12     | -0.463                         | 0.189   | 0.782   |
| P19                 | J49       | 20     | -0.381                         | 0.623   | 0.482   |
| P20                 | J50       | 46     | -0.518                         | 0.360   | 0.609   |
| P21                 | J39       | 15     | -0.549                         | 0.882   | -0.092  |
| P22                 | J54       | 12     | -0.249                         | 0.093   | 0.920   |
| P24                 | J56       | 40     | -0.707                         | -0.061  | 0.618   |
| P24                 | J64       | 13     | 0.217                          | 0.722   | 0.751   |
| P24                 | J67       | 10     | -0.125                         | 0.182   | 0.785   |
| P25                 | J36       | 10     | 0.290                          | 0.727   | 0.867   |
| P26                 | J58       | 13     | -0.411                         | 0.219   | 0.798   |
| P26                 | J62       | 31     | -0.649                         | 0.093   | 0.627   |
| P26                 | J69       | 53     | -0.580                         | 0.237   | 0.653   |
| P27                 | J55       | 15     | -0.657                         | 0.490   | 0.333   |
| P27                 | J71       | 27     | -0.494                         | 0.333   | 0.655   |
| P28                 | J39       | 24     | -0.682                         | 0.621   | 0.103   |
| P29                 | J59       | 16     | -0.324                         | 0.696   | 0.449   |
| P32                 | J72       | 34     | -0.412                         | 0.490   | 0.591   |
| P32                 | J79       | 96     | -0.257                         | 0.433   | 0.579   |
| P33                 | J77       | 22     | -0.782                         | 0.110   | 0.307   |
| P34                 | J62       | 28     | -0.767                         | -0.060  | 0.683   |
| P34                 | J81       | 13     | -0.538                         | 0.394   | 0.558   |
| P35                 | J32       | 14     | -0.384                         | 0.300   | 0.764   |
| P35                 | J38       | 36     | -0.439                         | 0.350   | 0.681   |
| Total / A           | Average   | 889    | -0.402                         | 0.391   | 0.605   |

# Table 8.10. Summary of Correlation Coefficients for Individual Tests for AC, AV, andVMA for Surface Course Projects

\* Values in **Bold** are significantly different from 0 at the 0.05 significance level. Values in *Italics* are significantly different from 0 at the 0.10 significance level.

| Project No  |                     | No of Lots  | Linear C | Correlation Co | efficient |  |  |
|-------------|---------------------|-------------|----------|----------------|-----------|--|--|
| Project No. | JIVIT NO.           | NO. OF LOIS | Den-AC*  | Den-AV*        | Den-VMA*  |  |  |
|             | Intermediate Course |             |          |                |           |  |  |
| P01         | J02                 | 4           | -0.470   | 0.059          | -0.575    |  |  |
| P01         | J10                 | 7           | -0.744   | 0.856          | 0.237     |  |  |
| P32         | J76                 | 12          | 0.067    | -0.352         | -0.123    |  |  |
| P33         | J73                 | 8           | 0.606    | 0.256          | 0.637     |  |  |
| Total / A   | Average             | 31          | -0.135   | 0.205          | 0.044     |  |  |
|             |                     | Surface     | Course   |                |           |  |  |
| P01         | J07                 | 4           | -0.216   | 0.164          | 0.062     |  |  |
| P01         | J07                 | 4           | 0.703    | 0.238          | 0.910     |  |  |
| P04         | J14                 | 5           | 0.903    | -0.523         | -0.100    |  |  |
| P06         | J24                 | 5           | 0.425    | 0.224          | 0.631     |  |  |
| P14         | J16                 | 6           | 0.603    | -0.271         | 0.426     |  |  |
| P16         | J20                 | 3           | 0.935    | -0.993         | -0.738    |  |  |
| P18         | J48                 | 3           | 0.999    | -0.238         | 0.188     |  |  |
| P20         | J50                 | 7           | 0.165    | -0.787         | -0.677    |  |  |
| P24         | J56                 | 7           | -0.649   | 0.168          | -0.204    |  |  |
| P26         | J62                 | 9           | 0.677    | -0.388         | 0.077     |  |  |
| P26         | J69                 | 16          | -0.105   | -0.310         | -0.407    |  |  |
| P27         | J55                 | 4           | 0.552    | -0.812         | -0.871    |  |  |
| P28         | J39                 | 4           | -0.592   | 0.554          | -0.099    |  |  |
| P32         | J72                 | 8           | 0.772    | -0.660         | -0.418    |  |  |
| P32         | J79                 | 24          | 0.437    | -0.101         | 0.221     |  |  |
| P33         | J77                 | 6           | 0.903    | -0.892         | -0.432    |  |  |
| P34         | J62                 | 4           | -0.089   | 0.270          | 0.540     |  |  |
| Total / A   | Verage              | 119         | 0.378    | -0.256         | -0.052    |  |  |

# Table 8.11. Summary of Correlation Coefficients for Lot Test Means for Density Compared with AC, AV, and VMA

\* Values in **Bold** are significantly different from 0 at the 0.05 significance level. Values in *Italics* are significantly different from 0 at the 0.10 significance level.

The results in Tables 8.9 and 8.10 indicate that the plant characteristics are probably not statistically independent of one another. Table 8.11 is less conclusive regarding potential correlations between Density and the plant characteristics of AC, AV, and VMA. It is logical to anticipate that the characteristics of the HMA will be correlated to the field Density since the characteristics of the mix should influence the ability to achieve compaction. However, there are many factors other than the mix that can influence the compaction in the field. Factors such as rolling patterns, climate conditions, waiting time prior to unloading, etc., may lead to the lack of correlation exhibited by the data.

Affect of Correlation on Payment. It has been shown that correlation among the characteristics used in a composite payment equation such as equation 8.10 will not impact the average payment that the contractor will receive in the long run for a given quality of material (3, 5, 18). For example, if the contractor produced the identical population for say 10,000 lots,

the average payment for these lots would be very near the correct payment that would be made for each of the individual lots if the constant population were known with certainty. If an infinite number of lots with the same population were produced, typically the same average payment would be obtained whether or not the payment characteristics were correlated or independent.

However, while the average payment would remain the same, the variability of the individual estimates about this average would tend to increase as the magnitude of the correlation coefficients increases. This is to be expected. There will be times when one of the variables is outside the specifications and has a corresponding price reduction. However, sometimes when this occurs the other variable will be well inside the specification and will have either full payment or a payment incentive (bonus). However, if the two variables are highly correlated, if one variable is outside the specification on the high side it is likely that the other variable will also be on the high side. In which case the two payment factors will both yield price reductions. On the other hand, if one variable is well within the specifications the other one is also likely well within the specifications, and this will lead to both variables indicating a bonus payment. The long–term average payment will be the same whether or not the two variables are correlated, but the correlated variables will have a greater amount of spread among the individual lot payment factors.

The affect of correlation among the payment characteristics will likely have more impact on the contractor than on the STD. This is because the STD will operate under the same specification on many more projects than will an individual contractor that performs a limited number of projects for the STD. The larger potential individual lot payment error associated with the correlated characteristics will have many more opportunities to offset one another on the high and low payment sides for the STD. If a large underpayment error occurs on a project, the contractor will likely not have sufficient additional lots for which overpayments can make up for the large underpayment.

## Summary

The potential variability of the population mean about the target value was considered in addition to the within-lot standard deviation values to develop an overall process standard deviation for each of the acceptance characteristics. These standard deviation values were then compared with the current SCDOT specification limits to investigate whether or not these limits are still appropriate.

The standard deviation that was identified as the typical overall variability for Density is greater than the one used by SCDOT to establish the specification limits. A STD may establish the typical standard deviation value based on data from a number of past projects that it considered "acceptable." Since nearly two-thirds of the projects from which density data were obtained had average project PWL values less than 90 PWL, SCDOT must decide whether or not it wishes to establish the typical project standard deviation based on the data provided for the current research study.

If SCDOT believes that these projects represent the state-of-the-art regarding the process capability of a typical contractor, then SCDOT may need to re-evaluate their target density value and their density specification limits. If SCDOT believes that these projects do not
represent what a typical contractor is capable of providing, then additional data from other representative projects will need to be obtained for analysis.

The values for typical standard deviations that SCDOT might consider to represent the typical overall variability used to evaluate existing specification limits include:

| Asphalt Conte | Base Course:         | 0.26% - 0.30% |
|---------------|----------------------|---------------|
|               | Intermediate Course: | 0.23% - 0.28% |
|               | Surface Course:      | 0.21% - 0.23% |
| Air Voids: 0. | 63% – 0.69%          |               |

**VMA:** 0.64% – 0.71%

In the plant test data there were no obvious inconsistencies among the currently assumed standard deviation values and those calculated based on the project data for the current research. There was therefore no compelling evidence to indicate that a change is specification limits is warranted.

Correlation analyses showed that there were correlations among the plant characteristics of AC, AV, and VMA. AC was negatively correlated with AV and positively correlated with VMA. AV was positively correlated with VMA. The correlation results were less consistent regarding correlations among Density and the plant characteristics, although there was some evidence that Density and AC may be positively correlated in Surface course mixes. These correlations would not impact the average payment that the contractor will receive in the long run for a given quality of material. However, the variability of the individual estimates about this average would tend to increase as the magnitude of the correlation coefficients increases.

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## **CHAPTER 9 — VERIFICATION TESTING**

## Background

Currently, the majority of STDs are using contractor tests for acceptance ( $\underline{8}$ ). During the 1990's many STDs experienced a decline in resources that meant staff cuts. QC and Acceptance Testing were observed to be an easy and practical area to place more responsibility on the contractor and to reduce work load on STD testing personnel. To do this, a methodology for verification testing is needed to ensure the STD is getting the quality it desires.

The SCDOT has adopted the use of contractor tests in the acceptance decision for HMA paving materials. SCDOT developed and implemented verification testing procedures that were in effect for the projects for which data were obtained for the current study. Verification tests were conducted on independent samples obtained by the SCDOT and tested for AC, AV, and VMA. The verification test results were compared with the contractors' acceptance tests to verify the contractor tests before they were used in the acceptance decision.

## **Verification Test Procedures**

An overview of the verification procedures that were used on the projects for which data were provided is presented first. The verification test data are then presented and analyzed in following sections.

In general, SCDOT personnel independently obtained samples that were then tested for AC, AV, and VMA in SCDOT verification laboratories. These verification test results were then compared with the contractor acceptance test results using the *F*-test to compare the variances of the two samples and the two-sample *t*-test to compare the means of the two samples. If neither of these tests declared a significant difference at the 0.05 level, then the contractor acceptance tests were used to determine the payment factors. If one or both of the tests concluded that the two samples were different, then the SCDOT verification tests were used to determine the payment factors.

The procedure called for the comparison of verification and acceptance tests to be conducted on 5-lot data sets. That is, the tests for lots 1-5 were compared and a decision was made whether to use the contractor's or the SCDOT's tests to determine the payment factors for the material in the 5 lots. This procedure was then repeated for lots 6-10, 11-15, etc., for each subsequent set of 5 lots on the project. If the last data set to compare had fewer than 5 lots, then previous lots were added to obtain the 5 lots used in the comparisons.

Note that SCDOT has modified the verification procedures, but the new procedures were not in effect on the projects for which data were obtained. The discussion of the data and their analyses is based on the verification procedures in effect at the time the projects were constructed. Comments concerning the new procedures are presented after the data analysis is presented and discussed.

## Verification Test Data

The acceptance test results and their corresponding verification test results were provided by SCDOT for 10 projects. Most of these projects were different than those that were analyzed above for determining typical process variability values. As such, the verification projects are referred to as V01 to V10. All of the test results along with the *F*-test and *t*-test results are presented in Appendix D.

**Asphalt Content Comparisons.** Table 9.1 presents a summary of the verification comparisons for AC. A total of 53 different data sets were compared, most of which consisted of 5 lots. One set had 7 lots and one had only 2 lots, although its results were disregarded by SCDOT when they decided to use the contractor's tests. In the table, the lots with the X + Y format indicate cases where the final comparison set had fewer than 5 lots (the number before the + sign) to which a number of lots (the number after the + sign) that had been used in previous comparisons were added to make a total of 5 lots.

The number of contractor tests in the comparisons varied from as few as 3 to as many as 28. The X + Y format is again used to indicate the number of new tests and previously used tests in the comparison. The number of SCDOT tests in the comparisons varied from 3 to 13.

Of the 53 AC comparisons, 13 times the contractor tests were rejected in favor of using the SCDOT verification tests to determine the payment factor. Six of these occurred on the same project, V05, and 3 of those were on the 3 Intermediate B lots. The *F*-test failed 6 times in the 53 comparisons, while the *t*-test failed 8 times.

Air Voids Comparisons. Table 9.2 presents a summary of the verification comparisons for AV. A total of 29 different data sets were compared, most of which consisted of 5 lots. One set had 7 lots and one had only 4 lots. The same X + Y format described for Table 9.1 indicates cases where the final comparison set had fewer than 5 lots to which a number of lots that had been used in previous comparisons were added to make a total of 5 lots.

The number of contractor tests in the comparisons varied from as few as 3 to as many as 28. The X + Y format is again used to indicate the number of new tests and previously used tests in the comparison. The number of SCDOT tests in the comparisons varied from 3 to 13.

Of the 29 AV comparisons, 14 times the contractor tests were rejected in favor of using the SCDOT verification tests to determine the payment factor. Seven of these occurred on the same project, V05, and 3 of those were on the 3 Intermediate B lots. The *F*-test and *t*-test each failed 7 times in the 29 comparisons. A rejection rate of nearly 50% (14/29) seems extremely high. Some potential reasons for the high failure rate are discussed in following sections.

| Draiget | Mix Tuno | No. of | No. of Tests |        | Res    | Use Contr.     |       |
|---------|----------|--------|--------------|--------|--------|----------------|-------|
| Project | wix type | Lots   | Contractor   | SCDOT  | F-test | <i>t</i> -test | Test? |
| V01     | Interm B | 4      | 19           | 7      | Pass   | Pass           | Yes   |
| VUI     | Surf A   | 5      | 7            | 6      | Fail   | Pass           | No    |
|         | Interm B | 5      | 7            | 5      | Pass   | Pass           | Yes   |
|         |          | 5      | 19           | 9      | Pass   | Pass           | Yes   |
|         |          | 5      | 18           | 7      | Fail   | Pass           | No    |
|         | Surf A   | 5      | 23           | 7      | Pass   | Pass           | Yes   |
| 1/02    |          | 5      | 20           | 9      | Pass   | Pass           | Yes   |
| V02     |          | 2 + 3* | 6 + 12*      | 1 + 5* | Pass   | Pass           | Yes   |
|         |          | 5      | 18           | 11     | Pass   | Pass           | Yes   |
|         | Surf D   | 5      | 18           | 7      | Pass   | Pass           | Yes   |
|         | Suirb    | 5      | 19           | 7      | Fail   | Pass           | No    |
|         |          | 5      | 13           | 6      | Pass   | Pass           | Yes   |
|         |          | 5      | 10           | 5      | Pass   | Pass           | Yes   |
|         |          | 5      | 7            | 5      | Pass   | Pass           | Yes   |
| V03     | Surf E   | 2      | 6            | 3      | Fail   | Pass           | Yes   |
| ¥03     | Suit     | 5      | 14           | 8      | Pass   | Pass           | Yes   |
|         |          | 5      | 18           | 8      | Pass   | Pass           | Yes   |
|         |          | 5      | 14           | 5      | Fail   | Pass           | No    |
| V04     | Surf B   | 6      | 25           | 11     | Fail   | Pass           | No    |
|         |          | 5      | 20           | 6      | Pass   | Fail           | No    |
|         | Interm B | 5      | 14           | 6      | Pass   | Fail           | No    |
|         |          | 4 + 1* | 11 + 4*      | 5 + 1* | Pass   | Fail           | No    |
|         |          | 5      | 20           | 5      | Pass   | Pass           | Yes   |
|         |          | 5      | 17           | 8      | Pass   | Pass           | Yes   |
|         | Surf A   | 5      | 22           | 10     | Pass   | Pass           | Yes   |
|         |          | 5      | 23           | 9      | Pass   | Fail           | No    |
|         |          | 5      | 15           | 5      | Pass   | Pass           | Yes   |
| V05     | Surf B   | 5      | 22           | 7      | Pass   | Pass           | Yes   |
| ¥03     |          | 3 + 2* | 12 + 8*      | 5 + 2* | Pass   | Fail           | No    |
|         |          | 4      | 4            | 5      | Pass   | Pass           | Yes   |
|         |          | 5      | 10           | 9      | Pass   | Pass           | Vos   |
|         |          | 3      | 10           | 0      | F ass  | Pass           | Vee   |
|         | Ourf E   | 3      | 5            | 4      | Pass   |                | res   |
|         | SurrE    | 5      | 5            | 6      | Pass   | Fall           | NO    |
|         |          | 5      | 5            | 6      | Pass   | Pass           | Yes   |
|         |          | 4      | 6            | 6      | Pass   | Pass           | Yes   |
| L       |          | 3      | 5            | 6      | Pass   | Pass           | Yes   |
| V06     | Interm C | 5      | 6            | 4      | Pass   | Pass           | Yes   |
|         |          | 5      | 15           | 5      | Pass   | Pass           | Yes   |
|         |          | 5      | 14           | 8      | Pass   | Pass           | Yes   |
|         |          | 5      | 7            | 4      | Pass   | Pass           | Yes   |
|         |          | 5      | 6            | 7      | Pass   | Pass           | Yes   |
| V07     | Base A   | 5      | 5            | 6      | Pass   | Pass           | Yes   |
|         |          | 5      | 5            | 5      | Pass   | Pass           | Yes   |
|         |          | 5      | 5            | 1      | Dass   | Dass           | Voc   |
|         |          | 5      | 5            |        | F doo  | F doo          | Vec   |
| 1/00    | Ourf E   | 5      | <u>э</u>     | 5      | rdss   | rdss           | res   |
| 807     | SurrE    | 5      | 5            | 8      | Pass   | Pass           | Y es  |
| V09     | Surf A   | 7      | 28           | 13     | Pass   | Pass           | Yes   |
|         | Surf E   | 5      | 9            | 7      | Pass   | Pass           | Yes   |
|         | Interm R | 5      | 16           | 7      | Pass   | Pass           | Yes   |
|         |          | 3 + 2* | 8 + 9*       | 5 + 2* | Pass   | Fail           | No    |
| 140     | Curf A   | 5      | 19           | 9      | Pass   | Pass           | Yes   |
| V10     | Suff A   | 2 + 3* | 4 + 11*      | 5 + 4* | Pass   | Fail           | No    |
|         |          | 5      | 5            | 6      | Pass   | Pass           | Yes   |
|         | Surf E   | 5      | 5            | 5      | Pass   | Pass           | Yes   |
|         |          | 5      | , J          |        | 1 400  | 1 400          |       |

Table 9.1. Summary of the Verification Comparisons for AC

the second number refers to lots/tests from the previous data set that were repeated in the current data set so as to have 5 lots for the verification comparisons

| Draiget | Mix Turne | No. of | No. of     | Tests  | Res            | sult   | Use Contr. |
|---------|-----------|--------|------------|--------|----------------|--------|------------|
| Project | witx Type | Lots   | Contractor | SCDOT  | <i>F</i> -test | t-test | Test?      |
| V01     | Interm B  | 4      | 19         | 7      | Pass           | Pass   | Yes        |
| VUI     | Surf A    | 5      | 7          | 6      | Pass           | Pass   | Yes        |
|         | Interm B  | 5      | 7          | 5      | Pass           | Pass   | Yes        |
|         |           | 5      | 19         | 9      | Fail           | Pass   | No         |
|         |           | 5      | 18         | 7      | Fail           | Pass   | No         |
|         | Surf A    | 5      | 23         | 7      | Fail           | Pass   | No         |
| V02     |           | 5      | 20         | 9      | Pass           | Pass   | Yes        |
| V02     |           | 2 + 3* | 6 + 12*    | 1 + 5* | Pass           | Pass   | Yes        |
|         |           | 5      | 18         | 11     | Pass           | Pass   | Yes        |
|         | Surf D    | 5      | 18         | 7      | Fail           | Pass   | No         |
|         | Sund      | 5      | 19         | 7      | Pass           | Fail   | No         |
|         |           | 5      | 13         | 6      | Pass           | Fail   | No         |
| V04     | Surf B    | 6      | 25         | 11     | Fail           | Pass   | No         |
|         |           | 5      | 20         | 6      | Fail           | Pass   | No         |
|         | Interm B  | 5      | 14         | 6      | Pass           | Fail   | No         |
|         |           | 4 + 1* | 11 + 4*    | 5 + 1* | Pass           | Pass   | Yes        |
|         |           | 5      | 20         | 5      | Pass           | Fail   | No         |
| VOE     |           | 5      | 17         | 8      | Pass           | Fail   | No         |
| V05     | Surf A    | 5      | 22         | 10     | Pass           | Fail   | No         |
|         |           | 5      | 23         | 9      | Pass           | Pass   | Yes        |
|         |           | 5      | 15         | 5      | Pass           | Pass   | Yes        |
|         | Currit D  | 5      | 22         | 7      | Pass           | Fail   | No         |
|         | Sun B     | 3 + 2* | 12 + 8*    | 5 + 2* | Fail           | Pass   | No         |
| V06     | Interm C  | 5      | 6          | 4      | Pass           | Pass   | Yes        |
| V09     | Surf A    | 7      | 28         | 13     | Pass           | Pass   | Yes        |
|         | later D   | 5      | 16         | 7      | Pass           | Pass   | Yes        |
| 140     | Interm B  | 3 + 2* | 8 + 9*     | 5 + 2* | Pass           | Pass   | Yes        |
| V10     | 0 ( )     | 5      | 19         | 9      | Pass           | Pass   | Yes        |
|         | Surr A    | 2 + 3* | 4 + 11*    | 9      | Pass           | Pass   | Yes        |

#### Table 9.2. Summary of the Verification Comparisons for AV

\* the second number refers to lots/tests from the previous data set that were repeated in the current data set so as to have 5 lots for the verification comparisons

**VMA Comparisons.** Table 9.3 presents a summary of the verification comparisons for AV. A total of 29 different data sets were compared, most of which consisted of 5 lots. One set had 7 lots and one had only 4 lots. The same X + Y format described for Table 9.1 indicates cases where the final comparison set had fewer than 5 lots to which a number of lots that had been used in previous comparisons were added to make a total of 5 lots.

The number of contractor tests in the comparisons varied from as few as 3 to as many as 28. The X + Y format is again used to indicate the number of new tests and previously used tests in the comparison. The number of SCDOT tests in the comparisons varied from 3 to 13.

Of the 29 AV comparisons, 16 times the contractor tests were rejected in favor of using the SCDOT verification tests to determine the payment factor. The *F*-test failed 4 times in the 29 comparisons, while the *t*-test failed 12 times. A rejection rate over 50% (16/29) seems extremely high. The verification procedures apparently did not work as planned on project V05 since all 10 of the VMA comparisons on the project failed. Unless the contractor was not concerned and ignored the differences, it would normally be expected that an investigation would find the source of the problem before 10 data sets failed to compare.

| Project | Mix Tupo   | No. of | No. of Tests |        | Re     | sult           | Use Contr. |
|---------|------------|--------|--------------|--------|--------|----------------|------------|
| Frojeci | wix type   | Lots   | Contractor   | SCDOT  | F-test | <i>t</i> -test | Test?      |
| V01     | Interm B   | 4      | 19           | 7      | Pass   | Pass           | Yes        |
| VUI     | V01 Surf A | 5      | 7            | 6      | Pass   | Pass           | Yes        |
|         | Interm B   | 5      | 7            | 5      | Pass   | Pass           | Yes        |
|         |            | 5      | 19           | 9      | Fail   | Pass           | No         |
|         |            | 5      | 18           | 7      | Pass   | Pass           | Yes        |
|         | Surf A     | 5      | 23           | 7      | Fail   | Pass           | No         |
| V02     |            | 5      | 20           | 9      | Pass   | Pass           | Yes        |
| V02     |            | 2 + 3* | 6 + 12*      | 1 + 5* | Pass   | Fail           | No         |
|         |            | 5      | 18           | 11     | Pass   | Pass           | Yes        |
|         | Surf B     | 5      | 18           | 7      | Fail   | Pass           | No         |
|         | Sun B      | 5      | 19           | 7      | Pass   | Pass           | Yes        |
|         |            | 5      | 13           | 6      | Pass   | Fail           | No         |
| V04     | Surf B     | 6      | 25           | 11     | Fail   | Pass           | No         |
|         |            | 5      | 20           | 6      | Pass   | Fail           | No         |
|         | Interm B   | 5      | 14           | 6      | Pass   | Fail           | No         |
|         |            | 4 + 1* | 11 + 4*      | 5 + 1* | Pass   | Fail           | No         |
|         |            | 5      | 20           | 5      | Pass   | Fail           | No         |
| VOE     |            | 5      | 17           | 8      | Pass   | Fail           | No         |
| V05     | Surf A     | 5      | 22           | 10     | Pass   | Fail           | No         |
|         |            | 5      | 23           | 9      | Pass   | Fail           | No         |
|         |            | 5      | 15           | 5      | Pass   | Fail           | No         |
|         | Curf D     | 5      | 22           | 7      | Pass   | Fail           | No         |
|         | Sun B      | 3 + 2* | 12 + 8*      | 5 + 2* | Pass   | Fail           | No         |
| V06     | Interm C   | 5      | 6            | 4      | Pass   | Pass           | Yes        |
| V09     | Surf A     | 7      | 28           | 13     | Pass   | Pass           | Yes        |
|         | laters D   | 5      | 16           | 7      | Pass   | Pass           | Yes        |
|         | Interm B   | 3 + 2* | 8 + 9*       | 5 + 2* | Pass   | Pass           | Yes        |
| V10     | Sturf A    | 5      | 19           | 9      | Pass   | Pass           | Yes        |
|         | Sull A     | 2 + 3* | 4 + 11*      | 9      | Pass   | Pass           | Yes        |

Table 9.3. Summary of the Verification Comparisons for VMA

\* the second number refers to lots/tests from the previous data set that were repeated in the current data set so as to have 5 lots for the verification comparisons

## **Issues with Verification Procedures**

A number of potential issues were identified while reviewing the verification procedures and analyzing the verification test result data. Each of these issues is discussed in the following sections.

**Variability and Specification Limits.** As discussed in Chapter 5, one of the most important issues for a STD is to develop a value for typical variability that is consistent with the way in which a lot is defined under the acceptance plan. Since the SCDOT specification is based on lot-by-lot acceptance, the variability used to establish the specification limits must be that which is appropriate for a typical lot. To determine this, the unbiased individual standard deviation values for each lot were calculated and then these lot standard deviations were averaged to get a typical "within-lot" standard deviation for the process.

The decision regarding the standard deviation value to use to establish the specification limits must be made subjectively by the SCDOT. Although, some ranges for possible values are presented in Chapters 6-8. Once this value is selected, the specification limits can be

established accordingly as discussed in Chapter 8. The verification procedure used by SCDOT includes comparing the acceptance and verification tests from 5 lots. If the values compare, then there is no issue since the contractor acceptance tests for each lot are then used to determine an individual payment factor for each lot. This is the way that the specification was intended to operate, and the specification limits have been established for this lot-by-lot acceptance approach.

An issue arises, however, if the acceptance and verification tests do not compare. In this instance, the SCDOT uses the verification test results to establish a single payment factor for the combined 5 lots. This is not the way in which the specification originally was intended to operate, and this approach is not necessarily consistent with the specification limits that were developed for lot-by-lot acceptance. That is, the within-lot variability, which does not include potential lot-to-lot variability of the process, may not be the same as the variability associated with 5-lot increments.

This means that the specification limits that SCDOT selected for lot-by-lot acceptance may be too narrow to use when basing the acceptance decision on tests obtained from 5 different lots. This fact is illustrated in Chapters 6 and 7 when both the Lot standard deviations and Project standard deviations were calculated. Table 9.4 summarizes the Lot and Project standard deviation results for AC, AV, and VMA. For each mean standard deviation the Project value is greater than the Lot value, and the same is the case for most of the percentile results as well.

To further investigate this situation, two projects with the largest numbers of lots and tests were explored in more detail. For these two projects, the individual Lot standard deviations were calculated as well as the standard deviations for the 5-Lot increments on each project. The averages for each of these types of standard deviations were then calculated. The example calculations for AC for one of the projects are shown in Table 9.5. A summary of the results for AC, AV, and VMA for both projects is presented in Table 9.6. As shown in the table, the average 5-lot standard deviations are all larger than their corresponding Lot standard deviations.

Since the selection of the standard deviation to use when developing specification limits is subjective, SCDOT will need to decide whether or not the use of different specification limits for lot-by-lot acceptance and for 5-Lot increment acceptance is warranted. The Project, Lot, and 5-Lot standard deviation values calculated in this report would seem to support the use of different specification limits.

|  | Characteristic | Course         | Avg/Percentile | Project *<br>Std Dev | Lot *<br>Std Dev |
|--|----------------|----------------|----------------|----------------------|------------------|
|  |                |                | Mean           | 0.2422               | 0.2357           |
|  |                |                | 50%            | 0.2421               | 0.2237           |
|  |                | Base           | 60%            | 0.2451               | 0.2457           |
|  |                | Dase           | 70%            | 0.2505               | 0.2940           |
|  |                |                | 80%            | 0.2656               | 0.3279           |
|  |                |                | 90%            | 0.3057               | 0.3369           |
|  |                |                | Mean           | 0.2190               | 0.2057           |
|  |                |                | 50%            | 0.2079               | 0.1864           |
|  | 10             | Intermediate   | 60%            | 0.2226               | 0.2072           |
|  | AC             | Internediate   | 70%            | 0.2380               | 0.2131           |
|  |                |                | 80%            | 0.2521               | 0.2480           |
|  |                |                | 90%            | 0.2729               | 0.2936           |
|  |                |                | Mean           | 0.1962               | 0.1708           |
|  |                | Surface        | 50%            | 0.1800               | 0.1648           |
|  |                |                | 60%            | 0.1929               | 0.1746           |
|  |                |                | 70%            | 0.2048               | 0.1900           |
|  |                |                | 80%            | 0.2181               | 0.2105           |
|  |                |                | 90%            | 0.2740               | 0.2529           |
|  |                |                | Mean           | 0.5363               | 0.4182           |
|  |                |                | 50%            | 0.5307               | 0.43070          |
|  | ۸\/            | Intermediate & | 60%            | 0.5677               | 0.45346          |
|  | AV             | Surface        | 70%            | 0.5957               | 0.50315          |
|  |                |                | 80%            | 0.6414               | 0.56246          |
|  |                |                | 90%            | 0.7389               | 0.59914          |
|  |                |                | Mean           | 0.4980               | 0.4432           |
|  |                |                | 50%            | 0.4910               | 0.4117           |
|  |                | Intermediate & | 60%            | 0.5214               | 0.4608           |
|  | VIVIA          | Surface        | 70%            | 0.5793               | 0.5120           |
|  |                |                | 80%            | 0.6190               | 0.5813           |
|  |                |                | 90%            | 0.6578               | 0.6481           |

# Table 9.4. Summary of the Lot and Project Standard Deviation Results for AC, AV, & VMA

\* **Project:** the unbiased standard deviation estimate of all individual test results on the project **Lot:** the average of the unbiased standard deviation estimates for all lots on the project

| Lot No. | No. of<br>Tests | Unbiased<br>Lot SD | 5-Lot<br>Increment | No. of Lots | Total No.<br>of Tests | Unbiased<br>5-Lot SD |
|---------|-----------------|--------------------|--------------------|-------------|-----------------------|----------------------|
| 2       | 6               | 0.0760             |                    |             |                       |                      |
| 3       | 5               | 0.0700             |                    |             |                       |                      |
| 4       | 4               | 0.1391             | 1                  | 5           | 22                    | 0.1442               |
| 5       | 3               | 0.1441             |                    |             |                       |                      |
| 6       | 4               | 0.1863             |                    |             |                       |                      |
| 7       | 3               | 0.0832             |                    |             |                       |                      |
| 8       | 3               | 0.0705             |                    |             |                       |                      |
| 9       | 3               | 0.0642             | 2                  | 5           | 18                    | 0.1200               |
| 10      | 4               | 0.1133             |                    |             |                       |                      |
| 11      | 5               | 0.2044             |                    |             |                       |                      |
| 12      | 4               | 0.1659             |                    |             |                       |                      |
| 13      | 5               | 0.1736             |                    | 5           | 22                    | 0.1905               |
| 14      | 3               | 0.1194             | 3                  |             |                       |                      |
| 15      | 5               | 0.0994             |                    |             |                       |                      |
| 16      | 5               | 0.1291             |                    |             |                       |                      |
| 17      | 5               | 0.2230             |                    |             |                       |                      |
| 18      | 5               | 0.1035             |                    |             |                       |                      |
| 19      | 3               | 0.0862             | 4                  | 5           | 21                    | 0.1820               |
| 20      | 5               | 0.2228             |                    |             |                       |                      |
| 21      | 3               | 0.0881             |                    |             |                       |                      |
| 22      | 3               | 0.1387             |                    |             |                       |                      |
| 23      | 4               | 0.1035             | 5                  | 1           | 12                    | 0.0071               |
| 24      | 3               | 0.0427             | 5                  | 4           | 13                    | 0.0971               |
| 25      | 3               | 0.1601             |                    |             |                       |                      |
| Ave     | rage            | 0.1253             |                    |             |                       | 0.1468               |

Table 9.5. Calculation of the Average Lot and 5-Lot Standard Deviations for AC forProject P32, JMF J79.

| Proj/JMF | Total No.<br>of Tests | No. of<br>Lots | No. of<br>Increments | Characteristic | Unbiased<br>Lot SD | Unbiased<br>5-Lot SD |
|----------|-----------------------|----------------|----------------------|----------------|--------------------|----------------------|
|          |                       |                |                      | AC             | 0.1253             | 0.1468               |
| P32/J79  | 96                    | 24             | 5                    | AV             | 0.4356             | 0.4822               |
|          |                       |                |                      | VMA            | 0.4482             | 0.5107               |
|          |                       |                |                      | AC             | 0.1531             | 0.1785               |
| P26/J69  | 53                    | 16*            | 3**                  | AV             | 0.4460             | 0.4714               |
|          |                       |                |                      | VMA            | 0.2928             | 0.4493               |

Table 9.6. Summary of the Lot and 5-Lot Standard Deviation Results

\* 2 of 18 lots had sample sizes of 1 and hence no standard deviation could be calculated

\*\* 3 increment of 5-lots were used; the final 3-lot increment was not used in calculations

**Sample Size, Lot Size, and Payment Risks.** The quality index approach to estimating PWL provides an unbiased estimate for the population PWL. As a result, as long as there is a sufficient bonus provision, the expected payment that a contractor would receive in the long run for a given quality of material will be equal to the payment that the contractor would receive if the population were known with certainty. However, while the average payment in the long run will be correct, due to sampling variability there is a high degree of variability in the individual lot payment factors that will be calculated for the given population. That is, sometimes a sample will give results that over-estimate the quality and thus the payment, while other times the sample will under-estimate the payment for a given population. However, over a large number of lots, the high and low estimates for lot PWL will tend to balance out to give the correct average payment factor.

If there are only a small number of lots on a project, then it will be possible that a significantly low estimated PWL value could negatively impact the payment that the contractor should have received. Similarly, larger PWL estimates could be obtained that would provide a larger payment than is deserved. Given the payment equation used by SCDOT, i.e., PF = 55 + 0.5(PWL), the under-payment error for an individual lot has the potential to be much greater than the over-payment error, which is limited to the maximum bonus of 5%.

Also, the variability associated with the estimate of the lot PWL can be reduced by increasing the sample size obtained from each lot. Therefore, the risks to both parties of the total project payment being in error can be reduced by having a larger number of smaller lots and/or by having a larger sample size for each lot. In the event that the SCDOT verification tests are used to determine the payment factor, the sample size may increase but the number of lots on the project is considerably reduced. Not only is the number of lots reduced, but the amount of material at risk is also greatly increased for each payment factor determination.

When the verification tests are used for payment determination instead of the larger number of acceptance tests, the risks to both SCDOT and the contractor will increase due to the greater amount of material that is being evaluated with typically much fewer tests. Rather than having each lot evaluated on the basis of 3-5 tests, 5 lots may be evaluated on the basis of 7-9 tests. In this scenario, based on the preceding discussions the contractor would seem to be exposed to a greater payment risk than would the SCDOT.

**Cause of the Difference.** *F*-tests and *t*-tests can determine when there may be a difference between the contractor acceptance tests and the STD verification tests. On the other hand, the fact that the test does not conclude that there is a difference does not prove that the two sets of test results are the same. A major drawback of the *F*-test and *t*-test procedures is that they can determine only whether or not a difference between the two data sets is likely. They do not, however, provide any information regarding the reason for the difference between the acceptance and verification tests.

These tests also do not indicate which of the data sets is "correct" and which is "wrong." Indeed, regardless of the result of the hypothesis test, either of the data sets could be "wrong," they both could be "wrong," or they both could be "correct." The lower the P-value the more confident we are that the two data sets actually are different, but they both could still be "wrong." However, most STDs will assume that their data are "correct" in the event that the *F*-test or *t*-test finds a difference between the acceptance and verification tests. In reality, an investigation should be conducted in an effort to determine "why" the two sets of tests were found to be different.

Any differences between the two sets of tests may be due to a number of different factors. The one that a STD is likely to first think of is that the contractor has "manipulated" the results to ensure that full payment is obtained. While there is always some chance that this is the case, other possibilities may be more likely. For example, differences in sampling or testing procedures could account for differences. In this event, the material sampled by both parties could be identical but differences still might be identified when comparing the results.

The smaller sample, which is usually the verification tests, could be influenced by one bad truck load from which one of the limited number of verification samples was taken. With a smaller sample size one errant value would have a bigger impact on the sample mean and standard deviation. It could be that only one "bad" lot caused the statistical tests to not compare. In such an instance the contractor could be penalized on all 5 lots for errors that occurred on only 1 of the lots in the comparison data.

One potential concern and a likely candidate for the cause of differences between contractor acceptance and STD verification test results is the difference in test procedures that is an inherent part of the process. For example, the acceptance samples taken by the contractor may very well be split, prepared, and tested within a very short time after being taken from the truck at the plant. In such cases the sample would likely not need to be re-heated. On the other hand, the STD verification sample must be transported to another lab and likely will require reheating. Additionally, the verification tests may be conducted anywhere from a few hours to several days after the sample was taken from the truck.

As a result, any differences between the acceptance and verification tests may well be due to differences in testing procedures rather than differences in the material. It may be that, due to the differences in procedures, the two sets of tests should not be expected to compare on a routine basis. The verification procedures used by SCDOT, and indeed by most if not all STDs, are based on the assumption that sampling, storage, and testing procedures do not contribute to any differences detected when comparing the different test results.

<u>Recommendation</u>. It is strongly recommended, therefore, that SCDOT implement a research study to examine whether or not re-heating, lack of re-heating, delays before testing, and lack of delay have any effect on the resulting test results. Without such a study it is difficult to state with confidence that differences between the acceptance tests and verification tests are due to differences in the material that was sampled and tested by the two parties.

**Procedural Issues.** The issues discussed above are major issues that could possibly cast doubt on the validity of the verification results. There are some other minor issues dealing with some of the procedures identified in the verification test results provided by SCDOT. The following discussions relate to the procedures that were being used on the projects for which verification test results were provided by SCDOT.

<u>Re-Use of Lot Test Results</u>. The SCDOT verification procedures contained the following statement: "If the last data set is less than 5 LOTS, then go back to the previous LOTS far enough to yield the 5 LOTS needed in the data set." This process was generally, but not always, used on the projects that were provided. For example, Table 9.1 shows 5 instances where this procedure was followed on the final verification data set to yield the necessary 5 lots for the verification comparisons. But the table also shows that on 2 other projects 6 lots and 7 lots were combined into a single verification data set for the project.

To illustrate the process, Table 9.7 shows the final two verification data sets for a project on which 3 lots were used in both of the data sets. This may raise a question concerning "double jeopardy." For example, what if both of the data sets did not compare, but this result was due to 1 or 2 of the lots that appeared in both of the comparisons? The question that arises then is could 1 bad lot be the cause of 6, 7, or 8 lots not comparing, with the result being that a limited number of verification tests replaced many valid contractor acceptance tests?

Note that in Table 9.7 the first 5-Lot data set passed both the *F*-test and *t*-test. The second 5-Lot data set, which included lots 3, 4, and 5 from the first 5-Lot data set, did not pass the *t*-test and as a result the contractor tests were not used. Only 4 new contractor acceptance tests and 5 SCDOT verification tests were included in the comparison, which included 11 contractor and 4 SCDOT tests that had already been "verified." If the 7 lots had been combined into a single verification data set, both the *F*-test and *t*-test would have passed for the 7 lots.

With any verification process there is no "right" answer since any assumption that is made has potential advantages and disadvantages. However, SCDOT may wish to consider a policy that would allow for the final verification data set to be comprised of up to 6 or 7 lots. Then another decision would need to be made regarding how to deal with the situation when there are 3 or 4 lots in the final data set. It would seem reasonable to consider 4 lots as sufficient for the final verification data set. The decision with 3 lots might be to use the 3 lots as the final data set, or possibly to take the last 8 lots and split them into two 4-lot data sets for verification purposes. This latter approach would be consistent with adopting 4 as the minimum lot size on which a verification decision can be made.

| 5-Lot<br>Data Set | Lot No. | Contractor | SCDOT | <i>F</i> -test | <i>t</i> -test | Use Contr.<br>Tests? |
|-------------------|---------|------------|-------|----------------|----------------|----------------------|
|                   |         | 4.60       | 4.72  |                |                |                      |
|                   | 1       | 4.22       | 4.90  |                |                |                      |
|                   | 1       | 4.73       | 4.70  |                |                |                      |
|                   |         | 4.37       |       |                |                |                      |
|                   |         | 4.60       |       |                |                |                      |
|                   | 2       | 4.99       | 4.56  |                |                |                      |
|                   | 2       | 4.72       | 4.77  |                |                |                      |
|                   |         | 4.61       |       |                |                |                      |
|                   |         | 4.84       |       |                |                |                      |
| 1                 | 2       | 5.05       |       | Pass           | Pass           | Yes                  |
|                   | 3       | 4.89       | 5.12  |                |                |                      |
|                   |         | 4.92       | 5.11  |                |                |                      |
|                   |         | 4.59       |       |                |                |                      |
|                   | 4       | 4.80       |       |                |                |                      |
|                   | 4       | 4.36       | 5.09  |                |                |                      |
|                   |         | 4.76       |       |                |                |                      |
|                   |         | 4.32       | 4.80  |                |                |                      |
|                   | 5       | 4.71       |       |                |                |                      |
|                   |         | 4.69       |       |                |                |                      |
|                   |         | 4.51       | 4.92  |                |                |                      |
|                   | 6       | 4.90       | 5.41  |                |                |                      |
|                   |         | 5.16       | 5.55  |                |                |                      |
|                   | 7       | 4.96       | 4.95  |                |                |                      |
|                   | 7       |            | 4.85  |                |                |                      |
|                   |         | 4.84       |       |                |                |                      |
|                   | 2       | 5.05       |       |                |                |                      |
| 2                 | 5       | 4.89       | 5.12  | Bass           | Foil           | No                   |
| 2                 |         | 4.92       | 5.11  | F 455          | Fall           | INO                  |
|                   |         | 4.59       |       |                |                |                      |
|                   | 1       | 4.80       |       |                |                |                      |
|                   | 4       | 4.36       | 5.09  |                |                |                      |
|                   |         | 4.76       |       |                |                |                      |
|                   |         | 4.32       | 4.80  |                |                |                      |
|                   | 5       | 4.71       |       |                |                |                      |
|                   |         | 4.69       |       | 1              |                |                      |

Table 9.7. Composition of Verification Lots for AC on Project V10, Surface A

<u>Test Distribution</u>. The uneven distribution of verification tests among the lots raised some potential issues. To illustrate some of these potential issues, Table 9.8 shows some examples of the distribution of verification tests within a number of selected verification data sets. While, if there is a constant process, there is nothing inherently wrong with not distributing the verification tests equally among the lots. However, the fact that lot-by-lot acceptance is being used indicates that some variability may be anticipated between lots. Some of the lots, which were selected solely for illustration, in Table 9.8 might raise some questions. For example, in the first data set <sup>2</sup>/<sub>3</sub> of the tests are from 2 of 5 lots. In many instances 2 of 5 lots had no sample taken from them. For project V07, 60% of the tests are from the last lot.

| Project | Number of Verification |       |       |       | Tests |       |
|---------|------------------------|-------|-------|-------|-------|-------|
| FIUJECI | Lot 1                  | Lot 2 | Lot 3 | Lot 4 | Lot 5 | Total |
|         | 4                      | 2     | 1     | 1     | 1     | 9     |
| V02     | 1                      | 0     | 2     | 2     | 1     | 6     |
|         | 2                      | 0     | 1     | 0     | 3     | 6     |
| 1/02    | 1                      | 0     | 2     | 2     | 0     | 5     |
| V03     | 1                      | 2     | 0     | 0     | 2     | 5     |
| V05     | 3                      | 0     | 2     | 0     | 2     | 7     |
| V07     | 1                      | 1     | 0     | 0     | 3     | 5     |
| V10     | 0                      | 3     | 2     | 2     | 0     | 7     |

| Table 9.8. Selected Examples of Distribution of Verification Test within 5-Lot Data Sets |
|--|
|--|

<u>Outliers</u>. A review of the verification test results shows that there were occasions where a single test result might have been responsible for the two data sets not comparing. An example of such an occurrence is shown in Table 9.9. The analyses in the table are for AV on project V02. The point in question is the first verification test. The value of 6.72 is 70% greater than the next largest verification test result. The other 3 verification tests taken on that lot were very close to the contractor's acceptance test results. If the 6.72 value is disregarded the *F*-test on the remaining data has a P-value of 0.18, and there would be no reason to believe that the variances were different between the two data sets.

SCDOT may wish to consider whether to implement an outlier procedure such as those presented in ASTM E-178-08, *Standard Practice for Dealing With Outlying Observations*. The procedure that would apply in this case is to calculate the test statistic,  $T_n$ , from equation 9.1 and then to compare it to the critical values in Table 1 of E-178.

$$T_n = \frac{(x_n - \overline{x})}{s}$$
(9.1)

In the example in Table 9.9, the sample mean,  $\overline{x}$ , is 3.324 and the sample standard deviation, *s*, is 1.4155. So,  $T_n = (6.72 - 3.324) / 1.4155 = 2.399$ . The critical value (from Table 1 in ASTM E-178) for the 0.01 significance level is 2.323. So, the value of 6.72 would be considered an outlier and eliminated from the data set.

While such a procedure would add complexity to the acceptance plan, it hopefully would rarely need to be employed.

|                | Contractor   | SCDOT  |
|----------------|--------------|--------|
| LOT NO.        | Tests        | Tests  |
|                | 4.06         | 6.72   |
| 4              | 2.46         | 3.93   |
| I              | 2.60         | 2.14   |
|                |              | 2.57   |
|                | 3.07         | 3.03   |
| 2              | 2.35         | 2.32   |
| 2              | 2.37         |        |
|                | 2.21         |        |
|                | 2.52         | 2.41   |
| 3              | 2.28         |        |
|                | 2.60         |        |
|                | 2.10         | 3.07   |
| 4              | 2.12         |        |
|                | 2.54         |        |
|                | 3.12         |        |
|                | 3.34         |        |
| Б              | 3.37         |        |
| 5              | 2.77         |        |
|                | 2.29         | 3.73   |
|                | 2.94         |        |
| E tost B Value | With 6.72    | 0.0002 |
| r-iesi r-value | Without 6.72 | 0.1815 |

Table 9.9. Illustration of a Possible Outlier Affecting the *F*-test for AV on Project V02

## Split Sample Comparisons

The SCDOT HMA quality assurance program includes a "Split Test Sample Program." The differences between the contractor's results and SCDOT results on the split samples are compared with the allowable differences shown in Table 9.10.

## Table 9.10. Allowable Differences between Contractor Tests and SCDOT Split Sample Tests

| Test Parame                 | Allowable Difference |         |
|-----------------------------|----------------------|---------|
| Asphalt Binder Content,     | %                    | ± 0.40  |
| Maximum Specific Gravit     | у                    | ± 0.035 |
| Bulk Specific Gravity of C  | Cores                | ± 0.035 |
| · · · · ·                   | 1/2" and greater     | ± 7.0   |
| Cradation                   | 3/8"                 | ± 6.0   |
| (Rase Shoulder Widening     | No. 4                | ± 6.0   |
| Surface Type E & OGFC only) | No. 8                | ± 5.0   |
|                             | No. 30               | ± 4.0   |
|                             | No. 100              | ± 3.0   |

There are two methods for establishing or evaluating allowable tolerances such as those in Table 9.10. The first is through a research testing program where split samples are tested in two labs and the standard deviation of the differences can be calculated for each characteristic. This is similar to a round-robin testing program that would be used to establish precision limits for an ASTM or AASHTO standard test method. However, the split sample research program would be based on plant mixed material, rather than laboratory-prepared specimens.

If a research study is not economical, then the D2S limits from the standard test procedures could serve as a starting point. These limits are developed under close to ideal condition, so they should be thought of as absolute lower limits on allowable tolerances. Without a research study to base decisions, a subjective decision regarding whether to use the D2S, or how much to increase them to account for the less than ideal conditions in the field, must be made by SCDOT.

Since no split sample test data were provided for the current research, it was not possible to perform any statistical analyses to evaluate the allowable tolerances in Table 9.10. The tolerances are, however, within the general range of similar tolerances used by other STDs that were identified during the literature search for the current project. Some of these tolerances are shown in Table 3.8, and are repeated here as Table 9.11.

| State  | Density | Air<br>Voids | AC<br>Content                             | Gradation<br>5/8" or<br>3/8"         | Gradation<br>No. 200                 | VMA  | Bulk<br>Specific<br>Gravity | Max.<br>Specific<br>gravity |
|--|---------|--------------|---|--------------------------------------|--------------------------------------|------|-----------------------------|-----------------------------|
| AR   | 2.0%    | 1.0%         | 0.30%                                     |                                      |                                      | 1.0% |                             |                             |
| FL   |         |              | 0.55%                                     | 5.5%                                 | 1.5%                                 |      | 0.016                       | 0.022                       |
| GA   |         |              | 0.50%                                     | 4.0%                                 | 2.0%                                 |      |                             |                             |
| MS   |         |              | 0.40%                                     | 6.0%                                 | 2.0%                                 |      | 0.030                       | 0.020                       |
| NE   |         | 0.5%         | 0.50%                                     | 5.0%                                 |                                      | 0.5% |                             |                             |
| NY   |         |              |   | 5.0%                                 |                                      |      | 0.200                       | 0.011                       |
| NC   | 2.0%    |              | 0.50%                                     | 5.0%                                 | 2.0%                                 | 1.0% | 0.030                       | 0.020                       |
| ND   |         |              |   | 7.0%                                 | 2.5%                                 |      | 0.040                       | 0.035                       |
| VA<br>1 test<br>2 tests<br>3 tests<br>4 tests<br>8 tests |         |              | 0.60%<br>0.43%<br>0.33%<br>0.30%<br>0.21% | 8.0%<br>5.7%<br>4.4%<br>4.0%<br>2.8% | 2.0%<br>1.4%<br>1.1%<br>1.0%<br>0.7% |      |                             |                             |

Table 9.11. Tolerances Used to Compare Acceptance and Verification Tests

## **Current SCDOT Verification Program**

The current SCDOT verification program requirements are stated in SC-T-97 (05/10), *Method for Verification of Contractor HMA Acceptance Test Results*. These requirements include procedure changes from those used when the data for the current research project were obtained. These new changes are discussed in the following sections.

**Verification Testing.** The new procedures call for taking verification samples that are split three ways: one for the contractor to test, one for the SCDOT verification test, and one to be retained as a possible dispute resolution sample. The verification sample will not be taken from the same truck as an acceptance sample. The contractor is required to test their portion of each day's first verification sample. The verification split sample cannot be used as an acceptance sample. The contractor has the option whether or not to test their portions of the other verification samples. The contractor and SCDOT split verification tests are compared with the allowable tolerances shown in Table 9.12. If the tests do not compare, the contractor can request to have the dispute resolution sample tested. Dispute resolution testing will be done at the OMR Central Laboratory, and the Central Laboratory's results will be used for verification purposes in lieu of the Field Verification Laboratory's results.

#### Table 9.12. Allowable Tolerances for Contractor-SCDOT Split-Sample Verification Tests

| Characteristic            | Tolerance |              |      |  |
|---------------------------|-----------|--------------|------|--|
| Characteristic            | Surface   | Intermediate | Base |  |
| Asphalt Binder Content, % | 0.36      | 0.43         | 0.50 |  |
| Air Voids, %              | 1.15      |              | —    |  |
| VMA, %                    | 1.15      |              | —    |  |

The procedure for establishing the verification data set for the *F*-test and *t*-test comparison has been revised. Rather than to require 5-Lot increments, the procedure now states the following (SC-T-97 (05/10)):

The data set to be evaluated will be test results of 7 or more verification tests conducted by the Department. Contractor HMA quality acceptance test results and SCDOT verification test results from Lot 1 thru a minimum of 7 verification tests will be statistically analyzed and a decision to accept the Contractor HMA quality acceptance test results will be based on whether the data set is believed equal and therefore, have come from the same population. If the analysis of the data set proves a non-comparison of the test results, then the SCDOT verification test results will be used for acceptance.

The second data set will comprise test results from the next Contractor's acceptance tests following data set 1 thru a minimum of 7 verification tests, statistically analyzed and a decision will be made whether to accept or reject the Contractor HMA quality acceptance test results.

The third data set will comprise test results from the next Contractor's acceptance tests following data set 2 thru a minimum of 7 verification tests, statistically analyzed and a

decision will be made whether to accept or reject the Contractor HMA quality acceptance test results.

This process continues until production is completed. If the last data set is less than the minimum of 7 verification tests, then go back to the previous LOTS far enough to yield the number of test needed in the data set.

The new procedure uses *F*-tests and *t*-tests; however the tests are now conducted at the 0.01 level of significance rather than at the 0.05 level that was used previously.

**Comments on the New Procedures.** The new procedures address some issues that were present with the old procedures, and create some additional ones.

<u>Split Sample Verification Tests.</u> The use of split samples for verification tests addresses a potential major concern of contractors since it provides the contractor with a "check" on the verification test results to be used by SCDOT. When the verification and acceptance tests do not check, it is natural that the contractor will be concerned that there was some issue or problem with the STD's verification sampling and testing. Having the contractor run the split sample test helps to alleviate this potential concern.

Since the verification sample cannot be used as an acceptance test, this places an additional testing load on the contractor. There will be at least one additional "required" test each time SCDOT personnel visit the plant to obtain verification samples. And, many contractors will also test some or all of the split samples that are "optional" for them to test. This is not necessarily an issue, since experience has shown that many contractors prefer to have their own split-sample results to compare with the SCDOT test results.

The allowable tolerances on the split sample test results are the same as the specification tolerances for each of the characteristics. As noted above, the best way to establish tolerances for split sample comparisons is through a research testing program to establish the standard deviation of the split sample differences for each characteristic. If a research study is not economical, then the D2S limits from the standard test procedures could serve as a starting point, with the limits being increased somewhat to account for the less than ideal conditions in the field.

There is not widespread precedent for using the specification tolerances as the allowable tolerances for split sample comparisons. The initial thought might be that they are likely to be on the large side since they should have been developed to account for more material variability than should be present in split samples. However, it is difficult to assess the use of these tolerances since the specification limits are established in a totally different manner than typically would be used to establish limits on allowable split sample tolerances.

The specification limits were established to allow an AQL population that has 90 PWL. As such, they were based on being 1.645 standard deviations from the target value. The standard deviation used is the one that was selected as the typical standard deviation to represent the process in question. On the other hand, split sample allowable tolerances are typically based on a selected level of significance. For example, for a 0.05 level of significance, the tolerances

would be established as 1.96 standard deviations (rounded to 2 in the D2S limits). The standard deviation used here is the standard deviation of the differences between the split samples if they came from the same population. This standard deviation would be expected to be smaller than the typical process standard deviation, and would be established by a research study. There is no way to know exactly how the split sample tolerances should compare with the specification tolerances that were established with a totally different purpose in mind.

<u>Recommendation</u>. It is strongly recommended that SCDOT implement a research study to determine appropriate standard deviations to use when establishing split sample allowable tolerances. Without such a study it is difficult to determine the appropriateness of the current tolerances that are shown in Table 9.12.

**7-Test Minimum for Verification Lots.** The new 7-test minimum for verification lots provides more flexibility and, depending upon how it is implemented, has the potential to benefit both the contractors and SCDOT. For example, if sufficient verification testing is performed, then statistical verification comparisons can be done more frequently than waiting tilll after 5 lots have been completed. This might allow for less material to be at risk when the final payment factor determination is made after the verification comparisons are completed.

One potential point of concern is the wording that says that the "data set to be evaluated will be test results of 7 <u>or more</u> verification tests." The term "or more" makes this an open-ended definition for the verification data set. Will this be interpreted to mean that a statistical analysis will take place after every 7 tests? If not, how will the completion of the data set be established? Who will decide how many verification tests will be necessary to trigger the statistical evaluations? SCDOT may wish to clarify the term "or more" by establishing an upper limit on the number of verification tests or lots before the *F*-test and *t*-test evaluations are performed.

**Level of Significance.** The change to the 0.01 level of significance should provide increased confidence that the two data sets actually are different when they do not compare in the F-tests or t-tests. It will make it less likely to incorrectly declare differences when the data sets are not different. However, the lower significance level will also make it more difficult to identify that the data sets are different when they actually are different. Since the ramifications of declaring the data sets different when they are not different can be severe, the switch to 0.01 would seem to be a good decision.

## Closing

The current procedure for establishing the data set for verification comparisons seems to be an improvement over the prior 5-lot approach. However, some more clarification regarding the upper limit of the size of the data set would be an improvement.

SCDOT should conduct two research studies. First, to establish how much, if any, the delay and re-heating aspects of SCDOT's verification tests impacts affects whether the contractor acceptance tests and SCDOT verification tests should compare with one another. The second project needs to determine appropriate standard deviations to use when establishing split sample allowable tolerances. Both of these studies are needed to be able to evaluate fully the verification procedures currently in use by SCDOT.

The addition of contractor and dispute resolution splits to the verification tests is an improvement to the verification procedures. This approach is similar to one in the literature review in Chapter 2, which was recommended in an FHWA technical advisory. The approaches would be the same if SCDOT takes a verification test from each lot on the project and if the contractor's split verification test also served as one of the acceptance tests. This procedure is outlined in Figure 2.1, which is repeated here as Figure 9.1.



Figure 9.1. Verification and IA Testing Utilizing Split Samples (after 4)

## Summary

Acceptance test results and their corresponding verification test results were provided by SCDOT for 10 projects. Most of these projects were different than those that were analyzed above for determining typical process variability values.

Of 53 AC comparisons that were made, 13 times the contractor acceptance tests were rejected in favor of using the SCDOT verification tests to determine the payment factor. For AV, 14 times out of 29 comparisons the contractor tests and SCDOT verification tests did not compare. Similarly, for VMA the tests did not compare in 16 of 29 comparisons.

A number of issues with the previous and the current SCDOT verification procedures were presented and discussed. For example, when SCDOT verification tests are used to determine the payment factor there is a question whether it is appropriate to use the specification limits that were developed for lot-by-lot acceptance since the verification data spanned 5 different lots. Sample calculations showed that the 5-lot standard deviation values were greater than the with-lot standard deviations.

Using the verification tests to determine payment factors for 5-lot increments causes a decrease in the number of lots and a corresponding increase in the size of the lots for which payment decisions are made. This will tend to increase the risks to both SCDOT and the contractor due to the greater amount of material that is being evaluated with typically much fewer tests.

The fact that the acceptance tests and verification tests are declared "different" by the statistical tests provides no information concerning the "cause" of the difference. Any differences between the two sets of tests may be due to a number of different factors. These factors could include differences in sampling and testing procedure, such as re-heating, the effect of one outlier in the smaller number of verification tests, or even contractor manipulated test result data. A procedure for identifying outliers, such as ASTM E-1780-08, should be considered as a possible addition to existing verification procedures.

SCDOT should conduct a research study to identify if differences in procedures, such as reheating and time delays before testing, can be the cause of the data sets failing to compare. Another study needs to be conducted to establish the standard deviation values to use to develop allowable tolerance limits for split sample comparisons.

## CHAPTER 10 — SUMMARY, FINDINGS, AND RECOMMENDATIONS

## Summary

This study was conducted to perform a formal and complete analysis of the SCDOT HMA specification in light of information that had become available since it was last analyzed. A Research Steering Committee comprised of SCDOT, FHWA, and Industry representatives provided oversight of the process.

A literature review was conducted to identify reports and publications that address various aspects of the use of contractor tests for acceptance as well as any procedures for validating contractor tests. In addition, a brief survey instrument was developed and sent by SCDOT to all state materials engineers by means of the Materials Engineer LISTSERVE. The survey instrument was also sent to FHWA's Federal Lands Highways division. To obtain more indepth information, it was planned that in-person interviews be conducted with a few selected STDs that use contractor test results in the acceptance decision.

Extensive statistical analyses were conducted to determine appropriate standard deviation values to represent the variability of each of the acceptance characteristics used by SCDOT. Test result data from SCDOT projects were obtained from SCDOT. A total of 1,260 density test results were provided. In all, density data were provided from 22 different projects, with some projects having multiple HMA mixes involved. A total of 1,775 asphalt content (AC) tests were provided from 30 different projects, with some projects having multiple HMA mixes involved. Since no voids testing was done on Base course mixes, open graded friction course (OGFC) mixes, or Surface E mixes, there were only 1,343 air voids (AV) and VMA tests provided.

Analyses were conducted on the project test results for Density, AC, AV, and VMA with the primary goal of determining values to use to represent the typical variability for each characteristic. This is a subjective decision that ultimately must be made by SCDOT. These variabilities are necessary to evaluate the appropriateness of the existing specification limits. A correlation analysis was also conducted to identify whether correlations existed among Density and the plant characteristics.

Finally, SCDOT verification test results were analyzed and compared with their corresponding contractor acceptance tests. The previous and current SCDOT verification procedures were evaluated and issues concerning each were presented and discussed.

## Findings

The general findings of each of the primary phases of the research effort are presented in the following sections.

**Literature Review.** From the publications identified in the literature search, it is apparent that there was no industry-wide consensus on the adequacy of using contractor tests for acceptance. The number of STDs identified during the literature review with statistical data analysis over a large number of projects was limited to GA, NC, FL, AL, KY, KS, CA, and NM.

These published results look at data from a statewide, multi-project standpoint down to a single project with 6 or more test results for analysis. Consistent results are not typical as there was no distinguishable pattern of data coming from the same or different populations.

There are a number of potential reasons that significant differences arise in contractor and STD performed tests. With knowledge of these potential reasons the STD can make an effort to minimize its chance of affecting the validation procedure. Some of these reasons are provided below in no particular order:

- The number of specimens tested by contractor and state agency technicians.
- The time differences between sampling and testing of specimens often found between contractors and state agencies.
- Differences in procedures.
- Failure to follow prescribed procedures.
- Incorrectly calibrated testing equipment.

**Survey Results.** A total of 42 states/agencies, including 40 states, the FHWA Western Federal Lands Highway Division (WFLHD) and the province of Ontario, Canada (ONT), responded to the survey. A majority of the responding agencies (28 of 42, or 67%) in some way incorporate contractor test results into the acceptance decision. Only 9 of these 28 agencies use *F*-tests and *t*-tests when comparing contractor acceptance tests with the agency's verification tests.

**Interview Results.** Due to the increasing workloads experienced by STDs, it was very difficult and time consuming to set up formal interviews. The interviews that were conducted did not yield significantly more information than could be obtained from the surveys and from the specifications and procedures manuals of the various STDs. It was therefore concluded that eliminating the formal interviews in favor of telephone calls and emails to solicit additional information on an as needed basis was a better approach than continuing with formal STD interviews.

**Results of Density Analyses.** The range of values that SCDOT might consider for the typical Density standard deviation used to evaluate existing specification limits includes 1.16% to 1.26%. These values are greater than the standard deviation of 1.09 that SCDOT used to establish the current Density specification limits. As a result, contractors on the projects for which data were obtained were not able consistently to meet the specification requirements.

**Results of Plant Tests Analyses.** The values for typical standard deviations that SCDOT might consider to represent the typical within-lot variability used to evaluate existing specification limits include:

| Asphalt Content:        | Base Course:<br>Intermediate Course:<br>Surface Course: | 0.25% - 0.295%<br>0.21% - 0.26%<br>0.195% - 0.215% |
|-------------------------|---|--|
| <b>Air Voids:</b> 0.525 | % – 0.59%   |  |

**VMA:** 0.55% – 0.63%

The above values consider only the "within-lot" process standard deviation for each of the characteristics. If SCDOT would also like to consider some form of "target-miss" variability, then the appropriate standard deviations should likely be larger than those shown above.

**Issues Concerning Payment.** The potential variability of the population mean about the target value was considered in addition to the within-lot standard deviation values to develop an overall "process" standard deviation for each of the acceptance characteristics. These standard deviation values were then compared with the current SCDOT specification limits to investigate whether or not these limits are still appropriate.

The standard deviation that was identified as the typical overall project variability for Density is greater than the one used by SCDOT to establish the specification limits. A STD may establish the typical standard deviation value based on data from a number of past projects that it considered "acceptable." Since nearly two-thirds of the projects from which Density data were obtained had average project PWL values less than 90 PWL, SCDOT must decide whether or not it wishes to establish the typical project standard deviation based on the data provided for the current research study.

If SCDOT believes that these projects represent the state-of-the-art regarding the process capability of a typical contractor, then SCDOT may need to re-evaluate their target density value and their density specification limits. If SCDOT believes that these projects do not represent what a typical contractor is capable of providing, then additional data from other representative projects will need to be obtained for analysis.

The values for typical standard deviations that SCDOT might consider to represent the typical overall project variability used to evaluate existing specification limits for plant tests include:

| Asphalt Content: | Base Course:         | 0.26% - 0.30% |
|------------------|----------------------|---------------|
|                  | Intermediate Course: | 0.23% - 0.28% |
|                  | Surface Course:      | 0.21% - 0.23% |

**Air Voids:** 0.63% - 0.69%

**VMA:** 0.64% – 0.71%

In the plant test data there were no obvious inconsistencies among the currently assumed standard deviation values and those calculated based on the project data for the current research. There was therefore no compelling evidence to indicate that a change in specification limits is warranted.

Correlation analyses showed that there were correlations among the plant characteristics of AC, AV, and VMA. AC was negatively correlated with AV and positively correlated with VMA. AV was positively correlated with VMA. The correlation results were less consistent regarding correlations among Density and the plant characteristics, although there was some evidence that Density and AC may be positively correlated in Surface course mixes. These correlations would not impact the average payment that the contractor will receive in the long run for a given quality of material. However, the variability of the individual estimates about this average payment would tend to increase as the magnitude of the correlation coefficients increases. This would therefore place on the contractor a greater payment risk than would be the case for statistically independent acceptance characteristics.

**Verification Testing.** Acceptance test results and their corresponding verification test results were provided by SCDOT for 10 projects. Most of these projects were different than those that were analyzed for determining typical process variability values.

Of 53 AC comparisons that were made, 13 times the contractor acceptance tests were rejected in favor of using the SCDOT verification tests to determine the payment factor. For AV, 14 times out of 29 comparisons the contractor tests and SCDOT verification tests did not compare. Similarly, for VMA the tests did not compare in 16 of 29 comparisons.

A number of issues with the previous and the current SCDOT verification procedures were presented and discussed. For example, when SCDOT verification tests are used to determine the payment factor there is a question whether it is appropriate to use the specification limits that were developed for lot-by-lot acceptance since the verification data spanned 5 different lots. Sample calculations showed that the 5-lot standard deviation values were greater than the within-lot standard deviations.

Using the verification tests to determine payment factors for 5-lot increments causes a decrease in the number of lots and a corresponding increase in the size of the lots for which payment decisions are made. This will tend to increase the risks to both SCDOT and the contractor due to the greater amount of material that is being evaluated with typically much fewer tests. However, the risks to the contractor will be greater than to SCDOT.

The fact that the acceptance tests and verification tests are declared "different" by the statistical tests provides no information concerning the "cause" of the difference. Any differences between the two sets of tests may be due to a number of different factors. These factors could include differences in sampling and testing procedure, such as re-heating; the effect of one outlier in the smaller number of verification tests; or even contractor manipulated test result data.

## Recommendations

Based on the data provided and the analyses that were conducted the following recommendations are made:

- Based on analyses of the Density test result data provided by SCDOT, the current Density specification requirements need to be modified, or else SCDOT needs to decide that the Density data provided are not representative of the quality of work that can be provided by qualified contractors. Based on the data provided, the specification limits need to be widened by a small amount and the Density target value needs to be lowered. If SCDOT believes that these data are not valid, then it should implement an additional research study to evaluate Density data from other projects that SCDOT believes to be representative. These new data would be analyzed to determine the appropriate standard deviation that would be used to evaluate the existing Density specification limits.
- The current specification limits for AC, AV, and VMA still appear to be appropriate based on the test result data that were provided and analyzed. Therefore, no changes are recommended for the specification tolerances for these characteristics.
- SCDOT should re-evaluate the specification limits that are used when the contractor acceptance tests do not compare during the verification process and the SCDOT verification tests are subsequently used to determine the payment factors. If the specification limits were developed for lot-by-lot acceptance, then they may not be appropriate to use when making the decision based on data from multiple lots. SCDOT needs to evaluate the analysis results presented in this report and then decide if they believe that the standard deviation values are different enough to warrant consideration for making changes to the specification limits when the verification tests are used for the acceptance decision.
- SCDOT may wish to consider modifying their verification procedures so that when the verification and acceptance tests compare, the contractor's portion of the split sample verification tests is used along with the acceptance tests. This would increase the lot size by 1 for any lot from which a verification test was taken. It also is allowable under the FHWA Technical Advisory on the use of contractor tests for acceptance (<u>4</u>). This approach is shown in Figures 2.1 and 9.1.
- It is recommended that SCDOT reconsider their procedure for determining the verification data set at the end of a project. Rather than using the same test results in two different verifications, it is recommended that they consider a combination of increasing the size of the last verification data set and adding the last partial data set to the previous data set and then dividing the resulting set into two equal sized sets.
- It is recommended that SCDOT obtain at least one verification sample from each lot on a project. The practice on the projects for which verification data were provided led to some rather uneven distributions of the verification tests among the 5 lots. On one project, 60% of the verification tests were from the last of five lots in the data set.

- It is strongly recommended that SCDOT implement a research study to examine whether or not re-heating, lack of re-heating, delays before testing, and lack of delay have an effect on the resulting test results. Without such a study it is difficult to state with confidence that differences between the acceptance tests and verification tests are due to differences in the material that was sampled and tested by the two parties, and not due to differences in testing procedures.
- It is recommended that SCDOT modify the current wording in SC-T-97 (5/10) that states that the "data set to be evaluated will be test results of 7 or more verification tests." The term "or more" makes this an open-ended definition for the verification data set and raises questions such as the following. Will this be interpreted to mean that a statistical analysis will take place after every 7 tests? If not, how will the completion of the data set be established? Who will decide how many verification tests will be necessary to trigger the statistical evaluations? SCDOT may wish to clarify the term "or more" by establishing an upper limit on the number of verification tests or lots before the *F*-test and *t*-test evaluations are performed.
- SCDOT should consider implementing a procedure for identifying outliers, such as ASTM E-1780-08, as a possible addition to existing verification procedures. This could prevent having a single outlier result in a verification data set failing to compare.
- It is strongly recommended that SCDOT implement a research study to determine appropriate standard deviations to use when establishing split sample allowable tolerances. Without such a study it is difficult to determine the appropriateness of the current tolerances that are the same as the specification tolerance limits. Specification tolerances and allowable differences for split samples serve two totally different purposes and generally are not developed using the same procedures.

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## APPENDIX A — TEST RESULT DATA

The following pages present all of the test result data from projects that were provided by SCDOT. The data are divided into 2 categories. The first category is the density results from the field. The second, plant test results, includes asphalt content (AC), air voids (AV), and voids in the mineral aggregate (VMA). Table A.1 contains the density test results and Table A.2 includes the plant test results.

In the following tables, each project is identified with a unique number, ranging from P01 to P36. Each of these numbered projects corresponds with a unique SCDOT project file number. Since many of the projects had more than one HMA mixture on the project, they also had more than one job mix formula (JMF) that was placed on the project. In the tables, each job mix number is identified with a unique number, ranging from J01 to J83.

## Table A.1. Density Test Results Data

| Proj.<br>No. | Mix<br>Type | JMF<br>No. | Lot<br>No. | Density |
|--------------|-------------|------------|------------|---------|
| P01          | Binder 1    | J02        | 1          | 95.54   |
| P01          | Binder 1    | J02        | 1          | 93.68   |
| P01          | Binder 1    | J02        | 1          | 93.76   |
| P01          | Binder 1    | J02        | 1          | 94.37   |
| P01          | Binder 1    | J02        | 1          | 93.07   |
| P01          | Binder 1    | J02        | 1          | 94.25   |
| P01          | Binder 1    | J02        | 1          | 94.12   |
| P01          | Binder 1    | J02        | 1          | 94.21   |
| P01          | Binder 1    | J02        | 1          | 95.58   |
| P01          | Binder 1    | J02        | 1          | 95.14   |
| P01          | Binder 1    | J02        | 2          | 92.47   |
| P01          | Binder 1    | J02        | 3          | 92.51   |
| P01          | Binder 1    | J02        | 3          | 94.05   |
| P01          | Binder 1    | J02        | 3          | 94.21   |
| P01          | Binder 1    | J02        | 3          | 94.37   |
| P01          | Binder 1    | J02        | 3          | 93.89   |
| P01          | Binder 1    | J02        | 4          | 92.47   |
| P01          | Binder 1    | J02        | 4          | 92.51   |
| P01          | Binder 1    | J02        | 4          | 94.05   |
| P01          | Binder 1    | J02        | 4          | 94.21   |
| P01          | Binder 1    | J02        | 4          | 94.37   |
| P01          | Binder 1    | J02        | 4          | 93.89   |
| P01          | Interm B    | J10        | 1          | 92.33   |
| P01          | Interm B    | J10        | 1          | 92.41   |
| P01          | Interm B    | J10        | 1          | 92.21   |
| P01          | Interm B    | J10        | 4          | 93.10   |
| P01          | Interm B    | J10        | 4          | 92.34   |
| P01          | Interm B    | J10        | 4          | 93.18   |
| P01          | Interm B    | J10        | 4          | 93.66   |
| P01          | Interm B    | J10        | 5          | 92.56   |
| P01          | Interm B    | J10        | 5          | 92.43   |
| P01          | Interm B    | J10        | 5          | 92.39   |
| P01          | Interm B    | J10        | 5          | 92.76   |
| P01          | Interm B    | J10        | 7          | 92.70   |
| P01          | Interm B    | J10        | 7          | 93.91   |
| P01          | Interm B    | J10        | 7          | 94.36   |
| P01          | Interm B    | J10        | 7          | 92.30   |
| P01          | Interm B    | J10        | 7          | 92.22   |
| P01          | Interm B    | J10        | 13         | 93.27   |
| P01          | Interm B    | J10        | 13         | 92.30   |
| P01          | Interm B    | J10        | 13         | 92.71   |
| P01          | Interm B    | J10        | 18         | 92.59   |
| P01          | Interm B    | J10        | 18         | 93.07   |
| P01          | Interm B    | J10        | 18         | 93.88   |
| P01          | Interm B    | J10        | 18         | 92.63   |
| P01          | Interm B    | J10        | 18         | 92.59   |
| P01          | Interm B    | J10        | 20         | 92.95   |
| P01          | Interm B    | J10        | 20         | 93.79   |
| P01          | Interm B    | J10        | 20         | 92.87   |
| P01          | Interm B    | J10        | 20         | 92.91   |

| Proj.<br>No | Mix<br>Type | JMF<br>No | Lot    | Density        |
|-------------|-------------|-----------|--------|----------------|
| P01         | Interm B    | .110      | 20     | 92 71          |
| P01         | Interm B    | 110       | 20     | 03.87          |
| P01         | Interm B    | .123      | 1      | 93.52          |
| P01         | Interm B    | 123       | 1      | 0/ 77          |
| P01         | Interm B    | 123       | 1      | 02.52          |
| P01         | Interm B    | 123       | 1      | 92.52          |
| P01         | Interm B    | 123       | 1      | 94.07          |
| P01         | Interm B    | 123       | 2      | 92.62          |
| P01         | Interm B    | 123       | 2      | 92.02          |
| P01         | Interm B    | 123       | 2      | 95.63          |
| P01         | Surf 1C     | 107       | 2<br>8 | 02.00          |
| P01         | Surf 1C     | 107       | 8      | 92.22          |
|             | Surf 1C     | 107       | 0      | 92.71          |
| P01         | Surf 1C     | 107       | 0      | 92.71          |
| P01         | Surf 1C     | 107       | 0      | 92.00          |
| P01         | Surf 1C     | 107       | 10     | 92.01          |
| P01         | Surf 1C     | 107       | 10     | 93.00          |
| P01         | Surf 1C     | 107       | 10     | 93.42          |
|             | Surf 1C     | 107       | 10     | 94.11          |
|             | Sull IC     | 307       | 10     | 93.10          |
| P01         | Sull IC     | J07       | 11     | 93.17          |
| P01         | Surf 1C     | J07       | 11     | 93.21          |
| P01         | Surf 1C     | J07       | 11     | 92.00          |
| PUI<br>D04  | Sull IC     | J07       | 11     | 93.00          |
| P01         | Surf 1C     | J07       | 11     | 93.01          |
| P01         | Surf 1C     | J07       | 11     | 93.42          |
| P01         | Surf 1C     | J07       | 12     | 94.49          |
|             | Surf 1C     | 107       | 12     | 92.90          |
|             | Surf 1C     | 107       | 12     | 92.75          |
| P01         | Surf 1C     | J07       | 12     | 95.51          |
| P01         | Surf 1C     | 107       | 12     | 92.00          |
|             | Surf 1C     | 107       | 12     | 93.93          |
|             | Surf D      | 107       | 12     | 93.93          |
| P01         | Surf B      | J07       | 2      | 92.70          |
| P01         | Surf D      | 107       | 2      | 92.00          |
| P01         | Surf B      | 107       | 2      | 92.00          |
| P01         | Surf B      | 107       | 2      | 92.27          |
| P01         | Surf B      | 107       | 2      | 93.20          |
| P01         | Surf B      | 107       | 4      | 92.21          |
|             | Surf D      | 107       | 4      | 92.09          |
|             |             | 107       | 4      | 93.30          |
|             |             | 107       | 4<br>5 | 93.04          |
|             |             | 107       | 5      | 92.40<br>02.79 |
|             |             | 107       | F      | 32.10<br>02.27 |
|             |             | 107       | 5<br>6 | 92.31          |
|             |             | 107       | e o    | 92.41          |
|             |             | 107       | 6      | 92.41<br>02.40 |
|             |             | 107       | 6      | 92.49<br>02.21 |
|             |             | 107       | e o    | 92.21          |
|             |             | 107       | 7      | 92.21          |
| FUI         | Sull D      | 307       | 1      | 92.49          |

| Table A.  | 1. Density | <b>Test Results</b> | Data | (continued) |
|-----------|------------|---------------------|------|-------------|
| 14810 / 4 |            | 1000110000100       | Bata | (oonanaoa)  |

| Proj.<br>No. | Mix<br>Type | JMF<br>No. | Lot<br>No. | Density        |
|--------------|-------------|------------|------------|----------------|
| P01          | Surf B      | J07        | 7          | 94.55          |
| P01          | Surf B      | J07        | 7          | 92.81          |
| P03          | Interm B    | J04        | 1          | 94.33          |
| P03          | Interm B    | J04        | 1          | 93.97          |
| P03          | Interm B    | J04        | 1          | 92.08          |
| P03          | Interm B    | J04        | 1          | 93.49          |
| P03          | Interm B    | J04        | 1          | 91.68          |
| P03          | Interm B    | J04        | 5          | 92.98          |
| P03          | Interm B    | J04        | 5          | 94.36          |
| P03          | Interm B    | J04        | 5          | 94.12          |
| P03          | Interm B    | J04        | 5          | 95.78          |
| P03          | Interm B    | J04        | 7          | 94.45          |
| P03          | Interm B    | J04        | 7          | 93.80          |
| P03          | Interm B    | J04        | 7          | 94.25          |
| P03          | Interm B    | J04        | 7          | 94.65          |
| P03          | Interm B    | J04        | 7          | 94.94          |
| P03          | Interm B    | J04        | 7          | 92.99          |
| P03          | Interm B    | J04        | 7          | 95.42          |
| P03          | Interm B    | J04        | 7          | 94.45          |
| P03          | Interm B    | J04        | 7          | 95.14          |
| P03          | Interm B    | J04        | 7          | 95.63          |
| P03          | Interm B    | J04        | 7          | 95.14          |
| P03          | Interm B    | .104       | 7          | 94 49          |
| P03          | Interm B    | .104       | 11         | 93.24          |
| P03          | Interm B    | .104       | 11         | 94.42          |
| P03          | Interm B    | .104       | 11         | 94.13          |
| P03          | Interm B    | .104       | 14         | 92.29          |
| P03          | Interm B    | .104       | 14         | 91 33          |
| P03          | Interm B    | .104       | 14         | 93.10          |
| P03          | Interm B    | .104       | 14         | 93 34          |
| P03          | Interm B    | 104        | 14         | 92.01          |
| P03          | Interm B    | 104        | 14         | 89.88          |
| P03          | Surf B      | 115        | 3          | 93.00          |
| P03          | Surf B      | 115        | 3          | 94.30          |
| P03          | Surf B      | 115        | 3          | 02.83          |
| P03          | Surf B      | 115        | 3          | 02.00          |
| P03          | Surf B      | 115        | 3          | 93.05          |
| P03          | Surf B      | 115        | 4          | 93.39          |
| P03          | Surf B      | 115        | 4          | 01.02          |
| P03          | Surf B      | 115        | 4          | 01.92          |
| P03          | Surf B      | J15        | 4<br>5     | 91.07          |
| P03          | Surf D      | 115        | 5          | 05 10          |
| P03          | Surf D      | 115        | 5          | 90.19<br>01.00 |
| P03          | Surf D      | 115        | 5          | 91.20          |
| P03          | Surf D      | 115        | 5          | 92.04          |
| FU3          |             | J15<br> 4E | 5<br>F     | 94.00          |
| F U3         |             | 115        | 5          | 90.70<br>02 04 |
| P03          |             | J15        | ວ<br>F     | 93.84          |
| P03          | Suff B      |            | 5<br>F     | 92.17          |
| P03          |             |            | о<br>Г     | 93.68          |
| P03          | Suff B      | J15        | 5          | 90.62          |

| Proj. | Mix     | JMF | Lot | Density |
|-------|---------|-----|-----|---------|
| No.   | Туре    | No. | No. | Density |
| P03   | Surf B  | J15 | 6   | 93.53   |
| P03   | Surf B  | J15 | 6   | 93.97   |
| P03   | Surf B  | J15 | 6   | 93.44   |
| P03   | Surf B  | J15 | 6   | 94.95   |
| P03   | Surf B  | J15 | 7   | 93.72   |
| P03   | Surf B  | J15 | 7   | 93.88   |
| P03   | Surf B  | J15 | 7   | 95.14   |
| P04   | Surf 1R | J14 | 1   | 88.54   |
| P04   | Surf 1R | J14 | 1   | 88.34   |
| P04   | Surf 1R | J14 | 1   | 88.38   |
| P04   | Surf 1R | J14 | 1   | 90.19   |
| P04   | Surf 1R | J14 | 1   | 88.89   |
| P04   | Surf 1R | J14 | 1   | 89.21   |
| P04   | Surf 1R | J14 | 1   | 90.89   |
| P04   | Surf 1R | J14 | 1   | 85.40   |
| P04   | Surf 1R | J14 | 2   | 90.43   |
| P04   | Surf 1R | J14 | 2   | 91.14   |
| P04   | Surf 1R | J14 | 2   | 90.67   |
| P04   | Surf 1R | J14 | 2   | 90.71   |
| P04   | Surf 1R | J14 | 2   | 89.39   |
| P04   | Surf 1R | J14 | 2   | 90.27   |
| P04   | Surf 1R | J14 | 2   | 90.17   |
| P04   | Surf 1R | J14 | 2   | 89.47   |
| P04   | Surf 1R | J14 | 3   | 89.48   |
| P04   | Surf 1R | J14 | 3   | 91.74   |
| P04   | Surf 1R | J14 | 3   | 89.24   |
| P04   | Surf 1R | J14 | 3   | 91.66   |
| P04   | Surf 1R | J14 | 3   | 89.44   |
| P04   | Surf 1R | J14 | 3   | 88.92   |
| P04   | Surf 1R | J14 | 4   | 91.24   |
| P04   | Surf 1R | J14 | 4   | 91.28   |
| P04   | Surf 1R | J14 | 4   | 88.25   |
| P04   | Surf 1R | J14 | 4   | 90.68   |
| P04   | Surf 1R | J14 | 4   | 89.13   |
| P04   | Surf 1R | J14 | 4   | 89.13   |
| P04   | Surf 1R | J14 | 4   | 90.00   |
| P04   | Surf 1R | J14 | 4   | 91.16   |
| P04   | Surf 1R | J14 | 4   | 88.69   |
| P04   | Surf 1R | J14 | 5   | 91.06   |
| P04   | Surf 1R | J14 | 5   | 91.10   |
| P04   | Surf 1R | J14 | 5   | 88.08   |
| P04   | Surf 1R | J14 | 5   | 90.50   |
| P04   | Surf 1R | J14 | 5   | 88.95   |
| P06   | Surf 1  | J26 | 1   | 89.98   |
| P06   | Surf 1  | J26 | 1   | 90.56   |
| P06   | Surf 1  | J26 | 1   | 89.57   |
| P06   | Surf 1  | J26 | 1   | 90.07   |
| P06   | Surf 1  | J26 | 1   | 89.61   |
| P06   | Surf 1  | J26 | 1   | 91.30   |
| P06   | Surf 1  | J26 | 1   | 92.12   |

| Table A.1. | Density | <b>Test Results</b> | Data | (continued) |
|------------|---------|---------------------|------|-------------|
|------------|---------|---------------------|------|-------------|

| Proj.<br>No. | Mix<br>Type | JMF<br>No. | Lot<br>No. | Density |
|--------------|-------------|------------|------------|---------|
| P06          | Surf 1      | J26        | 1          | 88.38   |
| P06          | Surf 1      | J26        | 1          | 88.38   |
| P06          | Surf 1      | J26        | 1          | 91.63   |
| P06          | Surf 1      | J26        | 1          | 89.04   |
| P06          | Surf 1      | J26        | 1          | 90.80   |
| P06          | Surf 1      | J26        | 1          | 90.35   |
| P06          | Surf 1      | J26        | 1          | 88.96   |
| P06          | Surf 1D     | J24        | 1          | 92.99   |
| P06          | Surf 1D     | J24        | 1          | 90.40   |
| P06          | Surf 1D     | J24        | 1          | 90.93   |
| P06          | Surf 1D     | J24        | 1          | 90.12   |
| P06          | Surf 1D     | J24        | 1          | 89.27   |
| P06          | Surf 1D     | J24        | 1          | 88.90   |
| P06          | Surf 1D     | J24        | 2          | 91.17   |
| P06          | Surf 1D     | J24        | 2          | 91.17   |
| P06          | Surf 1D     | J24        | 2          | 87.36   |
| P06          | Surf 1D     | J24        | 2          | 88.10   |
| P06          | Surf 1D     | J24        | 2          | 90.31   |
| P06          | Surf 1D     | J24        | 2          | 90.84   |
| P06          | Surf 1D     | J24        | 3          | 92.20   |
| P06          | Surf 1D     | J24        | 3          | 92.85   |
| P06          | Surf 1D     | J24        | 3          | 92.90   |
| P06          | Surf 1D     | J24        | 3          | 92.00   |
| P06          | Surf 1D     | J24        | 3          | 91.87   |
| P06          | Surf 1D     | J24        | 4          | 92.61   |
| P06          | Surf 1D     | J24        | 4          | 93.96   |
| P06          | Surf 1D     | J24        | 4          | 93.34   |
| P06          | Surf 1D     | J24        | 4          | 93.55   |
| P06          | Surf 1D     | J24        | 5          | 92.34   |
| P06          | Surf 1D     | J24        | 5          | 91.89   |
| P06          | Surf 1D     | J24        | 5          | 93.15   |
| P06          | Surf 1D     | J24        | 5          | 92.42   |
| P08          | Surf 1R     | J11        | 1          | 89.90   |
| P08          | Surf 1R     | J11        | 1          | 88.87   |
| P08          | Surf 1R     | J11        | 1          | 90.10   |
| P08          | Surf 1R     | J11        | 1          | 87.63   |
| P08          | Surf 1R     | J11        | 1          | 89.62   |
| P08          | Surf 1R     | J11        | 1          | 86.96   |
| P08          | Surf 1R     | J11        | 1          | 88.39   |
| P08          | Surf 1R     | J11        | 1          | 87.75   |
| P13          | Surf C      | J03        | 10         | 91.82   |
| P13          | Surf C      | J03        | 10         | 91.16   |
| P13          | Surf C      | J03        | 10         | 93.42   |
| P13          | Surf C      | J03        | 10         | 92.89   |
| P13          | Surf C      | J03        | 10         | 91.12   |
| P13          | Surf C      | J03        | 10         | 95.07   |
| P13          | Surf C      | J03        | 10         | 91.61   |
| P13          | Surf C      | J03        | 10         | 90.83   |
| P13          | Surf C      | J03        | 10         | 90.21   |
| P14          | Surf C      | J16        | 4          | 89.98   |

| Proj.<br>No. | Mix<br>Type | JMF<br>No. | Lot<br>No. | Density |
|--------------|-------------|------------|------------|---------|
| P14          | Surf C      | J16        | 4          | 92.10   |
| P14          | Surf C      | J16        | 4          | 93.78   |
| P14          | Surf C      | J16        | 4          | 93.70   |
| P14          | Surf C      | J16        | 4          | 93.37   |
| P14          | Surf C      | J16        | 4          | 93.17   |
| P14          | Surf C      | J16        | 7          | 91.49   |
| P14          | Surf C      | J16        | 7          | 93.62   |
| P14          | Surf C      | J16        | 7          | 94.44   |
| P14          | Surf C      | J16        | 7          | 92.55   |
| P14          | Surf C      | J16        | 7          | 91.82   |
| P14          | Surf C      | J16        | 7          | 93.33   |
| P14          | Surf C      | J16        | 7          | 93.17   |
| P14          | Surf C      | J16        | 8          | 92.37   |
| P14          | Surf C      | J16        | 8          | 93.85   |
| P14          | Surf C      | J16        | 8          | 92.86   |
| P14          | Surf C      | J16        | 8          | 92.99   |
| P14          | Surf C      | J16        | 8          | 91.67   |
| P14          | Surf C      | J16        | 8          | 92.62   |
| P14          | Surf C      | J16        | 10         | 92.19   |
| P14          | Surf C      | J16        | 10         | 93.60   |
| P14          | Surf C      | J16        | 10         | 90.20   |
| P14          | Surf C      | J16        | 10         | 93.97   |
| P14          | Surf C      | J16        | 10         | 90.44   |
| P14          | Surf C      | J16        | 10         | 90.32   |
| P14          | Surf C      | J16        | 10         | 93.68   |
| P14          | Surf C      | J16        | 10         | 92.70   |
| P14          | Surf C      | J16        | 10         | 88.68   |
| P14          | Surf C      | J16        | 10         | 91.76   |
| P14          | Surf C      | J16        | 11         | 92.66   |
| P14          | Surf C      | J16        | 11         | 91.71   |
| P14          | Surf C      | J16        | 11         | 92.82   |
| P14          | Surf C      | J16        | 11         | 91.43   |
| P14          | Surf C      | J16        | 11         | 92.00   |
| P14          | Surf C      | J16        | 15         | 94.42   |
| P14          | Surf C      | J16        | 15         | 92.50   |
| P14          | Surf C      | J16        | 15         | 93.52   |
| P14          | Surf C      | J16        | 15         | 91.84   |
| P15          | Surf C      | J44        | 1          | 92.90   |
| P15          | Surf C      | J44        | 1          | 93.42   |
| P15          | Surf C      | J44        | 1          | 91.94   |
| P15          | Surf C      | J44        | 2          | 92.71   |
| P15          | Surf C      | J44        | 2          | 93.23   |
| P15          | Surf C      | J44        | 2          | 91.75   |
| P15          | Surf C      | J44        | 3          | 91.37   |
| P15          | Surf C      | J44        | 3          | 94.36   |
| P15          | Surf C      | J44        | 3          | 94.08   |
| P15          | Surf C      | J44        | 3          | 90.57   |
| P15          | Surf C      | J44        | 4          | 91.66   |
| P15          | Surf C      | J44        | 4          | 94.67   |
| P15          | Surf C      | J44        | 4          | 94.39   |

| Table A.1 | I. Densitv | <b>Test Results</b> | Data   | (continued)                             |
|-----------|------------|---------------------|--------|---|
|           |            | 1 oot noouno        | - alla | (•••••••••••••••••••••••••••••••••••••• |

| Proj.<br>No. | Mix<br>Type | JMF<br>No. | Lot<br>No. | Density |
|--------------|-------------|------------|------------|---------|
| P15          | Surf C      | J44        | 4          | 90.86   |
| P15          | Surf C      | J44        | 5          | 91.37   |
| P15          | Surf C      | J44        | 5          | 94.36   |
| P15          | Surf C      | J44        | 5          | 94.08   |
| P15          | Surf C      | J44        | 5          | 90.57   |
| P16          | Surf C      | J20        | 1          | 90.47   |
| P16          | Surf C      | J20        | 1          | 93.43   |
| P16          | Surf C      | J20        | 1          | 90.27   |
| P16          | Surf C      | J20        | 1          | 91.33   |
| P16          | Surf C      | J20        | 2          | 91.90   |
| P16          | Surf C      | J20        | 2          | 91.08   |
| P16          | Surf C      | J20        | 2          | 90.96   |
| P16          | Surf C      | J20        | 2          | 90.67   |
| P16          | Surf C      | J20        | 3          | 91.76   |
| P16          | Surf C      | J20        | 3          | 91.60   |
| P16          | Surf C      | J20        | 3          | 93.66   |
| P16          | Surf C      | J20        | 3          | 91.85   |
| P18          | Surf C      | J48        | 2          | 92.06   |
| P18          | Surf C      | J48        | 2          | 90.37   |
| P18          | Surf C      | J48        | 2          | 91.32   |
| P18          | Surf C      | J48        | 2          | 94.20   |
| P18          | Surf C      | J48        | 2          | 91.73   |
| P18          | Surf C      | J48        | 2          | 93.25   |
| P18          | Surf C      | J48        | 2          | 88.44   |
| P18          | Surf C      | J48        | 4          | 93.78   |
| P18          | Surf C      | J48        | 4          | 92.34   |
| P18          | Surf C      | J48        | 4          | 89.91   |
| P18          | Surf C      | J48        | 5          | 92.36   |
| P18          | Surf C      | J48        | 5          | 93.35   |
| P18          | Surf C      | J48        | 5          | 89.20   |
| P18          | Surf C      | J48        | 5          | 93.02   |
| P18          | Surf C      | J48        | 5          | 92.24   |
| P18          | Surf C      | J48        | 5          | 88.75   |
| P18          | Surf C      | J48        | 5          | 89.33   |
| P18          | Surf C      | J48        | 5          | 92.24   |
| P20          | Surf C      | J50        | 2          | 92.73   |
| P20          | Surf C      | J50        | 2          | 93.80   |
| P20          | Surf C      | J50        | 2          | 92.94   |
| P20          | Surf C      | J50        | 2          | 94.13   |
| P20          | Surf C      | J50        | 2          | 93.51   |
| P20          | Surf C      | J50        | 2          | 92.03   |
| P20          | Surf C      | J50        | 2          | 91.83   |
| P20          | Surf C      | J50        | 2          | 91.83   |
| P20          | Surf C      | J50        | 2          | 91.42   |
| P20          | Surf C      | J50        | 2          | 93.10   |
| P20          | Surf C      | J50        | 2          | 91.66   |
| P20          | Surf C      | J50        | 4          | 91.75   |
| P20          | Surf C      | J50        | 4          | 92.00   |
| P20          | Surf C      | J50        | 4          | 91.88   |
| P20          | Surf C      | J50        | 4          | 93.64   |

| Proj. | Mix    | JMF  | Lot | Density        |
|-------|--------|------|-----|----------------|
| P20   | Surf C | .150 | 4   | 93 15          |
| P20   | Surf C | 150  | 4   | 00.10<br>01.14 |
| P20   | Surf C | 150  | 4   | 01.14<br>01.30 |
| P20   | Surf C | 150  | 4   | 01.63          |
| D20   | Surf C | 150  | 4   | 02.27          |
| P20   | Surf C | J50  | 4   | 92.37          |
| F20   | Sun C  | J50  | 4   | 91.00          |
| P20   | Surf C | J50  | 4   | 90.77          |
| P20   | SurrC  | J50  | 4   | 91.05          |
| P20   | Surf C | J50  | 7   | 91.96          |
| P20   | Surf C | J50  | /   | 91.77          |
| P20   | Surf C | J50  | 7   | 92.43          |
| P20   | Surf C | J50  | 7   | 91.89          |
| P20   | Surf C | J50  | 7   | 93.29          |
| P20   | Surf C | J50  | 7   | 91.52          |
| P20   | Surf C | J50  | 7   | 93.00          |
| P20   | Surf C | J50  | 7   | 92.22          |
| P20   | Surf C | J50  | 7   | 92.55          |
| P20   | Surf C | J50  | 7   | 90.04          |
| P20   | Surf C | J50  | 7   | 93.17          |
| P20   | Surf C | J50  | 8   | 92.08          |
| P20   | Surf C | J50  | 8   | 91.35          |
| P20   | Surf C | J50  | 8   | 93.48          |
| P20   | Surf C | J50  | 8   | 92.17          |
| P20   | Surf C | J50  | 8   | 92.08          |
| P20   | Surf C | J50  | 8   | 93.77          |
| P20   | Surf C | J50  | 8   | 92.08          |
| P20   | Surf C | J50  | 11  | 94.09          |
| P20   | Surf C | J50  | 11  | 92.94          |
| P20   | Surf C | J50  | 11  | 93.51          |
| P20   | Surf C | J50  | 11  | 91.58          |
| P20   | Surf C | J50  | 11  | 90.23          |
| P20   | Surf C | J50  | 11  | 93.39          |
| P20   | Surf C | J50  | 11  | 93.22          |
| P20   | Surf C | J50  | 11  | 92.77          |
| P20   | Surf C | J50  | 14  | 92.37          |
| P20   | Surf C | J50  | 14  | 92.82          |
| P20   | Surf C | J50  | 14  | 91.79          |
| P20   | Surf C | J50  | 14  | 91.96          |
| P20   | Surf C | J50  | 14  | 94.30          |
| P20   | Surf C | J50  | 14  | 94.34          |
| P20   | Surf C | J50  | 14  | 92.12          |
| P20   | Surf C | .150 | 14  | 92 70          |
| P20   | Surf C | J50  | 15  | 91.47          |
| P20   | Surf C | 150  | 15  | 93 15          |
| P20   | Surf C | .150 | 15  | 92.41          |
| P20   | Surf C | .150 | 15  | 92.66          |
| P20   | Surf C | 150  | 15  | 01.00          |
| P20   | Surf C | 150  | 15  | Q3 11          |
| D20   | Surf C | 150  | 15  | 02.22          |
| D20   | Surf C | 150  | 15  | 02.00          |
| F20   | Sun C  | 000  | 01  | 92.90          |

| Table A.1. Density Test Results Data (continued | ) |
|---|---|
|---|---|

| Proj.<br>No | Mix<br>Type | JMF<br>No | Lot<br>No | Density |
|-------------|-------------|-----------|-----------|---------|
| P20         | Surf C      | .150      | 15        | 91 98   |
| P20         | Surf C      | .150      | 15        | 91.59   |
| P23         | Interm B    | .133      | 1         | 92.23   |
| P23         | Interm B    | .133      | 1         | 93.40   |
| P23         | Interm B    | .133      | 1         | 90.26   |
| P23         | Interm B    | .133      | 2         | 91 49   |
| P23         | Interm B    | .133      | 2         | 92.65   |
| P23         | Interm B    | .133      | 2         | 89.54   |
| P23         | Interm B    | .133      | 3         | 93.66   |
| P23         | Interm B    | .133      | 3         | 92.98   |
| P23         | Interm B    | 133       | 3         | 90.66   |
| P23         | Interm B    | .133      | 3         | 91 50   |
| P23         | Interm B    | 133       | 3         | 90.42   |
| P23         | Interm B    | 133       | 4         | 03.72   |
| P23         | Interm B    | 133       | 4         | 92.61   |
| P23         | Interm B    | 133       | 4         | 90.30   |
| P23         | Interm B    | 133       | 4         | 01.13   |
| P23         | Interm B    | 133       | 4         | 91.15   |
| P23         | Surf B      | 163       | 1         | 92.81   |
| P23         | Surf B      | 163       | 1         | 02.01   |
| P23         | Surf B      | 163       | 1         | 92.23   |
| P23         | Surf B      | 163       | 2         | 03.15   |
| P23         | Surf B      | 163       | 2         | 92.59   |
| P23         | Surf B      | 163       | 2         | 92.59   |
| P23         | Surf B      | 163       | 2         | 02.80   |
| P23         | Surf B      | .163      | 3         | 92.09   |
| P23         | Surf B      | 163       | 3         | 02.02   |
| P23         | Surf B      |           | 4         | 92.93   |
| P23         | Surf B      | .163      | 4         | 92.36   |
| P23         | Surf B      | .163      | 4         | 93.33   |
| P23         | Surf B      |           | 5         | 92 85   |
| P23         | Surf B      | .163      | 5         | 94 10   |
| P23         | Surf B      | .163      | 5         | 93.26   |
| P23         | Surf B      | .163      | 6         | 93 15   |
| P23         | Surf B      | J63       | 6         | 94.41   |
| P23         | Surf B      | J63       | 6         | 93.56   |
| P24         | Surf C      | J56       | 2         | 95.28   |
| P24         | Surf C      | J56       | 2         | 95.28   |
| P24         | Surf C      | J56       | 2         | 91.58   |
| P24         | Surf C      | J56       | 2         | 91.29   |
| P24         | Surf C      | J56       | 2         | 90.35   |
| P24         | Surf C      | J56       | 2         | 91.75   |
| P24         | Surf C      | J56       | 2         | 92.32   |
| P24         | Surf C      | J56       | 2         | 93,18   |
| P24         | Surf C      | J56       | 2         | 94.29   |
| P24         | Surf C      | J56       | 2         | 92.69   |
| P24         | Surf C      | J56       | 2         | 93,84   |
| P24         | Surf C      | J56       | 6         | 93,43   |
| P24         | Surf C      | J56       | 6         | 93.63   |
| P24         | Surf C      | J56       | 6         | 93.39   |
| L           | -           | · · · · · |           |         |

| Proj. | Mix    | JMF  | Lot | Density |
|-------|--------|------|-----|---------|
| NO.   | Type   | NO.  | NO. |         |
| P24   | Surf C | J56  | 6   | 94.74   |
| P24   | Surf C | J56  | 9   | 93.95   |
| P24   | Surf C | J56  | 9   | 93.66   |
| P24   | Surf C | J56  | 9   | 95.02   |
| P24   | Surf C | J56  | 9   | 93.79   |
| P24   | Surf C | J56  | 9   | 91.73   |
| P24   | Surf C | J56  | 9   | 93.09   |
| P24   | Surf C | J56  | 11  | 91.67   |
| P24   | Surf C | J56  | 11  | 91.22   |
| P24   | Surf C | J56  | 11  | 93.49   |
| P24   | Surf C | J56  | 11  | 91.96   |
| P24   | Surf C | J56  | 11  | 93.08   |
| P24   | Surf C | J56  | 11  | 92.99   |
| P24   | Surf C | J56  | 11  | 93.03   |
| P24   | Surf C | J56  | 11  | 93.08   |
| P24   | Surf C | J56  | 14  | 92.92   |
| P24   | Surf C | J56  | 14  | 93.49   |
| P24   | Surf C | J56  | 14  | 94.65   |
| P24   | Surf C | J56  | 14  | 93.37   |
| P24   | Surf C | J56  | 14  | 92.05   |
| P24   | Surf C | J56  | 14  | 92.79   |
| P24   | Surf C | J56  | 14  | 93.90   |
| P24   | Surf C | J56  | 14  | 92.55   |
| P24   | Surf C | J56  | 14  | 94.60   |
| P24   | Surf C | J56  | 17  | 92.50   |
| P24   | Surf C | J56  | 17  | 93.86   |
| P24   | Surf C | J56  | 17  | 93.16   |
| P24   | Surf C | J56  | 17  | 92.25   |
| P24   | Surf C | J56  | 17  | 93.65   |
| P24   | Surf C | J56  | 17  | 92.70   |
| P24   | Surf C | J56  | 17  | 93.61   |
| P24   | Surf C | J56  | 17  | 93.90   |
| P24   | Surf C | J56  | 17  | 92.70   |
| P24   | Surf C | J56  | 18  | 94.16   |
| P24   | Surf C | J56  | 18  | 92.89   |
| P24   | Surf C | J56  | 18  | 90.75   |
| P24   | Surf C | J56  | 18  | 94.04   |
| P24   | Surf C | .156 | 18  | 93 71   |
| P24   | Surf C | .156 | 18  | 93.30   |
| P24   | Surf C | 156  | 18  | 92.30   |
| P24   | Surf C | 156  | 18  | 92.85   |
| D24   | Surf C | 156  | 18  | 02.00   |
| P26   | Surf A | .162 | 1   | 93.50   |
| P26   |        | 162  | 1   | 03.09   |
| P26   |        | 162  | 1   | 94.52   |
| P26   |        | 162  | 1   | 94.00   |
| D26   |        | 162  | 1   | 04.04   |
| F20   | Surf A | 102  | 1   | 94.21   |
| F20   | Surf A | 102  | 1   | 03.47   |
| F20   | Surf A | 102  | 1   | 92.00   |
| P26   | Surt A | J62  | 1   | 93.25   |
| Proj.<br>No. | Mix<br>Type | JMF<br>No. | Lot<br>No. | Density |
|--------------|-------------|------------|------------|---------|
| P26          | Surf A      | J62        | 2          | 93.47   |
| P26          | Surf A      | J62        | 2          | 92.95   |
| P26          | Surf A      | J62        | 2          | 94.83   |
| P26          | Surf A      | J62        | 2          | 94.19   |
| P26          | Surf A      | J62        | 3          | 92.67   |
| P26          | Surf A      | J62        | 3          | 92.63   |
| P26          | Surf A      | J62        | 3          | 92.14   |
| P26          | Surf A      | J62        | 4          | 92.68   |
| P26          | Surf A      | J62        | 4          | 92.36   |
| P26          | Surf A      | J62        | 4          | 90.48   |
| P26          | Surf A      | J62        | 4          | 89.68   |
| P26          | Surf A      | J62        | 4          | 93.28   |
| P26          | Surf A      | J62        | 5          | 93.29   |
| P26          | Surf A      | J62        | 5          | 94.38   |
| P26          | Surf A      | J62        | 5          | 92.41   |
| P26          | Surf A      | J62        | 5          | 91.12   |
| P26          | Surf A      | J62        | 5          | 92.85   |
| P26          | Surf A      | J62        | 6          | 92.50   |
| P26          | Surf A      | J62        | 6          | 92.30   |
| P26          | Surf A      | J62        | 6          | 93.78   |
| P26          | Surf A      | J62        | 6          | 93.38   |
| P26          | Surf A      | J62        | 7          | 93.56   |
| P26          | Surf A      | J62        | 7          | 92.95   |
| P26          | Surf A      | J62        | 7          | 91.58   |
| P26          | Surf A      | J62        | 7          | 93.64   |
| P26          | Surf A      | J62        | 7          | 93.60   |
| P26          | Surf A      | J62        | 8          | 93.18   |
| P26          | Surf A      | J62        | 8          | 92.90   |
| P26          | Surf A      | J62        | 8          | 93.62   |
| P26          | Surf A      | J62        | 9          | 91.57   |
| P26          | Surf A      | J62        | 9          | 90.93   |
| P26          | Surf A      | J62        | 9          | 92.37   |
| P26          | Surf A      | J62        | 9          | 91.97   |
| P26          | Surf A      | J62        | 9          | 93.42   |
| P26          | Surf A      | J69        | 1          | 91.60   |
| P26          | Surf A      | J69        | 1          | 94.01   |
| P26          | Surf A      | J69        | 1          | 94.25   |
| P26          | Surf A      | J69        | 1          | 92.32   |
| P26          | Surf A      | J69        | 1          | 94.17   |
| P26          | Surf A      | J69        | 2          | 91.10   |
| P26          | Surf A      | J69        | 2          | 89.70   |
| P26          | Surf A      | J69        | 2          | 94.57   |
| P26          | Surf A      | J69        | 2          | 93.22   |
| P26          | Surf A      | J69        | 2          | 95.89   |

| Proj.<br>No. | Mix<br>Type | JMF<br>No. | Lot<br>No. | Density |
|--------------|-------------|------------|------------|---------|
| P26          | Surf A      | J69        | 4          | 94.16   |
| P26          | Surf A      | J69        | 4          | 93.88   |
| P26          | Surf A      | J69        | 4          | 94.88   |
| P26          | Surf A      | J69        | 4          | 94.36   |
| P26          | Surf A      | J69        | 5          | 93.07   |
| P26          | Surf A      | J69        | 5          | 94.43   |
| P26          | Surf A      | J69        | 5          | 93.51   |
| P26          | Surf A      | J69        | 5          | 94.31   |
| P26          | Surf A      | J69        | 6          | 94.46   |
| P26          | Surf A      | J69        | 6          | 94.30   |
| P26          | Surf A      | J69        | 6          | 94.14   |
| P26          | Surf A      | J69        | 6          | 95.19   |
| P26          | Surf A      | J69        | 6          | 93.34   |
| P26          | Surf A      | J69        | 7          | 92.54   |
| P26          | Surf A      | J69        | 7          | 92.70   |
| P26          | Surf A      | J69        | 7          | 92.26   |
| P26          | Surf A      | .169       | 7          | 94.58   |
| P26          | Surf A      | .169       | 7          | 94.30   |
| P26          | Surf A      | .169       | 7          | 93.86   |
| P26          | Surf A      | .169       | 8          | 93.28   |
| P26          | Surf A      | 160        | 8          | 02.52   |
| P26          | Surf A      | 160        | 8          | 92.92   |
| T 20         | Surf A      | 160        | 0          | 02.94   |
| F20          | Surf A      | 160        | 0          | 92.04   |
| F20          | Sull A      | 109        | 0          | 92.00   |
| P26          | Surf A      | J69        | 9          | 92.39   |
| P20          | Sull A      | 109        | 9          | 92.87   |
| P26          | Suff A      | 109<br>J69 | 9          | 94.95   |
| P26          | Suff A      | 109<br>J69 | 9          | 93.23   |
| P26          | Surf A      | J69        | 9          | 93.23   |
| P26          | Surf A      | J69        | 10         | 93.91   |
| P26          | Surf A      | J69        | 10         | 91.95   |
| P26          | Surf A      | J69        | 10         | 93.07   |
| P26          | Surf A      | J69        | 10         | 92.27   |
| P26          | Surf A      | J69        | 10         | 95.11   |
| P26          | Surf A      | J69        | 11         | 92.40   |
| P26          | Surf A      | J69        | 11         | 91.84   |
| P26          | Surf A      | J69        | 11         | 93.64   |
| P26          | Surf A      | J69        | 11         | 92.64   |
| P26          | Surf A      | J69        | 11         | 93.40   |
| P26          | Surf A      | J69        | 12         | 92.29   |
| P26          | Surf A      | J69        | 12         | 91.25   |
| P26          | Surf A      | J69        | 12         | 92.57   |
| P26          | Surf A      | J69        | 12         | 91.49   |
| P26          | Surf A      | J69        | 12         | 94.13   |
| P26          | Surf A      | J69        | 12         | 92.53   |
| P26          | Surf A      | J69        | 13         | 93.92   |
| P26          | Surf A      | J69        | 13         | 93.12   |
| P26          | Surf A      | J69        | 13         | 93.28   |
| P26          | Surf A      | J69        | 13         | 95.28   |
| P26          | Surf A      | J69        | 13         | 93.68   |

P26

P26

P26

P26

P26

P26

Surf A

Surf A

Surf A

Surf A

Surf A

Surf A

J69

J69

J69

J69

J69

J69

2

3

3

3

3

4

93.54

91.04

94.68

91.00

94.56

93.36

| Table A.1. | Density | <b>Test Results</b> | Data | (continued) |
|------------|---------|---------------------|------|-------------|
|------------|---------|---------------------|------|-------------|

| Proj.<br>No. | Mix<br>Type | JMF<br>No. | Lot<br>No. | Density |
|--------------|-------------|------------|------------|---------|
| P26          | Surf A      | J69        | 13         | 93.48   |
| P26          | Surf A      | J69        | 14         | 93.95   |
| P26          | Surf A      | J69        | 14         | 95.07   |
| P26          | Surf A      | J69        | 14         | 94.71   |
| P26          | Surf A      | J69        | 14         | 95.15   |
| P26          | Surf A      | J69        | 14         | 93.63   |
| P26          | Surf A      | J69        | 14         | 93.79   |
| P26          | Surf A      | J69        | 15         | 92.63   |
| P26          | Surf A      | J69        | 15         | 91.46   |
| P26          | Surf A      | J69        | 15         | 92.10   |
| P26          | Surf A      | J69        | 15         | 95.69   |
| P26          | Surf A      | J69        | 15         | 93.35   |
| P26          | Surf A      | J69        | 16         | 94.11   |
| P26          | Surf A      | J69        | 16         | 93.67   |
| P26          | Surf A      | J69        | 16         | 92.83   |
| P26          | Surf C      | J59        | 2          | 90.30   |
| P26          | Surf C      | J59        | 2          | 92.94   |
| P26          | Surf C      | J59        | 2          | 91.62   |
| P26          | Surf C      | J59        | 2          | 91.14   |
| P26          | Surf C      | J59        | 2          | 91.62   |
| P26          | Surf C      | J59        | 2          | 92.50   |
| P26          | Surf C      | J59        | 3          | 92.01   |
| P26          | Surf C      | J59        | 3          | 93.60   |
| P26          | Surf C      | J59        | 3          | 91.22   |
| P26          | Surf C      | J59        | 3          | 92.65   |
| P26          | Surf C      | J59        | 3          | 90.39   |
| P26          | Surf C      | J59        | 3          | 92.09   |
| P26          | Surf C      | J59        | 3          | 92.25   |
| P26          | Surf C      | J59        | 3          | 92.53   |
| P26          | Surf C      | J59        | 4          | 90.82   |
| P26          | Surf C      | J59        | 4          | 91.38   |
| P26          | Surf C      | J59        | 4          | 92.53   |
| P26          | Surf C      | J59        | 4          | 88.68   |
| P26          | Surf C      | J59        | 4          | 89.31   |
| P26          | Surf C      | J59        | 4          | 89.47   |
| P26          | Surf C      | J59        | 4          | 90.62   |
| P26          | Surf C      | J59        | 5          | 89.96   |
| P26          | Surf C      | J59        | 5          | 91.31   |
| P26          | Surf C      | J59        | 5          | 91.07   |
| P26          | Surf C      | J59        | 5          | 91.19   |
| P26          | Surf C      | J59        | 5          | 89.96   |
| P26          | Surf C      | J59        | 5          | 89.08   |
| P26          | Surf C      | J59        | 5          | 90.95   |
| P26          | Surf C      | J59        | 5          | 92.89   |
| P26          | Surf C      | J59        | 5          | 88.29   |
| P26          | Surf C      | J59        | 5          | 91.19   |
| P26          | Surf C      | J59        | 5          | 90.55   |
| P26          | Surf C      | J59        | 6          | 91.72   |
| P26          | Surf C      | J59        | 6          | 90.01   |
| P26          | Surf C      | J59        | 6          | 91.52   |

| P26         Surf C         J59         6         90.61           P26         Surf C         J59         6         91.80           P26         Surf C         J59         7         90.24           P26         Surf C         J59         7         90.24           P26         Surf C         J59         7         91.19           P26         Surf C         J59         7         90.24           P26         Surf C         J59         7         90.24           P26         Surf C         J59         7         90.24           P26         Surf C         J59         7         90.79           P26         Surf C         J59         7         90.36           P26         Surf C         J59         8         89.59           P26         Surf C         J59         8         92.16           P26         Surf C         J59         8         90.02           P26         Surf C         J59         8         91.84           P26         Surf C         J59         8         91.84           P26         Surf C         J59         9         91.914 | Proj.<br>No. | Mix<br>Type | JMF<br>No. | Lot<br>No. | Density |
|--|--------------|-------------|------------|------------|---------|
| P26         Surf C         J59         6         91.80           P26         Surf C         J59         6         91.29           P26         Surf C         J59         7         90.24           P26         Surf C         J59         7         91.19           P26         Surf C         J59         7         91.79           P26         Surf C         J59         7         90.36           P26         Surf C         J59         7         90.36           P26         Surf C         J59         8         89.59           P26         Surf C         J59         8         89.59           P26         Surf C         J59         8         89.59           P26         Surf C         J59         8         89.212           P26         Surf C         J59         8         92.16           P26         Surf C         J59         8         90.02           P26         Surf C         J59         8         90.33           P26         Surf C         J59         9         91.34           P27         Surf B         J55         1         92.78 | P26          | Surf C      | J59        | 6          | 90.61   |
| P26         Surf C         J59         6         91.29           P26         Surf C         J59         7         90.24           P26         Surf C         J59         7         91.19           P26         Surf C         J59         7         92.06           P26         Surf C         J59         7         90.12           P26         Surf C         J59         7         90.36           P26         Surf C         J59         7         90.36           P26         Surf C         J59         8         89.59           P26         Surf C         J59         8         89.59           P26         Surf C         J59         8         89.59           P26         Surf C         J59         8         87.73           P26         Surf C         J59         8         87.73           P26         Surf C         J59         8         88.32           P26         Surf C         J59         8         90.02           P26         Surf C         J59         8         91.83           P27         Surf B         J55         1         92.09  | P26          | Surf C      | J59        | 6          | 91.80   |
| P26         Surf C         J59         7         90.24           P26         Surf C         J59         7         91.19           P26         Surf C         J59         7         92.06           P26         Surf C         J59         7         90.12           P26         Surf C         J59         7         90.36           P26         Surf C         J59         7         90.36           P26         Surf C         J59         8         89.59           P26         Surf C         J59         8         89.59           P26         Surf C         J59         8         89.73           P26         Surf C         J59         8         87.73           P26         Surf C         J59         8         87.73           P26         Surf C         J59         8         88.68           P26         Surf C         J59         8         90.02           P26         Surf C         J59         8         91.84           P26         Surf C         J59         8         91.33           P27         Surf B         J55         1         92.69  | P26          | Surf C      | J59        | 6          | 91.29   |
| P26         Surf C         J59         7         91.19           P26         Surf C         J59         7         92.06           P26         Surf C         J59         7         91.79           P26         Surf C         J59         7         90.12           P26         Surf C         J59         7         90.36           P26         Surf C         J59         8         89.59           P26         Surf C         J59         8         90.02           P26         Surf C         J59         8         91.88           P26         Surf C         J59         9         91.33           P27         Surf B         J55         1         92.09  | P26          | Surf C      | J59        | 7          | 90.24   |
| P26         Surf C         J59         7         92.06           P26         Surf C         J59         7         91.79           P26         Surf C         J59         7         90.12           P26         Surf C         J59         7         90.36           P26         Surf C         J59         8         89.59           P26         Surf C         J59         8         89.51           P26         Surf C         J59         8         90.02           P26         Surf C         J59         8         90.26           P26         Surf C         J59         8         91.84           P26         Surf C         J59         9         91.33           P26         Surf C         J59         9         91.94           P27         Surf B         J55         1         92.58           P27         Surf B         J55         1         92.54  | P26          | Surf C      | J59        | 7          | 91.19   |
| P26         Surf C         J59         7         91.79           P26         Surf C         J59         7         90.12           P26         Surf C         J59         7         90.36           P26         Surf C         J59         8         89.59           P26         Surf C         J59         8         89.59           P26         Surf C         J59         8         89.73           P26         Surf C         J59         8         87.73           P26         Surf C         J59         8         88.68           P26         Surf C         J59         8         90.02           P26         Surf C         J59         8         91.88           P26         Surf C         J59         9         91.33           P27         Surf B         J55         1         92.09           P27         Surf B         J55         1         92.58  | P26          | Surf C      | J59        | 7          | 92.06   |
| P26         Surf C         J59         7         90.12           P26         Surf C         J59         7         91.87           P26         Surf C         J59         7         90.36           P26         Surf C         J59         8         89.59           P26         Surf C         J59         8         89.12           P26         Surf C         J59         8         87.73           P26         Surf C         J59         8         88.68           P26         Surf C         J59         8         90.02           P26         Surf C         J59         8         91.88           P26         Surf C         J59         9         91.33           P27         Surf B         J55         1         92.09           P27         Surf B         J55         1         92.58           P27         Surf B         J55         1         92.54  | P26          | Surf C      | J59        | 7          | 91.79   |
| P26         Surf C         J59         7         91.87           P26         Surf C         J59         7         90.36           P26         Surf C         J59         8         89.59           P26         Surf C         J59         8         92.12           P26         Surf C         J59         8         87.73           P26         Surf C         J59         8         88.68           P26         Surf C         J59         8         90.02           P26         Surf C         J59         8         90.02           P26         Surf C         J59         8         90.02           P26         Surf C         J59         8         91.83           P26         Surf C         J59         9         91.33           P26         Surf C         J59         9         91.34           P27         Surf B         J55         1         92.78           P27         Surf B         J55         1         92.68           P27         Surf B         J55         3         91.33           P27         Surf B         J55         3         91.33  | P26          | Surf C      | J59        | 7          | 90.12   |
| P26         Surf C         J59         7         90.36           P26         Surf C         J59         8         89.59           P26         Surf C         J59         8         92.12           P26         Surf C         J59         8         87.73           P26         Surf C         J59         8         88.68           P26         Surf C         J59         8         90.02           P26         Surf C         J59         9         91.33           P26         Surf C         J59         9         91.34           P27         Surf B         J55         1         92.68           P27         Surf B         J55         1         92.69           P27         Surf B         J55         1         92.64           P27         Surf B         J55         3         91.33           P27         Surf B         J55         3         91.33  | P26          | Surf C      | J59        | 7          | 91.87   |
| P26         Surf C         J59         8         89.59           P26         Surf C         J59         8         92.12           P26         Surf C         J59         8         87.73           P26         Surf C         J59         8         88.68           P26         Surf C         J59         8         90.02           P26         Surf C         J59         8         90.02           P26         Surf C         J59         8         92.16           P26         Surf C         J59         8         91.88           P26         Surf C         J59         9         93.33           P26         Surf C         J59         9         91.94           P27         Surf B         J55         1         92.78           P27         Surf B         J55         1         92.09           P27         Surf B         J55         1         92.58           P27         Surf B         J55         1         92.54           P27         Surf B         J55         3         91.33           P27         Surf B         J55         3         91.33  | P26          | Surf C      | J59        | 7          | 90.36   |
| P26         Surf C         J59         8         92.12           P26         Surf C         J59         8         87.73           P26         Surf C         J59         8         88.68           P26         Surf C         J59         8         90.02           P26         Surf C         J59         8         90.02           P26         Surf C         J59         8         92.16           P26         Surf C         J59         8         91.88           P26         Surf C         J59         9         93.33           P26         Surf C         J59         9         91.94           P27         Surf B         J55         1         92.78           P27         Surf B         J55         1         92.09           P27         Surf B         J55         1         92.58           P27         Surf B         J55         1         92.54           P27         Surf B         J55         3         91.33           P27         Surf B         J55         3         91.37           P27         Surf B         J55         3         91.33  | P26          | Surf C      | J59        | 8          | 89.59   |
| P26         Surf C         J59         8         87.73           P26         Surf C         J59         8         88.68           P26         Surf C         J59         8         90.02           P26         Surf C         J59         8         90.02           P26         Surf C         J59         8         92.16           P26         Surf C         J59         8         91.88           P26         Surf C         J59         9         93.33           P26         Surf C         J59         9         91.94           P27         Surf B         J55         1         92.78           P27         Surf B         J55         1         92.69           P27         Surf B         J55         1         92.68           P27         Surf B         J55         1         92.54           P27         Surf B         J55         1         92.54           P27         Surf B         J55         3         91.33           P27         Surf B         J55         3         91.33           P27         Surf B         J55         3         91.33  | P26          | Surf C      | J59        | 8          | 92.12   |
| P26         Surf C         J59         8         88.68           P26         Surf C         J59         8         90.02           P26         Surf C         J59         8         92.16           P26         Surf C         J59         8         92.16           P26         Surf C         J59         8         91.88           P26         Surf C         J59         9         93.33           P26         Surf C         J59         9         93.33           P26         Surf C         J59         9         91.94           P27         Surf B         J55         1         92.78           P27         Surf B         J55         1         92.68           P27         Surf B         J55         1         92.58           P27         Surf B         J55         1         92.54           P27         Surf B         J55         1         92.54           P27         Surf B         J55         3         91.33           P27         Surf B         J55         3         91.33           P27         Surf B         J55         3         91.37  | P26          | Surf C      | J59        | 8          | 87.73   |
| P26         Surf C         J59         8         90.02           P26         Surf C         J59         8         88.32           P26         Surf C         J59         8         92.16           P26         Surf C         J59         8         91.88           P26         Surf C         J59         9         93.33           P26         Surf C         J59         9         91.94           P27         Surf B         J55         1         92.78           P27         Surf B         J55         1         92.09           P27         Surf B         J55         1         92.58           P27         Surf B         J55         1         92.54           P27         Surf B         J55         3         91.33           P27         Surf B         J55         3         91.71  | P26          | Surf C      | J59        | 8          | 88.68   |
| P26         Surf C         J59         8         88.32           P26         Surf C         J59         8         92.16           P26         Surf C         J59         8         91.88           P26         Surf C         J59         9         93.33           P26         Surf C         J59         9         91.94           P27         Surf B         J55         1         92.09           P27         Surf B         J55         1         92.09           P27         Surf B         J55         1         92.68           P27         Surf B         J55         1         92.58           P27         Surf B         J55         1         92.54           P27         Surf B         J55         3         91.33           P27         Surf B         J55         3         91.33           P27         Surf B         J55         3         91.33           P27         Surf B         J55         3         91.37           P27         Surf B         J55         3         91.37           P27         Surf B         J55         4         92.79  | P26          | Surf C      | J59        | 8          | 90.02   |
| P26         Surf C         J59         8         92.16           P26         Surf C         J59         8         91.88           P26         Surf C         J59         9         93.33           P26         Surf C         J59         9         91.94           P27         Surf B         J55         1         92.78           P27         Surf B         J55         1         92.09           P27         Surf B         J55         1         92.58           P27         Surf B         J55         1         92.58           P27         Surf B         J55         1         92.54           P27         Surf B         J55         3         91.33           P27         Surf B         J55         3         91.37           P27         Surf B         J55         3         91.37           P27         Surf B         J55         4         92.79  | P26          | Surf C      | J59        | 8          | 88.32   |
| P26         Surf C         J59         8         91.88           P26         Surf C         J59         9         93.33           P26         Surf C         J59         9         91.94           P27         Surf B         J55         1         92.78           P27         Surf B         J55         1         92.09           P27         Surf B         J55         1         92.58           P27         Surf B         J55         1         92.54           P27         Surf B         J55         3         91.33           P27         Surf B         J55         3         91.37           P27         Surf B         J55         3         91.37           P27         Surf B         J55         4         92.79           P27         Surf B         J55         4         92.26  | P26          | Surf C      | J59        | 8          | 92.16   |
| P26         Surf C         J59         9         93.33           P26         Surf C         J59         9         91.94           P27         Surf B         J55         1         92.78           P27         Surf B         J55         1         92.09           P27         Surf B         J55         1         92.09           P27         Surf B         J55         1         92.58           P27         Surf B         J55         1         92.54           P27         Surf B         J55         3         91.33           P27         Surf B         J55         3         91.37           P27         Surf B         J55         3         91.37           P27         Surf B         J55         4         92.79           P27         Surf B         J55         4         92.66  | P26          | Surf C      | J59        | 8          | 91.88   |
| P26         Surf C         J59         9         91.94           P27         Surf B         J55         1         92.78           P27         Surf B         J55         1         92.09           P27         Surf B         J55         1         92.58           P27         Surf B         J55         1         93.58           P27         Surf B         J55         1         92.54           P27         Surf B         J55         3         91.33           P27         Surf B         J55         3         92.41           P27         Surf B         J55         3         93.34           P27         Surf B         J55         3         91.37           P27         Surf B         J55         4         92.79           P27         Surf B         J55         4         92.26           P27         Surf B         J55         4         92.61  | P26          | Surf C      | J59        | 9          | 93.33   |
| P27         Surf B         J55         1         92.78           P27         Surf B         J55         1         92.09           P27         Surf B         J55         1         92.58           P27         Surf B         J55         1         93.58           P27         Surf B         J55         1         93.58           P27         Surf B         J55         1         92.54           P27         Surf B         J55         3         91.33           P27         Surf B         J55         3         93.34           P27         Surf B         J55         3         91.37           P27         Surf B         J55         3         91.37           P27         Surf B         J55         3         91.37           P27         Surf B         J55         4         92.79           P27         Surf B         J55         4         92.79           P27         Surf B         J55         4         92.26           P27         Surf B         J55         4         92.26           P27         Surf B         J55         4         92.87  | P26          | Surf C      | J59        | 9          | 91.94   |
| P27         Surf B         J55         1         92.09           P27         Surf B         J55         1         92.58           P27         Surf B         J55         1         93.58           P27         Surf B         J55         1         92.54           P27         Surf B         J55         3         91.33           P27         Surf B         J55         3         92.41           P27         Surf B         J55         3         93.34           P27         Surf B         J55         3         91.37           P27         Surf B         J55         4         92.79           P27         Surf B         J55         4         92.26           P27         Surf B         J55         4         92.26           P27         Surf B         J55         4         92.87           P27         Surf B         J55         4         92.87  | P27          | Surf B      | J55        | 1          | 92.78   |
| P27         Surf B         J55         1         92.58           P27         Surf B         J55         1         93.58           P27         Surf B         J55         1         92.54           P27         Surf B         J55         3         91.33           P27         Surf B         J55         3         92.41           P27         Surf B         J55         3         93.34           P27         Surf B         J55         3         91.37           P27         Surf B         J55         4         92.79           P27         Surf B         J55         4         92.26           P27         Surf B         J55         4         92.26           P27         Surf B         J55         4         92.26           P27         Surf B         J55         4         92.87           P27         Surf B         J55         4         92.87  | P27          | Surf B      | J55        | 1          | 92.09   |
| P27         Surf B         J55         1         93.58           P27         Surf B         J55         1         92.54           P27         Surf B         J55         3         91.33           P27         Surf B         J55         3         92.41           P27         Surf B         J55         3         93.34           P27         Surf B         J55         3         91.37           P27         Surf B         J55         4         92.79           P27         Surf B         J55         4         92.26           P27         Surf B         J55         4         92.26           P27         Surf B         J55         4         92.26           P27         Surf B         J55         4         92.87           P27         Surf B         J55         4         92.81           P27         Surf B         J55         5         91.95  | P27          | Surf B      | J55        | 1          | 92.58   |
| P27         Surf B         J55         1         92.54           P27         Surf B         J55         3         91.33           P27         Surf B         J55         3         92.41           P27         Surf B         J55         3         93.34           P27         Surf B         J55         3         93.34           P27         Surf B         J55         3         91.37           P27         Surf B         J55         3         91.37           P27         Surf B         J55         3         91.37           P27         Surf B         J55         4         92.79           P27         Surf B         J55         4         92.79           P27         Surf B         J55         4         92.66           P27         Surf B         J55         4         92.26           P27         Surf B         J55         4         92.26           P27         Surf B         J55         4         92.81           P27         Surf B         J55         4         92.51           P27         Surf B         J55         5         91.95  | P27          | Surf B      | J55        | 1          | 93.58   |
| P27         Surf B         J55         3         91.33           P27         Surf B         J55         3         92.41           P27         Surf B         J55         3         93.34           P27         Surf B         J55         3         93.34           P27         Surf B         J55         3         91.17           P27         Surf B         J55         3         91.37           P27         Surf B         J55         3         91.37           P27         Surf B         J55         4         92.79           P27         Surf B         J55         4         92.79           P27         Surf B         J55         4         92.26           P27         Surf B         J55         4         92.61           P27         Surf B         J55         4         92.81           P27         Surf B         J55         5         92.98  | P27          | Surf B      | J55        | 1          | 92.54   |
| P27         Surf B         J55         3         92.41           P27         Surf B         J55         3         93.34           P27         Surf B         J55         3         91.37           P27         Surf B         J55         4         92.79           P27         Surf B         J55         4         92.79           P27         Surf B         J55         4         92.79           P27         Surf B         J55         4         92.26           P27         Surf B         J55         4         92.26           P27         Surf B         J55         4         92.66           P27         Surf B         J55         4         92.06           P27         Surf B         J55         4         92.87           P27         Surf B         J55         5         92.98           P27         Surf B         J55         5         92.30  | P27          | Surf B      | J55        | 3          | 91.33   |
| P27         Surf B         J55         3         93.34           P27         Surf B         J55         3         91.17           P27         Surf B         J55         3         91.37           P27         Surf B         J55         3         91.37           P27         Surf B         J55         3         91.37           P27         Surf B         J55         4         92.79           P27         Surf B         J55         4         92.79           P27         Surf B         J55         4         92.26           P27         Surf B         J55         4         92.06           P27         Surf B         J55         4         92.87           P27         Surf B         J55         5         92.98           P27         Surf B         J55         5         92.30  | P27          | Surf B      | J55        | 3          | 92.41   |
| P27         Surf B         J55         3         91.17           P27         Surf B         J55         3         91.37           P27         Surf B         J55         3         91.37           P27         Surf B         J55         3         91.37           P27         Surf B         J55         4         92.79           P27         Surf B         J55         4         92.79           P27         Surf B         J55         4         92.26           P27         Surf B         J55         4         92.66           P27         Surf B         J55         4         92.87           P27         Surf B         J55         5         92.81           P27         Surf B         J55         5         91.67           P27         Surf B         J55         5         92.30  | P27          | Surf B      | J55        | 3          | 93.34   |
| P27         Surf B         J55         3         91.37           P27         Surf B         J55         3         91.37           P27         Surf B         J55         4         92.79           P27         Surf B         J55         4         92.79           P27         Surf B         J55         4         92.26           P27         Surf B         J55         4         92.06           P27         Surf B         J55         4         92.87           P27         Surf B         J55         5         92.98           P27         Surf B         J55         5         91.67           P27         Surf B         J55         5         92.30           P27         Surf B         J55         5         92.30  | P27          | Surf B      | J55        | 3          | 91.17   |
| P27         Surf B         J55         3         91.37           P27         Surf B         J55         4         92.79           P27         Surf B         J55         4         92.79           P27         Surf B         J55         4         92.26           P27         Surf B         J55         4         91.78           P27         Surf B         J55         4         92.26           P27         Surf B         J55         4         92.26           P27         Surf B         J55         4         92.06           P27         Surf B         J55         4         92.06           P27         Surf B         J55         4         92.87           P27         Surf B         J55         4         93.23           P27         Surf B         J55         5         92.98           P27         Surf B         J55         5         91.95           P27         Surf B         J55         5         91.67           P27         Surf B         J55         5         92.30           P27         Surf B         J55         5         92.30  | P27          | Surf B      | J55        | 3          | 91.37   |
| P27         Surf B         J55         4         92.79           P27         Surf B         J55         4         92.26           P27         Surf B         J55         4         92.26           P27         Surf B         J55         4         91.78           P27         Surf B         J55         4         92.06           P27         Surf B         J55         4         92.06           P27         Surf B         J55         4         92.87           P27         Surf B         J55         4         92.87           P27         Surf B         J55         4         92.81           P27         Surf B         J55         4         92.51           P27         Surf B         J55         5         92.98           P27         Surf B         J55         5         91.95           P27         Surf B         J55         5         91.67           P27         Surf B         J55         5         92.30           P27         Surf B         J55         5         92.30           P27         Surf B         J70         1         90.89  | P27          | Surf B      | J55        | 3          | 91.37   |
| P27         Surf B         J55         4         92.26           P27         Surf B         J55         4         91.78           P27         Surf B         J55         4         92.06           P27         Surf B         J55         4         92.06           P27         Surf B         J55         4         92.87           P27         Surf B         J55         4         92.87           P27         Surf B         J55         4         92.87           P27         Surf B         J55         4         92.51           P27         Surf B         J55         5         92.98           P27         Surf B         J55         5         91.95           P27         Surf B         J55         5         91.67           P27         Surf B         J55         5         92.30           P27         Surf B         J55         5         92.30           P27         Surf B         J55         5         91.71           P27         Surf B         J70         1         90.89           P27         Surf B         J70         1         93.45  | P27          | Surf B      | J55        | 4          | 92.79   |
| P27         Surf B         J55         4         91.78           P27         Surf B         J55         4         92.06           P27         Surf B         J55         4         92.06           P27         Surf B         J55         4         92.87           P27         Surf B         J55         4         93.23           P27         Surf B         J55         4         92.51           P27         Surf B         J55         5         92.98           P27         Surf B         J55         5         92.98           P27         Surf B         J55         5         91.95           P27         Surf B         J55         5         91.67           P27         Surf B         J55         5         92.30           P27         Surf B         J55         5         92.30           P27         Surf B         J55         5         92.30           P27         Surf B         J55         5         91.71           P27         Surf B         J70         1         93.45           P27         Surf B         J70         1         94.76  | P27          | Surf B      | J55        | 4          | 92.26   |
| P27         Surf B         J55         4         92.06           P27         Surf B         J55         4         92.87           P27         Surf B         J55         4         93.23           P27         Surf B         J55         4         93.23           P27         Surf B         J55         4         92.51           P27         Surf B         J55         5         92.98           P27         Surf B         J55         5         91.95           P27         Surf B         J55         5         91.95           P27         Surf B         J55         5         91.95           P27         Surf B         J55         5         92.30           P27         Surf B         J55         5         92.30           P27         Surf B         J55         5         92.30           P27         Surf B         J70         1         90.89           P27         Surf B         J70         1         93.45           P27         Surf B         J70         1         94.76           P27         Surf B         J70         1         94.20  | P27          | Surf B      | J55        | 4          | 91.78   |
| P27         Surf B         J55         4         92.87           P27         Surf B         J55         4         93.23           P27         Surf B         J55         4         93.23           P27         Surf B         J55         4         92.51           P27         Surf B         J55         5         92.98           P27         Surf B         J55         5         91.95           P27         Surf B         J55         5         91.95           P27         Surf B         J55         5         91.67           P27         Surf B         J55         5         92.30           P27         Surf B         J70         1         90.89           P27         Surf B         J70         1         93.45           P27         Surf B         J70         1         94.76           P27         Surf B         J70         1         94.20  | P27          | Surf B      | J55        | 4          | 92.06   |
| P27         Surf B         J55         4         93.23           P27         Surf B         J55         4         92.51           P27         Surf B         J55         5         92.98           P27         Surf B         J55         5         91.95           P27         Surf B         J55         5         91.95           P27         Surf B         J55         5         91.67           P27         Surf B         J55         5         92.30           P27         Surf B         J70         1         90.89           P27         Surf B         J70         1         93.45           P27         Surf B         J70         1         94.76           P27         Surf B         J70         1         94.20           P27         Surf B         J70         1         92.81  | P27          | Surf B      | J55        | 4          | 92.87   |
| P27         Surf B         J55         4         92.51           P27         Surf B         J55         5         92.98           P27         Surf B         J55         5         91.95           P27         Surf B         J55         5         91.95           P27         Surf B         J55         5         91.67           P27         Surf B         J55         5         92.30           P27         Surf B         J70         1         90.89           P27         Surf B         J70         1         93.45           P27         Surf B         J70         1         94.76           P27         Surf B         J70         1         94.20           P27         Surf B         J70         1         92.81           P27         Surf B         J70         1         92.81           P27         Surf B         J70         2         94.80  | P27          | Surf B      | J55        | 4          | 93.23   |
| P27         Surf B         J55         5         92.98           P27         Surf B         J55         5         91.95           P27         Surf B         J55         5         91.95           P27         Surf B         J55         5         91.67           P27         Surf B         J55         5         92.30           P27         Surf B         J70         1         90.89           P27         Surf B         J70         1         93.45           P27         Surf B         J70         1         94.76           P27         Surf B         J70         1         94.20           P27         Surf B         J70         1         92.81           P27         Surf B         J70         1         92.81           P27         Surf B         J70         2         94.80  | P27          | Surf B      | J55        | 4          | 92.51   |
| P27         Surf B         J55         5         91.95           P27         Surf B         J55         5         91.67           P27         Surf B         J55         5         92.30           P27         Surf B         J55         5         91.71           P27         Surf B         J70         1         90.89           P27         Surf B         J70         1         93.45           P27         Surf B         J70         1         94.76           P27         Surf B         J70         1         94.20           P27         Surf B         J70         1         92.81           P27         Surf B         J70         2         94.80   | P27          | Surf B      | J55        | 5          | 92.98   |
| P27         Surf B         J55         5         91.67           P27         Surf B         J55         5         92.30           P27         Surf B         J55         5         91.71           P27         Surf B         J70         1         90.89           P27         Surf B         J70         1         93.45           P27         Surf B         J70         1         94.76           P27         Surf B         J70         1         94.20           P27         Surf B         J70         1         92.81           P27         Surf B         J70         1         92.81           P27         Surf B         J70         2         94.80   | P27          | Surf B      | J55        | 5          | 91.95   |
| P27         Surf B         J55         5         92.30           P27         Surf B         J55         5         92.30           P27         Surf B         J55         5         92.30           P27         Surf B         J55         5         91.71           P27         Surf B         J70         1         90.89           P27         Surf B         J70         1         93.45           P27         Surf B         J70         1         94.76           P27         Surf B         J70         1         94.20           P27         Surf B         J70         1         92.81           P27         Surf B         J70         1         92.81           P27         Surf B         J70         2         94.80   | P27          | Surf B      | J55        | 5          | 91.67   |
| P27         Surf B         J55         5         92.30           P27         Surf B         J55         5         91.71           P27         Surf B         J70         1         90.89           P27         Surf B         J70         1         93.45           P27         Surf B         J70         1         94.76           P27         Surf B         J70         1         94.20           P27         Surf B         J70         1         92.81           P27         Surf B         J70         1         92.81           P27         Surf B         J70         2         94.80   | P27          | Surf B      | J55        | 5          | 92.30   |
| P27         Surf B         J55         5         91.71           P27         Surf B         J70         1         90.89           P27         Surf B         J70         1         93.45           P27         Surf B         J70         1         94.76           P27         Surf B         J70         1         94.20           P27         Surf B         J70         1         94.20           P27         Surf B         J70         1         92.81           P27         Surf B         J70         2         94.80  | P27          | Surf B      | J55        | 5          | 92.30   |
| P27         Surf B         J70         1         90.89           P27         Surf B         J70         1         93.45           P27         Surf B         J70         1         94.76           P27         Surf B         J70         1         94.76           P27         Surf B         J70         1         94.20           P27         Surf B         J70         1         92.81           P27         Surf B         J70         2         94.80   | P27          | Surf B      | J55        | 5          | 91.71   |
| P27         Surf B         J70         1         93.45           P27         Surf B         J70         1         94.76           P27         Surf B         J70         1         94.20           P27         Surf B         J70         1         94.20           P27         Surf B         J70         1         92.81           P27         Surf B         J70         2         94.80  | P27          | Surf B      | J70        | 1          | 90.89   |
| P27         Surf B         J70         1         94.76           P27         Surf B         J70         1         94.20           P27         Surf B         J70         1         94.20           P27         Surf B         J70         1         92.81           P27         Surf B         J70         2         94.80   | P27          | Surf B      | J70        | 1          | 93.45   |
| P27         Surf B         J70         1         94.20           P27         Surf B         J70         1         92.81           P27         Surf B         J70         2         94.80   | P27          | Surf B      | J70        | 1          | 94.76   |
| P27         Surf B         J70         1         92.81           P27         Surf B         J70         2         94.80  | P27          | Surf B      | J70        | 1          | 94,20   |
| P27 Surf B J70 2 94.80   | P27          | Surf B      | J70        | 1          | 92,81   |
|  | P27          | Surf B      | J70        | 2          | 94.80   |

| Table A.1 | l. Densitv | <b>Test Results</b> | Data   | (continued) |
|-----------|------------|---------------------|--------|-------------|
|           |            | 100111004110        | - alla | (           |

| Proj.<br>No. | Mix<br>Type | JMF<br>No. | Lot<br>No. | Density |
|--------------|-------------|------------|------------|---------|
| P27          | Surf B      | J70        | 2          | 92.91   |
| P27          | Surf B      | J70        | 2          | 92.91   |
| P27          | Surf B      | J70        | 2          | 93.92   |
| P27          | Surf B      | J70        | 2          | 92.27   |
| P27          | Surf B      | J70        | 2          | 92.51   |
| P27          | Surf B      | J70        | 2          | 94.20   |
| P27          | Surf B      | J70        | 4          | 91.86   |
| P27          | Surf B      | J70        | 4          | 93.10   |
| P27          | Surf B      | J70        | 4          | 92.34   |
| P27          | Surf B      | J70        | 4          | 91.98   |
| P27          | Surf B      | J70        | 7          | 92.77   |
| P27          | Surf B      | J70        | 7          | 93.13   |
| P27          | Surf B      | J70        | 7          | 93.01   |
| P27          | Surf B      | J70        | 7          | 91.09   |
| P27          | Surf B      | J70        | 7          | 93.77   |
| P27          | Surf B      | J70        | 8          | 93.71   |
| P27          | Surf B      | J70        | 8          | 93.91   |
| P27          | Surf B      | J70        | 8          | 92.51   |
| P27          | Surf B      | J70        | 9          | 93.43   |
| P27          | Surf B      | J70        | 9          | 92.06   |
| P27          | Surf B      | J70        | 9          | 93.67   |
| P27          | Surf B      | J70        | 9          | 91.26   |
| P27          | Surf B      | J70        | 9          | 91.90   |
| P27          | Surf B      | J70        | 9          | 93.87   |
| P27          | Surf B      | J70        | 10         | 92.99   |
| P27          | Surf B      | J70        | 10         | 91.39   |
| P27          | Surf B      | J70        | 10         | 93.79   |
| P28          | Surf C      | J39        | 4          | 93.31   |
| P28          | Surf C      | J39        | 4          | 92.97   |
| P28          | Surf C      | J39        | 4          | 93.06   |
| P28          | Surf C      | J39        | 4          | 94.68   |
| P28          | Surf C      | J39        | 4          | 91.60   |
| P28          | Surf C      | J39        | 4          | 93.26   |
| P28          | Surf C      | J39        | 4          | 91.98   |
| P28          | Surf C      | J39        | 5          | 92.94   |
| P28          | Surf C      | J39        | 5          | 93.32   |
| P28          | Surf C      | J39        | 5          | 91.37   |
| P28          | Surf C      | J39        | 5          | 93.90   |
| P28          | Surf C      | J39        | 5          | 94.11   |
| P28          | Surf C      | J39        | 5          | 91.78   |
| P28          | Surf C      | J39        | 5          | 92.65   |
| P28          | Surf C      | J39        | 5          | 93.77   |
| P28          | Surf C      | J39        | 5          | 93.03   |
| P28          | Surf C      | J39        | 5          | 96.10   |
| P28          | Surf C      | J39        | 5          | 94.10   |
| P28          | Surf C      | J39        | 6          | 94.65   |
| P28          | Surf C      | J39        | 6          | 91.32   |
| P28          | Surf C      | J39        | 6          | 90.66   |
| P28          | Surf C      | J39        | 6          | 94.35   |
| P28          | Surf C      | J39        | 6          | 95.43   |

| Proj. | Mix      | JMF  | Lot    | Density |
|-------|----------|------|--------|---------|
| NO.   | Туре     | NO.  | NO.    | 00.45   |
| P28   | Surf C   | J39  | 6      | 92.15   |
| P28   | Surf C   | J39  | 6      | 94.35   |
| P28   | Surf C   | J39  | 8      | 94.18   |
| P28   | Surf C   | J39  | 8      | 93.14   |
| P28   | Surf C   | J39  | 8      | 93.14   |
| P30   | Surf B   | J65  | 1      | 98.82   |
| P30   | Surf B   | J65  | 1      | 91.45   |
| P30   | Surf B   | J65  | 1      | 91.09   |
| P30   | Surf B   | J65  | 1      | 92.60   |
| P30   | Surf B   | J65  | 1      | 93.90   |
| P30   | Surf B   | J65  | 2      | 94.60   |
| P30   | Surf B   | J65  | 2      | 93.45   |
| P30   | Surf B   | J65  | 2      | 94.01   |
| P31   | Surf B   | J71  | 1      | 94.28   |
| P31   | Surf B   | J71  | 1      | 94.04   |
| P31   | Surf B   | J71  | 1      | 94.40   |
| P31   | Surf B   | J71  | 1      | 93.72   |
| P31   | Surf B   | J71  | 1      | 93.84   |
| P31   | Surf B   | J71  | 2      | 93.45   |
| P31   | Surf B   | J71  | 2      | 94.17   |
| P31   | Surf B   | J71  | 2      | 95.09   |
| P32   | Interm B | J76  | 2      | 93.80   |
| P32   | Interm B | J76  | 2      | 93.52   |
| P32   | Interm B | J76  | 2      | 94.28   |
| P32   | Interm B | J76  | 2      | 94.00   |
| P32   | Interm B | J76  | 2      | 94.60   |
| P32   | Interm B | J76  | 2      | 93.60   |
| P32   | Interm B | J76  | 2      | 93.08   |
| P32   | Interm B | J76  | 2      | 95.20   |
| P32   | Interm B | J76  | 2      | 92.44   |
| P32   | Interm B | J76  | 3      | 94.14   |
| P32   | Interm B | .176 | 3      | 95.93   |
| P32   | Interm B | .176 | 3      | 94 54   |
| P32   | Interm B | .176 | 3      | 94.06   |
| P32   | Interm B | .176 | 3      | 92.43   |
| P32   | Interm B | .176 | 3      | 94 30   |
| P32   | Interm B | .176 | 4      | 92.56   |
| P32   | Interm B | 176  | 4      | 02.68   |
| P32   | Interm B | 176  | 4      | 03.52   |
| T 32  | Interm D | 176  | 4      | 02.60   |
| P32   | Interm B | 176  | 4      | 92.00   |
| D22   |          | 176  | -+     | 02.22   |
| F32   |          | 176  | 4      | 92.32   |
| F 32  |          | 176  | 4      | 93.04   |
| F 32  |          | 176  | 4      | 90.00   |
| F32   |          | J/0  | 4      | 92.92   |
| F32   |          | J/0  | 4      | 92.70   |
| P32   | Interm B | J/0  | 5      | 93.20   |
| P32   | Interm B | J/0  | о<br>Г | 91.76   |
| P32   | Interm B | J/6  | 5      | 94.32   |
| P32   | Interm B | J/6  | 5      | 92.88   |

| Proj.<br>No | Mix<br>Type | JMF<br>No | Lot<br>No. | Density |
|-------------|-------------|-----------|------------|---------|
| P32         | Interm B    | J76       | 5          | 92.80   |
| P32         | Interm B    | J76       | 5          | 92.56   |
| P32         | Interm B    | .176      | 5          | 92.92   |
| P32         | Interm B    | .176      | 5          | 92.68   |
| D22         | Interm B    | 176       | 5          | 04.72   |
| P32         | Interm B    | 176       | 5          | 94.73   |
| P22         | Interm B    | 176       | 6          | 02.07   |
| F 32        |             | J70       | 6          | 92.97   |
| F 32        |             | J70       | 6          | 92.10   |
| F 32        |             | J70       | 0          | 93.20   |
| P32         | Interm B    | J76       | 0          | 93.16   |
| P32         | Interm B    | J76       | 6          | 93.52   |
| P32         | Interm B    | J76       | 6          | 93.88   |
| P32         | Interm B    | J76       | 6          | 91.88   |
| P32         | Interm B    | J76       | 6          | 92.12   |
| P32         | Interm B    | J76       | 6          | 93.12   |
| P32         | Interm B    | J76       | 6          | 94.08   |
| P32         | Interm B    | J76       | 7          | 94.44   |
| P32         | Interm B    | J76       | 7          | 92.40   |
| P32         | Interm B    | J76       | 7          | 91.96   |
| P32         | Interm B    | J76       | 7          | 90.72   |
| P32         | Interm B    | J76       | 7          | 92.56   |
| P32         | Interm B    | J76       | 7          | 90.48   |
| P32         | Interm B    | J76       | 8          | 93.31   |
| P32         | Interm B    | J76       | 8          | 90.83   |
| P32         | Interm B    | J76       | 8          | 92.91   |
| P32         | Interm B    | J76       | 8          | 91.99   |
| P32         | Interm B    | J76       | 8          | 93.63   |
| P32         | Interm B    | J76       | 8          | 92.95   |
| P32         | Interm B    | J76       | 8          | 91.79   |
| P32         | Interm B    | J76       | 9          | 95.32   |
| P32         | Interm B    | J76       | 9          | 95.60   |
| P32         | Interm B    | J76       | 9          | 91.39   |
| P32         | Interm B    | J76       | 9          | 92.39   |
| P32         | Interm B    | J76       | 9          | 93.11   |
| P32         | Interm B    | J76       | 9          | 92 19   |
| P32         | Interm B    | .176      | 10         | 93.65   |
| P32         | Interm B    | 176       | 10         | 92.34   |
| P32         | Interm R    | 176       | 10         | 94.25   |
| P32         | Interm R    | 176       | 10         | 94.20   |
| D22         |             | 176       | 10         | 04.00   |
| F32         |             | J/0       | 10         | 94.17   |
| F32         |             | J/0       | 10         | 92.01   |
| P32         | Interm B    | J/6       | 10         | 91.58   |
| P32         | Interm B    | J76       | 10         | 93.25   |
| P32         | Interm B    | J76       | 10         | 93.49   |
| P32         | Interm B    | J76       | 11         | 93.92   |
| P32         | Interm B    | J76       | 11         | 93.92   |
| P32         | Interm B    | J76       | 11         | 93.80   |
| P32         | Interm B    | J76       | 11         | 93.96   |
| P32         | Interm B    | J76       | 11         | 93.60   |
| P32         | Interm B    | J76       | 11         | 93.68   |

| Proj. | Mix      | JMF  | Lot    | Density        |
|-------|----------|------|--------|----------------|
| D32   | Interm B | 176  | 11     | 03.56          |
| F 32  | Interm D | 176  | 11     | 93.50          |
| F 32  | Interm D | 176  | 11     | 91.04          |
| F32   |          | J70  | 10     | 94.32          |
| P32   | Interm D | J76  | 12     | 93.80          |
| P32   | Interm B | J/6  | 12     | 93.92          |
| P32   | Interm B | J/6  | 12     | 93.68          |
| P32   | Interm B | J/6  | 12     | 93.48          |
| P32   | Interm B | J76  | 12     | 92.96          |
| P32   | Interm B | J76  | 12     | 93.68          |
| P32   | Interm B | J76  | 12     | 95.36          |
| P32   | Interm B | J76  | 12     | 95.12          |
| P32   | Interm B | J76  | 12     | 92.48          |
| P32   | Interm B | J76  | 12     | 92.44          |
| P32   | Interm B | J76  | 13     | 93.76          |
| P32   | Interm B | J76  | 13     | 94.20          |
| P32   | Interm B | J76  | 13     | 94.32          |
| P32   | Interm B | J76  | 13     | 93.63          |
| P32   | Interm B | J76  | 13     | 92.47          |
| P32   | Interm B | J76  | 13     | 92.59          |
| P32   | Interm B | J76  | 13     | 92.71          |
| P32   | Interm B | J76  | 14     | 94.28          |
| P32   | Interm B | J76  | 14     | 92.56          |
| P32   | Interm B | J76  | 14     | 95.24          |
| P32   | Interm B | J76  | 14     | 91.36          |
| P32   | Interm B | J76  | 14     | 93.84          |
| P32   | Interm B | J76  | 14     | 94.08          |
| P32   | Surf A   | J74  | 1      | 93.95          |
| P32   | Surf A   | J74  | 1      | 94.67          |
| P32   | Surf A   | J74  | 1      | 94.31          |
| P32   | Surf A   | J74  | 1      | 92.83          |
| P32   | Surf A   | J74  | 1      | 92.31          |
| P32   | Surf A   | J74  | 1      | 91.15          |
| P32   | Surf A   | J79  | 2      | 92.34          |
| P32   | Surf A   | J79  | 2      | 93.02          |
| P32   | Surf A   | J79  | 2      | 92.22          |
| P32   | Surf A   | .179 | 2      | 92.26          |
| P32   | Surf A   | J79  | 2      | 92.78          |
| P32   | Surf A   | .179 | 2      | 92.90          |
| P32   | Surf A   | J79  | 2      | 93.38          |
| P32   | Surf A   | .179 | 2      | 93 50          |
| P32   | Surf A   | .179 | 2      | 92 90          |
| P32   | Surf A   | .179 | 2      | 94 99          |
| P32   |          | 170  | 2      | 02.33          |
| 1 32  |          | 170  | 2      | 02 ED          |
| F 32  | Sull A   | 170  | 2      | 92.00<br>02.50 |
| P22   |          | 170  | 3<br>2 | 92.52          |
| F32   | Sull A   | J/9  | 3      | 93.20          |
| P32   | Suff A   | J/9  | 3      | 92.27          |
| P32   | Surf A   | J/9  | 3      | 92.40          |
| P32   | Surf A   | J/9  | 3      | 93.32          |
| P32   | Surf A   | J79  | 3      | 94.20          |

| Table A.  | 1. Density | <b>Test Results</b> | Data | (continued) |
|-----------|------------|---------------------|------|-------------|
| 14810 / 4 |            | 100011000010        | Bata | (oonanaoa)  |

| Proj.<br>No. | Mix<br>Type | JMF<br>No. | Lot<br>No. | Density |
|--------------|-------------|------------|------------|---------|
| P32          | Surf A      | J79        | 4          | 92.64   |
| P32          | Surf A      | J79        | 4          | 92.12   |
| P32          | Surf A      | J79        | 4          | 94.52   |
| P32          | Surf A      | J79        | 4          | 93.32   |
| P32          | Surf A      | J79        | 4          | 92.32   |
| P32          | Surf A      | J79        | 4          | 92.32   |
| P32          | Surf A      | J79        | 4          | 92.92   |
| P32          | Surf A      | J79        | 4          | 95.12   |
| P32          | Surf A      | J79        | 4          | 93.36   |
| P32          | Surf A      | J79        | 4          | 91.12   |
| P32          | Surf A      | J79        | 5          | 92.99   |
| P32          | Surf A      | J79        | 5          | 92.87   |
| P32          | Surf A      | J79        | 5          | 91.59   |
| P32          | Surf A      | J79        | 5          | 93.75   |
| P32          | Surf A      | J79        | 6          | 92.52   |
| P32          | Surf A      | J79        | 6          | 93.08   |
| P32          | Surf A      | J79        | 6          | 92.08   |
| P32          | Surf A      | J79        | 6          | 94.32   |
| P32          | Surf A      | J79        | 6          | 92.48   |
| P32          | Surf A      | J79        | 6          | 93.24   |
| P32          | Surf A      | J79        | 6          | 93.00   |
| P32          | Surf A      | J79        | 6          | 92.24   |
| P32          | Surf A      | J79        | 6          | 91.88   |
| P32          | Surf A      | J79        | 6          | 92.92   |
| P32          | Surf A      | J79        | 7          | 92.73   |
| P32          | Surf A      | J79        | 7          | 93.53   |
| P32          | Surf A      | J79        | 7          | 93.25   |
| P32          | Surf A      | J79        | 7          | 93.09   |
| P32          | Surf A      | J79        | 8          | 92.88   |
| P32          | Surf A      | J79        | 8          | 93.24   |
| P32          | Surf A      | J79        | 8          | 93.64   |
| P32          | Surf A      | J79        | 8          | 92.72   |
| P32          | Surf A      | J79        | 8          | 92.08   |
| P32          | Surf A      | J79        | 8          | 93.64   |
| P32          | Surf A      | J79        | 8          | 93.20   |
| P32          | Surf A      | J79        | 8          | 92.80   |
| P32          | Surf A      | J79        | 9          | 93.11   |
| P32          | Surf A      | J79        | 9          | 92.67   |
| P32          | Surf A      | J79        | 9          | 93.39   |
| P32          | Surf A      | J79        | 9          | 92.87   |
| P32          | Surf A      | J79        | 10         | 93.28   |
| P32          | Surf A      | J79        | 10         | 92.80   |
| P32          | Surf A      | J79        | 10         | 94.08   |
| P32          | Surf A      | J79        | 10         | 93.64   |
| P32          | Surf A      | J79        | 10         | 93.08   |
| P32          | Surf A      | J79        | 10         | 92.76   |
| P32          | Surf A      | J79        | 10         | 92.68   |
| P32          | Surf A      | J79        | 10         | 88.20   |
| P32          | Surf A      | J79        | 10         | 92.24   |
| P32          | Surf A      | J79        | 11         | 92.87   |

| Proj.<br>No | Mix<br>Type | JMF<br>No | Lot | Density |
|-------------|-------------|-----------|-----|---------|
| P32         | Surf A      | .179      | 11  | 91.51   |
| P32         | Surf A      | .179      | 11  | 92.87   |
| P32         | Surf A      | .179      | 11  | 92.93   |
| P32         | Surf A      | 179       | 11  | 02.00   |
| P22         |             | 170       | 11  | 02.70   |
| P32         | Surf A      | 170       | 11  | 92.79   |
| F 32        | Surf A      | 170       | 11  | 93.07   |
| P32         | Sull A      | J79       | 11  | 93.71   |
| P32         | Sull A      | J79       | 11  | 93.15   |
| P32         | Suff A      | J79       | 12  | 93.00   |
| P32         | Suff A      | J79       | 12  | 91.84   |
| P32         | Surf A      | J79       | 12  | 92.68   |
| P32         | Surf A      | J79       | 12  | 92.88   |
| P32         | Surf A      | J79       | 12  | 93.12   |
| P32         | Surf A      | J79       | 12  | 92.60   |
| P32         | Surf A      | J79       | 12  | 93.04   |
| P32         | Surf A      | J79       | 12  | 92.20   |
| P32         | Surf A      | J79       | 12  | 93.28   |
| P32         | Surf A      | J79       | 12  | 93.48   |
| P32         | Surf A      | J79       | 12  | 92.40   |
| P32         | Surf A      | J79       | 13  | 92.97   |
| P32         | Surf A      | J79       | 13  | 92.18   |
| P32         | Surf A      | J79       | 13  | 94.49   |
| P32         | Surf A      | J79       | 13  | 93.09   |
| P32         | Surf A      | J79       | 13  | 92.61   |
| P32         | Surf A      | J79       | 14  | 90.77   |
| P32         | Surf A      | J79       | 14  | 90.77   |
| P32         | Surf A      | J79       | 14  | 90.81   |
| P32         | Surf A      | J79       | 14  | 92.12   |
| P32         | Surf A      | J79       | 14  | 91.84   |
| P32         | Surf A      | J79       | 15  | 92.57   |
| P32         | Surf A      | J79       | 15  | 92.73   |
| P32         | Surf A      | J79       | 15  | 90.17   |
| P32         | Surf A      | J79       | 15  | 93.41   |
| P32         | Surf A      | J79       | 15  | 92.13   |
| P32         | Surf A      | J79       | 15  | 92.21   |
| P32         | Surf A      | J79       | 15  | 92.77   |
| P32         | Surf A      | J79       | 15  | 93.81   |
| P32         | Surf A      | J79       | 15  | 91.93   |
| P32         | Surf A      | J79       | 15  | 92.81   |
| P32         | Surf A      | J79       | 16  | 90.62   |
| P32         | Surf A      | J79       | 16  | 93.65   |
| P32         | Surf A      | J79       | 16  | 91.65   |
| P32         | Surf A      | ,179      | 16  | 91,81   |
| P32         | Surf A      | J79       | 16  | 93 21   |
| P32         | Surf A      | .179      | 16  | 92 33   |
| P32         | Surf A      | .179      | 17  | 92.00   |
| P32         |             | 170       | 17  | 92.24   |
| P32         |             | 170       | 17  | Q1 56   |
| P32         |             | 170       | 17  | 02.02   |
| P32         | Surf A      | .179      | 17  | 92.92   |
|             |             |           |     | 02.00   |

| Table A.1. De | ensity Test Results | Data (continued) |
|---------------|---------------------|------------------|
|---------------|---------------------|------------------|

| Proj.<br>No. | Mix<br>Type | JMF<br>No. | Lot<br>No. | Density |
|--------------|-------------|------------|------------|---------|
| P32          | Surf A      | J79        | 17         | 90.92   |
| P32          | Surf A      | J79        | 17         | 93.24   |
| P32          | Surf A      | J79        | 17         | 93.68   |
| P32          | Surf A      | J79        | 18         | 92.98   |
| P32          | Surf A      | J79        | 18         | 91.94   |
| P32          | Surf A      | J79        | 18         | 93.02   |
| P32          | Surf A      | J79        | 18         | 92.22   |
| P32          | Surf A      | J79        | 18         | 92.34   |
| P32          | Surf A      | J79        | 19         | 92.97   |
| P32          | Surf A      | J79        | 19         | 94.41   |
| P32          | Surf A      | J79        | 19         | 93.45   |
| P32          | Surf A      | J79        | 19         | 93.13   |
| P32          | Surf A      | J79        | 20         | 93.80   |
| P32          | Surf A      | J79        | 20         | 94.12   |
| P32          | Surf A      | J79        | 20         | 90.91   |
| P32          | Surf A      | J79        | 20         | 93.96   |
| P32          | Surf A      | J79        | 20         | 94.00   |
| P32          | Surf A      | J79        | 20         | 92.91   |
| P32          | Surf A      | J79        | 20         | 93.15   |
| P32          | Surf A      | .179       | 21         | 92.57   |
| P32          | Surf A      | .179       | 21         | 92.97   |
| P32          | Surf A      | .179       | 21         | 92.01   |
| P32          | Surf A      | .179       | 21         | 92.09   |
| P32          | Surf A      | .179       | 21         | 92.69   |
| P32          | Surf A      | .179       | 22         | 93.06   |
| P32          | Surf A      | .179       | 22         | 92.98   |
| P32          | Surf A      | .179       | 22         | 92.91   |
| P32          | Surf A      | .179       | 22         | 92.07   |
| P32          | Surf A      | .179       | 22         | 92.42   |
| P32          | Surf A      | .179       | 22         | 93.34   |
| P32          | Surf A      | .179       | 22         | 93.98   |
| P32          | Surf A      | .179       | 23         | 94 44   |
| P32          | Surf A      | .179       | 23         | 92.80   |
| P32          | Surf A      | .179       | 23         | 94 16   |
| P32          | Surf A      | .179       | 23         | 93.36   |
| P32          | Surf A      | .179       | 23         | 93.36   |
| P32          | Surf A      | .179       | 23         | 92.56   |
| P32          | Surf A      | .179       | 23         | 91.32   |
| P32          | Surf A      | .179       | 23         | 91.56   |
| P32          | Surf A      | 179        | 20         | 92.76   |
| P32          | Surf A      | .179       | 24         | 91.48   |
| P32          | Surf A      | .179       | 24         | 90.00   |
| P32          | Surf A      | 179        | 24         | 01.88   |
| P32          |             | .179       | 24         | 92.96   |
| P32          |             | .179       | 24         | 93.20   |
| P32          |             | .179       | 25         | 91 79   |
| P32          | Surf A      | .179       | 25         | 94 /7   |
| P32          | Surf A      | .179       | 25         | 93.47   |
| P32          | Surf B      | .172       | 1          | 91.84   |
| P32          | Surf B      | .172       | 1          | 92.69   |
| 1 52         | Our D       | 072        | 1          | 52.05   |

| Proj.<br>No. | Mix<br>Type | JMF<br>No. | Lot<br>No. | Density |
|--------------|-------------|------------|------------|---------|
| P32          | Surf B      | J72        | 1          | 93.17   |
| P32          | Surf B      | J72        | 1          | 93.69   |
| P32          | Surf B      | J72        | 1          | 92.04   |
| P32          | Surf B      | J72        | 1          | 93.89   |
| P32          | Surf B      | J72        | 1          | 92.33   |
| P32          | Surf B      | J72        | 1          | 93.65   |
| P32          | Surf B      | J72        | 1          | 93.01   |
| P32          | Surf B      | J72        | 1          | 93.09   |
| P32          | Surf B      | J72        | 1          | 93.01   |
| P32          | Surf B      | J72        | 1          | 94.13   |
| P32          | Surf B      | J72        | 2          | 93.44   |
| P32          | Surf B      | J72        | 2          | 93.00   |
| P32          | Surf B      | J72        | 2          | 94.37   |
| P32          | Surf B      | J72        | 2          | 92.72   |
| P32          | Surf B      | J72        | 2          | 93.08   |
| P32          | Surf B      | J72        | 2          | 91.91   |
| P32          | Surf B      | J72        | 2          | 92.52   |
| P32          | Surf B      | J72        | 2          | 92.24   |
| P32          | Surf B      | J72        | 2          | 93.52   |
| P32          | Surf B      | J72        | 2          | 92.36   |
| P32          | Surf B      | J72        | 2          | 93.24   |
| P32          | Surf B      | J72        | 2          | 92.40   |
| P32          | Surf B      | J72        | 2          | 92.52   |
| P32          | Surf B      | J72        | 2          | 93.16   |
| P32          | Surf B      | J72        | 3          | 92.72   |
| P32          | Surf B      | J72        | 3          | 91.92   |
| P32          | Surf B      | J72        | 3          | 93.29   |
| P32          | Surf B      | J72        | 3          | 91.23   |
| P32          | Surf B      | J72        | 3          | 92.36   |
| P32          | Surf B      | J72        | 4          | 93.29   |
| P32          | Surf B      | J72        | 4          | 92.01   |
| P32          | Surf B      | J72        | 4          | 93.09   |
| P32          | Surf B      | J72        | 4          | 95.54   |
| P32          | Surf B      | J72        | 4          | 93.05   |
| P32          | Surf B      | J72        | 5          | 92.21   |
| P32          | Surf B      | J72        | 5          | 92.97   |
| P32          | Surf B      | J72        | 5          | 92.73   |
| P32          | Surf B      | J72        | 5          | 93.25   |
| P32          | Surf B      | J72        | 5          | 94.34   |
| P32          | Surf B      | J72        | 5          | 95.18   |
| P32          | Surf B      | J72        | 5          | 91.40   |
| P32          | Surf B      | J72        | 5          | 95.54   |
| P32          | Surf B      | J72        | 5          | 92.77   |
| P32          | Surf B      | J72        | 5          | 92,93   |
| P32          | Surf B      | J72        | 6          | 93,26   |
| P32          | Surf B      | J72        | 6          | 93.62   |
| P32          | Surf B      | J72        | 6          | 93,86   |
| P32          | Surf B      | J72        | 6          | 93,10   |
| P32          | Surf B      | J72        | 6          | 94,41   |
| P32          | Surf B      | J72        | 6          | 92.65   |
|              |             |            | -          |         |

| Table A.  | 1. Density | <b>Test Results</b> | Data | (continued) |
|-----------|------------|---------------------|------|-------------|
| 14810 / 4 |            | 100011000010        | Bata | (oonanaoa)  |

| Proj.<br>No. | Mix<br>Type | JMF<br>No. | Lot<br>No. | Density |
|--------------|-------------|------------|------------|---------|
| P32          | Surf B      | J72        | 6          | 93.90   |
| P32          | Surf B      | J72        | 6          | 93.90   |
| P32          | Surf B      | J72        | 6          | 93.78   |
| P32          | Surf B      | J72        | 7          | 93.29   |
| P32          | Surf B      | J72        | 7          | 92.52   |
| P32          | Surf B      | J72        | 7          | 93.45   |
| P32          | Surf B      | J72        | 7          | 93.41   |
| P32          | Surf B      | J72        | 7          | 91.92   |
| P32          | Surf B      | J72        | 7          | 93.49   |
| P32          | Surf B      | J72        | 8          | 93.18   |
| P32          | Surf B      | J72        | 8          | 93.98   |
| P32          | Surf B      | J72        | 8          | 92.50   |
| P32          | Surf B      | J72        | 8          | 92.98   |
| P32          | Surf B      | J72        | 8          | 93.38   |
| P32          | Surf B      | J72        | 8          | 92.58   |
| P32          | Surf B      | J72        | 8          | 92.22   |
| P32          | Surf B      | J72        | 8          | 93.06   |
| P32          | Surf B      | J72        | 8          | 91.86   |
| P33          | Interm B    | J73        | 1          | 93.30   |
| P33          | Interm B    | J73        | 1          | 94.14   |
| P33          | Interm B    | J73        | 1          | 96.81   |
| P33          | Interm B    | J73        | 1          | 90.67   |
| P33          | Interm B    | J73        | 1          | 93.02   |
| P33          | Interm B    | J73        | 2          | 95.05   |
| P33          | Interm B    | J73        | 2          | 94.73   |
| P33          | Interm B    | J73        | 2          | 93.11   |
| P33          | Interm B    | J73        | 2          | 92.36   |
| P33          | Interm B    | J73        | 2          | 94.22   |
| P33          | Interm B    | J73        | 2          | 88.84   |
| P33          | Interm B    | J73        | 2          | 94.02   |
| P33          | Interm B    | J73        | 3          | 92.76   |
| P33          | Interm B    | J73        | 3          | 92.29   |
| P33          | Interm B    | J73        | 3          | 93.76   |
| P33          | Interm B    | J73        | 3          | 93.56   |
| P33          | Interm B    | J73        | 3          | 91.53   |
| P33          | Interm B    | J73        | 4          | 93.83   |
| P33          | Interm B    | J73        | 4          | 92.56   |
| P33          | Interm B    | J73        | 4          | 94.82   |
| P33          | Interm B    | J73        | 4          | 93.51   |
| P33          | Interm B    | J73        | 4          | 93.15   |
| P33          | Interm B    | J73        | 4          | 93.91   |
| P33          | Interm B    | J73        | 4          | 91.44   |
| P33          | Interm B    | J73        | 4          | 93.31   |
| P33          | Interm B    | J73        | 4          | 93.95   |
| P33          | Interm B    | J73        | 4          | 94.39   |
| P33          | Interm B    | J73        | 5          | 93.13   |
| P33          | Interm B    | J73        | 5          | 93.65   |
| P33          | Interm B    | J73        | 5          | 93.13   |
| P33          | Interm B    | J73        | 5          | 94.12   |
| P33          | Interm B    | J73        | 5          | 91.62   |

| Proi | Mix      | JMF | Lot |         |
|------|----------|-----|-----|---------|
| No.  | Туре     | No. | No. | Density |
| P33  | Interm B | J73 | 5   | 92.46   |
| P33  | Interm B | J73 | 5   | 94.60   |
| P33  | Interm B | J73 | 6   | 92.55   |
| P33  | Interm B | J73 | 6   | 92.39   |
| P33  | Interm B | J73 | 6   | 92.03   |
| P33  | Interm B | J73 | 6   | 91.24   |
| P33  | Interm B | J73 | 6   | 94.17   |
| P33  | Interm B | J73 | 6   | 94.65   |
| P33  | Interm B | J73 | 6   | 94.69   |
| P33  | Interm B | J73 | 6   | 91.71   |
| P33  | Interm B | J73 | 6   | 91.83   |
| P33  | Interm B | J73 | 7   | 95.91   |
| P33  | Interm B | J73 | 7   | 93.61   |
| P33  | Interm B | J73 | 7   | 92.46   |
| P33  | Interm B | J73 | 7   | 93.29   |
| P33  | Interm B | J73 | 7   | 93.49   |
| P33  | Interm B | J73 | 7   | 94.33   |
| P33  | Interm B | J73 | 7   | 91.59   |
| P33  | Interm B | J73 | 8   | 92.86   |
| P33  | Interm B | J73 | 8   | 94.05   |
| P33  | Interm B | J73 | 8   | 91.48   |
| P33  | Interm B | J73 | 8   | 91.04   |
| P33  | Interm B | J73 | 8   | 93.46   |
| P33  | Interm B | J73 | 8   | 93.58   |
| P33  | Surf A   | J77 | 1   | 90.95   |
| P33  | Surf A   | J77 | 1   | 92.38   |
| P33  | Surf A   | J77 | 1   | 92.90   |
| P33  | Surf A   | J77 | 1   | 91.43   |
| P33  | Surf A   | J77 | 1   | 92.15   |
| P33  | Surf A   | J77 | 1   | 91.43   |
| P33  | Surf A   | J77 | 1   | 90.71   |
| P33  | Surf A   | J77 | 1   | 91.75   |
| P33  | Surf A   | J77 | 2   | 92.30   |
| P33  | Surf A   | J77 | 2   | 92.26   |
| P33  | Surf A   | J77 | 2   | 94.50   |
| P33  | Surf A   | J77 | 2   | 94.10   |
| P33  | Surf A   | J77 | 2   | 93.86   |
| P33  | Surf A   | J77 | 2   | 95.29   |
| P33  | Surf A   | J77 | 2   | 92.30   |
| P33  | Surf A   | J77 | 2   | 93.74   |
| P33  | Surf A   | J77 | 3   | 92.70   |
| P33  | Surf A   | J77 | 3   | 93.50   |
| P33  | Surf A   | J77 | 3   | 94.31   |
| P33  | Surf A   | J77 | 3   | 94.23   |
| P33  | Surf A   | J77 | 3   | 94.27   |
| P33  | Surf A   | J77 | 3   | 93.46   |
| P33  | Surf A   | J77 | 3   | 93.99   |
| P33  | Surf A   | J77 | 4   | 91.52   |
| P33  | Surf A   | J77 | 4   | 91.20   |
| P33  | Surf A   | J77 | 4   | 90.08   |

| Proj.<br>No | Mix<br>Type | JMF<br>No | Lot<br>No | Density        |
|-------------|-------------|-----------|-----------|----------------|
| P33         | Surf A      | 177       | 4         | 93.16          |
| D33         |             | 177       |           | 03.10<br>Q3.40 |
| F 33        | Surf A      | 177       | 4         | 93.40          |
| F 33        | Sull A      | J77       | 4         | 93.92          |
| P33         | Sull A      | J//       | 4         | 00.40          |
| P33         | Surf A      | J//       | 5         | 94.13          |
| P33         | Surr A      | J//       | 5         | 91.17          |
| P33         | Surf A      | J//       | 5         | 92.37          |
| P33         | Surf A      | J//       | 5         | 92.85          |
| P33         | Surf A      | J77       | 5         | 89.90          |
| P33         | Surf A      | J77       | 5         | 91.73          |
| P33         | Surf A      | J77       | 6         | 94.64          |
| P33         | Surf A      | J77       | 6         | 93.00          |
| P33         | Surf A      | J77       | 6         | 93.08          |
| P33         | Surf A      | J77       | 6         | 93.48          |
| P34         | Surf A      | J62       | 1         | 94.25          |
| P34         | Surf A      | J62       | 1         | 95.41          |
| P34         | Surf A      | J62       | 1         | 92.60          |
| P34         | Surf A      | J62       | 1         | 93.96          |
| P34         | Surf A      | J62       | 1         | 93.92          |
| P34         | Surf A      | J62       | 2         | 92.78          |
| P34         | Surf A      | J62       | 2         | 92.25          |
| P34         | Surf A      | J62       | 2         | 93.50          |
| P34         | Surf A      | J62       | 2         | 90.52          |
| P34         | Surf A      | J62       | 2         | 93.87          |
| P34         | Surf A      | J62       | 3         | 90.43          |
| P34         | Surf A      | J62       | 3         | 91.52          |
| P34         | Surf A      | J62       | 3         | 90.43          |
| P34         | Surf A      | J62       | 3         | 92.24          |
| P34         | Surf A      | J62       | 3         | 94.57          |
| P34         | Surf A      | .162      | 3         | 92.68          |
| P34         | Surf A      | 162       | 3         | 90.80          |
| D3/         |             | 162       | 3         | 80.00          |
| D24         |             | 162       | 2         | 80.00          |
| F 34        | Surf A      | 162       | 3<br>3    | 04.00          |
| F 34        |             | 162       | 3         | 94.90          |
| P34         | Suff A      |           | 4         | 95.87          |
| P34         | Surf A      | J62       | 4         | 92.46          |
| P34         | Surf A      | J62       | 4         | 94.63          |
| P34         | Surf A      | J62       | 4         | 92.66          |
| P34         | Surf A      | J62       | 4         | 93.10          |
| P36         | Interm B    | J09       | 4         | 92.86          |
| P36         | Interm B    | J09       | 4         | 93.43          |
| P36         | Interm B    | J09       | 4         | 92.90          |
| P36         | Interm B    | J09       | 10        | 91.60          |
| P36         | Interm B    | J09       | 10        | 94.02          |
| P36         | Interm B    | J09       | 10        | 93.90          |
| P36         | Interm B    | J09       | 16        | 91.65          |
| P36         | Interm B    | J09       | 16        | 93.55          |
| P36         | Interm B    | J09       | 16        | 93.47          |
| P36         | Interm B    | J09       | 16        | 92.30          |
| P36         | Interm B    | J09       | 16        | 89.74          |

| Table A.1 | . Density | <b>Test Results</b> | Data | (continued) |
|-----------|-----------|---------------------|------|-------------|
|-----------|-----------|---------------------|------|-------------|

| Proj.<br>No | Mix<br>Type | JMF<br>No. | Lot<br>No. | Density |
|-------------|-------------|------------|------------|---------|
| P36         | Interm B    | .109       | 16         | 92,95   |
| P36         | Interm B    | J09        | 16         | 93.88   |
| P36         | Interm B    | .109       | 17         | 95.49   |
| P36         | Interm B    | .109       | 17         | 92.57   |
| P36         | Interm B    | .109       | 17         | 91 15   |
| P36         | Interm B    | .109       | 17         | 91.64   |
| P36         | Interm B    | 109        | 21         | 95.49   |
| P36         | Interm B    | 109        | 21         | 92 57   |
| P36         | Interm B    | .109       | 21         | 91 15   |
| P36         | Interm B    | .109       | 21         | 91.64   |
| 1.00        | Interni B   | 000        | 21         | 01.04   |
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|             |             |            |            |         |
|             | 1           |            |            |         |

Table A.2. Plant Test Results Data

| Proj. | Mix    | JMF | Lot | AC    | AV | VMA | ] | Proj. | Mix    | JMF        | Lot | AC    | AV | VMA     |
|-------|--------|-----|-----|-------|----|-----|---|-------|--------|------------|-----|-------|----|---------|
| P01   |        | 101 | 1   | 0.04  |    |     |   | P01   | Base A | 118        | 7   | 0.44  |    |         |
| P01   |        | 101 | 1   | 0.04  |    |     | - | P01   |        | 110        | 7   | 0.44  |    |         |
| P01   |        | 101 | 1   | -0.10 |    |     | - | P01   | Base A | 118        | 8   | 0.02  |    |         |
| P01   |        | 101 | 1   | 0.03  |    |     | - | P01   |        | 110        | 0   | 0.04  |    |         |
| P01   |        | 101 | 1   | -0.32 |    |     | - | P01   | Base A | J10        | 0   | -0.34 |    |         |
| P01   |        | 101 | 1   | 0.30  |    |     | - |       | Dase A | J10<br>110 | 0   | 0.02  |    |         |
| P01   |        | 101 | 2   | -0.03 |    |     | - | P01   | Base A | J10        | 10  | -0.27 |    |         |
| P01   |        | 101 | 2   | 0.44  |    |     | - | P01   | Base A | 110        | 10  | 0.04  |    |         |
|       |        | 101 | 2   | 0.05  |    |     |   |       | Dase A | 110        | 10  | -0.11 |    | ł – – – |
| P01   |        | J01 | 2   | 0.33  |    |     | - | P01   | Base A | J10<br>140 | 10  | -0.13 |    |         |
| P01   |        | J01 | 2   | -0.04 |    |     | - |       | Dase A | J10        | 11  | 0.10  |    |         |
| P01   | AABC 1 | J01 | 3   | 0.10  |    |     | - | P01   | Base A | J18        | 11  | -0.42 |    |         |
| P01   | AABC 1 | J01 | 3   | -0.04 |    |     | - | PUT   | Base A | J18        | 12  | -0.16 |    |         |
| P01   | AABC 1 | J01 | 3   | 0.52  |    |     | - | P01   | Base A | J18        | 15  | -0.06 |    |         |
| P01   | AABC 1 | J01 | 4   | 0.35  |    |     | - | PUT   | Base A | J18        | 15  | -0.32 |    |         |
| P01   | AABC 1 | J01 | 4   | 0.21  |    |     | - | P01   | Base A | J18        | 15  | 0.14  |    |         |
| P01   | AABC 1 | J01 | 4   | 0.08  |    |     | - | P01   | Base A | J18        | 15  | 0.40  |    |         |
| P01   | AABC 1 | J01 | 5   | -0.36 |    |     | - | P01   | Base A | J18        | 1/  | -0.52 |    |         |
| P01   | AABC 1 | J01 | 6   | -0.07 |    |     | - | P01   | Base A | J18        | 18  | 0.17  |    |         |
| P01   | AABC 1 | J01 | 6   | -0.15 |    |     | - | P01   | Base A | J18        | 18  | -0.24 |    |         |
| P01   | AABC 1 | J01 | 7   | 0.22  |    |     | - | P01   | Base A | J18        | 19  | 0.30  |    |         |
| P01   | AABC 1 | J01 | 8   | 0.07  |    |     | - | P01   | Base A | J18        | 19  | 0.93  |    |         |
| P01   | AABC 1 | J01 | 8   | -0.09 |    |     | - | P01   | Base A | J18        | 20  | 0.19  |    |         |
| P01   | AABC 1 | J06 | 1   | 0.38  |    |     | 1 | P01   | Base A | J18        | 21  | -0.28 |    |         |
| P01   | AABC 1 | J06 | 1   | 0.09  |    |     | _ | P01   | Base A | J18        | 22  | -0.09 |    |         |
| P01   | AABC 1 | J06 | 1   | 0.19  |    |     |   | P01   | Base A | J18        | 23  | -0.04 |    |         |
| P01   | AABC 1 | J06 | 2   | -0.16 |    |     |   | P01   | Base A | J18        | 23  | -0.43 |    |         |
| P01   | AABC 1 | J06 | 2   | 0.39  |    |     |   | P01   | Base A | J18        | 23  | -0.46 |    |         |
| P01   | AABC 1 | J06 | 2   | 0.01  |    |     |   | P01   | Base A | J18        | 23  | -0.49 |    |         |
| P01   | AABC 1 | J06 | 2   | -0.05 |    |     |   | P01   | Base A | J18        | 31  | 0.13  |    |         |
| P01   | AABC 1 | J06 | 3   | 0.20  |    |     |   | P01   | Base A | J18        | 31  | -0.02 |    |         |
| P01   | AABC 1 | J06 | 3   | -0.17 |    |     |   | P01   | Base A | J18        | 31  | -0.11 |    |         |
| P01   | Base A | J18 | 1   | 0.02  |    |     |   | P01   | Base A | J18        | 32  | 0.08  |    |         |
| P01   | Base A | J18 | 1   | 0.19  |    |     |   | P01   | Base A | J18        | 32  | 0.06  |    |         |
| P01   | Base A | J18 | 1   | -0.37 |    |     |   | P01   | Base A | J18        | 33  | -0.15 |    |         |
| P01   | Base A | J18 | 1   | -0.25 |    |     |   | P01   | Base A | J18        | 33  | -0.39 |    |         |
| P01   | Base A | J18 | 3   | 0.00  |    |     |   | P01   | Base A | J18        | 34  | -0.11 |    |         |
| P01   | Base A | J18 | 3   | 0.02  |    |     |   | P01   | Base A | J18        | 35  | 0.03  |    |         |
| P01   | Base A | J18 | 3   | -0.05 |    |     |   | P01   | Base A | J18        | 35  | -0.12 |    |         |
| P01   | Base A | J18 | 4   | 0.39  |    |     |   | P01   | Base A | J18        | 36  | 0.09  |    |         |
| P01   | Base A | J18 | 4   | -0.08 |    |     |   | P01   | Base A | J18        | 36  | 0.23  |    |         |
| P01   | Base A | J18 | 4   | -0.06 |    |     |   | P01   | Base A | J18        | 37  | 0.04  |    |         |
| P01   | Base A | J18 | 4   | -0.07 |    |     |   | P01   | Base A | J18        | 37  | -0.21 |    |         |
| P01   | Base A | J18 | 5   | -0.05 |    |     |   | P01   | Base A | J18        | 37  | -0.31 |    |         |
| P01   | Base A | J18 | 5   | 0.08  |    |     | ] | P01   | Base A | J18        | 39  | -0.07 |    |         |
| P01   | Base A | J18 | 5   | 0.00  |    |     | ] | P01   | Base A | J18        | 39  | 0.17  |    |         |
| P01   | Base A | J18 | 5   | 0.01  |    |     | 1 | P01   | Base A | J18        | 39  | -0.27 |    | 1       |
| P01   | Base A | J18 | 6   | -0.08 |    |     | 1 | P01   | Base A | J18        | 39  | -0.13 |    |         |
| P01   | Base A | J18 | 6   | 0.11  |    |     | 1 | P01   | Base A | J18        | 40  | 0.16  |    |         |
| P01   | Base A | J18 | 6   | -0.15 |    |     | 1 | P01   | Base A | J18        | 40  | -0.16 |    | 1       |
| P01   | Base A | J18 | 7   | -0.09 |    |     | 1 | P01   | Base A | J18        | 40  | -0.06 |    |         |

| Table A.2. | Plant | <b>Test Results</b> | Data | (continued) |
|------------|-------|---------------------|------|-------------|
|------------|-------|---------------------|------|-------------|

| P01         Base A         J16         J1         Out         P01         Binder 1         J02         3         0.29         -0.57         0.06           P01         Base A         J18         41         0.18         -0.17         P01         Binder 1         J02         4         -0.02         -0.22         -0.83         -0.06         -0.22         -0.83         -0.06         -0.02         -0.22         -0.83         -0.06         -0.02         -0.22         -0.83         -0.06         -0.02         -0.22         -0.83         -0.06         -0.01         -0.02         -0.23         -0.06         -0.22         -0.83         -0.06         -0.11         -0.02         -0.22         -0.23         -0.11         -0.02         -0.23         -0.11         -0.02         -0.23         -0.11         -0.02         -0.03         -0.02         -0.03         -0.02         -0.03         -0.02         -0.03         -0.03         -0.02         -0.03         -0.02         -0.03         -0.02         -0.03         -0.02         -0.03         -0.02         -0.03         -0.02         -0.03         -0.02         -0.03         -0.04         -0.19         -0.11         -0.04         -0.10         -0.17         -0.01 </th <th>Proj.<br/>No.</th> <th>Mix<br/>Type</th> <th>JMF<br/>No.</th> <th>Lot<br/>No.</th> <th>AC</th> <th>AV</th> <th>VMA</th> <th></th> <th>Proj.<br/>No.</th> <th>Mix<br/>Type</th> <th>JMF<br/>No.</th> <th>Lot<br/>No.</th> <th>AC</th> <th>AV</th> <th>VMA</th> | Proj.<br>No. | Mix<br>Type | JMF<br>No. | Lot<br>No. | AC    | AV    | VMA   |   | Proj.<br>No. | Mix<br>Type | JMF<br>No. | Lot<br>No. | AC    | AV    | VMA   |
|---|--------------|-------------|------------|------------|-------|-------|-------|---|--------------|-------------|------------|------------|-------|-------|-------|
| PO1         Base A         J18         41         0.18         P01         Binder 1         J02         4         -0.02         -0.03         -0.02         -0.03   | P01          | Base A      | J18        | 41         | -0.13 |       |       |   | P01          | Binder 1    | J02        | 3          | 0.29  | -0.57 | 0.06  |
| P01         Base A         J18         43         -0.17           P01         Base A         J18         43         -0.37           P01         Base A         J18         44         -0.17           P01         Base A         J18         44         -0.17           P01         Base A         J18         44         -0.17           P01         Base A         J18         45         -0.04           P01         Base A         J18         45         -0.04           P01         Base A         J18         60         -0.31           P01         Base A         J21         3         0.01           P01         Base A         J21         3         0.02           P01         Base A         J21         3         0.02           P01         Base A         J21         3         0.30   | P01          | Base A      | J18        | 41         | 0.18  |       |       |   | P01          | Binder 1    | J02        | 4          | -0.02 | -0.09 | -0.22 |
| P01         Base A         J18         43         -0.37           P01         Base A         J18         44         -0.17         P01         Interm B         J10         1         0.02         -1.02         0.82           P01         Base A         J18         45         -0.04         P01         Interm B         J10         1         0.02         -1.02         0.82           P01         Base A         J18         46         -0.15         P01         Interm B         J10         4         -0.17         -1.10         -0.57           P01         Base A         J18         60         -0.04         P01         Interm B         J10         4         -0.17         -1.10         -0.55         -0.04           P01         Base A         J21         1         0.22         -0.66         -0.33         P01         Interm B         J10         5         -0.04         -0.02         -0.77         -0.90           P01         Base A         J21         1         0.27         P01         Interm B         J10         7         -0.24         -0.20         -0.73           P01         Base A         J21         1         0.06   | P01          | Base A      | J18        | 43         | -0.17 |       |       |   | P01          | Interm B    | J10        | 1          | 0.25  | -0.80 | -0.17 |
| P01         Base A         J18         44         -0.17           P01         Base A         J18         44         -0.17         P01           P01         Base A         J18         44         -0.19         P01           P01         Base A         J18         45         -0.24         P01         Interm B         J10         4         -0.11         -0.32           P01         Base A         J18         46         -0.02         P01         Interm B         J10         4         -0.17         -0.53         -0.02           P01         Base A         J18         60         -0.03         -0.02         P01         Interm B         J10         4         -0.17         -0.55         -0.04           P01         Base A         J21         0.01         P01         Interm B         J10         5         -0.04         -0.02         P01         Interm B         J10         5         -0.04         -0.02         P01         Interm B         J10         7         -0.24         -0.22         -0.64           P01         Base A         J21         4         -0.05         -0.04         P01         Interm B         J10         7 <t< td=""><td>P01</td><td>Base A</td><td>J18</td><td>43</td><td>-0.37</td><td></td><td></td><td></td><td>P01</td><td>Interm B</td><td>J10</td><td>1</td><td>0.02</td><td>-1.02</td><td>-0.82</td></t<>  | P01          | Base A      | J18        | 43         | -0.37 |       |       |   | P01          | Interm B    | J10        | 1          | 0.02  | -1.02 | -0.82 |
| P01         Base A         J18         44         -0.19         P01         Interm B         J10         2         0.29         -1.11         -0.32           P01         Base A         J18         46         -0.64         P01         Interm B         J10         3         -0.44         -1.12         -0.30           P01         Base A         J18         46         -0.15         P01         Interm B         J10         4         -0.02         -0.03         -0.03         -0.02           P01         Base A         J18         60         -0.31         P01         Interm B         J10         4         -0.02         -0.03         -0.02         P01         Interm B         J10         4         -0.02         -0.03         -0.02         P01         Interm B         J10         5         -0.04         -0.01         -0.02         -0.03         P01         Interm B         J10         5         -0.04         -0.02         -0.03         P01         Interm B         J10         5         -0.04         -0.02         -0.03         P01         Interm B         J10         10         -0.02         -0.03         P01         Interm B         J10         10         -0.02  | P01          | Base A      | J18        | 44         | -0.17 |       |       |   | P01          | Interm B    | J10        | 1          | 0.08  | -1.03 | -0.74 |
| P01         Base A         J18         45         -0.04         P01           P01         Base A         J18         45         -0.24         P01         Interm B         J10         3         -0.44         -1.12         -2.00           P01         Base A         J18         46         -0.15         -         P01         Interm B         J10         4         -0.17         -0.55         -0.04           P01         Base A         J18         60         -0.01         -0.02         -0.03         -0.02         -0.03         -0.02         -0.07         -0.90           P01         Base A         J21         1         0.32         -0.10         -0.10         -0.10         -0.03         -0.33           P01         Base A         J21         3         0.01         P01         Interm B         J10         7         -0.24         -0.02         -0.73           P01         Base A         J21         3         0.27         P01         Interm B         J10         7         -0.24         -0.26         -0.33           P01         Base A         J21         4         -0.26         -0.33         P01         Interm B         J10   | P01          | Base A      | J18        | 44         | -0.19 |       |       |   | P01          | Interm B    | J10        | 2          | 0.29  | -1.11 | -0.32 |
| P01         Base A         J18         45         -0.24         P01           P01         Base A         J18         46         -0.15         P01         Interm B         J10         4         -0.17         -1.10         -0.54           P01         Base A         J18         60         -0.31         P01         Interm B         J10         4         -0.02         -0.03         -0.02           P01         Base A         J18         60         -0.01         -0.77         -0.90           P01         Base A         J21         1         0.32         P01         Interm B         J10         5         -0.04         -0.19         -0.19         -0.19         -0.19         -0.19         -0.19         -0.19         -0.19         -0.19         -0.19         -0.19         -0.19         -0.19         -0.19         -0.10         -0.77         -0.90         P01         Interm B         J10         5         -0.04         -0.02         -0.23         -0.02         -0.24         -0.24         -0.22         -0.23         -0.26         -0.41           P01         Base A         J21         4         -0.06         P01         Interm B         J10         10  | P01          | Base A      | J18        | 45         | -0.04 |       |       |   | P01          | Interm B    | J10        | 3          | -0.44 | -1.12 | -2.00 |
| P01         Base A         J18         46         -0.16           P01         Base A         J18         46         -0.04         P01           P01         Base A         J18         60         -0.01         P01         Interm B         J10         4         -0.02         -0.03         -0.02           P01         Base A         J18         60         -0.01         P01         Interm B         J10         4         -0.02         -0.03         -0.02           P01         Base A         J18         60         -0.01         P01         Interm B         J10         5         -0.10         -0.07         -0.90           P01         Base A         J21         2         0.01         P01         Interm B         J10         7         -0.04         -0.09         -0.52         -0.64           P01         Base A         J21         3         0.06         P01         Interm B         J10         7         -0.24         -0.26         -0.33           P01         Base A         J21         6         0.30         P01         Interm B         J10         10         -0.02         -0.33         P01         Interm B         J10 <t< td=""><td>P01</td><td>Base A</td><td>J18</td><td>45</td><td>-0.24</td><td></td><td></td><td></td><td>P01</td><td>Interm B</td><td>J10</td><td>4</td><td>-0.41</td><td>0.53</td><td>-0.37</td></t<>  | P01          | Base A      | J18        | 45         | -0.24 |       |       |   | P01          | Interm B    | J10        | 4          | -0.41 | 0.53  | -0.37 |
| P01         Base A         J18         46         0.04         P01           P01         Base A         J18         60         0.031         P01         Interm B         J10         4         -0.02         -0.03         -0.02           P01         Base A         J18         60         0.06         P01         Interm B         J10         4         -0.02         -0.03         -0.02           P01         Base A         J18         60         0.01         P01         Interm B         J10         5         -0.04         -0.19         -0.19         P01         Interm B         J10         5         -0.04         -0.19         -0.19         P01         Interm B         J10         7         -0.24         -0.20         -0.73         -0.14         -0.24         -0.20         -0.33           P01         Base A         J21         4         -0.19         P01         Interm B         J10         17         -0.24         -0.20         -0.73           P01         Base A         J21         4         -0.26         -0.33         P01         Interm B         J10         10         -0.07         -0.20         -0.35         P01         Interm B         J1   | P01          | Base A      | J18        | 46         | -0.15 |       |       |   | P01          | Interm B    | J10        | 4          | 0.17  | -1.10 | -0.54 |
| P01         Base A         J18         60         -0.31         P01           P01         Base A         J18         60         -0.06         P01         Interm B         J10         4         0.17         -0.55         -0.04           P01         Base A         J11         1         0.32         P01         Interm B         J10         5         -0.04         -0.19         -0.19         -0.19         -0.19         -0.19         -0.19         -0.19         -0.19         -0.19         -0.19         -0.19         -0.19         -0.13         -0.10         -0.63         -0.33         P01         Base A         J21         3         0.01         -0.11         P01         Interm B         J10         7         -0.24         -0.24         -0.26         -0.33           P01         Base A         J21         4         -0.06         -0.11         Interm B         J10         10         0.03         -0.13         -0.13         -0.13         -0.13         -0.13         -0.13         -0.13         -0.14         -0.46         -0.48         P01         Interm B         J10         11         -0.46         -0.46         P01         Interm B         J10         13         -0.06<  | P01          | Base A      | J18        | 46         | 0.04  |       |       |   | P01          | Interm B    | J10        | 4          | -0.02 | -0.03 | -0.02 |
| P01         Base A         J18         60         0.06         P01           P01         Base A         J18         60         0.01         P01         Interm B         J10         5         -0.10         -0.77         -0.90           P01         Base A         J21         1         0.32         P01         Interm B         J10         5         -0.10         -0.63         -0.33         -0.33           P01         Base A         J21         3         0.04         P01         Interm B         J10         7         -0.24         0.20         -0.73           P01         Base A         J21         3         0.27         P01         Interm B         J10         7         -0.24         0.20         -0.73           P01         Base A         J21         4         -0.06         P01         Interm B         J10         10         -0.07         -0.20         -0.35           P01         Base A         J21         4         -0.26         -0.37         P01         Interm B         J10         10         -0.40         -0.86         -0.41         -0.40         -0.86         -0.66         -0.43         -0.66         -0.33         -0.66   | P01          | Base A      | J18        | 60         | -0.31 |       |       |   | P01          | Interm B    | J10        | 4          | 0.17  | -0.55 | -0.04 |
| P01         Base A         J18         60         0.01         P01           P01         Base A         J21         1         0.32         P01         P01<   | P01          | Base A      | J18        | 60         | 0.06  |       |       |   | P01          | Interm B    | J10        | 5          | -0.10 | -0.77 | -0.90 |
| P01         Base A         J21         1         0.32         P01           P01         Base A         J21         2         0.17         P01         Interm B         J10         5         0.10         -0.63         -0.33           P01         Base A         J21         3         0.10         P01         Interm B         J10         7         -0.04         -0.02         -0.64           P01         Base A         J21         3         0.04         P01         Interm B         J10         7         -0.24         -0.20         -0.73           P01         Base A         J21         4         -0.06         P01         Interm B         J10         7         -0.24         -0.20         -0.73           P01         Base A         J21         4         -0.06         P01         Interm B         J10         10         -0.073         -0.24         -0.20         -0.33           P01         Base A         J21         6         -0.33         P01         Interm B         J10         11         0.06         -0.43           P01         Base A         J21         8         -0.36         P01         Interm B         J10         13 </td <td>P01</td> <td>Base A</td> <td>J18</td> <td>60</td> <td>0.01</td> <td></td> <td></td> <td></td> <td>P01</td> <td>Interm B</td> <td>J10</td> <td>5</td> <td>-0.04</td> <td>-0.19</td> <td>-0.19</td>   | P01          | Base A      | J18        | 60         | 0.01  |       |       |   | P01          | Interm B    | J10        | 5          | -0.04 | -0.19 | -0.19 |
| P01         Base A         J21         2         0.17         P01           P01         Base A         J21         3         0.10         P01         Interm B         J10         7         -0.44         -0.02         -0.73           P01         Base A         J21         3         0.04         P01         Interm B         J10         7         -0.24         -0.26         -0.33           P01         Base A         J21         4         -0.19         -0.64         -0.73           P01         Base A         J21         4         -0.06         P01         Interm B         J10         7         -0.24         -0.26         -0.33           P01         Base A         J21         4         -0.06         P01         Interm B         J10         10         -0.73         P02         -0.33         P01         Interm B         J10         10         -0.20         -0.35         P01         Interm B         J10         11         0.43         -0.14         0.20         -0.35         P01         Interm B         J10         11         0.43         -0.64         -0.43         P01         Interm B         J10         13         -0.04         -0.65  | P01          | Base A      | J21        | 1          | 0.32  |       |       |   | P01          | Interm B    | J10        | 5          | 0.10  | -0.63 | -0.33 |
| P01         Base A         J21         3         0.10         P01           P01         Base A         J21         3         0.04         P01           P01         Base A         J21         3         0.04         P01           P01         Base A         J21         4         -0.19         P01           P01         Base A         J21         4         -0.06         P01           P01         Base A         J21         4         -0.06         P01           P01         Base A         J21         4         0.26         P01         Interm B         J10         9         0.13         -0.13         0.20           P01         Base A         J21         6         0.30         P01         Interm B         J10         10         -0.07         -0.20         -0.35           P01         Base A         J21         6         0.30         P01         Interm B         J10         11         0.05         -0.64         P01         Interm B         J10         12         0.05         -0.64         P01         Interm B         J10         13         0.016         P01         P01         P01         P01         P01 <td>P01</td> <td>Base A</td> <td>J21</td> <td>2</td> <td>0.17</td> <td></td> <td></td> <td></td> <td>P01</td> <td>Interm B</td> <td>J10</td> <td>6</td> <td>0.14</td> <td>-0.44</td> <td>-0.02</td>   | P01          | Base A      | J21        | 2          | 0.17  |       |       |   | P01          | Interm B    | J10        | 6          | 0.14  | -0.44 | -0.02 |
| P01         Base A         J21         3         0.04         P01           P01         Base A         J21         3         0.04         P01         P01 </td <td>P01</td> <td>Base A</td> <td>J21</td> <td>3</td> <td>0.10</td> <td></td> <td></td> <td></td> <td>P01</td> <td>Interm B</td> <td>J10</td> <td>7</td> <td>-0.09</td> <td>-0.52</td> <td>-0.64</td>   | P01          | Base A      | J21        | 3          | 0.10  |       |       |   | P01          | Interm B    | J10        | 7          | -0.09 | -0.52 | -0.64 |
| P01         Base A         J21         3         0.27         P01           P01         Base A         J21         4         -0.19         P01         P01         Base A         J21         4         -0.26         -0.33           P01         Base A         J21         4         -0.26         P01         P01         Interm B         J10         9         0.13         -0.13         0.20           P01         Base A         J21         5         0.37         P01         Interm B         J10         10         -0.07         -0.20         -0.35           P01         Base A         J21         6         0.30         P01         Interm B         J10         11         0.05         -0.66         -0.43           P01         Base A         J21         6         0.36         P01         Interm B         J10         11         0.43         -0.14         P01         Interm B         J10         11         0.43         -0.44         P01  | P01          | Base A      | J21        | 3          | 0.04  |       |       |   | P01          | Interm B    | J10        | 7          | -0.24 | -0.20 | -0.73 |
| P01         Base A         J21         4         -0.19           P01         Base A         J21         4         -0.06         P01           P01         Base A         J21         4         -0.06         P01           P01         Base A         J21         4         -0.06         P01           P01         Base A         J21         4         -0.26         P01           P01         Base A         J21         6         0.30         P01         Interm B         J10         10         -0.07         -0.20         -0.36           P01         Base A         J21         6         0.31         -0.11         P01         Interm B         J10         11         0.03         -0.46         -0.43           P01         Base A         J21         8         0.59         P01         Interm B         J10         13         0.06         -0.46           P01         Base A         J21         10         0.00         P01         Interm B         J10         13         0.04         -0.08         -0.16           P01         Base A         J21         11         -0.45         -0.10         P01         Interm B   | P01          | Base A      | J21        | 3          | 0.27  |       |       |   | P01          | Interm B    | J10        | 7          | -0.24 | 0.26  | -0.33 |
| P01         Base A         J21         4         0.06         P01           P01         Base A         J21         4         0.06         P01         Interm B         J10         9         0.13         0.016         P01         Interm B         J10         11         0.033         0.06         P01         Interm B         J10         13         0.016         P01         Interm B         J10         13         0.006         P01         Interm B         J10         14         0.023         0.027         0.010         P01         Interm B         J10         14         0.023         0.   | P01          | Base A      | J21        | 4          | -0.19 |       |       |   | P01          | Interm B    | J10        | 8          | 0.18  | -0.63 | -0.13 |
| P01         Base A         J21         4         0.26           P01         Base A         J21         5         0.37         P01         Interm B         J10         10         -0.07         -0.20         -0.35           P01         Base A         J21         5         0.37         P01         Interm B         J10         11         0.05         -0.66         -0.43           P01         Base A         J21         6         0.36         P01         Interm B         J10         11         0.43         -0.14         0.86           P01         Base A         J21         6         0.36         P01         Interm B         J10         12         0.10         -0.33         -0.06           P01         Base A         J21         8         0.59         P01         Interm B         J10         13         0.06         -0.57         -0.37           P01         Base A         J21         10         0.00         P01         Interm B         J10         13         0.00         -0.02         -0.02           P01         Base A         J21         11         0.43         -0.16         P01         Interm B         J10         14 <td>P01</td> <td>Base A</td> <td>J21</td> <td>4</td> <td>-0.06</td> <td></td> <td></td> <td></td> <td>P01</td> <td>Interm B</td> <td>J10</td> <td>9</td> <td>0.13</td> <td>-0.13</td> <td>0.20</td>   | P01          | Base A      | J21        | 4          | -0.06 |       |       |   | P01          | Interm B    | J10        | 9          | 0.13  | -0.13 | 0.20  |
| P01         Base A         J21         5         0.37         P01         Interm B         J10         11         0.05         0.06         0.43           P01         Base A         J21         6         0.30         P01         Interm B         J10         11         0.05         0.06         0.43           P01         Base A         J21         6         0.30         P01         Interm B         J10         11         0.05         0.06         P01         Interm B         J10         12         0.10         0.03         0.06           P01         Base A         J21         8         0.30         P01         Interm B         J10         13         0.15         0.96         0.46           P01         Base A         J21         8         0.30         P01         Interm B         J10         13         0.06         P01         Interm B         J10         13         0.06         0.06           P01         Base A         J21         11         0.45         P01         Interm B         J10         13         0.06         0.02         0.03           P01         Base A         J21         11         0.45         P01   | P01          | Base A      | J21        | 4          | 0.26  |       |       |   | P01          | Interm B    | J10        | 10         | -0.07 | -0.20 | -0.35 |
| P01         Base A         J21         6         0.30           P01         Base A         J21         6         0.30         P01         Interm B         J10         11         0.43         -0.14         0.86           P01         Base A         J21         6         0.30         P01         Interm B         J10         11         0.43         -0.14         0.86           P01         Base A         J21         8         0.59         P01         Interm B         J10         12         0.00         -0.36         -0.18           P01         Base A         J21         8         0.30         P01         Interm B         J10         13         0.06         -0.57         -0.37           P01         Base A         J21         10         0.00         P01         Interm B         J10         13         0.00         -0.02         P01         Interm B         J10         14         0.33         -0.02         P01         P01         Interm B         J10         14         0.33         -0.02         P01         Interm B         J10         14         0.33         -0.02         P01         Interm B         J10         14         0.23   | P01          | Base A      | J21        | 5          | 0.37  |       |       |   | P01          | Interm B    | J10        | 11         | 0.05  | -0.66 | -0.43 |
| P01         Base A         J21         6         0.11         P01           P01         Base A         J21         6         0.11         P01         P01 </td <td>P01</td> <td>Base A</td> <td>J21</td> <td>6</td> <td>0.30</td> <td></td> <td></td> <td></td> <td>P01</td> <td>Interm B</td> <td>J10</td> <td>11</td> <td>0.43</td> <td>-0.14</td> <td>0.86</td>  | P01          | Base A      | J21        | 6          | 0.30  |       |       |   | P01          | Interm B    | J10        | 11         | 0.43  | -0.14 | 0.86  |
| P01         Base A         J21         6         -0.36         -0.36           P01         Base A         J21         8         0.59         -0.18         P01         Interm B         J10         12         0.05         -0.36         -0.18           P01         Base A         J21         8         0.59         -0.17         -0.05         -0.36         -0.18           P01         Base A         J21         8         0.30         -0.17         -0.01         -0.05         -0.37           P01         Base A         J21         9         0.06         -0.10         P01         Interm B         J10         13         -0.04         -0.08         -0.16           P01         Base A         J21         11         0.045         -0.10         P01         Interm B         J10         13         -0.02         -0.02         -0.02           P01         Base A         J21         11         0.45         -0.11         P01         Interm B         J10         14         0.23         -0.79         -0.13         -0.23           P01         Base A         J21         14         0.32         -0.17         -0.13         -0.23         -0.06  | P01          | Base A      | J21        | 6          | 0.11  |       |       |   | P01          | Interm B    | J10        | 12         | 0.10  | -0.33 | -0.06 |
| P01         Base A         J21         8         0.59         P01           P01         Base A         J21         8         0.59         P01           P01         Base A         J21         8         0.17         P01           P01         Base A         J21         8         0.30         P01           P01         Base A         J21         9         0.06         P01           P01         Base A         J21         10         0.00         P01           P01         Base A         J21         10         0.00         P01           P01         Base A         J21         11         0.45         P01         Interm B         J10         13         0.00         -0.02           P01         Base A         J21         11         0.45         P01         Interm B         J10         14         0.13         -0.13           P01         Base A         J21         13         -0.05         P01         Interm B         J10         17         -0.06         -0.13         -0.23           P01         Base A         J21         15         0.13         P01         Interm B         J10         18  | P01          | Base A      | J21        | 6          | -0.36 |       |       |   | P01          | Interm B    | J10        | 12         | 0.05  | -0.36 | -0.18 |
| P01       Base A       J21       8       -0.17         P01       Base A       J21       8       0.30       P01       Interm B       J10       13       0.06       -0.37         P01       Base A       J21       9       0.06       P01       Interm B       J10       13       0.06       -0.02       -0.02         P01       Base A       J21       10       0.00       P01       Interm B       J10       13       0.06       -0.02       -0.02         P01       Base A       J21       11       0.45       P01       Interm B       J10       14       0.13       -0.02       -0.02       -0.02         P01       Base A       J21       11       0.49       P01       Interm B       J10       14       0.13       -0.06       -0.13       -0.20       -0.23       -0.79       -0.10         P01       Base A       J21       15       -0.14       P01       Interm B       J10       17       -0.06       -0.13       -0.20       0.38       -0.12       P01       Interm B       J10       18       -0.20       0.38       -0.12       P01       Interm B       J10       19       -0.27  | P01          | Base A      | J21        | 8          | 0.59  |       |       |   | P01          | Interm B    | J10        | 13         | 0.15  | -0.96 | -0.46 |
| P01         Base A         J21         8         0.01         0.   | P01          | Base A      | J21        | 8          | -0.17 |       |       |   | P01          | Interm B    | J10        | 13         | 0.06  | -0.57 | -0.37 |
| Poil         Base A         J21         9         0.06           P01         Base A         J21         10         0.00         P01           P01         Base A         J21         10         0.00         P01           P01         Base A         J21         11         -0.45         P01         Interm B         J10         14         0.13         -0.02           P01         Base A         J21         11         -0.45         P01         Interm B         J10         14         0.13         -0.02           P01         Base A         J21         11         -0.45         P01         Interm B         J10         14         0.23         -0.79         -0.10           P01         Base A         J21         13         -0.05         P01         Interm B         J10         17         -0.13         -0.23           P01         Base A         J21         15         -0.14         P01         Interm B         J10         18         -0.20         0.38         -0.12           P01         Base A         J21         16         -0.11         P01         Interm B         J10         19         -0.20         0.38         -0.12<  | P01          | Base A      | J21        | 8          | 0.30  |       |       |   | P01          | Interm B    | J10        | 13         | -0.04 | -0.08 | -0.16 |
| P01         Base A         J21         10         0.00           P01         Base A         J21         11         0.00         P01           P01         Base A         J21         11         0.45         P01           P01         Base A         J21         11         0.49         P01           P01         Base A         J21         11         0.49         P01           P01         Base A         J21         13         0.05         P01         Interm B         J10         17         0.06         -0.13         -0.23           P01         Base A         J21         13         -0.05         P01         Interm B         J10         18         0.24         0.26         0.82           P01         Base A         J21         15         0.14         P01         Interm B         J10         18         0.24         0.26         0.82           P01         Base A         J21         15         0.13         P01         Interm B         J10         18         0.20         0.38         -0.12           P01         Base A         J21         16         -0.11         P01         Interm B         J10 <th< td=""><td>P01</td><td>Base A</td><td>J21</td><td>9</td><td>0.06</td><td></td><td></td><td></td><td>P01</td><td>Interm B</td><td>J10</td><td>13</td><td>0.00</td><td>-0.02</td><td>-0.02</td></th<>   | P01          | Base A      | J21        | 9          | 0.06  |       |       |   | P01          | Interm B    | J10        | 13         | 0.00  | -0.02 | -0.02 |
| P01         Base A         J21         11         -0.45           P01         Base A         J21         11         0.45         P01         Interm B         J10         14         0.23         -0.79         -0.10           P01         Base A         J21         11         0.49         P01         Interm B         J10         14         0.23         -0.79         -0.10           P01         Base A         J21         13         -0.05         P01         Interm B         J10         17         -0.06         -0.13         -0.23           P01         Base A         J21         13         -0.05         P01         Interm B         J10         17         -0.13         -0.23         P02           P01         Base A         J21         15         -0.14         P01         Interm B         J10         18         -0.20         0.38         -0.12           P01         Base A         J21         15         0.13         P01         Interm B         J10         19         -0.27         0.43         -0.26           P01         Base A         J21         16         -0.11         P01         Interm B         J10         20         <  | P01          | Base A      | J21        | 10         | 0.00  |       |       |   | P01          | Interm B    | J10        | 14         | 0.13  | -0.99 | -0.52 |
| P01         Base A         J21         11         0.49           P01         Base A         J21         11         0.49         P01           P01         Base A         J21         12         0.36         P01           P01         Base A         J21         13         -0.05         P01           P01         Base A         J21         14         0.32         P01         Interm B         J10         17         -0.06         -0.13         -0.02           P01         Base A         J21         13         -0.05         P01         Interm B         J10         17         -0.06         -0.13         -0.06           P01         Base A         J21         15         0.14         P01         Interm B         J10         18         0.20         0.38         -0.12           P01         Base A         J21         15         0.13         -0.07         P01         Interm B         J10         19         -0.27         0.43         -0.26           P01         Base A         J21         16         -0.11         P01         Interm B         J10         20         -0.23         0.40         -0.12           P01   | P01          | Base A      | J21        | 11         | -0.45 |       |       |   | P01          | Interm B    | J10        | 14         | 0.23  | -0.79 | -0.10 |
| P01         Base A         J21         12         0.36         P01         Interm B         J10         17         0.13         -0.43         -0.06           P01         Base A         J21         13         -0.05         P01         Interm B         J10         17         0.13         -0.43         -0.06           P01         Base A         J21         14         0.32         P01         Interm B         J10         18         0.24         0.26         0.82           P01         Base A         J21         15         0.14         P01         Interm B         J10         18         0.20         0.38         -0.12           P01         Base A         J21         15         0.13         P01         Interm B         J10         19         -0.20         0.38         -0.12           P01         Base A         J21         16         -0.07         P01         Interm B         J10         20         -0.37         -0.09         -0.83           P01         Binder 1         J02         1         0.00         P01         Interm B         J10         20         -0.23         0.40         -0.12           P01         Binder 1   | P01          | Base A      | J21        | 11         | 0.49  |       |       |   | P01          | Interm B    | J10        | 17         | -0.06 | -0.13 | -0.23 |
| P01         Base A         J21         13         -0.05           P01         Base A         J21         14         0.32         P01         Interm B         J10         18         0.24         0.26         0.82           P01         Base A         J21         14         0.32         P01         Interm B         J10         18         0.24         0.26         0.82           P01         Base A         J21         15         -0.14         P01         Interm B         J10         18         0.11         0.06         0.29           P01         Base A         J21         15         0.34         P01         Interm B         J10         18         -0.20         0.38         -0.12           P01         Base A         J21         16         -0.07         P01         Interm B         J10         19         -0.20         0.38         -0.12           P01         Base A         J21         16         -0.11         P01         Interm B         J10         20         -0.23         0.40         -0.12           P01         Binder 1         J02         1         0.05         P01         Interm B         J23         1         0.37  | P01          | Base A      | J21        | 12         | 0.36  |       |       |   | P01          | Interm B    | J10        | 17         | 0.13  | -0.43 | -0.06 |
| P01         Base A         J21         14         0.32         P01         Interm B         J10         18         0.11         0.06         0.29           P01         Base A         J21         15         -0.14         P01         Interm B         J10         18         -0.27         0.43         -0.26           P01         Base A         J21         15         0.13         P01         Interm B         J10         19         -0.27         0.43         -0.26           P01         Base A         J21         16         -0.07         P01         Interm B         J10         19         -0.20         0.38         -0.12           P01         Base A         J21         16         -0.11         P01         Interm B         J10         20         -0.37         -0.09         -0.83           P01         Binder 1         J02         1         0.00         P01         Interm B         J10         20         -0.23         0.40         -0.12           P01         Binder 1         J02         1         0.05         P01         Interm B         J23         1         0.37         -0.55         0.36           P01         Binder 1  | P01          | Base A      | J21        | 13         | -0.05 |       |       |   | P01          | Interm B    | J10        | 18         | 0.24  | 0.26  | 0.82  |
| P01         Base A         J21         15         -0.14   | P01          | Base A      | J21        | 14         | 0.32  |       |       |   | P01          | Interm B    | J10        | 18         | 0.11  | 0.06  | 0.29  |
| P01         Base A         J21         15         0.34         P01           P01         Base A         J21         15         0.13         P01         Interm B         J10         19         -0.27         0.43         -0.26           P01         Base A         J21         15         0.13         P01         Interm B         J10         19         -0.27         0.43         -0.26           P01         Base A         J21         16         -0.07         P01         Interm B         J10         20         -0.37         -0.09         -0.83           P01         Binder 1         J02         1         0.00         P01         Interm B         J10         20         -0.23         0.40         -0.12           P01         Binder 1         J02         1         0.00         P01         Interm B         J23         1         0.37         -0.55         0.36           P01         Binder 1         J02         1         0.00         P01         Interm B         J23         1         0.18         -0.28         0.19           P01         Binder 1         J02         1         0.38         -0.31         0.50         P01         I  | P01          | Base A      | J21        | 15         | -0.14 |       |       |   | P01          | Interm B    | J10        | 18         | -0.20 | 0.38  | -0.12 |
| P01         Base A         J21         15         0.13  | P01          | Base A      | J21        | 15         | 0.34  |       |       |   | P01          | Interm B    | J10        | 19         | -0.27 | 0.43  | -0.26 |
| P01         Base A         J21         16         -0.07         P01           P01         Base A         J21         16         -0.07         P01         P01         Interm B         J10         20         -0.37         -0.09         -0.83           P01         Binder 1         J02         1         0.00         P01         Interm B         J10         20         -0.05         -0.56         -0.57           P01         Binder 1         J02         1         0.00         P01         Interm B         J10         20         -0.23         0.40         -0.12           P01         Binder 1         J02         1         0.05         P01         Interm B         J23         1         0.37         -0.55         0.36           P01         Binder 1         J02         1         0.05         P01         Interm B         J23         1         0.55         -0.92         0.43           P01         Binder 1         J02         1         0.00         P01         Interm B         J23         1         0.18         -0.28         0.19           P01         Binder 1         J02         1         0.38         -0.31         0.50 <td< td=""><td>P01</td><td>Base A</td><td>J21</td><td>15</td><td>0.13</td><td></td><td></td><td></td><td>P01</td><td>Interm B</td><td>J10</td><td>19</td><td>-0.20</td><td>0.38</td><td>-0.12</td></td<>   | P01          | Base A      | J21        | 15         | 0.13  |       |       |   | P01          | Interm B    | J10        | 19         | -0.20 | 0.38  | -0.12 |
| P01         Base A         J21         16         -0.11         P01         Interm B         J10         20         -0.05         -0.56         -0.57           P01         Binder 1         J02         1         0.00         P01         Interm B         J10         20         -0.23         0.40         -0.12           P01         Binder 1         J02         1         0.10         P01         Interm B         J10         20         -0.23         0.40         -0.12           P01         Binder 1         J02         1         0.10         P01         Interm B         J23         1         0.37         -0.55         0.36           P01         Binder 1         J02         1         0.05         P01         Interm B         J23         1         0.55         -0.92         0.43           P01         Binder 1         J02         1         0.00         P01         Interm B         J23         1         0.18         -0.28         0.19           P01         Binder 1         J02         1         0.38         -0.31         0.50         P01         Interm B         J23         2         -0.27         -0.21         -0.76  | P01          | Base A      | J21        | 16         | -0.07 |       |       |   | P01          | Interm B    | J10        | 20         | -0.37 | -0.09 | -0.83 |
| P01         Binder 1         J02         1         0.00         P01           P01         Binder 1         J02         1         0.10         P01         Interm B         J10         20         -0.23         0.40         -0.12           P01         Binder 1         J02         1         0.10         P01         Interm B         J23         1         0.37         -0.55         0.36           P01         Binder 1         J02         1         0.00         P01         Interm B         J23         1         0.37         -0.55         0.36           P01         Binder 1         J02         1         0.00         P01         Interm B         J23         1         0.55         -0.92         0.43           P01         Binder 1         J02         1         -0.13         -0.10         -0.46         P01         Interm B         J23         1         0.18         -0.28         0.19           P01         Binder 1         J02         2         0.11         -0.62         -0.31         P01         Interm B         J23         2         0.40         -0.30         0.64           P01         Binder 1         J02         2   | P01          | Base A      | J21        | 16         | -0.11 |       |       |   | P01          | Interm B    | J10        | 20         | -0.05 | -0.56 | -0.57 |
| P01         Binder 1         J02         1         0.10         P01           P01         Binder 1         J02         1         0.05         P01         Interm B         J23         1         0.37         -0.55         0.36           P01         Binder 1         J02         1         0.05         P01         Interm B         J23         1         0.55         -0.92         0.43           P01         Binder 1         J02         1         0.00         P01         Interm B         J23         1         0.18         -0.28         0.19           P01         Binder 1         J02         1         -0.13         -0.10         -0.46         P01         Interm B         J23         1         0.04         -0.37         -0.23           P01         Binder 1         J02         2         0.11         -0.62         -0.31         P01         Interm B         J23         2         -0.27         -0.21         -0.76           P01         Binder 1         J02         2         0.40         -1.10         -0.13         P01         Interm B         J23         2         0.40         -0.30         0.64           P01         Binder 1  | P01          | Binder 1    | J02        | 1          | 0.00  |       |       |   | P01          | Interm B    | J10        | 20         | -0.23 | 0.40  | -0.12 |
| P01         Binder 1         J02         1         0.05         P01           P01         Binder 1         J02         1         0.05         P01         Interm B         J23         1         0.55         -0.92         0.43           P01         Binder 1         J02         1         0.00         P01         Interm B         J23         1         0.18         -0.28         0.19           P01         Binder 1         J02         1         -0.13         -0.10         -0.46         P01         Interm B         J23         1         0.18         -0.28         0.19           P01         Binder 1         J02         1         0.38         -0.31         0.50         P01         Interm B         J23         1         0.04         -0.37         -0.23           P01         Binder 1         J02         2         0.11         -0.62         -0.31         P01         Interm B         J23         2         -0.27         -0.21         -0.76           P01         Binder 1         J02         2         0.40         -1.10         -0.13         P01         Interm B         J23         2         -0.38         0.36         -0.53   | P01          | Binder 1    | J02        | 1          | 0.10  |       |       |   | P01          | Interm B    | J23        | 1          | 0.37  | -0.55 | 0.36  |
| P01         Binder 1         J02         1         0.00         P01         Interm B         J23         1         0.18         -0.28         0.19           P01         Binder 1         J02         1         -0.13         -0.10         -0.46         P01         Interm B         J23         1         0.18         -0.28         0.19           P01         Binder 1         J02         1         -0.33         -0.10         -0.46         P01         Interm B         J23         1         0.18         -0.28         0.19           P01         Binder 1         J02         1         0.38         -0.31         0.50         P01         Interm B         J23         1         0.04         -0.37         -0.23           P01         Binder 1         J02         2         0.11         -0.62         -0.31         P01         Interm B         J23         2         -0.27         -0.21         -0.76           P01         Binder 1         J02         2         0.40         -1.10         -0.13         P01         Interm B         J23         2         -0.38         0.36         -0.53           P01         Binder 1         J02         2         0.25  | P01          | Binder 1    | J02        | 1          | 0.05  |       |       | 1 | P01          | Interm B    | J23        | 1          | 0.55  | -0.92 | 0.43  |
| P01         Binder 1         J02         1         -0.13         -0.10         -0.46           P01         Binder 1         J02         1         0.38         -0.31         0.50           P01         Binder 1         J02         1         0.38         -0.31         0.50           P01         Binder 1         J02         2         0.11         -0.62         -0.31           P01         Binder 1         J02         2         0.40         -1.10         -0.13           P01         Binder 1         J02         2         0.40         -1.10         -0.13           P01         Binder 1         J02         2         0.40         -1.10         -0.13           P01         Binder 1         J02         2         0.25         0.82         1.12           P01         Binder 1         J02         3         0.03         -0.44         -0.39           P01         Binder 1         J02         3         0.03         -0.44         -0.39           P01         Interm B         J23         4         0.31         -0.60         0.22   | P01          | Binder 1    | J02        | 1          | 0.00  |       |       | 1 | P01          | Interm B    | J23        | 1          | 0.18  | -0.28 | 0.19  |
| P01         Binder 1         J02         1         0.38         -0.31         0.50           P01         Binder 1         J02         2         0.11         -0.62         -0.31           P01         Binder 1         J02         2         0.11         -0.62         -0.31           P01         Binder 1         J02         2         0.40         -1.10         -0.13           P01         Binder 1         J02         2         0.40         -1.10         -0.13           P01         Binder 1         J02         2         0.25         0.82         1.12           P01         Binder 1         J02         3         0.03         -0.44         -0.39           P01         Binder 1         J02         3         0.03         -0.44         -0.39           P01         Interm B         J23         3         -0.60         0.19           P01         Binder 1         J02         3         0.03         -0.44         -0.39  | P01          | Binder 1    | J02        | 1          | -0.13 | -0.10 | -0.46 |   | P01          | Interm B    | J23        | 1          | 0.04  | -0.37 | -0.23 |
| P01         Binder 1         J02         2         0.11         -0.62         -0.31           P01         Binder 1         J02         2         0.40         -1.10         -0.13           P01         Binder 1         J02         2         0.40         -1.10         -0.13           P01         Binder 1         J02         2         0.25         0.82         1.12           P01         Binder 1         J02         3         0.03         -0.44         -0.39           P01         Binder 1         J02         3         0.03         -0.44         -0.39   | P01          | Binder 1    | J02        | 1          | 0.38  | -0.31 | 0.50  | 1 | P01          | Interm B    | J23        | 2          | -0.27 | -0.21 | -0.76 |
| P01         Binder 1         J02         2         0.40         -1.10         -0.13           P01         Binder 1         J02         2         0.25         0.82         1.12           P01         Binder 1         J02         2         0.25         0.82         1.12           P01         Binder 1         J02         3         0.03         -0.44         -0.39           P01         Interm B         J23         4         0.31         -0.60         0.22  | P01          | Binder 1    | J02        | 2          | 0.11  | -0.62 | -0.31 | 1 | P01          | Interm B    | J23        | 2          | 0.40  | -0.30 | 0.64  |
| P01         Binder 1         J02         2         0.25         0.82         1.12         P01         Interm B         J23         3         -0.06         0.19         0.08           P01         Binder 1         J02         3         0.03         -0.44         -0.39         P01         Interm B         J23         4         0.31         -0.60         0.22   | P01          | Binder 1    | J02        | 2          | 0.40  | -1.10 | -0.13 | 1 | P01          | Interm B    | J23        | 2          | -0.38 | 0.36  | -0.53 |
| P01         Binder 1         J02         3         0.03         -0.44         -0.39         P01         Interm B         J23         4         0.31         -0.60         0.22  | P01          | Binder 1    | J02        | 2          | 0.25  | 0.82  | 1.12  | 1 | P01          | Interm B    | J23        | 3          | -0.06 | 0.19  | 0.08  |
|   | P01          | Binder 1    | J02        | 3          | 0.03  | -0.44 | -0.39 |   | P01          | Interm B    | J23        | 4          | 0.31  | -0.60 | 0.22  |

| Proj.      | Mix              | JMF        | Lot    | AC    | AV    | VMA   | 1 | Proj. | Mix      | JMF        | Lot | AC    | AV    | VMA   |
|------------|------------------|------------|--------|-------|-------|-------|---|-------|----------|------------|-----|-------|-------|-------|
| P01        | Interm B         | 123        | NO.    | -0.20 | -0.21 | -0.80 |   | P01   | Surf C   | 110        | 18  | 0.09  | -1.00 | -0.54 |
| P01        | Interm B         | 122        |        | -0.23 | -0.21 | -0.00 |   | P02   | Base A   | 117        | 10  | 0.03  | -1.00 | -0.34 |
| P01        | Interm B         | 123        | 6      | 0.00  | -0.50 | -0.24 |   | P02   | Base A   | 117        | 1   | -0.10 |       |       |
| P01        | Surf 1C          | 107        | 8      | -0.04 | -0.30 | -0.24 |   | P02   | Base A   | 117        | 1   | -0.13 |       |       |
| P01        | Surf 1C          | 107        | 0      | -0.04 | 0.12  | 0.00  |   | P02   |          | 117        | 2   | -0.17 |       |       |
| P01        | Surf 1C          | 107        | 0<br>8 | 0.20  | -0.30 | -0.25 |   | P02   | Base A   | 117        | 2   | 0.00  |       |       |
| P01        | Surf 1C          | 107        | 0      | -0.18 | -0.20 | -0.20 |   | P02   | Base A   | 117        | 2   | -0.32 |       |       |
| P01        | Surf 1C          | 107        | 10     | -0.10 | -0.54 | -0.93 |   | P02   | Base A   | 117        | 2   | -0.32 |       |       |
| P01        | Surf 1C          | 107        | 10     | -0.21 | -0.54 | -0.33 |   | P02   | Base A   | 117        | 2   | -0.23 |       |       |
| P01        | Surf 1C          | 107        | 10     | 0.10  | -0.04 | -0.12 |   | P02   | Base A   | 117        | 3   | -0.16 |       |       |
| P01        | Surf 1C          | 107        | 11     | -0.34 | 0.20  | -0.11 |   | P02   | Base A   | 117        | 3   | 0.10  |       |       |
| P01        | Surf 1C          | 107        | 11     | -0.34 | 0.59  | -0.41 |   | P02   |          | 117        | 3   | 0.04  |       |       |
| P01        | Surf 1C          | 107        | 11     | -0.25 | 0.34  | -0.10 |   | P02   |          | 117        | 4   | -0.10 |       |       |
| P01        | Surf 1C          | 107        | 11     | -0.29 | 0.07  | 0.14  |   | P02   |          | 117        | 4   | -0.31 |       |       |
| P01        | Surf 1C          | 107        | 11     | -0.10 | 0.70  | 0.40  |   | P02   |          | 117        | 4   | -0.11 |       |       |
|            | Surf 1C          | 107        | 10     | -0.00 | 0.00  | 0.30  |   | F02   | Dase A   | 117        | 5   | 0.30  |       |       |
|            | Surf 1C          | 107        | 12     | 0.20  | -0.03 | -0.11 |   | P02   | Dase A   | J17<br>117 | 5   | 0.13  |       |       |
|            | Sulf 1C          | 107        | 12     | 0.05  | 0.01  | 0.02  |   | F02   | Dase A   | J17        | 5   | -0.40 |       |       |
|            | Sulf 1C          | 107        | 12     | -0.17 | 0.70  | 0.22  |   | F02   | Dase A   | 120        | 0   | 0.16  |       |       |
|            |                  | 307        | 12     | -0.07 | 0.03  | 0.55  |   | F02   | Dase A   | J20        | 1   | 0.05  |       |       |
| P01        | SUILD<br>Suint D | J07        | 4      | -0.04 | 0.79  | 0.63  |   | P02   | Dase A   | J28        | 1   | -0.15 |       |       |
| PUI<br>DO1 | SUILD<br>Curf D  | J07        | 4      | 0.33  | -0.27 | 0.53  |   | P02   | Dase A   | J28        | 1   | 0.26  |       |       |
| PUI<br>DO1 | SUILD<br>Curf D  | J07        | 4      | 0.07  | 0.49  | 0.61  |   | P02   | Dase A   | J28        | 2   | 0.10  |       |       |
| PUI<br>DO1 | SUILD<br>Curf D  | J07        | 5<br>5 | -0.14 | -0.41 | -0.69 |   | P02   | Dase A   | J28        | 2   | 0.02  |       |       |
| PUI        | SUILD            | J07        | 5      | 0.03  | 0.51  | 0.55  |   | P02   | Dase A   | J28        | 2   | 0.09  |       |       |
| P01        | Surf D           | J07        | 5      | 0.15  | 0.77  | 1.04  |   | P02   | Base A   | J28        | 3   | 0.03  |       |       |
| PUI        |                  | J07        | 6      | -0.43 | 0.49  | -0.54 |   | P02   | Dase A   | J28        | 4   | 0.00  |       |       |
| PUT        | Surf D           | J07        | 6      | -0.11 | 1.04  | 0.67  |   | P02   | Base A   | J28        | 5   | -0.37 |       |       |
| P01        | Surf D           | J07        | 6      | 0.18  | 0.20  | 0.59  |   | P02   | Base A   | J28        | 5   | 0.08  |       |       |
| P01        | Surf D           | J07        | 6      | 0.01  | 0.51  | 0.49  |   | P02   | Base A   | J28        | 6   | 0.32  |       |       |
| PUI        |                  | J07        | 0      | 0.09  | 0.45  | 0.63  |   | P02   | Dase A   | J28        | 6   | -0.23 |       |       |
| PUT        | Surf D           | J07        | 7      | -0.05 | 0.50  | 0.34  |   | P02   | Base A   | J28        | 6   | -0.32 |       |       |
| PUT        | Surf D           | J07        | 7      | 0.02  | 0.61  | 0.61  |   | P02   | Base A   | J28        | 6   | 0.30  |       |       |
| PUT        | Surf C           | J07        | /      | 0.14  | 0.62  | 0.87  |   | P02   | Base A   | J28        | 7   | 0.27  |       |       |
| PUI<br>DO1 | Sun C            | J19        | 2      | 0.02  | -0.67 | -0.42 |   | P02   | Dase A   | J28        | 7   | 0.24  |       |       |
|            | Sun C            | J19        | 3      | 0.20  | 0.25  | 0.00  |   | F02   | Dase A   | J20        |     | -0.01 |       |       |
| P01        | Surf C           | J19<br>110 | 4      | -0.06 | -0.92 | -0.80 |   | P02   | Base A   | J28        | 0   | 0.00  |       |       |
|            | Sun C            | J19        | 4      | 0.00  | -0.20 | -0.12 |   | F02   | Dase A   | J20        | 0   | -0.05 |       |       |
| PUI<br>DO1 | Sun C            | J19        | 5<br>5 | -0.04 | -0.77 | -0.00 |   | P02   | Dase A   | J28        | 0   | 0.11  |       |       |
| PUI        | Sun C            | J19        | 5      | -0.15 | -0.07 | -0.27 |   | P02   | Dase A   | J28        | 0   | 0.31  |       |       |
| P01        | Surf C           | J19        | 0      | 0.02  | -1.03 | -0.70 |   | P02   | Base A   | J28        | 9   | 0.13  |       |       |
| PUI        | Sun C            | J19        | /      | 0.14  | -0.29 | 0.28  |   | P02   | Dase A   | J28        | 9   | 0.14  |       |       |
| PUT        | Surf C           | J19        | 8      | 0.14  | 0.76  | 1.13  |   | P02   | Base A   | J28        | 9   | 0.08  |       |       |
| PU1        | Surf C           | J19        | 9      | 0.22  | 0.59  | 1.13  |   | P02   | Dase A   | J20        | 10  | -0.07 |       |       |
| PUT        | Surf C           | J19        | 11     | 0.21  | -0.48 | 0.16  |   | P02   | Base A   | J28        | 11  | -0.18 |       |       |
| PU1        | Surf C           | J19        | 11     | -0.01 | 0.19  | 0.24  |   | P02   | Dase A   | J20        | 11  | -0.22 |       |       |
| PUT        | Sunto            | J19        | 12     | 0.02  | -0.95 | -0.60 |   | P02   | Dase A   | J20        | 11  | -0.16 |       |       |
| P01        | Suff C           | J19        | 13     | 0.01  | -0.05 | 0.20  |   | P02   | Dase A   | J28        | 13  | 0.79  |       |       |
| PU1        | Sunto            | J19        | 10     | -0.03 | -1.05 | -0.81 |   | P02   | Dase A   | J28        | 14  | -0.41 | 0.40  | 0.50  |
| P01        | Surf C           | J19        | 16     | 0.24  | -0.71 | 0.10  |   | P02   | Interm B | JU4        | 1   | 0.17  | 0.12  | 0.59  |
| P01        | Sun C            | J19        | 17     | 0.41  | -1.07 | 0.17  | 1 | P02   | Interm B | J04        | 1   | 0.16  | 0.11  | 0.58  |

Table A.2. Plant Test Results Data (continued)

| Proj.<br>No. | Mix<br>Type | JMF<br>No. | Lot<br>No. | AC    | AV    | VMA   | Proj.<br>No. | Mix<br>Type | JMF<br>No. | Lot<br>No. | AC    | AV    | VMA   |
|--------------|-------------|------------|------------|-------|-------|-------|--------------|-------------|------------|------------|-------|-------|-------|
| P02          | Interm B    | J04        | 1          | 0.03  | -0.03 | 0.11  | P02          | Interm B    | J09        | 15         | 0.21  | 0.40  | 0.96  |
| P02          | Interm B    | J04        | 1          | 0.38  | -0.34 | 0.66  | P02          | Interm B    | J09        | 16         | 0.04  | 0.13  | 0.32  |
| P02          | Interm B    | J04        | 2          | 0.25  | 0.20  | 0.84  | P02          | Interm B    | J09        | 16         | -0.18 | 0.32  | -0.09 |
| P02          | Interm B    | J04        | 3          | 0.00  | -0.44 | -0.32 | P02          | Interm B    | J09        | 16         | 0.03  | -0.74 | -0.55 |
| P02          | Interm B    | J04        | 3          | 0.06  | -0.48 | -0.21 | P02          | Interm B    | J09        | 16         | 0.33  | -0.08 | 0.75  |
| P02          | Interm B    | J04        | 4          | 0.38  | -0.32 | 0.68  | P02          | Interm B    | J09        | 17         | -0.27 | 0.01  | -0.57 |
| P02          | Interm B    | J04        | 4          | 0.12  | -0.52 | -0.11 | P02          | Interm B    | J09        | 17         | -0.19 | -0.60 | -0.92 |
| P02          | Interm B    | J04        | 5          | 0.25  | -0.59 | 0.04  | P02          | Interm B    | J09        | 18         | -0.18 | 0.03  | -0.34 |
| P02          | Interm B    | J04        | 5          | -0.05 | -0.61 | -0.67 | P02          | Interm B    | J09        | 19         | 0.02  | 0.06  | 0.18  |
| P02          | Interm B    | J04        | 5          | 0.27  | -0.80 | -0.08 | P02          | Interm B    | J09        | 19         | -0.12 | -0.08 | -0.32 |
| P02          | Interm B    | J04        | 5          | -0.02 | -0.75 | -0.69 | P02          | Interm B    | J09        | 20         | 0.18  | 0.78  | 1.10  |
| P02          | Interm B    | J04        | 6          | 0.78  | -1.02 | 0.99  | P02          | Interm B    | J09        | 20         | -0.35 | 1.06  | 0.24  |
| P02          | Interm B    | J04        | 7          | -0.14 | -0.35 | -0.53 | P02          | Surf B      | J15        | 2          | 0.32  | 0.42  | 1.12  |
| P02          | Interm B    | J04        | 7          | 0.00  | -0.87 | -0.81 | P02          | Surf B      | J15        | 3          | 0.16  | 0.31  | 0.67  |
| P02          | Interm B    | J04        | 7          | 0.30  | -0.83 | -0.06 | P02          | Surf B      | J15        | 3          | -0.03 | 0.93  | 0.67  |
| P02          | Interm B    | .104       | . 7        | -0.01 | -0.76 | -0.71 | P02          | Surf B      | .115       | 3          | -0.07 | 0.73  | 0.44  |
| P02          | Interm B    | .104       | 8          | 0.36  | 0.05  | 0.95  | P02          | Surf B      | .115       | 3          | -0.06 | 0.78  | 0.53  |
| P02          | Interm B    | .104       | 9          | 0.00  | 0.06  | 1 10  | P02          | Surf B      | .115       | 4          | -0.08 | 0.70  | 0.00  |
| P02          | Interm B    | .104       | 10         | 0.00  | -0.15 | 0.49  | P02          | Surf B      | .115       | 4          | -0.13 | 1.03  | 0.54  |
| P02          | Interm B    | 104        | 10         | -0.16 | 0.10  | -0.04 | P02          | Surf B      | 115        | -т<br>Д    | -0.26 | 1.00  | 0.04  |
| P02          | Interm B    | 104        | 11         | 0.10  | -0.72 | -0.04 | P02          | Surf B      | 115        | 4          | -0.20 | 0.72  | 0.30  |
| P02          | Interm B    | 104        | 11         | -0.15 | -0.72 | 0.17  | P02          | Surf B      | 115        | 5          | -0.13 | 0.72  | 0.14  |
| P02          | Interm B    | 104        | 11         | -0.13 | 0.40  | 0.11  | P02          | Surf B      | 115        | 5          | -0.00 | 0.70  | 0.07  |
| F 02         | Interm B    | 104        | 12         | 0.03  | -0.32 | -0.19 | P02          | Sulf B      | 115        | 5          | -0.21 | 0.00  | 0.07  |
| P02          |             | J04        | 12         | 0.21  | 0.20  | 0.62  | P02          |             | J15        | 5          | -0.12 | 0.99  | 0.60  |
| P02          | Interm B    | J04        | 13         | -0.09 | 0.83  | 0.62  | P02          | Surf D      | J 15       | 5<br>5     | 0.14  | 0.84  | 1.04  |
| P02          |             | J04        | 14         | 0.00  | 0.57  | 0.77  | P02          | Sull D      | J15        | 5          | 0.40  | 0.07  | 1.03  |
| P02          |             | J04        | 14         | -0.32 | 1.04  | 0.30  | P02          | SUIL D      | J 15       | 0          | -0.26 | -0.46 | -1.03 |
| P02          |             | J04        | 14         | 0.02  | 1.12  | 1.14  | P02          | SUIL D      | J 15       | 0          | -0.10 | 0.80  | 0.52  |
| P02          |             | J09        | 1          | 0.22  | -0.20 | 0.40  | P02          | SUIL D      | J15        | 0          | 0.07  | 0.09  | 0.21  |
| P02          |             | J09        | 2          | -0.02 | 0.72  | 0.79  | P02          |             | J15        | 1          | 0.20  | -1.07 | -0.52 |
| P02          | Interm B    | J09        | 2          | 0.08  | 0.13  | 0.40  | P02          | Sur C       | J05        | 1          | 0.01  | 0.67  | 0.66  |
| P02          | Interm B    | J09        | 3          | 0.43  | -0.84 | 0.15  | P02          | Sun C       | J05        | 1          | -0.02 | 0.32  | 0.29  |
| P02          | Interm B    | J09        | 4          | 0.54  | -0.39 | 0.92  | P02          | Surf C      | J05        | 2          | -0.07 | 0.63  | 0.45  |
| P02          | Interm B    | J09        | 4          | -0.12 | 0.06  | -0.14 | P02          | Surf C      | J05        | 3          | -0.04 | 0.06  | 0.01  |
| P02          | Interm B    | J09        | 4          | 0.45  | -1.09 | 0.14  | P02          | Surf C      | J05        | 3          | 0.11  | -0.48 | -0.09 |
| P02          | Interm B    | J09        | 5          | 0.11  | -0.35 | -0.03 | P02          | Surf C      | J05        | 4          | -0.12 | 0.45  | 0.22  |
| P02          | Interm B    | J09        | 5          | -0.29 | 0.12  | -0.52 | P02          | Surf C      | J05        | 5          | -0.19 | 0.87  | 0.45  |
| P02          | Interm B    | J09        | 6          | 0.24  | -0.17 | 0.44  | P02          | Suff C      | J05        | 6          | 0.28  | 0.13  | 0.83  |
| P02          | Interm B    | J09        | 6          | 0.06  | 0.54  | 0.66  | P02          | Suff C      | J13        | 1          | 0.19  | 0.33  | 0.66  |
| P02          | Interm B    | J09        | 7          | -0.45 | -0.39 | -1.35 | P02          | Surf C      | J13        | 2          | -0.02 | -0.08 | -0.23 |
| P02          | Interm B    | J09        | 8          | 0.10  | 0.14  | 0.44  | P02          | Surf C      | J13        | 3          | 0.21  | 0.81  | 1.15  |
| P02          | Interm B    | J09        | 9          | -0.07 | -0.81 | -0.80 | P02          | Surf C      | J13        | 3          | 0.22  | 0.58  | 0.97  |
| P02          | Interm B    | J09        | 9          | -0.18 | -0.81 | -1.00 | P02          | Surf C      | J13        | 5          | 0.18  | 0.88  | 1.06  |
| P02          | Interm B    | J09        | 10         | 0.31  | 0.17  | 0.96  | P02          | Surf C      | J13        | 6          | -0.18 | 0.90  | 0.28  |
| P02          | Interm B    | J09        | 10         | 0.10  | -0.36 | -0.01 | P02          | Surf C      | J13        | 7          | 0.39  | -0.43 | 0.39  |
| P02          | Interm B    | J09        | 10         | 0.31  | -0.81 | 0.10  | P02          | Surf C      | J13        | 8          | -0.25 | 0.98  | 0.19  |
| P02          | Interm B    | J09        | 13         | -0.15 | -0.31 | -0.52 | P02          | Surf C      | J13        | 8          | -0.41 | 0.53  | -0.40 |
| P02          | Interm B    | J09        | 13         | -0.13 | 0.28  | 0.08  | P02          | Surf C      | J13        | 9          | -0.35 | 0.35  | -0.60 |
| P02          | Interm B    | J09        | 14         | -0.34 | -0.34 | -0.97 | P02          | Surf C      | J13        | 11         | -0.33 | -0.11 | -0.76 |
| P02          | Interm B    | J09        | 14         | 0.02  | 0.32  | 0.47  | P02          | Surf C      | J13        | 12         | -0.17 | 0.67  | 0.18  |

| Proj. | Mix      | JMF | Lot | AC    | AV    | VMA   | Proj. | Mix      | JMF | Lot | AC    | AV    | VMA   |
|-------|----------|-----|-----|-------|-------|-------|-------|----------|-----|-----|-------|-------|-------|
| No.   | Туре     | No. | No. |       |       |       | No.   | Туре     | No. | No. |       |       |       |
| P02   | Surf C   | J13 | 13  | 0.00  | 0.55  | 0.38  | P05   | Interm C | J27 | 11  | -0.22 | 0.52  | 0.13  |
| P02   | Surf C   | J13 | 14  | -0.36 | 0.74  | -0.18 | P05   | Interm C | J27 | 11  | -0.16 | 0.46  | 0.17  |
| P02   | Surf C   | J13 | 14  | -0.58 | 0.66  | -0.69 | P05   | Interm C | J27 | 12  | -0.16 | -0.22 | -0.47 |
| P02   | Surf C   | J13 | 15  | 0.06  | 0.60  | 0.64  | P05   | Interm C | J27 | 12  | -0.02 | -0.75 | -0.71 |
| P02   | Surf C   | J13 | 15  | -0.06 | 1.14  | 0.97  | P05   | Interm C | J27 | 13  | -0.06 | 0.06  | 0.02  |
| P02   | Surf C   | J13 | 16  | 0.43  | -0.87 | 0.18  | P05   | Interm C | J27 | 13  | -0.12 | 0.22  | 0.02  |
| P04   | Binder 1 | J08 | 11  | 0.11  |       |       | P05   | Interm C | J27 | 14  | -0.14 | 0.12  | -0.11 |
| P04   | Binder 1 | J08 | 11  | 0.01  |       |       | P05   | Interm C | J27 | 15  | -0.10 | 0.89  | 0.67  |
| P04   | Binder 1 | J08 | 12  | -0.05 |       |       | P05   | Interm C | J27 | 15  | -0.39 | 0.43  | -0.41 |
| P04   | Binder 1 | J08 | 12  | 0.42  |       |       | P05   | Surf D   | J25 | 1   | -0.41 | -0.68 | -1.40 |
| P04   | Binder 1 | J08 | 13  | 0.53  |       |       | P05   | Surf D   | J25 | 2   | -0.02 | 0.05  | 0.03  |
| P04   | Binder 1 | J08 | 14  | -0.04 |       |       | P05   | Surf D   | J25 | 3   | -0.11 | -0.07 | -0.27 |
| P04   | Binder 1 | J08 | 14  | -0.08 |       |       | P05   | Surf D   | J25 | 4   | -0.11 | -0.85 | -0.99 |
| P04   | Binder 1 | J08 | 15  | -0.43 |       |       | P05   | Surf D   | J25 | 5   | -0.25 | 0.10  | -0.37 |
| P04   | Binder 1 | J08 | 15  | 0.22  |       |       | P05   | Surf D   | J25 | 6   | 0.21  | 0.58  | 1.00  |
| P04   | Binder 1 | J08 | 16  | 0.22  |       |       | P05   | Surf D   | J25 | 8   | -0.13 | 0.46  | 0.14  |
| P04   | Binder 1 | J08 | 16  | 0.42  |       |       | P05   | Surf D   | J25 | 9   | -0.23 | 0.50  | 0.09  |
| P04   | Binder 1 | J08 | 17  | -0.50 | 0.16  | -1.11 | P05   | Surf E   | J40 | 2   | -0.20 |       |       |
| P04   | Binder 1 | J08 | 17  | 0.39  | -0.20 | 0.65  | P05   | Surf E   | J40 | 2   | -0.43 |       |       |
| P04   | Binder 1 | J08 | 18  | 0.38  | -0.65 | 0.28  | P05   | Surf E   | J40 | 2   | 0.04  |       |       |
| P04   | Binder 1 | J08 | 18  | 0.36  | 0.43  | 1.13  | P05   | Surf E   | J40 | 3   | -0.19 |       |       |
| P04   | Binder 1 | J08 | 19  | 0.14  | 0.31  | 0.52  | P05   | Surf E   | J40 | 3   | -0.10 |       |       |
| P04   | Binder 1 | J08 | 19  | 0.50  | 0.11  | 1.20  | P05   | Surf E   | J40 | 3   | -0.05 |       |       |
| P04   | Binder 1 | J08 | 20  | 0.74  | -0.14 | 1.52  | P05   | Surf E   | J40 | 4   | -0.32 |       |       |
| P04   | Binder 1 | J08 | 20  | 0.19  | 0.35  | 0.65  | P05   | Surf E   | J40 | 5   | -0.07 |       |       |
| P04   | Binder 1 | J08 | 21  | 0.12  | -0.04 | 0.15  | P05   | Surf E   | J40 | 6   | 0.11  |       |       |
| P04   | Binder 1 | J08 | 21  | 0.13  | 1.00  | 1.08  | P06   | Surf 1D  | J24 | 1   | -0.09 | 0.09  | -0.02 |
| P04   | Surf 1R  | J14 | 1   | -0.28 | 0.61  | 0.00  | P06   | Surf 1D  | J24 | 1   | -0.18 | -0.40 | -0.66 |
| P04   | Surf 1R  | J14 | 1   | 0.02  | 0.66  | 0.78  | P06   | Surf 1D  | J24 | 1   | -0.19 | -0.46 | -0.80 |
| P04   | Surf 1R  | J14 | 1   | -0.11 | 0.59  | 0.35  | P06   | Surf 1D  | J24 | 2   | 0.00  | -0.84 | -0.79 |
| P04   | Surf 1R  | J14 | 2   | 0.32  | -0.69 | 0.13  | P06   | Surf 1D  | J24 | 2   | -0.01 | -0.09 | -0.13 |
| P04   | Surf 1R  | J14 | 2   | 0.01  | -0.35 | -0.38 | P06   | Surf 1D  | J24 | 2   | 0.39  | -0.55 | 0.36  |
| P04   | Surf 1R  | J14 | 2   | 0.03  | 0.61  | 0.89  | P06   | Surf 1D  | J24 | 3   | 0.03  | -0.18 | -0.08 |
| P04   | Surf 1R  | J14 | 2   | -0.05 | -0.12 | -0.36 | P06   | Surf 1D  | J24 | 3   | 0.21  | -0.77 | -0.20 |
| P04   | Surf 1R  | J14 | 3   | 0.32  | 0.46  | 1.10  | P06   | Surf 1D  | J24 | 3   | 0.17  | -0.53 | -0.14 |
| P04   | Surf 1R  | J14 | 3   | -0.24 | 0.68  | 0.06  | P06   | Surf 1D  | J24 | 4   | 0.17  | 0.35  | 0.97  |
| P04   | Surf 1R  | J14 | 3   | 0.19  | 0.68  | 1.00  | P06   | Surf 1D  | J24 | 4   | 0.08  | -1.03 | -0.73 |
| P04   | Surf 1R  | J14 | 3   | 0.17  | 0.73  | 1.01  | P06   | Surf 1D  | J24 | 4   | 0.11  | 0.31  | -0.08 |
| P04   | Surf 1R  | J14 | 4   | -0.14 | 0.98  | 0.53  | P06   | Surf 1D  | J24 | 5   | 0.28  | -0.81 | -0.06 |
| P04   | Surf 1R  | J14 | 4   | 0.31  | -0.02 | 0.64  | P06   | Surf 1D  | J24 | 5   | 0.14  | -0.27 | 0.09  |
| P04   | Surf 1R  | J14 | 4   | 0.05  | 0.04  | 0.06  | P06   | Surf 1D  | J24 | 5   | -0.14 | -0.68 | -0.88 |
| P04   | Surf 1R  | J14 | 5   | 0.09  | -0.69 | -0.41 | P07   | Surf 3   | J30 | 1   | -0.04 | 0.57  | 0.46  |
| P04   | Surf 1R  | J14 | 5   | 0.31  | -0.02 | 0.64  | P07   | Surf 3   | J30 | 1   | -0.06 | 0.28  | 0.23  |
| P04   | Surf 1R  | J14 | 5   | 0.05  | 0.00  | 0.02  | P07   | Surf 3   | J30 | 1   | -0.12 | 0.57  | 0.40  |
| P05   | Interm C | J27 | 8   | 0.06  | 0.06  | 0.31  | P07   | Surf 3   | J30 | 2   | -0.06 | 0.28  | 0.23  |
| P05   | Interm C | J27 | 8   | -0.32 | 0.32  | -0.28 | P07   | Surf 3   | J30 | - 3 | -0.17 | 0.24  | 0.02  |
| P05   | Interm C | J27 | 9   | -0.02 | 0.59  | 0.63  | P07   | Surf 3   | J30 | 4   | -0.12 | 0.76  | 0.59  |
| P05   | Interm C | J27 | 9   | -0.05 | 0.03  | 0.06  | P07   | Surf 3   | J30 | 5   | -0.06 | -0.37 | -0.27 |
| P05   | Interm C | J27 | 10  | 0.07  | 0.48  | 0.72  | P07   | Surf 3   | J30 | 5   | 0.54  | -0.49 | 0.92  |
| P05   | Interm C | J27 | 10  | -0.15 | 0.28  | 0.02  | P07   | Surf 3   | J30 | 5   | -0.30 | 0.50  | -0.05 |

| Table A.2. | Plant | Test | Results | Data | (continued) |
|------------|-------|------|---------|------|-------------|
|------------|-------|------|---------|------|-------------|

| Proj. | Mix      | JMF  | Lot | AC    | AV    | VMA   |   | Proj. | Mix      | JMF  | Lot | AC    | AV    | VMA   |
|-------|----------|------|-----|-------|-------|-------|---|-------|----------|------|-----|-------|-------|-------|
| NO.   | Туре     | NO.  | NO. | 0.00  | 0.40  | 0.05  |   | NO.   | Туре     | NO.  | NO. | 0.50  | 0.04  | 4.04  |
| P07   | Suff 3   | J30  | 5   | 0.08  | -0.12 | 0.25  |   | P10   | Interm C | J31  | 3   | 0.52  | -0.21 | 1.01  |
| P07   | Suff 3   | J30  | 6   | -0.03 | 0.07  | 0.14  |   | P10   | Interm C | J31  | 3   | 0.08  | 0.50  | 0.77  |
| P07   | Suff 3   | J30  | 6   | -0.09 | 0.39  | 0.31  |   | P10   | Interm C | J31  | 5   | 0.19  | 0.34  | 0.77  |
| P07   | Suff 3   | J30  | /   | 0.00  | -1.06 | -0.75 |   | P10   | Interm C | J31  | 5   | -0.28 | 0.49  | -0.16 |
| P07   | Surf 3   | J30  | 7   | -0.02 | -0.24 | -0.09 |   | P10   | Interm C | J31  | 6   | -0.08 | 0.45  | 0.32  |
| P07   | Surf 3   | J30  | 8   | -0.15 | 0.23  | 0.07  |   | P10   | Interm C | J31  | 6   | -0.50 | 0.75  | -0.38 |
| P07   | Surf 3   | J30  | 9   | -0.20 | 0.32  | 0.01  |   | P10   | Interm C | J31  | 7   | -0.03 | 1.02  | 1.00  |
| P07   | Surf 3   | J30  | 9   | -0.13 | 0.24  | 0.09  |   | P10   | Interm C | J31  | 8   | 0.05  | 0.74  | 0.90  |
| P07   | Surf 3   | J30  | 9   | -0.05 | -0.47 | -0.34 |   | P10   | Interm C | J31  | 8   | -0.31 | 0.64  | -0.05 |
| P07   | Surf 3   | J30  | 10  | -0.17 | -0.91 | -1.01 |   | P10   | Interm C | J31  | 9   | 0.15  | -0.23 | 0.21  |
| P07   | Surf 3   | J30  | 10  | -0.11 | -0.23 | -0.26 |   | P10   | Interm C | J31  | 9   | 0.00  | 0.28  | 0.34  |
| P07   | Surf 3   | J30  | 10  | 0.08  | -0.16 | 0.20  |   | P10   | Interm C | J31  | 10  | 0.41  | -0.07 | 0.90  |
| P07   | Surf 3   | J30  | 11  | -0.09 | 0.05  | -0.08 |   | P10   | Interm C | J31  | 11  | 0.27  | -0.54 | 0.18  |
| P07   | Surf 3   | J30  | 11  | -0.09 | 0.28  | 0.16  |   | P10   | Interm C | J31  | 11  | -0.07 | 0.78  | 0.64  |
| P07   | Surf 3   | J30  | 11  | 0.10  | 0.60  | 0.90  |   | P10   | Interm C | J31  | 12  | -0.40 | 0.98  | 0.11  |
| P07   | Surf 3   | J30  | 12  | -0.19 | -0.65 | -0.83 |   | P10   | Interm C | J31  | 12  | -0.37 | 0.94  | 0.14  |
| P07   | Surf 3   | J30  | 12  | -0.12 | 0.45  | 0.29  |   | P10   | Interm C | J31  | 13  | 0.01  | 0.70  | 0.68  |
| P07   | Surf 3   | J30  | 12  | -0.24 | 0.74  | 0.26  |   | P10   | Interm C | J31  | 13  | -0.02 | 0.95  | 0.90  |
| P07   | Surf 3   | J30  | 13  | -0.13 | -0.34 | -0.43 |   | P10   | Interm C | J31  | 14  | 0.13  | 1.06  | 1.27  |
| P07   | Surf 3   | J30  | 13  | -0.01 | -0.85 | -0.60 |   | P10   | Interm C | J31  | 14  | 0.06  | 0.41  | 0.56  |
| P07   | Surf 3   | J30  | 14  | -0.14 | -0.74 | -0.76 |   | P10   | Interm C | J31  | 15  | 0.14  | 0.38  | 0.71  |
| P07   | Surf 3   | J30  | 14  | -0.28 | 0.58  | 0.07  |   | P10   | Interm C | J31  | 15  | 0.22  | 0.41  | 0.92  |
| P07   | Surf 3   | J30  | 14  | -0.21 | -0.13 | -0.39 |   | P10   | Interm C | J31  | 16  | 0.33  | 0.25  | 1.00  |
| P07   | Surf 3   | J30  | 15  | -0.22 | -0.19 | -0.49 |   | P10   | Interm C | J31  | 16  | -0.24 | 0.47  | -0.07 |
| P07   | Surf 3   | J30  | 15  | -0.23 | -0.06 | -0.34 |   | P10   | Interm C | J31  | 17  | 0.29  | 0.47  | 1.10  |
| P07   | Surf 3   | J30  | 15  | -0.19 | -0.21 | -0.43 |   | P10   | Interm C | J31  | 17  | -0.39 | 1.12  | 0.19  |
| P07   | Surf 3   | .130 | 16  | -0.08 | 0.36  | 0.32  |   | P10   | Interm C | .131 | 18  | -0.14 | 0.86  | 0.53  |
| P07   | Surf 3   | .130 | 17  | -0.11 | -0.78 | -0.73 |   | P10   | Interm C | .131 | 18  | -0.17 | 0.00  | 0.55  |
| P07   | Surf 3   | .130 | 17  | -0.23 | 0.70  | 0.06  |   | P10   | Interm C | .131 | 19  | 0.03  | 0.02  | 0.00  |
| P07   | Surf 3   | 130  | 18  | -0.25 | 0.47  | 0.00  |   | P10   | Interm C | 131  | 10  | 0.00  | -0.07 | 1.06  |
| P07   | Surf 3   | 130  | 10  | 0.23  | 0.75  | 0.00  |   | P10   | Interm C | 131  | 28  | 0.40  | 0.07  | 1.00  |
| P00   | Surf CM  | 135  | 13  | 0.13  | 1.04  | 1 17  |   | P10   | Interm C | 131  | 20  | -0.37 | 0.27  | -0.68 |
| P09   | Surf CM  | 135  | 1   | -0.12 | 0.59  | 0.25  |   | P10   | Interm C | 131  | 20  | -0.37 | -0.07 | -0.00 |
| P09   | Surf CM  | 125  | 1   | -0.13 | 0.59  | 0.23  |   | P10   |          | 121  | 29  | -0.14 | -0.07 | -0.37 |
| P09   | Surf CM  | 125  | 2   | -0.33 | 0.55  | -0.10 |   | P10   |          | 121  | 29  | -0.11 | 0.04  | 0.40  |
| F 09  | Surf CM  | 135  | 2   | 0.00  | -0.41 | -0.19 |   | P10   | Interm C | 121  | 30  | -0.08 | 0.90  | 0.09  |
| P09   | Surf CM  | 135  | 2   | 0.02  | -0.04 | 0.01  |   | P10   | Interm C | 121  | 30  | 0.02  | 0.55  | 0.57  |
| P09   |          | 135  | 2   | 0.04  | -0.13 | 0.01  |   | P10   |          | J31  | 31  | 0.41  | -0.02 | 0.90  |
| P09   | Suff CM  | J35  | 3   | 0.04  | 0.56  | 0.57  |   | P10   | Interm C | J31  | 31  | -0.29 | -0.20 | -0.82 |
| P09   | SUITCM   | J35  | 3   | 0.10  | -0.18 | 0.06  |   | P10   | Interm C | J31  | 32  | 0.34  | -0.14 | 0.65  |
| P09   | Suff CM  | J35  | 3   | -0.10 | 0.66  | 0.37  |   | P10   | Interm C | J31  | 33  | 0.43  | -0.24 | 0.70  |
| P09   | Suff CM  | J83  | 1   | -0.10 | -0.17 | -0.30 |   | P10   | Interm C | J31  | 33  | -0.31 | 0.39  | -0.38 |
| P09   | Surf CM  | J83  | 1   | -0.40 | 0.40  | -0.45 |   | P10   | Interm C | J31  | 34  | -0.15 | -0.36 | -0.70 |
| P09   | Surf CM  | J83  | 1   | 0.18  | 0.39  | 0.71  |   | P10   | Interm C | J31  | 34  | 0.15  | -1.07 | -0.74 |
| P09   | Surf CM  | J83  | 2   | -0.04 | 0.17  | 0.10  |   | P10   | Interm C | J31  | 35  | 0.09  | -0.62 | -0.37 |
| P09   | Surf CM  | J83  | 2   | 0.15  | -0.85 | -0.40 |   | P10   | Interm C | J31  | 35  | -0.42 | -0.15 | -1.09 |
| P09   | Surf CM  | J83  | 2   | -0.18 | -0.84 | -1.09 | l | P10   | Interm C | J31  | 36  | -0.05 | 0.45  | 0.34  |
| P09   | Surf CM  | J83  | 3   | 0.00  | -1.04 | -0.90 |   | P10   | Interm C | J31  | 36  | 0.16  | -0.38 | 0.02  |
| P09   | Surf CM  | J83  | 3   | 0.06  | -0.54 | -0.32 |   | P10   | Interm C | J31  | 37  | 0.07  | -0.64 | -0.42 |
| P10   | Interm C | J31  | 2   | -0.18 | -0.80 | -1.09 |   | P10   | Interm C | J31  | 38  | -0.43 | 0.15  | -0.80 |
| P10   | Interm C | J31  | 2   | 0.11  | -0.68 | -0.37 |   | P10   | Interm C | J31  | 38  | -0.02 | -1.04 | -1.02 |

| Proj. | Mix      | JMF        | Lot | AC    | AV    | VMA   | Proj. | Mix      | JMF | Lot    | AC    | AV    | VMA   |
|-------|----------|------------|-----|-------|-------|-------|-------|----------|-----|--------|-------|-------|-------|
| NO.   | I ype    | NO.        | NO. | 0.17  | 0.65  | 0.17  | NO.   | I ype    | NO. | NO.    | 0.00  | 0.44  | 0.00  |
| P10   |          | J31        | 39  | 0.17  | -0.65 | -0.17 | P10   |          | J82 | 2      | -0.22 | 0.44  | -0.08 |
| P10   |          | J31        | 39  | -0.19 | -0.63 | -1.05 | P10   |          | J82 | 3      | 0.00  | 0.95  | 0.80  |
| P10   | Interm C | J31<br>121 | 40  | 0.00  | 0.49  | 0.50  | P10   | Interm C | 102 | 3      | 0.25  | 0.79  | 1.30  |
| P10   |          | J31        | 40  | 0.16  | -0.06 | 0.29  | P10   |          | J82 | 4      | 0.11  | 1.05  | 1.24  |
| P10   | Interm C | J31        | 41  | -0.52 | 1.09  | -0.03 | P10   | Interm C | J82 | 4      | -0.06 | 1.17  | 1.01  |
| P10   |          | J31        | 41  | 0.06  | 0.05  | 0.23  | P10   |          | J82 | 5<br>5 | -0.21 | 0.92  | 0.26  |
| P10   | Interm C | J31        | 42  | 0.03  | 1.03  | 1.13  | P10   | Interm C | J82 | 5      | 0.00  | 0.59  | 0.50  |
| P10   |          | J31        | 42  | 0.09  | -0.05 | 0.18  | P10   |          | J82 | 6      | 0.09  | 0.82  | 1.01  |
| P10   | Interm C | J31        | 43  | 0.10  | 0.67  | 0.97  | P10   | Interm C | J82 | 7      | 0.23  | 0.73  | 1.14  |
| P10   | Interm C | J31        | 43  | -0.12 | -0.35 | -0.57 | P10   | Interm C | J82 | 1      | 0.29  | 0.82  | 1.39  |
| P10   | Interm C | J31        | 44  | 0.27  | 0.38  | 0.98  | P10   | Interm C | J82 | 14     | -0.24 | 0.86  | 0.25  |
| P10   | Interm C | J31        | 44  | 0.02  | -0.22 | -0.17 | P10   | Interm C | J82 | 14     | -0.10 | 1.06  | 0.75  |
| P10   | Interm C | J31        | 45  | 0.23  | 0.50  | 0.97  | P10   | Surf 4   | J12 | 1      | 0.54  | -0.37 | 0.71  |
| P10   | Interm C | J31        | 45  | 0.13  | 0.32  | 0.58  | P10   | Surf 4   | J12 | 2      | 0.03  | 0.55  | 0.69  |
| P10   | Interm C | J31        | 46  | 0.10  | -0.36 | -0.10 | P10   | Surf 4   | J12 | 3      | 0.33  | 0.29  | 0.94  |
| P10   | Interm C | J31        | 46  | 0.35  | -0.67 | 0.16  | P10   | Surf 4   | J12 | 4      | 0.30  | 0.53  | 1.05  |
| P10   | Interm C | J31        | 47  | 0.01  | -0.26 | -0.18 | P10   | Surf 4   | J12 | 4      | 0.15  | 0.88  | 1.09  |
| P10   | Interm C | J31        | 47  | -0.51 | 0.28  | -0.88 | P10   | Surf 4   | J12 | 5      | -0.32 | 0.96  | 0.16  |
| P10   | Interm C | J31        | 48  | 0.14  | -0.81 | -0.40 | P10   | Surf 4   | J12 | 6      | -0.29 | 1.04  | 0.32  |
| P10   | Interm C | J31        | 48  | 0.40  | -0.10 | 0.94  | P10   | Surf 4   | J12 | 7      | -0.23 | 0.01  | -0.47 |
| P10   | Interm C | J31        | 49  | 0.36  | -0.93 | 0.03  | P10   | Surf 4   | J12 | 9      | -0.32 | -0.14 | -0.75 |
| P10   | Interm C | J31        | 49  | -0.40 | 0.42  | -0.47 | P10   | Surf 4   | J12 | 10     | -0.21 | 2.41  | 1.63  |
| P10   | Interm C | J31        | 50  | 0.36  | -0.24 | 0.61  | P10   | Surf 4   | J12 | 10     | 0.35  | 0.21  | 1.03  |
| P10   | Interm C | J31        | 50  | -0.17 | -0.12 | -0.46 | P10   | Surf 4   | J12 | 11     | 0.05  | 0.22  | 0.22  |
| P10   | Interm C | J31        | 51  | 0.04  | 0.32  | 0.37  | P10   | Surf 4   | J12 | 11     | -0.01 | 0.01  | -0.09 |
| P10   | Interm C | J37        | 1   | 0.14  | 0.85  | 0.87  | P10   | Surf 4   | J12 | 12     | -0.25 | 0.41  | -0.27 |
| P10   | Interm C | J37        | 2   | -0.01 | 0.14  | -0.12 | P10   | Surf 4   | J12 | 12     | -0.17 | 0.46  | -0.07 |
| P10   | Interm C | J37        | 2   | -0.02 | -0.11 | -0.39 | P10   | Surf 4   | J12 | 13     | -0.22 | 0.41  | -0.20 |
| P10   | Interm C | J37        | 3   | 0.22  | -0.54 | -0.24 | P10   | Surf 4   | J12 | 13     | -0.28 | 0.06  | -0.64 |
| P10   | Interm C | J37        | 3   | 0.03  | 0.00  | -0.11 | P10   | Surf 4   | J12 | 16     | -0.33 | 0.30  | -0.55 |
| P10   | Interm C | J37        | 4   | -0.30 | 0.62  | -0.31 | P10   | Surf 4   | J12 | 16     | 0.17  | -0.35 | -0.07 |
| P10   | Interm C | J37        | 4   | 0.01  | 0.62  | 0.35  | P11   | Surf C   | J41 | 1      | -0.25 | 0.99  | 0.29  |
| P10   | Interm C | J37        | 5   | 0.15  | 0.80  | 0.87  | P11   | Surf C   | J41 | 1      | -0.13 | 0.23  | -0.04 |
| P10   | Interm C | J37        | 5   | -0.29 | 0.41  | -0.49 | P11   | Surf C   | J41 | 1      | 0.06  | 0.50  | 0.62  |
| P10   | Interm C | J37        | 6   | 0.26  | 0.32  | 0.65  | P11   | Surf C   | J41 | 2      | 0.03  | 0.19  | 0.29  |
| P10   | Interm C | J37        | 7   | 0.05  | 0.83  | 0.64  | P11   | Surf C   | J41 | 3      | 0.20  | -0.55 | -0.04 |
| P10   | Interm C | J37        | 7   | 0.31  | 0.42  | 0.87  | P11   | Surf C   | J41 | 3      | 0.26  | -0.09 | 0.54  |
| P10   | Interm C | J37        | 8   | 0.38  | 0.18  | 2.80  | P11   | Surf C   | J41 | 4      | 0.26  | -0.09 | 0.54  |
| P10   | Interm C | J37        | 8   | -0.01 | 0.55  | 0.26  | P11   | Surf C   | J41 | 4      | 0.03  | 0.01  | 0.16  |
| P10   | Interm C | J37        | 9   | 0.17  | 0.85  | 0.90  | P11   | Surf C   | J41 | 4      | 0.21  | -0.12 | 0.49  |
| P10   | Interm C | J37        | 9   | 0.00  | 0.73  | 0.41  | P11   | Surf C   | J41 | 4      | 0.04  | -0.01 | 0.18  |
| P10   | Interm C | J37        | 10  | -0.21 | 0.92  | 0.11  | P12   | Surf C   | J38 | 1      | -0.29 | -0.22 | -0.87 |
| P10   | Interm C | J37        | 10  | -0.25 | 0.79  | -0.11 | P12   | Surf C   | J38 | 1      | -0.01 | -0.45 | -0.50 |
| P10   | Interm C | J37        | 11  | 0.15  | 0.87  | 0.87  | P12   | Surf C   | J38 | 1      | -0.11 | -0.84 | -1.00 |
| P10   | Interm C | J37        | 11  | 0.22  | 0.68  | 0.88  | P12   | Surf C   | J38 | 1      | 0.18  | -0.90 | -0.41 |
| P10   | Interm C | J37        | 12  | -0.17 | 0.85  | 0.13  | P12   | Surf C   | J38 | 2      | 0.32  | -2.28 | -1.38 |
| P10   | Interm C | J37        | 12  | -0.28 | 0.94  | 0.00  | P12   | Surf C   | J38 | 2      | 0.22  | -1.44 | -0.79 |
| P10   | Interm C | J82        | 1   | -0.25 | 0.14  | -0.36 | P12   | Surf C   | J38 | 3      | 0.20  | -1.42 | -0.81 |
| P10   | Interm C | J82        | 1   | -0.29 | 0.38  | -0.34 | P12   | Surf C   | J38 | 4      | -0.13 | -0.56 | -0.77 |
| P10   | Interm C | J82        | 2   | -0.07 | 1.05  | 0.83  | P12   | Surf C   | J38 | 5      | -0.05 | -0.48 | -0.53 |

| Table A.2. | Plant | Test | Results | Data | (continued) |
|------------|-------|------|---------|------|-------------|
|------------|-------|------|---------|------|-------------|

| Proj. | Mix    | JMF | Lot | ۸С    | ۸٧    | VMA   | 1 | Proj. | Mix      | JMF | Lot | ۸С    | ۸V    | VMA   |
|-------|--------|-----|-----|-------|-------|-------|---|-------|----------|-----|-----|-------|-------|-------|
| No.   | Туре   | No. | No. | ~~    | ~     | VINA  |   | No.   | Туре     | No. | No. | 70    | ~     | VINA  |
| P12   | Surf C | J38 | 5   | 0.01  | -0.04 | 0.05  |   | P14   | Surf C   | J16 | 7   | 0.13  | -0.59 | -0.14 |
| P12   | Surf C | J38 | 5   | 0.17  | -0.13 | 0.30  |   | P14   | Surf C   | J16 | 7   | -0.03 | -1.22 | -1.04 |
| P12   | Surf C | J38 | 8   | 0.28  | 0.58  | 1.13  |   | P14   | Surf C   | J16 | 7   | -0.22 | 0.64  | 0.17  |
| P12   | Surf C | J38 | 8   | 0.04  | -1.03 | -0.82 |   | P14   | Surf C   | J16 | 8   | 0.05  | -0.95 | -0.66 |
| P12   | Surf C | J38 | 8   | -0.08 | 0.21  | 0.05  |   | P14   | Surf C   | J16 | 8   | -0.05 | -0.87 | -0.80 |
| P13   | Surf C | J03 | 2   | -0.17 | -0.54 | -0.74 |   | P14   | Surf C   | J16 | 8   | -0.07 | -0.62 | -0.64 |
| P13   | Surf C | J03 | 2   | 0.10  | -1.09 | -0.56 |   | P14   | Surf C   | J16 | 10  | -0.16 | -2.21 | -2.25 |
| P13   | Surf C | J03 | 2   | 0.16  | -1.01 | -0.36 |   | P14   | Surf C   | J16 | 10  | -0.30 | -0.25 | -0.79 |
| P13   | Surf C | J03 | 3   | 0.01  | 0.21  | 0.34  |   | P14   | Surf C   | J16 | 10  | -0.58 | 0.67  | -0.63 |
| P13   | Surf C | J03 | 3   | -0.58 | 0.95  | -0.31 |   | P14   | Surf C   | J16 | 10  | -0.28 | 0.07  | -0.45 |
| P13   | Surf C | J03 | 3   | 0.18  | -0.84 | -0.18 |   | P14   | Surf C   | J16 | 11  | -0.76 | 1.67  | -0.08 |
| P13   | Surf C | J03 | 4   | -0.43 | 0.72  | -0.16 |   | P14   | Surf C   | J16 | 11  | 0.09  | -1.34 | -0.97 |
| P13   | Surf C | J03 | 6   | -0.06 | -0.18 | -0.17 |   | P14   | Surf C   | J16 | 11  | -0.16 | -1.14 | -1.28 |
| P13   | Surf C | J03 | 6   | 0.02  | -0.56 | -0.29 |   | P14   | Surf C   | J16 | 11  | -0.08 | -1.07 | -1.05 |
| P13   | Surf C | J03 | 6   | 0.60  | -1.04 | 0.42  |   | P14   | Surf C   | J16 | 12  | -0.13 | -0.46 | -0.59 |
| P13   | Surf C | J03 | 7   | -0.06 | -0.18 | -0.17 |   | P14   | Surf C   | J16 | 12  | -0.42 | 0.15  | -0.75 |
| P13   | Surf C | J03 | 8   | 0.02  | -0.56 | -0.29 |   | P14   | Surf C   | J16 | 13  | -0.29 | -0.80 | -1.25 |
| P13   | Surf C | J03 | 10  | 0.26  | -0.62 | 0.14  |   | P14   | Surf C   | J16 | 14  | -0.07 | -0.84 | -0.79 |
| P13   | Surf C | J03 | 10  | -0.03 | 0.13  | 0.12  |   | P14   | Surf C   | J16 | 14  | 0.11  | -0.91 | -0.56 |
| P13   | Surf C | J03 | 10  | -0.18 | 0.09  | -0.22 |   | P14   | Surf C   | J16 | 15  | -0.26 | -0.26 | -0.80 |
| P13   | Surf C | J03 | 11  | 0.00  | 1.13  | 1.01  |   | P14   | Surf C   | J16 | 15  | -0.12 | -0.47 | -0.67 |
| P13   | Surf C | J43 | 12  | 0.17  | -0.81 | -0.26 |   | P14   | Surf C   | J16 | 15  | -0.29 | -0.50 | -0.95 |
| P13   | Surf C | J43 | 12  | 0.31  | -0.36 | 0.48  |   | P16   | Surf C   | J20 | 1   | -0.36 | -0.06 | -0.81 |
| P13   | Surf C | J43 | 13  | 0.06  | -1.12 | -0.79 |   | P16   | Surf C   | J20 | 1   | -0.35 | 0.12  | -0.64 |
| P13   | Surf C | J43 | 13  | -0.02 | 0.38  | 0.35  |   | P16   | Surf C   | J20 | 1   | -0.18 | 1.08  | 0.60  |
| P13   | Surf C | J43 | 14  | -0.05 | -0.66 | -0.59 |   | P16   | Surf C   | J20 | 2   | -0.47 | 0.97  | -0.13 |
| P13   | Surf C | J43 | 14  | 0.07  | -0.63 | -0.32 |   | P16   | Surf C   | J20 | 2   | -0.39 | 1.18  | 0.24  |
| P13   | Surf C | J43 | 15  | 0.00  | 0.16  | 0.24  |   | P16   | Surf C   | J20 | 2   | 0.11  | -0.77 | -0.47 |
| P13   | Surf C | J43 | 15  | -0.24 | 1.07  | 0.51  |   | P16   | Surf C   | J20 | 3   | -0.16 | 0.11  | -0.24 |
| P13   | Surf C | J43 | 16  | 0.00  | 0.92  | 0.90  |   | P16   | Surf C   | J20 | 3   | 0.06  | -0.38 | -0.19 |
| P13   | Surf C | J43 | 16  | 0.06  | -0.80 | -0.46 |   | P16   | Surf C   | J20 | 3   | 0.11  | -0.77 | -0.47 |
| P13   | Surf C | J43 | 16  | 0.30  | -0.69 | 0.17  |   | P17   | Interm C | J22 | 5   | 0.18  | -0.88 | -0.47 |
| P13   | Surf C | J43 | 17  | 0.03  | -0.47 | -0.27 |   | P17   | Interm C | J22 | 5   | 0.23  | -0.86 | -0.39 |
| P13   | Surf C | J43 | 17  | -0.20 | 0.78  | 0.31  |   | P17   | Interm C | J22 | 6   | -0.01 | -0.98 | -1.07 |
| P13   | Surf C | J43 | 17  | 0.10  | -0.74 | -0.30 |   | P17   | Interm C | J22 | 6   | -0.10 | -0.55 | -0.79 |
| P13   | Surf C | J43 | 17  | -0.10 | 0.75  | 0.59  |   | P17   | Interm C | J22 | 7   | 0.11  | -0.90 | -0.65 |
| P13   | Surf C | J43 | 18  | -0.21 | -0.08 | -0.38 |   | P17   | Interm C | J22 | 7   | 0.07  | 0.14  | 0.22  |
| P13   | Surf C | J43 | 18  | -0.09 | 1.12  | 0.84  |   | P17   | Interm C | J22 | 8   | -0.25 | 0.01  | -0.70 |
| P13   | Surf C | J43 | 18  | -0.10 | 0.75  | 0.59  |   | P17   | Interm C | J22 | 9   | -0.13 | -0.84 | -1.15 |
| P13   | Surf C | J43 | 20  | -0.11 | 1.71  | 1.33  |   | P17   | Interm C | J22 | 9   | 0.03  | 0.16  | 0.16  |
| P14   | Surf C | J16 | 2   | -0.45 | 0.50  | -0.42 |   | P17   | Interm C | J22 | 10  | -0.53 | 0.67  | -0.64 |
| P14   | Surf C | J16 | 3   | -0.16 | -0.03 | -0.27 |   | P17   | Interm C | J22 | 10  | 0.44  | -0.63 | 0.33  |
| P14   | Surf C | J16 | 3   | -0.27 | -0.24 | -0.68 |   | P18   | Surf C   | J48 | 1   | 0.52  | -1.50 | -0.11 |
| P14   | Surf C | J16 | 4   | -0.55 | -0.74 | -1.78 |   | P18   | Surf C   | J48 | 2   | 0.11  | -1.11 | -0.62 |
| P14   | Surf C | J16 | 4   | -0.20 | -0.95 | -1.22 |   | P18   | Surf C   | J48 | 2   | 0.06  | -0.48 | -0.21 |
| P14   | Surf C | J16 | 4   | -0.04 | -0.78 | -0.68 |   | P18   | Surf C   | J48 | 2   | 0.20  | -1.15 | -0.51 |
| P14   | Surf C | J16 | 5   | 0.12  | 0.29  | 0.60  |   | P18   | Surf C   | J48 | 3   | -0.05 | -1.07 | -0.93 |
| P14   | Surf C | J16 | 5   | -0.11 | 0.15  | -0.05 |   | P18   | Surf C   | J48 | 4   | 0.25  | -0.60 | 0.10  |
| P14   | Surf C | J16 | 6   | -0.06 | -0.30 | -0.32 |   | P18   | Surf C   | J48 | 4   | 0.16  | -0.25 | 0.19  |
| P14   | Surf C | J16 | 7   | -0.05 | -0.89 | -0.82 |   | P18   | Surf C   | J48 | 5   | -0.31 | -0.21 | -0.79 |

| Proj. | Mix    | JMF  | Lot | AC    | AV    | VMA   | Proj. | Mix      | JMF  | Lot | AC    | AV    | VMA   |
|-------|--------|------|-----|-------|-------|-------|-------|----------|------|-----|-------|-------|-------|
| P18   | Surf C | .148 | 5   | 0.13  | -0.13 | 0.30  | P20   | Surf C   | .150 | 11  | -0.10 | -0.75 | -0.89 |
| P18   | Surf C | .148 | 5   | 0.10  | -0.03 | 0.69  | P20   | Surf C   | .150 | 11  | 0.29  | -1.02 | -0.31 |
| P18   | Surf C | J48  | 6   | 0.08  | -0.45 | -0.13 | P20   | Surf C   | J50  | 11  | 0.10  | 0.35  | 0.47  |
| P18   | Surf C | J48  | 7   | -0.10 | 1.68  | 1.33  | P20   | Surf C   | J50  | 11  | -0.08 | 0.12  | -0.11 |
| P19   | Surf D | .149 | 3   | -0.12 | 0.37  | 0.04  | P20   | Surf C   | .150 | 12  | -0.10 | -0.75 | -0.89 |
| P19   | Surf D | J49  | 3   | -0.01 | -0.03 | -0.07 | P20   | Surf C   | J50  | 13  | 0.29  | -1.02 | -0.31 |
| P19   | Surf D | J49  | 4   | -0.13 | 0.04  | -0.21 | P20   | Surf C   | J50  | 13  | 0.10  | 0.35  | 0.47  |
| P19   | Surf D | J49  | 5   | -0.06 | -0.96 | -0.93 | P20   | Surf C   | J50  | 14  | 0.07  | -0.58 | -0.38 |
| P19   | Surf D | J49  | 5   | -0.13 | -0.53 | -0.77 | P20   | Surf C   | J50  | 14  | -0.03 | -0.62 | -0.63 |
| P19   | Surf D | J49  | 5   | 0.26  | -1.06 | -0.35 | P20   | Surf C   | J50  | 14  | 0.11  | -0.78 | -0.47 |
| P19   | Surf D | .149 | 6   | 0.03  | -0.49 | -0.36 | P20   | Surf C   | J50  | 14  | -0.01 | 0.26  | 0.17  |
| P19   | Surf D | J49  | 6   | 0.07  | -1.06 | -0.78 | P20   | Surf C   | J50  | 15  | 0.12  | -0.61 | -0.32 |
| P19   | Surf D | J49  | 6   | 0.03  | -0.40 | -0.21 | P20   | Surf C   | J50  | 15  | -0.24 | 1.36  | 0.64  |
| P19   | Surf D | J49  | 6   | 0.21  | -0.88 | -0.31 | P20   | Surf C   | J50  | 15  | -0.21 | -0.17 | -0.65 |
| P19   | Surf D | J49  | 7   | 0.01  | -0.57 | -0.44 | P20   | Surf C   | J50  | 15  | -0.26 | 0.25  | -0.39 |
| P19   | Surf D | .149 | . 7 | -0.44 | 0.32  | -0.64 | P20   | Surf C   | .150 | 15  | -0.12 | 0.22  | -0.11 |
| P19   | Surf D | .149 | 7   | -0.88 | -0.46 | -2 29 | P20   | Surf C   | .150 | 16  | 0.12  | -0.76 | -0.37 |
| P19   | Surf D | .149 | 7   | 0.00  | -1 27 | -0.85 | P20   | Surf C   | .150 | 16  | 0.36  | -1.01 | -0.19 |
| P19   | Surf D | .149 | . 8 | 0.00  | 0.34  | 0.67  | P20   | Surf C   | .150 | 17  | -0.07 | 0.11  | -0.07 |
| P19   | Surf D | .149 | 8   | 0.02  | -1 49 | -1 27 | P20   | Surf C   | .150 | 17  | 0.01  | 0.02  | 0.01  |
| P19   | Surf D | .149 | 8   | -0.06 | -1.07 | -0.89 | P21   | Interm C | .134 | 3   | 0.01  | -0.28 | 0.01  |
| P19   | Surf D | .149 | 9   | 0.00  | -1.01 | -0.84 | P21   | Interm C | .134 | 3   | 0.00  | -0.74 | 0.40  |
| P19   | Surf D | .149 | 9   | -0.40 | 0.10  | -0.76 | P21   | Interm C | .134 | 3   | 0.07  | 0.74  | 0.10  |
| P19   | Surf D | .149 | 9   | -0.40 | -0.17 | -0.70 | P21   | Interm C | .134 | 3   | 0.14  | -0.09 | 0.00  |
| P20   | Surf C | 150  | 1   | 0.20  | -1.54 | -0.51 | P21   | Interm C | 134  | 5   | -0.06 | 0.00  | 0.10  |
| P20   | Surf C | .150 | 2   | 0.00  | -0.90 | -0.71 | P21   | Interm C | .134 | 5   | -0.10 | 0.20  | 0.00  |
| P20   | Surf C | 150  | 2   | 0.02  | -0.79 | -0.56 | P21   | Interm C | 134  | 5   | 0.10  | -0.09 | 0.12  |
| P20   | Surf C | .150 | 2   | -0.05 | -0.70 | -0.67 | P21   | Interm C | .134 | 6   | -0.08 | 0.00  | 0.10  |
| P20   | Surf C | .150 | 2   | -0.19 | -0.40 | -0.71 | P21   | Surf C   | .139 | 1   | 0.09  | -0.84 | -0.51 |
| P20   | Surf C | .150 | 2   | -0.41 | -0.15 | -0.97 | P21   | Surf C   | .139 | 2   | 0.06  | -0.80 | -0.55 |
| P20   | Surf C | .150 | - 3 | 0.04  | -0.79 | -0.56 | P21   | Surf C   | .139 | 2   | 0.00  | -0.99 | -0.61 |
| P20   | Surf C | .150 | 3   | -0.49 | 0.70  | -0.91 | P21   | Surf C   | .139 | 2   | 0.06  | -0.82 | -0.56 |
| P20   | Surf C | J50  | 4   | -0.07 | 0.46  | 0.22  | P21   | Surf C   | J39  | 2   | 0.06  | -0.80 | -0.55 |
| P20   | Surf C | J50  | 4   | -0.16 | 0.48  | 0.03  | P21   | Surf C   | J39  | 3   | 0.11  | -0.99 | -0.61 |
| P20   | Surf C | J50  | 4   | -0.04 | 0.08  | -0.07 | P21   | Surf C   | J39  | 3   | 0.06  | -0.82 | -0.56 |
| P20   | Surf C | J50  | 4   | -0.10 | 0.23  | -0.08 | P21   | Surf C   | J39  | 4   | -0.13 | -0.89 | -1.02 |
| P20   | Surf C | J50  | 5   | 0.03  | 0.21  | 0.19  | P21   | Surf C   | J39  | 4   | 0.06  | -0.99 | -0.70 |
| P20   | Surf C | J50  | 6   | 0.09  | 0.16  | 0.31  | P21   | Surf C   | J39  | 4   | 0.08  | -0.74 | -0.46 |
| P20   | Surf C | J50  | 6   | 0.18  | 0.24  | 0.51  | P21   | Surf C   | J39  | 4   | -0.13 | -0.89 | -1.02 |
| P20   | Surf C | J50  | 7   | 0.30  | -0.36 | 0.27  | P21   | Surf C   | J39  | 5   | 0.13  | -0.98 | -0.57 |
| P20   | Surf C | J50  | 7   | 0.25  | -0.05 | 0.43  | P21   | Surf C   | J39  | 5   | -0.28 | -0.61 | -1.11 |
| P20   | Surf C | J50  | . 7 | 0.00  | 0.20  | 0.14  | P21   | Surf C   | J39  | 5   | -0.13 | -0.89 | -1.02 |
| P20   | Surf C | J50  | 7   | 0.14  | -0.36 | -0.07 | P21   | Surf C   | J39  | 6   | -0.14 | -0.46 | -0.68 |
| P20   | Surf C | J50  | 7   | 0.02  | -0.45 | -0.41 | P22   | Surf D   | J54  | 1   | 0.00  | -1.18 | -1.07 |
| P20   | Surf C | J50  | . 8 | 0.10  | -0.66 | -0.37 | P22   | Surf D   | J54  | 1   | 0.02  | -1.15 | -1.02 |
| P20   | Surf C | J50  | 8   | 0.22  | -0.34 | 0.14  | P22   | Surf D   | J54  | 1   | 0.21  | 0.34  | 0.70  |
| P20   | Surf C | J50  | 8   | -0.12 | -0.10 | -0.36 | P22   | Surf D   | J54  | 1   | 0.09  | -0.42 | -0.21 |
| P20   | Surf C | J50  | 9   | 0.34  | -0.77 | 0.02  | P22   | Surf D   | J54  | 1   | 0.17  | -0.44 | 0.55  |
| P20   | Surf C | J50  | 10  | -0.12 | -0.10 | -0.36 | P22   | Surf D   | J54  | 1   | -0.07 | 1.96  | 1.52  |
| P20   | Surf C | J50  | 11  | 0.15  | -0.48 | -0.10 | P22   | Surf D   | J54  | 2   | 0.00  | 0.95  | 0.81  |

| Table A.2. | Plant | Test | Results | Data | (continued) |
|------------|-------|------|---------|------|-------------|
|------------|-------|------|---------|------|-------------|

| Proj. | Mix      | JMF | Lot | AC    | AV    | VMA   | ] | Proj. | Mix    | JMF | Lot | AC    | AV    | VMA   |
|-------|----------|-----|-----|-------|-------|-------|---|-------|--------|-----|-----|-------|-------|-------|
| NO.   |          | NO. | NO. | 0.04  | 0.40  | 0.00  |   | NO.   | Type   | NO. | NO. | 4.00  | 4 40  | 0.00  |
| P22   | Sull D   | J54 | 2   | 0.01  | 0.13  | 0.09  |   | P24   | Sun C  | J20 | 5   | -1.02 | 1.43  | -0.80 |
| P22   | Sun D    | J54 | 2   | 0.01  | 0.42  | 0.38  |   | P24   | Sun C  | J56 | 0   | -0.18 | 0.14  | -0.20 |
| P22   | Sun D    | J54 | 2   | -0.01 | 0.25  | 0.19  |   | P24   | Sun C  | J56 | 0   | 0.00  | -0.27 | -0.18 |
| P22   | Surr D   | J54 | 2   | 0.01  | -0.06 | -0.07 |   | P24   | Sun C  | J20 | 6   | -0.06 | -0.24 | -0.28 |
| P22   | Surr D   | J54 | 3   | 0.12  | 0.54  | 0.73  |   | P24   | Surf C | J56 | /   | 0.18  | -0.83 | -0.18 |
| P24   | Base C   | J57 | 1   | 0.03  |       |       |   | P24   | Sur C  | J20 | 8   | 0.23  | -1.04 | -0.37 |
| P24   | Base C   | J57 | 1   | 0.10  |       |       |   | P24   | Sur C  | J20 | 9   | 0.17  | -1.32 | -0.70 |
| P24   | Base C   | J57 | 2   | 0.09  |       |       |   | P24   | Surf C | J56 | 9   | 0.17  | -0.50 | 0.00  |
| P24   | Base C   | J57 | 2   | 0.18  |       |       |   | P24   | Surf C | J56 | 9   | -0.21 | 0.26  | -0.22 |
| P24   | BaseC    | J57 | 3   | 0.08  |       |       |   | P24   | SurrC  | J56 | 10  | 0.14  | -0.98 | -0.46 |
| P24   | Base C   | J57 | 3   | -0.03 |       |       |   | P24   | Surf C | J56 | 11  | 0.07  | 0.07  | 0.26  |
| P24   | Base C   | J57 | 4   | 0.08  |       |       |   | P24   | Surf C | J56 | 11  | 0.03  | -0.46 | -0.29 |
| P24   | Base C   | J57 | 4   | 0.06  |       |       |   | P24   | Surf C | J56 | 11  | -0.16 | 0.38  | 0.01  |
| P24   | Base C   | J57 | 5   | 0.26  |       |       |   | P24   | Surf C | J56 | 11  | 0.73  | -2.50 | -0.54 |
| P24   | Base C   | J57 | 5   | 0.20  |       |       |   | P24   | Surf C | J56 | 12  | 0.04  | 0.32  | 0.42  |
| P24   | Base C   | J57 | 6   | 0.30  |       |       |   | P24   | Surf C | J56 | 12  | 0.05  | 0.46  | 0.62  |
| P24   | Base C   | J57 | 6   | 0.30  |       |       |   | P24   | Surf C | J56 | 13  | 0.08  | 1.30  | 1.42  |
| P24   | Interm C | J51 | 1   | -0.04 |       |       |   | P24   | Surf C | J56 | 14  | -0.03 | -0.54 | -0.48 |
| P24   | Interm C | J51 | 3   | 0.18  |       |       |   | P24   | Surf C | J56 | 14  | -0.31 | 1.06  | 0.28  |
| P24   | Interm C | J51 | 3   | 0.02  |       |       |   | P24   | Surf C | J56 | 14  | -0.06 | -0.72 | -0.80 |
| P24   | Interm C | J51 | 4   | 0.29  |       |       |   | P24   | Surf C | J56 | 15  | 0.01  | -0.48 | -0.33 |
| P24   | Interm C | J51 | 5   | 0.39  |       |       |   | P24   | Surf C | J56 | 16  | -0.13 | -0.08 | -0.33 |
| P24   | Interm C | J51 | 6   | -0.26 |       |       |   | P24   | Surf C | J56 | 16  | 0.22  | -1.00 | -0.28 |
| P24   | Interm C | J51 | 6   | 0.05  |       |       |   | P24   | Surf C | J56 | 17  | 0.12  | -0.78 | -0.38 |
| P24   | Interm C | J51 | 7   | 0.06  |       |       |   | P24   | Surf C | J56 | 17  | 0.19  | -1.11 | -0.49 |
| P24   | Interm C | J51 | 8   | -0.03 |       |       |   | P24   | Surf C | J56 | 17  | 0.04  | -1.13 | -0.86 |
| P24   | Interm C | J51 | 8   | -0.04 |       |       |   | P24   | Surf C | J56 | 17  | -0.07 | -0.90 | -0.92 |
| P24   | Interm C | J51 | 9   | -0.06 |       |       |   | P24   | Surf C | J56 | 18  | -0.12 | 0.70  | 0.42  |
| P24   | Interm C | J51 | 9   | 0.37  |       |       |   | P24   | Surf C | J56 | 18  | 0.30  | 0.02  | -1.27 |
| P24   | Interm C | J51 | 10  | -0.06 |       |       |   | P24   | Surf C | J56 | 18  | 0.02  | 0.52  | 0.51  |
| P24   | Interm C | J51 | 10  | -0.13 |       |       |   | P24   | Surf C | J67 | 1   | 1.67  | 0.03  | -0.04 |
| P24   | Interm C | J51 | 11  | 0.02  |       |       |   | P24   | Surf C | J67 | 2   | -0.51 | 1.17  | 0.03  |
| P24   | Interm C | J51 | 12  | -0.11 |       |       |   | P24   | Surf C | J67 | 3   | 0.05  | -1.13 | -0.81 |
| P24   | Interm C | J51 | 12  | 0.04  |       |       |   | P24   | Surf C | J67 | 4   | -0.14 | -0.66 | -0.85 |
| P24   | Interm C | J51 | 13  | -0.17 |       |       |   | P24   | Surf C | J67 | 4   | 0.02  | -0.66 | -0.47 |
| P24   | Interm C | J51 | 13  | 0.11  |       |       |   | P24   | Surf C | J67 | 5   | -0.32 | -0.07 | -0.72 |
| P24   | Interm C | J51 | 14  | 0.01  |       |       |   | P24   | Surf C | J67 | 5   | -0.14 | -0.36 | -0.54 |
| P24   | Interm C | J51 | 15  | 0.13  |       |       |   | P24   | Surf C | J67 | 5   | -0.14 | 0.53  | 0.24  |
| P24   | Interm C | J51 | 15  | -0.09 |       |       |   | P24   | Surf C | J67 | 7   | 0.03  | 0.18  | 0.29  |
| P24   | Interm C | J51 | 16  | -0.02 |       |       |   | P24   | Surf C | J67 | 7   | 0.07  | -0.95 | -0.67 |
| P24   | Surf C   | J56 | 1   | -0.36 | 1.10  | 0.24  |   | P24   | Surf D | J64 | 1   | 0.16  | 0.00  | 0.00  |
| P24   | Surf C   | J56 | 2   | -0.04 | 0.85  | 0.72  |   | P24   | Surf D | J64 | 2   | 0.26  | -0.48 | 0.28  |
| P24   | Surf C   | J56 | 2   | -0.10 | 0.30  | 0.09  |   | P24   | Surf D | J64 | 2   | 0.17  | -0.78 | -0.26 |
| P24   | Surf C   | J56 | 2   | -0.04 | -0.73 | -0.66 | 1 | P24   | Surf D | J64 | 3   | 0.13  | -0.82 | -0.39 |
| P24   | Surf C   | J56 | 2   | -0.14 | -0.49 | -0.66 | 1 | P24   | Surf D | J64 | 3   | 0.21  | -1.05 | -0.36 |
| P24   | Surf C   | J56 | 2   | 0.11  | -1.10 | -0.65 | 1 | P24   | Surf D | J64 | 4   | 0.13  | -0.59 | -0.12 |
| P24   | Surf C   | J56 | 3   | -0.01 | -0.25 | -0.13 | 1 | P24   | Surf D | J64 | 4   | 0.18  | -0.24 | 0.23  |
| P24   | Surf C   | J56 | 4   | 0.20  | -0.94 | -0.34 | 1 | P24   | Surf D | J64 | 5   | 0.08  | -0.82 | -0.53 |
| P24   | Surf C   | J56 | 4   | 0.09  | -0.70 | -0.36 | 1 | P24   | Surf D | J64 | 5   | 0.04  | -0.73 | -0.52 |
| P24   | Surf C   | J56 | 4   | -0.11 | -0.34 | -0.42 | 1 | P24   | Surf D | J64 | 6   | 0.10  | -0.62 | -0.28 |
| L     | 1        |     | 1   |       | 1     |       |   | L     |        |     |     |       |       |       |

| Proj. | Mix      | JMF  | Lot | 40    | A.V/  |       | Proj. | Mix    | JMF  | Lot         | 40    | A1/   |       |
|-------|----------|------|-----|-------|-------|-------|-------|--------|------|-------------|-------|-------|-------|
| No.   | Туре     | No.  | No. | AC    | AV    | VMA   | No.   | Туре   | No.  | No.         | AC    | AV    | VMA   |
| P24   | Surf D   | J64  | 6   | 0.14  | -0.52 | -0.09 | P26   | Surf A | J62  | 1           | 0.06  | -0.51 | -0.36 |
| P24   | Surf D   | J64  | 7   | 0.14  | -0.73 | -0.27 | P26   | Surf A | J62  | 1           | 0.18  | 0.14  | 0.53  |
| P24   | Surf D   | J64  | 7   | 0.12  | -0.97 | -0.45 | P26   | Surf A | J62  | 1           | 0.24  | -1.10 | -0.44 |
| P25   | Interm C | J29  | 1   | -0.19 | 0.15  | -0.10 | P26   | Surf A | J62  | 1           | 0.16  | -0.47 | -0.11 |
| P25   | Interm C | J29  | 1   | 0.21  | 0.44  | 0.99  | P26   | Surf A | J62  | 2           | 0.15  | 0.95  | 1.19  |
| P25   | Interm C | J29  | 2   | -0.52 | 1.68  | 0.56  | P26   | Surf A | J62  | 2           | -0.18 | 0.87  | 0.37  |
| P25   | Interm C | J29  | 2   | -0.13 | 0.94  | 0.73  | P26   | Surf A | J62  | 2           | 0.04  | 0.21  | 0.24  |
| P25   | Interm C | J29  | 3   | -0.15 | 0.58  | 0.40  | P26   | Surf A | J62  | 2           | 0.04  | 0.64  | 0.64  |
| P25   | Interm C | J29  | 3   | 0.10  | 0.67  | 1.08  | P26   | Surf A | J62  | 3           | -0.23 | 0.66  | 0.05  |
| P25   | Interm C | J29  | 4   | -0.34 | 0.58  | -0.04 | P26   | Surf A | J62  | 3           | 0.03  | 0.53  | 0.51  |
| P25   | Interm C | J29  | 4   | -0.38 | 0.80  | 0.06  | P26   | Surf A | J62  | 3           | -0.12 | 0.47  | 0.15  |
| P25   | Interm C | J29  | 5   | -0.12 | -0.38 | -0.44 | P26   | Surf A | J62  | 4           | -0.21 | 0.23  | -0.28 |
| P25   | Interm C | J29  | 6   | -0.11 | 0.56  | 0.58  | P26   | Surf A | J62  | 4           | -0.03 | 0.80  | 0.63  |
| P25   | Interm C | J29  | 6   | 0.01  | 0.56  | 0.81  | P26   | Surf A | J62  | 4           | -0.27 | 1.68  | 0.92  |
| P25   | Interm C | J29  | 8   | -0.26 | 1.05  | 0.62  | P26   | Surf A | J62  | 5           | 0.18  | 0.41  | 0.72  |
| P25   | Surf D   | J36  | 1   | 0.12  | 0.48  | 0.87  | P26   | Surf A | J62  | 5           | -0.12 | 0.78  | 0.40  |
| P25   | Surf D   | J36  | 2   | -0.12 | -1.13 | -0.97 | P26   | Surf A | J62  | 5           | -0.10 | 1.06  | 0.70  |
| P25   | Surf D   | J36  | 2   | -0.01 | 0.15  | 0.33  | P26   | Surf A | J62  | 6           | -0.06 | 0.21  | 1.01  |
| P25   | Surf D   | J36  | 3   | -0.04 | 0.18  | 0.40  | P26   | Surf A | J62  | 6           | -0.09 | 0.53  | 0.23  |
| P25   | Surf D   | J36  | 3   | 0.42  | 0.64  | 1.65  | P26   | Surf A | J62  | 6           | 0.10  | 0.70  | 0.84  |
| P25   | Surf D   | J36  | 3   | -0.08 | 0.50  | 0.52  | P26   | Surf A | J62  | 7           | 0.08  | -0.03 | 0.11  |
| P25   | Surf D   | J36  | 4   | -0.10 | 1.13  | 1.08  | P26   | Surf A | J62  | 7           | -0.06 | -0.52 | -0.69 |
| P25   | Surf D   | J36  | 4   | 0.42  | 0.64  | 1.65  | P26   | Surf A | J62  | 7           | 0.00  | 0.53  | 0.43  |
| P25   | Surf D   | J36  | 5   | 0.00  | 0.31  | 0.51  | P26   | Surf A | J62  | 7           | 0.15  | -0.15 | 0.42  |
| P25   | Surf D   | J36  | 6   | -0.04 | 0.85  | 0.96  | P26   | Surf A | J62  | 8           | 0.16  | 0.02  | 0.37  |
| P26   | Base A   | J45  | 1   | -0.03 |       |       | P26   | Surf A | J62  | 8           | -0.17 | 1.16  | 0.62  |
| P26   | Base A   | J45  | 1   | -0.46 |       |       | P26   | Surf A | J62  | 8           | 0.47  | -0.51 | 0.55  |
| P26   | Base A   | J45  | 1   | 0.86  |       |       | P26   | Surf A | J62  | 9           | 0.12  | 0.16  | 0.39  |
| P26   | Base A   | J45  | 1   | 0.08  |       |       | P26   | Surf A | J62  | 9           | -0.32 | 0.92  | 0.11  |
| P26   | Base A   | J45  | 2   | 0.43  |       |       | P26   | Surf A | J62  | 9           | 0.29  | -0.13 | 0.49  |
| P26   | Base A   | J45  | 2   | 0.04  |       |       | P26   | Surf A | J62  | 9           | -0.04 | 0.13  | -0.02 |
| P26   | Base A   | J45  | 2   | -0.10 |       |       | P26   | Surf A | J69  | 1           | 0.21  | -0.35 | 0.13  |
| P26   | Base A   | J45  | 3   | -0.12 |       |       | P26   | Surf A | J69  | 1           | 0.36  | 0.32  | 1.02  |
| P26   | Base A   | J45  | 3   | -0.14 |       |       | P26   | Surf A | J69  | 1           | 0.27  | -0.06 | 0.53  |
| P26   | Base A   | J45  | 5   | -0.38 |       |       | P26   | Surf A | J69  | 1           | 0.23  | -0.58 | 0.07  |
| P26   | Base A   | J45  | 5   | 0.34  |       |       | P26   | Surf A | J69  | 2           | 0.15  | -0.61 | -0.16 |
| P26   | Base A   | J45  | 5   | 0.23  |       |       | P26   | Surf A | J69  | 2           | -0.24 | 0.44  | -0.06 |
| P26   | OGFC     | J68  | 1   | -1.03 |       |       | P26   | Surf A | J69  | 2           | -0.03 | -0.19 | -0.19 |
| P26   | OGFC     | J68  | 1   | -0.12 |       |       | P26   | Surf A | J69  | 3           | 0.04  | -0.29 | -0.13 |
| P26   | OGEC     | J68  | 1   | 0.30  |       |       | P26   | Surf A | J69  | 3           | -0.22 | 0.34  | -0.15 |
| P26   | OGFC     | J68  | 2   | -0.23 |       |       | P26   | Surf A | J69  | 3           | -0.26 | -0.25 | -0.80 |
| P26   | OGEC     | .168 | 2   | -0.19 |       |       | P26   | Surf A | .169 | 4           | -0.01 | -0.53 | -0.47 |
| P26   | OGEC     | .168 | 2   | -0.24 |       |       | P26   | Surf A | .169 | -<br>-<br>- | 0.01  | -0.01 | 0.47  |
| P26   | OGEC     | .168 | 2   | -0.16 |       |       | P26   | Surf A | .169 | -<br>-<br>- | 0.10  | 0.21  | 0.20  |
| P26   | OGEC     | .168 | 3   | -0.19 |       |       | P26   | Surf A | .169 | 5           | 0.01  | -0.26 | 0.09  |
| P26   | OGEC     | .168 | 2   | -0.04 |       |       | P26   | Surf A | .160 | 5           | 0.10  | -0.34 | 0.00  |
| P26   | OGEC     | .168 | 3   | 0.04  |       |       | P26   | Surf A | 169  | 5           | -0.04 | 0.04  | 0.02  |
| P26   | OGEC     | .168 | 1   | 0.00  |       |       | P26   | Surf A | .160 | 6           | 0.04  | -0.16 | 0.02  |
| P26   | OGEC     | .168 |     | 0.00  |       |       | P26   | Surf A | .160 | 6           | -0.04 | 0.10  | 0.27  |
| P26   | OGEC     | 168  | 4   | -0.34 |       |       | P26   |        | 160  | 6           | 0.04  | -0.04 | -0.61 |
| 1 20  |          | 000  | 4   | -0.54 |       |       | 1 20  |        | 209  | 0           | 0.10  | -0.94 | -0.01 |

| Table A.2. | Plant | Test | Results | Data | (continued) |
|------------|-------|------|---------|------|-------------|
|------------|-------|------|---------|------|-------------|

| Proj. | Mix    | JMF | Lot    | AC    | AV    | VMA   | Proj. | Mix    | JMF | Lot | AC    | AV | VMA |
|-------|--------|-----|--------|-------|-------|-------|-------|--------|-----|-----|-------|----|-----|
| P26   | Surf A | 169 | 7      | 0.27  | -1.00 | -0.28 | P26   | Surf F | 152 | 2   | 0.06  |    |     |
| P26   |        | 160 | 7      | -0.10 | 0.10  | -0.20 | P26   | Surf E | 152 | 2   | -0.30 |    |     |
| P26   |        | 169 | 7      | 0.10  | -0.62 | -0.02 | P26   | Surf E | 152 | 3   | -0.30 |    | -   |
| P26   |        | 169 | 8      | -0.23 | 0.67  | 0.23  | P26   | Surf E | 152 | 4   | -0.17 |    | -   |
| P26   |        | 160 | 8      | -0.23 | 0.07  | 0.11  | P26   |        | 152 | -   | 0.12  |    | -   |
| P26   |        | 169 | 8      | -0.07 | 0.34  | 0.14  | P26   | Surf E | 152 | 5   | -0.09 |    | -   |
| P26   |        | 169 | 0<br>0 | -0.15 | 0.13  | 0.24  | P26   | Surf E | 152 | 5   | -0.00 |    |     |
| P26   |        | 160 | 9      | -0.15 | 0.42  | 0.00  | P26   | Surf E | 152 | 6   | -0.10 |    |     |
| P26   |        | 160 | 9      | -0.03 | -0.52 | -0.68 | P26   | Surf E | 152 | 6   | 0.12  |    |     |
| P26   |        | 160 | 10     | -0.03 | -0.32 | -0.00 | P26   | Surf E | 152 | 7   | 0.13  |    |     |
| P26   |        | 160 | 10     | -0.14 | 0.00  | 0.40  | P26   | Surf E | 152 | 0   | 0.03  |    |     |
| P26   |        | 160 | 10     | 0.27  | -0.04 | 0.58  | F20   | Surf E | 152 | 0   | -0.12 |    |     |
| F20   |        | 160 | 10     | 0.13  | 0.10  | 0.40  | P20   | Surf E | J52 | 0   | -0.02 |    |     |
| P26   |        | 160 | 10     | 0.11  | -0.12 | 0.10  | F20   | Surf E | 152 | 9   | 0.00  |    |     |
| F20   |        | 160 | 11     | -0.10 | 1.03  | 1.21  | P20   | Surf E | J52 | 9   | 0.12  |    |     |
| F 20  |        | 109 | 11     | 0.30  | 0.07  | 1.31  | F20   | Surf E | 152 | 10  | 0.02  |    |     |
| P20   | Sull A | 160 | 10     | -0.03 | 1.00  | 1.34  | P20   | Suite  | J52 | 10  | -0.12 |    |     |
| P20   | Sull A | 160 | 12     | -0.14 | 0.63  | 0.28  | P20   | Sull E | J52 | 11  | -0.04 |    | -   |
| P20   | Sull A | 160 | 12     | 0.02  | 0.61  | 0.62  | P20   | Sull E | J52 | 10  | -0.09 |    | -   |
| P20   |        | J69 | 12     | -0.13 | 0.75  | 0.40  | P20   | Sull E | J52 | 12  | -0.10 |    | -   |
| P26   | Surf A | J69 | 12     | 0.00  | 1.12  | 1.10  | P26   | SurrE  | J52 | 12  | -0.06 |    | -   |
| P26   | Surf A | J69 | 13     | -0.40 | 0.80  | -0.15 | P26   | Suff E | J52 | 13  | 0.27  |    |     |
| P26   | Surf A | J69 | 13     | -0.21 | 0.38  | -0.10 | P26   | Suff E | J52 | 14  | -0.08 |    |     |
| P26   | Surf A | J69 | 13     | 0.02  | -0.12 | -0.06 | P26   | Suff E | J52 | 14  | 0.05  |    |     |
| P26   | Surf A | J69 | 14     | -0.27 | 0.73  | 0.07  | P26   | Suff E | J52 | 15  | -0.15 |    |     |
| P26   | Surf A | J69 | 14     | -0.35 | 0.43  | -0.39 | P26   | Surf E | J52 | 15  | 0.18  |    |     |
| P26   | Surf A | J69 | 14     | -0.09 | 0.29  | 0.04  | P26   | Surf E | J52 | 15  | 0.22  |    |     |
| P26   | Surf A | J69 | 15     | 0.09  | -0.33 | -0.11 | P26   | Surf E | J52 | 16  | -0.18 |    |     |
| P26   | Surf A | J69 | 15     | 0.16  | -0.41 | -0.03 | P26   | Surf E | J52 | 16  | -0.25 |    |     |
| P26   | Surf A | J69 | 15     | 0.33  | -0.56 | 0.20  | P26   | Surf E | J52 | 17  | -0.26 |    |     |
| P26   | Surf A | J69 | 16     | 0.13  | 0.14  | 0.42  | P26   | Surf E | J52 | 18  | -0.20 |    |     |
| P26   | Surf A | J69 | 16     | -0.12 | 0.91  | 0.57  | P26   | Surf E | J52 | 18  | -0.35 |    |     |
| P26   | Surf A | J69 | 16     | 0.16  | -0.41 | -0.03 | P26   | Surf E | J52 | 18  | -0.33 |    |     |
| P26   | Surf A | J69 | 17     | -0.53 | 1.91  | 0.60  | P26   | Surf E | J52 | 19  | -0.10 |    |     |
| P26   | Surf A | J69 | 18     | 0.06  | 1.01  | 1.08  | P26   | Surf E | J52 | 19  | -0.16 |    |     |
| P26   | Surf C | J58 | 1      | -0.19 | -0.05 | -0.42 | P26   | Surf E | J52 | 20  | -0.10 |    |     |
| P26   | Surf C | J58 | 2      | 0.13  | -0.63 | -0.24 | P26   | Surf E | J52 | 21  | 0.05  |    |     |
| P26   | Surf C | J58 | 3      | -0.01 | 0.37  | 0.37  | P26   | Surf E | J52 | 21  | 0.01  |    |     |
| P26   | Surf C | J58 | 4      | -0.25 | 0.94  | 0.38  | P26   | Surf E | J52 | 21  | 0.16  |    |     |
| P26   | Surf C | J58 | 5      | -0.12 | -0.30 | -0.47 | P26   | Surf E | J52 | 22  | -0.14 |    |     |
| P26   | Surf C | J58 | 6      | 0.23  | -0.30 | 0.32  | P26   | Surf E | J52 | 22  | 0.03  |    |     |
| P26   | Surf C | J58 | 7      | 0.05  | 0.27  | 0.40  | P26   | Surf E | J52 | 22  | 0.06  |    |     |
| P26   | Surf C | J58 | 8      | -0.03 | 0.12  | 0.05  | P26   | Surf E | J52 | 23  | -0.21 |    |     |
| P26   | Surf C | J58 | 9      | 0.17  | -0.35 | 0.12  | P26   | Surf E | J52 | 23  | 0.01  |    |     |
| P26   | Surf C | J58 | 10     | -0.06 | 0.21  | 0.08  | P26   | Surf E | J52 | 23  | 0.02  |    |     |
| P26   | Surf C | J58 | 11     | 0.04  | 1.58  | 1.49  | P26   | Surf E | J52 | 24  | -0.02 |    |     |
| P26   | Surf C | J58 | 11     | -0.24 | 1.35  | 0.72  | P26   | Surf E | J52 | 24  | -0.26 |    |     |
| P26   | Surf C | J58 | 12     | 0.24  | 0.44  | 0.95  | P26   | Surf E | J52 | 24  | -0.28 |    |     |
| P26   | Surf E | J52 | 1      | -0.15 |       |       | P26   | Surf E | J52 | 25  | 0.11  |    |     |
| P26   | Surf E | J52 | 2      | -0.10 |       |       | P26   | Surf E | J52 | 26  | -0.19 |    |     |
| P26   | Surf E | J52 | 2      | -0.12 |       |       | P26   | Surf E | J52 | 26  | -0.30 |    |     |

VMA

0.96

-0.19

0.10

-0.05

0.36

0.80

0.44

0.67

0.66

0.45

0.65

0.10

0.45

0.63

0.91

0.26

0.32

0.78

0.20

0.24

0.17

0.79

-0.64

-0.23 0.62

1.13

-0.03

0.28

0.03

0.94

0.40

-0.30

0.31

0.23

0.16

-0.30

0.16

0.48

0.81

0.15

0.48

0.81

0.41

-0.07

-1.26

0.08

-0.38

0.37

-0.55

-0.66

AC

0.64

-0.11

0.11

0.02

0.11

0.23

0.30

0.04

0.05

-0.15

0.26

0.23

0.04

0.01

0.15

-0.28

0.14

0.25

0.10

0.20

-0.14

0.13

-0.23

-0.24

0.18

0.16

-0.05

0.14

0.03

0.19

-0.25

0.28

0.03

0.22

0.00

0.15

0.17

0.01

0.07

0.17

0.01

0.07

0.00

-0.05

-0.30

0.05

0.08

-0.06

0.02

-0.05

AV

-0.58

0.03

-0.24

-0.16

0.06

0.28

-0.31

0.61

0.60

0.82

0.01

-0.51

0.28

0.59

0.52

1.01

0.00

0.22

-0.02

-0.24

0.53

0.53

-0.15

0.35

0.24

0.10

-0.06

-0.04

0.59

1.05

-1.03

0.25

-0.29

0.18

-0.66

-0.23

0.55

0.75

-0.26

0.55

0.74

0.31

-0.06

-0.93

-0.31

-0.80

0.40

-0.90

-0.81

| Proi | Mix      | IME | Lot |       |       |       |  | Proi | Mix      | IME | Lot |
|------|----------|-----|-----|-------|-------|-------|--|------|----------|-----|-----|
| No.  | Type     | No. | No. | AC    | AV    | VMA   |  | No.  | Type     | No. | No. |
| P26  | Surf E   | J52 | 26  | 0.11  |       |       |  | P27  | Surf B   | J55 | 1   |
| P26  | Surf E   | J52 | 27  | -0.07 |       |       |  | P27  | Surf B   | J55 | 1   |
| P26  | Surf E   | J52 | 28  | 0.12  |       |       |  | P27  | Surf B   | J55 | 1   |
| P26  | Surf E   | J52 | 29  | -0.09 |       |       |  | P27  | Surf B   | J55 | 2   |
| P26  | Surf E   | J52 | 30  | 0.01  |       |       |  | P27  | Surf B   | J55 | 2   |
| P27  | Base A   | J66 | 1   | 0.02  |       |       |  | P27  | Surf B   | J55 | 2   |
| P27  | Base A   | J66 | 2   | -0.15 |       |       |  | P27  | Surf B   | J55 | 3   |
| P27  | Base A   | J66 | 3   | 0.01  |       |       |  | P27  | Surf B   | J55 | 3   |
| P27  | Base A   | J66 | 4   | 0.13  |       |       |  | P27  | Surf B   | J55 | 3   |
| P27  | Base A   | J66 | 5   | -0.10 |       |       |  | P27  | Surf B   | J55 | 4   |
| P27  | Base A   | J66 | 6   | -0.24 |       |       |  | P27  | Surf B   | J55 | 4   |
| P27  | Base A   | J66 | 7   | 0.31  |       |       |  | P27  | Surf B   | J55 | 4   |
| P27  | Base A   | J66 | 8   | 0.19  |       |       |  | P27  | Surf B   | J55 | 5   |
| P27  | Base A   | J66 | 9   | 0.37  |       |       |  | P27  | Surf B   | J55 | 5   |
| P27  | Base A   | J66 | 10  | -0.16 |       |       |  | P27  | Surf B   | J55 | 5   |
| P27  | Base A   | J66 | 11  | 0.12  |       |       |  | P27  | Surf B   | J71 | 1   |
| P27  | Interm B | J60 | 1   | 0.12  | 0.86  | 1.05  |  | P27  | Surf B   | J71 | 1   |
| P27  | Interm B | J60 | 2   | 0.43  | 0.11  | 1.11  |  | P27  | Surf B   | J71 | 1   |
| P27  | Interm B | J60 | 3   | 0.35  | 0.06  | 0.85  |  | P27  | Surf B   | J71 | 2   |
| P27  | Interm B | J60 | 4   | -0.10 | 1.09  | 0.74  |  | P27  | Surf B   | J71 | 2   |
| P27  | Interm B | J60 | 5   | 0.26  | -0.39 | 0.27  |  | P27  | Surf B   | J71 | 2   |
| P27  | Interm B | J60 | 6   | 0.41  | -0.21 | 0.76  |  | P27  | Surf B   | J71 | 2   |
| P27  | Interm B | J60 | 7   | 0.16  | -0.45 | -0.01 |  | P27  | Surf B   | J71 | 4   |
| P27  | Interm B | J60 | 8   | 0.55  | 0.50  | 1.75  |  | P27  | Surf B   | J71 | 4   |
| P27  | Interm B | J60 | 9   | 0.43  | -0.86 | 0.20  |  | P27  | Surf B   | J71 | 4   |
| P27  | Interm B | J60 | 10  | 0.40  | 0.11  | 0.98  |  | P27  | Surf B   | J71 | 5   |
| P27  | Interm B | J60 | 11  | -0.19 | 0.45  | -0.01 |  | P27  | Surf B   | J71 | 5   |
| P27  | Interm B | J60 | 12  | 0.25  | 0.22  | 0.79  |  | P27  | Surf B   | J71 | 6   |
| P27  | Interm B | J60 | 13  | -0.12 | 0.47  | 0.18  |  | P27  | Surf B   | J71 | 7   |
| P27  | Interm B | J60 | 14  | 0.42  | -1.08 | -0.02 |  | P27  | Surf B   | J71 | 7   |
| P27  | Interm B | J60 | 15  | 0.55  | -0.76 | 0.52  |  | P27  | Surf B   | J71 | 7   |
| P27  | Interm C | J53 | 1   | 0.02  | -0.84 | -0.71 |  | P27  | Surf B   | J71 | 8   |
| P27  | Interm C | J53 | 1   | -0.25 |       |       |  | P27  | Surf B   | J71 | 8   |
| P27  | Interm C | J53 | 2   | -0.21 |       |       |  | P27  | Surf B   | J71 | 8   |
| P27  | Interm C | J53 | 2   | -0.15 |       |       |  | P27  | Surf B   | J71 | 9   |
| P27  | Interm C | J53 | 3   | -0.22 |       |       |  | P27  | Surf B   | J71 | 9   |
| P27  | Interm C | J53 | 4   | -0.20 | 0.30  | -0.10 |  | P27  | Surf B   | J71 | 9   |
| P27  | Interm C | J53 | 5   | -0.25 | -0.24 | -0.73 |  | P27  | Surf B   | J71 | 9   |
| P27  | Interm C | J53 | 6   | -0.26 | 0.22  | -0.35 |  | P27  | Surf B   | J71 | 9   |
| P27  | Interm C | J53 | 7   | 0.32  | -0.75 | 0.12  |  | P27  | Surf B   | J71 | 10  |
| P27  | Interm C | J53 | 8   | 0.18  | -0.15 | 0.37  |  | P27  | Surf B   | J71 | 10  |
| P27  | Interm C | J53 | 8   | -0.02 | -0.20 | -0.17 |  | P27  | Surf B   | J71 | 10  |
| P27  | Interm C | J53 | 9   | 0.07  | -0.27 | 0.02  |  | P27  | Surf CM  | J61 | 1   |
| P27  | Interm C | J53 | 10  | 0.01  | -0.02 | 0.12  |  | P27  | Surf CM  | J61 | 2   |
| P27  | Interm C | J53 | 11  | 0.13  | -0.28 | 0.13  |  | P27  | Surf CM  | J61 | 3   |
| P27  | Interm C | J53 | 12  | -0.07 | 0.09  | 0.01  |  | P27  | Surt CM  | J61 | 4   |
| P27  | Interm C | J53 | 13  | 0.10  | -0.22 | 0.11  |  | P27  | Surf CM  | J61 | 5   |
| P27  | Interm C | J53 | 14  | 0.39  | -1.05 | 0.02  |  | P27  | Surt CM  | J61 | 6   |
| P27  | Interm C | J53 | 15  | 0.22  | 0.07  | 0.61  |  | P27  | Surf CM  | J61 | 7   |
| P27  | Interm C | 153 | 16  | 0.19  | 0.63  | 1.07  |  | P27  | SUIT CIM | J61 | 8   |

Table A.2. Plant Test Results Data (continued)

| Table A.2. | Plant | Test | Results | Data | (continued) |
|------------|-------|------|---------|------|-------------|
|------------|-------|------|---------|------|-------------|

| Proj. | Mix      | JMF  | Lot     | AC    | AV    | VMA   | ] | Proj. | Mix      | JMF  | Lot | AC    | AV    | VMA   |
|-------|----------|------|---------|-------|-------|-------|---|-------|----------|------|-----|-------|-------|-------|
| NO.   | Type     | NO.  | NO.     | 0.00  | 0.10  | 0.51  |   | NO.   | Type     | NO.  | NO. | 0.1.1 | 0.61  | 0.20  |
| P27   |          | J01  | 9       | -0.22 | -0.18 | -0.51 |   | P20   | Sun C    | 139  | 0   | 0.11  | -0.61 | -0.30 |
| P28   | Base B   | J47  | 1       | 0.05  |       |       |   | P28   | Sun C    | 139  | 8   | 0.06  | -0.40 | -0.22 |
| P28   | Base B   | J47  | 2       | 0.01  |       |       |   | P28   | Surr C   | J39  | 9   | 0.00  | -0.53 | -0.45 |
| P28   | Base B   | J47  | 2       | -0.10 |       |       |   | P28   | Suff C   | J39  | 10  | -0.29 | 0.15  | -0.45 |
| P28   | Base B   | J47  | 3       | -0.29 |       |       |   | P29   | Surf C   | J59  | 1   | -0.11 | -0.03 | -0.21 |
| P28   | Base B   | J47  | 4       | -0.36 |       |       |   | P29   | Surf C   | J59  | 2   | 0.19  | -0.36 | 0.17  |
| P28   | Base B   | J47  | 5       | 0.06  |       |       |   | P29   | Surf C   | J59  | 2   | 0.20  | -0.31 | 0.22  |
| P28   | Base B   | J47  | 6       | -0.24 |       |       |   | P29   | Surf C   | J59  | 2   | 0.05  | 0.13  | 0.28  |
| P28   | Base B   | J47  | 7       | -0.05 |       |       |   | P29   | Surf C   | J59  | 3   | 0.04  | 0.43  | 0.52  |
| P28   | Base B   | J47  | 7       | -0.27 |       |       |   | P29   | Surf C   | J59  | 3   | 0.13  | 0.03  | 0.44  |
| P28   | Base B   | J47  | 8       | 0.44  |       |       |   | P29   | Surf C   | J59  | 3   | -0.25 | 0.39  | -0.14 |
| P28   | Base B   | J47  | 8       | -0.16 |       |       |   | P29   | Surf C   | J59  | 4   | -0.16 | -0.01 | -0.26 |
| P28   | Base B   | J47  | 9       | 0.13  |       |       |   | P29   | Surf C   | J59  | 4   | -0.02 | -0.35 | -0.29 |
| P28   | Base B   | J47  | 9       | 0.07  |       |       |   | P29   | Surf C   | J59  | 4   | 0.03  | -0.18 | 0.02  |
| P28   | Base B   | J47  | 10      | 0.36  |       |       |   | P29   | Surf C   | J59  | 5   | -0.18 | 0.86  | 0.45  |
| P28   | Interm C | J42  | 1       | -0.08 | -0.71 | -0.82 |   | P29   | Surf C   | J59  | 5   | -0.19 | 0.10  | -0.25 |
| P28   | Interm C | J42  | 1       | 0.03  | 0.35  | 0.37  |   | P29   | Surf C   | J59  | 5   | 0.14  | 0.29  | 0.64  |
| P28   | Interm C | J42  | 2       | -0.03 | 0.83  | 0.68  |   | P29   | Surf C   | J59  | 6   | -0.02 | -0.23 | -0.19 |
| P28   | Interm C | J42  | 3       | -0.29 | 0.01  | -0.62 |   | P29   | Surf C   | J59  | 6   | 0.07  | -0.23 | 0.05  |
| P28   | Interm C | J42  | 4       | -0.16 | 0.82  | 0.39  |   | P29   | Surf C   | J59  | 6   | -0.05 | 0.14  | 0.08  |
| P28   | Interm C | J42  | 5       | -0.06 | -0.04 | -0.17 | 1 | P29   | Surf C   | J59  | 7   | 0.22  | -0.11 | 0.49  |
| P28   | Interm C | J42  | 6       | 0.09  | -0.36 | -0.14 |   | P29   | Surf C   | J59  | 7   | -0.13 | 0.07  | -0.11 |
| P28   | Interm C | J42  | 7       | 0.37  | 0.01  | 0.94  | 1 | P29   | Surf C   | J59  | 7   | -0.27 | 0.10  | -0.41 |
| P28   | Interm C | J42  | 8       | 0.37  | 0.01  | 0.94  | 1 | P29   | Surf C   | J59  | 7   | -0.13 | -0.24 | -0.42 |
| P28   | Interm C | J42  | 9       | 0.07  | 0.00  | 0.16  |   | P29   | Surf C   | J59  | 8   | -0.04 | -0.23 | -0.16 |
| P28   | Interm C | J42  | 9       | 0.24  | -0.28 | 0.26  |   | P29   | Surf C   | J59  | 8   | -0.15 | -0.08 | -0.27 |
| P28   | Interm C | J42  | 10      | 0.12  | 0.03  | 0.27  |   | P29   | Surf C   | J59  | 8   | -0.15 | 0.04  | -0.17 |
| P28   | Interm C | J42  | 11      | 0.18  | -0.01 | 0.37  |   | P29   | Surf C   | J59  | 9   | -0.11 | -0.36 | -0.47 |
| P28   | Interm C | J42  | 12      | 0.11  | -0.55 | -0.26 |   | P29   | Surf C   | J59  | 9   | -0.15 | -0.08 | -0.27 |
| P28   | Interm C | J42  | 13      | 0.31  | -0.55 | 0.16  |   | P29   | Surf C   | J59  | 9   | -0.15 | 0.04  | -0.17 |
| P28   | Surf C   | .139 | 1       | 0.31  | -1 13 | -0.29 |   | P30   | Surf B   | .165 | 1   | -0.15 | 1.09  | 0.71  |
| P28   | Surf C   | .139 | 1       | 0.25  | -0.86 | -0.20 |   | P30   | Surf B   | .165 | 1   | -0.07 | 0.41  | 0.27  |
| P28   | Surf C   | .139 | 1       | -0.15 | -0.59 | -0.77 |   | P30   | Surf B   | .165 | 1   | 0.04  | 0.42  | 0.50  |
| P28   | Surf C   | .139 | 3       | -0.03 | -0.90 | -0.84 |   | P30   | Surf B   | .165 | 2   | 0.09  | 0.45  | 0.63  |
| P28   | Surf C   | .139 | 4       | 0.00  | -0.28 | -0.23 |   | P30   | Surf B   | .165 | 2   | -0.07 | 0.41  | 0.00  |
| P28   | Surf C   | 130  | -т<br>Д | 0.00  | -0.96 | -0.41 |   | P30   | Surf B   | 165  | 2   | 0.04  | 0.41  | 0.27  |
| P28   | Surf C   | .139 | 4       | 0.20  | -0.61 | -0.30 |   | P30   | Surf B   | .165 | 3   | 0.04  | 0.42  | 0.63  |
| P28   | Surf C   | 130  | -       | 0.11  | -0.01 | -0.36 |   | P30   | Surf B   | 165  | 4   | -0.05 | 0.43  | 0.00  |
| P28   | Surf C   | 130  | 5       | -0.23 | -0.55 | -0.30 |   | P32   | Interm B | 176  | 2   | -0.03 | -0.82 | -0.64 |
| F 20  | Surf C   | 130  | 5       | -0.22 | -0.07 | -1.01 |   | F 32  | Interm D | 176  | 2   | -0.08 | -0.02 | -0.04 |
| P20   | Surf C   | 139  | 5<br>5  | 0.19  | -0.82 | -0.30 |   | P32   | Interm P | J70  | 2   | -0.05 | -0.52 | -0.41 |
| F20   |          | 129  | 5       | 0.02  | -0.59 | -0.47 |   | F 32  |          | J70  | 2   | 0.20  | -0.34 | 0.03  |
| P28   | Surf C   | J39  | 5       | -0.11 | -0.73 | -0.50 |   | P32   | Interm B | J76  | 2   | 0.25  | -0.96 | 0.04  |
| P28   | Surf C   | J39  | 5       | 0.09  | -0.56 | -0.31 |   | P32   | Interm B | J76  | 3   | -0.16 | -0.72 | -0.74 |
| P28   | Surf C   | J39  | 6       | -0.11 | -0.29 | -0.47 |   | P32   | Interm B | J/6  | 3   | -0.14 | -0.71 | -0.63 |
| P28   | Surf C   | J39  | 6       | -0.11 | -0.32 | -0.47 |   | P32   | Interm B | J/6  | 3   | -0.15 | -0.18 | -0.17 |
| P28   | Surt C   | J39  | 6       | 0.21  | -0.89 | -0.34 |   | P32   | Interm B | J76  | 4   | 0.31  | -0.48 | 0.57  |
| P28   | Surf C   | J39  | 6       | 0.06  | -0.46 | -0.28 |   | P32   | Interm B | J76  | 4   | 0.47  | -1.02 | 0.48  |
| P28   | Surf C   | J39  | 6       | 0.06  | -0.40 | -0.22 | l | P32   | Interm B | J76  | 4   | 0.05  | 0.09  | 0.49  |
| P28   | Surf C   | J39  | 7       | 0.09  | -0.40 | -0.17 |   | P32   | Interm B | J76  | 4   | 0.08  | -0.58 | -0.06 |
| P28   | Surf C   | J39  | 8       | 0.06  | -0.51 | -0.31 |   | P32   | Interm B | J76  | 4   | -0.31 | -0.63 | -0.99 |

| Table A.2. | Plant Tes | t Results | Data | (continued) |
|------------|-----------|-----------|------|-------------|
|------------|-----------|-----------|------|-------------|

| Proj. | Mix      | JMF  | Lot | AC    | AV    | VMA   | Proj. | Mix    | JMF  | Lot | AC    | AV    | VMA   |
|-------|----------|------|-----|-------|-------|-------|-------|--------|------|-----|-------|-------|-------|
| P32   | Interm B | .176 | 5   | 0.15  | 0.40  | 0 47  | P32   | Surf A | .179 | 6   | -0.09 | 0.13  | -0.05 |
| P32   | Interm B | .176 | 5   | 0.03  | -0.66 | -0.25 | P32   | Surf A | .179 | 6   | 0.00  | -0.12 | 0.00  |
| P32   | Interm B | J76  | 5   | -0.01 | -0.54 | -0.24 | P32   | Surf A | J79  | 6   | 0.13  | -0.27 | 0.09  |
| P32   | Interm B | J76  | 5   | 0.14  | -0.92 | -0.22 | P32   | Surf A | J79  | 7   | 0.11  | -0.26 | 0.09  |
| P32   | Interm B | .176 | 6   | 0.17  | -0.72 | 0.02  | P32   | Surf A | .179 | . 7 | 0.08  | -0.45 | -0.16 |
| P32   | Interm B | J76  | 6   | 0.23  | -0.33 | 0.55  | P32   | Surf A | J79  | 7   | 0.22  | -0.29 | 0.30  |
| P32   | Interm B | J76  | 6   | 0.17  | -0.49 | 0.21  | P32   | Surf A | J79  | . 8 | 0.06  | 0.54  | 0.67  |
| P32   | Interm B | J76  | 7   | -0.20 | -0.38 | -0.55 | P32   | Surf A | J79  | 8   | 0.09  | 0.29  | 0.51  |
| P32   | Interm B | J76  | 7   | -0.35 | -0.40 | -0.91 | P32   | Surf A | J79  | 8   | 0.18  | -0.78 | -0.26 |
| P32   | Interm B | J76  | 7   | 0.23  | -0.65 | 0.20  | P32   | Surf A | J79  | 9   | 0.28  | 0.49  | 1.11  |
| P32   | Interm B | J76  | 9   | 0.06  | -0.47 | -0.03 | P32   | Surf A | J79  | 9   | 0.20  | 0.01  | 0.50  |
| P32   | Interm B | J76  | 9   | 0.02  | -0.52 | -0.13 | P32   | Surf A | J79  | 9   | 0.17  | 0.16  | 0.53  |
| P32   | Interm B | J76  | 9   | 0.00  | -0.70 | -0.36 | P32   | Surf A | J79  | 10  | 0.22  | -0.19 | 0.39  |
| P32   | Interm B | J76  | 10  | -0.15 | 0.21  | 0.13  | P32   | Surf A | J79  | 10  | 0.18  | 0.19  | 0.63  |
| P32   | Interm B | J76  | 10  | 0.32  | -0.79 | 0.36  | P32   | Surf A | J79  | 10  | 0.35  | 0.27  | 1.09  |
| P32   | Interm B | J76  | 10  | 0.19  | -0.84 | -0.01 | P32   | Surf A | J79  | 10  | 0.10  | -0.30 | -0.02 |
| P32   | Interm B | J76  | 10  | 0.23  | -0.78 | 0.14  | P32   | Surf A | J79  | 11  | 0.01  | 0.34  | 0.34  |
| P32   | Interm B | J76  | 11  | -0.11 | -0.54 | -0.45 | P32   | Surf A | J79  | 11  | 0.07  | 0.94  | 1.10  |
| P32   | Interm B | J76  | 11  | -0.08 | -0.98 | -0.79 | P32   | Surf A | J79  | 11  | 0.31  | -0.43 | 0.33  |
| P32   | Interm B | J76  | 11  | 0.05  | -0.90 | -0.41 | P32   | Surf A | J79  | 11  | -0.07 | -0.58 | -0.68 |
| P32   | Interm B | J76  | 11  | 0.07  | -0.94 | -0.39 | P32   | Surf A | J79  | 11  | 0.37  | -0.64 | 0.29  |
| P32   | Interm B | J76  | 12  | 0.02  | -0.48 | -0.10 | P32   | Surf A | J79  | 12  | 0.13  | 0.01  | 0.34  |
| P32   | Interm B | J76  | 12  | 0.23  | -0.96 | -0.04 | P32   | Surf A | J79  | 12  | -0.14 | -0.47 | -0.72 |
| P32   | Interm B | J76  | 12  | 0.43  | -0.84 | 0.53  | P32   | Surf A | J79  | 12  | 0.20  | 0.16  | -2.33 |
| P32   | Interm B | J76  | 12  | 0.08  | -0.90 | -0.33 | P32   | Surf A | J79  | 12  | 0.15  | -0.40 | 0.00  |
| P32   | Interm B | J76  | 13  | 0.52  | -1.06 | 0.56  | P32   | Surf A | J79  | 13  | 0.02  | 0.02  | 0.12  |
| P32   | Interm B | J76  | 13  | -0.02 | -0.82 | -0.51 | P32   | Surf A | J79  | 13  | -0.36 | 0.28  | -0.53 |
| P32   | Interm B | J76  | 13  | 0.15  | -0.76 | -0.06 | P32   | Surf A | J79  | 13  | -0.31 | 0.37  | -0.31 |
| P32   | Interm B | J76  | 14  | 0.11  | -0.08 | 0.47  | P32   | Surf A | J79  | 13  | -0.07 | -0.49 | -0.55 |
| P32   | Interm B | J76  | 14  | 0.56  | -0.58 | -0.24 | P32   | Surf A | J79  | 13  | -0.10 | 0.13  | -0.08 |
| P32   | Interm B | J76  | 14  | 0.23  | -0.54 | 0.33  | P32   | Surf A | J79  | 14  | -0.19 | 0.48  | 0.04  |
| P32   | Surf A   | J79  | 2   | 0.16  | 0.34  | 0.67  | P32   | Surf A | J79  | 14  | -0.03 | 0.01  | 0.03  |
| P32   | Surf A   | J79  | 2   | 0.25  | 0.03  | 0.57  | P32   | Surf A | J79  | 14  | -0.23 | 0.46  | -0.02 |
| P32   | Surf A   | J79  | 2   | 0.17  | -0.78 | -0.28 | P32   | Surf A | J79  | 15  | 0.08  | -0.43 | -0.14 |
| P32   | Surf A   | J79  | 2   | 0.28  | -1.12 | -0.32 | P32   | Surf A | J79  | 15  | 0.08  | -0.32 | -0.03 |
| P32   | Surf A   | J79  | 2   | 0.33  | -0.58 | 0.26  | P32   | Surf A | J79  | 15  | 0.28  | 0.03  | 0.79  |
| P32   | Surf A   | J79  | 2   | 0.16  | -0.37 | 0.07  | P32   | Surf A | J79  | 15  | 0.19  | -0.90 | -0.36 |
| P32   | Surf A   | J79  | 3   | 0.29  | 0.04  | 0.77  | P32   | Surf A | J79  | 15  | 0.25  | -0.95 | -0.21 |
| P32   | Surf A   | J79  | 3   | 0.19  | -0.09 | 0.38  | P32   | Surf A | J79  | 16  | 0.34  | -1.20 | -0.26 |
| P32   | Surf A   | J79  | 3   | 0.20  | 0.05  | 0.54  | P32   | Surf A | J79  | 16  | 0.10  | -0.95 | -0.59 |
| P32   | Surf A   | J79  | 3   | 0.30  | -0.60 | 0.19  | P32   | Surf A | J79  | 16  | 0.04  | -0.24 | -0.03 |
| P32   | Surf A   | J79  | 3   | 0.34  | -0.51 | 0.40  | P32   | Surf A | J79  | 16  | 0.06  | -0.28 | -0.03 |
| P32   | Surf A   | J79  | 4   | 0.22  | 0.13  | 0.66  | P32   | Surf A | J79  | 16  | 0.10  | 0.31  | 0.61  |
| P32   | Surf A   | J79  | 4   | 0.23  | 0.18  | 0.75  | P32   | Surf A | J79  | 17  | 0.20  | -0.86 | -0.35 |
| P32   | Surf A   | J79  | 4   | 0.01  | -0.07 | 0.00  | P32   | Surf A | J79  | 17  | 0.03  | -1.05 | -0.80 |
| P32   | Surf A   | J79  | 4   | 0.31  | -0.74 | 0.08  | P32   | Surf A | J79  | 17  | 0.10  | -0.67 | -0.32 |
| P32   | Surf A   | J79  | 5   | 0.11  | -0.83 | -0.43 | P32   | Surf A | J79  | 17  | -0.11 | -0.87 | -0.98 |
| P32   | Surf A   | J79  | 5   | 0.36  | -1.10 | -0.13 | P32   | Surf A | J79  | 17  | -0.34 | -0.27 | -0.95 |
| P32   | Surf A   | J79  | 5   | 0.19  | -0.09 | 0.38  | P32   | Surf A | J79  | 18  | 0.11  | -0.54 | -0.14 |
| P32   | Surf A   | J79  | 6   | -0.23 | -0.23 | -0.71 | P32   | Surf A | J79  | 18  | 0.32  | -0.24 | 0.62  |

| Table A.2. | Plant | Test | Results | Data | (continued) |
|------------|-------|------|---------|------|-------------|
|------------|-------|------|---------|------|-------------|

| Proj. | Mix    | JMF | Lot | AC    | AV    | VMA   | Proj. | Mix             | JMF | Lot | AC    | AV    | VMA   |
|-------|--------|-----|-----|-------|-------|-------|-------|-----------------|-----|-----|-------|-------|-------|
| NO.   | I ype  | NO. | NO. | 0.09  | 0.00  | 0.00  | NO.   | Iype<br>Surf D  | NO. | NO. | 0.10  | 0.10  | 0.20  |
| P32   |        | J79 | 10  | 0.08  | -0.20 | 0.09  | P32   |                 | J72 | 0   | 0.19  | -0.19 | 0.29  |
| P32   | Sull A | J79 | 10  | 0.11  | -0.12 | 0.21  | P32   | SUILD<br>Surf D | J72 | 6   | -0.04 | -0.81 | -0.80 |
| P32   | Sull A | J79 | 10  | 0.12  | -0.02 | 0.31  | P32   | SUILD<br>Surf D | J72 | 6   | 0.17  | -0.54 | -0.08 |
| P32   |        | J79 | 19  | 0.17  | 0.29  | 0.74  | P32   |                 | J72 | 0   | 0.19  | -0.47 | 0.05  |
| P32   | Surf A | J79 | 19  | 0.32  | -0.25 | 0.55  | P32   | SUIT B          | J72 | 7   | 0.31  | -0.82 | 0.00  |
| P32   | Sull A | J79 | 19  | 0.22  | -0.95 | -0.29 | P32   |                 | J72 | 7   | 0.06  | -0.33 | -0.14 |
| P32   | Surf A | J79 | 20  | 0.16  | -0.24 | 0.18  | P32   | SUIT B          | J72 | /   | 0.07  | -0.42 | -0.21 |
| P32   | Sull A | J79 | 20  | 0.38  | 0.16  | 1.03  | P32   | SUILD<br>Surf D | J72 | 0   | 0.38  | -0.79 | 0.24  |
| P32   | Sull A | J79 | 20  | 0.36  | -0.23 | 0.69  | P32   | SUILD<br>Surf D | J72 | 0   | -0.36 | 0.20  | -0.55 |
| P32   |        | J79 | 20  | 0.22  | -0.47 | 0.13  | P32   |                 | J72 | 0   | 0.16  | -0.31 | 0.12  |
| P32   |        | J79 | 20  | -0.14 | 0.23  | -0.09 | P32   | Surf B          | J72 | 8   | 0.00  | -0.22 | -0.19 |
| P32   |        | J79 | 21  | 0.07  | 0.84  | 0.96  | P32   | Surf E          | J46 | 1   | 0.22  |       |       |
| P32   |        | J79 | 21  | -0.06 | -0.23 | -0.29 | P32   | Surf E          | J46 | 2   | 0.06  |       |       |
| P32   |        | J79 | 21  | -0.07 | 0.33  | 0.17  | P32   | Surf E          | J46 | 3   | -0.25 |       |       |
| P32   | Surf A | J79 | 22  | 0.25  | 0.08  | 0.72  | P32   | SurrE           | J46 | 5   | -0.12 |       |       |
| P32   | Surf A | J79 | 22  | 0.02  | 0.27  | 0.37  | P32   | Surf E          | J46 | 6   | -0.36 |       |       |
| P32   | Surf A | J79 | 22  | 0.06  | -0.42 | -0.17 | P32   | Surf E          | J46 | /   | -0.29 |       |       |
| P32   | Surf A | J79 | 23  | 0.18  | -1.10 | -0.63 | P32   | Surf E          | J46 | 1   | 0.06  |       |       |
| P32   | Surf A | J79 | 23  | -0.02 | 0.00  | 0.01  | P32   | Surf E          | J46 | 8   | -0.08 |       |       |
| P32   | Surf A | J79 | 23  | 0.06  | -0.09 | 0.11  | P32   | Surf E          | J46 | 8   | 0.12  |       |       |
| P32   | Surf A | J79 | 23  | 0.17  | -0.99 | -0.42 | P32   | Surf E          | J46 | 9   | 0.12  |       |       |
| P32   | Surf A | J79 | 24  | 0.14  | -1.09 | -0.57 | P32   | Surf E          | J46 | 9   | -0.08 |       |       |
| P32   | Surf A | J79 | 24  | 0.08  | -0.51 | -0.22 | P32   | Surf E          | J46 | 10  | -0.32 |       |       |
| P32   | Surf A | J79 | 24  | 0.07  | -0.70 | -0.45 | P32   | Surf E          | J46 | 10  | 0.01  |       |       |
| P32   | Surf A | J79 | 25  | 0.17  | -1.45 | -0.86 | P32   | Surf E          | J46 | 10  | 0.31  |       |       |
| P32   | Surf A | J79 | 25  | -0.11 | -0.63 | -0.78 | P32   | Surf E          | J46 | 11  | -0.08 |       |       |
| P32   | Surf A | J79 | 25  | 0.07  | -0.70 | -0.45 | P32   | Surf E          | J46 | 12  | 0.31  |       |       |
| P32   | Surf B | J72 | 1   | -0.04 | 0.50  | 0.35  | P32   | Surf E          | J46 | 14  | 0.15  |       |       |
| P32   | Surf B | J72 | 1   | -0.19 | 0.07  | -0.36 | P32   | Surf E          | J46 | 18  | -0.03 |       |       |
| P32   | Surf B | J72 | 1   | 0.14  | 0.24  | 0.53  | P32   | Surf E          | J46 | 19  | 0.12  |       |       |
| P32   | Surf B | J72 | 1   | 0.05  | 0.40  | 0.48  | P32   | Surf E          | J46 | 21  | 0.08  |       |       |
| P32   | Surf B | J72 | 1   | 0.17  | 0.35  | 0.72  | P32   | Surf E          | J46 | 22  | -0.04 |       |       |
| P32   | Surf B | J72 | 2   | 0.06  | 1.01  | 0.99  | P32   | Surf E          | J46 | 24  | 0.18  |       |       |
| P32   | Surf B | J72 | 2   | 0.22  | 0.18  | 0.66  | P32   | Surf E          | J46 | 25  | 0.04  |       |       |
| P32   | Surf B | J72 | 2   | -0.15 | 1.03  | 0.56  | P32   | Surf E          | J46 | 26  | -0.06 |       |       |
| P32   | Surf B | J72 | 2   | 0.11  | 0.74  | 0.87  | P32   | Surf E          | J46 | 27  | 0.11  |       |       |
| P32   | Surf B | J72 | 2   | -0.06 | 0.32  | 0.16  | P32   | Surf E          | J46 | 28  | -0.07 |       |       |
| P32   | Surf B | J72 | 2   | -0.14 | 0.25  | -0.09 | P32   | Surf E          | J46 | 30  | -0.04 |       |       |
| P32   | Surf B | J72 | 3   | -0.10 | 0.36  | 0.08  | P32   | Surf E          | J46 | 30  | 0.02  |       |       |
| P32   | Surf B | J72 | 3   | 0.22  | 0.48  | 0.93  | P32   | Surf E          | J46 | 31  | 0.19  |       |       |
| P32   | Surf B | J72 | 3   | -0.22 | 0.50  | -0.06 | P32   | Surf E          | J46 | 31  | -0.05 |       |       |
| P32   | Surf B | J72 | 4   | 0.13  | -0.27 | 0.08  | P32   | Surf E          | J46 | 32  | -0.16 |       |       |
| P32   | Surf B | J72 | 4   | 0.29  | -0.38 | 0.35  | P32   | Surf E          | J46 | 32  | -0.17 |       |       |
| P32   | Surf B | J72 | 4   | 0.22  | -0.25 | 0.32  | P32   | Surf E          | J46 | 33  | -0.41 |       |       |
| P32   | Surf B | J72 | 5   | 0.08  | -0.39 | -0.12 | P32   | Surf E          | J46 | 35  | -0.07 |       |       |
| P32   | Surf B | J72 | 5   | -0.05 | -0.37 | -0.43 | P32   | Surf E          | J46 | 36  | -0.24 |       |       |
| P32   | Surf B | J72 | 5   | 0.18  | -0.44 | 0.01  | P32   | Surf E          | J46 | 37  | 0.34  |       |       |
| P32   | Surf B | J72 | 5   | -0.14 | -0.41 | -0.67 | P32   | Surf E          | J46 | 38  | -0.05 |       |       |
| P32   | Surf B | J72 | 5   | 0.32  | -0.06 | 0.70  | P32   | Surf E          | J46 | 38  | -0.21 |       |       |
| P32   | Surf B | J72 | 6   | 0.17  | -0.49 | 0.00  | P32   | Surf E          | J46 | 38  | -0.09 |       |       |

| Proj. | Mix         | JMF | Lot    | AC    | AV    | VMA   | Proj. | Mix    | JMF | Lot | AC    | AV    | VMA   |
|-------|-------------|-----|--------|-------|-------|-------|-------|--------|-----|-----|-------|-------|-------|
| NO.   | Line Curf E | NO. | NO.    | 0.02  |       |       | NO.   | Surf A | NO. | NO. | 0.20  | 0.21  | 0.59  |
| P32   | Surf E      | 140 | 41     | -0.02 |       |       | P33   |        | 177 | 2   | 0.29  | -0.31 | -0.58 |
| P32   | Jotorm B    | 172 | 40     | -0.03 | 0.22  | 0.42  | P33   |        | 177 | 3   | 0.32  | -0.50 | -0.70 |
| P33   | Interm B    | 172 | 2      | 0.32  | -0.23 | 0.42  | P33   |        | 177 | 4   | -0.01 | 0.74  | 1.04  |
| F 33  | Interm P    | 173 | 2      | 0.01  | 0.54  | 0.27  | F 33  |        | 177 | 4   | 0.20  | 0.74  | 0.02  |
| F 33  | Interm B    | J73 | 2      | -0.10 | 0.55  | 0.06  | F33   | Sull A | 177 | 4   | -0.24 | 0.00  | 0.02  |
| F 33  | Interm B    | 173 | 2      | 0.30  | -0.09 | 0.50  | F 33  |        | 177 | 4   | 0.10  | 0.10  | 0.40  |
| F 33  | Interm P    | J73 | 3      | -0.22 | -0.37 | -0.92 | F33   | Sull A | 177 | 5   | -0.20 | 0.90  | 0.25  |
| F 33  | Interm P    | J73 | 3      | -0.31 | -0.01 | -0.62 | F33   | Sull A | 177 | 5   | 0.11  | 0.79  | 0.99  |
| F 33  | Interm P    | J73 | 3      | 0.00  | -1.40 | -0.03 | F33   | Sull A | 177 | 5   | 0.09  | 0.90  | 0.59  |
| F 33  |             | J73 | 4      | -0.05 | 0.14  | -0.05 | F33   | Sull A | J77 | 0   | -0.09 | 0.70  | 0.00  |
| P33   |             | J73 | 4      | -0.12 | 0.58  | 0.11  | P33   | Sun A  | J77 | 0   | 0.30  | 0.18  | 0.86  |
| P33   |             | J73 | 4      | 0.34  | -0.57 | 0.14  | P33   | Sun A  | J77 | 0   | 0.56  | -0.84 | 0.55  |
| P33   |             | J73 | 4      | -0.12 | 0.69  | 0.25  | P33   | Sull E | J75 | 1   | -0.10 |       |       |
| P33   |             | J73 | 4      | 0.21  | -0.50 | -0.10 | P33   | Sull E | J75 | 2   | -0.15 |       |       |
| P33   |             | J73 | 5<br>5 | 0.15  | 0.37  | 0.63  | P33   | Sull E | J75 | 3   | 0.05  |       |       |
| P33   | Interm B    | J73 | 5      | -0.31 | 0.38  | -0.49 | P33   | Surf E | J75 | 4   | -0.16 |       |       |
| P33   | Interm B    | J73 | 5      | -0.04 | 0.66  | 0.42  | P33   | SurfE  | J75 | 5   | -0.03 |       |       |
| P33   | Interm B    | J73 | 5      | 0.03  | 0.55  | 0.47  | P33   | SurfE  | J75 | 6   | 0.37  |       |       |
| P33   | Interm B    | J73 | 6      | 0.04  | 0.06  | 0.09  | P33   | SurfE  | J75 | /   | -0.17 |       |       |
| P33   | Interm B    | J/3 | 6      | 0.16  | -0.26 | 0.05  | P33   | Surf E | J75 | 8   | -0.10 |       |       |
| P33   | Interm B    | J/3 | 6      | -0.03 | 0.30  | 0.14  | P33   | Surf E | J75 | 9   | -0.10 |       |       |
| P33   | Interm B    | J73 | 7      | 0.43  | -0.24 | 0.68  | P33   | Surf E | J75 | 10  | 0.24  |       |       |
| P33   | Interm B    | J73 | 7      | 0.04  | 0.92  | 0.84  | P34   | Surf A | J62 | 1   | 0.26  | -0.58 | 0.08  |
| P33   | Interm B    | J73 | 7      | -0.01 | 0.55  | 0.42  | P34   | Surf A | J62 | 1   | 0.08  | 0.02  | 0.22  |
| P33   | Interm B    | J73 | 8      | -0.12 | 0.35  | -0.05 | P34   | Surf A | J62 | 1   | -0.27 | 0.46  | -0.15 |
| P33   | Interm B    | J73 | 8      | 0.17  | -0.11 | 0.22  | P34   | Surf A | J62 | 1   | -0.09 | 0.79  | 0.53  |
| P33   | Interm B    | J73 | 8      | -0.01 | 0.55  | 0.42  | P34   | Surf A | J62 | 2   | 0.21  | -0.45 | 0.10  |
| P33   | OGFC        | J78 | 1      | -0.07 |       |       | P34   | Surf A | J62 | 2   | 0.24  | -0.72 | -0.10 |
| P33   | OGFC        | J78 | 1      | 0.74  |       |       | P34   | Surf A | J62 | 2   | 0.11  | -0.59 | -0.26 |
| P33   | OGFC        | J78 | 1      | -0.40 |       |       | P34   | Surf A | J62 | 2   | 0.26  | -0.62 | 0.05  |
| P33   | OGFC        | J78 | 1      | 0.28  |       |       | P34   | Surf A | J62 | 3   | 0.02  | 0.09  | 0.17  |
| P33   | OGFC        | J78 | 2      | -0.01 |       |       | P34   | Surf A | J62 | 3   | 0.00  | 0.23  | 0.29  |
| P33   | OGFC        | J78 | 2      | 0.15  |       |       | P34   | Surf A | J62 | 3   | -0.09 | 0.35  | 0.13  |
| P33   | OGFC        | J78 | 2      | 0.50  |       |       | P34   | Surf A | J62 | 3   | -0.09 | 0.65  | 0.41  |
| P33   | OGFC        | J78 | 3      | -0.50 |       |       | P34   | Surf A | J62 | 3   | -0.32 | 0.09  | -0.67 |
| P33   | OGFC        | J78 | 3      | 0.10  |       |       | P34   | Surf A | J62 | 3   | -0.12 | 0.76  | 0.37  |
| P33   | OGFC        | J78 | 3      | -0.21 |       |       | P34   | Surf A | J62 | 4   | -0.01 | -0.39 | -0.35 |
| P33   | OGFC        | J78 | 4      | 0.02  |       |       | P34   | Surf A | J62 | 4   | -0.20 | 0.82  | 0.35  |
| P33   | OGFC        | J78 | 4      | 0.25  |       |       | P34   | Surf A | J62 | 4   | -0.18 | 1.59  | 1.10  |
| P33   | OGFC        | J78 | 4      | -0.21 |       |       | P34   | Surf A | J62 | 4   | -0.10 | 0.96  | 0.70  |
| P33   | Surf A      | J77 | 1      | 0.00  | 1.43  | 0.34  | P34   | Surf A | J62 | 5   | -0.36 | 0.94  | 0.08  |
| P33   | Surf A      | J77 | 1      | -0.38 | 1.55  | -0.44 | P34   | Surf A | J62 | 5   | 0.11  | 0.23  | 0.49  |
| P33   | Surf A      | J77 | 1      | 0.13  | 0.76  | 0.03  | P34   | Surf A | J62 | 5   | 0.21  | -1.19 | -0.58 |
| P33   | Surf A      | J77 | 1      | -0.23 | 0.80  | -0.77 | P34   | Surf A | J62 | 5   | -0.55 | 1.23  | -0.08 |
| P33   | Surf A      | J77 | 2      | 0.00  | 0.04  | -0.92 | P34   | Surf A | J62 | 6   | 0.23  | -0.74 | -0.23 |
| P33   | Surf A      | J77 | 2      | 0.39  | 0.22  | 0.11  | P34   | Surf A | J62 | 6   | 0.06  | 0.68  | 0.67  |
| P33   | Surf A      | J77 | 2      | 0.12  | 0.37  | -0.30 | P34   | Surf A | J62 | 6   | 0.06  | 0.13  | 0.20  |
| P33   | Surf A      | J77 | 2      | 0.01  | 0.81  | -0.18 | P34   | Surf A | J62 | 6   | 0.06  | -0.23 | -0.14 |
| P33   | Surf A      | J77 | 3      | 0.24  | -0.05 | -0.46 | P34   | Surf A | J62 | 7   | -0.08 | -0.21 | -0.43 |
| P33   | Surf A      | J77 | 3      | 0.45  | -0.37 | -0.33 | P34   | Surf A | J62 | 7   | -0.10 | -0.04 | -0.30 |

| Table A.2. | Plant | Test | Results | Data | (continued) |
|------------|-------|------|---------|------|-------------|
|------------|-------|------|---------|------|-------------|

| Proj. | Mix    | JMF | Lot | AC    | AV    | VMA   |   | Proj. | Mix    | JMF | Lot | AC    | AV    | VMA   |
|-------|--------|-----|-----|-------|-------|-------|---|-------|--------|-----|-----|-------|-------|-------|
| No.   | Туре   | No. | No. |       |       |       |   | No.   | Туре   | No. | No. |       |       |       |
| P34   | Surf C | J81 | 1   | -0.06 | 1.06  | 0.82  |   | P35   | Surf C | J38 | 13  | -0.16 | 0.10  | -0.25 |
| P34   | Surf C | J81 | 1   | -0.11 | 1.12  | 0.78  |   | P35   | Surf C | J38 | 14  | 0.32  | -0.39 | 0.38  |
| P34   | Surf C | J81 | 2   | 0.13  | 0.46  | 0.76  |   | P35   | Surf C | J38 | 14  | 0.25  | -0.86 | -0.20 |
| P34   | Surf C | J81 | 2   | -0.13 | 0.28  | 0.03  |   | P35   | SurrC  | J38 | 14  | 0.18  | -0.55 | -0.08 |
| P34   | Surf C | J81 | 3   | 0.16  | 0.29  | 0.65  |   | P35   | Surf C | J38 | 15  | 0.08  | -0.27 | -0.05 |
| P34   | Surf C | J81 | 4   | -0.08 | 0.08  | -0.07 |   | P35   | SurrC  | J38 | 15  | 0.18  | -0.89 | -0.37 |
| P34   | Surf C | J81 | 4   | 0.40  | -0.75 | 0.30  |   | P35   | Surf C | J38 | 15  | 0.02  | 0.14  | 0.19  |
| P34   | Surf C | J81 | 5   | -0.03 | -0.18 | -0.24 |   | P35   | Sur C  | J38 | 15  | 0.05  | 0.06  | 0.17  |
| P34   | Surf C | J81 | 5   | 0.42  | -0.62 | 0.44  |   | P35   | Surf C | J38 | 15  | 0.15  | 0.21  | 0.51  |
| P34   | SurrC  | J81 | 6   | -0.03 | -0.20 | -0.26 |   | P35   | SurrC  | J38 | 10  | 0.02  | 0.14  | 0.19  |
| P34   | Surf C | J81 | 6   | 0.06  | -0.13 | 0.04  |   | P35   | Surf C | J38 | 16  | 0.15  | 0.21  | 0.51  |
| P34   | Surf C | J81 | /   | 0.02  | -0.46 | -0.39 |   | P35   | Surf C | J38 | 17  | -0.03 | 0.06  | 0.00  |
| P34   | Surf C | J81 | /   | 0.45  | 0.03  | 0.95  |   | P35   | Surf C | J38 | 17  | 0.09  | 0.08  | 0.26  |
| P34   | SurfE  | J80 | 1   | -0.09 |       |       |   | P35   | Surf C | J38 | 17  | 0.09  | 0.14  | 0.33  |
| P34   | SurrE  | J80 | 1   | 0.00  |       |       |   | P35   | SurrC  | J38 | 17  | 0.09  | -0.09 | 0.13  |
| P34   | Surf E | J80 | 2   | 0.03  |       |       |   | P35   | Surf C | J38 | 18  | -0.03 | 0.27  | 0.22  |
| P34   | Surf E | J80 | 2   | 0.13  |       |       |   | P35   | Surf C | J38 | 18  | 0.14  | 0.26  | 0.57  |
| P34   | Surf E | J80 | 3   | 0.12  |       |       |   | P35   | Surf C | J38 | 18  | -0.09 | 0.26  | 0.05  |
| P34   | Surf E | J80 | 3   | -0.04 |       |       |   | P35   | Surf C | J38 | 19  | -0.02 | 0.03  | 0.01  |
| P34   | Surf E | J80 | 3   | 0.10  |       |       |   | P35   | Surf C | J38 | 19  | -0.09 | 0.26  | 0.05  |
| P34   | Surf E | J80 | 4   | -0.01 |       |       |   | P35   | Surf C | J38 | 19  | 0.14  | 0.26  | 0.57  |
| P34   | Surf E | J80 | 5   | 0.03  |       |       |   | P35   | Surf C | J38 | 20  | -0.22 | 0.67  | 0.15  |
| P34   | Surf E | J80 | 5   | -0.06 |       |       |   | P35   | Surf C | J38 | 20  | 0.00  | 0.52  | 0.50  |
| P34   | Surf E | J80 | 5   | -0.05 |       |       |   | P35   | Surf C | J38 | 21  | -0.02 | 0.62  | 0.55  |
| P34   | Surf E | J80 | 6   | -0.23 |       |       |   | P35   | Surf C | J38 | 22  | -0.07 | 0.45  | 0.30  |
| P35   | Surf C | J32 | 2   | 0.20  | -1.07 | -0.53 |   |       |        |     |     |       |       |       |
| P35   | Surf C | J32 | 2   | -0.18 | 0.97  | 0.49  |   |       |        |     |     |       |       |       |
| P35   | Surf C | J32 | 2   | -0.18 | 0.17  | -0.27 |   |       |        |     |     |       |       |       |
| P35   | Surf C | J32 | 4   | -0.18 | 0.17  | -0.27 |   |       |        |     |     |       |       |       |
| P35   | Surf C | J32 | 5   | -0.11 | 0.48  | 0.16  |   |       |        |     |     |       |       |       |
| P35   | Surf C | J32 | 5   | 0.04  | 0.04  | 0.12  |   |       |        |     |     |       |       |       |
| P35   | Surf C | J32 | 5   | 0.02  | 0.60  | 0.56  |   |       |        |     |     |       |       |       |
| P35   | Surf C | J32 | 6   | -0.09 | 0.53  | 0.26  |   |       |        | -   |     |       |       |       |
| P35   | Surf C | J32 | 6   | -0.24 | 0.42  | -0.14 |   |       |        | -   |     |       |       |       |
| P35   | Surf C | J32 | 6   | -0.08 | 0.10  | -0.08 |   |       |        |     |     |       |       |       |
| P35   | Surf C | J32 | /   | 0.04  | 0.85  | 0.81  |   |       |        |     |     |       |       |       |
| P35   | SurrC  | J32 | 7   | -0.12 | 0.92  | 0.56  |   |       |        |     |     |       |       |       |
| P35   | Surf C | J32 | /   | -0.10 | 0.90  | 0.58  |   |       |        |     |     |       |       |       |
| P35   | SurrC  | J32 | 8   | 0.27  | 0.51  | 1.01  |   |       |        |     |     |       |       |       |
| P35   | Surf C | J38 | /   | -0.20 | -0.05 | -0.46 |   |       |        |     |     |       |       |       |
| P35   | SurrC  | J38 | /   | -0.06 | -0.36 | -0.43 |   |       |        |     |     |       |       |       |
| P35   | Surf C | J38 | 8   | 0.10  | -0.08 | 0.14  |   |       |        |     |     |       |       |       |
| P35   | Surf C | 138 | ×   | 0.02  | -0.53 | -0.41 |   |       |        |     |     |       |       |       |
| P35   | Surf C | 138 | 9   | 0.26  | -0.30 | 0.35  |   |       |        |     |     |       |       |       |
| P35   | Surf C | 138 | 10  | 0.13  | 0.72  | 0.93  |   |       |        |     |     |       |       |       |
| P35   | SurrC  | J38 | 10  | 0.02  | -0.36 | -0.26 |   |       |        |     |     |       |       |       |
| P35   | Surf C | J38 | 11  | 0.04  | 0.22  | 0.30  |   |       |        |     |     |       |       |       |
| P35   | Surf C | J38 | 11  | 0.10  | 0.20  | 0.40  |   |       |        |     |     |       |       |       |
| P35   | Surf C | J38 | 12  | 0.16  | 0.04  | 0.19  |   |       |        |     |     |       |       |       |
| P35   | Surf C | J38 | 13  | 0.14  | 0.10  | 0.40  | l |       |        |     |     |       |       |       |

## APPENDIX B — CALCULATION OF UNBIASED STANDARD DEVIATION VALUES FOR EACH LOT FOR EACH PROJECT

This appendix includes the calculations involved and lists the unbiased standard deviation for each lot on each project for which density or plant test results were obtained. The following tables also show the average unbiased lot standard deviation for each project. The calculations that are involved are illustrated in Exhibit B.1. The  $c_4$  factors used in the calculations are shown in Table B.1.

| Lot No.  | Lot Size   | Lot Mean | Lot St<br>Dev* | <i>C</i> 4 <sup>**</sup> | Unbiased<br>Lot St Dev*** |  |  |  |  |  |
|--|--|----------|----------------|--------------------------|---------------------------|--|--|--|--|--|
| 1  | 5  | 92.71    | 0.546          | 0.9400                   | 0.581                     |  |  |  |  |  |
| 3  | 6  | 91.83    | 0.863          | 0.9515                   | 0.907                     |  |  |  |  |  |
| 4  | 7  | 92.50    | 0.504          | 0.9594                   | 0.525                     |  |  |  |  |  |
| 5  | 6  | 92.15    | 0.489          | 0.9515                   | 0.514                     |  |  |  |  |  |
|  | Average  | 92.3     | 0.601          |                          | 0.632****                 |  |  |  |  |  |
| * calculated fr<br>** obtained fr<br>*** calculated  | * calculated from $s = \sqrt{\frac{\sum_{i=1}^{n} (X_i - \overline{X})^2}{n-1}}$<br>** obtained from Table B.1 for the sample size, $n$<br>*** calculated as $\frac{s}{c_4}$ |          |                |                          |                           |  |  |  |  |  |
| **** calculated as $\frac{\frac{S_1}{c_{4_1}} + \frac{S_3}{c_{4_3}} + \frac{S_4}{c_{4_4}} + \frac{S_5}{c_{4_5}}}{4}$ |  |          |                |                          |                           |  |  |  |  |  |

Exhibit B.1. Example of Calculating Unbiased Std Dev for Project P27, JMF J55

| Table B.1. c4 Factors for | <sup>.</sup> Various Sample Sizes, <i>n</i> |
|---------------------------|---|
|---------------------------|---|

| Sample Size, | _                     |
|--------------|-----------------------|
| n            | <i>c</i> <sub>4</sub> |
| 2            | 0.7979                |
| 3            | 0.8862                |
| 4            | 0.9213                |
| 5            | 0.9400                |
| 6            | 0.9515                |
| 7            | 0.9594                |
| 8            | 0.9650                |
| 9            | 0.9693                |
| 10           | 0.9727                |
| 11           | 0.9754                |
| 12           | 0.9776                |
| 13           | 0.9794                |
| 14           | 0.9810                |
| 15           | 0.9823                |
| 16           | 0.9835                |
| 17           | 0.9845                |
| 18           | 0.9854                |
| 19           | 0.9862                |
| 20           | 0.9869                |
| 21           | 0.9876                |
| 22           | 0.9882                |
| 23           | 0.9887                |
| 24           | 0.9892                |
| 25           | 0.9896                |
| Over 25      | а                     |

<sup>*a*</sup> 
$$(4n-4)/(4n-3)$$

| Project<br>Number | JMF<br>Number | Lot Size | Lot Mean | Lot St Dev<br>(biased) | $c_4$  | Lot St Dev<br>(unbiased) | Average   | Avg Lot SD | Course  |
|-------------------|---------------|----------|----------|------------------------|--------|--------------------------|-----------|------------|---------|
| P01               | J02           | 10       | 94.37    | 0.821                  | 0.9727 | 0.844                    | 201 11041 | ensideed   | Interm  |
| P01               | J02           | 1        | 92.47    | _                      | _      | _                        |           |            | Interm  |
| P01               | J02           | 5        | 93.81    | 0.746                  | 0.9400 | 0.794                    |           |            | Interm  |
| P01               | J02           | 6        | 93.58    | 0.862                  | 0.9515 | 0.906                    | 93.56     | 0.848      | Interm  |
| P01               | J10           | 1        | 92.32    | 0.101                  | 0.8862 | 0.114                    |           |            | Interm  |
| P01               | J10           | 4        | 93.07    | 0.546                  | 0.9213 | 0.593                    |           |            | Interm  |
| P01               | J10           | 5        | 92.54    | 0.167                  | 0.9213 | 0.181                    |           |            | Interm  |
| P01               | J10           | 7        | 93.10    | 0.977                  | 0.9400 | 1.039                    |           |            | Interm  |
| P01               | J10           | 13       | 92.76    | 0.487                  | 0.8862 | 0.550                    |           |            | Interm  |
| P01               | J10           | 18       | 92.95    | 0.557                  | 0.9400 | 0.593                    |           |            | Interm  |
| P01               | J10           | 20       | 93.18    | 0.508                  | 0.9515 | 0.534                    | 92.85     | 0.515      | Interm  |
| P23               | J33           | 1        | 91.96    | 1.587                  | 0.8862 | 1.791                    |           |            | Interm  |
| P23               | J33           | 2        | 91.23    | 1.572                  | 0.8862 | 1.774                    |           |            | Interm  |
| P23               | J33           | 3        | 91.84    | 1.426                  | 0.9400 | 1.517                    |           |            | Interm  |
| P23               | J33           | 4        | 91.48    | 1.422                  | 0.9400 | 1.513                    | 91.63     | 1.649      | Interm  |
| P32               | J76           | 2        | 93.84    | 0.817                  | 0.9693 | 0.843                    |           |            | Interm  |
| P32               | J76           | 3        | 94.23    | 1.120                  | 0.9515 | 1.177                    |           |            | Interm  |
| P32               | J76           | 4        | 92.79    | 0.548                  | 0.9727 | 0.563                    |           |            | Interm  |
| P32               | J76           | 5        | 93.09    | 0.856                  | 0.9727 | 0.880                    |           |            | Interm  |
| P32               | J76           | 6        | 93.02    | 0.750                  | 0.9727 | 0.771                    |           |            | Interm  |
| P32               | J76           | 7        | 92.09    | 1.437                  | 0.9515 | 1.510                    |           |            | Interm  |
| P32               | J76           | 8        | 92.49    | 0.988                  | 0.9594 | 1.030                    |           |            | Interm  |
| P32               | J76           | 9        | 93.33    | 1.738                  | 0.9515 | 1.827                    |           |            | Interm  |
| P32               | J76           | 10       | 93.34    | 0.964                  | 0.9693 | 0.995                    |           |            | Interm  |
| P32               | J76           | 11       | 93.60    | 0.770                  | 0.9693 | 0.794                    |           |            | Interm  |
| P32               | J76           | 12       | 93.69    | 0.972                  | 0.9727 | 0.999                    |           |            | Interm  |
| P32               | J76           | 13       | 93.38    | 0.781                  | 0.9594 | 0.814                    |           |            | Interm  |
| P32               | J76           | 14       | 93.56    | 1.381                  | 0.9515 | 1.451                    | 93.27     | 1.050      | Interm  |
| P33               | J73           | 5        | 93.59    | 2.214                  | 0.9400 | 2.355                    |           |            | Interm  |
| P33               | J73           | 7        | 93.19    | 2.129                  | 0.9594 | 2.219                    |           |            | Interm  |
| P33               | J73           | 5        | 92.78    | 0.918                  | 0.9400 | 0.977                    |           |            | Interm  |
| P33               | J73           | 10       | 93.49    | 0.960                  | 0.9727 | 0.987                    |           |            | Interm  |
| P33               | J73           | 7        | 93.24    | 1.004                  | 0.9594 | 1.046                    |           |            | Interm  |
| P33               | J73           | 9        | 92.81    | 1.335                  | 0.9693 | 1.377                    |           |            | Interm  |
| P33               | J73           | 7        | 93.53    | 1.371                  | 0.9594 | 1.429                    |           |            | Interm  |
| P33               | J73           | 6        | 92.75    | 1.219                  | 0.9515 | 1.281                    | 93.17     | 1.459      | Interm  |
| P01               | J07           | 5        | 92.50    | 0.217                  | 0.9400 | 0.231                    |           |            | Surface |
| P01               | J07           | 4        | 93.55    | 0.396                  | 0.9213 | 0.430                    |           |            | Surface |
| P01               | J07           | 6        | 93.19    | 0.346                  | 0.9515 | 0.364                    |           |            | Surface |
| P01               | J07           | 7        | 93.70    | 1.101                  | 0.9594 | 1.148                    | 93.24     | 0.543      | Surface |

Table B.2. Summary of Unbiased Lot Std Dev for Density for Each Interstate Paving Project

| Project | JMF    |          |          | Lot St Dev | _                     | Lot St Dev | Average  | Avg Lot SD | C       |
|---------|--------|----------|----------|------------|-----------------------|------------|----------|------------|---------|
| Number  | Number | Lot Size | Lot Mean | (biased)   | <i>c</i> <sub>4</sub> | (unbiased) | Lot Mean | Unbiased   | Course  |
| P26     | J62    | 8        | 93.39    | 2.154      | 0.9650                | 2.232      |          |            | Surface |
| P26     | J62    | 4        | 93.86    | 0.823      | 0.9213                | 0.893      |          |            | Surface |
| P26     | J62    | 3        | 92.48    | 0.295      | 0.8862                | 0.333      |          |            | Surface |
| P26     | J62    | 5        | 91.70    | 1.538      | 0.9400                | 1.636      |          |            | Surface |
| P26     | J62    | 5        | 92.81    | 1.195      | 0.9400                | 1.271      |          |            | Surface |
| P26     | J62    | 4        | 92.99    | 0.705      | 0.9213                | 0.765      |          |            | Surface |
| P26     | J62    | 5        | 93.07    | 0.878      | 0.9400                | 0.934      |          |            | Surface |
| P26     | J62    | 3        | 93.23    | 0.363      | 0.8862                | 0.410      |          |            | Surface |
| P26     | J62    | 5        | 92.05    | 0.931      | 0.9400                | 0.990      | 92.84    | 1.052      | Surface |
| P26     | J69    | 5        | 93.27    | 1.226      | 0.9400                | 1.304      |          |            | Surface |
| P26     | J69    | 6        | 93.00    | 2.265      | 0.9515                | 2.380      |          |            | Surface |
| P26     | J69    | 4        | 92.82    | 2.080      | 0.9213                | 2.258      |          |            | Surface |
| P26     | J69    | 5        | 94.13    | 0.564      | 0.9400                | 0.600      |          |            | Surface |
| P26     | J69    | 4        | 93.83    | 0.651      | 0.9213                | 0.707      |          |            | Surface |
| P26     | J69    | 5        | 94.29    | 0.664      | 0.9400                | 0.706      |          |            | Surface |
| P26     | J69    | 6        | 93.37    | 0.994      | 0.9515                | 1.045      |          |            | Surface |
| P26     | J69    | 5        | 93.10    | 0.721      | 0.9400                | 0.767      |          |            | Surface |
| P26     | J69    | 5        | 93.33    | 0.967      | 0.9400                | 1.029      |          |            | Surface |
| P26     | J69    | 5        | 93.26    | 1.282      | 0.9400                | 1.364      |          |            | Surface |
| P26     | J69    | 5        | 92.78    | 0.737      | 0.9400                | 0.784      |          |            | Surface |
| P26     | J69    | 6        | 92.38    | 1.020      | 0.9515                | 1.072      |          |            | Surface |
| P26     | J69    | 6        | 93.79    | 0.782      | 0.9515                | 0.822      |          |            | Surface |
| P26     | J69    | 6        | 94.38    | 0.674      | 0.9515                | 0.708      |          |            | Surface |
| P26     | J69    | 5        | 93.05    | 1.633      | 0.9400                | 1.737      |          |            | Surface |
| P26     | J69    | 3        | 93.54    | 0.650      | 0.8862                | 0.733      | 93.40    | 1.126      | Surface |
| P32     | J74    | 6        | 93.20    | 1.348      | 0.9515                | 1.417      | 93.20    | 1.417      | Surface |
| P32     | J79    | 10       | 93.03    | 0.817      | 0.9727                | 0.840      |          |            | Surface |
| P32     | J79    | 8        | 92.99    | 0.655      | 0.9650                | 0.679      |          |            | Surface |
| P32     | J79    | 10       | 92.98    | 1.174      | 0.9727                | 1.207      |          |            | Surface |
| P32     | J79    | 4        | 92.80    | 0.896      | 0.9213                | 0.973      |          |            | Surface |
| P32     | J79    | 10       | 92.78    | 0.706      | 0.9727                | 0.726      |          |            | Surface |
| P32     | J79    | 4        | 93.15    | 0.334      | 0.9213                | 0.363      |          |            | Surface |
| P32     | J79    | 8        | 93.03    | 0.520      | 0.9650                | 0.539      |          |            | Surface |
| P32     | J79    | 4        | 93.01    | 0.311      | 0.9213                | 0.338      |          |            | Surface |
| P32     | J79    | 9        | 92.53    | 1.713      | 0.9693                | 1.767      |          |            | Surface |
| P32     | J79    | 9        | 92.93    | 0.609      | 0.9693                | 0.628      |          |            | Surface |
| P32     | J79    | 11       | 92.77    | 0.489      | 0.9754                | 0.501      |          |            | Surface |
| P32     | J79    | 5        | 93.07    | 0.870      | 0.9400                | 0.926      |          |            | Surface |
| P32     | J79    | 5        | 91.26    | 0.663      | 0.9400                | 0.705      |          |            | Surface |
| P32     | J79    | 10       | 92.45    | 0.985      | 0.9727                | 1.013      |          |            | Surface |
| P32     | J79    | 6        | 92.21    | 1.104      | 0.9515                | 1.160      |          |            | Surface |
| P32     | J79    | 8        | 92.61    | 1.033      | 0.9650                | 1.070      |          |            | Surface |
| P32     | J79    | 5        | 92.50    | 0.479      | 0.9400                | 0.510      |          |            | Surface |
| P32     | J79    | 4        | 93.49    | 0.645      | 0.9213                | 0.700      |          |            | Surface |

## Table B.2. Summary of Unbiased Lot Std Dev for Density for Each Interstate Paving Project (continued)

| Project | JMF    | Lot Size | L of Mean | Lot St Dev | <b>C</b> . | Lot St Dev | Average  | Avg Lot SD | Course  |
|---------|--------|----------|-----------|------------|------------|------------|----------|------------|---------|
| Number  | Number | LOI SIZE |           | (biased)   | C4         | (unbiased) | Lot Mean | Unbiased   | Course  |
| P32     | J79    | 7        | 93.26     | 1.135      | 0.9594     | 1.183      |          |            | Surface |
| P32     | J79    | 5        | 92.47     | 0.408      | 0.9400     | 0.434      |          |            | Surface |
| P32     | J79    | 7        | 92.97     | 0.617      | 0.9594     | 0.643      |          |            | Surface |
| P32     | J79    | 8        | 92.95     | 1.120      | 0.9650     | 1.161      |          |            | Surface |
| P32     | J79    | 6        | 92.05     | 1.201      | 0.9515     | 1.262      |          |            | Surface |
| P32     | J79    | 3        | 93.19     | 1.344      | 0.8862     | 1.517      | 92.77    | 0.868      | Surface |
| P33     | J77    | 8        | 91.71     | 0.736      | 0.9650     | 0.763      |          |            | Surface |
| P33     | J77    | 8        | 93.54     | 1.144      | 0.9650     | 1.185      |          |            | Surface |
| P33     | J77    | 7        | 93.78     | 0.594      | 0.9594     | 0.619      |          |            | Surface |
| P33     | J77    | 7        | 91.68     | 1.967      | 0.9594     | 2.050      |          |            | Surface |
| P33     | J77    | 6        | 92.03     | 1.454      | 0.9515     | 1.528      |          |            | Surface |
| P33     | J77    | 4        | 93.55     | 0.756      | 0.9213     | 0.821      | 92.72    | 1.161      | Surface |
| P34     | J62    | 5        | 94.03     | 1.002      | 0.9400     | 1.066      |          |            | Surface |
| P34     | J62    | 5        | 92.58     | 1.314      | 0.9400     | 1.398      |          |            | Surface |
| P34     | J62    | 10       | 91.67     | 1.927      | 0.9727     | 1.981      |          |            | Surface |
| P34     | J62    | 5        | 93.74     | 1.461      | 0.9400     | 1.554      | 93.01    | 1.500      | Surface |
| P01     | J07    | 5        | 92.70     | 0.369      | 0.9400     | 0.393      |          |            | Surface |
| P01     | J07    | 4        | 92.99     | 0.648      | 0.9213     | 0.703      |          |            | Surface |
| P01     | J07    | 3        | 92.53     | 0.217      | 0.8862     | 0.245      |          |            | Surface |
| P01     | J07    | 5        | 92.35     | 0.128      | 0.9400     | 0.136      |          |            | Surface |
| P01     | J07    | 3        | 93.28     | 1.109      | 0.8862     | 1.251      | 92.77    | 0.546      | Surface |
| P03     | J15    | 4        | 93.56     | 0.606      | 0.9213     | 0.658      |          |            | Surface |
| P03     | J15    | 4        | 92.49     | 0.801      | 0.9213     | 0.869      |          |            | Surface |
| P03     | J15    | 10       | 92.80     | 1.583      | 0.9727     | 1.627      |          |            | Surface |
| P03     | J15    | 4        | 93.97     | 0.692      | 0.9213     | 0.751      |          |            | Surface |
| P03     | J15    | 3        | 94.25     | 0.778      | 0.8862     | 0.878      | 93.41    | 0.957      | Surface |
| P23     | J63    | 3        | 92.76     | 0.487      | 0.8862     | 0.550      |          |            | Surface |
| P23     | J63    | 3        | 93.10     | 0.487      | 0.8862     | 0.550      |          |            | Surface |
| P23     | J63    | 3        | 92.83     | 0.487      | 0.8862     | 0.550      |          |            | Surface |
| P23     | J63    | 3        | 92.87     | 0.487      | 0.8862     | 0.550      |          |            | Surface |
| P23     | J63    | 3        | 93.40     | 0.637      | 0.8862     | 0.719      |          |            | Surface |
| P23     | J63    | 3        | 93.71     | 0.643      | 0.8862     | 0.726      | 93.11    | 0.607      | Surface |
| P32     | J72    | 12       | 93.05     | 0.726      | 0.9776     | 0.743      |          |            | Surface |
| P32     | J72    | 14       | 92.89     | 0.641      | 0.9810     | 0.653      |          |            | Surface |
| P32     | J72    | 5        | 92.30     | 0.783      | 0.9400     | 0.833      |          |            | Surface |
| P32     | J72    | 5        | 93.40     | 1.298      | 0.9400     | 1.381      |          |            | Surface |
| P32     | J72    | 10       | 93.33     | 1.303      | 0.9727     | 1.340      |          |            | Surface |
| P32     | J72    | 9        | 93.61     | 0.525      | 0.9693     | 0.542      |          |            | Surface |
| P32     | J72    | 6        | 93.01     | 0.647      | 0.9515     | 0.680      |          |            | Surface |
| P32     | J72    | 9        | 92.86     | 0.642      | 0.9693     | 0.662      | 93.06    | 0.854      | Surface |

## Table B.2. Summary of Unbiased Lot Std Dev for Density for Each Interstate Paving Project (continued)

| Project<br>Number | JMF<br>Number | Lot Size | Lot Mean | Lot St Dev<br>(biased) | C4     | Lot St Dev<br>(unbiased) | Average<br>Lot Mean | Avg Lot SD<br>Unbiased | Course  |
|-------------------|---------------|----------|----------|------------------------|--------|--------------------------|---------------------|------------------------|---------|
| P01               | J23           | 5        | 93.68    | 0.970                  | 0.9400 | 1.032                    |                     |                        | Interm  |
| P01               | J23           | 3        | 93.86    | 1.572                  | 0.8862 | 1.774                    | 93.77               | 1.403                  | Interm  |
| P03               | J04           | 5        | 93.11    | 1.170                  | 0.9400 | 1.245                    |                     |                        | Interm  |
| P03               | J04           | 4        | 94.31    | 1.150                  | 0.9213 | 1.248                    |                     |                        | Interm  |
| P03               | J04           | 12       | 94.61    | 0.729                  | 0.9776 | 0.746                    |                     |                        | Interm  |
| P03               | J04           | 3        | 93.93    | 0.615                  | 0.8862 | 0.694                    |                     |                        | Interm  |
| P03               | J04           | 6        | 91.99    | 1.267                  | 0.9515 | 1.332                    | 93.59               | 1.053                  | Interm  |
| P36               | J09           | 3        | 93.06    | 0.318                  | 0.8862 | 0.359                    |                     |                        | Interm  |
| P36               | J09           | 3        | 93.17    | 1.364                  | 0.8862 | 1.539                    |                     |                        | Interm  |
| P36               | J09           | 7        | 92.51    | 1.445                  | 0.9594 | 1.506                    |                     |                        | Interm  |
| P36               | J09           | 4        | 92.71    | 1.943                  | 0.9213 | 2.109                    |                     |                        | Interm  |
| P36               | J09           | 4        | 92.71    | 1.943                  | 0.9213 | 2.109                    | 92.83               | 1.524                  | Interm  |
| P06               | J26           | 14       | 90.05    | 1.159                  | 0.9810 | 1.181                    | 90.05               | 1.181                  | Surface |
| P06               | J24           | 6        | 90.44    | 1.455                  | 0.9515 | 1.529                    |                     |                        | Surface |
| P06               | J24           | 6        | 89.83    | 1.669                  | 0.9515 | 1.754                    |                     |                        | Surface |
| P06               | J24           | 5        | 92.36    | 0.481                  | 0.9400 | 0.512                    |                     |                        | Surface |
| P06               | J24           | 4        | 93.37    | 0.565                  | 0.9213 | 0.613                    |                     |                        | Surface |
| P06               | J24           | 4        | 92.45    | 0.522                  | 0.9213 | 0.567                    | 91.69               | 0.995                  | Surface |
| P04               | J14           | 8        | 88.73    | 1.624                  | 0.9650 | 1.683                    |                     |                        | Surface |
| P04               | J14           | 8        | 90.28    | 0.605                  | 0.9650 | 0.627                    |                     |                        | Surface |
| P04               | J14           | 6        | 90.08    | 1.271                  | 0.9515 | 1.336                    |                     |                        | Surface |
| P04               | J14           | 9        | 89.95    | 1.186                  | 0.9693 | 1.224                    |                     |                        | Surface |
| P04               | J14           | 5        | 89.94    | 1.356                  | 0.9400 | 1.443                    | 89.80               | 1.262                  | Surface |
| P08               | J11           | 8        | 88.65    | 1.161                  | 0.9650 | 1.203                    | 88.65               | 1.203                  | Surface |
| P27               | J55           | 5        | 92.71    | 0.546                  | 0.9400 | 0.581                    |                     |                        | Surface |
| P27               | J55           | 6        | 91.83    | 0.863                  | 0.9515 | 0.907                    |                     |                        | Surface |
| P27               | J55           | 7        | 92.50    | 0.504                  | 0.9594 | 0.525                    |                     |                        | Surface |
| P27               | J55           | 6        | 92.15    | 0.489                  | 0.9515 | 0.514                    | 92.30               | 0.632                  | Surface |
| P27               | J70           | 5        | 93.22    | 1.498                  | 0.9400 | 1.594                    |                     |                        | Surface |
| P27               | J70           | 7        | 93.36    | 0.949                  | 0.9594 | 0.989                    |                     |                        | Surface |
| P27               | J70           | 4        | 92.32    | 0.559                  | 0.9213 | 0.607                    |                     |                        | Surface |
| P27               | J70           | 5        | 92.75    | 1.001                  | 0.9400 | 1.065                    |                     |                        | Surface |
| P27               | J70           | 3        | 93.38    | 0.757                  | 0.8862 | 0.854                    |                     |                        | Surface |
| P27               | J70           | 6        | 92.70    | 1.092                  | 0.9515 | 1.148                    |                     |                        | Surface |
| P27               | J70           | 3        | 92.72    | 1.222                  | 0.8862 | 1.379                    | 92.92               | 1.091                  | Surface |
| P30               | J65           | 5        | 93.57    | 3.130                  | 0.9400 | 3.330                    |                     |                        | Surface |
| P30               | J65           | 3        | 94.02    | 0.575                  | 0.8862 | 0.649                    | 93.80               | 1.989                  | Surface |
| P31               | J71           | 5        | 94.06    | 0.286                  | 0.9400 | 0.304                    |                     |                        | Surface |
| P31               | J71           | 3        | 94.24    | 0.822                  | 0.8862 | 0.928                    | 94.15               | 0.616                  | Surface |

## Table B.3. Summary of Unbiased Lot Std Dev for Density for Each Other Paving Project

| Project | JMF    | Lot Size | Lot Mean | Lot St Dev | 0      | Lot St Dev | Average  | Avg Lot SD | Course  |
|---------|--------|----------|----------|------------|--------|------------|----------|------------|---------|
| Number  | Number | LUI SIZE |          | (biased)   | C4     | (unbiased) | Lot Mean | Unbiased   | Course  |
| P13     | J03    | 9        | 92.01    | 1.519      | 0.9693 | 1.567      | 92.01    | 1.567      | Surface |
| P14     | J16    | 6        | 92.68    | 1.456      | 0.9515 | 1.530      |          |            | Surface |
| P14     | J16    | 7        | 92.92    | 1.035      | 0.9594 | 1.079      |          |            | Surface |
| P14     | J16    | 6        | 92.73    | 0.722      | 0.9515 | 0.759      |          |            | Surface |
| P14     | J16    | 10       | 91.75    | 1.788      | 0.9727 | 1.838      |          |            | Surface |
| P14     | J16    | 5        | 92.12    | 0.600      | 0.9400 | 0.638      |          |            | Surface |
| P14     | J16    | 4        | 93.07    | 1.135      | 0.9213 | 1.232      | 92.55    | 1.179      | Surface |
| P15     | J44    | 3        | 92.75    | 0.751      | 0.8862 | 0.847      |          |            | Surface |
| P15     | J44    | 3        | 92.56    | 0.751      | 0.8862 | 0.847      |          |            | Surface |
| P15     | J44    | 4        | 92.60    | 1.908      | 0.9213 | 2.071      |          |            | Surface |
| P15     | J44    | 4        | 92.90    | 1.919      | 0.9213 | 2.083      |          |            | Surface |
| P15     | J44    | 4        | 92.60    | 1.908      | 0.9213 | 2.071      | 92.68    | 1.584      | Surface |
| P16     | J20    | 4        | 91.38    | 1.445      | 0.9213 | 1.568      |          |            | Surface |
| P16     | J20    | 4        | 91.15    | 0.527      | 0.9213 | 0.572      |          |            | Surface |
| P16     | J20    | 4        | 92.22    | 0.967      | 0.9213 | 1.050      | 91.58    | 1.063      | Surface |
| P18     | J48    | 7        | 91.62    | 1.883      | 0.9594 | 1.963      |          |            | Surface |
| P18     | J48    | 3        | 92.01    | 1.960      | 0.8862 | 2.212      |          |            | Surface |
| P18     | J48    | 8        | 91.31    | 1.884      | 0.9650 | 1.952      | 91.65    | 2.042      | Surface |
| P20     | J50    | 11       | 92.63    | 0.936      | 0.9754 | 0.960      |          |            | Surface |
| P20     | J50    | 12       | 91.85    | 0.850      | 0.9776 | 0.869      |          |            | Surface |
| P20     | J50    | 11       | 92.17    | 0.916      | 0.9754 | 0.939      |          |            | Surface |
| P20     | J50    | 7        | 92.43    | 0.866      | 0.9594 | 0.903      |          |            | Surface |
| P20     | J50    | 8        | 92.72    | 1.239      | 0.9650 | 1.284      |          |            | Surface |
| P20     | J50    | 8        | 92.80    | 1.000      | 0.9650 | 1.036      |          |            | Surface |
| P20     | J50    | 10       | 92.36    | 0.610      | 0.9727 | 0.627      | 92.42    | 0.945      | Surface |
| P24     | J56    | 11       | 92.90    | 1.636      | 0.9754 | 1.677      |          |            | Surface |
| P24     | J56    | 4        | 93.80    | 0.637      | 0.9213 | 0.691      |          |            | Surface |
| P24     | J56    | 6        | 93.54    | 1.088      | 0.9515 | 1.143      |          |            | Surface |
| P24     | J56    | 8        | 92.57    | 0.825      | 0.9650 | 0.855      |          |            | Surface |
| P24     | J56    | 9        | 93.37    | 0.894      | 0.9693 | 0.922      |          |            | Surface |
| P24     | J56    | 9        | 93.15    | 0.629      | 0.9693 | 0.649      |          |            | Surface |
| P24     | J56    | 9        | 93.05    | 1.037      | 0.9693 | 1.070      | 93.20    | 1.001      | Surface |
| P26     | J59    | 6        | 91.69    | 0.945      | 0.9515 | 0.993      |          |            | Surface |
| P26     | J59    | 8        | 92.09    | 0.961      | 0.9650 | 0.996      |          |            | Surface |
| P26     | J59    | 7        | 90.40    | 1.338      | 0.9594 | 1.395      |          |            | Surface |
| P26     | J59    | 11       | 90.59    | 1.235      | 0.9754 | 1.266      |          |            | Surface |
| P26     | J59    | 6        | 91.16    | 0.706      | 0.9515 | 0.742      |          |            | Surface |
| P26     | J59    | 7        | 91.09    | 0.841      | 0.9594 | 0.877      |          |            | Surface |
| P26     | J59    | 8        | 90.06    | 1.795      | 0.9650 | 1.860      |          |            | Surface |
| P26     | J59    | 2        | 92.64    | 0.983      | 0.7979 | 1.232      | 91.22    | 1.170      | Surface |
| P28     | J39    | 7        | 92.98    | 0.999      | 0.9594 | 1.041      |          |            | Surface |
| P28     | J39    | 11       | 93.37    | 1.278      | 0.9754 | 1.310      |          |            | Surface |
| P28     | J39    | 7        | 93.27    | 1.861      | 0.9594 | 1.940      |          |            | Surface |
| P28     | J39    | 3        | 93.49    | 0.600      | 0.8862 | 0.677      | 93.56    | 0.848      | Surface |

 Table B.3. Summary of Unbiased Lot Std Dev for Density for Each Other Paving Project (continued)

| Project    | JMF | Lot Size | Lot Mean | Lot St Dev | <i>c</i> <sub>4</sub> | Lot St Dev | Average  | Avg Lot SD | Course  |
|------------|-----|----------|----------|------------|-----------------------|------------|----------|------------|---------|
|            |     | 6        | 0.022    |            | 0.0515                |            | Lot wear | Unbiaseu   | Paga    |
| P01        | 101 | 0        | -0.023   | 0.209      | 0.9010                | 0.220      |          |            | Dase    |
|            | 101 | 4        | 0.195    | 0.227      | 0.9213                | 0.240      |          |            | Dase    |
|            | 101 | <u> </u> | 0.193    | 0.291      | 0.0002                | 0.329      |          |            | Dase    |
| P01        | J01 | 3<br>1   | 0.213    | 0.135      | 0.0002                | 0.152      |          |            | Dase    |
| P01        | J01 | 1        | -0.360   | -          | 0 7070                | -          |          |            | Dase    |
| PUI<br>D04 | J01 | 2        | -0.110   | 0.057      | 0.7979                | 0.071      |          |            | Base    |
| P01        | J01 | 1        | 0.220    | -          | -                     | -          | 0.040    | 0.102      | Base    |
| PUI<br>D01 | J01 | 2        | -0.010   | 0.113      | 0.7979                | 0.142      | 0.040    | 0.193      | Base    |
| P01        | J02 | 6        | 0.067    | 0.172      | 0.9515                | 0.180      |          |            | Interm  |
| P01        | J02 | 3        | 0.253    | 0.145      | 0.8862                | 0.164      |          |            | Interm  |
| P01        | J02 | 2        | 0.160    | 0.184      | 0.7979                | 0.230      | 0.445    | 0.404      | Interm  |
| P01        | J02 | 1        | -0.020   | -          | -                     | -          | 0.115    | 0.191      | Interm  |
| P01        | J06 | 3        | 0.220    | 0.147      | 0.8862                | 0.166      |          |            | Base    |
| P01        | J06 | 4        | 0.048    | 0.239      | 0.9213                | 0.259      | 0.004    | 0.054      | Base    |
| P01        | J06 | 2        | 0.015    | 0.262      | 0.7979                | 0.328      | 0.094    | 0.251      | Base    |
| P01        | J07 | 3        | 0.120    | 0.190      | 0.8862                | 0.214      |          |            | Surface |
| P01        | J07 | 3        | 0.013    | 0.146      | 0.8862                | 0.164      |          |            | Surface |
| P01        | J07 | 5        | -0.052   | 0.237      | 0.9400                | 0.252      |          |            | Surface |
| P01        | J07 | 3        | 0.037    | 0.096      | 0.8862                | 0.108      |          |            | Surface |
| P01        | J07 | 3        | 0.073    | 0.163      | 0.8862                | 0.184      |          |            | Surface |
| P01        | J07 | 1        | -0.180   | -          | -                     | _          |          |            | Surface |
| P01        | J07 | 3        | 0.003    | 0.198      | 0.8862                | 0.223      |          |            | Surface |
| P01        | J07 | 5        | -0.208   | 0.122      | 0.9400                | 0.130      |          | 0.101      | Surface |
| P01        | J07 | 4        | 0.003    | 0.159      | 0.9213                | 0.173      | -0.021   | 0.181      | Surface |
| P01        | J10 | 3        | 0.117    | 0.119      | 0.8862                | 0.135      |          |            | Interm  |
| P01        | J10 | 1        | 0.290    | -          | -                     | -          |          |            | Interm  |
| P01        | J10 | 1        | -0.440   | -          | -                     | -          |          |            | Interm  |
| P01        | J10 | 4        | -0.023   | 0.273      | 0.9213                | 0.297      |          |            | Interm  |
| P01        | J10 | 3        | -0.013   | 0.103      | 0.8862                | 0.116      |          |            | Interm  |
| P01        | J10 | 1        | 0.140    | -          | -                     | -          |          |            | Interm  |
| P01        | J10 | 3        | -0.190   | 0.087      | 0.8862                | 0.098      |          |            | Interm  |
| P01        | J10 | 1        | 0.180    | _          | -                     | -          |          |            | Interm  |
| P01        | J10 | 1        | 0.130    | _          | -                     | -          |          |            | Interm  |
| P01        | J10 | 1        | -0.070   | -          | -                     | -          |          |            | Interm  |
| P01        | J10 | 2        | 0.240    | 0.269      | 0.7979                | 0.337      |          |            | Interm  |
| P01        | J10 | 2        | 0.075    | 0.035      | 0.7979                | 0.044      |          |            | Interm  |
| P01        | J10 | 4        | 0.043    | 0.083      | 0.9213                | 0.090      |          |            | Interm  |
| P01        | J10 | 2        | 0.180    | 0.071      | 0.7979                | 0.089      |          |            | Interm  |
| P01        | J10 | 2        | 0.035    | 0.134      | 0.7979                | 0.168      |          |            | Interm  |
| P01        | J10 | 3        | 0.050    | 0.226      | 0.8862                | 0.255      |          |            | Interm  |
| P01        | J10 | 2        | -0.235   | 0.049      | 0.7979                | 0.062      | 0.040    | 0.450      | Interm  |
| P01        | J10 | 3        | -0.217   | 0.160      | 0.8862                | 0.181      | 0.016    | 0.156      | Interm  |
| P01        | J18 | 4        | -0.103   | 0.254      | 0.9213                | 0.276      |          |            | Base    |
| P01        | J18 | 3        | -0.010   | 0.036      | 0.8862                | 0.041      |          |            | Base    |
| P01        | J18 | 4        | 0.045    | 0.230      | 0.9213                | 0.250      |          |            | Base    |
| P01        | J18 | 4        | 0.010    | 0.054      | 0.9213                | 0.058      |          |            | Base    |
| P01        | J18 | 3        | -0.040   | 0.135      | 0.8862                | 0.152      |          |            | Base    |

Table B.4. Summary of Unbiased Lot Std Dev for AC for Each Project

| Number         Classe         Classe <thclasse< th=""> <thclasse< th=""> <thclasse< th="" th<=""><th>Project</th><th>JMF</th><th>Lot Size</th><th>Lot Mean</th><th>Lot St Dev</th><th><math>c_4</math></th><th>Lot St Dev</th><th>Average</th><th>Avg Lot SD</th><th>Course</th></thclasse<></thclasse<></thclasse<>  | Project | JMF    | Lot Size | Lot Mean | Lot St Dev | $c_4$  | Lot St Dev | Average  | Avg Lot SD | Course  |
|--|---------|--------|----------|----------|------------|--------|------------|----------|------------|---------|
| P01         J18         J         0.123         0.230         0.8662         0.559         Base           P01         J18         4         -0.118         0.127         0.9213         0.138         Base           P01         J18         4         -0.118         0.127         0.9213         0.138         Base           P01         J18         4         -0.140         0.7979         0.514         Base           P01         J18         4         0.040         0.305         0.9213         0.331         Base           P01         J18         4         0.040         0.305         0.9213         0.331         Base           P01         J18         2         -0.035         0.290         0.7979         0.363         Base           P01         J18         1         -0.280         -         -         -         Base           P01         J18         1         -0.280         -         -         -         Base           P01         J18         1         -0.020         -         -         -         Base           P01         J18         2         0.070         0.014         0.7979         <   |         | Number | 2        | 0.400    | (blased)   | 0.0000 | (unblased) | Lot mean | Unblased   | Deee    |
| P01         J18         3         0.107         0.496         0.8213         0.138         Base           P01         J18         4         -0.130         0.410         0.7979         0.514         Base           P01         J18         1         -0.160         -         -         -         Base           P01         J18         1         -0.620         -         -         -         Base           P01         J18         1         -0.520         -         -         -         Base           P01         J18         2         -0.035         0.290         0.7979         0.363         Base           P01         J18         1         0.190         -         -         -         Base           P01         J18         1         -0.090         -         -         -         Base           P01         J18         1         -0.090         -         -         -         Base           P01         J18         3         0.000         0.121         0.8862         0.137         Base           P01         J18         2         0.010         0.7979         0.133         Base   | PUI     | J18    | 3        | 0.123    | 0.280      | 0.8862 | 0.316      |          |            | Base    |
| P01         J18         4         -0.118         0.127         0.123         0.138         Base           P01         J18         1         -0.160         -         -         -         Base           P01         J18         1         -0.160         -         -         -         Base           P01         J18         4         0.040         0.305         0.9213         0.331         Base           P01         J18         2         -0.035         0.290         0.7979         0.568         Base           P01         J18         2         -0.051         0.445         0.7979         0.558         Base           P01         J18         1         -0.280         -         -         -         Base           P01         J18         1         -0.090         -         -         -         Base           P01         J18         2         0.070         0.014         0.7979         0.018         Base           P01         J18         2         -0.070         0.170         0.7979         0.124         Base           P01         J18         2         -0.160         0.8962         0.203 <td>P01</td> <td>J18</td> <td>3</td> <td>0.107</td> <td>0.496</td> <td>0.8862</td> <td>0.559</td> <td></td> <td></td> <td>Base</td>   | P01     | J18    | 3        | 0.107    | 0.496      | 0.8862 | 0.559      |          |            | Base    |
| P01         J18         2         -0.130         0.410         0.7979         0.514         Base           P01         J18         4         0.040         0.305         0.9213         0.331         Base           P01         J18         1         -0.520         -         -         -         Base           P01         J18         2         0.615         0.240         0.7979         0.568         Base           P01         J18         1         0.190         -         -         -         Base           P01         J18         1         0.020         -         -         -         Base           P01         J18         1         -0.090         -         -         -         Base           P01         J18         3         0.000         0.121         0.8862         0.137         Base           P01         J18         2         -0.070         0.014         0.7979         0.133         Base           P01         J18         2         -0.045         0.106         0.7979         0.133         Base           P01         J18         2         -0.160         0.999         0.7979   | P01     | J18    | 4        | -0.118   | 0.127      | 0.9213 | 0.138      |          |            | Base    |
| P01         J18         1         -0.160         -         -         -         -         Base           P01         J18         1         -0.520         -         -         -         -         Base           P01         J18         2         -0.036         0.290         0.7979         0.363         Base           P01         J18         2         -0.036         0.490         0.7979         0.558         Base           P01         J18         1         0.190         -         -         -         Base           P01         J18         1         -0.280         -         -         -         Base           P01         J18         1         -0.280         -         -         -         Base           P01         J18         -0.280         0.121         0.8213         0.223         Base           P01         J18         -0.045         0.121         0.822         0.133         Base           P01         J18         2         -0.270         0.170         0.7979         0.213         Base           P01         J18         2         -0.160         0.180         0.8213 <t< td=""><td>P01</td><td>J18</td><td>2</td><td>-0.130</td><td>0.410</td><td>0.7979</td><td>0.514</td><td></td><td></td><td>Base</td></t<>  | P01     | J18    | 2        | -0.130   | 0.410      | 0.7979 | 0.514      |          |            | Base    |
| P01         J18         4         0.040         0.305         0.9213         0.331         Base           P01         J18         2         -0.035         0.290         0.7979         0.363         Base           P01         J18         2         -0.035         0.290         0.7979         0.558         Base           P01         J18         1         -0.280         -         -         -         Base           P01         J18         1         -0.090         -         -         -         Base           P01         J18         1         -0.090         -         -         -         Base           P01         J18         1         -0.090         -         -         -         Base           P01         J18         3         0.000         0.121         0.8862         0.137         Base           P01         J18         2         -0.070         0.014         0.7979         0.133         Base           P01         J18         2         -0.045         0.106         0.7979         0.124         Base           P01         J18         3         -0.160         0.8862         0.203 <td>P01</td> <td>J18</td> <td>1</td> <td>-0.160</td> <td>-</td> <td>-</td> <td>_</td> <td></td> <td></td> <td>Base</td>  | P01     | J18    | 1        | -0.160   | -          | -      | _          |          |            | Base    |
| P01         J18         1         -0.520         -         -         -         -         -         Base           P01         J18         2         -0.035         0.290         0.7979         0.363         Base           P01         J18         1         0.190         -         -         -         Base           P01         J18         1         -0.280         -         -         -         Base           P01         J18         1         -0.080         -         -         -         Base           P01         J18         4         -0.355         0.211         0.8213         0.229         Base           P01         J18         2         0.070         0.014         0.7979         0.213         Base           P01         J18         2         -0.270         0.170         0.7979         0.124         Base           P01         J18         2         -0.160         0.180         0.8862         0.203         Base           P01         J18         3         -0.020         0.144         0.8862         0.203         Base           P01         J18         3         -0.020   | P01     | J18    | 4        | 0.040    | 0.305      | 0.9213 | 0.331      |          |            | Base    |
| P01         J18         2         -0.035         0.290         0.7979         0.363         Base           P01         J18         1         0.190         -         -         -         Base           P01         J18         1         0.280         -         -         -         Base           P01         J18         1         -0.280         -         -         -         Base           P01         J18         4         -0.355         0.211         0.9213         0.229         Base           P01         J18         4         -0.355         0.211         0.8862         0.137         Base           P01         J18         2         -0.070         0.014         0.7979         0.131         Base           P01         J18         2         -0.045         0.106         0.7979         0.133         Base           P01         J18         2         -0.160         0.8862         0.203         Base           P01         J18         3         -0.020         0.164         0.9213         0.199         Base           P01         J18         3         -0.020         0.164         0.8862   | P01     | J18    | 1        | -0.520   | -          | —      | _          |          |            | Base    |
| P01         J18         2         0.615         0.445         0.7979         0.558         Base           P01         J18         1         0.190         -         -         -         Base           P01         J18         1         -0.280         -         -         -         Base           P01         J18         1         -0.280         -         -         -         Base           P01         J18         4         -0.355         0.211         0.9213         0.229         Base           P01         J18         2         0.070         0.014         0.7979         0.018         Base           P01         J18         1         -0.110         -         -         -         Base           P01         J18         1         -0.110         -         -         -         Base           P01         J18         2         -0.045         0.106         0.7979         0.133         Base           P01         J18         3         -0.160         0.8862         0.185         Base           P01         J18         2         -0.270         0.141         0.7979         0.177 <td< td=""><td>P01</td><td>J18</td><td>2</td><td>-0.035</td><td>0.290</td><td>0.7979</td><td>0.363</td><td></td><td></td><td>Base</td></td<>   | P01     | J18    | 2        | -0.035   | 0.290      | 0.7979 | 0.363      |          |            | Base    |
| P01         J18         1         0.190         -         -         -         -         Base           P01         J18         1         -0.280         -         -         -         Base           P01         J18         4         -0.355         0.211         0.9213         0.229         Base           P01         J18         3         0.000         0.121         0.8862         0.137         Base           P01         J18         2         -0.70         0.014         0.7979         0.213         Base           P01         J18         2         -0.270         0.170         0.7979         0.123         Base           P01         J18         2         -0.660         0.099         0.7979         0.124         Base           P01         J18         2         -0.610         0.160         0.7979         0.124         Base           P01         J18         3         -0.160         0.8862         0.203         Base           P01         J18         3         -0.025         0.129         0.7979         0.775         Base           P01         J18         2         -0.140         0.141  | P01     | J18    | 2        | 0.615    | 0.445      | 0.7979 | 0.558      |          |            | Base    |
| P01         J18         1         -0.280         -         -         -         -         Base           P01         J18         1         -0.090         -         -         -         Base           P01         J18         4         -0.355         0.211         0.8862         0.137         Base           P01         J18         2         0.070         0.014         0.7979         0.018         Base           P01         J18         2         -0.270         0.170         0.7979         0.133         Base           P01         J18         2         -0.245         0.106         0.7979         0.133         Base           P01         J18         2         0.160         0.8862         0.203         Base           P01         J18         3         -0.160         0.180         0.8862         0.203         Base           P01         J18         2         0.025         0.219         0.7979         0.275         Base           P01         J18         2         -0.250         0.141         0.7979         0.177         Base           P01         J18         2         -0.155         0.134  | P01     | J18    | 1        | 0.190    | -          | -      | _          |          |            | Base    |
| P01         J18         1         -0.090         -         -         -         -         Base           P01         J18         4         -0.355         0.211         0.9213         0.229         Base           P01         J18         2         0.070         0.014         0.7979         0.018         Base           P01         J18         2         -0.270         0.170         0.7979         0.213         Base           P01         J18         2         -0.045         0.106         0.7979         0.133         Base           P01         J18         2         -0.045         0.106         0.7979         0.124         Base           P01         J18         2         -0.045         0.106         0.7979         0.124         Base           P01         J18         3         -0.160         0.862         0.185         Base           P01         J18         3         -0.020         0.164         0.862         0.185         Base           P01         J18         2         -0.140         0.141         0.7979         0.177         Base           P01         J18         2         -0.140 <t< td=""><td>P01</td><td>J18</td><td>1</td><td>-0.280</td><td>-</td><td>_</td><td>-</td><td></td><td></td><td>Base</td></t<>   | P01     | J18    | 1        | -0.280   | -          | _      | -          |          |            | Base    |
| P01         J18         4         -0.355         0.211         0.9213         0.229         Base           P01         J18         3         0.000         0.121         0.8862         0.137         Base           P01         J18         2         0.070         0.014         0.7979         0.213         Base           P01         J18         1         -0.110         -         -         -         Base           P01         J18         2         -0.045         0.106         0.7979         0.124         Base           P01         J18         2         -0.160         0.099         0.7979         0.124         Base           P01         J18         3         -0.160         0.180         0.8862         0.203         Base           P01         J18         3         -0.020         0.164         0.8862         0.203         Base           P01         J18         2         -0.270         0.141         0.7979         0.275         Base           P01         J18         2         -0.180         0.014         0.7979         0.177         Base           P01         J18         3         -0.080  | P01     | J18    | 1        | -0.090   | -          | _      | -          |          |            | Base    |
| P01         J18         3         0.000         0.121         0.8862         0.137         Base           P01         J18         2         0.070         0.014         0.7979         0.018         Base           P01         J18         2         0.270         0.170         0.7979         0.213         Base           P01         J18         1         -0.110         -         -         -         Base           P01         J18         2         -0.045         0.106         0.7979         0.133         Base           P01         J18         3         -0.160         0.180         0.8862         0.203         Base           P01         J18         3         -0.020         0.164         0.8862         0.185         Base           P01         J18         2         -0.270         0.141         0.7979         0.275         Base           P01         J18         2         -0.180         0.014         0.7979         0.177         Base           P01         J18         2         -0.160         0.141         0.7979         0.168         Base           P01         J18         3         -0.080   | P01     | J18    | 4        | -0.355   | 0.211      | 0.9213 | 0.229      |          |            | Base    |
| P01         J18         2         0.070         0.014         0.7979         0.018         Base           P01         J18         2         -0.270         0.170         0.7979         0.213         Base           P01         J18         1         -0.105         0.106         0.7979         0.133         Base           P01         J18         2         -0.045         0.106         0.7979         0.124         Base           P01         J18         2         -0.160         0.180         0.8622         0.203         Base           P01         J18         4         -0.075         0.184         0.9213         0.199         Base           P01         J18         3         -0.020         0.141         0.7979         0.275         Base           P01         J18         2         -0.270         0.141         0.7979         0.177         Base           P01         J18         2         -0.140         0.141         0.7979         0.177         Base           P01         J18         2         -0.055         0.134         0.7979         0.168         Base           P01         J19         1         0.0   | P01     | J18    | 3        | 0.000    | 0.121      | 0.8862 | 0.137      |          |            | Base    |
| P01         J18         2         -0.270         0.170         0.7979         0.213         Base           P01         J18         1         -0.110         -         -         -         Base           P01         J18         2         -0.045         0.106         0.7979         0.133         Base           P01         J18         2         -0.160         0.180         0.8862         0.203         Base           P01         J18         3         -0.020         0.164         0.8862         0.185         Base           P01         J18         2         -0.025         0.219         0.7979         0.177         Base           P01         J18         2         -0.025         0.219         0.7979         0.177         Base           P01         J18         2         -0.270         0.141         0.7979         0.177         Base           P01         J18         2         -0.140         0.141         0.7979         0.177         Base           P01         J18         3         -0.055         0.134         0.7979         0.168         Base           P01         J19         1         0.260   | P01     | J18    | 2        | 0.070    | 0.014      | 0.7979 | 0.018      |          |            | Base    |
| P01         J18         1         -0.110         -         -         -         -         Base           P01         J18         2         -0.045         0.106         0.7979         0.133         Image: State Sta   | P01     | J18    | 2        | -0.270   | 0.170      | 0.7979 | 0.213      |          |            | Base    |
| P01         J18         2         -0.045         0.106         0.7979         0.133         Base           P01         J18         2         0.160         0.099         0.7979         0.124         Base           P01         J18         3         -0.160         0.180         0.8862         0.203         Base           P01         J18         3         -0.020         0.164         0.8862         0.199         Base           P01         J18         2         0.025         0.219         0.7979         0.275         Base           P01         J18         2         -0.270         0.141         0.7979         0.177         Base           P01         J18         2         -0.160         0.141         0.7979         0.177         Base           P01         J18         2         -0.160         0.141         0.7979         0.168         Base           P01         J18         2         -0.055         0.134         0.7979         0.168         Base           P01         J19         1         0.200         -         -         -         Surface           P01         J19         1         0.200   | P01     | J18    | 1        | -0.110   | -          | _      | —          |          |            | Base    |
| P01         J18         2         0.160         0.099         0.7979         0.124         Base           P01         J18         3         -0.160         0.180         0.8862         0.203         Base           P01         J18         4         -0.075         0.184         0.9213         0.199         Base           P01         J18         2         0.020         0.164         0.8862         0.185         Base           P01         J18         2         0.025         0.219         0.7979         0.177         Base           P01         J18         2         -0.270         0.141         0.7979         0.177         Base           P01         J18         2         -0.140         0.141         0.7979         0.168         Base           P01         J18         2         -0.140         0.441         0.7979         0.168         Base           P01         J18         2         -0.050         0.214         0.8862         0.227         -0.056         0.224         Base           P01         J19         1         0.200         -         -         -         Surface           P01         J19   | P01     | J18    | 2        | -0.045   | 0.106      | 0.7979 | 0.133      |          |            | Base    |
| P01       J18       3       -0.160       0.180       0.8862       0.203       Image: constraint of the state of the sta         | P01     | J18    | 2        | 0.160    | 0.099      | 0.7979 | 0.124      |          |            | Base    |
| P01         J18         4         -0.075         0.184         0.9213         0.199         Image: constraint of the system           P01         J18         3         -0.020         0.164         0.8862         0.185         Image: constraint of the system         Base           P01         J18         2         0.025         0.219         0.7979         0.275         Image: constraint of the system         Base           P01         J18         2         -0.270         0.141         0.7979         0.177         Image: constraint of the system         Base           P01         J18         2         -0.140         0.141         0.7979         0.177         Image: constraint of the system         Base           P01         J18         2         -0.055         0.134         0.7979         0.168         Image: constraint of the system         Base           P01         J18         3         -0.080         0.201         0.8862         0.227         -0.056         0.224         Base           P01         J19         1         0.260         -         -         -         Surface           P01         J19         1         0.200         -         -         -         Surface  | P01     | J18    | 3        | -0.160   | 0.180      | 0.8862 | 0.203      |          |            | Base    |
| P01         J18         3         -0.020         0.164         0.8862         0.185         Image: constraint of the system           P01         J18         2         0.025         0.219         0.7979         0.275         Image: constraint of the system           P01         J18         2         -0.270         0.141         0.7979         0.177         Image: constraint of the system           P01         J18         2         -0.140         0.141         0.7979         0.177         Image: constraint of the system           P01         J18         2         -0.140         0.141         0.7979         0.168         Image: constraint of the system           P01         J18         2         -0.055         0.134         0.7979         0.168         Image: constraint of the system           P01         J18         3         -0.080         0.201         0.8862         0.227         -0.056         0.224         Base           P01         J19         1         0.020         -         -         -         Surface           P01         J19         1         0.260         -         -         -         Surface           P01         J19         1         0.020   | P01     | J18    | 4        | -0.075   | 0.184      | 0.9213 | 0.199      |          |            | Base    |
| P01         J18         2         0.025         0.219         0.7979         0.275         Base           P01         J18         2         -0.270         0.141         0.7979         0.177         Base           P01         J18         2         -0.180         0.014         0.7979         0.018         Base           P01         J18         2         -0.140         0.141         0.7979         0.177         Base           P01         J18         2         -0.055         0.134         0.7979         0.168         Base           P01         J18         2         -0.055         0.134         0.7979         0.168         Base           P01         J18         3         -0.080         0.201         0.8862         0.227         -0.056         0.224         Base           P01         J19         1         0.200         -         -         -         Surface           P01         J19         2         -0.030         0.042         0.7979         0.053         Surface           P01         J19         1         0.140         -         -         -         Surface           P01         J19   | P01     | J18    | 3        | -0.020   | 0.164      | 0.8862 | 0.185      |          |            | Base    |
| P01         J18         2         -0.270         0.141         0.7979         0.177         Image: Margin and Strath and St | P01     | J18    | 2        | 0.025    | 0.219      | 0.7979 | 0.275      |          |            | Base    |
| P01         J18         2         -0.180         0.014         0.7979         0.018         Image: constraint of the state of t | P01     | J18    | 2        | -0.270   | 0.141      | 0.7979 | 0.177      |          |            | Base    |
| P01         J18         2         -0.140         0.141         0.7979         0.177         Image: constraint of the straint of th | P01     | J18    | 2        | -0.180   | 0.014      | 0.7979 | 0.018      |          |            | Base    |
| P01         J18         2         -0.055         0.134         0.7979         0.168         Image: Married Science Scien | P01     | J18    | 2        | -0.140   | 0.141      | 0.7979 | 0.177      |          |            | Base    |
| P01         J18         3         -0.080         0.201         0.8862         0.227         -0.056         0.224         Base           P01         J19         1         0.020         -         -         -         Surface           P01         J19         1         0.260         -         -         -         Surface           P01         J19         2         -0.030         0.042         0.7979         0.053         Surface           P01         J19         2         -0.095         0.078         0.7979         0.097         Surface           P01         J19         1         0.020         -         -         -         Surface           P01         J19         1         0.140         -         -         -         Surface           P01         J19         1         0.140         -         -         -         Surface           P01         J19         1         0.200         -         -         -         Surface           P01         J19         1         0.020         -         -         -         Surface           P01         J19         1         0.010         - </td <td>P01</td> <td>J18</td> <td>2</td> <td>-0.055</td> <td>0.134</td> <td>0.7979</td> <td>0.168</td> <td></td> <td></td> <td>Base</td>  | P01     | J18    | 2        | -0.055   | 0.134      | 0.7979 | 0.168      |          |            | Base    |
| P01         J19         1         0.020         -         -         -         -         Surface           P01         J19         1         0.260         -         -         -         -         Surface           P01         J19         2         -0.030         0.042         0.7979         0.053         Surface           P01         J19         2         -0.095         0.078         0.7979         0.097         Surface           P01         J19         1         0.020         -         -         -         Surface           P01         J19         1         0.140         -         -         -         Surface           P01         J19         1         0.140         -         -         -         Surface           P01         J19         1         0.140         -         -         -         Surface           P01         J19         1         0.220         -         -         -         Surface           P01         J19         1         0.020         -         -         -         Surface           P01         J19         1         0.020         -         - <td>P01</td> <td>J18</td> <td>3</td> <td>-0.080</td> <td>0.201</td> <td>0.8862</td> <td>0.227</td> <td>-0.056</td> <td>0.224</td> <td>Base</td>  | P01     | J18    | 3        | -0.080   | 0.201      | 0.8862 | 0.227      | -0.056   | 0.224      | Base    |
| P01         J19         1         0.260         -         -         -         -         Surface           P01         J19         2         -0.030         0.042         0.7979         0.053         Surface           P01         J19         2         -0.095         0.078         0.7979         0.097         Surface           P01         J19         1         0.020         -         -         -         Surface           P01         J19         1         0.140         -         -         -         Surface           P01         J19         1         0.140         -         -         -         Surface           P01         J19         1         0.140         -         -         -         Surface           P01         J19         1         0.220         -         -         -         Surface           P01         J19         1         0.220         -         -         -         Surface           P01         J19         1         0.020         -         -         -         Surface           P01         J19         1         0.010         -         -         - <td>P01</td> <td>J19</td> <td>1</td> <td>0.020</td> <td>_</td> <td>_</td> <td>_</td> <td></td> <td></td> <td>Surface</td>  | P01     | J19    | 1        | 0.020    | _          | _      | _          |          |            | Surface |
| P01         J19         2         -0.030         0.042         0.7979         0.053         Surface           P01         J19         2         -0.095         0.078         0.7979         0.097         Surface           P01         J19         1         0.020         -         -         -         Surface           P01         J19         1         0.140         -         -         -         Surface           P01         J19         1         0.220         -         -         -         Surface           P01         J19         1         0.020         -         -         -         Surface           P01         J19         1         0.010         -         -         -         Surface           P01         J19         1         0.010         -         -         -         Surf   | P01     | J19    | 1        | 0.260    | _          | _      | _          |          |            | Surface |
| P01         J19         2         -0.095         0.078         0.7979         0.097         Surface           P01         J19         1         0.020         -         -         -         Surface           P01         J19         1         0.140         -         -         -         Surface           P01         J19         1         0.220         -         -         -         Surface           P01         J19         1         0.220         -         -         -         Surface           P01         J19         1         0.020         -         -         -         Surface           P01         J19         1         0.010         -         -         -         Surface           P01         J19         1         0.010         -         -         -         Surface     <  | P01     | J19    | 2        | -0.030   | 0.042      | 0.7979 | 0.053      |          |            | Surface |
| P01         J19         1         0.020         -         -         -         -         Surface           P01         J19         1         0.140         -         -         -         Surface           P01         J19         1         0.140         -         -         -         Surface           P01         J19         1         0.220         -         -         -         Surface           P01         J19         1         0.220         -         -         -         Surface           P01         J19         1         0.220         -         -         -         Surface           P01         J19         1         0.020         -         -         -         Surface           P01         J19         1         0.010         -         -         -         Surface           P01         J19         1         0.010         -         -         -         Surface           P01         J19         1         0.010         -         -         -         Surface           P01         J19         1         0.410         -         -         -         O.101  | P01     | J19    | 2        | -0.095   | 0.078      | 0.7979 | 0.097      |          |            | Surface |
| P01         J19         1         0.140         -         -         -         -         Surface           P01         J19         1         0.140         -         -         -         -         Surface           P01         J19         1         0.220         -         -         -         -         Surface           P01         J19         2         0.100         0.156         0.7979         0.195         Surface           P01         J19         1         0.020         -         -         -         Surface           P01         J19         1         0.020         -         -         -         Surface           P01         J19         1         0.010         -         -         -         Surface           P01         J19         1         0.010         -         -         -         Surface           P01         J19         1         0.010         -         -         -         Surface           P01         J19         1         0.410         -         -         -         Surface           P01         J19         1         0.410         -   | P01     | J19    | 1        | 0.020    | _          | -      | _          |          |            | Surface |
| P01         J19         1         0.140         -         -         -         -         Surface           P01         J19         1         0.220         -         -         -         -         Surface           P01         J19         2         0.100         0.156         0.7979         0.195         Surface           P01         J19         1         0.020         -         -         -         Surface           P01         J19         1         0.020         -         -         -         Surface           P01         J19         1         0.010         -         -         -         Surface           P01         J19         1         0.010         -         -         -         Surface           P01         J19         1         0.010         -         -         -         Surface           P01         J19         1         0.410         -         -         -         Surface           P01         J19         1         0.090         -         -         -         0.101         0.146         Surface           P01         J21         1         0.320   | P01     | J19    | 1        | 0.140    | _          | _      | _          |          |            | Surface |
| P01         J19         1         0.220         -         -         -         -         Surface           P01         J19         2         0.100         0.156         0.7979         0.195         Surface           P01         J19         1         0.020         -         -         -         Surface           P01         J19         1         0.020         -         -         -         Surface           P01         J19         1         0.010         -         -         -         Surface           P01         J19         1         0.010         -         -         -         Surface           P01         J19         2         0.105         0.191         0.7979         0.239         Surface           P01         J19         1         0.410         -         -         -         Surface           P01         J19         1         0.090         -         -         -         0.101         0.146         Surface           P01         J21         1         0.320         -         -         -         -         Base           P01         J21         3         0.137   | P01     | J19    | 1        | 0.140    | _          | -      | _          |          |            | Surface |
| P01         J19         2         0.100         0.156         0.7979         0.195         Surface           P01         J19         1         0.020         -         -         -         Surface           P01         J19         1         0.010         -         -         -         Surface           P01         J19         1         0.010         -         -         -         Surface           P01         J19         2         0.105         0.191         0.7979         0.239         Surface           P01         J19         1         0.410         -         -         -         Surface           P01         J19         1         0.410         -         -         -         Surface           P01         J19         1         0.410         -         -         -         0.101         0.146         Surface           P01         J21         1         0.320         -         -         -         -         Base           P01         J21         1         0.170         -         -         -         -         Base           P01         J21         3         0.137 <td>P01</td> <td>J19</td> <td>1</td> <td>0.220</td> <td>_</td> <td>-</td> <td>_</td> <td></td> <td></td> <td>Surface</td>  | P01     | J19    | 1        | 0.220    | _          | -      | _          |          |            | Surface |
| P01         J19         1         0.020         -         -         -         -         Surface           P01         J19         1         0.010         -         -         -         -         Surface           P01         J19         1         0.010         -         -         -         -         Surface           P01         J19         2         0.105         0.191         0.7979         0.239         Surface           P01         J19         1         0.410         -         -         -         Surface           P01         J19         1         0.090         -         -         -         0.101         0.146         Surface           P01         J21         1         0.320         -         -         -         0.101         0.146         Surface           P01         J21         1         0.320         -         -         -         Base           P01         J21         1         0.170         -         -         -         Base           P01         J21         3         0.137         0.119         0.8862         0.135         Base           P01 <td>P01</td> <td>J19</td> <td>2</td> <td>0.100</td> <td>0.156</td> <td>0.7979</td> <td>0.195</td> <td></td> <td></td> <td>Surface</td>  | P01     | J19    | 2        | 0.100    | 0.156      | 0.7979 | 0.195      |          |            | Surface |
| P01         J19         1         0.010         -         -         -         -         Surface           P01         J19         2         0.105         0.191         0.7979         0.239         Surface           P01         J19         1         0.410         -         -         -         Surface           P01         J19         1         0.410         -         -         -         Surface           P01         J19         1         0.090         -         -         -         0.101         0.146         Surface           P01         J21         1         0.320         -         -         -         0.101         0.146         Surface           P01         J21         1         0.320         -         -         -         -         Base           P01         J21         1         0.170         -         -         -         Base           P01         J21         3         0.137         0.119         0.8862         0.135         Base           P01         J21         3         0.003         0.232         0.8862         0.261         Base           P01   | P01     | J19    | 1        | 0.020    | _          | _      | _          |          |            | Surface |
| P01         J19         2         0.105         0.191         0.7979         0.239         Surface           P01         J19         1         0.410         -         -         -         Surface           P01         J19         1         0.410         -         -         -         Surface           P01         J19         1         0.090         -         -         -         0.101         0.146         Surface           P01         J21         1         0.320         -         -         -         0.101         0.146         Surface           P01         J21         1         0.320         -         -         -         Base           P01         J21         1         0.170         -         -         -         Base           P01         J21         3         0.137         0.119         0.8862         0.135         Base           P01         J21         3         0.003         0.232         0.8862         0.261         Base           P01         J21         1         0.370         -         -         -          Base   | P01     | J19    | 1        | 0.010    | _          | _      | -          |          |            | Surface |
| P01         J19         1         0.410         -         -         -         Surface           P01         J19         1         0.090         -         -         -         0.101         0.146         Surface           P01         J19         1         0.090         -         -         -         0.101         0.146         Surface           P01         J21         1         0.320         -         -         -         Base           P01         J21         1         0.170         -         -         -         Base           P01         J21         3         0.137         0.119         0.8862         0.135         Base           P01         J21         3         0.003         0.232         0.8862         0.261         Base           P01         J21         1         0.370         -         -         -         Base   | P01     | J19    | 2        | 0.105    | 0.191      | 0.7979 | 0.239      |          |            | Surface |
| P01         J19         1         0.090         -         -         -         0.101         0.146         Surface           P01         J21         1         0.320         -         -         -         0.101         0.146         Surface           P01         J21         1         0.320         -         -         -         -         Base           P01         J21         1         0.170         -         -         -         Base           P01         J21         3         0.137         0.119         0.8862         0.135         Base           P01         J21         3         0.003         0.232         0.8862         0.261         Base           P01         J21         1         0.370         -         -         -         Base   | P01     | J19    | 1        | 0.410    | _          | _      | _          |          |            | Surface |
| P01         J21         1         0.320         -         -         -         -         Base           P01         J21         1         0.170         -         -         -         Base           P01         J21         1         0.170         -         -         -         Base           P01         J21         3         0.137         0.119         0.8862         0.135         Base           P01         J21         3         0.003         0.232         0.8862         0.261         Base           P01         J21         1         0.370         -         -         -         Base  | P01     | J19    | 1        | 0.090    | _          | _      | _          | 0.101    | 0.146      | Surface |
| P01         J21         1         0.170         -         -         -         Base           P01         J21         3         0.137         0.119         0.8862         0.135         Base           P01         J21         3         0.003         0.232         0.8862         0.261         Base           P01         J21         3         0.003         0.232         0.8862         0.261         Base   | P01     | J21    | 1        | 0.320    | _          | _      | _          |          |            | Base    |
| P01         J21         3         0.137         0.119         0.8862         0.135         Base           P01         J21         3         0.003         0.232         0.8862         0.261         Base           P01         J21         3         0.003         0.232         0.8862         0.261         Base           P01         J21         1         0.370         -         -         -         Base   | P01     | J21    | 1        | 0.170    | _          | _      | _          |          |            | Base    |
| P01         J21         3         0.003         0.232         0.8862         0.261         Base           P01         J21         1         0.370         -         -         -         Base   | P01     | J21    | 3        | 0.137    | 0.119      | 0,8862 | 0.135      |          |            | Base    |
| P01  | P01     | J21    | 3        | 0.003    | 0.232      | 0.8862 | 0.261      |          |            | Base    |
|  | P01     | J21    | 1        | 0.370    | _          | -      | _          |          |            | Base    |

Table B.4. Summary of Unbiased Lot Std Dev for AC for Each Project (continued)

| Project | JMF  | Lot Size | Lot Mean | Lot St Dev | <i>c</i> <sub>4</sub> | Lot St Dev | Average   | Avg Lot SD | Course  |
|---------|------|----------|----------|------------|-----------------------|------------|-----------|------------|---------|
|         |      | 3        | 0.017    | 0.340      | 0.8862                |            | LOUIVIEAN | Unbiaseu   | Base    |
| P01     | 121  | 3        | 0.017    | 0.340      | 0.0002                | 0.303      |           |            | Base    |
| P01     | 121  | 1        | 0.240    | 0.304      | 0.0002                | 0.433      |           |            | Base    |
| P01     | 121  | 1        | 0.000    |            |                       |            |           |            | Base    |
| P01     | 121  | 2        | 0.000    | 0.665      | 0 7070                | 0.833      |           |            | Base    |
| P01     | 121  | 1        | 0.020    | 0.000      | 0.1313                | 0.000      |           |            | Base    |
| P01     | .121 | 1        | -0.050   | _          | _                     | _          |           |            | Base    |
| P01     | .121 | 1        | 0.000    | _          | _                     | _          |           |            | Base    |
| P01     | .121 | 3        | 0.020    | 0 241      | 0 8862                | 0.272      |           |            | Base    |
| P01     | J21  | 2        | -0.090   | 0.028      | 0 7979                | 0.035      | 0 132     | 0.336      | Base    |
| P01     | .123 | 4        | 0.285    | 0.222      | 0.9213                | 0.241      | 01102     | 0.000      | Interm  |
| P01     | .123 | 3        | -0.083   | 0.422      | 0.8862                | 0.476      |           |            | Interm  |
| P01     | J23  | 1        | -0.060   | _          | -                     | _          |           |            | Interm  |
| P01     | J23  | 2        | 0.010    | 0.424      | 0.7979                | 0.532      |           |            | Interm  |
| P01     | J23  | 1        | 0.330    | _          | _                     | -          |           |            | Interm  |
| P01     | J23  | 1        | 0.080    | _          | _                     | _          | 0.094     | 0.417      | Interm  |
| P02     | J04  | 4        | 0.185    | 0.145      | 0.9213                | 0.157      |           |            | Interm  |
| P02     | J04  | 1        | 0.250    | _          | _                     | _          |           |            | Interm  |
| P02     | J04  | 2        | 0.030    | 0.042      | 0.7979                | 0.053      |           |            | Interm  |
| P02     | J04  | 2        | 0.250    | 0.184      | 0.7979                | 0.230      |           |            | Interm  |
| P02     | J04  | 4        | 0.113    | 0.171      | 0.9213                | 0.186      |           |            | Interm  |
| P02     | J04  | 1        | 0.780    | _          | _                     | _          |           |            | Interm  |
| P02     | J04  | 4        | 0.038    | 0.186      | 0.9213                | 0.202      |           |            | Interm  |
| P02     | J04  | 1        | 0.360    | _          | _                     | _          |           |            | Interm  |
| P02     | J04  | 1        | 0.380    | _          | _                     | _          |           |            | Interm  |
| P02     | J04  | 2        | 0.030    | 0.269      | 0.7979                | 0.337      |           |            | Interm  |
| P02     | J04  | 3        | 0.087    | 0.270      | 0.8862                | 0.304      |           |            | Interm  |
| P02     | J04  | 1        | 0.210    | _          | _                     | _          |           |            | Interm  |
| P02     | J04  | 1        | -0.090   | _          | -                     | _          |           |            | Interm  |
| P02     | J04  | 3        | -0.080   | 0.209      | 0.8862                | 0.236      | 0.182     | 0.213      | Interm  |
| P02     | J05  | 2        | -0.005   | 0.021      | 0.7979                | 0.027      |           |            | Surface |
| P02     | J05  | 1        | -0.070   | _          | _                     | _          |           |            | Surface |
| P02     | J05  | 2        | 0.035    | 0.106      | 0.7979                | 0.133      |           |            | Surface |
| P02     | J05  | 1        | -0.120   | -          | I                     | _          |           |            | Surface |
| P02     | J05  | 1        | -0.190   | -          | I                     | _          |           |            | Surface |
| P02     | J05  | 1        | 0.280    | _          | -                     | —          | -0.012    | 0.080      | Surface |
| P02     | J09  | 1        | 0.220    | _          | -                     | _          |           |            | Interm  |
| P02     | J09  | 2        | 0.030    | 0.071      | 0.7979                | 0.089      |           |            | Interm  |
| P02     | J09  | 1        | 0.430    | _          | -                     | _          |           |            | Interm  |
| P02     | J09  | 3        | 0.290    | 0.358      | 0.8862                | 0.404      |           |            | Interm  |
| P02     | J09  | 2        | -0.090   | 0.283      | 0.7979                | 0.354      |           |            | Interm  |
| P02     | J09  | 2        | 0.150    | 0.127      | 0.7979                | 0.160      |           |            | Interm  |
| P02     | J09  | 1        | -0.450   | -          | _                     | -          |           |            | Interm  |
| P02     | J09  | 1        | 0.100    | -          | -                     | -          |           |            | Interm  |
| P02     | J09  | 2        | -0.125   | 0.078      | 0.7979                | 0.097      |           |            | Interm  |
| P02     | J09  | 3        | 0.240    | 0.121      | 0.8862                | 0.137      |           |            | Interm  |
| P02     | J09  | 2        | -0.140   | 0.014      | 0.7979                | 0.018      |           |            | Interm  |

| Table B.4. Summary of Unbiased | Lot Std Dev for | AC for Each P | roject (continued) |
|--------------------------------|-----------------|---------------|--------------------|
|--------------------------------|-----------------|---------------|--------------------|
| Project | JMF<br>Number | Lot Size | Lot Mean | Lot St Dev | <i>c</i> <sub>4</sub> | Lot St Dev | Average  | Avg Lot SD | Course  |
|---------|---------------|----------|----------|------------|-----------------------|------------|----------|------------|---------|
|         |               | 2        | -0.160   | 0 255      | 0 7070                |            | LOUINEan | Unbiaseu   | Interm  |
| P02     | 100           | <br>1    | -0.100   | 0.200      | 0.7979                | 0.519      |          |            | Interm  |
| P02     | 100           | 1        | 0.210    | - 0.210    | 0.0212                | -          |          |            | Interm  |
| P02     | 100           | 4        | 0.000    | 0.210      | 0.9213                | 0.227      |          |            | Interm  |
| P02     | 109           |          | -0.230   | 0.057      | 0.7979                | 0.071      |          |            | Interm  |
| P02     | 100           | 1        | -0.160   | -          | 0 7070                | -          |          |            | Interm  |
| P02     | 109           | 2        | -0.050   | 0.099      | 0.7979                | 0.124      | 0.010    | 0.206      | Interm  |
| P02     | J09           |          | -0.000   | 0.375      | 0.7979                | 0.470      | 0.012    | 0.200      | Surface |
| P02     | J13           | 1        | 0.190    | _          | _                     | _          |          |            | Surface |
| P02     | J13<br>142    | 1        | -0.020   | -          | 0 7070                | -          |          |            | Surface |
| P02     | J13           |          | 0.215    | 0.007      | 0.7979                | 0.009      |          |            | Surface |
| P02     | J13           | 1        | 0.100    | _          |                       | _          |          |            | Sunace  |
| P02     | J13           | 1        | -0.180   | _          | -                     | _          |          |            | Surface |
| P02     | J13           | 1        | 0.390    | -          | -                     | -          |          |            | Surface |
| P02     | J13           |          | -0.330   | 0.113      | 0.7979                | 0.142      |          |            | Surface |
| P02     | J13           | 1        | -0.350   | _          | _                     | _          |          |            | Surface |
| P02     | J13           | 1        | -0.330   | _          | _                     | _          |          |            | Surface |
| P02     | J13           | 1        | -0.170   | _          | -                     | _          |          |            | Surface |
| P02     | J13           | 1        | 0.000    | -          | -                     | -          |          |            | Surface |
| P02     | J13           | 2        | -0.470   | 0.156      | 0.7979                | 0.195      |          |            | Surface |
| P02     | J13           | 2        | 0.000    | 0.085      | 0.7979                | 0.106      |          | 0.110      | Surface |
| P02     | J13           | 1        | 0.430    | _          | -                     | —          | -0.032   | 0.113      | Surface |
| P02     | J15           | 1        | 0.320    | -          | -                     | -          |          |            | Surface |
| P02     | J15           | 4        | 0.000    | 0.108      | 0.9213                | 0.117      |          |            | Surface |
| P02     | J15           | 4        | -0.165   | 0.078      | 0.9213                | 0.084      |          |            | Surface |
| P02     | J15           | 5        | 0.042    | 0.277      | 0.9400                | 0.294      |          |            | Surface |
| P02     | J15           | 3        | -0.097   | 0.165      | 0.8862                | 0.186      |          |            | Surface |
| P02     | J15           | 1        | 0.200    | -          | -                     | -          | 0.050    | 0.171      | Surface |
| P02     | J17           | 3        | -0.070   | 0.191      | 0.8862                | 0.215      |          |            | Base    |
| P02     | J17           | 4        | 0.030    | 0.432      | 0.9213                | 0.469      |          |            | Base    |
| P02     | J17           | 3        | 0.110    | 0.311      | 0.8862                | 0.351      |          |            | Base    |
| P02     | J17           | 3        | -0.200   | 0.101      | 0.8862                | 0.115      |          |            | Base    |
| P02     | J17           | 3        | -0.017   | 0.410      | 0.8862                | 0.463      |          |            | Base    |
| P02     | J17           | 1        | 0.160    | -          | _                     | —          | 0.002    | 0.322      | Base    |
| P02     | J28           | 3        | 0.053    | 0.205      | 0.8862                | 0.231      |          |            | Base    |
| P02     | J28           | 3        | 0.070    | 0.044      | 0.8862                | 0.049      |          |            | Base    |
| P02     | J28           | 1        | 0.030    | -          | -                     | -          |          |            | Base    |
| P02     | J28           | 1        | 0.000    | -          | _                     | —          |          |            | Base    |
| P02     | J28           | 2        | -0.145   | 0.318      | 0.7979                | 0.399      |          |            | Base    |
| P02     | J28           | 4        | 0.018    | 0.340      | 0.9213                | 0.369      |          |            | Base    |
| P02     | J28           | 3        | 0.167    | 0.154      | 0.8862                | 0.173      |          |            | Base    |
| P02     | J28           | 4        | 0.093    | 0.160      | 0.9213                | 0.173      |          |            | Base    |
| P02     | J28           | 3        | 0.117    | 0.032      | 0.8862                | 0.036      |          |            | Base    |
| P02     | J28           | 1        | -0.070   | -          | _                     | -          |          |            | Base    |
| P02     | J28           | 3        | -0.187   | 0.031      | 0.8862                | 0.034      |          |            | Base    |
| P02     | J28           | 1        | 0.790    | -          | -                     | -          |          |            | Base    |
| P02     | J28           | 1        | -0.410   | -          | -                     | -          | 0.040    | 0.183      | Base    |
| P04     | J08           | 2        | 0.060    | 0.071      | 0.7979                | 0.089      |          |            | Interm  |

| Table B.4. Summary of Unbiased Lot | Std Dev for AC for | Each Project (continued) |
|------------------------------------|--------------------|--------------------------|
|------------------------------------|--------------------|--------------------------|

| Project | JMF<br>Number | Lot Size | Lot Mean | Lot St Dev | <i>c</i> <sub>4</sub> | Lot St Dev | Average  | Avg Lot SD | Course  |
|---------|---------------|----------|----------|------------|-----------------------|------------|----------|------------|---------|
|         |               | 2        | 0 185    | 0 332      | 0 7070                |            | LOUINEan | Unbiased   | Interm  |
| P04     | 108           | 1        | 0.100    | 0.552      | 0.1313                | 0.417      |          |            | Interm  |
| P04     | 108           | 2        | -0.060   | 0.028      | 0 7070                | - 0.035    |          |            | Interm  |
| P04     | 108           | 2        | -0.000   | 0.020      | 0.7979                | 0.035      |          |            | Interm  |
| P04     | 108           | 2        | 0.103    | 0.400      | 0.7979                | 0.370      |          |            | Interm  |
| P04     | 108           | 2        | 0.320    | 0.141      | 0.7979                | 0.177      |          |            | Interm  |
| P04     | 108           | 2        | -0.000   | 0.029      | 0.7979                | 0.789      |          |            | Interm  |
| P04     | 108           | 2        | 0.370    | 0.014      | 0.7979                | 0.018      |          |            | Interm  |
| P04     | 100           | 2        | 0.320    | 0.200      | 0.7979                | 0.319      |          |            | Interm  |
| P04     | 100           | 2        | 0.400    | 0.309      | 0.7979                | 0.467      | 0.106    | 0.202      | Interm  |
| P04     | J00           | 2        | 0.120    | 0.007      | 0.7979                | 0.009      | 0.190    | 0.292      | Surface |
| P04     | J14           | 3        | -0.123   | 0.150      | 0.0002                | 0.170      |          |            | Sunace  |
| P04     | J14           | 4        | 0.076    | 0.100      | 0.9213                | 0.179      |          |            | Surface |
| P04     | J14           | 4        | 0.110    | 0.243      | 0.9213                | 0.263      |          |            | Sunace  |
| P04     | J14           | 3        | 0.073    | 0.220      | 0.8862                | 0.255      | 0.050    | 0.005      | Surface |
| P04     | J14           | 3        | 0.150    | 0.140      | 0.8862                | 0.158      | 0.058    | 0.205      | Surface |
| P05     | J25           | 1        | -0.410   | _          | _                     | _          |          |            | Surface |
| P05     | J25           | 1        | -0.020   | _          | -                     | -          |          |            | Surface |
| P05     | J25           | 1        | -0.110   | _          | _                     | _          |          |            | Surface |
| P05     | J25           | 1        | -0.110   | _          | _                     | -          |          |            | Surface |
| P05     | J25           | 1        | -0.250   | _          | -                     | -          |          |            | Surface |
| P05     | J25           | 1        | 0.210    | -          | -                     | -          |          |            | Surface |
| P05     | J25           | 1        | -0.130   | -          | -                     | -          |          |            | Surface |
| P05     | J25           | 1        | -0.230   | -          | -                     | -          | -0.131   | -          | Surface |
| P05     | J27           | 2        | -0.130   | 0.269      | 0.7979                | 0.337      |          |            | Interm  |
| P05     | J27           | 2        | -0.035   | 0.021      | 0.7979                | 0.027      |          |            | Interm  |
| P05     | J27           | 2        | -0.040   | 0.156      | 0.7979                | 0.195      |          |            | Interm  |
| P05     | J27           | 2        | -0.190   | 0.042      | 0.7979                | 0.053      |          |            | Interm  |
| P05     | J27           | 2        | -0.090   | 0.099      | 0.7979                | 0.124      |          |            | Interm  |
| P05     | J27           | 2        | -0.090   | 0.042      | 0.7979                | 0.053      |          |            | Interm  |
| P05     | J27           | 1        | -0.140   | -          | -                     | _          |          |            | Interm  |
| P05     | J27           | 2        | -0.245   | 0.205      | 0.7979                | 0.257      | -0.120   | 0.149      | Interm  |
| P05     | J40           | 3        | -0.197   | 0.235      | 0.8862                | 0.265      |          |            | Surface |
| P05     | J40           | 3        | -0.113   | 0.071      | 0.8862                | 0.080      |          |            | Surface |
| P05     | J40           | 1        | -0.320   | -          | -                     | _          |          |            | Surface |
| P05     | J40           | 1        | -0.070   | _          | -                     | -          |          |            | Surface |
| P05     | J40           | 1        | 0.110    | _          | _                     | —          | -0.118   | 0.173      | Surface |
| P06     | J24           | 3        | -0.153   | 0.055      | 0.8862                | 0.062      |          |            | Surface |
| P06     | J24           | 3        | 0.127    | 0.228      | 0.8862                | 0.257      |          |            | Surface |
| P06     | J24           | 3        | 0.137    | 0.095      | 0.8862                | 0.107      |          |            | Surface |
| P06     | J24           | 3        | 0.120    | 0.046      | 0.8862                | 0.052      |          |            | Surface |
| P06     | J24           | 3        | 0.093    | 0.214      | 0.8862                | 0.241      | 0.065    | 0.144      | Surface |
| P07     | J30           | 3        | -0.073   | 0.042      | 0.8862                | 0.047      |          |            | Surface |
| P07     | J30           | 1        | -0.060   | -          | -                     | -          |          |            | Surface |
| P07     | J30           | 1        | -0.170   | -          | -                     | -          |          |            | Surface |
| P07     | J30           | 1        | -0.120   | _          | _                     | -          |          |            | Surface |
| P07     | J30           | 4        | 0.065    | 0.353      | 0.9213                | 0.384      |          |            | Surface |
| P07     | J30           | 2        | -0.060   | 0.042      | 0.7979                | 0.053      |          |            | Surface |

Table B.4. Summary of Unbiased Lot Std Dev for AC for Each Project (continued)

| Project | JMF    | Lot Size | Lot Mean | Lot St Dev | C4     | Lot St Dev | Average  | Avg Lot SD | Course     |
|---------|--------|----------|----------|------------|--------|------------|----------|------------|------------|
| Number  | Number | 0        | 0.010    | (blased)   | 0 7070 | (unbiased) | Lot Mean | Unbiased   | Currée e e |
| P07     | J30    | 2        | -0.010   | 0.014      | 0.7979 | 0.018      |          |            | Surface    |
| P07     | J30    | 1        | -0.150   | -          | -      | -          |          |            | Surface    |
| P07     | J30    | 3        | -0.127   | 0.075      | 0.8862 | 0.085      |          |            | Surface    |
| P07     | J30    | 3        | -0.067   | 0.131      | 0.8862 | 0.147      |          |            | Surface    |
| P07     | J30    | 3        | -0.027   | 0.110      | 0.8862 | 0.124      |          |            | Surface    |
| P07     | J30    | 3        | -0.183   | 0.060      | 0.8862 | 0.068      |          |            | Surface    |
| P07     | J30    | 2        | -0.070   | 0.085      | 0.7979 | 0.106      |          |            | Surface    |
| P07     | J30    | 3        | -0.210   | 0.070      | 0.8862 | 0.079      |          |            | Surface    |
| P07     | J30    | 3        | -0.213   | 0.021      | 0.8862 | 0.023      |          |            | Surface    |
| P07     | J30    | 1        | -0.080   | -          | -      | -          |          |            | Surface    |
| P07     | J30    | 2        | -0.170   | 0.085      | 0.7979 | 0.106      |          |            | Surface    |
| P07     | J30    | 1        | -0.250   | -          | —      | _          |          |            | Surface    |
| P07     | J30    | 1        | 0.130    | _          | _      | _          | -0.097   | 0.103      | Surface    |
| P09     | J35    | 3        | -0.113   | 0.225      | 0.8862 | 0.254      |          |            | Surface    |
| P09     | J35    | 3        | 0.047    | 0.031      | 0.8862 | 0.034      |          |            | Surface    |
| P09     | J35    | 3        | 0.013    | 0.103      | 0.8862 | 0.116      | -0.018   | 0.135      | Surface    |
| P09     | J83    | 3        | -0.107   | 0.290      | 0.8862 | 0.327      |          |            | Surface    |
| P09     | J83    | 3        | -0.023   | 0.166      | 0.8862 | 0.187      |          |            | Surface    |
| P09     | J83    | 2        | 0.030    | 0.042      | 0.7979 | 0.053      | -0.033   | 0.189      | Surface    |
| P10     | J12    | 1        | 0.540    | -          | —      | -          |          |            | Surface    |
| P10     | J12    | 1        | 0.030    | -          | _      | -          |          |            | Surface    |
| P10     | J12    | 1        | 0.330    | -          | —      | -          |          |            | Surface    |
| P10     | J12    | 2        | 0.225    | 0.106      | 0.7979 | 0.133      |          |            | Surface    |
| P10     | J12    | 1        | -0.320   | -          | —      | -          |          |            | Surface    |
| P10     | J12    | 1        | -0.290   | -          | —      | —          |          |            | Surface    |
| P10     | J12    | 1        | -0.230   | _          | -      | _          |          |            | Surface    |
| P10     | J12    | 1        | -0.320   | -          | —      | -          |          |            | Surface    |
| P10     | J12    | 2        | 0.070    | 0.396      | 0.7979 | 0.496      |          |            | Surface    |
| P10     | J12    | 2        | 0.020    | 0.042      | 0.7979 | 0.053      |          |            | Surface    |
| P10     | J12    | 2        | -0.210   | 0.057      | 0.7979 | 0.071      |          |            | Surface    |
| P10     | J12    | 2        | -0.250   | 0.042      | 0.7979 | 0.053      |          |            | Surface    |
| P10     | J12    | 2        | -0.080   | 0.354      | 0.7979 | 0.443      | -0.037   | 0.208      | Surface    |
| P10     | J31    | 2        | -0.035   | 0.205      | 0.7979 | 0.257      |          |            | Interm     |
| P10     | J31    | 2        | 0.300    | 0.311      | 0.7979 | 0.390      |          |            | Interm     |
| P10     | J31    | 2        | -0.045   | 0.332      | 0.7979 | 0.417      |          |            | Interm     |
| P10     | J31    | 2        | -0.290   | 0.297      | 0.7979 | 0.372      |          |            | Interm     |
| P10     | J31    | 1        | -0.030   | -          | _      | —          |          |            | Interm     |
| P10     | J31    | 2        | -0.130   | 0.255      | 0.7979 | 0.319      |          |            | Interm     |
| P10     | J31    | 2        | 0.075    | 0.106      | 0.7979 | 0.133      |          |            | Interm     |
| P10     | J31    | 1        | 0.410    | _          | _      | -          |          |            | Interm     |
| P10     | J31    | 2        | 0.100    | 0.240      | 0.7979 | 0.301      |          |            | Interm     |
| P10     | J31    | 2        | -0.385   | 0.021      | 0.7979 | 0.027      |          |            | Interm     |
| P10     | J31    | 2        | -0.005   | 0.021      | 0.7979 | 0.027      |          |            | Interm     |
| P10     | J31    | 2        | 0.095    | 0.049      | 0.7979 | 0.062      |          |            | Interm     |
| P10     | J31    | 2        | 0.180    | 0.057      | 0.7979 | 0.071      |          |            | Interm     |
| P10     | J31    | 2        | 0.045    | 0.403      | 0.7979 | 0.505      |          |            | Interm     |
| P10     | J31    | 2        | -0.050   | 0.481      | 0.7979 | 0.603      |          |            | Interm     |

Table B.4. Summary of Unbiased Lot Std Dev for AC for Each Project (continued)

| Project<br>Number | JMF<br>Number | Lot Size | Lot Mean | Lot St Dev<br>(biased) | <i>c</i> <sub>4</sub> | Lot St Dev | Average  | Avg Lot SD | Course  |
|-------------------|---------------|----------|----------|------------------------|-----------------------|------------|----------|------------|---------|
| P10               | .131          | 2        | -0 155   | 0.021                  | 0 7979                | 0.027      | Lot mean | Unblased   | Interm  |
| P10               | .131          | 2        | 0.255    | 0.318                  | 0 7979                | 0.399      |          |            | Interm  |
| P10               | J31           | 2        | -0.040   | 0.610                  | 0 7979                | 0.585      |          |            | Interm  |
| P10               | .131          | 2        | -0.125   | 0.021                  | 0 7979                | 0.027      |          |            | Interm  |
| P10               | J31           | 2        | -0.030   | 0.071                  | 0 7979                | 0.089      |          |            | Interm  |
| P10               | J31           | 2        | 0.060    | 0.495                  | 0.7979                | 0.620      |          |            | Interm  |
| P10               | J31           | 1        | 0.340    | _                      | _                     | -          |          |            | Interm  |
| P10               | J31           | 2        | 0.060    | 0.523                  | 0.7979                | 0.656      |          |            | Interm  |
| P10               | J31           | 2        | 0.000    | 0.212                  | 0.7979                | 0.266      |          |            | Interm  |
| P10               | J31           | 2        | -0.165   | 0.361                  | 0.7979                | 0.452      |          |            | Interm  |
| P10               | J31           | 2        | 0.055    | 0.148                  | 0.7979                | 0.186      |          |            | Interm  |
| P10               | J31           | 1        | 0.070    | _                      | _                     | _          |          |            | Interm  |
| P10               | J31           | 2        | -0.225   | 0.290                  | 0.7979                | 0.363      |          |            | Interm  |
| P10               | J31           | 2        | -0.010   | 0.255                  | 0.7979                | 0.319      |          |            | Interm  |
| P10               | J31           | 2        | 0.080    | 0.113                  | 0.7979                | 0.142      |          |            | Interm  |
| P10               | J31           | 2        | -0.230   | 0.410                  | 0.7979                | 0.514      |          |            | Interm  |
| P10               | J31           | 2        | 0.060    | 0.042                  | 0.7979                | 0.053      |          |            | Interm  |
| P10               | J31           | 2        | -0.010   | 0.156                  | 0.7979                | 0.195      |          |            | Interm  |
| P10               | J31           | 2        | 0.145    | 0.177                  | 0.7979                | 0.222      |          |            | Interm  |
| P10               | J31           | 2        | 0.180    | 0.071                  | 0.7979                | 0.089      |          |            | Interm  |
| P10               | J31           | 2        | 0.225    | 0.177                  | 0.7979                | 0.222      |          |            | Interm  |
| P10               | J31           | 2        | -0.250   | 0.368                  | 0.7979                | 0.461      |          |            | Interm  |
| P10               | J31           | 2        | 0.270    | 0.184                  | 0.7979                | 0.230      |          |            | Interm  |
| P10               | J31           | 2        | -0.020   | 0.537                  | 0.7979                | 0.674      |          |            | Interm  |
| P10               | J31           | 2        | 0.095    | 0.375                  | 0.7979                | 0.470      |          |            | Interm  |
| P10               | J31           | 1        | 0.040    | _                      | _                     | _          | 0.022    | 0.298      | Interm  |
| P10               | J37           | 1        | 0.140    | -                      | _                     | —          |          |            | Interm  |
| P10               | J37           | 2        | -0.015   | 0.007                  | 0.7979                | 0.009      |          |            | Interm  |
| P10               | J37           | 2        | 0.125    | 0.134                  | 0.7979                | 0.168      |          |            | Interm  |
| P10               | J37           | 2        | -0.145   | 0.219                  | 0.7979                | 0.275      |          |            | Interm  |
| P10               | J37           | 2        | -0.070   | 0.311                  | 0.7979                | 0.390      |          |            | Interm  |
| P10               | J37           | 1        | 0.260    | -                      | -                     | -          |          |            | Interm  |
| P10               | J37           | 2        | 0.180    | 0.184                  | 0.7979                | 0.230      |          |            | Interm  |
| P10               | J37           | 2        | 0.185    | 0.276                  | 0.7979                | 0.346      |          |            | Interm  |
| P10               | J37           | 2        | 0.085    | 0.120                  | 0.7979                | 0.151      |          |            | Interm  |
| P10               | J37           | 2        | -0.230   | 0.028                  | 0.7979                | 0.035      |          |            | Interm  |
| P10               | J37           | 2        | 0.185    | 0.049                  | 0.7979                | 0.062      |          |            | Interm  |
| P10               | J37           | 2        | -0.225   | 0.078                  | 0.7979                | 0.097      | 0.040    | 0.176      | Interm  |
| P10               | J82           | 2        | -0.270   | 0.028                  | 0.7979                | 0.035      |          |            | Interm  |
| P10               | J82           | 2        | -0.145   | 0.106                  | 0.7979                | 0.133      |          |            | Interm  |
| P10               | J82           | 2        | 0.125    | 0.177                  | 0.7979                | 0.222      |          |            | Interm  |
| P10               | J82           | 2        | 0.025    | 0.120                  | 0.7979                | 0.151      |          |            | Interm  |
| P10               | J82           | 2        | -0.105   | 0.148                  | 0.7979                | 0.186      |          |            | Interm  |
| P10               | J82           | 1        | 0.090    | _                      | -                     | -          |          |            | Interm  |
| P10               | J82           | 2        | 0.260    | 0.042                  | 0.7979                | 0.053      |          |            | Interm  |
| P10               | J82           | 2        | -0.170   | 0.099                  | 0.7979                | 0.124      | -0.024   | 0.129      | Interm  |
| P11               | J41           | 3        | -0.107   | 0.156                  | 0.8862                | 0.176      |          |            | Surface |

| Table B.4. Summar | y of Unbiased L | ot Std Dev for A | C for Each Pro | ject ( <i>continued</i> ) |
|-------------------|-----------------|------------------|----------------|---------------------------|
|-------------------|-----------------|------------------|----------------|---------------------------|

| Project<br>Number | JMF<br>Number | Lot Size | Lot Mean | Lot St Dev<br>(biased) | <i>c</i> <sub>4</sub> | Lot St Dev<br>(unbiased) | Average  | Avg Lot SD | Course  |
|-------------------|---------------|----------|----------|------------------------|-----------------------|--------------------------|----------|------------|---------|
| P11               | J41           | 1        | 0.030    | -                      | _                     |                          | Lot moun | Chibladea  | Surface |
| P11               | J41           | 2        | 0.230    | 0.042                  | 0.7979                | 0.053                    |          |            | Surface |
| P11               | J41           | 4        | 0.135    | 0.117                  | 0.9213                | 0.127                    | 0.072    | 0.119      | Surface |
| P12               | J38           | 4        | -0.058   | 0.196                  | 0.9213                | 0.213                    | 0.012    | 00         | Surface |
| P12               | J38           | 2        | 0.270    | 0.071                  | 0.7979                | 0.089                    |          |            | Surface |
| P12               | J38           | 1        | 0.200    | _                      | _                     | -                        |          |            | Surface |
| P12               | J38           | 1        | -0.130   | _                      | _                     | _                        |          |            | Surface |
| P12               | J38           | 3        | 0.043    | 0.114                  | 0.8862                | 0.128                    |          |            | Surface |
| P12               | J38           | 3        | 0.080    | 0.183                  | 0.8862                | 0.207                    | 0.068    | 0.159      | Surface |
| P13               | J03           | 3        | 0.030    | 0.176                  | 0.8862                | 0.198                    | 0.000    |            | Surface |
| P13               | J03           | 3        | -0.130   | 0.399                  | 0.8862                | 0.450                    |          |            | Surface |
| P13               | J03           | 1        | -0.430   | _                      | _                     | _                        |          |            | Surface |
| P13               | J03           | 3        | 0.187    | 0.360                  | 0.8862                | 0.406                    |          |            | Surface |
| P13               | J03           | 1        | -0.060   | _                      | _                     | _                        |          |            | Surface |
| P13               | J03           | 1        | 0.020    | _                      | _                     | _                        |          |            | Surface |
| P13               | J03           | 3        | 0.017    | 0.224                  | 0.8862                | 0.252                    |          |            | Surface |
| P13               | J03           | 1        | 0.000    | _                      | _                     | _                        | -0.046   | 0.327      | Surface |
| P13               | J43           | 2        | 0.240    | 0.099                  | 0.7979                | 0.124                    | 0.010    | 0.021      | Surface |
| P13               | J43           | 2        | 0.020    | 0.057                  | 0.7979                | 0.071                    |          |            | Surface |
| P13               | J43           | 2        | 0.010    | 0.085                  | 0.7979                | 0.106                    |          |            | Surface |
| P13               | J43           | 2        | -0.120   | 0.170                  | 0.7979                | 0.213                    |          |            | Surface |
| P13               | J43           | 3        | 0.120    | 0.159                  | 0.8862                | 0.179                    |          |            | Surface |
| P13               | J43           | 4        | -0.043   | 0.134                  | 0.9213                | 0.145                    |          |            | Surface |
| P13               | J43           | 3        | -0.133   | 0.067                  | 0.8862                | 0.075                    |          |            | Surface |
| P13               | J43           | 1        | -0.110   | _                      | _                     | _                        | -0.002   | 0.130      | Surface |
| P14               | J16           | 1        | -0.450   | _                      | _                     | _                        |          |            | Surface |
| P14               | J16           | 2        | -0.215   | 0.078                  | 0.7979                | 0.097                    |          |            | Surface |
| P14               | J16           | 3        | -0.263   | 0.261                  | 0.8862                | 0.294                    |          |            | Surface |
| P14               | J16           | 2        | 0.005    | 0.163                  | 0.7979                | 0.204                    |          |            | Surface |
| P14               | J16           | 1        | -0.060   | _                      | _                     | _                        |          |            | Surface |
| P14               | J16           | 4        | -0.043   | 0.143                  | 0.9213                | 0.155                    |          |            | Surface |
| P14               | J16           | 3        | -0.023   | 0.064                  | 0.8862                | 0.073                    |          |            | Surface |
| P14               | J16           | 4        | -0.330   | 0.178                  | 0.9213                | 0.193                    |          |            | Surface |
| P14               | J16           | 4        | -0.228   | 0.370                  | 0.9213                | 0.402                    |          |            | Surface |
| P14               | J16           | 2        | -0.275   | 0.205                  | 0.7979                | 0.257                    |          |            | Surface |
| P14               | J16           | 1        | -0.290   | _                      | _                     | _                        |          |            | Surface |
| P14               | J16           | 2        | 0.020    | 0.127                  | 0.7979                | 0.160                    |          |            | Surface |
| P14               | J16           | 3        | -0.223   | 0.091                  | 0.8862                | 0.102                    | -0.183   | 0.194      | Surface |
| P16               | J20           | 3        | -0.297   | 0.101                  | 0.8862                | 0.114                    |          |            | Surface |
| P16               | J20           | 3        | -0.250   | 0.314                  | 0.8862                | 0.355                    |          |            | Surface |
| P16               | J20           | 3        | 0.003    | 0.144                  | 0.8862                | 0.162                    | -0.181   | 0.210      | Surface |
| P17               | J22           | 2        | 0.205    | 0.035                  | 0.7979                | 0.044                    |          |            | Interm  |
| P17               | J22           | 2        | -0.055   | 0.064                  | 0.7979                | 0.080                    |          |            | Interm  |
| P17               | J22           | 2        | 0.090    | 0.028                  | 0.7979                | 0.035                    |          |            | Interm  |
| P17               | J22           | 1        | -0.250   | _                      | _                     | -                        |          |            | Interm  |
| P17               | J22           | 2        | -0.050   | 0.113                  | 0.7979                | 0.142                    |          |            | Interm  |
| P17               | J22           | 2        | -0.045   | 0.686                  | 0.7979                | 0.860                    | -0.018   | 0.232      | Interm  |

Table B.4. Summary of Unbiased Lot Std Dev for AC for Each Project (continued)

| Project<br>Number | JMF<br>Number | Lot Size | Lot Mean | Lot St Dev | <i>c</i> <sub>4</sub> | Lot St Dev | Average  | Avg Lot SD | Course  |
|-------------------|---------------|----------|----------|------------|-----------------------|------------|----------|------------|---------|
| P18               | J48           | 1        | 0.520    | -          | _                     |            | Lot moun | ensideed   | Surface |
| P18               | J48           | 3        | 0.123    | 0.071      | 0.8862                | 0.080      |          |            | Surface |
| P18               | J48           | 1        | -0.050   | _          | _                     | -          |          |            | Surface |
| P18               | J48           | 2        | 0.205    | 0.064      | 0.7979                | 0.080      |          |            | Surface |
| P18               | J48           | 3        | 0.037    | 0.311      | 0.8862                | 0.351      |          |            | Surface |
| P18               | J48           | 1        | 0.080    | _          | _                     | _          |          |            | Surface |
| P18               | J48           | 1        | -0.100   | _          | _                     | _          | 0.116    | 0.170      | Surface |
| P19               | J49           | 2        | -0.065   | 0.078      | 0.7979                | 0.097      |          |            | Surface |
| P19               | J49           | 1        | -0.130   | _          | _                     | _          |          |            | Surface |
| P19               | J49           | 3        | 0.023    | 0.208      | 0.8862                | 0.235      |          |            | Surface |
| P19               | J49           | 4        | 0.085    | 0.085      | 0.9213                | 0.093      |          |            | Surface |
| P19               | J49           | 4        | -0.305   | 0.449      | 0.9213                | 0.487      |          |            | Surface |
| P19               | J49           | 3        | 0.037    | 0.106      | 0.8862                | 0.120      |          |            | Surface |
| P19               | J49           | 3        | -0.197   | 0.205      | 0.8862                | 0.231      | -0.079   | 0.210      | Surface |
| P20               | J50           | 1        | 0.380    | _          | _                     | _          |          |            | Surface |
| P20               | J50           | 5        | -0.118   | 0.186      | 0.9400                | 0.198      |          |            | Surface |
| P20               | J50           | 2        | -0.225   | 0.375      | 0.7979                | 0.470      |          |            | Surface |
| P20               | J50           | 4        | -0.093   | 0.051      | 0.9213                | 0.056      |          |            | Surface |
| P20               | J50           | 1        | 0.030    | _          | _                     | _          |          |            | Surface |
| P20               | J50           | 2        | 0.135    | 0.064      | 0.7979                | 0.080      |          |            | Surface |
| P20               | J50           | 5        | 0.142    | 0.134      | 0.9400                | 0.142      |          |            | Surface |
| P20               | J50           | 3        | 0.067    | 0.172      | 0.8862                | 0.195      |          |            | Surface |
| P20               | J50           | 1        | 0.340    | _          | -                     | -          |          |            | Surface |
| P20               | J50           | 1        | -0.120   | _          | _                     | -          |          |            | Surface |
| P20               | J50           | 5        | 0.072    | 0.164      | 0.9400                | 0.174      |          |            | Surface |
| P20               | J50           | 1        | -0.100   | _          | -                     | _          |          |            | Surface |
| P20               | J50           | 2        | 0.195    | 0.134      | 0.7979                | 0.168      |          |            | Surface |
| P20               | J50           | 4        | 0.035    | 0.066      | 0.9213                | 0.072      |          |            | Surface |
| P20               | J50           | 5        | -0.142   | 0.156      | 0.9400                | 0.166      |          |            | Surface |
| P20               | J50           | 2        | 0.255    | 0.148      | 0.7979                | 0.186      |          |            | Surface |
| P20               | J50           | 2        | -0.030   | 0.057      | 0.7979                | 0.071      | 0.048    | 0.165      | Surface |
| P21               | J34           | 4        | 0.240    | 0.128      | 0.9213                | 0.139      |          |            | Interm  |
| P21               | J34           | 3        | -0.020   | 0.106      | 0.8862                | 0.119      |          |            | Interm  |
| P21               | J34           | 1        | -0.080   | -          | -                     | -          | 0.047    | 0.129      | Interm  |
| P21               | J39           | 1        | 0.090    | -          | -                     | _          |          |            | Surface |
| P21               | J39           | 4        | 0.073    | 0.025      | 0.9213                | 0.027      |          |            | Surface |
| P21               | J39           | 2        | 0.085    | 0.035      | 0.7979                | 0.044      |          |            | Surface |
| P21               | J39           | 4        | -0.030   | 0.116      | 0.9213                | 0.126      |          |            | Surface |
| P21               | J39           | 3        | -0.093   | 0.207      | 0.8862                | 0.234      |          |            | Surface |
| P21               | J39           | 1        | -0.140   | -          | -                     | -          | -0.003   | 0.108      | Surface |
| P22               | J54           | 6        | 0.070    | 0.107      | 0.9515                | 0.112      |          |            | Surface |
| P22               | J54           | 5        | 0.004    | 0.009      | 0.9400                | 0.010      |          |            | Surface |
| P22               | J54           | 1        | 0.120    | _          | -                     | -          | 0.065    | 0.061      | Surface |
| P24               | J51           | 1        | -0.040   | -          | -                     | -          |          |            | Interm  |
| P24               | J51           | 2        | 0.100    | 0.113      | 0.7979                | 0.142      |          |            | Interm  |
| P24               | J51           | 1        | 0.290    | -          | -                     | -          |          |            | Interm  |
| P24               | J51           | 1        | 0.390    | —          | _                     |            |          |            | Interm  |

| Table B.4. Summa | ry of Unbiased Lo | Std Dev for AC for | r Each Project | (continued) |
|------------------|-------------------|--------------------|----------------|-------------|
|------------------|-------------------|--------------------|----------------|-------------|

| Project | JMF    | Lot Size | Lot Mean | Lot St Dev | C4     | Lot St Dev | Average  | Avg Lot SD | Course  |
|---------|--------|----------|----------|------------|--------|------------|----------|------------|---------|
| Number  | Number |          | 0.405    | (biased)   | 0 7070 | (unbiased) | Lot Mean | Unbiased   |         |
| P24     | J51    | 2        | -0.105   | 0.219      | 0.7979 | 0.275      |          |            | Interm  |
| P24     | J51    | 1        | 0.060    | -          | -      | -          |          |            | Interm  |
| P24     | J51    | 2        | -0.035   | 0.007      | 0.7979 | 0.009      |          |            | Interm  |
| P24     | J51    | 2        | 0.155    | 0.304      | 0.7979 | 0.381      |          |            | Interm  |
| P24     | J51    | 2        | -0.095   | 0.049      | 0.7979 | 0.062      |          |            | Interm  |
| P24     | J51    | 1        | 0.020    | -          | -      | -          |          |            | Interm  |
| P24     | J51    | 2        | -0.035   | 0.106      | 0.7979 | 0.133      |          |            | Interm  |
| P24     | J51    | 2        | -0.030   | 0.198      | 0.7979 | 0.248      |          |            | Interm  |
| P24     | J51    | 1        | 0.010    | -          | -      | -          |          |            | Interm  |
| P24     | J51    | 2        | 0.020    | 0.156      | 0.7979 | 0.195      | 0.040    | 0.404      | Interm  |
| P24     | J51    | 1        | -0.020   | -          | -      | —          | 0.046    | 0.181      | Interm  |
| P24     | J56    | 1        | -0.360   | -          | -      | -          |          |            | Surface |
| P24     | J56    | 5        | -0.042   | 0.095      | 0.9400 | 0.101      |          |            | Surface |
| P24     | J56    | 1        | -0.010   | -          | -      | -          |          |            | Surface |
| P24     | J56    | 3        | 0.060    | 0.157      | 0.8862 | 0.177      |          |            | Surface |
| P24     | J56    | 1        | -1.020   | -          | -      | _          |          |            | Surface |
| P24     | J56    | 3        | 1.793    | 0.318      | 0.8862 | 0.359      |          |            | Surface |
| P24     | J56    | 1        | 0.180    | -          | -      | —          |          |            | Surface |
| P24     | J56    | 1        | 0.230    | -          | -      | -          |          |            | Surface |
| P24     | J56    | 3        | 0.043    | 0.219      | 0.8862 | 0.248      |          |            | Surface |
| P24     | J56    | 1        | 0.140    | -          | -      | _          |          |            | Surface |
| P24     | J56    | 4        | 0.168    | 0.388      | 0.9213 | 0.421      |          |            | Surface |
| P24     | J56    | 2        | 0.045    | 0.007      | 0.7979 | 0.009      |          |            | Surface |
| P24     | J56    | 1        | 0.080    | -          | _      | _          |          |            | Surface |
| P24     | J56    | 3        | -0.133   | 0.154      | 0.8862 | 0.173      |          |            | Surface |
| P24     | J56    | 1        | 0.010    | -          | -      | _          |          |            | Surface |
| P24     | J56    | 2        | 0.045    | 0.247      | 0.7979 | 0.310      |          |            | Surface |
| P24     | J56    | 4        | 0.070    | 0.112      | 0.9213 | 0.121      |          |            | Surface |
| P24     | J56    | 3        | 0.067    | 0.214      | 0.8862 | 0.241      | 0.076    | 0.216      | Surface |
| P24     | J57    | 2        | 0.065    | 0.049      | 0.7979 | 0.062      |          |            | Base    |
| P24     | J57    | 2        | 0.135    | 0.064      | 0.7979 | 0.080      |          |            | Base    |
| P24     | J57    | 2        | 0.025    | 0.078      | 0.7979 | 0.097      |          |            | Base    |
| P24     | J57    | 2        | 0.070    | 0.014      | 0.7979 | 0.018      |          |            | Base    |
| P24     | J57    | 2        | 0.230    | 0.042      | 0.7979 | 0.053      |          |            | Base    |
| P24     | J57    | 2        | 0.300    | 0.000      | 0.7979 | 0.000      | 0.138    | 0.052      | Base    |
| P24     | J64    | 1        | 0.160    | -          | -      | -          |          |            | Surface |
| P24     | J64    | 2        | 0.215    | 0.064      | 0.7979 | 0.080      |          |            | Surface |
| P24     | J64    | 2        | 0.170    | 0.057      | 0.7979 | 0.071      |          |            | Surface |
| P24     | J64    | 2        | 0.155    | 0.035      | 0.7979 | 0.044      |          |            | Surface |
| P24     | J64    | 2        | 0.060    | 0.028      | 0.7979 | 0.035      |          |            | Surface |
| P24     | J64    | 2        | 0.120    | 0.028      | 0.7979 | 0.035      | 0.4.4.4  | 0.017      | Surface |
| P24     | J64    | 2        | 0.130    | 0.014      | 0.7979 | 0.018      | 0.144    | 0.047      | Surface |
| P24     | J67    | 1        | 1.670    | -          | -      | -          |          |            | Surface |
| P24     | J67    | 1        | -0.510   | -          | _      | -          |          |            | Surface |
| P24     | J67    | 1        | 0.050    | -          | -      | -          |          |            | Surface |
| P24     | J67    | 2        | -0.060   | 0.113      | 0.7979 | 0.142      |          |            | Surface |
| P24     | J67    | 3        | -0.200   | 0.104      | 0.8862 | 0.117      |          |            | Surface |

Table B.4. Summary of Unbiased Lot Std Dev for AC for Each Project (continued)

| Project<br>Number | JMF<br>Number | Lot Size | Lot Mean | Lot St Dev | <i>c</i> <sub>4</sub> | Lot St Dev | Average | Avg Lot SD | Course  |
|-------------------|---------------|----------|----------|------------|-----------------------|------------|---------|------------|---------|
| P24               |               | 2        | 0.050    | 0.028      | 0 7979                | 0.035      | 0 167   | 0.098      | Surface |
| P25               | .129          | 2        | 0.000    | 0.020      | 0 7979                | 0.354      | 0.107   | 0.000      | Interm  |
| P25               | .129          | 2        | -0.325   | 0.276      | 0 7979                | 0.346      |         |            | Interm  |
| P25               | .129          | 2        | -0.025   | 0.177      | 0 7979                | 0.222      |         |            | Interm  |
| P25               | .129          | 2        | -0.360   | 0.028      | 0 7979                | 0.035      |         |            | Interm  |
| P25               | J29           | 1        | -0.120   | -          | _                     | -          |         |            | Interm  |
| P25               | J29           | 2        | -0.050   | 0.085      | 0.7979                | 0.106      |         |            | Interm  |
| P25               | J29           | 1        | -0.260   | 0.325      | _                     | _          | -0.161  | 0.213      | Interm  |
| P25               | J36           | 1        | 0.120    | _          | _                     | _          |         |            | Surface |
| P25               | J36           | 2        | -0.065   | 0.078      | 0.7979                | 0.097      |         |            | Surface |
| P25               | J36           | 3        | 0.100    | 0.278      | 0.8862                | 0.314      |         |            | Surface |
| P25               | J36           | 2        | 0.160    | 0.368      | 0.7979                | 0.461      |         |            | Surface |
| P25               | J36           | 1        | 0.000    | _          | _                     | _          |         |            | Surface |
| P25               | J36           | 1        | -0.040   | _          | _                     | -          | 0.046   | 0.291      | Surface |
| P26               | J45           | 4        | 0.113    | 0.550      | 0.9213                | 0.597      |         |            | Base    |
| P26               | J45           | 3        | 0.123    | 0.275      | 0.8862                | 0.310      |         |            | Base    |
| P26               | J45           | 2        | -0.130   | 0.014      | 0.7979                | 0.018      |         |            | Base    |
| P26               | J45           | 3        | 0.063    | 0.388      | 0.8862                | 0.438      | 0.042   | 0.341      | Base    |
| P26               | J52           | 1        | -0.150   | _          | -                     | _          |         |            | Surface |
| P26               | J52           | 3        | -0.053   | 0.099      | 0.8862                | 0.111      |         |            | Surface |
| P26               | J52           | 2        | -0.235   | 0.092      | 0.7979                | 0.115      |         |            | Surface |
| P26               | J52           | 2        | 0.025    | 0.205      | 0.7979                | 0.257      |         |            | Surface |
| P26               | J52           | 2        | -0.095   | 0.007      | 0.7979                | 0.009      |         |            | Surface |
| P26               | J52           | 2        | 0.005    | 0.177      | 0.7979                | 0.222      |         |            | Surface |
| P26               | J52           | 1        | 0.030    | _          | _                     | _          |         |            | Surface |
| P26               | J52           | 2        | -0.070   | 0.071      | 0.7979                | 0.089      |         |            | Surface |
| P26               | J52           | 2        | 0.060    | 0.085      | 0.7979                | 0.106      |         |            | Surface |
| P26               | J52           | 2        | -0.050   | 0.099      | 0.7979                | 0.124      |         |            | Surface |
| P26               | J52           | 2        | -0.065   | 0.035      | 0.7979                | 0.044      |         |            | Surface |
| P26               | J52           | 2        | -0.080   | 0.028      | 0.7979                | 0.035      |         |            | Surface |
| P26               | J52           | 1        | 0.270    | Ι          |                       | -          |         |            | Surface |
| P26               | J52           | 2        | -0.015   | 0.092      | 0.7979                | 0.115      |         |            | Surface |
| P26               | J52           | 3        | 0.083    | 0.203      | 0.8862                | 0.229      |         |            | Surface |
| P26               | J52           | 2        | -0.215   | 0.049      | 0.7979                | 0.062      |         |            | Surface |
| P26               | J52           | 1        | -0.260   | _          | _                     | _          |         |            | Surface |
| P26               | J52           | 3        | -0.293   | 0.081      | 0.8862                | 0.092      |         |            | Surface |
| P26               | J52           | 2        | -0.130   | 0.042      | 0.7979                | 0.053      |         |            | Surface |
| P26               | J52           | 1        | -0.100   | _          | _                     | _          |         |            | Surface |
| P26               | J52           | 3        | 0.073    | 0.078      | 0.8862                | 0.088      |         |            | Surface |
| P26               | J52           | 3        | -0.017   | 0.108      | 0.8862                | 0.122      |         |            | Surface |
| P26               | J52           | 3        | -0.060   | 0.130      | 0.8862                | 0.147      |         |            | Surface |
| P26               | J52           | 3        | -0.187   | 0.145      | 0.8862                | 0.163      |         |            | Surface |
| P26               | J52           | 1        | 0.110    | —          | -                     | _          |         |            | Surface |
| P26               | J52           | 3        | -0.127   | 0.212      | 0.8862                | 0.239      |         |            | Surface |
| P26               | J52           | 1        | -0.070   | _          | -                     | -          |         |            | Surface |
| P26               | J52           | 1        | 0.120    | —          | -                     | _          |         |            | Surface |
| P26               | J52           | 1        | -0.090   | —          | —                     | -          |         |            | Surface |

Table B.4. Summary of Unbiased Lot Std Dev for AC for Each Project (continued)

| Project | JMF    | Lot Size | Lot Mean | Lot St Dev | C <sub>4</sub> | Lot St Dev | Average  | Avg Lot SD | Course  |
|---------|--------|----------|----------|------------|----------------|------------|----------|------------|---------|
| Number  | Number | 4        | 0.040    | (blased)   |                | (unbiased) | Lot Mean | Unbiased   | 0       |
| P26     | J52    | 1        | 0.010    | _          | -              | _          | -0.053   | 0.121      | Surface |
| P26     | J58    | 1        | -0.190   | -          | -              | _          |          |            | Surface |
| P26     | J58    | 1        | 0.130    | 0.042      | _              | _          |          |            | Surface |
| P26     | J58    | 1        | -0.010   | 0.007      | -              | -          |          |            | Surface |
| P26     | J58    | 1        | -0.250   | 0.177      | _              | -          |          |            | Surface |
| P26     | J58    | 1        | -0.120   | 0.085      | _              | -          |          |            | Surface |
| P26     | J58    | 1        | 0.230    | 0.163      | _              | -          |          |            | Surface |
| P26     | J58    | 1        | 0.050    | 0.035      | _              | -          |          |            | Surface |
| P26     | J58    | 1        | -0.030   | 0.021      | -              | -          |          |            | Surface |
| P26     | J58    | 1        | 0.170    | 0.035      | _              | -          |          |            | Surface |
| P26     | J58    | 1        | -0.060   | -          | -              | -          |          |            | Surface |
| P26     | J58    | 2        | -0.100   | 0.198      | 0.7979         | 0.248      | 0.005    | 0.040      | Surface |
| P26     | J58    | 1        | 0.240    | -          | -              | -          | 0.005    | 0.248      | Surface |
| P26     | J62    | 4        | 0.160    | 0.075      | 0.9213         | 0.081      |          |            | Surface |
| P26     | J62    | 4        | 0.013    | 0.138      | 0.9213         | 0.150      |          |            | Surface |
| P26     | J62    | 3        | -0.107   | 0.131      | 0.8862         | 0.147      |          |            | Surface |
| P26     | J62    | 3        | -0.170   | 0.125      | 0.8862         | 0.141      |          |            | Surface |
| P26     | J62    | 3        | -0.013   | 0.168      | 0.8862         | 0.189      |          |            | Surface |
| P26     | J62    | 3        | -0.017   | 0.102      | 0.8862         | 0.115      |          |            | Surface |
| P26     | J62    | 4        | 0.043    | 0.092      | 0.9213         | 0.100      |          |            | Surface |
| P26     | J62    | 3        | 0.153    | 0.320      | 0.8862         | 0.361      |          |            | Surface |
| P26     | J62    | 4        | 0.013    | 0.259      | 0.9213         | 0.282      | 0.008    | 0.174      | Surface |
| P26     | J68    | 3        | -0.283   | 0.680      | 0.8862         | 0.767      |          |            | Surface |
| P26     | J68    | 4        | -0.205   | 0.037      | 0.9213         | 0.040      |          |            | Surface |
| P26     | J68    | 3        | -0.057   | 0.126      | 0.8862         | 0.142      |          |            | Surface |
| P26     | J68    | 3        | 0.193    | 0.631      | 0.8862         | 0.712      | -0.088   | 0.415      | Surface |
| P26     | J69    | 4        | 0.268    | 0.067      | 0.9213         | 0.072      |          |            | Surface |
| P26     | J69    | 3        | -0.040   | 0.195      | 0.8862         | 0.220      |          |            | Surface |
| P26     | J69    | 3        | -0.147   | 0.163      | 0.8862         | 0.184      |          |            | Surface |
| P26     | J69    | 3        | 0.033    | 0.059      | 0.8862         | 0.066      |          |            | Surface |
| P26     | J69    | 3        | 0.103    | 0.132      | 0.8862         | 0.149      |          |            | Surface |
| P26     | J69    | 3        | 0.080    | 0.111      | 0.8862         | 0.126      |          |            | Surface |
| P26     | J69    | 3        | 0.093    | 0.186      | 0.8862         | 0.209      |          |            | Surface |
| P26     | J69    | 3        | -0.090   | 0.131      | 0.8862         | 0.148      |          |            | Surface |
| P26     | J69    | 3        | -0.097   | 0.050      | 0.8862         | 0.057      |          |            | Surface |
| P26     | J69    | 4        | 0.093    | 0.171      | 0.9213         | 0.185      |          |            | Surface |
| P26     | J69    | 3        | 0.057    | 0.214      | 0.8862         | 0.241      |          |            | Surface |
| P26     | J69    | 4        | -0.063   | 0.084      | 0.9213         | 0.091      |          |            | Surface |
| P26     | J69    | 3        | -0.197   | 0.210      | 0.8862         | 0.237      |          |            | Surface |
| P26     | J69    | 3        | -0.237   | 0.133      | 0.8862         | 0.150      |          |            | Surface |
| P26     | J69    | 3        | 0.193    | 0.123      | 0.8862         | 0.139      |          |            | Surface |
| P26     | J69    | 3        | 0.057    | 0.154      | 0.8862         | 0.173      |          |            | Surface |
| P26     | J69    | 1        | -0.530   | -          | _              | -          |          |            | Surface |
| P26     | J69    | 1        | 0.060    | _          | _              | _          | -0.020   | 0.153      | Surface |
| P27     | J53    | 2        | -0.115   | 0.191      | 0.7979         | 0.239      |          |            | Interm  |
| P27     | J53    | 2        | -0.180   | 0.042      | 0.7979         | 0.053      |          |            | Interm  |
| P27     | J53    | 1        | -0.220   | _          | _              | _          |          |            | Interm  |

Table B.4. Summary of Unbiased Lot Std Dev for AC for Each Project (continued)

| Project<br>Number | JMF<br>Number | Lot Size | Lot Mean | Lot St Dev<br>(biased) | <i>c</i> <sub>4</sub> | Lot St Dev<br>(unbiased) | Average  | Avg Lot SD<br>Unbiased | Course  |
|-------------------|---------------|----------|----------|------------------------|-----------------------|--------------------------|----------|------------------------|---------|
| P27               | J53           | 1        | -0.200   |                        | _                     |                          | Lot moun | <b>U</b> IIDIGUUU      | Interm  |
| P27               | J53           | 1        | -0.250   | _                      | _                     | _                        |          |                        | Interm  |
| P27               | J53           | 1        | -0.260   | _                      | _                     | _                        |          |                        | Interm  |
| P27               | J53           | 1        | 0.320    | _                      | _                     | _                        |          |                        | Interm  |
| P27               | J53           | 2        | 0.080    | 0.141                  | 0.7979                | 0.177                    |          |                        | Interm  |
| P27               | J53           | 1        | 0.070    | _                      | _                     | _                        |          |                        | Interm  |
| P27               | J53           | 1        | 0.010    | _                      | _                     | _                        |          |                        | Interm  |
| P27               | J53           | 1        | 0.130    | _                      | _                     | _                        |          |                        | Interm  |
| P27               | J53           | 1        | -0.070   | _                      | _                     | _                        |          |                        | Interm  |
| P27               | J53           | 1        | 0.100    | -                      | -                     | _                        |          |                        | Interm  |
| P27               | J53           | 1        | 0.390    | -                      | -                     | _                        |          |                        | Interm  |
| P27               | J53           | 1        | 0.220    | -                      | -                     | _                        |          |                        | Interm  |
| P27               | J53           | 1        | 0.190    | -                      | -                     | -                        | 0.013    | 0.157                  | Interm  |
| P27               | J55           | 3        | 0.213    | 0.386                  | 0.8862                | 0.435                    |          |                        | Surface |
| P27               | J55           | 3        | 0.120    | 0.105                  | 0.8862                | 0.119                    |          |                        | Surface |
| P27               | J55           | 3        | 0.130    | 0.147                  | 0.8862                | 0.166                    |          |                        | Surface |
| P27               | J55           | 3        | 0.113    | 0.229                  | 0.8862                | 0.258                    |          |                        | Surface |
| P27               | J55           | 3        | 0.067    | 0.074                  | 0.8862                | 0.083                    | 0.129    | 0.212                  | Surface |
| P27               | J60           | 1        | 0.120    | _                      | _                     | _                        |          |                        | Interm  |
| P27               | J60           | 1        | 0.430    | _                      | _                     | _                        |          |                        | Interm  |
| P27               | J60           | 1        | 0.350    | _                      | _                     | _                        |          |                        | Interm  |
| P27               | J60           | 1        | -0.100   | -                      | _                     | -                        |          |                        | Interm  |
| P27               | J60           | 1        | 0.260    | -                      | _                     | -                        |          |                        | Interm  |
| P27               | J60           | 1        | 0.410    | _                      | _                     | -                        |          |                        | Interm  |
| P27               | J60           | 1        | 0.160    | _                      | _                     | -                        |          |                        | Interm  |
| P27               | J60           | 1        | 0.550    | Ι                      | -                     | _                        |          |                        | Interm  |
| P27               | J60           | 1        | 0.430    | Ι                      | I                     | _                        |          |                        | Interm  |
| P27               | J60           | 1        | 0.400    | Ι                      | I                     | _                        |          |                        | Interm  |
| P27               | J60           | 1        | -0.190   | -                      | -                     | —                        |          |                        | Interm  |
| P27               | J60           | 1        | 0.250    | -                      | -                     | _                        |          |                        | Interm  |
| P27               | J60           | 1        | -0.120   | -                      | -                     | _                        |          |                        | Interm  |
| P27               | J60           | 1        | 0.420    | _                      | _                     | -                        |          |                        | Interm  |
| P27               | J60           | 1        | 0.550    | _                      | _                     | -                        | 0.261    | -                      | Interm  |
| P27               | J61           | 1        | 0.000    | _                      | _                     | -                        |          |                        | Surface |
| P27               | J61           | 1        | -0.050   | -                      | -                     | _                        |          |                        | Surface |
| P27               | J61           | 1        | -0.300   | -                      | -                     | _                        |          |                        | Surface |
| P27               | J61           | 1        | 0.050    | _                      | _                     | _                        |          |                        | Surface |
| P27               | J61           | 1        | 0.080    | _                      | _                     | _                        |          |                        | Surface |
| P27               | J61           | 1        | -0.060   | _                      | _                     | _                        |          |                        | Surface |
| P27               | J61           | 1        | 0.020    | —                      | -                     | _                        |          |                        | Surface |
| P27               | J61           | 1        | -0.050   | —                      | -                     | _                        |          |                        | Surface |
| P27               | J61           | 1        | -0.220   | —                      | _                     | -                        | -0.059   | _                      | Surface |
| P27               | J66           | 1        | 0.020    | —                      | _                     | -                        |          |                        | Base    |
| P27               | J66           | 1        | -0.150   | —                      | _                     | -                        |          |                        | Base    |
| P27               | J66           | 1        | 0.010    | —                      | _                     | -                        |          |                        | Base    |
| P27               | J66           | 1        | 0.130    | —                      | _                     | -                        |          |                        | Base    |
| P27               | J66           | 1        | -0.100   | —                      | _                     | -                        |          |                        | Base    |

# Table B.4. Summary of Unbiased Lot Std Dev for AC for Each Project (continued)

| Project | JMF        | Lot Size | Lot Mean | Lot St Dev | $c_4$  | Lot St Dev | Average  | Avg Lot SD | Course  |
|---------|------------|----------|----------|------------|--------|------------|----------|------------|---------|
|         |            | 1        | 0.240    | (biaseu)   |        | (unbiaseu) | Lot mean | Unbiaseu   | Paga    |
| P27     | 100        | 1        | -0.240   | _          | -      |            |          |            | Dase    |
| P27     | 100        | 1        | 0.310    | _          | _      |            |          |            | Base    |
| P27     | 100        | 1        | 0.190    | _          |        |            |          |            | Dase    |
| P27     | 100        | 1        | 0.370    | _          |        |            |          |            | Dase    |
| P27     | 100<br>100 | 1        | -0.160   | -          | -      |            | 0.045    |            | Base    |
| P27     | J00        | 1        | 0.120    | -          | -      | -          | 0.045    | _          | Base    |
| P27     | J/1        | 3        | 0.037    | 0.280      | 0.8862 | 0.316      |          |            | Surface |
| P27     | J/1        | 4        | 0.073    | 0.148      | 0.9213 | 0.160      |          |            | Surface |
| P27     | J/1        | 3        | -0.097   | 0.240      | 0.8862 | 0.270      |          |            | Surface |
| P27     | J71        |          | 0.055    | 0.148      | 0.7979 | 0.186      |          |            | Surface |
| P27     | J/1        |          | 0.140    | -          | -      | -          |          |            | Surface |
| P27     | J/1        | 3        | -0.010   | 0.223      | 0.8862 | 0.251      |          |            | Surface |
| P27     | J71        | 3        | 0.177    | 0.131      | 0.8862 | 0.147      |          |            | Surface |
| P27     | J/1        | 5        | 0.080    | 0.078      | 0.9400 | 0.083      | 0.000    | 0.400      | Surface |
| P27     | J/1        | 3        | 0.083    | 0.081      | 0.8862 | 0.091      | 0.060    | 0.188      | Surface |
| P28     | J39        | 3        | 0.137    | 0.250      | 0.8862 | 0.282      |          |            | Surface |
| P28     | J39        | 1        | -0.030   | -          | -      | -          |          |            | Surface |
| P28     | J39        | 4        | 0.135    | 0.103      | 0.9213 | 0.112      |          |            | Surface |
| P28     | J39        | 5        | -0.006   | 0.162      | 0.9400 | 0.172      |          |            | Surface |
| P28     | J39        | 5        | 0.022    | 0.135      | 0.9400 | 0.144      |          |            | Surface |
| P28     | J39        | 1        | 0.090    | -          | -      | -          |          |            | Surface |
| P28     | J39        | 3        | 0.077    | 0.029      | 0.8862 | 0.033      |          |            | Surface |
| P28     | J39        | 1        | 0.000    | -          | -      | _          |          |            | Surface |
| P28     | J39        | 1        | -0.290   | -          | -      | _          | 0.015    | 0.149      | Surface |
| P28     | J42        | 2        | -0.025   | 0.078      | 0.7979 | 0.097      |          |            | Interm  |
| P28     | J42        | 1        | -0.030   | -          | _      | _          |          |            | Interm  |
| P28     | J42        | 1        | -0.290   | -          | —      | _          |          |            | Interm  |
| P28     | J42        | 1        | -0.160   | -          | —      | _          |          |            | Interm  |
| P28     | J42        | 1        | -0.060   | -          | -      |            |          |            | Interm  |
| P28     | J42        | 1        | 0.090    | -          | -      |            |          |            | Interm  |
| P28     | J42        | 1        | 0.370    | -          | _      | _          |          |            | Interm  |
| P28     | J42        | 1        | 0.370    | -          | -      | -          |          |            | Interm  |
| P28     | J42        | 2        | 0.155    | 0.120      | 0.7979 | 0.151      |          |            | Interm  |
| P28     | J42        | 1        | 0.120    | -          | -      | -          |          |            | Interm  |
| P28     | J42        | 1        | 0.180    | -          | _      | -          |          |            | Interm  |
| P28     | J42        | 1        | 0.110    | -          | _      | -          |          |            | Interm  |
| P28     | J42        | 1        | 0.310    | _          | _      | -          | 0.088    | 0.124      | Interm  |
| P28     | J47        | 1        | 0.050    | -          | -      | -          |          |            | Base    |
| P28     | J47        | 2        | -0.045   | 0.078      | 0.7979 | 0.097      |          |            | Base    |
| P28     | J47        | 1        | -0.290   | -          | _      | -          |          |            | Base    |
| P28     | J47        | 1        | -0.360   | -          | -      | -          |          |            | Base    |
| P28     | J47        | 1        | 0.060    | -          | -      | -          |          |            | Base    |
| P28     | J47        | 1        | -0.240   | -          | _      | -          |          |            | Base    |
| P28     | J47        | 2        | -0.160   | 0.156      | 0.7979 | 0.195      |          |            | Base    |
| P28     | J47        | 2        | 0.140    | 0.424      | 0.7979 | 0.532      |          |            | Base    |
| P28     | J47        | 2        | 0.100    | 0.042      | 0.7979 | 0.053      |          |            | Base    |
| P28     | J47        | 1        | 0.360    | -          | —      | -          | -0.039   | 0.219      | Base    |

| Table B.4. Summa | y of Unbiased Lot Ste | Dev for AC for Each | Project (continued) |
|------------------|-----------------------|---------------------|---------------------|
|------------------|-----------------------|---------------------|---------------------|

| Project | JMF<br>Number | Lot Size | Lot Mean | Lot St Dev | <i>c</i> <sub>4</sub> | Lot St Dev | Average  | Avg Lot SD | Course  |
|---------|---------------|----------|----------|------------|-----------------------|------------|----------|------------|---------|
| P29     | .159          | 1        | -0 110   | _          | _                     |            | Lot moun | Chibladea  | Surface |
| P29     | 159           | 3        | 0 147    | 0.084      | 0 8862                | 0.095      |          |            | Surface |
| P29     | J59           | 3        | -0.027   | 0.199      | 0.8862                | 0.224      |          |            | Surface |
| P29     | J59           | 3        | -0.050   | 0.098      | 0.8862                | 0.111      |          |            | Surface |
| P29     | J59           | 3        | -0.077   | 0.188      | 0.8862                | 0.212      |          |            | Surface |
| P29     | J59           | 3        | 0.000    | 0.062      | 0.8862                | 0.070      |          |            | Surface |
| P29     | J59           | 4        | -0.078   | 0.209      | 0.9213                | 0.227      |          |            | Surface |
| P29     | J59           | 3        | -0.113   | 0.064      | 0.8862                | 0.072      |          |            | Surface |
| P29     | J59           | 3        | -0.137   | 0.023      | 0.8862                | 0.026      | -0.049   | 0.130      | Surface |
| P30     | J65           | 3        | -0.060   | 0.095      | 0.8862                | 0.108      |          |            | Surface |
| P30     | J65           | 3        | 0.020    | 0.082      | 0.8862                | 0.092      |          |            | Surface |
| P30     | J65           | 1        | 0.090    | _          | _                     | _          |          |            | Surface |
| P30     | J65           | 1        | -0.050   | _          | _                     | _          | 0.000    | 0.100      | Surface |
| P32     | J46           | 1        | 0.220    | _          | _                     | _          |          |            | Surface |
| P32     | J46           | 1        | 0.060    | _          | _                     | _          |          |            | Surface |
| P32     | J46           | 1        | -0.250   | _          | _                     | _          |          |            | Surface |
| P32     | J46           | 1        | -0.120   | _          | _                     | -          |          |            | Surface |
| P32     | J46           | 1        | -0.360   | _          | _                     | _          |          |            | Surface |
| P32     | J46           | 2        | -0.115   | 0.247      | 0.7979                | 0.310      |          |            | Surface |
| P32     | J46           | 2        | 0.020    | 0.141      | 0.7979                | 0.177      |          |            | Surface |
| P32     | J46           | 2        | 0.020    | 0.141      | 0.7979                | 0.177      |          |            | Surface |
| P32     | J46           | 3        | 0.000    | 0.315      | 0.8862                | 0.356      |          |            | Surface |
| P32     | J46           | 1        | -0.080   | _          | _                     | _          |          |            | Surface |
| P32     | J46           | 1        | 0.310    | _          | _                     | _          |          |            | Surface |
| P32     | J46           | 1        | 0.150    | _          | _                     | _          |          |            | Surface |
| P32     | J46           | 1        | -0.030   | _          | _                     | _          |          |            | Surface |
| P32     | J46           | 1        | 0.120    | Ι          | I                     | -          |          |            | Surface |
| P32     | J46           | 1        | 0.080    | -          | -                     | _          |          |            | Surface |
| P32     | J46           | 1        | -0.040   | Ι          | I                     | -          |          |            | Surface |
| P32     | J46           | 1        | 0.180    | 1          |                       | —          |          |            | Surface |
| P32     | J46           | 1        | 0.040    | -          | -                     | —          |          |            | Surface |
| P32     | J46           | 1        | -0.060   | -          | -                     | —          |          |            | Surface |
| P32     | J46           | 1        | 0.110    | _          | -                     | —          |          |            | Surface |
| P32     | J46           | 1        | -0.070   | _          | _                     | -          |          |            | Surface |
| P32     | J46           | 2        | -0.010   | 0.042      | 0.7979                | 0.053      |          |            | Surface |
| P32     | J46           | 2        | 0.070    | 0.170      | 0.7979                | 0.213      |          |            | Surface |
| P32     | J46           | 2        | -0.165   | 0.007      | 0.7979                | 0.009      |          |            | Surface |
| P32     | J46           | 1        | -0.410   | _          | -                     | _          |          |            | Surface |
| P32     | J46           | 1        | -0.070   | _          | -                     | _          |          |            | Surface |
| P32     | J46           | 1        | -0.240   | _          | _                     | _          |          |            | Surface |
| P32     | J46           | 1        | 0.340    | _          | _                     | _          |          |            | Surface |
| P32     | J46           | 3        | -0.117   | 0.083      | 0.8862                | 0.094      |          |            | Surface |
| P32     | J46           | 1        | -0.020   | —          | -                     | -          |          |            | Surface |
| P32     | J46           | 1        | -0.050   | _          | -                     | -          | -0.016   | 0.174      | Surface |
| P32     | J72           | 5        | 0.026    | 0.146      | 0.9400                | 0.155      |          |            | Surface |
| P32     | J72           | 6        | 0.007    | 0.148      | 0.9515                | 0.156      |          |            | Surface |
| P32     | J72           | 3        | -0.033   | 0.227      | 0.8862                | 0.257      |          |            | Surface |

Table B.4. Summary of Unbiased Lot Std Dev for AC for Each Project (continued)

| Name         172         3         0.213         0.080         0.8862         0.091         Surface           P32         J72         5         0.078         0.182         0.9400         0.194         Surface           P32         J72         5         0.078         0.182         0.9400         0.105         Surface           P32         J72         3         0.147         0.142         0.8862         0.160         Surface           P32         J76         4         0.045         0.3213         0.208         Interm           P32         J76         5         0.130         0.341         0.9400         0.362         Interm           P32         J76         3         0.150         0.060         0.8213         0.087         Interm           P32         J76         3         0.107         0.301         0.8862         0.034         Interm           P32         J76         4         0.148         0.2213         0.028         Interm           P32         J76         4         0.148         0.2213         0.024         Interm           P32         J76         3         0.217         0.230         0.8862 <th>Project</th> <th>JMF<br/>Number</th> <th>Lot Size</th> <th>Lot Mean</th> <th>Lot St Dev</th> <th><i>c</i><sub>4</sub></th> <th>Lot St Dev</th> <th>Average</th> <th>Avg Lot SD</th> <th>Course</th> | Project | JMF<br>Number | Lot Size | Lot Mean | Lot St Dev | <i>c</i> <sub>4</sub> | Lot St Dev | Average | Avg Lot SD | Course  |
|---|---------|---------------|----------|----------|------------|-----------------------|------------|---------|------------|---------|
| P32         J72         5         0.12         0.032         0.0400         0.194         Surface           P32         J72         5         0.136         0.099         0.9400         0.194         Surface           P32         J72         3         0.147         0.142         0.8862         0.160         Surface           P32         J76         4         0.040         0.9213         0.338         0.077         0.182         Surface           P32         J76         4         0.010         0.8862         0.011         Interm           P32         J76         5         0.130         0.031         0.8862         0.039         Interm           P32         J76         3         0.017         0.3862         0.039         Interm           P32         J76         3         0.027         0.031         0.8862         0.034         Interm           P32         J76         4         0.148         0.20213         0.223         Interm           P32         J76         4         0.148         0.20213         0.223         Interm           P32         J76         3         0.225         0.272         0.2845 <th>P32</th> <th></th> <th>3</th> <th>0.213</th> <th></th> <th>0.8862</th> <th></th> <th></th> <th>Unblased</th> <th>Surface</th>   | P32     |               | 3        | 0.213    |            | 0.8862                |            |         | Unblased   | Surface |
| P32         J72         5         0.076         0.124         0.9400         0.155         Surface           P32         J72         3         0.147         0.142         0.8862         0.160         Surface           P32         J72         4         0.045         0.312         0.2013         0.338         0.077         0.182         Surface           P32         J76         4         0.100         0.191         0.208         Interm           P32         J76         5         0.130         0.341         0.9400         0.362         Interm           P32         J76         4         0.078         0.080         0.9213         0.087         Interm           P32         J76         3         0.190         0.035         0.8862         0.039         Interm           P32         J76         4         0.148         0.206         0.9213         0.223         Interm           P32         J76         4         0.148         0.206         0.9213         0.986         Interm           P32         J76         4         0.148         0.9213         0.198         Interm           P32         J76         3   | P32     | 172           | 5        | 0.210    | 0.000      | 0.0002                | 0.001      |         |            | Surface |
| P32         J72         J         0.143         0.045         0.0460         0.0460         0.0460         0.0460         0.0460         0.03862         0.0160         0.0170         0.182         Surface           P32         J76         4         0.040         0.191         0.9213         0.286         0.011         Interm           P32         J76         5         0.130         0.341         0.9400         0.362         Interm           P32         J76         5         0.130         0.341         0.9400         0.362         Interm           P32         J76         3         0.017         0.301         0.8862         0.030         Interm           P32         J76         3         0.017         0.301         0.8862         0.034         Interm           P32         J76         4         0.148         0.260         0.9213         0.023         Interm           P32         J76         4         0.018         0.9213         0.023         Interm           P32         J76         3         0.217         0.276         0.8862         0.312         Interm           P32         J76         3         0.217  | P32     | 172           | 5        | 0.070    | 0.102      | 0.3400                | 0.194      |         |            | Surface |
| P32         J72         J         0.147         0.132         0.0213         0.138         0.077         0.182         Surface           P32         J76         4         0.100         0.191         0.9213         0.208         0.077         0.182         Surface           P32         J76         5         0.130         0.341         0.9400         0.362         0.11         Interm           P32         J76         4         0.078         0.0862         0.039         Interm           P32         J76         3         0.107         0.301         0.8862         0.340         Interm           P32         J76         3         0.027         0.031         0.8862         0.340         Interm           P32         J76         4         0.148         0.206         0.9213         0.223         Interm           P32         J76         4         0.148         0.206         0.9213         0.283         Interm           P32         J76         4         0.190         0.183         0.9213         0.198         Interm           P32         J76         3         0.207         0.2813         0.198         Interm  | D32     | 172           | 3        | 0.130    | 0.033      | 0.3400                | 0.100      |         |            | Surface |
| P32         J76         4         0.043         0.512         0.5213         0.538         0.077         0.162         Sufface           P32         J76         3         -0.150         0.010         0.8862         0.011         Interm           P32         J76         5         0.130         0.341         0.9400         0.362         Interm           P32         J76         4         0.078         0.080         0.3213         0.087         Interm           P32         J76         3         -0.107         0.301         0.8862         0.034         Interm           P32         J76         3         0.027         0.031         0.8862         0.034         Interm           P32         J76         4         0.148         0.206         0.9213         0.028         Interm           P32         J76         4         0.190         0.183         0.9213         0.098         Interm           P32         J76         3         0.217         0.276         0.8862         0.312         Interm           P32         J76         3         0.226         0.072         0.515         0.076         Surface           P32<   | P32     | 172           | 3        | 0.147    | 0.142      | 0.0002                | 0.100      | 0.077   | 0.192      | Surface |
| P32         J76         3         0.101         0.213         0.2205         Interm           P32         J76         5         0.130         0.341         0.9400         0.362         Interm           P32         J76         5         0.130         0.341         0.9400         0.362         Interm           P32         J76         3         0.070         0.030         0.8862         0.039         Interm           P32         J76         3         0.027         0.031         0.8862         0.034         Interm           P32         J76         4         0.148         0.206         0.223         Interm           P32         J76         4         0.148         0.206         0.312         Interm           P32         J76         4         0.190         0.183         0.9213         0.098         Interm           P32         J76         3         0.217         0.276         0.8862         0.312         Interm           P32         J76         3         0.220         0.283         0.8862         0.663         0.092         0.181         Interm           P32         J79         5         0.264   | P32     | 176           | 4        | 0.045    | 0.312      | 0.9213                | 0.338      | 0.077   | 0.102      | Intorm  |
| P32         J76         S         0.100         0.010         0.0362         0.011         Interm           P32         J76         4         0.078         0.080         0.3213         0.087         Interm           P32         J76         3         0.190         0.035         0.8862         0.039         Interm           P32         J76         3         0.027         0.031         0.8862         0.034         Interm           P32         J76         3         0.027         0.031         0.8862         0.034         Interm           P32         J76         4         0.148         0.206         0.9213         0.223         Interm           P32         J76         4         0.190         0.831         0.9213         0.098         Interm           P32         J76         3         0.217         0.276         0.8862         0.312         Interm           P32         J76         3         0.217         0.276         0.8862         0.023         0.181         Interm           P32         J79         5         0.264         0.066         0.4400         0.070         Surface           P32         J79  | P22     | 176           | 4        | 0.100    | 0.191      | 0.9213                | 0.208      |         |            | Interm  |
| P32         J76         4         0.787         0.541         0.540         0.322         Interm           P32         J76         3         0.190         0.035         0.8862         0.039         Interm           P32         J76         3         -0.107         0.301         0.8862         0.039         Interm           P32         J76         3         -0.027         0.031         0.8862         0.034         Interm           P32         J76         4         -0.148         0.206         0.9213         0.223         Interm           P32         J76         4         -0.148         0.206         0.3213         0.038         Interm           P32         J76         4         -0.180         0.9213         0.198         Interm           P32         J76         3         0.217         0.276         0.8862         0.312         Interm           P32         J76         6         0.225         0.072         0.9213         0.192         Interm           P32         J79         6         0.226         0.072         0.213         0.139         Surface           P32         J79         3         0.127   | F 32    | 176           | 5        | -0.130   | 0.010      | 0.0002                | 0.011      |         |            | Interm  |
| P32         J76         3         0.1078         0.1080         0.03213         0.1087         Interm           P32         J76         3         -0.107         0.301         0.8862         0.034         Interm           P32         J76         3         -0.107         0.301         0.8862         0.034         Interm           P32         J76         4         0.148         0.2206         0.9213         0.098         Interm           P32         J76         4         0.148         0.206         0.312         Interm           P32         J76         4         0.190         0.183         0.9213         0.098         Interm           P32         J76         3         0.207         0.2862         0.312         Interm           P32         J76         3         0.300         0.233         0.8862         0.263         0.092         0.181         Interm           P32         J79         6         0.225         0.072         0.9515         0.076         Surface           P32         J79         3         0.220         0.128         0.8262         0.144         Surface           P32         J79         3 </td <td>P32</td> <td>176</td> <td>5</td> <td>0.130</td> <td>0.341</td> <td>0.9400</td> <td>0.302</td> <td></td> <td></td> <td>Interm</td>  | P32     | 176           | 5        | 0.130    | 0.341      | 0.9400                | 0.302      |         |            | Interm  |
| P32         J76         3         0.190         0.030         0.0302         0.0303         0.0303         0.0303         0.0303         0.0303         0.0303         0.0303         0.0303         0.0303         0.0303         0.0303         0.0303         0.0303         0.0303         0.0303         0.0303         0.0303         0.0304         Interm           P32         J76         4         0.018         0.0213         0.0223         Interm           P32         J76         4         0.0190         0.183         0.9213         0.098         Interm           P32         J76         3         0.217         0.276         0.8862         0.312         Interm           P32         J76         3         0.217         0.276         0.8862         0.0263         0.092         0.181         Interm           P32         J79         6         0.225         0.072         0.9515         0.076         Surface           P32         J79         4         0.193         0.128         0.8213         0.139         Surface           P32         J79         3         0.127         0.9213         0.144         Surface           P32         J79   | P22     | 176           | 4        | 0.070    | 0.000      | 0.9213                | 0.007      |         |            | Interm  |
| P32         J76         3         0.107         0.301         0.8002         0.340         Interm           P32         J76         4         0.148         0.206         0.9213         0.223         Interm           P32         J76         4         0.018         0.9213         0.098         Interm           P32         J76         4         0.018         0.9213         0.098         Interm           P32         J76         3         0.217         0.276         0.8862         0.312         Interm           P32         J76         3         0.217         0.276         0.8862         0.263         0.092         0.181         Interm           P32         J79         6         0.225         0.072         0.9515         0.076         Surface           P32         J79         4         0.193         0.128         0.8862         0.144         Surface           P32         J79         3         0.127         0.9213         0.186         Surface           P32         J79         3         0.110         0.062         0.8862         0.070         Surface           P32         J79         3         0.117   | P22     | 176           | 2        | 0.190    | 0.000      | 0.0002                | 0.039      |         |            | Interm  |
| P32         J76         3         0.027         0.037         0.0302         0.034         Interm           P32         J76         4         0.18         0.0213         0.223         Interm           P32         J76         4         0.190         0.183         0.9213         0.098         Interm           P32         J76         3         0.217         0.276         0.8862         0.312         Interm           P32         J76         3         0.300         0.233         0.8862         0.263         0.092         0.181         Interm           P32         J79         6         0.225         0.072         0.9515         0.076         Surface           P32         J79         4         0.193         0.128         0.9213         0.139         Surface           P32         J79         4         0.020         0.172         0.9213         0.186         Surface           P32         J79         3         0.127         0.0213         0.186         Surface           P32         J79         3         0.117         0.9213         0.186         Surface           P32         J79         3         0.217   | P22     | 176           | 2        | -0.107   | 0.301      | 0.0002                | 0.340      |         |            | Interm  |
| P32         J76         4         -0.148         0.203         0.2213         0.223         1.118111           P32         J76         4         0.190         0.183         0.9213         0.098         Interm           P32         J76         3         0.217         0.276         0.8862         0.312         Interm           P32         J76         3         0.300         0.233         0.8862         0.263         0.092         0.181         Interm           P32         J79         6         0.225         0.072         0.9515         0.076         Surface           P32         J79         4         0.193         0.128         0.9213         0.139         Surface           P32         J79         4         0.193         0.128         0.8862         0.144         Surface           P32         J79         3         0.137         0.074         0.8862         0.063         Surface           P32         J79         3         0.110         0.662         0.8862         0.064         Surface           P32         J79         3         0.127         0.9213         0.113         Surface           P32  | P32     | 176           | 3        | 0.027    | 0.031      | 0.0002                | 0.034      |         |            | Interm  |
| P32         J76         4         -0.018         0.021         0.020         1116111           P32         J76         3         0.217         0.276         0.8862         0.312         Interm           P32         J76         3         0.217         0.276         0.8862         0.312         Interm           P32         J76         3         0.300         0.233         0.8862         0.263         0.092         0.181         Interm           P32         J79         6         0.225         0.072         0.9515         0.076         Surface           P32         J79         4         0.193         0.128         0.9213         0.139         Surface           P32         J79         4         -0.020         0.128         0.8862         0.044         Surface           P32         J79         3         0.137         0.074         0.8862         0.063         Surface           P32         J79         3         0.110         0.062         0.8862         0.064         Surface           P32         J79         3         0.217         0.057         0.8862         0.064         Surface           P32         J   | P22     | 176           | 4        | 0.140    | 0.200      | 0.9213                | 0.223      |         |            | Interm  |
| P32         J76         3         0.180         0.183         0.180         Interm           P32         J76         3         0.300         0.233         0.8862         0.263         0.092         0.181         Interm           P32         J79         6         0.225         0.072         0.9515         0.076         Surface           P32         J79         6         0.225         0.072         0.9515         0.076         Surface           P32         J79         6         0.226         0.0128         0.8862         0.144         Surface           P32         J79         3         0.120         0.172         0.9213         0.186         Surface           P32         J79         3         0.137         0.074         0.8862         0.083         Surface           P32         J79         3         0.110         0.062         0.8862         0.064         Surface           P32         J79         3         0.110         0.062         0.8862         0.113         Surface           P32         J79         4         0.213         0.113         0.113         Surface           P32         J79         5 <td>P22</td> <td>176</td> <td>4</td> <td>-0.010</td> <td>0.091</td> <td>0.9213</td> <td>0.098</td> <td></td> <td></td> <td>Interm</td>   | P22     | 176           | 4        | -0.010   | 0.091      | 0.9213                | 0.098      |         |            | Interm  |
| P32         J76         3         0.217         0.276         0.302         0.312         1         Interm           P32         J76         3         0.300         0.233         0.8862         0.263         0.092         0.181         Interm           P32         J79         6         0.225         0.072         0.9515         0.076         Surface           P32         J79         4         0.193         0.128         0.9213         0.139         Surface           P32         J79         4         0.020         0.172         0.9213         0.186         Surface           P32         J79         3         0.137         0.074         0.8862         0.083         Surface           P32         J79         3         0.110         0.062         0.8862         0.064         Surface           P32         J79         3         0.217         0.057         0.8862         0.064         Surface           P32         J79         4         0.0213         0.113         Surface           P32         J79         5         0.138         0.192         0.9400         0.204         Surface           P32         J79 <td>P22</td> <td>176</td> <td>4</td> <td>0.190</td> <td>0.103</td> <td>0.9213</td> <td>0.190</td> <td></td> <td></td> <td>Interm</td>  | P22     | 176           | 4        | 0.190    | 0.103      | 0.9213                | 0.190      |         |            | Interm  |
| P32         J79         G         0.325         0.3002         0.203         0.092         0.181         Internit           P32         J79         6         0.225         0.072         0.9915         0.076         Surface           P32         J79         4         0.193         0.128         0.9213         0.139         Surface           P32         J79         4         0.193         0.128         0.8862         0.144         Surface           P32         J79         4         -0.020         0.172         0.9213         0.186         Surface           P32         J79         3         0.137         0.074         0.8862         0.083         Surface           P32         J79         3         0.110         0.062         0.8862         0.064         Surface           P32         J79         3         0.217         0.057         0.8862         0.064         Surface           P32         J79         3         0.217         0.057         0.8862         0.064         Surface           P32         J79         5         0.138         0.192         0.204         Surface           P32         J79  | P32     | 176           | 2        | 0.217    | 0.270      | 0.0002                | 0.312      | 0.002   | 0.191      | Interm  |
| P32         J79         5         0.224         0.072         0.313         0.070         Surface           P32         J79         5         0.264         0.066         0.9400         0.070         Surface           P32         J79         4         0.193         0.128         0.8862         0.144         Surface           P32         J79         4         -0.020         0.172         0.9213         0.186         Surface           P32         J79         3         0.137         0.074         0.8862         0.083         Surface           P32         J79         3         0.110         0.062         0.8862         0.070         Surface           P32         J79         3         0.217         0.057         0.8862         0.064         Surface           P32         J79         4         0.213         0.104         0.9213         0.113         Surface           P32         J79         5         0.138         0.192         0.9400         0.204         Surface           P32         J79         5         0.164         0.63         0.9400         0.174         Surface           P32         J79         5<   | P32     | 170           | 6        | 0.300    | 0.233      | 0.0002                | 0.203      | 0.092   | 0.101      | Surface |
| P32         J79         J         0.200         0.000         0.0130         0.0133         0.0144         Surface           P32         J79         4         0.193         0.128         0.9213         0.139         Surface           P32         J79         4         -0.020         0.172         0.9213         0.186         Surface           P32         J79         3         0.137         0.074         0.8862         0.083         Surface           P32         J79         3         0.110         0.062         0.8862         0.083         Surface           P32         J79         3         0.217         0.057         0.8862         0.064         Surface           P32         J79         4         0.213         0.104         0.9213         0.113         Surface           P32         J79         5         0.138         0.192         0.9400         0.204         Surface           P32         J79         5         0.164         0.163         0.9400         0.174         Surface           P32         J79         5         0.164         0.163         0.9400         0.129         Surface           P32  | P32     | 170           | 5        | 0.223    | 0.072      | 0.9313                | 0.070      |         |            | Surface |
| P32         J79         3         0.120         0.121         0.134         Surface           P32         J79         3         0.220         0.128         0.8862         0.144         Surface           P32         J79         4         -0.020         0.172         0.9213         0.186         Surface           P32         J79         3         0.137         0.074         0.8862         0.083         Surface           P32         J79         3         0.110         0.062         0.8862         0.064         Surface           P32         J79         4         0.213         0.104         0.9213         0.113         Surface           P32         J79         4         0.213         0.104         0.9213         0.113         Surface           P32         J79         4         0.085         0.153         0.9213         0.166         Surface           P32         J79         5         0.164         0.163         0.9400         0.174         Surface           P32         J79         5         0.176         0.933         0.9400         0.223         Surface           P32         J79         5         0.148   | P32     | 170           | 3        | 0.204    | 0.000      | 0.9400                | 0.070      |         |            | Surface |
| P32       J79       J       J.22       0.122       0.123       0.0202       0.144       Surface         P32       J79       3       0.137       0.074       0.8862       0.083       Surface         P32       J79       3       0.110       0.062       0.8862       0.070       Surface         P32       J79       3       0.217       0.057       0.8862       0.064       Surface         P32       J79       4       0.213       0.104       0.9213       0.113       Surface         P32       J79       4       0.213       0.104       0.9213       0.113       Surface         P32       J79       4       0.085       0.153       0.9213       0.166       Surface         P32       J79       5       -0.164       0.163       0.9400       0.204       Surface         P32       J79       5       0.176       0.093       0.9400       0.174       Surface         P32       J79       5       0.128       0.121       0.9400       0.223       Surface         P32       J79       5       0.128       0.210       0.9400       0.223       Surface  | P32     | 170           | - 4      | 0.195    | 0.120      | 0.9213                | 0.139      |         |            | Surface |
| P32       J79       3       0.137       0.074       0.8862       0.083       Surface         P32       J79       3       0.117       0.062       0.8862       0.070       Surface         P32       J79       3       0.217       0.057       0.8862       0.070       Surface         P32       J79       4       0.213       0.114       0.9213       0.113       Surface         P32       J79       4       0.213       0.104       0.9213       0.113       Surface         P32       J79       5       0.138       0.192       0.9400       0.204       Surface         P32       J79       5       0.164       0.163       0.9400       0.174       Surface         P32       J79       5       0.164       0.163       0.9400       0.199       Surface         P32       J79       5       0.176       0.093       0.9400       0.129       Surface         P32       J79       5       0.128       0.121       0.9400       0.129       Surface         P32       J79       5       0.124       0.210       0.9400       0.223       Surface         P32  | P32     | 170           | 1        | -0.020   | 0.120      | 0.0002                | 0.144      |         |            | Surface |
| P32       J79       3       0.137       0.074       0.002       0.003       Surface         P32       J79       3       0.217       0.057       0.8862       0.070       Surface         P32       J79       4       0.217       0.057       0.8862       0.064       Surface         P32       J79       4       0.213       0.104       0.9213       0.113       Surface         P32       J79       4       0.085       0.153       0.9213       0.166       Surface         P32       J79       5       -0.164       0.163       0.9400       0.174       Surface         P32       J79       5       -0.164       0.163       0.9400       0.174       Surface         P32       J79       5       0.176       0.093       0.9400       0.099       Surface         P32       J79       5       0.128       0.121       0.9400       0.129       Surface         P32       J79       5       0.128       0.121       0.9400       0.223       Surface         P32       J79       5       0.148       0.097       0.9400       0.223       Surface         P32   | P32     | 170           | 4        | -0.020   | 0.172      | 0.9213                | 0.100      |         |            | Surface |
| P32       J79       3       0.217       0.057       0.8862       0.064       Surface         P32       J79       4       0.213       0.104       0.9213       0.113       Surface         P32       J79       4       0.213       0.104       0.9213       0.113       Surface         P32       J79       5       0.138       0.192       0.9400       0.204       Surface         P32       J79       5       -0.164       0.163       0.9400       0.174       Surface         P32       J79       5       -0.164       0.163       0.9400       0.174       Surface         P32       J79       5       0.176       0.093       0.9400       0.129       Surface         P32       J79       5       0.128       0.121       0.9400       0.129       Surface         P32       J79       5       0.148       0.097       0.9400       0.223       Surface         P32       J79       5       0.148       0.097       0.9400       0.223       Surface         P32       J79       3       0.237       0.076       0.8862       0.086       Surface         P32  | P32     | 170           | 3        | 0.137    | 0.074      | 0.0002                | 0.000      |         |            | Surface |
| P32       J79       4       0.213       0.104       0.9213       0.113       Surface         P32       J79       5       0.138       0.192       0.9400       0.204       Surface         P32       J79       5       0.138       0.192       0.9400       0.204       Surface         P32       J79       5       -0.164       0.163       0.9213       0.166       Surface         P32       J79       5       -0.164       0.163       0.9400       0.174       Surface         P32       J79       5       -0.164       0.166       0.8862       0.119       Surface         P32       J79       5       0.176       0.093       0.9400       0.129       Surface         P32       J79       5       0.128       0.121       0.9400       0.129       Surface         P32       J79       5       0.128       0.121       0.9400       0.223       Surface         P32       J79       5       0.148       0.097       0.9400       0.104       Surface         P32       J79       3       0.237       0.076       0.8862       0.086       Surface         P32   | P32     | 170           | 3        | 0.110    | 0.002      | 0.0002                | 0.070      |         |            | Surface |
| P32       J79       4       0.213       0.104       0.9213       0.113       Surface         P32       J79       5       0.138       0.192       0.9400       0.204       Surface         P32       J79       4       0.085       0.153       0.9213       0.166       Surface         P32       J79       5       -0.164       0.163       0.9400       0.174       Surface         P32       J79       5       0.176       0.093       0.9400       0.099       Surface         P32       J79       5       0.176       0.093       0.9400       0.129       Surface         P32       J79       5       0.128       0.121       0.9400       0.129       Surface         P32       J79       5       0.128       0.121       0.9400       0.223       Surface         P32       J79       5       0.148       0.097       0.9400       0.104       Surface         P32       J79       5       0.196       0.209       0.9400       0.223       Surface         P32       J79       3       0.020       0.078       0.8862       0.086       Surface         P32   | P32     | 170           | 3        | 0.217    | 0.037      | 0.0002                | 0.004      |         |            | Surface |
| P32       J79       4       0.085       0.132       0.9213       0.166       Surface         P32       J79       5       -0.164       0.163       0.9400       0.174       Surface         P32       J79       5       -0.164       0.163       0.9400       0.174       Surface         P32       J79       5       -0.164       0.163       0.9400       0.099       Surface         P32       J79       5       0.176       0.093       0.9400       0.099       Surface         P32       J79       5       0.128       0.121       0.9400       0.129       Surface         P32       J79       5       -0.024       0.210       0.9400       0.223       Surface         P32       J79       5       -0.148       0.097       0.9400       0.223       Surface         P32       J79       5       0.148       0.097       0.9400       0.223       Surface         P32       J79       5       0.196       0.209       0.9400       0.223       Surface         P32       J79       3       -0.020       0.078       0.8862       0.086       Surface         P32 <td>P32</td> <td>179</td> <td>5</td> <td>0.213</td> <td>0.104</td> <td>0.9213</td> <td>0.113</td> <td></td> <td></td> <td>Surface</td>   | P32     | 179           | 5        | 0.213    | 0.104      | 0.9213                | 0.113      |         |            | Surface |
| P32       J79       5       -0.164       0.163       0.9400       0.174       Surface         P32       J79       3       -0.150       0.106       0.8862       0.119       Surface         P32       J79       5       0.176       0.093       0.9400       0.099       Surface         P32       J79       5       0.176       0.093       0.9400       0.129       Surface         P32       J79       5       0.128       0.121       0.9400       0.129       Surface         P32       J79       5       0.128       0.121       0.9400       0.223       Surface         P32       J79       5       0.148       0.097       0.9400       0.104       Surface         P32       J79       5       0.148       0.097       0.9400       0.104       Surface         P32       J79       3       0.237       0.076       0.8862       0.086       Surface         P32       J79       3       0.1020       0.078       0.8862       0.088       Surface         P32       J79       3       0.110       0.123       0.8862       0.103       Surface         P32   | P32     | 170           | 3        | 0.130    | 0.192      | 0.9400                | 0.204      |         |            | Surface |
| P32       J79       3       -0.104       0.103       0.9400       0.174       Surface         P32       J79       5       0.176       0.093       0.9400       0.099       Surface         P32       J79       5       0.128       0.121       0.9400       0.129       Surface         P32       J79       5       0.128       0.121       0.9400       0.129       Surface         P32       J79       5       0.128       0.121       0.9400       0.223       Surface         P32       J79       5       0.148       0.097       0.9400       0.104       Surface         P32       J79       5       0.148       0.097       0.9400       0.104       Surface         P32       J79       5       0.196       0.209       0.9400       0.223       Surface         P32       J79       3       0.020       0.078       0.8862       0.086       Surface         P32       J79       3       0.110       0.123       0.8862       0.088       Surface         P32       J79       3       0.097       0.038       0.8862       0.043       Surface         P32   | P32     | 170           | 5        | -0.164   | 0.100      | 0.9213                | 0.100      |         |            | Surface |
| P32       J79       5       0.130       0.100       0.9400       0.099       Surface         P32       J79       5       0.128       0.121       0.9400       0.129       Surface         P32       J79       5       0.128       0.121       0.9400       0.129       Surface         P32       J79       5       0.024       0.210       0.9400       0.223       Surface         P32       J79       5       0.148       0.097       0.9400       0.223       Surface         P32       J79       5       0.148       0.097       0.9400       0.104       Surface         P32       J79       5       0.196       0.209       0.9400       0.223       Surface         P32       J79       3       0.237       0.076       0.8862       0.086       Surface         P32       J79       3       0.1020       0.078       0.8862       0.088       Surface         P32       J79       3       0.110       0.123       0.8862       0.139       Surface         P32       J79       3       0.097       0.038       0.8862       0.043       Surface         P32   | P32     | 179           | 3        | -0.104   | 0.105      | 0.3400                | 0.174      |         |            | Surface |
| P32       J79       5       0.170       0.033       0.13400       0.033       0.033       0.033       0.033       0.033       0.033       0.033       0.033       0.033       0.033       0.033       0.033       0.033       0.033       0.033       0.0129       Surface         P32       J79       5       0.024       0.210       0.9400       0.223       Surface         P32       J79       5       0.148       0.097       0.9400       0.104       Surface         P32       J79       3       0.237       0.076       0.8862       0.086       Surface         P32       J79       5       0.196       0.209       0.9400       0.223       Surface         P32       J79       3       -0.020       0.078       0.8862       0.088       Surface         P32       J79       3       0.110       0.123       0.8862       0.139       Surface         P32       J79       3       0.097       0.038       0.8862       0.043       Surface         P32       J79       3       0.043       0.142       0.8862       0.043       Surface         P32       J79       3       0.04  | P32     | 179           | 5        | 0.176    | 0.100      | 0.0002                | 0.119      |         |            | Surface |
| P32       J79       5       -0.024       0.210       0.9400       0.223       Surface         P32       J79       5       0.148       0.097       0.9400       0.104       Surface         P32       J79       5       0.148       0.097       0.9400       0.104       Surface         P32       J79       3       0.237       0.076       0.8862       0.086       Surface         P32       J79       5       0.196       0.209       0.9400       0.223       Surface         P32       J79       3       -0.020       0.078       0.8862       0.086       Surface         P32       J79       3       -0.020       0.078       0.8862       0.088       Surface         P32       J79       3       0.110       0.123       0.8862       0.139       Surface         P32       J79       3       0.097       0.038       0.8862       0.043       Surface         P32       J79       3       0.097       0.038       0.8862       0.043       Surface         P32       J79       3       0.043       0.142       0.8862       0.160       0.111       0.125       Surface <td>P32</td> <td>179</td> <td>5</td> <td>0.170</td> <td>0.000</td> <td>0.0400</td> <td>0.000</td> <td></td> <td></td> <td>Surface</td>  | P32     | 179           | 5        | 0.170    | 0.000      | 0.0400                | 0.000      |         |            | Surface |
| P32       J79       5       0.148       0.097       0.9400       0.104       Surface         P32       J79       3       0.237       0.076       0.8862       0.086       Surface         P32       J79       3       0.237       0.076       0.8862       0.086       Surface         P32       J79       5       0.196       0.209       0.9400       0.223       Surface         P32       J79       3       -0.020       0.078       0.8862       0.088       Surface         P32       J79       3       0.110       0.123       0.8862       0.139       Surface         P32       J79       3       0.097       0.038       0.8862       0.139       Surface         P32       J79       3       0.097       0.038       0.8862       0.043       Surface         P32       J79       3       0.097       0.038       0.8862       0.043       Surface         P32       J79       3       0.043       0.142       0.8862       0.043       Surface         P33       J73       1       0.320       -       -       -       Interm         P33       J73 <td>P32</td> <td>179</td> <td>5</td> <td>-0.024</td> <td>0.121</td> <td>0.9400</td> <td>0.123</td> <td></td> <td></td> <td>Surface</td>   | P32     | 179           | 5        | -0.024   | 0.121      | 0.9400                | 0.123      |         |            | Surface |
| P32       J79       3       0.237       0.076       0.8862       0.086       Surface         P32       J79       5       0.196       0.209       0.9400       0.223       Surface         P32       J79       3       -0.020       0.078       0.8862       0.088       Surface         P32       J79       3       -0.020       0.078       0.8862       0.088       Surface         P32       J79       3       0.110       0.123       0.8862       0.139       Surface         P32       J79       4       0.098       0.095       0.9213       0.103       Surface         P32       J79       3       0.097       0.038       0.8862       0.043       Surface         P32       J79       3       0.043       0.142       0.8862       0.043       Surface         P32       J79       3       0.043       0.142       0.8862       0.043       Surface         P32       J79       3       0.043       0.142       0.8862       0.160       0.111       0.125       Surface         P33       J73       1       0.320       -       -       -       Interm  | P32     | 179           | 5        | 0.024    | 0.210      | 0.3400                | 0.223      |         |            | Surface |
| P32       J79       5       0.196       0.209       0.9400       0.223       Surface         P32       J79       3       -0.020       0.078       0.8862       0.088       Surface         P32       J79       3       0.110       0.123       0.8862       0.088       Surface         P32       J79       3       0.110       0.123       0.8862       0.139       Surface         P32       J79       4       0.098       0.095       0.9213       0.103       Surface         P32       J79       3       0.097       0.038       0.8862       0.043       Surface         P32       J79       3       0.097       0.038       0.8862       0.043       Surface         P32       J79       3       0.043       0.142       0.8862       0.043       Surface         P33       J73       1       0.320       -       -       -       Interm         P33       J73       3       0.050       0.233       0.8862       0.262       Interm         P33       J73       3       0.052       0.211       0.9400       0.224       Interm         P33       J73   | P32     | 179           | 3        | 0.140    | 0.037      | 0.8862                | 0.086      |         |            | Surface |
| P32       J79       3       -0.020       0.078       0.8862       0.088       Surface         P32       J79       3       0.110       0.123       0.8862       0.088       Surface         P32       J79       3       0.110       0.123       0.8862       0.139       Surface         P32       J79       4       0.098       0.095       0.9213       0.103       Surface         P32       J79       3       0.097       0.038       0.8862       0.043       Surface         P32       J79       3       0.097       0.038       0.8862       0.043       Surface         P32       J79       3       0.043       0.142       0.8862       0.043       Surface         P33       J73       1       0.320       -       -       -       Interm         P33       J73       3       0.050       0.233       0.8862       0.262       Interm         P33       J73       3       0.023       0.501       0.8862       0.566       Interm         P33       J73       5       0.052       0.211       0.9400       0.224       Interm         P33       J73  | P32     | 179           | 5        | 0.207    | 0.070      | 0.0002                | 0.000      |         |            | Surface |
| P32       J79       3       0.110       0.123       0.8862       0.139       Surface         P32       J79       4       0.098       0.095       0.9213       0.103       Surface         P32       J79       3       0.097       0.038       0.8862       0.043       Surface         P32       J79       3       0.097       0.038       0.8862       0.043       Surface         P32       J79       3       0.043       0.142       0.8862       0.043       Surface         P33       J73       1       0.320       -       -       -       Interm         P33       J73       3       0.050       0.233       0.8862       0.262       Interm         P33       J73       3       0.023       0.501       0.8862       0.262       Interm         P33       J73       3       0.023       0.501       0.8862       0.262       Interm         P33       J73       5       0.052       0.211       0.9400       0.224       Interm         P33       J73       4       -0.043       0.195       0.9213       0.211       Interm         P33       J73  | P32     | .179          | 3        | -0.020   | 0.200      | 0.8862                | 0.220      |         |            | Surface |
| P32       J79       4       0.098       0.095       0.9213       0.103       Surface         P32       J79       3       0.097       0.038       0.8862       0.043       Surface         P32       J79       3       0.097       0.038       0.8862       0.043       Surface         P32       J79       3       0.043       0.142       0.8862       0.043       Surface         P33       J73       1       0.320       -       -       -       Interm         P33       J73       3       0.050       0.233       0.8862       0.262       Interm         P33       J73       3       0.050       0.233       0.8862       0.262       Interm         P33       J73       3       0.023       0.501       0.8862       0.262       Interm         P33       J73       5       0.052       0.211       0.9400       0.224       Interm         P33       J73       4       -0.043       0.195       0.9213       0.211       Interm         P33       J73       3       0.057       0.096       0.8862       0.108       Interm   | P32     | .179          | 3        | 0.020    | 0.070      | 0.8862                | 0.000      |         |            | Surface |
| P32       J79       3       0.097       0.038       0.8862       0.043       Surface         P32       J79       3       0.043       0.142       0.8862       0.043       Surface         P32       J79       3       0.043       0.142       0.8862       0.160       0.111       0.125       Surface         P33       J73       1       0.320       -       -       -       Interm         P33       J73       3       0.050       0.233       0.8862       0.262       Interm         P33       J73       3       0.050       0.233       0.8862       0.262       Interm         P33       J73       3       0.052       0.211       0.9400       0.224       Interm         P33       J73       4       -0.043       0.195       0.9213       0.211       Interm         P33       J73       3       0.057       0.096       0.8862       0.108       Interm  | P32     | .179          | 4        | 0.098    | 0.095      | 0.0002                | 0.103      |         |            | Surface |
| P32       J79       3       0.043       0.142       0.8862       0.160       0.111       0.125       Surface         P33       J73       1       0.320       -       -       -       Interm         P33       J73       3       0.050       0.233       0.8862       0.262       Interm         P33       J73       3       0.050       0.233       0.8862       0.262       Interm         P33       J73       3       0.052       0.211       0.9400       0.224       Interm         P33       J73       4       -0.043       0.195       0.9213       0.211       Interm         P33       J73       3       0.057       0.096       0.8862       0.108       Interm  | P32     | .179          | 3        | 0.000    | 0.038      | 0.8862                | 0.100      |         |            | Surface |
| P33       J73       1       0.320       -       -       -       Interm         P33       J73       3       0.050       0.233       0.8862       0.262       Interm         P33       J73       3       0.050       0.233       0.8862       0.262       Interm         P33       J73       3       0.023       0.501       0.8862       0.566       Interm         P33       J73       5       0.052       0.211       0.9400       0.224       Interm         P33       J73       4       -0.043       0.195       0.9213       0.211       Interm         P33       J73       3       0.057       0.096       0.8862       0.108       Interm   | P32     | .179          | 3        | 0.043    | 0 142      | 0.8862                | 0.160      | 0 111   | 0 125      | Surface |
| P33         J73         3         0.050         0.233         0.8862         0.262         Interm           P33         J73         3         0.023         0.501         0.8862         0.262         Interm           P33         J73         3         0.023         0.501         0.8862         0.566         Interm           P33         J73         5         0.052         0.211         0.9400         0.224         Interm           P33         J73         4         -0.043         0.195         0.9213         0.211         Interm           P33         J73         3         0.057         0.096         0.8862         0.108         Interm  | P33     | .173          | 1        | 0.320    | _          | -                     | _          | 0.111   | 0.120      | Interm  |
| P33         J73         3         0.023         0.501         0.8862         0.566         Interm           P33         J73         5         0.052         0.211         0.9400         0.224         Interm           P33         J73         4         -0.043         0.195         0.9213         0.211         Interm           P33         J73         3         0.057         0.096         0.8862         0.108         Interm  | P33     | .173          | 3        | 0.020    | 0.233      | 0 8862                | 0 262      |         |            | Interm  |
| P33         J73         5         0.052         0.201         0.0002   | P33     | .173          | 3        | 0.023    | 0.501      | 0.8862                | 0.566      |         |            | Interm  |
| P33         J73         4         -0.043         0.195         0.9213         0.211         Interm           P33         J73         3         0.057         0.096         0.8862         0.108         Interm  | P33     | .173          | 5        | 0.052    | 0.211      | 0.9400                | 0.224      |         |            | Interm  |
| P33 .73 3 0.057 0.096 0.8862 0.108 Interm   | P33     | .173          | 4        | -0.043   | 0 195      | 0.0213                | 0.211      |         |            | Interm  |
|   | P33     | .173          | 3        | 0.057    | 0.096      | 0.8862                | 0.108      |         |            | Interm  |

Table B.4. Summary of Unbiased Lot Std Dev for AC for Each Project (continued)

| Project | JMF<br>Number | Lot Size | Lot Mean | Lot St Dev | <i>c</i> <sub>4</sub> | Lot St Dev | Average  | Avg Lot SD | Course  |
|---------|---------------|----------|----------|------------|-----------------------|------------|----------|------------|---------|
| P33     |               | 3        | 0 153    | 0.241      | 0 8862                | 0.272      | Lot moun | Unblaced   | Interm  |
| P33     | .173          | 3        | 0.013    | 0.146      | 0.8862                | 0.165      | 0.078    | 0.258      | Interm  |
| P33     | J75           | 1        | -0 100   | _          | -                     | -          | 0.070    | 0.200      | Surface |
| P33     | J75           | 1        | -0 150   | _          | _                     | _          |          |            | Surface |
| P33     | J75           | 1        | 0.050    | _          | _                     | _          |          |            | Surface |
| P33     | J75           | 1        | -0.160   | _          | _                     | _          |          |            | Surface |
| P33     | J75           | 1        | -0.030   | _          | _                     | _          |          |            | Surface |
| P33     | J75           | 1        | 0.370    | _          | _                     | _          |          |            | Surface |
| P33     | J75           | 1        | -0.170   | _          | _                     | _          |          |            | Surface |
| P33     | J75           | 1        | -0.100   | -          | _                     | _          |          |            | Surface |
| P33     | J75           | 1        | -0.100   | -          | _                     | _          |          |            | Surface |
| P33     | J75           | 1        | 0.240    | -          | _                     | _          | -0.015   | _          | Surface |
| P33     | J77           | 4        | -0.120   | 0.228      | 0.9213                | 0.248      |          |            | Surface |
| P33     | J77           | 4        | 0.130    | 0.182      | 0.9213                | 0.197      |          |            | Surface |
| P33     | J77           | 4        | 0.325    | 0.090      | 0.9213                | 0.097      |          |            | Surface |
| P33     | J77           | 4        | 0.028    | 0.200      | 0.9213                | 0.217      |          |            | Surface |
| P33     | J77           | 3        | -0.027   | 0.220      | 0.8862                | 0.248      |          |            | Surface |
| P33     | J77           | 3        | 0.257    | 0.327      | 0.8862                | 0.369      | 0.099    | 0.229      | Surface |
| P33     | J78           | 4        | 0.138    | 0.488      | 0.9213                | 0.530      |          |            | Surface |
| P33     | J78           | 3        | 0.213    | 0.261      | 0.8862                | 0.294      |          |            | Surface |
| P33     | J78           | 3        | -0.203   | 0.300      | 0.8862                | 0.339      |          |            | Surface |
| P33     | J78           | 3        | 0.020    | 0.230      | 0.8862                | 0.260      | 0.042    | 0.356      | Surface |
| P34     | J62           | 4        | -0.005   | 0.227      | 0.9213                | 0.247      |          |            | Surface |
| P34     | J62           | 4        | 0.205    | 0.067      | 0.9213                | 0.072      |          |            | Surface |
| P34     | J62           | 6        | -0.100   | 0.121      | 0.9515                | 0.127      |          |            | Surface |
| P34     | J62           | 4        | -0.123   | 0.087      | 0.9213                | 0.094      |          |            | Surface |
| P34     | J62           | 4        | -0.148   | 0.366      | 0.9213                | 0.397      |          |            | Surface |
| P34     | J62           | 4        | 0.103    | 0.085      | 0.9213                | 0.092      |          |            | Surface |
| P34     | J62           | 2        | -0.090   | 0.014      | 0.7979                | 0.018      | -0.023   | 0.150      | Surface |
| P34     | J80           | 2        | -0.045   | 0.064      | 0.7979                | 0.080      |          |            | Surface |
| P34     | J80           | 2        | 0.080    | 0.071      | 0.7979                | 0.089      |          |            | Surface |
| P34     | J80           | 3        | 0.060    | 0.087      | 0.8862                | 0.098      |          |            | Surface |
| P34     | J80           | 1        | -0.010   | -          | -                     | -          |          |            | Surface |
| P34     | J80           | 3        | -0.027   | 0.049      | 0.8862                | 0.056      |          |            | Surface |
| P34     | J80           | 1        | -0.230   | _          | _                     | -          | -0.029   | 0.081      | Surface |
| P34     | J81           | 2        | -0.085   | 0.035      | 0.7979                | 0.044      |          |            | Surface |
| P34     | J81           | 2        | 0.000    | 0.184      | 0.7979                | 0.230      |          |            | Surface |
| P34     | J81           | 1        | 0.160    | -          | -                     | _          |          |            | Surface |
| P34     | J81           | 2        | 0.160    | 0.339      | 0.7979                | 0.425      |          |            | Surface |
| P34     | J81           | 2        | 0.195    | 0.318      | 0.7979                | 0.399      |          |            | Surface |
| P34     | J81           | 2        | 0.015    | 0.064      | 0.7979                | 0.080      | 0.007    | 0.000      | Surface |
| P34     | J81           | 2        | 0.235    | 0.304      | 0.7979                | 0.381      | 0.097    | 0.260      | Surface |
| P35     | J32           | 3        | -0.053   | 0.219      | 0.8862                | 0.248      |          |            | Surface |
| P35     | J32           | 1        | -0.180   | -          | -                     | -          |          |            | Surface |
| P35     | J32           | 3        | -0.017   | 0.081      | 0.8862                | 0.092      |          |            | Surface |
| P35     | J32           | 3        | -0.137   | 0.090      | 0.8862                | 0.101      |          |            | Surface |
| P35     | J32           | 3        | -0.060   | 0.087      | 0.8862                | 0.098      |          |            | Surface |

# Table B.4. Summary of Unbiased Lot Std Dev for AC for Each Project (continued)

| P35         J32         1         0.270         -         -         -         -         -0.029         0.135         Surface           P35         J38         2         -0.130         0.099         0.7979         0.071         Surface           P35         J38         1         0.260         -         -         -         -         Surface           P35         J38         1         0.260         -         -         -         -         Surface           P35         J38         2         0.075         0.078         0.7979         0.063         Surface           P35         J38         2         0.070         0.42         0.7979         0.053         Surface           P35         J38         1         0.160         -         -         -         -         Surface           P35         J38         3         0.250         0.070         0.8862         0.072         Surface           P35         J38         3         0.007         0.119         0.862         0.133         Surface           P35         J38         1         -0.020         -         -         -         Surface <t< th=""><th>Project<br/>Number</th><th>JMF<br/>Number</th><th>Lot Size</th><th>Lot Mean</th><th>Lot St Dev<br/>(biased)</th><th><math>c_4</math></th><th>Lot St Dev<br/>(unbiased)</th><th>Average<br/>Lot Mean</th><th>Avg Lot SD<br/>Unbiased</th><th>Course</th></t<>   | Project<br>Number | JMF<br>Number | Lot Size | Lot Mean | Lot St Dev<br>(biased) | $c_4$  | Lot St Dev<br>(unbiased) | Average<br>Lot Mean | Avg Lot SD<br>Unbiased | Course  |
|--|-------------------|---------------|----------|----------|------------------------|--------|--------------------------|---------------------|------------------------|---------|
| P35         J38         2         -0.130         0.099         0.7979         0.124         Surface           P35         J38         1         0.060         0.077         0.7979         0.071         Surface           P35         J38         2         0.075         0.7979         0.097         Surface           P35         J38         2         0.070         0.042         0.7979         0.053         Surface           P35         J38         2         0.070         0.042         0.7979         0.053         Surface           P35         J38         2         0.010         0.212         0.7979         0.266         Surface           P35         J38         3         0.250         0.070         0.862         0.072         Surface           P35         J38         2         0.085         0.940         0.072         Surface           P35         J38         2         0.060         0.862         0.135         Surface           P35         J38         3         0.010         0.118         0.8862         0.135         Surface           P35         J38         1         -0.020         -         -   | P35               | J32           | 1        | 0.270    | _                      | _      | _                        | -0.029              | 0.135                  | Surface |
| P35         J38         2         0.060         0.057         0.7979         0.071         Surface           P35         J38         1         0.260         -         -         -         Surface           P35         J38         2         0.075         0.078         0.097         Surface           P35         J38         2         0.070         0.042         0.7979         0.053         Surface           P35         J38         1         0.160         -         -         -         Surface           P35         J38         2         -0.010         0.212         0.7979         0.266         Surface           P35         J38         3         0.250         0.070         0.8862         0.072         Surface           P35         J38         5         0.096         0.9213         0.066         Surface           P35         J38         3         0.007         0.118         0.8862         0.133         Surface           P35         J38         1         -0.020         -         -         -         Surface           P35         J38         1         -0.070         -         -         - <td>P35</td> <td>J38</td> <td>2</td> <td>-0.130</td> <td>0.099</td> <td>0.7979</td> <td>0.124</td> <td></td> <td></td> <td>Surface</td>   | P35               | J38           | 2        | -0.130   | 0.099                  | 0.7979 | 0.124                    |                     |                        | Surface |
| P35         J38         1         0.260         -         -         -         Surface           P35         J38         2         0.075         0.078         0.7979         0.097         Surface           P35         J38         1         0.160         -         -         -         Surface           P35         J38         1         0.160         -         -         -         Surface           P35         J38         2         -0.010         0.212         0.7979         0.266         Surface           P35         J38         3         0.200         0.070         0.8862         0.079         Surface           P35         J38         4         0.060         0.067         0.9400         0.072         Surface           P35         J38         4         0.060         0.061         0.9213         0.065         Surface           P35         J38         3         0.007         0.118         0.8862         0.133         Surface           P35         J38         1         -0.020         -         -         -         Surface           P35         J38         1         -0.070         -   | P35               | J38           | 2        | 0.060    | 0.057                  | 0.7979 | 0.071                    |                     |                        | Surface |
| P35         J38         2         0.075         0.078         0.7979         0.097         Surface           P35         J38         2         0.070         0.042         0.7979         0.063         Surface           P35         J38         1         0.160         -         -         -         Surface           P35         J38         2         -0.010         0.212         0.7979         0.266         Surface           P35         J38         3         0.250         0.070         0.8862         0.079         Surface           P35         J38         5         0.096         0.9400         0.072         Surface           P35         J38         2         0.085         0.092         0.7979         0.115         Surface           P35         J38         3         0.007         0.118         0.8862         0.133         Surface           P35         J38         1         -0.020         -         -         -         Surface           P35         J38         1         -0.070         -         -         -         0.050         0.117         Surface           P35         J38         1  | P35               | J38           | 1        | 0.260    | _                      | _      | _                        |                     |                        | Surface |
| P35         J38         2         0.070         0.042         0.7979         0.053         Surface           P35         J38         1         0.160         -         -         -         Surface           P35         J38         2         -0.010         0.212         0.7979         0.266         Surface           P35         J38         5         0.096         0.067         0.9400         0.072         Surface           P35         J38         2         0.086         0.092         0.7979         0.115         Surface           P35         J38         2         0.080         0.0921         0.065         Surface           P35         J38         3         0.007         0.119         0.8862         0.133         Surface           P35         J38         3         0.007         -         -         -         Surface           P35         J38         1         -0.020         -         -         -         0.050         0.117         Surface           P35         J38         1         -0.020         -         -         -         0.050         0.117         Surface           P36         J3  | P35               | J38           | 2        | 0.075    | 0.078                  | 0.7979 | 0.097                    |                     |                        | Surface |
| P35         J38         1         0.160         -         -         -         -         Surface           P35         J38         2         -0.010         0.212         0.7979         0.266         Surface           P35         J38         5         0.096         0.067         0.9400         0.072         Surface           P35         J38         2         0.085         0.092         0.7979         0.115         Surface           P35         J38         4         0.060         0.060         0.0213         O.065         Surface           P35         J38         4         0.060         0.9213         O.065         Surface           P35         J38         3         0.007         0.118         0.8862         0.133         Surface           P35         J38         1         -0.020         -         -         -         Surface           P35         J38         1         -0.070         -         -         -         0.050         0.117         Surface           P35         J38         1         -0.070         -         -         -         0.050         0.117         Surface           P36  | P35               | J38           | 2        | 0.070    | 0.042                  | 0.7979 | 0.053                    |                     |                        | Surface |
| P35         J38         2         -0.010         0.212         0.7979         0.266         Surface           P35         J38         3         0.250         0.070         0.8862         0.079         Surface           P35         J38         2         0.085         0.092         0.7979         0.115         Surface           P35         J38         2         0.085         0.092         0.7979         0.115         Surface           P35         J38         4         0.060         0.0213         0.065         Surface           P35         J38         3         0.007         0.118         0.8862         0.133         Surface           P35         J38         2         -0.110         0.156         0.7979         0.195         Surface           P35         J38         1         -0.070         -         -         -         0.050         0.117         Surface           P35         J38         1         -0.070         -         -         -         0.050         0.117         Surface           P35         J38         1         -0.070         -         -         -         0.050         0.117         Surfac   | P35               | J38           | 1        | 0.160    | _                      | _      | -                        |                     |                        | Surface |
| P35         J38         3         0.250         0.070         0.8862         0.079         Surface           P35         J38         5         0.096         0.067         0.9400         0.072         Surface           P35         J38         2         0.085         0.092         0.779         0.115         Surface           P35         J38         4         0.060         0.9213         0.065         Surface           P35         J38         3         0.007         0.119         0.8862         0.135         Surface           P35         J38         3         0.007         0.119         0.8862         0.135         Surface           P35         J38         1         -0.020         -         -         -         0.050         0.117         Surface           P35         J38         1         -0.070         -         -         -         0.050         0.117         Surface           P35         J38         1         -0.070         -         -         -         0.050         0.117         Surface           P36         J38         1         -0.070         -         -         -         0.050 <t< td=""><td>P35</td><td>J38</td><td>2</td><td>-0.010</td><td>0.212</td><td>0.7979</td><td>0.266</td><td></td><td></td><td>Surface</td></t<>   | P35               | J38           | 2        | -0.010   | 0.212                  | 0.7979 | 0.266                    |                     |                        | Surface |
| P35         J38         5         0.067         0.9400         0.072         Surface           P35         J38         2         0.085         0.092         0.7979         0.115         Surface           P35         J38         3         0.007         0.119         0.065         Surface           P35         J38         3         0.007         0.119         0.8662         0.133         Surface           P35         J38         3         0.010         0.118         0.8862         0.133         Surface           P35         J38         1         -0.020         -         -         -         Surface           P35         J38         1         -0.070         -         -         -         0.050         0.117         Surface           P35         J38         1         -0.070         -         -         -         0.050         0.117         Surface           P35         J38         1         -0.070         -         -         -         0.050         0.117         Surface           P36         J38         1         -0.070         -         -         -         0.050         0.117         Surface <td>P35</td> <td>J38</td> <td>3</td> <td>0.250</td> <td>0.070</td> <td>0.8862</td> <td>0.079</td> <td></td> <td></td> <td>Surface</td>  | P35               | J38           | 3        | 0.250    | 0.070                  | 0.8862 | 0.079                    |                     |                        | Surface |
| P35         J38         2         0.085         0.092         0.7979         0.115         Surface           P35         J38         4         0.060         0.0213         0.065         Surface           P35         J38         3         0.007         0.119         0.8862         0.133         Surface           P35         J38         2         -0.110         0.156         0.7979         0.195         Surface           P35         J38         1         -0.020         -         -         -         0.050         0.117         Surface           P35         J38         1         -0.070         -         -         -         0.050         0.117         Surface           P35         J38         1         -0.070         -         -         -         0.050         0.117         Surface           P36         J38         1         -0.070         -         -         -         0.050         0.117         Surface           P37         J38         1         -0.070         -         -         -         0.050         0.117         Surface           P37         J38         1         -0.070         -   | P35               | J38           | 5        | 0.096    | 0.067                  | 0.9400 | 0.072                    |                     |                        | Surface |
| P35         J38         4         0.060         0.0213         0.065         Surface           P35         J38         3         0.007         0.119         0.8862         0.135         Surface           P35         J38         2         -0.110         0.156         0.7979         0.195         Surface           P35         J38         1         -0.020         -         -         -         0.050         0.117         Surface           P35         J38         1         -0.020         -         -         -         -         Surface           P35         J38         1         -0.020         -         -         -         Surface           P36         J38         1         -0.020         -         -         -         Surface           P36         J38         1         -0.020 <td< td=""><td>P35</td><td>J38</td><td>2</td><td>0.085</td><td>0.092</td><td>0.7979</td><td>0.115</td><td></td><td></td><td>Surface</td></td<>   | P35               | J38           | 2        | 0.085    | 0.092                  | 0.7979 | 0.115                    |                     |                        | Surface |
| P35       J38       3       0.007       0.119       0.8862       0.135       Surface         P35       J38       2       -0.110       0.118       0.8862       0.133       Surface         P35       J38       2       -0.110       0.156       0.7979       0.195       Surface         P35       J38       1       -0.020       -       -       -       0.050       0.117       Surface         P35       J38       1       -0.020       -       -       -       0.050       0.117       Surface         P35       J38       1       -0.070       -       -       -       0.050       0.117       Surface         P35       J38       1       -0.070       -       -       -       0.050       0.117       Surface         P35       J38       1       -0.070       -       -       -       0.050       0.117       Surface         P36       J38       1       -0.070       -       -       -       0.050       0.117       Surface         P37       J38       1       -0.070       -       -       -       0.117       Surface         P37<   | P35               | J38           | 4        | 0.060    | 0.060                  | 0.9213 | 0.065                    |                     |                        | Surface |
| P35       J38       3       0.010       0.118       0.8862       0.133       Surface         P35       J38       1       -0.020       -       -       -       Surface         P35       J38       1       -0.020       -       -       -       -       Surface         P35       J38       1       -0.070       -       -       -       0.050       0.117       Surface         P35       J38       1       -0.070       -       -       -       0.050       0.117       Surface         P35       J38       1       -0.070       -       -       -       0.050       0.117       Surface         P35       J38       1       -0.070       -       -       -       0.050       0.117       Surface         P35       J38       1       -0.070       -       -       -       0.050       0.117       Surface         P36       J38       1       -0.070       -       -       -       0.010       0.117       Surface         P37       P38       1       -0.070       -       -       -       -       -       -       -       -  | P35               | J38           | 3        | 0.007    | 0.119                  | 0.8862 | 0.135                    |                     |                        | Surface |
| P35       J38       2       -0.110       0.156       0.7979       0.195       Surface         P35       J38       1       -0.020       -       -       -       -       Surface         P35       J38       1       -0.070       -       -       -       0.050       0.117       Surface         P35       J38       1       -0.070       -       -       -       0.050       0.117       Surface         P36       J38       1       -0.070       -       -       -       0.050       0.117       Surface         P36       J38       1       -0.070       -       -       -       0.050       0.117       Surface         P36       J38       1       -       0.70       -       -       -       0.050       0.117       Surface         P37       I  | P35               | J38           | 3        | 0.010    | 0.118                  | 0.8862 | 0.133                    |                     |                        | Surface |
| P35         J38         1         -0.020 $      0.050$ $0.117$ Surface           P35         J38         1         -0.070 $   0.050$ $0.117$ Surface           P35         J38         1         - $   0.050$ $0.117$ Surface           P36         I  | P35               | J38           | 2        | -0.110   | 0.156                  | 0.7979 | 0.195                    |                     |                        | Surface |
| P35       J38       1       -0.070       -       -       -       0.050       0.117       Surface         Image: Second seco   | P35               | J38           | 1        | -0.020   | -                      | _      | -                        |                     |                        | Surface |
| Image: series of the series  | P35               | J38           | 1        | -0.070   | -                      | —      | _                        | 0.050               | 0.117                  | Surface |
| Image: series of the series  |                   |               |          |          |                        |        |                          |                     |                        |         |
| Image: series of the series  |                   |               |          |          |                        |        |                          |                     |                        |         |
| Image: series of the series  |                   |               |          |          |                        |        |                          |                     |                        |         |
| Image: section of the section of th |                   |               |          |          |                        |        |                          |                     |                        |         |
| Image: series of the series  |                   |               |          |          |                        |        |                          |                     |                        |         |
| Image: series of the series  |                   |               |          |          |                        |        |                          |                     |                        |         |
| Image: series of the series  |                   |               |          |          |                        |        |                          |                     |                        |         |
| Image: series of the series  |                   |               |          |          |                        |        |                          |                     |                        |         |
| Image: series of the series  |                   |               |          |          |                        |        |                          |                     |                        |         |
| Image: series of the series  |                   |               |          |          |                        |        |                          |                     |                        |         |
| Image: series of the series  |                   |               |          |          |                        |        |                          |                     |                        |         |
| Image: series of the series  |                   |               |          |          |                        |        |                          |                     |                        |         |
| Image: series of the series  |                   |               |          |          |                        |        |                          |                     |                        |         |
| Image: series of the series  |                   |               |          |          |                        |        |                          |                     |                        |         |
| Image: series of the series  |                   |               |          |          |                        |        |                          |                     |                        |         |
| Image: series of the series  |                   |               |          |          |                        |        |                          |                     |                        |         |
| Image: state in the state in |                   |               |          |          |                        |        |                          |                     |                        |         |
| Image: series of the series  |                   |               |          |          |                        |        |                          |                     |                        |         |
| Image: state of the state of |                   |               |          |          |                        |        |                          |                     |                        |         |
| Image: state of the state of |                   |               |          |          |                        |        |                          |                     |                        |         |
| Image: state of the state of |                   |               |          |          |                        |        |                          |                     |                        |         |
| Image: state of the state o  |                   |               |          |          |                        |        |                          |                     |                        |         |
| Image: state of the state o  |                   |               |          |          |                        |        |                          |                     |                        |         |
| Image: state of the state o  |                   |               |          |          |                        |        |                          |                     |                        |         |
| Image: state   |                   |               |          |          |                        |        |                          |                     |                        |         |
|  | <u> </u>          |               | ļ        |          |                        |        |                          | ļ                   |                        |         |
|  |                   |               |          |          |                        |        |                          |                     |                        |         |
|  |                   |               |          |          |                        |        |                          |                     |                        |         |
|  |                   |               |          |          |                        |        |                          |                     |                        |         |

Table B.4. Summary of Unbiased Lot Std Dev for AC for Each Project (continued)

| Project | JMF  | Lot Size | Lot Mean | Lot St Dev | C4     | Lot St Dev | Average  | Avg Lot SD | Course  |
|---------|------|----------|----------|------------|--------|------------|----------|------------|---------|
|         |      | 2        | 0.205    |            | 0 7070 |            | Lot wean | Unbiased   | Interm  |
|         | J02  | 2        | -0.205   | 0.140      | 0.7979 | 0.100      |          |            | Interm  |
| P01     | J02  | <u> </u> | -0.300   | 0.999      | 0.0002 | 0.115      |          |            | Interm  |
| P01     | J02  |          | -0.505   | 0.092      | 0.7979 | 0.115      | 0.075    | 0.470      | Interm  |
| P01     | J02  | 1        | -0.090   | -          | -      | -          | -0.275   | 0.476      | Interm  |
| PUI     | J07  | 3        | 0.337    | 0.546      | 0.8862 | 0.617      |          |            | Surface |
| P01     | J07  | 3        | 0.290    | 0.620      | 0.8862 | 0.700      |          |            | Surface |
| P01     | J07  | 5        | 0.538    | 0.307      | 0.94   | 0.327      |          |            | Surface |
| P01     | J07  | 3        | 0.577    | 0.067      | 0.8862 | 0.075      |          |            | Surface |
| PUI     | J07  | 3        | -0.180   | 0.265      | 0.8862 | 0.299      |          |            | Surface |
| P01     | J07  | 1        | 0.890    | -          | -      | -          |          |            | Surface |
| P01     | J07  | 3        | -0.470   | 0.214      | 0.8862 | 0.241      |          |            | Surface |
| P01     | J07  | C d      | 0.032    | 0.188      | 0.94   | 0.200      | 0.000    | 0.000      | Surface |
| PUI     | J07  | 4        | 0.378    | 0.678      | 0.9213 | 0.736      | 0.332    | 0.399      | Surface |
| P01     | J10  | 3        | -0.950   | 0.130      | 0.8862 | 0.147      |          |            | Interm  |
| P01     | J10  | 1        | -1.110   | _          | _      |            |          |            | Interm  |
| P01     | J10  | 1        | -1.120   | -          | -      | -          |          |            | Interm  |
| P01     | J10  | 4        | -0.288   | 0.698      | 0.9213 | 0.758      |          |            | Interm  |
| P01     | J10  | 3        | -0.530   | 0.303      | 0.8862 | 0.342      |          |            | Interm  |
| P01     | J10  | 1        | -0.440   | -          | -      | -          |          |            | Intern  |
| P01     | J10  | 3        | -0.155   | 0.392      | 0.0002 | 0.442      |          |            | Interm  |
| P01     | J10  | 1        | -0.630   | _          | _      |            |          |            | Interm  |
|         | 110  | 1        | -0.130   |            |        |            |          |            | Interm  |
| P01     | 110  | 2        | -0.200   |            | -      | -          |          |            | Interm  |
| P01     | 110  | 2        | -0.400   | 0.000      | 0.7979 | 0.401      |          |            | Interm  |
| P01     | 110  | <u> </u> | -0.343   | 0.021      | 0.7373 | 0.027      |          |            | Interm  |
| P01     | .110 | 2        | -0.400   | 0.443      | 0.3213 | 0.401      |          |            | Interm  |
| P01     | .110 | 2        | -0.280   | 0.141      | 0.7979 | 0.266      |          |            | Interm  |
| P01     | .110 | 3        | 0.200    | 0.162      | 0.8862 | 0.200      |          |            | Interm  |
| P01     | .110 | 2        | 0.405    | 0.035      | 0 7979 | 0.044      |          |            | Interm  |
| P01     | .110 | 3        | -0.083   | 0.480      | 0.8862 | 0.542      | -0 407   | 0.322      | Interm  |
| P01     | J19  | 1        | -0.670   | _          | -      | -          | 0.107    | 0.022      | Surface |
| P01     | J19  | 1        | 0.250    | _          | _      | _          |          |            | Surface |
| P01     | J19  | 2        | -0.590   | 0.467      | 0.7979 | 0.585      |          |            | Surface |
| P01     | J19  | 2        | -0.420   | 0.495      | 0.7979 | 0.620      |          |            | Surface |
| P01     | J19  | 1        | -1.030   | _          | _      | _          |          |            | Surface |
| P01     | J19  | 1        | -0.290   | _          | _      | _          |          |            | Surface |
| P01     | J19  | 1        | 0.760    | _          | _      | _          |          |            | Surface |
| P01     | J19  | 1        | 0.590    | _          | _      | _          |          |            | Surface |
| P01     | J19  | 2        | -0.145   | 0.474      | 0.7979 | 0.594      |          |            | Surface |
| P01     | J19  | 1        | -0.950   | _          | _      | _          |          |            | Surface |
| P01     | J19  | 1        | -0.050   | _          | _      | _          |          |            | Surface |
| P01     | J19  | 2        | -0.880   | 0.240      | 0.7979 | 0.301      |          |            | Surface |
| P01     | J19  | 1        | -1.070   | -          | -      | -          |          |            | Surface |
| P01     | J19  | 1        | -1.000   | _          | -      | -          | -0.393   | 0.525      | Surface |
| P01     | J23  | 4        | -0.530   | 0.283      | 0.9213 | 0.307      |          |            | Interm  |
| P01     | J23  | 3        | -0.050   | 0.358      | 0.8862 | 0.404      |          |            | Interm  |

Table B.5. Summary of Unbiased Lot Std Dev for AV for Each Project

| Project<br>Number | JMF<br>Number | Lot Size | Lot Mean | Lot St Dev<br>(biased) | <i>c</i> <sub>4</sub> | Lot St Dev<br>(unbiased) | Average<br>Lot Mean | Avg Lot SD<br>Unbiased | Course  |
|-------------------|---------------|----------|----------|------------------------|-----------------------|--------------------------|---------------------|------------------------|---------|
| P01               | J23           | 1        | 0.190    | –                      | _                     | -                        |                     |                        | Interm  |
| P01               | J23           | 2        | -0.405   | 0.276                  | 0.7979                | 0.346                    |                     |                        | Interm  |
| P01               | J23           | 1        | -0.550   | _                      | _                     | _                        |                     |                        | Interm  |
| P01               | J23           | 1        | -0.500   | _                      | _                     | _                        | -0.308              | 0.352                  | Interm  |
| P02               | J04           | 4        | -0.035   | 0.215                  | 0.9213                | 0.233                    |                     |                        | Interm  |
| P02               | J04           | 1        | 0.200    | _                      | _                     | _                        |                     |                        | Interm  |
| P02               | J04           | 2        | -0.460   | 0.028                  | 0.7979                | 0.035                    |                     |                        | Interm  |
| P02               | J04           | 2        | -0.420   | 0.141                  | 0.7979                | 0.177                    |                     |                        | Interm  |
| P02               | J04           | 4        | -0.688   | 0.103                  | 0.9213                | 0.112                    |                     |                        | Interm  |
| P02               | J04           | 1        | -1.020   | _                      | _                     | _                        |                     |                        | Interm  |
| P02               | J04           | 4        | -0.703   | 0.239                  | 0.9213                | 0.260                    |                     |                        | Interm  |
| P02               | J04           | 1        | 0.050    | _                      | _                     | _                        |                     |                        | Interm  |
| P02               | J04           | 1        | 0.060    | _                      | _                     | _                        |                     |                        | Interm  |
| P02               | J04           | 2        | 0.055    | 0.290                  | 0.7979                | 0.363                    |                     |                        | Interm  |
| P02               | J04           | 3        | -0.213   | 0.568                  | 0.8862                | 0.640                    |                     |                        | Interm  |
| P02               | J04           | 1        | 0.260    | _                      | _                     | _                        |                     |                        | Interm  |
| P02               | J04           | 1        | 0.830    | _                      | _                     | _                        |                     |                        | Interm  |
| P02               | J04           | 3        | 0.910    | 0.297                  | 0.8862                | 0.335                    | -0.084              | 0.270                  | Interm  |
| P02               | J05           | 2        | 0.495    | 0.247                  | 0.7979                | 0.310                    | 0.001               | 0.2.0                  | Surface |
| P02               | .105          | 1        | 0.630    | -                      | _                     | _                        |                     |                        | Surface |
| P02               | .105          | 2        | -0.210   | 0.382                  | 0 7979                | 0 479                    |                     |                        | Surface |
| P02               | .105          | 1        | 0.450    | -                      |                       | -                        |                     |                        | Surface |
| P02               | .105          | 1        | 0.870    | _                      | _                     | _                        |                     |                        | Surface |
| P02               | .105          | 1        | 0.130    | _                      | _                     | _                        | 0.394               | 0.394                  | Surface |
| P02               | .109          | 1        | -0.200   | _                      | _                     | _                        | 0.004               | 0.00-                  | Interm  |
| P02               | .109          | 2        | 0.200    | 0 417                  | 0 7979                | 0.523                    |                     |                        | Interm  |
| P02               | .109          | 1        | -0.840   | -                      |                       | -                        |                     |                        | Interm  |
| P02               | .109          | 3        | -0.473   | 0.580                  | 0 8862                | 0.654                    |                     |                        | Interm  |
| P02               | .109          | 2        | -0.115   | 0.332                  | 0.0002                | 0.001                    |                     |                        | Interm  |
| P02               | .109          | 2        | 0.185    | 0.502                  | 0 7979                | 0.629                    |                     |                        | Interm  |
| P02               | .109          | 1        | -0.390   | -                      | _                     | -                        |                     |                        | Interm  |
| P02               | .109          | 1        | 0.000    | _                      | _                     | _                        |                     |                        | Interm  |
| P02               | .109          | 2        | -0.810   | 0.000                  | 0 7979                | 0.000                    |                     |                        | Interm  |
| P02               | .109          | 3        | -0.333   | 0.000                  | 0.8862                | 0.554                    |                     |                        | Interm  |
| P02               | .109          | 2        | -0.015   | 0.417                  | 0.0002                | 0.523                    |                     |                        | Interm  |
| P02               | 109           | 2        | -0.010   | 0.467                  | 0.7070                | 0.585                    |                     |                        | Interm  |
| P02               | .109          | 1        | 0.010    | -                      |                       | -                        |                     |                        | Interm  |
| P02               | 109           | 4        | -0.093   | 0.462                  | 0 9213                | 0.501                    |                     |                        | Interm  |
| P02               | 100           | 2        | -0.205   | 0.402                  | 0.3213                | 0.501                    |                     |                        | Interm  |
| P02               | 100           | 1        | 0.230    |                        | 0.1313                | 0.541                    |                     |                        | Interm  |
| P02               | 100           | 2        | -0.010   | 0 000                  | 0 7070                | 0 1 2 /                  |                     |                        | Interm  |
| P02               | 100           | 2        | 0.010    | 0.099                  | 0.7979                | 0.124                    | -0 082              | 0 //1                  | Interm  |
| P02               | 112           | <u> </u> | 0.320    | 0.190                  | 0.1919                | 0.240                    | -0.002              | 0.441                  | Surface |
| P02               | 112           | 1        | -0.030   |                        |                       |                          |                     |                        | Surface |
| P02               | 112           | 2        | 0.000    | 0 163                  | 0 7070                | 0.204                    |                     |                        | Surface |
| D02               | 112           | <u> </u> | 0.090    | 0.103                  | 0.1919                | 0.204                    |                     |                        | Surface |
| P02               | 112           | 1        | 0.000    |                        | _                     |                          |                     |                        | Surface |
| FU2               | 515           | I        | 0.900    | —                      | _                     | -                        |                     |                        | Sunace  |

| Table B.5. Summary of Unbiased Lot Std Dev for AV for Each Project (continue | ed) |
|--|-----|
|--|-----|

| Project | JMF  | Lot Size | Lot Mean | Lot St Dev | <i>c</i> <sub>4</sub> | Lot St Dev | Average  | Avg Lot SD | Course  |
|---------|------|----------|----------|------------|-----------------------|------------|----------|------------|---------|
| P02     |      | 1        | -0.430   | (biaseu)   | _                     |            | LOUIWEan | Unbiaseu   | Surface |
| P02     | 113  | 2        | 0.755    | 0.318      | 0 7070                | 0 300      |          |            | Surface |
| P02     | 113  | 1        | 0.750    | 0.510      | 0.1313                | 0.555      |          |            | Surface |
| P02     | 113  | 1        | -0.110   |            |                       |            |          |            | Surface |
| P02     | 113  | 1        | 0.670    |            |                       |            |          |            | Surface |
| P02     | 113  | 1        | 0.070    |            | _                     |            |          |            | Surface |
| P02     | .113 | 2        | 0.000    | 0.057      | 0 7979                | 0.071      |          |            | Surface |
| P02     | .113 | 2        | 0.870    | 0.382      | 0.7979                | 0.071      |          |            | Surface |
| P02     | .113 | 1        | -0.870   |            |                       | -          | 0.372    | 0.288      | Surface |
| P02     | J15  | 1        | 0.420    | _          | _                     | _          | 0.012    | 0.200      | Surface |
| P02     | J15  | 4        | 0.688    | 0 266      | 0 9213                | 0.288      |          |            | Surface |
| P02     | .115 | 4        | 0.783    | 0.359      | 0.9213                | 0.390      |          |            | Surface |
| P02     | J15  | 5        | 0.772    | 0.142      | 0.94                  | 0.151      |          |            | Surface |
| P02     | J15  | 3        | 0.163    | 0.663      | 0.8862                | 0.748      |          |            | Surface |
| P02     | J15  | 1        | -1.070   | _          | _                     | _          | 0.293    | 0.394      | Surface |
| P04     | J08  | 2        | -0.020   | 0.255      | 0.7979                | 0.319      | 0.200    | 0.001      | Interm  |
| P04     | J08  | 2        | -0.110   | 0.764      | 0.7979                | 0.957      |          |            | Interm  |
| P04     | J08  | 2        | 0.210    | 0.141      | 0.7979                | 0.177      |          |            | Interm  |
| P04     | J08  | 2        | 0.105    | 0.346      | 0.7979                | 0.434      |          |            | Interm  |
| P04     | J08  | 2        | 0.480    | 0.735      | 0.7979                | 0.922      | 0.133    | 0.562      | Interm  |
| P04     | J14  | 3        | 0.620    | 0.036      | 0.8862                | 0.041      | 0.100    | 0.001      | Surface |
| P04     | J14  | 4        | -0.138   | 0.551      | 0.9213                | 0.598      |          |            | Surface |
| P04     | J14  | 4        | 0.638    | 0.121      | 0.9213                | 0.131      |          |            | Surface |
| P04     | J14  | 3        | 0.333    | 0.561      | 0.8862                | 0.633      |          |            | Surface |
| P04     | J14  | 3        | -0.237   | 0.393      | 0.8862                | 0.443      | 0.243    | 0.369      | Surface |
| P05     | J25  | 1        | -0.680   | _          | _                     | _          |          |            | Surface |
| P05     | J25  | 1        | 0.050    | _          | _                     | _          |          |            | Surface |
| P05     | J25  | 1        | -0.070   | _          | _                     | _          |          |            | Surface |
| P05     | J25  | 1        | -0.850   | _          | _                     | _          |          |            | Surface |
| P05     | J25  | 1        | 0.100    | _          | _                     | _          |          |            | Surface |
| P05     | J25  | 1        | 0.580    | -          | _                     | _          |          |            | Surface |
| P05     | J25  | 1        | 0.460    | -          | _                     | _          |          |            | Surface |
| P05     | J25  | 1        | 0.500    | -          | _                     | _          | 0.011    | #DIV/0!    | Surface |
| P05     | J27  | 2        | 0.190    | 0.184      | 0.7979                | 0.230      |          |            | Interm  |
| P05     | J27  | 2        | 0.310    | 0.396      | 0.7979                | 0.496      |          |            | Interm  |
| P05     | J27  | 2        | 0.380    | 0.141      | 0.7979                | 0.177      |          |            | Interm  |
| P05     | J27  | 2        | 0.490    | 0.042      | 0.7979                | 0.053      |          |            | Interm  |
| P05     | J27  | 2        | -0.485   | 0.375      | 0.7979                | 0.470      |          |            | Interm  |
| P05     | J27  | 2        | 0.140    | 0.113      | 0.7979                | 0.142      |          |            | Interm  |
| P05     | J27  | 1        | 0.120    | _          | _                     | -          |          |            | Interm  |
| P05     | J27  | 2        | 0.660    | 0.325      | 0.7979                | 0.408      | 0.226    | 0.282      | Interm  |
| P06     | J24  | 3        | -0.257   | 0.302      | 0.8862                | 0.340      |          |            | Surface |
| P06     | J24  | 3        | -0.493   | 0.378      | 0.8862                | 0.427      |          |            | Surface |
| P06     | J24  | 3        | -0.493   | 0.297      | 0.8862                | 0.335      |          |            | Surface |
| P06     | J24  | 3        | -0.123   | 0.785      | 0.8862                | 0.886      |          |            | Surface |
| P06     | J24  | 3        | -0.587   | 0.282      | 0.8862                | 0.318      | -0.391   | 0.461      | Surface |
| P07     | J30  | 3        | 0.473    | 0.167      | 0.8862                | 0.189      |          |            | Surface |

# Table B.5. Summary of Unbiased Lot Std Dev for AV for Each Project (continued)

| Project | JMF | Lot Size | Lot Mean | Lot St Dev | $c_4$  | Lot St Dev | Average  | Avg Lot SD | Course  |
|---------|-----|----------|----------|------------|--------|------------|----------|------------|---------|
|         |     | 1        | 0.280    | (biaseu)   |        | (unbiaseu) | LULIWEAN | Unbiaseu   | Surface |
| P07     | 130 | 1        | 0.200    | _          |        | _          |          |            | Surface |
| P07     | 130 | 1        | 0.240    | _          | -      | _          |          |            | Surface |
| P07     | 130 | 1        | 0.700    | -          | 0.0212 | - 0.470    |          |            | Surface |
|         | 120 | 4        | -0.120   | 0.441      | 0.9213 | 0.479      |          |            | Surface |
| P07     | 130 | 2        | 0.230    | 0.220      | 0.7979 | 0.204      |          |            | Surface |
|         | 120 | 2<br>1   | -0.000   | 0.000      | 0.7979 | 0.727      |          |            | Surface |
|         | 120 | 2        | 0.230    | -          | 0.0060 | -          |          |            | Surface |
| P07     | 130 | <u> </u> | 0.030    | 0.435      | 0.0002 | 0.491      |          |            | Surface |
| P07     | 130 | <u> </u> | -0.433   | 0.414      | 0.0002 | 0.467      |          |            | Surface |
| P07     | 130 | <u> </u> | 0.310    | 0.270      | 0.0002 | 0.312      |          |            | Surface |
| P07     | J30 | 3        | 0.160    | 0.733      | 0.0002 | 0.627      |          |            | Sunace  |
| P07     | J30 | 2        | -0.595   | 0.301      | 0.7979 | 0.452      |          |            | Surface |
| P07     | J30 | 3        | -0.097   | 0.001      | 0.8862 | 0.745      |          |            | Surface |
| P07     | J30 | 3        | -0.153   | 0.081      | 0.8862 | 0.092      |          |            | Surface |
| P07     | J30 | 1        | 0.360    | -          | -      | -          |          |            | Surface |
| P07     | J30 | 2        | -0.155   | 0.884      | 0.7979 | 1.108      |          |            | Surface |
| P07     | J30 | 1        | 0.790    | _          | _      | _          | 0.000    | 0.54.4     | Surface |
| P07     | J30 | 1        | 0.000    | -          | -      | -          | 0.088    | 0.514      | Surface |
| P09     | J35 | 3        | 0.727    | 0.272      | 0.8862 | 0.307      |          |            | Surface |
| P09     | J35 | 3        | -0.193   | 0.193      | 0.8862 | 0.218      | 0.000    | 0.040      | Surface |
| P09     | J35 | 3        | 0.347    | 0.459      | 0.8862 | 0.518      | 0.293    | 0.348      | Surface |
| P09     | J83 | 3        | 0.207    | 0.326      | 0.8862 | 0.368      |          |            | Surface |
| P09     | J83 | 3        | -0.507   | 0.586      | 0.8862 | 0.661      |          |            | Surface |
| P09     | J83 | 2        | -0.790   | 0.354      | 0.7979 | 0.443      | -0.363   | 0.491      | Surface |
| P10     | J12 | 1        | -0.370   | -          | -      | _          |          |            | Surface |
| P10     | J12 | 1        | 0.550    | _          | -      | _          |          |            | Surface |
| P10     | J12 | 1        | 0.290    | -          | _      | _          |          |            | Surface |
| P10     | J12 | 2        | 0.705    | 0.247      | 0.7979 | 0.310      |          |            | Surface |
| P10     | J12 | 1        | 0.960    | -          | -      | -          |          |            | Surface |
| P10     | J12 | 1        | 1.040    | -          | -      | -          |          |            | Surface |
| P10     | J12 | 1        | 0.010    | -          | -      | -          |          |            | Surface |
| P10     | J12 | 1        | -0.140   | -          | -      | —          |          |            | Surface |
| P10     | J12 | 2        | 1.310    | 1.556      | 0.7979 | 1.950      |          |            | Surface |
| P10     | J12 | 2        | 0.115    | 0.148      | 0.7979 | 0.186      |          |            | Surface |
| P10     | J12 | 2        | 0.435    | 0.035      | 0.7979 | 0.044      |          |            | Surface |
| P10     | J12 | 2        | 0.235    | 0.247      | 0.7979 | 0.310      |          |            | Surface |
| P10     | J12 | 2        | -0.025   | 0.460      | 0.7979 | 0.576      | 0.393    | 0.563      | Surface |
| P10     | J31 | 2        | -0.740   | 0.085      | 0.7979 | 0.106      |          |            | Interm  |
| P10     | J31 | 2        | 0.145    | 0.502      | 0.7979 | 0.629      |          |            | Interm  |
| P10     | J31 | 2        | 0.415    | 0.106      | 0.7979 | 0.133      |          |            | Interm  |
| P10     | J31 | 2        | 0.600    | 0.212      | 0.7979 | 0.266      |          |            | Interm  |
| P10     | J31 | 1        | 1.020    | -          | -      | -          |          |            | Interm  |
| P10     | J31 | 2        | 0.690    | 0.071      | 0.7979 | 0.089      |          |            | Interm  |
| P10     | J31 | 2        | 0.025    | 0.361      | 0.7979 | 0.452      |          |            | Interm  |
| P10     | J31 | 1        | -0.070   | —          | _      | -          |          |            | Interm  |
| P10     | J31 | 2        | 0.120    | 0.933      | 0.7979 | 1.170      |          |            | Interm  |
| P10     | J31 | 2        | 0.960    | 0.028      | 0.7979 | 0.035      |          |            | Interm  |

Table B.5. Summary of Unbiased Lot Std Dev for AV for Each Project (continued)

| Project<br>Number | JMF<br>Number | Lot Size | Lot Mean | Lot St Dev<br>(biased) | <i>c</i> <sub>4</sub> | Lot St Dev | Average  | Avg Lot SD | Course |
|-------------------|---------------|----------|----------|------------------------|-----------------------|------------|----------|------------|--------|
| P10               |               | 2        | 0 825    | 0 177                  | 0 7979                | 0 222      | Lot mean | onblased   | Interm |
| P10               | .131          | 2        | 0.020    | 0.460                  | 0 7979                | 0.576      |          |            | Interm |
| P10               | J31           | 2        | 0.395    | 0.021                  | 0 7979                | 0.027      |          |            | Interm |
| P10               | .131          | 2        | 0.360    | 0.021                  | 0 7979                | 0.195      |          |            | Interm |
| P10               | J31           | 2        | 0 795    | 0.460                  | 0 7979                | 0.576      |          |            | Interm |
| P10               | J31           | 2        | 0.890    | 0.042                  | 0.7979                | 0.053      |          |            | Interm |
| P10               | J31           | 2        | -0.020   | 0.071                  | 0.7979                | 0.089      |          |            | Interm |
| P10               | J31           | 2        | 0.220    | 0.071                  | 0.7979                | 0.089      |          |            | Interm |
| P10               | J31           | 2        | 0.285    | 0.502                  | 0.7979                | 0.629      |          |            | Interm |
| P10               | J31           | 2        | 0.715    | 0.262                  | 0.7979                | 0.328      |          |            | Interm |
| P10               | J31           | 2        | -0.110   | 0.127                  | 0.7979                | 0.160      |          |            | Interm |
| P10               | J31           | 1        | -0.140   | _                      | _                     | _          |          |            | Interm |
| P10               | J31           | 2        | 0.075    | 0.445                  | 0.7979                | 0.558      |          |            | Interm |
| P10               | J31           | 2        | -0.715   | 0.502                  | 0.7979                | 0.629      |          |            | Interm |
| P10               | J31           | 2        | -0.385   | 0.332                  | 0.7979                | 0.417      |          |            | Interm |
| P10               | J31           | 2        | 0.035    | 0.587                  | 0.7979                | 0.736      |          |            | Interm |
| P10               | J31           | 1        | -0.640   | _                      | _                     | _          |          |            | Interm |
| P10               | J31           | 2        | -0.445   | 0.841                  | 0.7979                | 1.055      |          |            | Interm |
| P10               | J31           | 2        | -0.640   | 0.014                  | 0.7979                | 0.018      |          |            | Interm |
| P10               | J31           | 2        | 0.215    | 0.389                  | 0.7979                | 0.487      |          |            | Interm |
| P10               | J31           | 2        | 0.570    | 0.735                  | 0.7979                | 0.922      |          |            | Interm |
| P10               | J31           | 2        | 0.490    | 0.764                  | 0.7979                | 0.957      |          |            | Interm |
| P10               | J31           | 2        | 0.160    | 0.721                  | 0.7979                | 0.904      |          |            | Interm |
| P10               | J31           | 2        | 0.080    | 0.424                  | 0.7979                | 0.532      |          |            | Interm |
| P10               | J31           | 2        | 0.410    | 0.127                  | 0.7979                | 0.160      |          |            | Interm |
| P10               | J31           | 2        | -0.515   | 0.219                  | 0.7979                | 0.275      |          |            | Interm |
| P10               | J31           | 2        | 0.010    | 0.382                  | 0.7979                | 0.479      |          |            | Interm |
| P10               | J31           | 2        | -0.455   | 0.502                  | 0.7979                | 0.629      |          |            | Interm |
| P10               | J31           | 2        | -0.255   | 0.955                  | 0.7979                | 1.196      |          |            | Interm |
| P10               | J31           | 2        | -0.180   | 0.085                  | 0.7979                | 0.106      |          |            | Interm |
| P10               | J31           | 1        | 0.320    | -                      | _                     | _          | 0.152    | 0.441      | Interm |
| P10               | J37           | 1        | 0.850    | -                      | —                     | -          |          |            | Interm |
| P10               | J37           | 2        | 0.015    | 0.177                  | 0.7979                | 0.222      |          |            | Interm |
| P10               | J37           | 2        | -0.270   | 0.382                  | 0.7979                | 0.479      |          |            | Interm |
| P10               | J37           | 2        | 0.620    | 0.000                  | 0.7979                | 0.000      |          |            | Interm |
| P10               | J37           | 2        | 0.605    | 0.276                  | 0.7979                | 0.346      |          |            | Interm |
| P10               | J37           | 1        | 0.320    | _                      | -                     | -          |          |            | Interm |
| P10               | J37           | 2        | 0.625    | 0.290                  | 0.7979                | 0.363      |          |            | Interm |
| P10               | J37           | 2        | 0.365    | 0.262                  | 0.7979                | 0.328      |          |            | Interm |
| P10               | J37           | 2        | 0.790    | 0.085                  | 0.7979                | 0.106      |          |            | Interm |
| P10               | J37           | 2        | 0.855    | 0.092                  | 0.7979                | 0.115      |          |            | Interm |
| P10               | J37           | 2        | 0.775    | 0.134                  | 0.7979                | 0.168      |          |            | Interm |
| P10               | J37           | 2        | 0.895    | 0.064                  | 0.7979                | 0.080      | 0.537    | 0.221      | Interm |
| P10               | J82           | 2        | 0.260    | 0.170                  | 0.7979                | 0.213      |          |            | Interm |
| P10               | J82           | 2        | 0.745    | 0.431                  | 0.7979                | 0.541      |          |            | Interm |
| P10               | J82           | 2        | 0.870    | 0.113                  | 0.7979                | 0.142      |          |            | Interm |
| P10               | J82           | 2        | 1.110    | 0.085                  | 0.7979                | 0.106      |          |            | Interm |

Table B.5. Summary of Unbiased Lot Std Dev for AV for Each Project (continued)

| Project | JMF        | Lot Size | Lot Mean | Lot St Dev | $c_4$  | Lot St Dev | Average | Avg Lot SD | Course  |
|---------|------------|----------|----------|------------|--------|------------|---------|------------|---------|
|         |            | 2        | 0 755    |            | 0 7070 |            | LOUWEAN | Unbiaseu   | Intorm  |
|         | 102        | 2<br>1   | 0.755    | 0.235      | 0.7979 | 0.292      |         |            | Interm  |
| P10     | 102        | 2        | 0.020    | -          | 0 7070 | -          |         |            | Interm  |
| P10     | 102        | 2        | 0.775    | 0.004      | 0.7979 | 0.080      | 0 797   | 0.222      | Interm  |
|         | J02        | 2        | 0.900    | 0.141      | 0.7979 | 0.177      | 0.707   | 0.222      | Surface |
|         | J41<br>1/1 | 3<br>1   | 0.573    | 0.300      | 0.0002 | 0.435      |         |            | Surface |
|         | J41        | 2        | 0.190    | -          | 0 7070 | -          |         |            | Surface |
|         | J41        | <u>∠</u> | -0.320   | 0.323      | 0.7979 | 0.400      | 0.000   | 0.202      | Surface |
|         | 120        | 4        | -0.000   | 0.002      | 0.9213 | 0.000      | 0.090   | 0.303      | Surface |
| P12     | 130        | 4        | -0.003   | 0.524      | 0.9213 | 0.331      |         |            | Surface |
|         | 130        | 2<br>1   | -1.000   | 0.594      | 0.7979 | 0.744      |         |            | Surface |
|         | 130        | 1        | -1.420   | _          | -      | _          |         |            | Surface |
| P12     | 138        | 3        | -0.300   | -          | 0.8862 | -          |         |            | Surface |
| P12     | 138        | 3        | -0.217   | 0.232      | 0.0002 | 0.202      | -0 700  | 0.577      | Surface |
| P13     | 103        | 3        | -0.000   | 0.043      | 0.0002 | 0.335      | -0.730  | 0.377      | Surface |
| P13     | 103        | 3        | 0.000    | 0.237      | 0.0002 | 1.015      |         |            | Surface |
| P13     | 103        | 1        | 0.720    | 0.033      | 0.0002 | 1.013      |         |            | Surface |
| P13     | 103        | 3        | -0.593   | 0.431      | 0.8862 | 0.486      |         |            | Surface |
| P13     | .103       | 1        | -0.180   | -          | -      | -          |         |            | Surface |
| P13     | 103        | 1        | -0.560   | _          | _      | _          |         |            | Surface |
| P13     | 103        | 3        | -0.133   | 0 422      | 0.8862 | 0.476      |         |            | Surface |
| P13     | .103       | 1        | 1 1 3 0  | -          | -      | -          | -0 049  | 0.578      | Surface |
| P13     | .143       | 2        | -0.585   | 0.318      | 0 7979 | 0 399      | 0.040   | 0.070      | Surface |
| P13     | J43        | 2        | -0.370   | 1 061      | 0 7979 | 1 329      |         |            | Surface |
| P13     | J43        | 2        | -0.645   | 0.021      | 0.7979 | 0.027      |         |            | Surface |
| P13     | .143       | 2        | 0.615    | 0.643      | 0 7979 | 0.806      |         |            | Surface |
| P13     | J43        | 3        | -0.190   | 0.963      | 0.8862 | 1.087      |         |            | Surface |
| P13     | J43        | 4        | 0.080    | 0.799      | 0.9213 | 0.867      |         |            | Surface |
| P13     | J43        | 3        | 0.597    | 0.615      | 0.8862 | 0.693      |         |            | Surface |
| P13     | J43        | 1        | 1.710    | _          | _      | _          | 0.151   | 0.744      | Surface |
| P14     | J16        | 1        | 0.500    | _          | _      | _          |         |            | Surface |
| P14     | J16        | 2        | -0.135   | 0.148      | 0.7979 | 0.186      |         |            | Surface |
| P14     | J16        | 3        | -0.823   | 0.112      | 0.8862 | 0.126      |         |            | Surface |
| P14     | J16        | 2        | 0.220    | 0.099      | 0.7979 | 0.124      |         |            | Surface |
| P14     | J16        | 1        | -0.300   | _          | _      | _          |         |            | Surface |
| P14     | J16        | 4        | -0.515   | 0.812      | 0.9213 | 0.881      |         |            | Surface |
| P14     | J16        | 3        | -0.813   | 0.172      | 0.8862 | 0.194      |         |            | Surface |
| P14     | J16        | 4        | -0.430   | 1.246      | 0.9213 | 1.353      |         |            | Surface |
| P14     | J16        | 4        | -0.470   | 1.431      | 0.9213 | 1.554      |         |            | Surface |
| P14     | J16        | 2        | -0.155   | 0.431      | 0.7979 | 0.541      |         |            | Surface |
| P14     | J16        | 1        | -0.800   | -          | _      | -          |         |            | Surface |
| P14     | J16        | 2        | -0.875   | 0.050      | 0.7979 | 0.062      |         |            | Surface |
| P14     | J16        | 3        | -0.410   | 0.131      | 0.8862 | 0.148      | -0.385  | 0.517      | Surface |
| P16     | J20        | 3        | 0.380    | 0.613      | 0.8862 | 0.692      |         |            | Surface |
| P16     | J20        | 3        | 0.460    | 1.070      | 0.8862 | 1.208      |         |            | Surface |
| P16     | J20        | 3        | -0.347   | 0.441      | 0.8862 | 0.498      | 0.164   | 0.799      | Surface |
| P17     | J22        | 2        | -0.870   | 0.014      | 0.7979 | 0.018      |         |            | Interm  |

Table B.5. Summary of Unbiased Lot Std Dev for AV for Each Project (continued)

| Project     | JMF    | Lot Size | Lot Mean | Lot St Dev | <i>C</i> <sub>4</sub> | Lot St Dev | Average  | Avg Lot SD | Course  |
|-------------|--------|----------|----------|------------|-----------------------|------------|----------|------------|---------|
|             | Number | 2        | 0.765    |            | 0 7070                |            | Lot Mean | Unblased   | Intorm  |
|             | 122    | 2        | -0.705   | 0.304      | 0.7979                | 0.301      |          |            | Interm  |
| P17         | J22    | 1        | -0.360   | 0.735      | 0.7979                | 0.922      |          |            | Interm  |
|             | 122    | 2        | 0.010    | -          | -                     | -          |          |            | Interm  |
| P17         | J22    | 2        | -0.340   | 0.707      | 0.7979                | 0.000      | 0.200    | 0.670      | Interm  |
|             | J22    |          | 0.020    | 0.919      | 0.7979                | 1.152      | -0.300   | 0.072      | Surface |
| P10         | J40    | 1        | -1.500   | -          | -                     | -          |          |            | Surface |
| P18         | J48    | 3        | -0.913   | 0.376      | 0.8862                | 0.424      |          |            | Surface |
| P18         | J48    | 1        | -1.070   | -          | -                     | -          |          |            | Surface |
| P18<br>D10  | J48    | 2        | -0.425   | 0.247      | 0.7979                | 0.310      |          |            | Surface |
|             | J40    | 3        | -0.123   | 0.090      | 0.0002                | 0.102      |          |            | Surface |
| P18         | J48    | 1        | -0.450   | _          |                       |            | 0.400    | 0.070      | Surface |
| P10         | J40    | 1        | 1.000    | -          | -                     | -          | -0.400   | 0.279      | Surface |
| P 19<br>D10 | J49    |          | 0.170    | 0.263      | 0.7979                | 0.354      |          |            | Surface |
| P 19<br>D10 | J49    | 1        | 0.040    | -          | -                     | -          |          |            | Surface |
| P 19        | J49    | 3        | -0.650   | 0.202      | 0.0002                | 0.316      |          |            | Surface |
| P 19        | J49    | 4        | -0.708   | 0.314      | 0.9213                | 0.341      |          |            | Surface |
| P 19<br>D10 | J49    | 4        | -0.495   | 0.051      | 0.9213                | 0.707      |          |            | Surface |
| P 19<br>D10 | J49    | <u> </u> | -0.740   | 0.959      | 0.0002                | 1.062      | 0.420    | 0.576      | Surface |
| P 19        | J49    | 3        | -0.360   | 0.579      | 0.0002                | 0.655      | -0.420   | 0.576      | Surface |
| P20         | 150    | 5        | -1.340   | -          | -                     | -          |          |            | Surface |
| P20         | 150    | 2        | -0.300   | 0.307      | 0.94                  | 0.327      |          |            | Surface |
| P20         | 150    | <u> </u> | -0.345   | 0.029      | 0.7979                | 0.789      |          |            | Surface |
| P20         | 150    | 4        | 0.313    | 0.192      | 0.9213                | 0.200      |          |            | Surface |
| P20         | 150    | 2        | 0.210    | 0.057      | 0 7070                | 0.071      |          |            | Surface |
| P20         | 150    | 5        | -0.200   | 0.007      | 0.7373                | 0.071      |          |            | Surface |
| P20         | .150   | 3        | -0.367   | 0.272      | 0.8862                | 0.203      |          |            | Surface |
| P20         | 150    | 1        | -0.770   | 0.201      | 0.0002                | 0.017      |          |            | Surface |
| P20         | .150   | 1        | -0.100   | _          | _                     | _          |          |            | Surface |
| P20         | .150   | 5        | -0.356   | 0.578      | 0 94                  | 0.615      |          |            | Surface |
| P20         | J50    | 1        | -0 750   | -          | -                     | -          |          |            | Surface |
| P20         | .150   | 2        | -0.335   | 0.969      | 0 7979                | 1 214      |          |            | Surface |
| P20         | J50    | 4        | -0 430   | 0.468      | 0.9213                | 0.508      |          |            | Surface |
| P20         | J50    | 5        | 0.210    | 0.732      | 0.94                  | 0.778      |          |            | Surface |
| P20         | J50    | 2        | -0.885   | 0.177      | 0.7979                | 0.222      |          |            | Surface |
| P20         | J50    | 2        | 0.065    | 0.064      | 0.7979                | 0.080      | -0.334   | 0.452      | Surface |
| P21         | J34    | 4        | -0.210   | 0.421      | 0.9213                | 0.456      | 0.001    | 0.10       | Interm  |
| P21         | J34    | 3        | 0.150    | 0.212      | 0.8862                | 0.239      |          |            | Interm  |
| P21         | J34    | 1        | 0.310    | _          | _                     | _          | 0.083    | 0.348      | Interm  |
| P21         | J39    | 1        | -0.840   | _          | _                     | _          |          |            | Surface |
| P21         | J39    | 4        | -0.853   | 0.092      | 0.9213                | 0.100      |          |            | Surface |
| P21         | J39    | 2        | -0.905   | 0.120      | 0.7979                | 0.151      |          |            | Surface |
| P21         | J39    | 4        | -0.878   | 0.103      | 0.9213                | 0.112      |          |            | Surface |
| P21         | J39    | 3        | -0.827   | 0.193      | 0.8862                | 0.218      |          |            | Surface |
| P21         | J39    | 1        | -0.460   | _          | _                     | _          | -0.794   | 0.145      | Surface |
| P22         | J54    | 6        | -0.148   | 1.176      | 0.9515                | 1.236      |          |            | Surface |
| P22         | J54    | 5        | 0.338    | 0.384      | 0.94                  | 0.409      |          |            | Surface |

| Table B.5. Summar | y of Unbiased | Lot Std Dev for | AV for Each Pro | oject (continued) |
|-------------------|---------------|-----------------|-----------------|-------------------|
|-------------------|---------------|-----------------|-----------------|-------------------|

| Project<br>Number | JMF<br>Number | Lot Size | Lot Mean | Lot St Dev<br>(biased) | <i>c</i> <sub>4</sub> | Lot St Dev | Average | Avg Lot SD | Course  |
|-------------------|---------------|----------|----------|------------------------|-----------------------|------------|---------|------------|---------|
| P22               | J54           | 1        | 0.540    | -                      | _                     |            | 0 243   | 0.822      | Surface |
| P24               | .156          | 1        | 1 100    | _                      | _                     | _          | 0.2.10  | 0.022      | Surface |
| P24               | .156          | 5        | -0 234   | 0 794                  | 0 94                  | 0.845      |         |            | Surface |
| P24               | .156          | 1        | -0.250   | -                      | -                     | -          |         |            | Surface |
| P24               | .156          | 3        | -0.660   | 0.302                  | 0 8862                | 0 341      |         |            | Surface |
| P24               | .156          | 1        | 1 430    | -                      | 0.0002                | -          |         |            | Surface |
| P24               | .156          | 3        | -0.123   | 0 229                  | 0 8862                | 0.258      |         |            | Surface |
| P24               | 156           | 1        | -0.830   | -                      | 0.0002                | 0.200      |         |            | Surface |
| P24               | 156           | 1        | -1 040   | _                      |                       | _          |         |            | Surface |
| P24               | .156          | 3        | -0.520   | 0 790                  | 0 8862                | 0.892      |         |            | Surface |
| P24               | .156          | 1        | -0.980   | -                      | -                     | -          |         |            | Surface |
| P24               | .156          | 4        | -0.628   | 1 296                  | 0 9213                | 1 406      |         |            | Surface |
| P24               | .156          | 2        | 0.390    | 0.099                  | 0 7979                | 0 124      |         |            | Surface |
| P24               | J56           | 1        | 1 300    | _                      | _                     | _          |         |            | Surface |
| P24               | J56           | 3        | -0.067   | 0.980                  | 0 8862                | 1 106      |         |            | Surface |
| P24               | J56           | 1        | -0.480   | _                      | -                     | _          |         |            | Surface |
| P24               | J56           | 2        | -0.540   | 0.651                  | 0 7979                | 0.815      |         |            | Surface |
| P24               | J56           | 4        | -0.980   | 0.169                  | 0.9213                | 0.184      |         |            | Surface |
| P24               | J56           | 3        | 0.413    | 0.352                  | 0.8862                | 0.398      | -0.150  | 0.637      | Surface |
| P24               | J64           | 1        | 0.000    | _                      | _                     | _          | 000     | 0.001      | Surface |
| P24               | J64           | 2        | -0.630   | 0.212                  | 0.7979                | 0.266      |         |            | Surface |
| P24               | J64           | 2        | -0.935   | 0.163                  | 0.7979                | 0.204      |         |            | Surface |
| P24               | J64           | 2        | -0.415   | 0.247                  | 0.7979                | 0.310      |         |            | Surface |
| P24               | J64           | 2        | -0.775   | 0.064                  | 0.7979                | 0.080      |         |            | Surface |
| P24               | J64           | 2        | -0.570   | 0.071                  | 0.7979                | 0.089      |         |            | Surface |
| P24               | J64           | 2        | -0.850   | 0.170                  | 0.7979                | 0.213      | -0.596  | 0.193      | Surface |
| P24               | J67           | 1        | 0.030    | _                      | _                     | _          |         |            | Surface |
| P24               | J67           | 1        | 1.170    | _                      | _                     | _          |         |            | Surface |
| P24               | J67           | 1        | -1.130   | -                      | _                     | _          |         |            | Surface |
| P24               | J67           | 2        | -0.660   | 0.000                  | 0.7979                | 0.000      |         |            | Surface |
| P24               | J67           | 3        | 0.033    | 0.454                  | 0.8862                | 0.512      |         |            | Surface |
| P24               | J67           | 2        | -0.385   | 0.799                  | 0.7979                | 1.001      | -0.157  | 0.505      | Surface |
| P25               | J29           | 2        | 0.295    | 0.205                  | 0.7979                | 0.257      |         |            | Interm  |
| P25               | J29           | 2        | 1.310    | 0.523                  | 0.7979                | 0.656      |         |            | Interm  |
| P25               | J29           | 2        | 0.625    | 0.064                  | 0.7979                | 0.080      |         |            | Interm  |
| P25               | J29           | 2        | 0.690    | 0.156                  | 0.7979                | 0.195      |         |            | Interm  |
| P25               | J29           | 1        | -0.380   | -                      |                       | —          |         |            | Interm  |
| P25               | J29           | 2        | 0.560    | 0.000                  | 0.7979                | 0.000      |         |            | Interm  |
| P25               | J29           | 1        | 1.050    | -                      | I                     | _          | 0.593   | 0.238      | Interm  |
| P25               | J36           | 1        | 0.480    | -                      |                       | —          |         |            | Surface |
| P25               | J36           | 2        | -0.490   | 0.905                  | 0.7979                | 1.134      |         |            | Surface |
| P25               | J36           | 3        | 0.440    | 0.236                  | 0.8862                | 0.266      |         |            | Surface |
| P25               | J36           | 2        | 0.885    | 0.346                  | 0.7979                | 0.434      |         |            | Surface |
| P25               | J36           | 1        | 0.310    | -                      | _                     | -          |         |            | Surface |
| P25               | J36           | 1        | 0.850    | -                      | _                     | -          | 0.413   | 0.612      | Surface |
| P26               | J58           | 1        | -0.050   | -                      | _                     | -          |         |            | Surface |
| P26               | J58           | 1        | -0.630   | -                      | -                     | -          |         |            | Surface |

| Table B.5. Summary of Unbiased Lot | Std Dev for AV for | Each Project (continued) |
|------------------------------------|--------------------|--------------------------|
|------------------------------------|--------------------|--------------------------|

| Project | JMF    | Lot Size | Lot Mean | Lot St Dev | C4     | Lot St Dev | Average  | Avg Lot SD | Course  |
|---------|--------|----------|----------|------------|--------|------------|----------|------------|---------|
| Number  | Number | 4        | 0.070    | (blased)   |        | (unbiased) | Lot Mean | Unbiased   | Curfaga |
| P26     | J58    | 1        | 0.370    | _          | -      | _          |          |            | Surface |
| P26     | J58    | 1        | 0.940    | _          | -      | _          |          |            | Surface |
| P26     | J58    | 1        | -0.300   | _          | _      | _          |          |            | Surface |
| P26     | J58    | 1        | -0.300   | _          | _      | —          |          |            | Surface |
| P26     | J58    | 1        | 0.270    | -          | -      | -          |          |            | Surface |
| P26     | J58    | 1        | 0.120    | -          | -      | -          |          |            | Surface |
| P26     | J58    | 1        | -0.350   | -          | -      | -          |          |            | Surface |
| P26     | J58    | 1        | 0.210    | _          | _      | _          |          |            | Surface |
| P26     | J58    | 2        | 1.465    | 0.163      | 0.7979 | 0.204      |          |            | Surface |
| P26     | J58    | 1        | 0.440    | _          | _      | _          | 0.182    | 0.204      | Surface |
| P26     | J62    | 4        | -0.485   | 0.507      | 0.9213 | 0.550      |          |            | Surface |
| P26     | J62    | 4        | 0.668    | 0.332      | 0.9213 | 0.360      |          |            | Surface |
| P26     | J62    | 3        | 0.553    | 0.097      | 0.8862 | 0.110      |          |            | Surface |
| P26     | J62    | 3        | 0.903    | 0.731      | 0.8862 | 0.824      |          |            | Surface |
| P26     | J62    | 3        | 0.750    | 0.326      | 0.8862 | 0.368      |          |            | Surface |
| P26     | J62    | 3        | 0.480    | 0.249      | 0.8862 | 0.281      |          |            | Surface |
| P26     | J62    | 4        | -0.043   | 0.435      | 0.9213 | 0.472      |          |            | Surface |
| P26     | J62    | 3        | 0.223    | 0.853      | 0.8862 | 0.963      |          |            | Surface |
| P26     | J62    | 4        | 0.270    | 0.452      | 0.9213 | 0.491      | 0.369    | 0.491      | Surface |
| P26     | J69    | 4        | -0.168   | 0.388      | 0.9213 | 0.422      |          |            | Surface |
| P26     | J69    | 3        | -0.120   | 0.528      | 0.8862 | 0.596      |          |            | Surface |
| P26     | J69    | 3        | -0.067   | 0.353      | 0.8862 | 0.398      |          |            | Surface |
| P26     | J69    | 3        | -0.110   | 0.380      | 0.8862 | 0.429      |          |            | Surface |
| P26     | J69    | 3        | -0.170   | 0.229      | 0.8862 | 0.258      |          |            | Surface |
| P26     | J69    | 3        | -0.330   | 0.545      | 0.8862 | 0.615      |          |            | Surface |
| P26     | J69    | 3        | -0.477   | 0.608      | 0.8862 | 0.686      |          |            | Surface |
| P26     | J69    | 3        | 0.380    | 0.272      | 0.8862 | 0.307      |          |            | Surface |
| P26     | J69    | 3        | 0.047    | 0.499      | 0.8862 | 0.563      |          |            | Surface |
| P26     | J69    | 4        | 0.205    | 0.416      | 0.9213 | 0.452      |          |            | Surface |
| P26     | J69    | 3        | 1.083    | 0.442      | 0.8862 | 0.499      |          |            | Surface |
| P26     | J69    | 4        | 0.778    | 0.237      | 0.9213 | 0.257      |          |            | Surface |
| P26     | J69    | 3        | 0.353    | 0.461      | 0.8862 | 0.520      |          |            | Surface |
| P26     | J69    | 3        | 0.483    | 0.225      | 0.8862 | 0.254      |          |            | Surface |
| P26     | J69    | 3        | -0.433   | 0.117      | 0.8862 | 0.132      |          |            | Surface |
| P26     | J69    | 3        | 0.213    | 0.663      | 0.8862 | 0.748      |          |            | Surface |
| P26     | J69    | 1        | 1.910    | Ι          | -      | _          |          |            | Surface |
| P26     | J69    | 1        | 1.010    | _          | -      | -          | 0.255    | 0.446      | Surface |
| P27     | J53    | 1        | -0.840   | Ι          | -      | _          |          |            | Interm  |
| P27     | J53    | 1        | 0.300    | _          | _      | -          |          |            | Interm  |
| P27     | J53    | 1        | -0.240   | -          | _      | -          |          |            | Interm  |
| P27     | J53    | 1        | 0.220    | -          | _      | _          |          |            | Interm  |
| P27     | J53    | 1        | -0.750   | _          | _      | -          |          |            | Interm  |
| P27     | J53    | 2        | -0.175   | 0.035      | 0.7979 | 0.044      |          |            | Interm  |
| P27     | J53    | 1        | -0.270   | _          | _      | -          |          |            | Interm  |
| P27     | J53    | 1        | -0.020   | _          | _      | -          |          |            | Interm  |
| P27     | J53    | 1        | -0.280   | _          | -      | -          |          |            | Interm  |
| P27     | J53    | 1        | 0.090    | _          | _      | -          |          |            | Interm  |

# Table B.5. Summary of Unbiased Lot Std Dev for AV for Each Project (continued)

| Project | JMF    | Lot Size | Lot Mean | Lot St Dev | <i>c</i> <sub>4</sub> | Lot St Dev | Average  | Avg Lot SD | Course  |
|---------|--------|----------|----------|------------|-----------------------|------------|----------|------------|---------|
|         | Number | 1        | 0.000    | (blased)   | · ·                   | (unbiased) | Lot mean | Unblased   | Intorm  |
| P27     | J23    | 1        | -0.220   | _          |                       | _          |          |            |         |
| P27     | J53    | 1        | -1.050   | _          | -                     | _          |          |            |         |
| P27     | J23    |          | 0.070    | -          | -                     | -          |          |            | Interm  |
| P27     | J55    | 3        | -0.263   | 0.306      | 0.8862                | 0.345      |          |            | Surface |
| P27     | J55    | 3        | 0.060    | 0.220      | 0.8862                | 0.248      |          |            | Surface |
| P27     | J55    | 3        | 0.300    | 0.528      | 0.8862                | 0.596      |          |            | Surface |
| P27     | J55    | 3        | 0.107    | 0.670      | 0.8862                | 0.756      | 0.400    | 0.400      | Surface |
| P27     | J55    | 3        | 0.463    | 0.163      | 0.8862                | 0.183      | 0.133    | 0.426      | Surface |
| P27     | J60    | 1        | 0.860    | _          | -                     | -          |          |            | Interm  |
| P27     | J60    | 1        | 0.110    | _          | _                     | —          |          |            | Interm  |
| P27     | J60    | 1        | 0.060    | _          | _                     | —          |          |            | Interm  |
| P27     | J60    | 1        | 1.090    | -          | _                     | —          |          |            | Interm  |
| P27     | J60    | 1        | -0.390   | _          | _                     | —          |          |            | Interm  |
| P27     | J60    | 1        | -0.210   | -          | _                     | —          |          |            | Interm  |
| P27     | J60    | 1        | -0.450   | -          | -                     | -          |          |            | Interm  |
| P27     | J60    | 1        | 0.500    | _          | -                     | _          |          |            | Interm  |
| P27     | J60    | 1        | -0.860   | -          | -                     | _          |          |            | Interm  |
| P27     | J60    | 1        | 0.110    | -          | -                     | _          |          |            | Interm  |
| P27     | J60    | 1        | 0.450    | -          | -                     | _          |          |            | Interm  |
| P27     | J60    | 1        | 0.220    | _          | -                     | -          |          |            | Interm  |
| P27     | J60    | 1        | 0.470    | -          | _                     | -          |          |            | Interm  |
| P27     | J60    | 1        | -1.080   | -          | -                     | -          |          |            | Interm  |
| P27     | J60    | 1        | -0.760   | -          | _                     | -          |          |            | Interm  |
| P27     | J60    | 1        | 0.630    | -          | -                     | —          | 0.047    | —          | Interm  |
| P27     | J61    | 1        | 0.310    | -          | -                     | —          |          |            | Surface |
| P27     | J61    | 1        | -0.060   | -          | -                     | -          |          |            | Surface |
| P27     | J61    | 1        | -0.930   | -          | -                     | —          |          |            | Surface |
| P27     | J61    | 1        | -0.310   | -          | -                     | -          |          |            | Surface |
| P27     | J61    | 1        | -0.800   | -          | -                     | -          |          |            | Surface |
| P27     | J61    | 1        | 0.400    | -          | -                     | -          |          |            | Surface |
| P27     | J61    | 1        | -0.900   | -          | -                     | -          |          |            | Surface |
| P27     | J61    | 1        | -0.810   | -          | -                     | —          |          |            | Surface |
| P27     | J61    | 1        | -0.180   | _          | -                     | —          | -0.364   | #DIV/0!    | Surface |
| P27     | J71    | 3        | 0.410    | 0.531      | 0.8862                | 0.599      |          |            | Surface |
| P27     | J71    | 4        | 0.200    | 0.391      | 0.9213                | 0.425      |          |            | Surface |
| P27     | J71    | 3        | 0.147    | 0.263      | 0.8862                | 0.296      |          |            | Surface |
| P27     | J71    | 2        | 0.500    | 0.566      | 0.7979                | 0.709      |          |            | Surface |
| P27     | J71    | 1        | -0.060   | —          | _                     | _          |          |            | Surface |
| P27     | J71    | 3        | 0.533    | 0.547      | 0.8862                | 0.617      |          |            | Surface |
| P27     | J71    | 3        | -0.357   | 0.643      | 0.8862                | 0.725      |          |            | Surface |
| P27     | J71    | 5        | 0.118    | 0.574      | 0.94                  | 0.610      |          |            | Surface |
| P27     | J71    | 3        | 0.343    | 0.531      | 0.8862                | 0.599      | 0.204    | 0.573      | Surface |
| P28     | J39    | 3        | -0.860   | 0.270      | 0.8862                | 0.305      |          |            | Surface |
| P28     | J39    | 1        | -0.900   | _          | _                     | -          |          |            | Surface |
| P28     | J39    | 4        | -0.700   | 0.324      | 0.9213                | 0.351      |          |            | Surface |
| P28     | J39    | 5        | -0.674   | 0.106      | 0.94                  | 0.112      |          |            | Surface |
| P28     | J39    | 5        | -0.472   | 0.243      | 0.94                  | 0.259      |          |            | Surface |

Table B.5. Summary of Unbiased Lot Std Dev for AV for Each Project (continued)

| Project<br>Number | JMF<br>Number | Lot Size | Lot Mean | Lot St Dev<br>(biased) | <i>c</i> <sub>4</sub> | Lot St Dev | Average  | Avg Lot SD | Course  |
|-------------------|---------------|----------|----------|------------------------|-----------------------|------------|----------|------------|---------|
| P28               | J39           | 1        | -0.400   | _                      | _                     |            | Lot moun | Chiblacea  | Surface |
| P28               | J39           | 3        | -0.507   | 0.105                  | 0.8862                | 0.119      |          |            | Surface |
| P28               | J39           | 1        | -0.530   | _                      | _                     | _          |          |            | Surface |
| P28               | J39           | 1        | 0.150    | _                      | _                     | _          | -0.544   | 0.229      | Surface |
| P28               | J42           | 2        | -0.180   | 0.750                  | 0.7979                | 0.939      |          |            | Interm  |
| P28               | J42           | 1        | 0.830    | _                      | _                     | _          |          |            | Interm  |
| P28               | J42           | 1        | 0.010    | _                      | _                     | _          |          |            | Interm  |
| P28               | J42           | 1        | 0.820    | _                      | _                     | _          |          |            | Interm  |
| P28               | J42           | 1        | -0.040   | _                      | -                     | _          |          |            | Interm  |
| P28               | J42           | 1        | -0.360   | _                      | _                     | _          |          |            | Interm  |
| P28               | J42           | 1        | 0.010    | _                      | _                     | _          |          |            | Interm  |
| P28               | J42           | 1        | 0.010    | _                      | _                     | _          |          |            | Interm  |
| P28               | J42           | 2        | -0.140   | 0.198                  | 0.7979                | 0.248      |          |            | Interm  |
| P28               | J42           | 1        | 0.030    | _                      | _                     | -          |          |            | Interm  |
| P28               | J42           | 1        | -0.010   | _                      | _                     | -          |          |            | Interm  |
| P28               | J42           | 1        | -0.550   | _                      | _                     | -          |          |            | Interm  |
| P28               | J42           | 1        | -0.550   | _                      | _                     | -          | -0.009   | 0.594      | Interm  |
| P29               | J59           | 1        | -0.030   | -                      | -                     | -          |          |            | Surface |
| P29               | J59           | 3        | -0.180   | 0.270                  | 0.8862                | 0.304      |          |            | Surface |
| P29               | J59           | 3        | 0.283    | 0.220                  | 0.8862                | 0.249      |          |            | Surface |
| P29               | J59           | 3        | -0.180   | 0.170                  | 0.8862                | 0.192      |          |            | Surface |
| P29               | J59           | 3        | 0.417    | 0.396                  | 0.8862                | 0.446      |          |            | Surface |
| P29               | J59           | 3        | -0.107   | 0.214                  | 0.8862                | 0.241      |          |            | Surface |
| P29               | J59           | 4        | -0.045   | 0.160                  | 0.9213                | 0.173      |          |            | Surface |
| P29               | J59           | 3        | -0.090   | 0.135                  | 0.8862                | 0.153      |          |            | Surface |
| P29               | J59           | 3        | -0.133   | 0.205                  | 0.8862                | 0.232      | -0.007   | 0.249      | Surface |
| P30               | J65           | 3        | 0.640    | 0.390                  | 0.8862                | 0.440      |          |            | Surface |
| P30               | J65           | 3        | 0.427    | 0.021                  | 0.8862                | 0.023      |          |            | Surface |
| P30               | J65           | 1        | 0.450    | -                      | -                     | _          |          |            | Surface |
| P30               | J65           | 1        | 0.430    | -                      | _                     | _          | 0.487    | 0.232      | Surface |
| P32               | J72           | 5        | 0.312    | 0.165                  | 0.94                  | 0.175      |          |            | Surface |
| P32               | J72           | 6        | 0.588    | 0.387                  | 0.9515                | 0.407      |          |            | Surface |
| P32               | J72           | 3        | 0.447    | 0.076                  | 0.8862                | 0.085      |          |            | Surface |
| P32               | J72           | 3        | -0.300   | 0.070                  | 0.8862                | 0.079      |          |            | Surface |
| P32               | J72           | 5        | -0.334   | 0.155                  | 0.94                  | 0.165      |          |            | Surface |
| P32               | J72           | 5        | -0.500   | 0.221                  | 0.94                  | 0.235      |          |            | Surface |
| P32               | J72           | 3        | -0.523   | 0.261                  | 0.8862                | 0.294      |          |            | Surface |
| P32               | J72           | 4        | -0.265   | 0.430                  | 0.9213                | 0.467      | -0.072   | 0.238      | Surface |
| P32               | J76           | 4        | -0.660   | 0.281                  | 0.9213                | 0.305      |          |            | Interm  |
| P32               | J76           | 3        | -0.537   | 0.309                  | 0.8862                | 0.349      |          |            | Interm  |
| P32               | J76           | 5        | -0.524   | 0.400                  | 0.94                  | 0.425      |          |            | Interm  |
| P32               | J76           | 4        | -0.430   | 0.576                  | 0.9213                | 0.625      |          |            | Interm  |
| P32               | J76           | 3        | -0.513   | 0.196                  | 0.8862                | 0.221      |          |            | Interm  |
| P32               | J76           | 3        | -0.477   | 0.150                  | 0.8862                | 0.170      |          |            | Interm  |
| P32               | J76           | 3        | -0.563   | 0.121                  | 0.8862                | 0.137      |          |            | Interm  |
| P32               | J76           | 4        | -0.550   | 0.507                  | 0.9213                | 0.551      |          |            | Interm  |
| P32               | J76           | 4        | -0.840   | 0.203                  | 0.9213                | 0.220      |          |            | Interm  |

# Table B.5. Summary of Unbiased Lot Std Dev for AV for Each Project (continued)

| Project<br>Number | JMF<br>Number | Lot Size | Lot Mean | Lot St Dev<br>(biased) | $c_4$  | Lot St Dev<br>(unbiased) | Average<br>Lot Mean | Avg Lot SD<br>Unbiased | Course  |
|-------------------|---------------|----------|----------|------------------------|--------|--------------------------|---------------------|------------------------|---------|
| P32               | J76           | 4        | -0.795   | 0.216                  | 0.9213 | 0.234                    |                     |                        | Interm  |
| P32               | J76           | 3        | -0.880   | 0 159                  | 0.8862 | 0 179                    |                     |                        | Interm  |
| P32               | J76           | 3        | -0.400   | 0.278                  | 0.8862 | 0.314                    | -0.597              | 0.311                  | Interm  |
| P32               | J79           | 6        | -0.413   | 0.534                  | 0.9515 | 0.562                    | 0.001               | 0.011                  | Surface |
| P32               |               | 5        | -0.222   | 0.311                  | 0.94   | 0.330                    |                     |                        | Surface |
| P32               | J79           | 4        | -0.125   | 0.424                  | 0.9213 | 0.460                    |                     |                        | Surface |
| P32               |               | 3        | -0.673   | 0.523                  | 0.8862 | 0.590                    |                     |                        | Surface |
| P32               |               | 4        | -0.123   | 0.180                  | 0.9213 | 0.195                    |                     |                        | Surface |
| P32               |               | 3        | -0.333   | 0.102                  | 0.8862 | 0.115                    |                     |                        | Surface |
| P32               | J79           | 3        | 0.017    | 0.701                  | 0.8862 | 0.791                    |                     |                        | Surface |
| P32               |               | 3        | 0.220    | 0.246                  | 0.8862 | 0.277                    |                     |                        | Surface |
| P32               |               | 4        | -0.008   | 0.280                  | 0.9213 | 0.304                    |                     |                        | Surface |
| P32               | J79           | 5        | -0.074   | 0.690                  | 0.94   | 0.734                    |                     |                        | Surface |
| P32               | J79           | 4        | -0.175   | 0.308                  | 0.9213 | 0.334                    |                     |                        | Surface |
| P32               | J79           | 5        | 0.062    | 0.337                  | 0.94   | 0.358                    |                     |                        | Surface |
| P32               | J79           | 3        | 0.317    | 0.266                  | 0.8862 | 0.300                    |                     |                        | Surface |
| P32               | J79           | 5        | -0.514   | 0.412                  | 0.94   | 0.439                    |                     |                        | Surface |
| P32               | J79           | 5        | -0.472   | 0.604                  | 0.94   | 0.643                    |                     |                        | Surface |
| P32               | J79           | 5        | -0.744   | 0.297                  | 0.94   | 0.316                    |                     |                        | Surface |
| P32               | J79           | 5        | -0.224   | 0.196                  | 0.94   | 0.208                    |                     |                        | Surface |
| P32               | J79           | 3        | -0.303   | 0.622                  | 0.8862 | 0.702                    |                     |                        | Surface |
| P32               | J79           | 5        | -0.110   | 0.296                  | 0.94   | 0.314                    |                     |                        | Surface |
| P32               | J79           | 3        | 0.313    | 0.535                  | 0.8862 | 0.604                    |                     |                        | Surface |
| P32               | J79           | 3        | -0.023   | 0.356                  | 0.8862 | 0.402                    |                     |                        | Surface |
| P32               | J79           | 4        | -0.545   | 0.580                  | 0.9213 | 0.630                    |                     |                        | Surface |
| P32               | J79           | 3        | -0.767   | 0.296                  | 0.8862 | 0.334                    |                     |                        | Surface |
| P32               | J79           | 3        | -0.927   | 0.455                  | 0.8862 | 0.513                    | -0.244              | 0.436                  | Surface |
| P33               | J73           | 1        | -0.230   | -                      | I      | _                        |                     |                        | Interm  |
| P33               | J73           | 3        | 0.267    | 0.326                  | 0.8862 | 0.368                    |                     |                        | Interm  |
| P33               | J73           | 3        | -0.613   | 0.755                  | 0.8862 | 0.852                    |                     |                        | Interm  |
| P33               | J73           | 5        | 0.068    | 0.588                  | 0.94   | 0.626                    |                     |                        | Interm  |
| P33               | J73           | 4        | 0.490    | 0.140                  | 0.9213 | 0.152                    |                     |                        | Interm  |
| P33               | J73           | 3        | 0.033    | 0.281                  | 0.8862 | 0.317                    |                     |                        | Interm  |
| P33               | J73           | 3        | 0.410    | 0.593                  | 0.8862 | 0.669                    |                     |                        | Interm  |
| P33               | J73           | 3        | 0.263    | 0.338                  | 0.8862 | 0.382                    | 0.086               | 0.481                  | Interm  |
| P33               | J77           | 4        | 1.135    | 0.413                  | 0.9213 | 0.448                    |                     |                        | Surface |
| P33               | J77           | 4        | 0.360    | 0.329                  | 0.9213 | 0.357                    |                     |                        | Surface |
| P33               | J77           | 4        | -0.308   | 0.189                  | 0.9213 | 0.205                    |                     |                        | Surface |
| P33               | J77           | 4        | 0.645    | 0.429                  | 0.9213 | 0.466                    |                     |                        | Surface |
| P33               | J77           | 3        | 0.903    | 0.098                  | 0.8862 | 0.111                    |                     |                        | Surface |
| P33               | J77           | 3        | 0.040    | 0.819                  | 0.8862 | 0.924                    | 0.463               | 0.419                  | Surface |
| P34               | J62           | 4        | 0.173    | 0.593                  | 0.9213 | 0.643                    |                     |                        | Surface |
| P34               | J62           | 4        | -0.595   | 0.112                  | 0.9213 | 0.121                    |                     |                        | Surface |
| P34               | J62           | 6        | 0.362    | 0.285                  | 0.9515 | 0.300                    |                     |                        | Surface |
| P34               | J62           | 4        | 0.745    | 0.827                  | 0.9213 | 0.898                    |                     |                        | Surface |
| P34               | J62           | 4        | 0.303    | 1.080                  | 0.9213 | 1.172                    |                     |                        | Surface |
| P34               | J62           | 4        | -0.040   | 0.598                  | 0.9213 | 0.649                    |                     |                        | Surface |

Table B.5. Summary of Unbiased Lot Std Dev for AV for Each Project (continued)

| Project<br>Number | JMF<br>Number | Lot Size | Lot Mean | Lot St Dev<br>(biased) | <i>c</i> <sub>4</sub> | Lot St Dev<br>(unbiased) | Average<br>Lot Mean | Avg Lot SD<br>Unbiased | Course  |
|-------------------|---------------|----------|----------|------------------------|-----------------------|--------------------------|---------------------|------------------------|---------|
| P34               | J62           | 2        | -0.125   | 0.120                  | 0.7979                | 0.151                    | 0.117               | 0.562                  | Surface |
| P34               | J81           | 2        | 1.090    | 0.042                  | 0.7979                | 0.053                    |                     |                        | Surface |
| P34               | J81           | 2        | 0.370    | 0.127                  | 0.7979                | 0.160                    |                     |                        | Surface |
| P34               | J81           | 1        | 0.290    | _                      | _                     | _                        |                     |                        | Surface |
| P34               | J81           | 2        | -0.335   | 0.587                  | 0.7979                | 0.736                    |                     |                        | Surface |
| P34               | J81           | 2        | -0.400   | 0.311                  | 0.7979                | 0.390                    |                     |                        | Surface |
| P34               | J81           | 2        | -0.165   | 0.050                  | 0.7979                | 0.062                    |                     |                        | Surface |
| P34               | J81           | 2        | -0.215   | 0.346                  | 0.7979                | 0.434                    | 0.091               | 0.306                  | Surface |
| P35               | J32           | 3        | 0.023    | 1.028                  | 0.8862                | 1.160                    |                     |                        | Surface |
| P35               | J32           | 1        | 0.170    | _                      | _                     | _                        |                     |                        | Surface |
| P35               | J32           | 3        | 0.373    | 0.295                  | 0.8862                | 0.333                    |                     |                        | Surface |
| P35               | J32           | 3        | 0.350    | 0.223                  | 0.8862                | 0.252                    |                     |                        | Surface |
| P35               | J32           | 3        | 0.890    | 0.036                  | 0.8862                | 0.041                    |                     |                        | Surface |
| P35               | J32           | 1        | 0.510    | _                      | -                     | _                        | 0.386               | 0.446                  | Surface |
| P35               | J38           | 2        | -0.205   | 0.219                  | 0.7979                | 0.275                    |                     |                        | Surface |
| P35               | J38           | 2        | -0.305   | 0.318                  | 0.7979                | 0.399                    |                     |                        | Surface |
| P35               | J38           | 1        | -0.300   | -                      | -                     | -                        |                     |                        | Surface |
| P35               | J38           | 2        | 0.180    | 0.764                  | 0.7979                | 0.957                    |                     |                        | Surface |
| P35               | J38           | 2        | 0.210    | 0.014                  | 0.7979                | 0.018                    |                     |                        | Surface |
| P35               | J38           | 1        | 0.040    | -                      | —                     | _                        |                     |                        | Surface |
| P35               | J38           | 2        | 0.100    | 0.000                  | 0.7979                | 0.000                    |                     |                        | Surface |
| P35               | J38           | 3        | -0.600   | 0.239                  | 0.8862                | 0.270                    |                     |                        | Surface |
| P35               | J38           | 5        | -0.150   | 0.453                  | 0.94                  | 0.482                    |                     |                        | Surface |
| P35               | J38           | 2        | 0.175    | 0.050                  | 0.7979                | 0.062                    |                     |                        | Surface |
| P35               | J38           | 4        | 0.048    | 0.098                  | 0.9213                | 0.106                    |                     |                        | Surface |
| P35               | J38           | 3        | 0.263    | 0.006                  | 0.8862                | 0.007                    |                     |                        | Surface |
| P35               | J38           | 3        | 0.183    | 0.133                  | 0.8862                | 0.150                    |                     |                        | Surface |
| P35               | J38           | 2        | 0.595    | 0.106                  | 0.7979                | 0.133                    |                     |                        | Surface |
| P35               | J38           | 1        | 0.620    | _                      | _                     | _                        |                     |                        | Surface |
| P35               | J38           | 1        | 0.450    | _                      | _                     | -                        | 0.082               | 0.238                  | Surface |
|                   |               |          |          |                        |                       |                          |                     |                        |         |
|                   |               |          |          |                        |                       |                          |                     |                        |         |
|                   |               |          |          |                        |                       |                          |                     |                        |         |
|                   |               |          |          |                        |                       |                          |                     |                        |         |
|                   |               |          |          |                        |                       |                          |                     |                        |         |
|                   |               |          |          |                        |                       |                          |                     |                        |         |
| -                 |               |          |          |                        |                       |                          |                     |                        |         |
|                   |               |          |          |                        |                       |                          |                     |                        |         |
| -                 |               |          |          |                        |                       |                          |                     |                        |         |
|                   |               |          |          |                        |                       |                          |                     |                        |         |
|                   |               |          |          |                        |                       |                          |                     |                        |         |
|                   |               |          |          |                        |                       |                          |                     |                        |         |
|                   |               |          |          |                        |                       |                          |                     |                        |         |
|                   |               |          |          |                        |                       |                          |                     |                        |         |
|                   |               |          |          |                        |                       |                          |                     |                        |         |
|                   |               |          |          |                        |                       |                          |                     |                        |         |

| Table B.5. Summar | y of Unbiased Lot | Std Dev for AV for | Each Project | (continued) |
|-------------------|-------------------|--------------------|--------------|-------------|
|-------------------|-------------------|--------------------|--------------|-------------|

| Project<br>Number | JMF<br>Number | Lot Size | Lot Mean | Lot St Dev<br>(biased) | <i>c</i> <sub>4</sub> | Lot St Dev | Average<br>Lot Mean | Avg Lot SD | Course  |
|-------------------|---------------|----------|----------|------------------------|-----------------------|------------|---------------------|------------|---------|
| P01               | .102          | 2        | 0.020    | 0.679                  | 0 7979                | 0.851      | Lot moun            | Chibladea  | Interm  |
| P01               | .102          | 3        | 0.020    | 0.779                  | 0.8862                | 0.879      |                     |            | Interm  |
| P01               | .102          | 2        | -0.165   | 0.318                  | 0 7979                | 0.399      |                     |            | Interm  |
| P01               | .102          | 1        | -0.220   | -                      | _                     | -          | -0.035              | 0 70948    | Interm  |
| P01               | J07           | 3        | 0.590    | 0.053                  | 0.8862                | 0.060      | 0.000               | 011 00 10  | Surface |
| P01               | J07           | 3        | 0.300    | 0.892                  | 0.8862                | 1 006      |                     |            | Surface |
| P01               | J07           | 5        | 0.368    | 0.512                  | 0.9400                | 0.545      |                     |            | Surface |
| P01               | J07           | 3        | 0.607    | 0.265                  | 0.8862                | 0.299      |                     |            | Surface |
| P01               | J07           | 3        | -0.010   | 0.245                  | 0.8862                | 0.277      |                     |            | Surface |
| P01               | J07           | 1        | 0.400    | _                      | _                     | _          |                     |            | Surface |
| P01               | J07           | 3        | -0.387   | 0.471                  | 0.8862                | 0.531      |                     |            | Surface |
| P01               | J07           | 5        | 0.094    | 0.357                  | 0.9400                | 0.380      |                     |            | Surface |
| P01               | J07           | 4        | 0.320    | 0.336                  | 0.9213                | 0.364      | 0.254               | 0.43264    | Surface |
| P01               | J10           | 3        | -0.577   | 0.354                  | 0.8862                | 0.400      |                     |            | Interm  |
| P01               | J10           | 1        | -0.320   | _                      | _                     | _          |                     |            | Interm  |
| P01               | J10           | 1        | -2.000   | _                      | _                     | _          |                     |            | Interm  |
| P01               | J10           | 4        | -0.243   | 0.255                  | 0.9213                | 0.277      |                     |            | Interm  |
| P01               | J10           | 3        | -0.473   | 0.376                  | 0.8862                | 0.424      |                     |            | Interm  |
| P01               | J10           | 1        | -0.020   | -                      | _                     | _          |                     |            | Interm  |
| P01               | J10           | 3        | -0.567   | 0.210                  | 0.8862                | 0.237      |                     |            | Interm  |
| P01               | J10           | 1        | -0.130   | _                      | _                     | _          |                     |            | Interm  |
| P01               | J10           | 1        | 0.200    | _                      | _                     | _          |                     |            | Interm  |
| P01               | J10           | 1        | -0.350   | -                      | I                     | -          |                     |            | Interm  |
| P01               | J10           | 2        | 0.215    | 0.912                  | 0.7979                | 1.143      |                     |            | Interm  |
| P01               | J10           | 2        | -0.120   | 0.085                  | 0.7979                | 0.106      |                     |            | Interm  |
| P01               | J10           | 4        | -0.253   | 0.200                  | 0.9213                | 0.217      |                     |            | Interm  |
| P01               | J10           | 2        | -0.310   | 0.297                  | 0.7979                | 0.372      |                     |            | Interm  |
| P01               | J10           | 2        | -0.145   | 0.120                  | 0.7979                | 0.151      |                     |            | Interm  |
| P01               | J10           | 3        | 0.330    | 0.471                  | 0.8862                | 0.532      |                     |            | Interm  |
| P01               | J10           | 2        | -0.190   | 0.099                  | 0.7979                | 0.124      |                     |            | Interm  |
| P01               | J10           | 3        | -0.507   | 0.359                  | 0.8862                | 0.405      | -0.303              | 0.36569    | Interm  |
| P01               | J19           | 1        | -0.420   | -                      | —                     | -          |                     |            | Surface |
| P01               | J19           | 1        | 0.860    | -                      | —                     | -          |                     |            | Surface |
| P01               | J19           | 2        | -0.460   | 0.481                  | 0.7979                | 0.603      |                     |            | Surface |
| P01               | J19           | 2        | -0.465   | 0.276                  | 0.7979                | 0.346      |                     |            | Surface |
| P01               | J19           | 1        | -0.700   | -                      | —                     | -          |                     |            | Surface |
| P01               | J19           | 1        | 0.280    | -                      | —                     | -          |                     |            | Surface |
| P01               | J19           | 1        | 1.130    | -                      | —                     | -          |                     |            | Surface |
| P01               | J19           | 1        | 1.130    | _                      | —                     | -          |                     |            | Surface |
| P01               | J19           | 2        | 0.200    | 0.057                  | 0.7979                | 0.071      |                     |            | Surface |
| P01               | J19           | 1        | -0.600   | _                      | —                     | -          |                     |            | Surface |
| P01               | J19           | 1        | 0.200    | _                      | _                     | _          |                     |            | Surface |
| P01               | J19           | 2        | -0.355   | 0.643                  | 0.7979                | 0.806      |                     |            | Surface |
| P01               | J19           |          | 0.170    | _                      | -                     | -          | 0.001               | 0.450.10   | Surface |
| P01               | J19           |          | -0.540   | -                      | -                     | -          | 0.031               | 0.45640    | Surface |
| P01               | J23           | 4        | 0.188    | 0.296                  | 0.9213                | 0.321      |                     |            | Interm  |
| P01               | J23           | 3        | -0.217   | 0.751                  | 0.8862                | 0.847      |                     |            | Interm  |

 Table B.6. Summary of Unbiased Lot Std Dev for VMA for Each Project

| Project<br>Number | JMF<br>Number | Lot Size | Lot Mean | Lot St Dev<br>(biased) | <i>c</i> <sub>4</sub> | Lot St Dev<br>(unbiased) | Average<br>Lot Mean | Avg Lot SD<br>Unbiased | Course  |
|-------------------|---------------|----------|----------|------------------------|-----------------------|--------------------------|---------------------|------------------------|---------|
| P01               | J23           | 1        | 0.080    |                        | -                     | -                        |                     |                        | Interm  |
| P01               | J23           | 2        | -0.290   | 0.721                  | 0.7979                | 0.904                    |                     |                        | Interm  |
| P01               | J23           | 1        | 0.340    | -                      | _                     | _                        |                     |                        | Interm  |
| P01               | J23           | 1        | -0.240   | -                      | _                     | _                        | -0.023              | 0.69080                | Interm  |
| P02               | J04           | 4        | 0.485    | 0.253                  | 0.9213                | 0.274                    |                     |                        | Interm  |
| P02               | J04           | 1        | 0.840    | -                      | _                     | _                        |                     |                        | Interm  |
| P02               | J04           | 2        | -0.265   | 0.078                  | 0.7979                | 0.097                    |                     |                        | Interm  |
| P02               | J04           | 2        | 0.285    | 0.559                  | 0.7979                | 0.700                    |                     |                        | Interm  |
| P02               | J04           | 4        | -0.350   | 0.384                  | 0.9213                | 0.417                    |                     |                        | Interm  |
| P02               | J04           | 1        | 0.990    | _                      | _                     | -                        |                     |                        | Interm  |
| P02               | J04           | 4        | -0.528   | 0.333                  | 0.9213                | 0.361                    |                     |                        | Interm  |
| P02               | J04           | 1        | 0.950    | -                      | _                     | _                        |                     |                        | Interm  |
| P02               | J04           | 1        | 1.100    | -                      | _                     | _                        |                     |                        | Interm  |
| P02               | J04           | 2        | 0.225    | 0.375                  | 0.7979                | 0.470                    |                     |                        | Interm  |
| P02               | J04           | 3        | 0.030    | 0.193                  | 0.8862                | 0.218                    |                     |                        | Interm  |
| P02               | J04           | 1        | 0.820    | _                      | _                     | _                        |                     |                        | Interm  |
| P02               | J04           | 1        | 0.620    | _                      | _                     | _                        |                     |                        | Interm  |
| P02               | J04           | 3        | 0.737    | 0.421                  | 0.8862                | 0.475                    | 0.424               | 0.37651                | Interm  |
| P02               | J05           | 2        | 0.475    | 0.262                  | 0.7979                | 0.328                    |                     |                        | Surface |
| P02               | J05           | 1        | 0.450    | _                      | _                     | _                        |                     |                        | Surface |
| P02               | J05           | 2        | -0.040   | 0.071                  | 0.7979                | 0.089                    |                     |                        | Surface |
| P02               | J05           | 1        | 0.220    | -                      | _                     | -                        |                     |                        | Surface |
| P02               | J05           | 1        | 0.450    | -                      | _                     | -                        |                     |                        | Surface |
| P02               | J05           | 1        | 0.830    | Ι                      | I                     | _                        | 0.398               | 0.20826                | Surface |
| P02               | J09           | 1        | 0.400    | Ι                      | I                     | _                        |                     |                        | Interm  |
| P02               | J09           | 2        | 0.595    | 0.276                  | 0.7979                | 0.346                    |                     |                        | Interm  |
| P02               | J09           | 1        | 0.150    | -                      | -                     | _                        |                     |                        | Interm  |
| P02               | J09           | 3        | 0.307    | 0.549                  | 0.8862                | 0.620                    |                     |                        | Interm  |
| P02               | J09           | 2        | -0.275   | 0.346                  | 0.7979                | 0.434                    |                     |                        | Interm  |
| P02               | J09           | 2        | 0.550    | 0.156                  | 0.7979                | 0.195                    |                     |                        | Interm  |
| P02               | J09           | 1        | -1.350   | _                      | _                     | _                        |                     |                        | Interm  |
| P02               | J09           | 1        | 0.440    | —                      | -                     | _                        |                     |                        | Interm  |
| P02               | J09           | 2        | -0.900   | 0.141                  | 0.7979                | 0.177                    |                     |                        | Interm  |
| P02               | J09           | 3        | 0.350    | 0.531                  | 0.8862                | 0.599                    |                     |                        | Interm  |
| P02               | J09           | 2        | -0.220   | 0.424                  | 0.7979                | 0.532                    |                     |                        | Interm  |
| P02               | J09           | 2        | -0.250   | 1.018                  | 0.7979                | 1.276                    |                     |                        | Interm  |
| P02               | J09           | 1        | 0.960    | -                      | -                     | -                        |                     |                        | Interm  |
| P02               | J09           | 4        | 0.108    | 0.557                  | 0.9213                | 0.604                    |                     |                        | Interm  |
| P02               | J09           | 2        | -0.745   | 0.247                  | 0.7979                | 0.310                    |                     |                        | Interm  |
| P02               | J09           | 1        | -0.340   | -                      | -                     | -                        |                     |                        | Interm  |
| P02               | J09           | 2        | -0.070   | 0.354                  | 0.7979                | 0.443                    |                     |                        | Interm  |
| P02               | J09           | 2        | 0.670    | 0.608                  | 0.7979                | 0.762                    | 0.021               | 0.52488                | Interm  |
| P02               | J13           | 1        | 0.660    | -                      | -                     | -                        |                     |                        | Surface |
| P02               | J13           | 1        | -0.230   | -                      | -                     | -                        |                     |                        | Surface |
| P02               | J13           | 2        | 1.060    | 0.127                  | 0.7979                | 0.160                    |                     |                        | Surface |
| P02               | J13           | 1        | 1.060    | -                      | -                     | -                        |                     |                        | Surface |
| P02               | J13           | 1        | 0.280    | —                      | —                     | -                        |                     |                        | Surface |

# Table B.6. Summary of Unbiased Lot Std Dev for VMA for Each Project (continued)

| Project<br>Number | JMF<br>Number | Lot Size | Lot Mean | Lot St Dev<br>(biased) | <i>c</i> <sub>4</sub> | Lot St Dev | Average  | Avg Lot SD | Course  |
|-------------------|---------------|----------|----------|------------------------|-----------------------|------------|----------|------------|---------|
| P02               | J13           | 1        | 0.390    | _                      | _                     |            | Lot moun | ensideed   | Surface |
| P02               | J13           | 2        | -0.105   | 0.417                  | 0.7979                | 0.523      |          |            | Surface |
| P02               | J13           | 1        | -0.600   | _                      | _                     | _          |          |            | Surface |
| P02               | J13           | 1        | -0.760   | _                      | _                     | _          |          |            | Surface |
| P02               | J13           | 1        | 0.180    | _                      | _                     | _          |          |            | Surface |
| P02               | J13           | 1        | 0.380    | _                      | _                     | _          |          |            | Surface |
| P02               | J13           | 2        | -0.435   | 0.361                  | 0.7979                | 0.452      |          |            | Surface |
| P02               | J13           | 2        | 0.805    | 0.233                  | 0.7979                | 0.292      |          |            | Surface |
| P02               | J13           | 1        | 0.180    | _                      | _                     | _          | 0.205    | 0.35670    | Surface |
| P02               | J15           | 1        | 1.120    | _                      | _                     | _          | 0.200    | 0.00010    | Surface |
| P02               | J15           | 4        | 0.578    | 0.113                  | 0.9213                | 0.123      |          |            | Surface |
| P02               | J15           | 4        | 0.255    | 0.218                  | 0.9213                | 0.237      |          |            | Surface |
| P02               | J15           | 5        | 0.730    | 0.619                  | 0.9400                | 0.659      |          |            | Surface |
| P02               | J15           | 3        | -0.100   | 0.820                  | 0.8862                | 0.926      |          |            | Surface |
| P02               | J15           | 1        | -0.520   | _                      | _                     | _          | 0.344    | 0.48596    | Surface |
| P04               | J08           | 2        | -0.230   | 1.245                  | 0.7979                | 1.560      |          |            | Interm  |
| P04               | J08           | 2        | 0.705    | 0.601                  | 0.7979                | 0.753      |          |            | Interm  |
| P04               | J08           | 2        | 0.860    | 0.481                  | 0.7979                | 0.603      |          |            | Interm  |
| P04               | J08           | 2        | 1.085    | 0.615                  | 0.7979                | 0.771      |          |            | Interm  |
| P04               | J08           | 2        | 0.615    | 0.658                  | 0.7979                | 0.824      | 0.607    | 0.90216    | Interm  |
| P04               | J14           | 3        | 0.377    | 0.391                  | 0.8862                | 0.441      |          |            | Surface |
| P04               | J14           | 4        | 0.070    | 0.595                  | 0.9213                | 0.646      |          |            | Surface |
| P04               | J14           | 4        | 0.793    | 0.490                  | 0.9213                | 0.532      |          |            | Surface |
| P04               | J14           | 3        | 0.410    | 0.308                  | 0.8862                | 0.348      |          |            | Surface |
| P04               | J14           | 3        | 0.083    | 0.528                  | 0.8862                | 0.596      | 0.347    | 0.51253    | Surface |
| P05               | J25           | 1        | -1.400   | -                      | _                     | _          |          |            | Surface |
| P05               | J25           | 1        | 0.030    | _                      | _                     | _          |          |            | Surface |
| P05               | J25           | 1        | -0.270   | -                      | _                     | -          |          |            | Surface |
| P05               | J25           | 1        | -0.990   | -                      | _                     | -          |          |            | Surface |
| P05               | J25           | 1        | -0.370   | -                      | _                     | _          |          |            | Surface |
| P05               | J25           | 1        | 1.000    | -                      | —                     | _          |          |            | Surface |
| P05               | J25           | 1        | 0.140    | -                      | —                     | _          |          |            | Surface |
| P05               | J25           | 1        | 0.090    | -                      | _                     | —          | -0.221   | #DIV/0!    | Surface |
| P05               | J27           | 2        | 0.015    | 0.417                  | 0.7979                | 0.523      |          |            | Interm  |
| P05               | J27           | 2        | 0.345    | 0.403                  | 0.7979                | 0.505      |          |            | Interm  |
| P05               | J27           | 2        | 0.370    | 0.495                  | 0.7979                | 0.620      |          |            | Interm  |
| P05               | J27           | 2        | 0.150    | 0.028                  | 0.7979                | 0.035      |          |            | Interm  |
| P05               | J27           | 2        | -0.590   | 0.170                  | 0.7979                | 0.213      |          |            | Interm  |
| P05               | J27           | 2        | 0.020    | 0.000                  | 0.7979                | 0.000      |          |            | Interm  |
| P05               | J27           | 1        | -0.110   | _                      | _                     | -          |          |            | Interm  |
| P05               | J27           | 2        | 0.130    | 0.764                  | 0.7979                | 0.957      | 0.041    | 0.40766    | Interm  |
| P06               | J24           | 3        | -0.493   | 0.416                  | 0.8862                | 0.469      |          |            | Surface |
| P06               | J24           | 3        | -0.187   | 0.577                  | 0.8862                | 0.651      |          |            | Surface |
| P06               | J24           | 3        | -0.140   | 0.060                  | 0.8862                | 0.068      |          |            | Surface |
| P06               | J24           | 3        | 0.053    | 0.858                  | 0.8862                | 0.968      |          |            | Surface |
| P06               | J24           | 3        | -0.283   | 0.522                  | 0.8862                | 0.589      | -0.210   | 0.54906    | Surface |
| P07               | J30           | 3        | 0.363    | 0.119                  | 0.8862                | 0.135      |          |            | Surface |

| Table B.6. Summary of Unbiased Lot Std D | Dev for VMA for Each Project (continued) |
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|--|--|

| Project | JMF  | Lot Size | Lot Mean | Lot St Dev | <i>c</i> <sub>4</sub> | Lot St Dev | Average  | Avg Lot SD | Course  |
|---------|------|----------|----------|------------|-----------------------|------------|----------|------------|---------|
| P07     | .130 | 1        | 0.230    | (biaseu)   | _                     |            | Lot mean | Unblased   | Surface |
| P07     | .130 | 1        | 0.020    | _          | _                     | _          |          |            | Surface |
| P07     | .130 | 1        | 0.590    | _          | _                     | _          |          |            | Surface |
| P07     | .130 | 4        | 0.000    | 0 518      | 0 9213                | 0 562      |          |            | Surface |
| P07     | .130 | 2        | 0.210    | 0.010      | 0.0210                | 0.002      |          |            | Surface |
| P07     | .130 | 2        | -0.420   | 0.120      | 0.7979                | 0.585      |          |            | Surface |
| P07     | J30  | 1        | 0.070    | _          | _                     | -          |          |            | Surface |
| P07     | J30  | 3        | -0.080   | 0.229      | 0.8862                | 0.258      |          |            | Surface |
| P07     | J30  | 3        | -0.357   | 0.611      | 0.8862                | 0.689      |          |            | Surface |
| P07     | J30  | 3        | 0.327    | 0.511      | 0.8862                | 0.576      |          |            | Surface |
| P07     | J30  | 3        | -0.093   | 0.638      | 0.8862                | 0.720      |          |            | Surface |
| P07     | J30  | 2        | -0.515   | 0.120      | 0.7979                | 0.151      |          |            | Surface |
| P07     | J30  | 3        | -0.360   | 0.416      | 0.8862                | 0.469      |          |            | Surface |
| P07     | J30  | 3        | -0.420   | 0.076      | 0.8862                | 0.085      |          |            | Surface |
| P07     | J30  | 1        | 0.320    | _          | _                     | _          |          |            | Surface |
| P07     | J30  | 2        | -0.335   | 0.559      | 0.7979                | 0.700      |          |            | Surface |
| P07     | J30  | 1        | 0.300    | _          | _                     | _          |          |            | Surface |
| P07     | J30  | 1        | 0.420    | _          | _                     | _          | 0.026    | 0.42341    | Surface |
| P09     | J35  | 3        | 0.413    | 0.690      | 0.8862                | 0.778      |          |            | Surface |
| P09     | J35  | 3        | -0.057   | 0.115      | 0.8862                | 0.130      |          |            | Surface |
| P09     | J35  | 3        | 0.333    | 0.257      | 0.8862                | 0.290      | 0.230    | 0.39950    | Surface |
| P09     | J83  | 3        | -0.013   | 0.631      | 0.8862                | 0.712      |          |            | Surface |
| P09     | J83  | 3        | -0.463   | 0.598      | 0.8862                | 0.674      |          |            | Surface |
| P09     | J83  | 2        | -0.610   | 0.410      | 0.7979                | 0.514      | -0.362   | 0.63339    | Surface |
| P10     | J12  | 1        | 0.710    | _          | _                     | _          |          |            | Surface |
| P10     | J12  | 1        | 0.690    | _          | _                     | _          |          |            | Surface |
| P10     | J12  | 1        | 0.940    | I          | _                     | -          |          |            | Surface |
| P10     | J12  | 2        | 1.070    | 0.028      | 0.7979                | 0.035      |          |            | Surface |
| P10     | J12  | 1        | 0.160    | I          | _                     | -          |          |            | Surface |
| P10     | J12  | 1        | 0.320    | -          | -                     | —          |          |            | Surface |
| P10     | J12  | 1        | -0.470   | _          | -                     | _          |          |            | Surface |
| P10     | J12  | 1        | -0.750   | _          | _                     | _          |          |            | Surface |
| P10     | J12  | 2        | 1.330    | 0.424      | 0.7979                | 0.532      |          |            | Surface |
| P10     | J12  | 2        | 0.065    | 0.219      | 0.7979                | 0.275      |          |            | Surface |
| P10     | J12  | 2        | -0.170   | 0.141      | 0.7979                | 0.177      |          |            | Surface |
| P10     | J12  | 2        | -0.420   | 0.311      | 0.7979                | 0.390      |          |            | Surface |
| P10     | J12  | 2        | -0.310   | 0.339      | 0.7979                | 0.425      | 0.243    | 0.30574    | Surface |
| P10     | J31  | 2        | -0.730   | 0.509      | 0.7979                | 0.638      |          |            | Interm  |
| P10     | J31  | 2        | 0.890    | 0.170      | 0.7979                | 0.213      |          |            | Interm  |
| P10     | J31  | 2        | 0.305    | 0.658      | 0.7979                | 0.824      |          |            | Interm  |
| P10     | J31  | 2        | -0.030   | 0.495      | 0.7979                | 0.620      |          |            | Interm  |
| P10     | J31  | 1        | 1.000    | -          | _                     | -          |          |            | Interm  |
| P10     | J31  | 2        | 0.425    | 0.672      | 0.7979                | 0.842      |          |            | Interm  |
| P10     | J31  | 2        | 0.275    | 0.092      | 0.7979                | 0.115      |          |            | Interm  |
| P10     | J31  | 1        | 0.900    | _          | _                     | -          |          |            | Interm  |
| P10     | J31  | 2        | 0.410    | 0.325      | 0.7979                | 0.408      |          |            | Interm  |
| P10     | J31  | 2        | 0.125    | 0.021      | 0.7979                | 0.027      |          |            | Interm  |

# Table B.6. Summary of Unbiased Lot Std Dev for VMA for Each Project (continued)

| Project | JMF    | I ot Size | l ot Mean | Lot St Dev | C 4    | Lot St Dev | Average  | Avg Lot SD | Course |
|---------|--------|-----------|-----------|------------|--------|------------|----------|------------|--------|
| Number  | Number |           | Lot moun  | (biased)   | C4     | (unbiased) | Lot Mean | Unbiased   |        |
| P10     | J31    | 2         | 0.790     | 0.156      | 0.7979 | 0.195      |          |            | Interm |
| P10     | J31    | 2         | 0.915     | 0.502      | 0.7979 | 0.629      |          |            | Interm |
| P10     | J31    | 2         | 0.815     | 0.148      | 0.7979 | 0.186      |          |            | Interm |
| P10     | J31    | 2         | 0.465     | 0.757      | 0.7979 | 0.948      |          |            | Interm |
| P10     | J31    | 2         | 0.645     | 0.643      | 0.7979 | 0.806      |          |            | Interm |
| P10     | J31    | 2         | 0.540     | 0.014      | 0.7979 | 0.018      |          |            | Interm |
| P10     | J31    | 2         | 0.590     | 0.665      | 0.7979 | 0.833      |          |            | Interm |
| P10     | J31    | 2         | 0.175     | 1.209      | 0.7979 | 1.515      |          |            | Interm |
| P10     | J31    | 2         | 0.015     | 0.544      | 0.7979 | 0.682      |          |            | Interm |
| P10     | J31    | 2         | 0.630     | 0.085      | 0.7979 | 0.106      |          |            | Interm |
| P10     | J31    | 2         | 0.070     | 1.259      | 0.7979 | 1.577      |          |            | Interm |
| P10     | J31    | 1         | 0.650     | -          | _      | —          |          |            | Interm |
| P10     | J31    | 2         | 0.160     | 0.764      | 0.7979 | 0.957      |          |            | Interm |
| P10     | J31    | 2         | -0.720    | 0.028      | 0.7979 | 0.035      |          |            | Interm |
| P10     | J31    | 2         | -0.730    | 0.509      | 0.7979 | 0.638      |          |            | Interm |
| P10     | J31    | 2         | 0.180     | 0.226      | 0.7979 | 0.284      |          |            | Interm |
| P10     | J31    | 1         | -0.420    | -          | _      | —          |          |            | Interm |
| P10     | J31    | 2         | -0.910    | 0.156      | 0.7979 | 0.195      |          |            | Interm |
| P10     | J31    | 2         | -0.610    | 0.622      | 0.7979 | 0.780      |          |            | Interm |
| P10     | J31    | 2         | 0.395     | 0.148      | 0.7979 | 0.186      |          |            | Interm |
| P10     | J31    | 2         | 0.100     | 0.184      | 0.7979 | 0.230      |          |            | Interm |
| P10     | J31    | 2         | 0.655     | 0.672      | 0.7979 | 0.842      |          |            | Interm |
| P10     | J31    | 2         | 0.200     | 1.089      | 0.7979 | 1.365      |          |            | Interm |
| P10     | J31    | 2         | 0.405     | 0.813      | 0.7979 | 1.019      |          |            | Interm |
| P10     | J31    | 2         | 0.775     | 0.276      | 0.7979 | 0.346      |          |            | Interm |
| P10     | J31    | 2         | 0.030     | 0.184      | 0.7979 | 0.230      |          |            | Interm |
| P10     | J31    | 2         | -0.530    | 0.495      | 0.7979 | 0.620      |          |            | Interm |
| P10     | J31    | 2         | 0.270     | 0.948      | 0.7979 | 1.188      |          |            | Interm |
| P10     | J31    | 2         | -0.220    | 0.354      | 0.7979 | 0.443      |          |            | Interm |
| P10     | J31    | 2         | 0.075     | 0.757      | 0.7979 | 0.948      |          |            | Interm |
| P10     | J31    | 1         | 0.370     | -          | -      | —          | 0.228    | 0.59696    | Interm |
| P10     | J37    | 1         | 0.870     | -          | _      | _          |          |            | Interm |
| P10     | J37    | 2         | -0.255    | 0.191      | 0.7979 | 0.239      |          |            | Interm |
| P10     | J37    | 2         | -0.175    | 0.092      | 0.7979 | 0.115      |          |            | Interm |
| P10     | J37    | 2         | 0.020     | 0.467      | 0.7979 | 0.585      |          |            | Interm |
| P10     | J37    | 2         | 0.190     | 0.962      | 0.7979 | 1.205      |          |            | Interm |
| P10     | J37    | 1         | 0.650     | -          | _      | _          |          |            | Interm |
| P10     | J37    | 2         | 0.755     | 0.163      | 0.7979 | 0.204      |          |            | Interm |
| P10     | J37    | 2         | 1.530     | 1.796      | 0.7979 | 2.251      |          |            | Interm |
| P10     | J37    | 2         | 0.655     | 0.346      | 0.7979 | 0.434      |          |            | Interm |
| P10     | J37    | 2         | 0.000     | 0.156      | 0.7979 | 0.195      |          |            | Interm |
| P10     | J37    | 2         | 0.875     | 0.007      | 0.7979 | 0.009      |          |            | Interm |
| P10     | J37    | 2         | 0.065     | 0.092      | 0.7979 | 0.115      | 0.432    | 0.53527    | Interm |
| P10     | J82    | 2         | -0.350    | 0.014      | 0.7979 | 0.018      |          |            | Interm |
| P10     | J82    | 2         | 0.375     | 0.643      | 0.7979 | 0.806      |          |            | Interm |
| P10     | J82    | 2         | 1.080     | 0.311      | 0.7979 | 0.390      |          |            | Interm |
| P10     | J82    | 2         | 1.125     | 0.163      | 0.7979 | 0.204      |          |            | Interm |

| Table B.6. Summary of Unbiased Lot | Std Dev for VMA for | or Each Project (continued) |
|------------------------------------|---------------------|-----------------------------|
|------------------------------------|---------------------|-----------------------------|

| Project | JMF  | Lot Size | Lot Mean | Lot St Dev | <i>c</i> <sub>4</sub> | Lot St Dev | Average  | Avg Lot SD | Course  |
|---------|------|----------|----------|------------|-----------------------|------------|----------|------------|---------|
| P10     | .182 | 2        | 0 380    | 0 170      | 0 7979                | 0.213      | Lot mean | Unblased   | Interm  |
| P10     | 182  | 1        | 1 010    |            | 0.7070                |            |          |            | Interm  |
| P10     | .182 | 2        | 1.010    | 0 177      | 0 7979                | 0.222      |          |            | Interm  |
| P10     | .182 | 2        | 0.500    | 0.354      | 0 7979                | 0.443      | 0.673    | 0.32790    | Interm  |
| P11     | .141 | 3        | 0.290    | 0.330      | 0.8862                | 0.372      | 0.010    | 0.02700    | Surface |
| P11     | .J41 | 1        | 0.290    | -          | -                     | -          |          |            | Surface |
| P11     | J41  | 2        | 0.250    | 0.410      | 0.7979                | 0.514      |          |            | Surface |
| P11     | J41  | 4        | 0.343    | 0.200      | 0.9213                | 0.218      | 0.293    | 0.36796    | Surface |
| P12     | J38  | 4        | -0.695   | 0.285      | 0.9213                | 0.309      |          |            | Surface |
| P12     | J38  | 2        | -1.085   | 0.417      | 0.7979                | 0.523      |          |            | Surface |
| P12     | J38  | 1        | -0.810   | _          | _                     | _          |          |            | Surface |
| P12     | J38  | 1        | -0.770   | _          | _                     | _          |          |            | Surface |
| P12     | J38  | 3        | -0.060   | 0.426      | 0.8862                | 0.480      |          |            | Surface |
| P12     | J38  | 3        | 0.120    | 0.977      | 0.8862                | 1.102      | -0.550   | 0.60363    | Surface |
| P13     | J03  | 3        | -0.553   | 0.190      | 0.8862                | 0.215      |          |            | Surface |
| P13     | J03  | 3        | -0.050   | 0.344      | 0.8862                | 0.388      |          |            | Surface |
| P13     | J03  | 1        | -0.160   | _          | _                     | _          |          |            | Surface |
| P13     | J03  | 3        | -0.013   | 0.380      | 0.8862                | 0.429      |          |            | Surface |
| P13     | J03  | 1        | -0.170   | _          | _                     | -          |          |            | Surface |
| P13     | J03  | 1        | -0.290   | _          | _                     | -          |          |            | Surface |
| P13     | J03  | 3        | 0.013    | 0.202      | 0.8862                | 0.228      |          |            | Surface |
| P13     | J03  | 1        | 1.010    | -          | -                     | -          | -0.027   | 0.31494    | Surface |
| P13     | J43  | 2        | 0.110    | 0.523      | 0.7979                | 0.656      |          |            | Surface |
| P13     | J43  | 2        | -0.220   | 0.806      | 0.7979                | 1.010      |          |            | Surface |
| P13     | J43  | 2        | -0.455   | 0.191      | 0.7979                | 0.239      |          |            | Surface |
| P13     | J43  | 2        | 0.375    | 0.191      | 0.7979                | 0.239      |          |            | Surface |
| P13     | J43  | 3        | 0.203    | 0.681      | 0.8862                | 0.768      |          |            | Surface |
| P13     | J43  | 4        | 0.083    | 0.440      | 0.9213                | 0.477      |          |            | Surface |
| P13     | J43  | 3        | 0.350    | 0.644      | 0.8862                | 0.727      |          |            | Surface |
| P13     | J43  | 1        | 1.330    | _          | _                     | —          | 0.222    | 0.58815    | Surface |
| P14     | J16  | 1        | -0.420   | _          | _                     | —          |          |            | Surface |
| P14     | J16  | 2        | -0.475   | 0.290      | 0.7979                | 0.363      |          |            | Surface |
| P14     | J16  | 3        | -1.227   | 0.550      | 0.8862                | 0.621      |          |            | Surface |
| P14     | J16  | 2        | 0.275    | 0.460      | 0.7979                | 0.576      |          |            | Surface |
| P14     | J16  | 1        | -0.320   | _          | -                     |            |          |            | Surface |
| P14     | J16  | 4        | -0.458   | 0.567      | 0.9213                | 0.616      |          |            | Surface |
| P14     | J16  | 3        | -0.700   | 0.087      | 0.8862                | 0.098      |          |            | Surface |
| P14     | J16  | 4        | -1.030   | 0.825      | 0.9213                | 0.896      |          |            | Surface |
| P14     | J16  | 4        | -0.845   | 0.527      | 0.9213                | 0.572      |          |            | Surface |
| P14     | J16  | 2        | -0.670   | 0.113      | 0.7979                | 0.142      |          |            | Surface |
| P14     | J16  | 1        | -1.250   | -          | -                     | -          |          |            | Surface |
| P14     | J16  | 2        | -0.675   | 0.163      | 0.7979                | 0.204      | 0.000    | 0.40.17.1  | Surface |
| P14     | J16  | 3        | -0.807   | 0.140      | 0.8862                | 0.158      | -0.662   | 0.42451    | Surface |
| P16     | J20  | 3        | -0.283   | 0.770      | 0.8862                | 0.869      |          |            | Surface |
| P16     | J20  | 3        | -0.120   | 0.355      | 0.8862                | 0.401      | 0.004    | 0.47005    | Surface |
| P16     | J20  | 3        | -0.300   | 0.149      | 0.8862                | 0.169      | -0.234   | 0.47925    | Surrace |
| P1/     | J22  | 2        | -0.430   | 0.057      | 0.7979                | 0.071      |          |            | Interm  |

| Table B.6. Summa | ry of Unbiased | Lot Std Dev for | VMA for Each | Project ( | (continued) |
|------------------|----------------|-----------------|--------------|-----------|-------------|
|------------------|----------------|-----------------|--------------|-----------|-------------|

| Project | JMF    | Lot Size | Lot Mean | Lot St Dev | <i>c</i> <sub>4</sub> | Lot St Dev | Average  | Avg Lot SD | Course    |
|---------|--------|----------|----------|------------|-----------------------|------------|----------|------------|-----------|
| Number  | Number | 0        | 0.020    | (blased)   | 0 7070                | (unblased) | Lot Mean | Unblased   | liatariaa |
|         | J22    | 2        | -0.930   | 0.196      | 0.7979                | 0.240      |          |            |           |
| P17     | J22    | 2        | -0.215   | 0.615      | 0.7979                | 0.771      |          |            |           |
|         | JZZ    | 1        | -0.700   | -          | -                     | -          |          |            |           |
| P17     | JZZ    | 2        | -0.495   | 0.926      | 0.7979                | 1.161      | 0.400    | 0.0004.0   | Interm    |
| P17     | J22    | 2        | -0.155   | 0.686      | 0.7979                | 0.860      | -0.488   | 0.62212    | Interm    |
| P18     | J48    | 1        | -0.110   | -          | -                     | -          |          |            | Surface   |
| P18     | J48    | 3        | -0.447   | 0.212      | 0.8862                | 0.239      |          |            | Surface   |
| P18     | J48    | 1        | -0.930   | -          | -                     | -          |          |            | Surface   |
| P18     | J48    | 2        | 0.145    | 0.064      | 0.7979                | 0.080      |          |            | Surface   |
| P18     | J48    | 3        | 0.067    | 0.767      | 0.8862                | 0.866      |          |            | Surface   |
| P18     | J48    | 1        | -0.130   | _          | _                     | _          | 0.044    | 0.00404    | Surface   |
| P18     | J48    | 1        | 1.330    | -          | -                     | -          | -0.011   | 0.39494    | Surface   |
| P19     | J49    | 2        | -0.015   | 0.078      | 0.7979                | 0.097      |          |            | Surface   |
| P19     | J49    | 1        | -0.210   | -          | -                     | -          |          |            | Surface   |
| P19     | J49    | 3        | -0.683   | 0.300      | 0.8862                | 0.338      |          |            | Surface   |
| P19     | J49    | 4        | -0.415   | 0.251      | 0.9213                | 0.273      |          |            | Surface   |
| P19     | J49    | 4        | -1.055   | 0.840      | 0.9213                | 0.912      |          |            | Surface   |
| P19     | J49    | 3        | -0.497   | 1.028      | 0.8862                | 1.160      | 0.540    | 0.40050    | Surface   |
| P19     | J49    | 3        | -0.713   | 0.155      | 0.8862                | 0.175      | -0.513   | 0.49258    | Surface   |
| P20     | J50    | 1        | -0.510   | -          | -                     | -          |          |            | Surface   |
| P20     | J50    | 5        | -0.724   | 0.151      | 0.9400                | 0.160      |          |            | Surface   |
| P20     | J50    | 2        | -0.735   | 0.247      | 0.7979                | 0.310      |          |            | Surface   |
| P20     | J50    | 4        | 0.025    | 0.139      | 0.9213                | 0.151      |          |            | Surface   |
| P20     | J50    | 1        | 0.190    | -          | -                     | _          |          |            | Surface   |
| P20     | J50    | 2        | 0.410    | 0.141      | 0.7979                | 0.177      |          |            | Surface   |
| P20     | J50    | 5        | 0.072    | 0.326      | 0.9400                | 0.347      |          |            | Surface   |
| P20     | J50    | 3        | -0.197   | 0.292      | 0.8862                | 0.329      |          |            | Surface   |
| P20     | J50    | 1        | 0.020    | -          | _                     | -          |          |            | Surface   |
| P20     | J50    | 1        | -0.360   | -          | -                     | _          |          |            | Surface   |
| P20     | J50    | 5        | -0.188   | 0.488      | 0.9400                | 0.520      |          |            | Surface   |
| P20     | J50    | 1        | -0.890   | -          | _                     | _          |          |            | Surface   |
| P20     | J50    | 2        | 0.080    | 0.552      | 0.7979                | 0.691      |          |            | Surface   |
| P20     | J50    | 4        | -0.328   | 0.347      | 0.9213                | 0.377      |          |            | Surface   |
| P20     | J50    | 5        | -0.166   | 0.490      | 0.9400                | 0.521      |          |            | Surface   |
| P20     | J50    | 2        | -0.280   | 0.127      | 0.7979                | 0.160      |          |            | Surface   |
| P20     | J50    | 2        | -0.030   | 0.057      | 0.7979                | 0.071      | -0.212   | 0.31784    | Surface   |
| P21     | J34    | 4        | 0.333    | 0.190      | 0.9213                | 0.206      |          |            | Interm    |
| P21     | J34    | 3        | 0.130    | 0.046      | 0.8862                | 0.052      |          |            | Interm    |
| P21     | J34    | 1        | 0.120    | -          | _                     | _          | 0.194    | 0.12896    | Interm    |
| P21     | J39    | 1        | -0.510   | -          | -                     | -          |          |            | Surface   |
| P21     | J39    | 4        | -0.568   | 0.029      | 0.9213                | 0.031      |          |            | Surface   |
| P21     | J39    | 2        | -0.585   | 0.035      | 0.7979                | 0.044      |          |            | Surface   |
| P21     | J39    | 4        | -0.800   | 0.272      | 0.9213                | 0.296      |          |            | Surface   |
| P21     | J39    | 3        | -0.900   | 0.289      | 0.8862                | 0.326      |          |            | Surface   |
| P21     | J39    | 1        | -0.680   | _          | _                     | -          | -0.674   | 0.17437    | Surface   |
| P22     | J54    | 6        | 0.078    | 1.029      | 0.9515                | 1.082      |          |            | Surface   |
| P22     | J54    | 5        | 0.280    | 0.338      | 0.9400                | 0.360      |          |            | Surface   |

| Table B.6. Summary of Unbiased Lot | Std Dev for VMA for | Each Project (continued) |
|------------------------------------|---------------------|--------------------------|
|------------------------------------|---------------------|--------------------------|

| Project<br>Number | JMF<br>Number | Lot Size | Lot Mean | Lot St Dev<br>(biased) | $c_4$  | Lot St Dev<br>(unbiased) | Average<br>Lot Mean | Avg Lot SD<br>Unbiased | Course  |
|-------------------|---------------|----------|----------|------------------------|--------|--------------------------|---------------------|------------------------|---------|
| P22               | J54           | 1        | 0.730    |                        | _      |                          | 0.363               | 0.72070                | Surface |
| P24               | J56           | 1        | 0.240    | _                      | _      | _                        | 0.000               | 0.1.201.0              | Surface |
| P24               | J56           | 5        | -0.232   | 0.623                  | 0.9400 | 0.662                    |                     |                        | Surface |
| P24               | J56           | 1        | -0.130   | _                      | _      | _                        |                     |                        | Surface |
| P24               | J56           | 3        | -0.373   | 0.042                  | 0.8862 | 0.047                    |                     |                        | Surface |
| P24               | J56           | 1        | -0.800   | _                      | _      | _                        |                     |                        | Surface |
| P24               | J56           | 3        | -0.220   | 0.053                  | 0.8862 | 0.060                    |                     |                        | Surface |
| P24               | J56           | 1        | -0.180   | _                      | _      | _                        |                     |                        | Surface |
| P24               | J56           | 1        | -0.370   | _                      | _      | _                        |                     |                        | Surface |
| P24               | J56           | 3        | -0.307   | 0.358                  | 0.8862 | 0.404                    |                     |                        | Surface |
| P24               | J56           | 1        | -0.460   | -                      | -      | _                        |                     |                        | Surface |
| P24               | J56           | 4        | -0.140   | 0.349                  | 0.9213 | 0.379                    |                     |                        | Surface |
| P24               | J56           | 2        | 0.520    | 0.141                  | 0.7979 | 0.177                    |                     |                        | Surface |
| P24               | J56           | 1        | 1.420    | _                      | _      | _                        |                     |                        | Surface |
| P24               | J56           | 3        | -0.333   | 0.555                  | 0.8862 | 0.626                    |                     |                        | Surface |
| P24               | J56           | 1        | -0.330   | _                      | _      | -                        |                     |                        | Surface |
| P24               | J56           | 2        | -0.305   | 0.035                  | 0.7979 | 0.044                    |                     |                        | Surface |
| P24               | J56           | 4        | -0.663   | 0.268                  | 0.9213 | 0.290                    |                     |                        | Surface |
| P24               | J56           | 3        | -0.113   | 1.003                  | 0.8862 | 1.131                    | -0.154              | 0.38212                | Surface |
| P24               | J64           | 1        | 0.000    | 1                      | I      | _                        |                     |                        | Surface |
| P24               | J64           | 2        | 0.010    | 0.382                  | 0.7979 | 0.479                    |                     |                        | Surface |
| P24               | J64           | 2        | -0.375   | 0.021                  | 0.7979 | 0.027                    |                     |                        | Surface |
| P24               | J64           | 2        | 0.055    | 0.247                  | 0.7979 | 0.310                    |                     |                        | Surface |
| P24               | J64           | 2        | -0.525   | 0.007                  | 0.7979 | 0.009                    |                     |                        | Surface |
| P24               | J64           | 2        | -0.185   | 0.134                  | 0.7979 | 0.168                    |                     |                        | Surface |
| P24               | J64           | 2        | -0.360   | 0.127                  | 0.7979 | 0.160                    | -0.197              | 0.19201                | Surface |
| P24               | J67           | 1        | -0.040   | -                      | -      | —                        |                     |                        | Surface |
| P24               | J67           | 1        | 0.030    | -                      | -      | —                        |                     |                        | Surface |
| P24               | J67           | 1        | -0.810   | _                      | _      | -                        |                     |                        | Surface |
| P24               | J67           | 2        | -0.660   | 0.269                  | 0.7979 | 0.337                    |                     |                        | Surface |
| P24               | J67           | 3        | -0.340   | 0.510                  | 0.8862 | 0.576                    |                     |                        | Surface |
| P24               | J67           | 2        | -0.190   | 0.679                  | 0.7979 | 0.851                    | -0.335              | 0.58778                | Surface |
| P25               | J29           | 2        | 0.445    | 0.771                  | 0.7979 | 0.966                    |                     |                        | Interm  |
| P25               | J29           | 2        | 0.645    | 0.120                  | 0.7979 | 0.151                    |                     |                        | Interm  |
| P25               | J29           | 2        | 0.740    | 0.481                  | 0.7979 | 0.603                    |                     |                        | Interm  |
| P25               | J29           | 2        | 0.010    | 0.071                  | 0.7979 | 0.089                    |                     |                        | Interm  |
| P25               | J29           | 1        | -0.440   | _                      | -      | -                        |                     |                        | Interm  |
| P25               | J29           | 2        | 0.695    | 0.163                  | 0.7979 | 0.204                    |                     |                        | Interm  |
| P25               | J29           | 1        | 0.620    | _                      | -      | -                        | 0.388               | 0.40234                | Interm  |
| P25               | J36           | 1        | 0.870    | -                      | -      | -                        |                     |                        | Surface |
| P25               | J36           | 2        | -0.320   | 0.919                  | 0.7979 | 1.152                    |                     |                        | Surface |
| P25               | J36           | 3        | 0.857    | 0.690                  | 0.8862 | 0.778                    |                     |                        | Surface |
| P25               | J36           | 2        | 1.365    | 0.403                  | 0.7979 | 0.505                    |                     |                        | Surface |
| P25               | J36           | 1        | 0.510    | -                      | -      | -                        |                     |                        | Surface |
| P25               | J36           | 1        | 0.960    | -                      | -      | -                        | 0.707               | 0.81181                | Surface |
| P26               | J58           | 1        | -0.420   | -                      | -      | -                        |                     |                        | Surface |
| P26               | J58           | 1        | -0.240   | —                      | —      | -                        |                     |                        | Surface |

# Table B.6. Summary of Unbiased Lot Std Dev for VMA for Each Project (continued)
| Number         Partial State         Charace         Charace | Project | JMF    | Lot Size | Lot Mean | Lot St Dev | C4     | Lot St Dev | Average  | Avg Lot SD | Course  |
|--|---------|--------|----------|----------|------------|--------|------------|----------|------------|---------|
| P26         J36         1         0.370         -         -         -         -         Surface           P26         J58         1         0.470         -         -         -         Surface           P26         J58         1         0.420         -         -         -         Surface           P26         J58         1         0.400         -         -         -         Surface           P26         J58         1         0.050         -         -         -         Surface           P26         J58         1         0.050         -         -         -         Surface           P26         J58         1         0.050         -         -         -         0.200         0.6823         Surface           P26         J62         4         0.0610         0.213         0.477         Surface         Surface           P26         J62         3         0.626         0.8862         0.707         Surface           P26         J62         3         0.610         0.423         0.8623         0.717         Surface           P26         J62         3         0.613         0.228  | Doc     | Number | 1        | 0.270    | (blased)   | •      | (unbiased) | Lot Mean | Unblased   | Surface |
| P26         J58         1         0.380         -         -         -         -         Surface           P26         J58         1         0.320         -         -         -         Surface           P26         J58         1         0.400         -         -         -         Surface           P26         J58         1         0.050         -         -         -         Surface           P26         J58         1         0.020         -         -         -         Surface           P26         J58         1         0.090         -         -         -         Surface           P26         J58         1         0.950         -         -         -         0.220         0.6823         Surface           P26         J62         4         0.610         0.421         0.9213         0.477         Surface           P26         J62         3         0.623         0.227         Surface         Surface           P26         J62         3         0.623         0.237         0.242         0.862         0.273         Surface           P26         J62         3         0.607 </td <td>P20</td> <td>J20</td> <td>1</td> <td>0.370</td> <td>_</td> <td></td> <td></td> <td></td> <td></td> <td>Sunace</td>  | P20     | J20    | 1        | 0.370    | _          |        |            |          |            | Sunace  |
| P26         J38         1         -0.470         -         -         -         Surface           P26         J58         1         0.400         -         -         -         Surface           P26         J58         1         0.050         -         -         -         Surface           P26         J58         1         0.020         -         -         -         Surface           P26         J58         1         0.020         -         -         -         Surface           P26         J58         1         0.950         -         -         -         0.220         0.6823         Surface           P26         J62         4         0.095         0.440         0.9213         0.477         Surface           P26         J62         3         0.237         0.242         0.8862         0.707         Surface           P26         J62         3         0.620         0.8862         0.707         Surface           P26         J62         3         0.610         0.8862         0.463         Surface           P26         J62         4         0.243         0.238         0.89213  | P20     | J28    | 1        | 0.380    | -          | _      | _          |          |            | Surface |
| P26         J38         1         0.320         -         -         -         -         Surface           P26         J58         1         0.050         -         -         -         Surface           P26         J58         1         0.020         -         -         -         Surface           P26         J58         1         0.080         -         -         -         Surface           P26         J58         1         0.950         -         -         -         0.220         0.68238         Surface           P26         J62         4         0.095         0.440         0.9213         0.457         Surface           P26         J62         3         0.423         0.2213         0.457         Surface           P26         J62         3         0.623         0.6862         0.273         Surface           P26         J62         3         0.623         0.6862         0.202         Surface           P26         J62         3         0.613         0.129         0.8862         0.403         Surface           P26         J62         3         0.513         0.129         0.8   | P20     | J28    | 1        | -0.470   | -          | -      | _          |          |            | Surface |
| P26         J38         1         0.400         -         -         -         -         Surface           P26         J58         1         0.120         -         -         -         Surface           P26         J58         1         0.080         -         -         -         Surface           P26         J58         1         0.080         -         -         -         Octobe           P26         J58         1         0.950         -         -         -         0.220         0.68238         Surface           P26         J62         4         -0.095         0.440         0.9213         0.4477         Surface           P26         J62         3         0.423         0.282         0.707         Surface           P26         J62         3         0.693         0.410         0.8862         0.707         Surface           P26         J62         3         0.613         0.129         0.8862         0.463         Surface           P26         J62         4         0.243         0.238         0.9213         0.571         Surface           P26         J62         4         0.2   | P20     | J28    | 1        | 0.320    | -          | -      | _          |          |            | Surface |
| P26         J38         1         0.030         -         -         -         -         Surface           P26         J58         1         0.080         -         -         -         Surface           P26         J58         1         0.080         -         -         -         Surface           P26         J58         1         0.950         -         -         -         0.220         0.68238         Surface           P26         J62         4         0.610         0.421         0.9213         0.477         Surface           P26         J62         3         0.423         0.826         0.273         Surface           P26         J62         3         0.423         0.8662         0.707         Surface           P26         J62         3         0.663         0.410         0.8862         0.463         Surface           P26         J62         3         0.613         0.129         0.8862         0.461         Surface           P26         J62         4         0.243         0.238         0.3862         0.366         0.39487         Surface           P26         J69         3   | P26     | J58    | 1        | 0.400    | -          | _      | _          |          |            | Surface |
| P26         J38         1         0.120         -         -         -         Surface           P26         J58         1         0.080         -         -         -         0.220         0.6823         Surface           P26         J58         1         0.950         -         -         -         0.220         0.6823         Surface           P26         J62         4         0.095         0.440         0.9213         0.477         Surface           P26         J62         3         0.623         0.423         0.8862         0.273         Surface           P26         J62         3         0.607         0.179         0.8862         0.202         Surface           P26         J62         3         0.607         0.179         0.8862         0.403         Surface           P26         J62         4         0.068         0.9213         0.571         Surface           P26         J62         4         0.238         0.9213         0.258         0.366         0.39487         Surface           P26         J69         3         0.0137         0.068         0.8862         0.017         Surface <t< td=""><td>P20</td><td>J28</td><td>1</td><td>0.050</td><td>-</td><td>-</td><td></td><td></td><td></td><td>Surface</td></t<>   | P20     | J28    | 1        | 0.050    | -          | -      |            |          |            | Surface |
| P26         J38         1         0.080         -         -         -         -         Surface           P26         J58         1         0.950         -         -         -         0.6823         Surface           P26         J52         4         0.0950         -         -         -         0.220         0.68238         Surface           P26         J62         4         0.610         0.421         0.9213         0.477         Surface           P26         J62         3         0.237         0.242         0.8862         0.273         Surface           P26         J62         3         0.607         0.179         0.8862         0.202         Surface           P26         J62         3         0.663         0.410         0.8862         0.202         Surface           P26         J62         3         0.663         0.410         0.8862         0.203         Surface           P26         J62         3         0.513         0.129         0.8862         0.463         Surface           P26         J69         3         0.137         0.028         0.9213         0.476         Surface   | P20     | J28    | 1        | 0.120    | -          | -      |            |          |            | Surface |
| P26         J58         2         1.105         0.544         0.1979         0.682         Surface           P26         J62         4         -0.095         0.440         0.9213         0.477         Surface           P26         J62         4         -0.095         0.440         0.9213         0.457         Surface           P26         J62         3         0.237         0.2421         0.8662         0.273         Surface           P26         J62         3         0.423         0.626         0.8862         0.202         Surface           P26         J62         3         0.607         0.179         0.8862         0.463         Surface           P26         J62         4         0.068         0.526         0.9213         0.571         Surface           P26         J62         4         0.0433         0.439         0.571         Surface           P26         J62         4         0.243         0.238         0.9213         0.268         0.366         0.39487         Surface           P26         J69         3         -0.137         0.8862         0.177         Surface           P26         J69  | P26     | J58    | 1        | 0.080    | -          | -      | -          |          |            | Surface |
| P26         J36         1         0.90         -         -         -         0.20         0.6236         Surface           P26         J62         4         0.610         0.421         0.9213         0.457         Surface           P26         J62         3         0.237         0.242         0.8862         0.273         Surface           P26         J62         3         0.607         0.179         0.8862         0.202         Surface           P26         J62         3         0.603         0.410         0.8862         0.463         Surface           P26         J62         3         0.663         0.526         0.9213         0.571         Surface           P26         J62         4         0.243         0.238         0.9213         0.576         Surface           P26         J62         4         0.243         0.238         0.9213         0.476         Surface           P26         J69         3         -0.137         0.068         0.8862         0.177         Surface           P26         J69         3         -0.107         0.926         0.8862         0.107         Surface           P26  | P26     | J58    | 2        | 1.105    | 0.544      | 0.7979 | 0.682      | 0.000    | 0.00000    | Surface |
| P26         J62         4         -0.093         0.1440         0.9213         0.477         SUrface           P26         J62         3         0.237         0.242         0.8862         0.273         Surface           P26         J62         3         0.423         0.626         0.8862         0.707         Surface           P26         J62         3         0.603         0.410         0.8862         0.202         Surface           P26         J62         3         0.603         0.410         0.8862         0.463         Surface           P26         J62         4         0.068         0.526         0.9213         0.571         Surface           P26         J62         4         0.0243         0.238         0.9213         0.476         Surface           P26         J69         4         0.438         0.439         0.9213         0.476         Surface           P26         J69         3         -0.137         0.068         0.8862         0.077         Surface           P26         J69         3         -0.107         0.4421         0.8862         0.476         Surface           P26         J69  | P20     | 100    | 1        | 0.950    | -          | -      | -          | 0.220    | 0.68238    | Surface |
| P26         J62         4         0.610         0.421         0.9213         0.437         Sufface           P26         J62         3         0.423         0.626         0.8862         0.273         Surface           P26         J62         3         0.607         0.179         0.8862         0.202         Surface           P26         J62         3         0.693         0.410         0.8862         0.202         Surface           P26         J62         4         0.068         0.526         0.9213         0.571         Surface           P26         J62         4         0.243         0.238         0.9213         0.476         Surface           P26         J69         4         0.438         0.439         0.9213         0.476         Surface           P26         J69         3         -0.137         0.068         0.8862         0.077         Surface           P26         J69         3         -0.107         0.421         0.8862         0.476         Surface           P26         J69         3         -0.107         0.421         0.8862         0.515         Surface           P26         J69 <t< td=""><td>P20</td><td>J02</td><td>4</td><td>-0.095</td><td>0.440</td><td>0.9213</td><td>0.477</td><td></td><td></td><td>Surface</td></t<>   | P20     | J02    | 4        | -0.095   | 0.440      | 0.9213 | 0.477      |          |            | Surface |
| P26         J62         J63         J513         J129         J8862         J146         Surface           P26         J62         4         0.243         0.238         0.9213         0.476         Surface           P26         J69         3         -0.137         0.068         0.8862         0.077         Surface           P26         J69         3         -0.107         0.421         0.8862         0.476         Surface           P26         J69         3         -0.100         0.456         0.8862         0.515         Surface           P26         J69         3         -0.163         0.  | P20     | J02    | 4        | 0.010    | 0.421      | 0.9213 | 0.457      |          |            | Surface |
| P26         J62         J63         J13         D.253         D.2713         D.356         D.366         D.39487         Surface           P26         J69         4         0.438         0.439         0.9213         0.476         Surface           P26         J69         3         -0.137         0.068         0.8862         0.476         Surface           P26         J69         3         -0.107         0.421         0.8862         0.515         Surface           P26         J69         3         -0.107         0.946         0.8862         0.077         Surface           P26  | P20     | J02    | <u> </u> | 0.237    | 0.242      | 0.0002 | 0.273      |          |            | Surface |
| P26         J62         3         0.607         0.179         0.8662         0.202         Surface           P26         J62         4         0.068         0.526         0.9213         0.571         Surface           P26         J62         4         0.243         0.238         0.9213         0.571         Surface           P26         J62         4         0.243         0.238         0.9213         0.258         0.366         0.39487         Surface           P26         J69         4         0.438         0.439         0.9213         0.476         Surface           P26         J69         3         -0.137         0.068         0.8862         0.476         Surface           P26         J69         3         -0.177         0.421         0.8862         0.476         Surface           P26         J69         3         -0.107         0.426         0.8862         0.515         Surface           P26         J69         3         -0.100         0.456         0.8862         0.077         Surface           P26         J69         3         -0.163         0.6862         0.077         Surface           P26   | P20     | J02    | <u> </u> | 0.423    | 0.020      | 0.0002 | 0.707      |          |            | Surface |
| P26         J62         3         0.683         0.440         0.6862         0.463         Surface           P26         J62         3         0.513         0.129         0.8862         0.146         Surface           P26         J62         4         0.243         0.238         0.9213         0.571         Surface           P26         J69         4         0.438         0.439         0.9213         0.476         Surface           P26         J69         3         -0.137         0.068         0.8862         0.077         Surface           P26         J69         3         -0.137         0.068         0.8862         0.476         Surface           P26         J69         3         -0.107         0.9421         0.8862         0.476         Surface           P26         J69         3         -0.107         0.966         0.8862         0.173         Surface           P26         J69         3         -0.100         0.456         0.8862         0.773         Surface           P26         J69         3         -0.163         0.8862         0.077         Surface           P26         J69         3 <t< td=""><td>P20</td><td>J02</td><td><u> </u></td><td>0.607</td><td>0.179</td><td>0.0002</td><td>0.202</td><td></td><td></td><td>Surface</td></t<>                                     | P20     | J02    | <u> </u> | 0.607    | 0.179      | 0.0002 | 0.202      |          |            | Surface |
| P26         J62         4         0.080         0.326         0.9213         0.371         Surface           P26         J62         3         0.513         0.129         0.8862         0.146         Surface           P26         J69         4         0.438         0.439         0.9213         0.476         Surface           P26         J69         3         -0.137         0.068         0.8862         0.077         Surface           P26         J69         3         -0.137         0.068         0.8862         0.476         Surface           P26         J69         3         0.017         0.421         0.8862         0.476         Surface           P26         J69         3         0.017         0.421         0.8862         0.108         Surface           P26         J69         3         -0.100         0.456         0.8862         0.173         Surface           P26         J69         3         -0.163         0.068         0.8862         0.077         Surface           P26         J69         3         -0.163         0.4862         0.6505         Surface           P26         J69         3 <td< td=""><td>P20</td><td>J02</td><td>3</td><td>0.093</td><td>0.410</td><td>0.0002</td><td>0.463</td><td></td><td></td><td>Surface</td></td<>   | P20     | J02    | 3        | 0.093    | 0.410      | 0.0002 | 0.463      |          |            | Surface |
| P26         J62         3         0.313         0.123         0.3602         0.146         Surface           P26         J69         4         0.238         0.9213         0.258         0.366         0.39487         Surface           P26         J69         3         -0.137         0.068         0.8862         0.077         Surface           P26         J69         3         -0.360         0.381         0.8862         0.476         Surface           P26         J69         3         -0.107         0.421         0.8862         0.476         Surface           P26         J69         3         -0.100         0.426         0.8862         0.476         Surface           P26         J69         3         -0.100         0.456         0.8862         0.515         Surface           P26         J69         3         -0.163         0.4862         0.677         Surface           P26         J69         3         -0.163         0.448         0.8862         0.695         Surface           P26         J69         3         1.123         0.350         0.8862         0.393         Surface           P26         J69   | P20     | J02    | 4        | 0.000    | 0.520      | 0.9213 | 0.571      |          |            | Surface |
| P26       J69       4       0.243       0.236       0.3213       0.2476       0.306       0.3940       Surface         P26       J69       3       -0.137       0.068       0.8862       0.077       Surface         P26       J69       3       -0.137       0.068       0.8862       0.430       Surface         P26       J69       3       0.017       0.421       0.8862       0.476       Surface         P26       J69       3       0.017       0.421       0.8862       0.476       Surface         P26       J69       3       -0.100       0.456       0.8862       0.108       Surface         P26       J69       3       -0.107       0.153       0.8862       0.773       Surface         P26       J69       3       -0.163       0.448       0.8862       0.505       Surface         P26       J69       4       0.423       0.171       0.9213       0.186       Surface         P26       J69       4       0.600       0.362       0.9213       0.393       Surface         P26       J69       3       -0.103       0.448       0.8862       0.51       Surfac   | P26     | 162    | 3        | 0.013    | 0.129      | 0.0002 | 0.140      | 0.266    | 0.20497    | Surface |
| P26       J69       4       0.438       0.439       0.9213       0.476       Surface         P26       J69       3       -0.137       0.068       0.8862       0.077       Surface         P26       J69       3       -0.360       0.381       0.8862       0.430       Surface         P26       J69       3       0.017       0.421       0.8862       0.476       Surface         P26       J69       3       -0.107       0.096       0.8862       0.108       Surface         P26       J69       3       -0.100       0.456       0.8862       0.515       Surface         P26       J69       3       -0.197       0.153       0.8862       0.077       Surface         P26       J69       3       -0.163       0.448       0.8862       0.077       Surface         P26       J69       3       -0.163       0.448       0.8862       0.505       Surface         P26       J69       3       -0.163       0.448       0.8862       0.395       Surface         P26       J69       3       -0.103       0.045       0.8862       0.395       Surface         P26<   | P20     | 160    | 4        | 0.243    | 0.230      | 0.9213 | 0.236      | 0.300    | 0.39407    | Surface |
| P26         J69         3         -0.137         0.086         0.8862         0.017         Surface           P26         J69         3         -0.360         0.381         0.8862         0.430         Surface           P26         J69         3         0.017         0.096         0.8862         0.476         Surface           P26         J69         3         -0.100         0.456         0.8862         0.103         Surface           P26         J69         3         -0.100         0.456         0.8862         0.173         Surface           P26         J69         3         -0.163         0.486         0.8862         0.077         Surface           P26         J69         3         -0.163         0.448         0.8862         0.505         Surface           P26         J69         3         -0.130         0.448         0.8862         0.505         Surface           P26         J69         3         -0.130         0.448         0.8862         0.395         Surface           P26         J69         3         -0.103         0.045         0.8862         0.051         Surface           P26         J69   | P20     | 160    | 4        | 0.430    | 0.439      | 0.9213 | 0.470      |          |            | Surface |
| P26       J69       3       0.017       0.421       0.8862       0.476       Surface         P26       J69       3       0.017       0.421       0.8862       0.108       Surface         P26       J69       3       -0.100       0.456       0.8862       0.103       Surface         P26       J69       3       -0.197       0.153       0.8862       0.077       Surface         P26       J69       3       -0.163       0.448       0.8862       0.077       Surface         P26       J69       3       -0.163       0.448       0.8862       0.505       Surface         P26       J69       4       0.423       0.171       0.9213       0.186       Surface         P26       J69       4       0.600       0.362       0.395       Surface         P26       J69       3       -0.103       0.045       0.8862       0.051       Surface         P26       J69       3       -0.003       0.257       0.8862       0.290       Surface         P26       J69       3       0.200       0.161       0.8862       0.352       Surface         P26       J69  | P20     | 160    | 2        | -0.137   | 0.000      | 0.0002 | 0.077      |          |            | Surface |
| P26       J69       3       0.017       0.921       0.0022       0.170       0.0022       0.170       0.0022       0.170       0.0022       0.170       0.0022       0.170       0.0022       0.170       0.0022       0.170       0.0022       0.170       0.0022       0.170       0.0022       0.170       0.163       0.002       0.171       0.002       0.171       0.002       0.171       0.002       0.171       0.0183       0.002       0.1713       0.0174       0.0173       0.0174       0.0173       0.0174       0.0174       0.0173       0.0174       0.0174       0.0173       0.0174       0.0173       0.0174       0.0173       0.0174       0.0173       0.0174       0.0173       0.0174       0.0173       0.0174       0.0173       0.0174       0.0173       0.0174       0.0173       0.0174       0.0173       0.0174       0.0173       0.0174       0.0173       0.0174       0.0173       0.0174       0.0173       0.0174       0.0173       0.0174       0.0173       0.0174       0.0174       0.0173       0.0174       0.0174       0.0174       0.0174       0.0174       0.0174       0.0174       0.0174       0.0174       0.0174       0.0174       0.0174       0.0174       0.   | P26     | 160    | 3        | -0.300   | 0.301      | 0.0002 | 0.430      |          |            | Surface |
| P26       J69       3       -0.100       0.456       0.8862       0.115       Surface         P26       J69       3       -0.107       0.153       0.8862       0.173       Surface         P26       J69       3       -0.163       0.068       0.8862       0.077       Surface         P26       J69       3       -0.163       0.448       0.8862       0.505       Surface         P26       J69       4       0.423       0.171       0.9213       0.186       Surface         P26       J69       3       1.123       0.350       0.8862       0.395       Surface         P26       J69       3       -0.103       0.045       0.8862       0.393       Surface         P26       J69       3       -0.103       0.045       0.8862       0.051       Surface         P26       J69       3       -0.003       0.257       0.8862       0.051       Surface         P26       J69       3       0.320       0.312       0.8862       0.182       Surface         P26       J69       1       0.600       -       -       -       Surface         P26   | P26     | 160    | 3        | 0.017    | 0.421      | 0.0002 | 0.470      |          |            | Surface |
| P26       J69       3       -0.197       0.153       0.8862       0.173       Surface         P26       J69       3       -0.163       0.068       0.8862       0.077       Surface         P26       J69       3       -0.163       0.448       0.8862       0.077       Surface         P26       J69       4       0.423       0.171       0.9213       0.186       Surface         P26       J69       4       0.423       0.171       0.9213       0.393       Surface         P26       J69       4       0.600       0.362       0.9213       0.393       Surface         P26       J69       3       -0.103       0.045       0.8862       0.051       Surface         P26       J69       3       -0.093       0.257       0.8862       0.290       Surface         P26       J69       3       0.020       0.161       0.8862       0.182       Surface         P26       J69       3       0.320       0.312       0.8862       0.352       Surface         P26       J69       1       0.600       -       -       -       O.208       0.29281       Surface </td <td>P26</td> <td>160</td> <td>3</td> <td>-0.107</td> <td>0.090</td> <td>0.0002</td> <td>0.100</td> <td></td> <td></td> <td>Surface</td>  | P26     | 160    | 3        | -0.107   | 0.090      | 0.0002 | 0.100      |          |            | Surface |
| P26       J69       3       0.163       0.068       0.8862       0.077       Surface         P26       J69       3       -0.163       0.448       0.8862       0.505       Surface         P26       J69       4       0.423       0.171       0.9213       0.186       Surface         P26       J69       4       0.423       0.171       0.9213       0.395       Surface         P26       J69       3       1.123       0.350       0.8862       0.395       Surface         P26       J69       3       -0.103       0.045       0.8862       0.051       Surface         P26       J69       3       -0.033       0.257       0.8862       0.290       Surface         P26       J69       3       -0.033       0.257       0.8862       0.182       Surface         P26       J69       3       0.320       0.312       0.8862       0.352       Surface         P26       J69       1       0.600       -       -       -       O.208       0.29281       Surface         P26       J69       1       1.080       -       -       -       O.208       0.29281   | P26     | 169    | 3        | -0.100   | 0.450      | 0.0002 | 0.313      |          |            | Surface |
| P26       J69       3       -0.163       0.300       0.3002       0.505       Surface         P26       J69       4       0.423       0.171       0.9213       0.186       Surface         P26       J69       3       1.123       0.350       0.8862       0.395       Surface         P26       J69       3       1.123       0.350       0.8862       0.395       Surface         P26       J69       4       0.600       0.362       0.9213       0.393       Surface         P26       J69       3       -0.103       0.045       0.8862       0.051       Surface         P26       J69       3       -0.093       0.257       0.8862       0.290       Surface         P26       J69       3       0.200       0.161       0.8862       0.352       Surface         P26       J69       1       0.600       -       -       -       Surface         P26       J69       1       0.600       -       -       -       Surface         P26       J69       1       0.600       -       -       -       -       Surface         P27       J53   | P26     | 169    | 3        | 0.163    | 0.155      | 0.8862 | 0.173      |          |            | Surface |
| P26       J69       4       0.423       0.171       0.9213       0.186       Surface         P26       J69       3       1.123       0.350       0.8862       0.395       Surface         P26       J69       4       0.600       0.362       0.9213       0.393       Surface         P26       J69       4       0.600       0.362       0.9213       0.393       Surface         P26       J69       3       -0.103       0.045       0.8862       0.051       Surface         P26       J69       3       -0.093       0.257       0.8862       0.290       Surface         P26       J69       3       0.020       0.161       0.8862       0.352       Surface         P26       J69       3       0.320       0.312       0.8862       0.352       Surface         P26       J69       1       0.600       -       -       -       0.208       0.29281       Surface         P26       J69       1       1.080       -       -       -       0.208       0.29281       Surface         P27       J53       1       -0.700       -       -       -       Int   | P26     | 169    | 3        | -0.163   | 0.000      | 0.8862 | 0.505      |          |            | Surface |
| P26       J69       3       1.123       0.350       0.8862       0.395       Surface         P26       J69       4       0.600       0.362       0.9213       0.393       Surface         P26       J69       4       0.600       0.362       0.9213       0.393       Surface         P26       J69       3       -0.103       0.045       0.8862       0.051       Surface         P26       J69       3       -0.093       0.257       0.8862       0.290       Surface         P26       J69       3       0.020       0.161       0.8862       0.182       Surface         P26       J69       3       0.320       0.312       0.8862       0.352       Surface         P26       J69       1       0.600       -       -       -       Surface         P26       J69       1       0.600       -       -       -       Surface         P26       J69       1       0.600       -       -       -       -       Surface         P27       J53       1       -0.710       -       -       -       Interm         P27       J53       1   | P26     | 169    | 1        | 0.103    | 0.440      | 0.0002 | 0.305      |          |            | Surface |
| P26       J69       4       0.600       0.362       0.9213       0.393       Surface         P26       J69       3       -0.103       0.045       0.8862       0.051       Surface         P26       J69       3       -0.093       0.257       0.8862       0.290       Surface         P26       J69       3       -0.093       0.257       0.8862       0.290       Surface         P26       J69       3       0.020       0.161       0.8862       0.352       Surface         P26       J69       3       0.320       0.312       0.8862       0.352       Surface         P26       J69       1       0.600       -       -       -       O.208       0.29281       Surface         P26       J69       1       0.600       -       -       -       O.208       0.29281       Surface         P27       J53       1       -0.710       -       -       -       Interm         P27       J53       1       -0.100       -       -       -       Interm         P27       J53       1       -0.350       -       -       -       Interm <t< td=""><td>P26</td><td>169</td><td></td><td>1 1 2 3</td><td>0.171</td><td>0.3213</td><td>0.100</td><td></td><td></td><td>Surface</td></t<>   | P26     | 169    |          | 1 1 2 3  | 0.171      | 0.3213 | 0.100      |          |            | Surface |
| P26       J69       3       -0.103       0.045       0.8862       0.051       Surface         P26       J69       3       -0.093       0.257       0.8862       0.290       Surface         P26       J69       3       -0.093       0.257       0.8862       0.290       Surface         P26       J69       3       0.020       0.161       0.8862       0.182       Surface         P26       J69       3       0.320       0.312       0.8862       0.352       Surface         P26       J69       1       0.600       -       -       -       Surface         P26       J69       1       0.600       -       -       -       Surface         P26       J69       1       1.080       -       -       -       0.208       0.29281       Surface         P27       J53       1       -0.710       -       -       -       Interm         P27       J53       1       -0.730       -       -       -       Interm         P27       J53       1       0.120       -       -       -       Interm         P27       J53       1   | P26     |        | 4        | 0.600    | 0.362      | 0.0002 | 0.393      |          |            | Surface |
| P26       J69       3       -0.093       0.257       0.8862       0.290       Surface         P26       J69       3       0.020       0.161       0.8862       0.182       Surface         P26       J69       3       0.320       0.312       0.8862       0.352       Surface         P26       J69       1       0.600       -       -       -       Surface         P26       J69       1       0.600       -       -       -       Surface         P26       J69       1       0.600       -       -       -       Surface         P26       J69       1       1.080       -       -       -       Surface         P27       J53       1       -0.710       -       -       -       Interm         P27       J53       1       -0.100       -       -       -       Interm         P27       J53       1       -0.350       -       -       -       Interm         P27       J53       1       0.120       -       -       -       Interm         P27       J53       1       0.020       -       -       -   | P26     |        | 3        | -0.103   | 0.002      | 0.8862 | 0.050      |          |            | Surface |
| P26       J69       3       0.020       0.161       0.8862       0.182       Surface         P26       J69       3       0.320       0.312       0.8862       0.352       Surface         P26       J69       1       0.600       -       -       -       Surface         P26       J69       1       0.600       -       -       -       Surface         P26       J69       1       1.080       -       -       -       0.208       0.29281       Surface         P27       J53       1       -0.710       -       -       -       0.208       0.29281       Surface         P27       J53       1       -0.710       -       -       -       0.208       0.29281       Surface         P27       J53       1       -0.700       -       -       -       Interm         P27       J53       1       -0.100       -       -       -       Interm         P27       J53       1       -0.350       -       -       -       Interm         P27       J53       1       0.120       -       -       -       -       Interm   | P26     |        | 3        | -0.093   | 0.040      | 0.8862 | 0.290      |          |            | Surface |
| P26       J69       3       0.320       0.312       0.8862       0.352       Surface         P26       J69       1       0.600       -       -       -       Surface         P26       J69       1       0.600       -       -       -       Surface         P26       J69       1       1.080       -       -       -       0.208       0.29281       Surface         P27       J53       1       -0.710       -       -       -       Interm         P27       J53       1       -0.700       -       -       -       Interm         P27       J53       1       -0.730       -       -       -       Interm         P27       J53       1       -0.350       -       -       -       Interm         P27       J53       1       0.120       -       -       -       Interm         P27       J53       1       0.120       -       -       -       Interm         P27       J53       1       0.020       -       -       -       Interm         P27       J53       1       0.120       -       -  | P26     | .169   | 3        | 0.020    | 0.161      | 0.8862 | 0.182      |          |            | Surface |
| P26       J69       1       0.600       -       -       -       Surface         P26       J69       1       0.600       -       -       -       0.208       0.29281       Surface         P27       J53       1       -0.710       -       -       -       0.208       0.29281       Surface         P27       J53       1       -0.710       -       -       -       0.208       0.29281       Surface         P27       J53       1       -0.710       -       -       -       -       Interm         P27       J53       1       -0.100       -       -       -       -       Interm         P27       J53       1       -0.100       -       -       -       -       Interm         P27       J53       1       -0.730       -       -       -       -       Interm         P27       J53       1       0.120       -       -       -       -       Interm         P27       J53       1       0.020       -       -       -       -       Interm         P27       J53       1       0.120       - <t< td=""><td>P26</td><td>.169</td><td>3</td><td>0.320</td><td>0.312</td><td>0.8862</td><td>0.352</td><td></td><td></td><td>Surface</td></t<>  | P26     | .169   | 3        | 0.320    | 0.312      | 0.8862 | 0.352      |          |            | Surface |
| P26       J69       1       1.080       -       -       -       0.208       0.29281       Surface         P27       J53       1       -0.710       -       -       -       -       0.208       0.29281       Surface         P27       J53       1       -0.710       -       -       -       -       Interm         P27       J53       1       -0.100       -       -       -       -       Interm         P27       J53       1       -0.730       -       -       -       -       Interm         P27       J53       1       -0.350       -       -       -       -       Interm         P27       J53       1       0.120       -       -       -       -       Interm         P27       J53       2       0.100       0.382       0.7979       0.479       Interm         P27       J53       1       0.020       -       -       -       -       Interm         P27       J53       1       0.120       -       -       -       Interm         P27       J53       1       0.130       -       - <t< td=""><td>P26</td><td>.169</td><td>1</td><td>0.600</td><td>-</td><td>-</td><td>-</td><td></td><td></td><td>Surface</td></t<>   | P26     | .169   | 1        | 0.600    | -          | -      | -          |          |            | Surface |
| P27       J53       1       -0.710       -       -       -       -       Interm         P27       J53       1       -0.710       -       -       -       -       Interm         P27       J53       1       -0.100       -       -       -       -       Interm         P27       J53       1       -0.730       -       -       -       Interm         P27       J53       1       -0.730       -       -       -       Interm         P27       J53       1       0.0350       -       -       -       Interm         P27       J53       1       0.120       -       -       -       Interm         P27       J53       1       0.120       -       -       -       Interm         P27       J53       1       0.020       -       -       -       Interm         P27       J53       1       0.120       -       -       -       Interm         P27       J53       1       0.120       -       -       -       Interm         P27       J53       1       0.130       -       -   | P26     | J69    | 1        | 1 080    | _          | _      | _          | 0 208    | 0 29281    | Surface |
| P27       J53       1       -0.100       -       -       -       Interm         P27       J53       1       -0.730       -       -       -       Interm         P27       J53       1       -0.730       -       -       -       Interm         P27       J53       1       -0.350       -       -       -       Interm         P27       J53       1       0.120       -       -       -       Interm         P27       J53       1       0.120       -       -       -       Interm         P27       J53       1       0.020       -       -       -       Interm         P27       J53       1       0.120       -       -       -       Interm         P27       J53       1       0.120       -       -       -       Interm         P27       J53       1       0.130       -       -       -       Interm         P27       J53       1       0.010       -       -       -       Interm         P27       J53       1       0.010       -       -       -       -       Interm <td>P27</td> <td>J53</td> <td>1</td> <td>-0.710</td> <td>_</td> <td>_</td> <td>_</td> <td>0.200</td> <td>0.20201</td> <td>Interm</td>  | P27     | J53    | 1        | -0.710   | _          | _      | _          | 0.200    | 0.20201    | Interm  |
| P27         J53         1         -0.730         -         -         -         Interm           P27         J53         1         -0.730         -         -         -         Interm           P27         J53         1         -0.350         -         -         -         Interm           P27         J53         1         0.120         -         -         -         Interm           P27         J53         1         0.120         -         -         -         Interm           P27         J53         2         0.100         0.382         0.7979         0.479         Interm           P27         J53         1         0.020         -         -         -         Interm           P27         J53         1         0.120         -         -         -         Interm           P27         J53         1         0.130         -         -         -         Interm           P27         J53         1         0.010         -         -         -         Interm  | P27     | J53    | 1        | -0 100   | _          | _      | _          |          |            | Interm  |
| P27         J53         1         -0.350         -         -         -         -         Interm           P27         J53         1         0.120         -         -         -         Interm           P27         J53         1         0.120         -         -         -         Interm           P27         J53         2         0.100         0.382         0.7979         0.479         Interm           P27         J53         1         0.020         -         -         -         Interm           P27         J53         1         0.120         -         -         -         Interm           P27         J53         1         0.120         -         -         -         Interm           P27         J53         1         0.120         -         -         -         Interm           P27         J53         1         0.130         -         -         -         Interm           P27         J53         1         0.010         -         -         -         Interm  | P27     | J53    | 1        | -0.730   | _          | _      | _          |          |            | Interm  |
| P27         J53         1         0.120         -         -         -         Interm           P27         J53         2         0.100         0.382         0.7979         0.479         Interm           P27         J53         1         0.020         -         -         -         Interm           P27         J53         1         0.020         -         -         -         Interm           P27         J53         1         0.120         -         -         -         Interm           P27         J53         1         0.120         -         -         -         Interm           P27         J53         1         0.130         -         -         -         Interm           P27         J53         1         0.010         -         -         -         Interm   | P27     | J53    | 1        | -0.350   | _          | _      | _          |          |            | Interm  |
| P27         J53         2         0.100         0.382         0.7979         0.479         Interm           P27         J53         1         0.020         -         -         -         Interm           P27         J53         1         0.020         -         -         -         Interm           P27         J53         1         0.120         -         -         -         Interm           P27         J53         1         0.120         -         -         -         Interm           P27         J53         1         0.130         -         -         -         Interm           P27         J53         1         0.010         -         -         -         Interm  | P27     | J53    | 1        | 0.120    | _          | _      | _          |          |            | Interm  |
| P27         J53         1         0.020         -         -         -         Interm           P27         J53         1         0.120         -         -         -         Interm           P27         J53         1         0.120         -         -         -         Interm           P27         J53         1         0.130         -         -         -         Interm           P27         J53         1         0.010         -         -         -         Interm   | P27     | J53    | 2        | 0.100    | 0.382      | 0.7979 | 0.479      |          |            | Interm  |
| P27         J53         1         0.120         -         -         -         Interm           P27         J53         1         0.130         -         -         -         Interm           P27         J53         1         0.130         -         -         -         Interm           P27         J53         1         0.010         -         -         -         Interm  | P27     | J53    | 1        | 0.020    | -          | _      | _          |          |            | Interm  |
| P27         J53         1         0.130         -         -         -         Interm           P27         J53         1         0.010         -         -         -         Interm  | P27     | J53    | 1        | 0.120    | _          | _      | _          |          |            | Interm  |
| P27 J53 1 0.010 Interm   | P27     | J53    | 1        | 0.130    | _          | _      | _          |          |            | Interm  |
|  | P27     | J53    | 1        | 0.010    | _          | _      | _          |          |            | Interm  |

| Table B.6. Summary of Unbiased Lot Std D | Dev for VMA for Each Project (continued) |
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| Project | JMF<br>Number | Lot Size | Lot Mean | Lot St Dev | <i>c</i> <sub>4</sub> | Lot St Dev | Average  | Avg Lot SD | Course  |
|---------|---------------|----------|----------|------------|-----------------------|------------|----------|------------|---------|
| P27     | .153          | 1        | 0 1 1 0  | (Diased)   | _                     |            | Lot mean | Unblased   | Interm  |
| P27     | .153          | 1        | 0.020    | _          | _                     | _          |          |            | Interm  |
| P27     | .153          | 1        | 0.610    | _          | _                     | _          |          |            | Interm  |
| P27     | .153          | 1        | 1 070    | _          | _                     | _          | 0.030    | 0 47856    | Interm  |
| P27     | .155          | 3        | 0.290    | 0 598      | 0 8862                | 0.675      | 0.000    | 0.11000    | Surface |
| P27     | J55           | 3        | 0.370    | 0.000      | 0.8862                | 0.480      |          |            | Surface |
| P27     | J55           | 3        | 0.590    | 0.130      | 0.8862                | 0.147      |          |            | Surface |
| P27     | J55           | 3        | 0.400    | 0.278      | 0.8862                | 0.314      |          |            | Surface |
| P27     | J55           | 3        | 0.663    | 0.232      | 0.8862                | 0.262      | 0.463    | 0.37539    | Surface |
| P27     | J60           | 1        | 1.050    | _          | _                     | _          |          |            | Interm  |
| P27     | J60           | 1        | 1.110    | _          | _                     | _          |          |            | Interm  |
| P27     | J60           | 1        | 0.850    | _          | _                     | _          |          |            | Interm  |
| P27     | J60           | 1        | 0.740    | _          | _                     | _          |          |            | Interm  |
| P27     | J60           | 1        | 0.270    | _          | _                     | _          |          |            | Interm  |
| P27     | J60           | 1        | 0.760    | _          | _                     | _          |          |            | Interm  |
| P27     | J60           | 1        | -0.010   | -          | _                     | _          |          |            | Interm  |
| P27     | J60           | 1        | 1.750    | _          | _                     | _          |          |            | Interm  |
| P27     | J60           | 1        | 0.200    | -          | _                     | _          |          |            | Interm  |
| P27     | J60           | 1        | 0.980    | -          | _                     | _          |          |            | Interm  |
| P27     | J60           | 1        | -0.010   | -          | _                     | -          |          |            | Interm  |
| P27     | J60           | 1        | 0.790    | _          | _                     | _          |          |            | Interm  |
| P27     | J60           | 1        | 0.180    | -          | _                     | _          |          |            | Interm  |
| P27     | J60           | 1        | -0.020   | -          | _                     | _          |          |            | Interm  |
| P27     | J60           | 1        | 0.520    | _          | -                     | -          | 0.611    | #DIV/0!    | Interm  |
| P27     | J61           | 1        | 0.410    | _          | _                     | _          |          |            | Surface |
| P27     | J61           | 1        | -0.070   | Ι          | _                     | _          |          |            | Surface |
| P27     | J61           | 1        | -1.260   | -          | _                     | —          |          |            | Surface |
| P27     | J61           | 1        | 0.080    | -          | -                     | —          |          |            | Surface |
| P27     | J61           | 1        | -0.380   | _          | _                     | _          |          |            | Surface |
| P27     | J61           | 1        | 0.370    | —          | -                     | _          |          |            | Surface |
| P27     | J61           | 1        | -0.550   | —          | -                     | _          |          |            | Surface |
| P27     | J61           | 1        | -0.660   | —          | -                     | _          |          |            | Surface |
| P27     | J61           | 1        | -0.510   | _          | -                     | -          | -0.286   | #DIV/0!    | Surface |
| P27     | J71           | 3        | 0.453    | 0.284      | 0.8862                | 0.321      |          |            | Surface |
| P27     | J71           | 4        | 0.350    | 0.295      | 0.9213                | 0.320      |          |            | Surface |
| P27     | J71           | 3        | -0.082   | 0.642      | 0.8862                | 0.725      |          |            | Surface |
| P27     | J71           | 2        | 0.550    | 0.820      | 0.7979                | 1.028      |          |            | Surface |
| P27     | J71           | 1        | 0.280    | —          | _                     | -          |          |            | Surface |
| P27     | J71           | 3        | 0.457    | 0.458      | 0.8862                | 0.516      |          |            | Surface |
| P27     | J71           | 3        | 0.080    | 0.332      | 0.8862                | 0.374      |          |            | Surface |
| P27     | J71           | 5        | 0.262    | 0.414      | 0.9400                | 0.440      |          | 0.510      | Surface |
| P27     | J71           | 3        | 0.480    | 0.330      | 0.8862                | 0.372      | 0.314    | 0.51209    | Surface |
| P28     | J39           | 3        | -0.420   | 0.306      | 0.8862                | 0.346      |          |            | Surface |
| P28     | J <u>3</u> 9  | 1        | -0.840   | -          | -                     | -          |          |            | Surface |
| P28     | J39           | 4        | -0.325   | 0.078      | 0.9213                | 0.084      |          |            | Surface |
| P28     | J39           | 5        | -0.518   | 0.290      | 0.9400                | 0.308      |          |            | Surface |
| P28     | J39           | 5        | -0.356   | 0.112      | 0.9400                | 0.120      |          |            | Surface |

## Table B.6. Summary of Unbiased Lot Std Dev for VMA for Each Project (continued)

| Project<br>Number | JMF<br>Number | Lot Size | Lot Mean | Lot St Dev<br>(biased) | <i>c</i> <sub>4</sub> | Lot St Dev<br>(unbiased) | Average<br>Lot Mean | Avg Lot SD<br>Unbiased | Course  |
|-------------------|---------------|----------|----------|------------------------|-----------------------|--------------------------|---------------------|------------------------|---------|
| P28               | J39           | 1        | -0.170   |                        | _                     | - <i>(</i>               |                     |                        | Surface |
| P28               | J39           | 3        | -0.277   | 0.049                  | 0.8862                | 0.056                    |                     |                        | Surface |
| P28               | J39           | 1        | -0.450   | _                      | _                     | _                        |                     |                        | Surface |
| P28               | J39           | 1        | -0.450   | _                      | _                     | _                        | -0.423              | 0.18268                | Surface |
| P28               | J42           | 2        | -0.225   | 0.841                  | 0.7979                | 1.055                    |                     |                        | Interm  |
| P28               | J42           | 1        | 0.680    | _                      | _                     | _                        |                     |                        | Interm  |
| P28               | J42           | 1        | -0.620   | _                      | _                     | _                        |                     |                        | Interm  |
| P28               | J42           | 1        | 0.390    | _                      | _                     | _                        |                     |                        | Interm  |
| P28               | J42           | 1        | -0.170   | _                      | _                     | _                        |                     |                        | Interm  |
| P28               | J42           | 1        | -0.140   | _                      | _                     | _                        |                     |                        | Interm  |
| P28               | J42           | 1        | 0.940    | _                      | _                     | _                        |                     |                        | Interm  |
| P28               | J42           | 1        | 0.940    | _                      | _                     | _                        |                     |                        | Interm  |
| P28               | J42           | 2        | 0.210    | 0.071                  | 0.7979                | 0.089                    |                     |                        | Interm  |
| P28               | J42           | 1        | 0.270    | _                      | _                     | _                        |                     |                        | Interm  |
| P28               | J42           | 1        | 0.370    | _                      | -                     | _                        |                     |                        | Interm  |
| P28               | J42           | 1        | -0.260   | _                      | -                     | _                        |                     |                        | Interm  |
| P28               | J42           | 1        | 0.160    | _                      | _                     | _                        | 0.196               | 0.57161                | Interm  |
| P29               | J59           | 1        | -0.210   | _                      | -                     | -                        |                     |                        | Surface |
| P29               | J59           | 3        | 0.223    | 0.055                  | 0.8862                | 0.062                    |                     |                        | Surface |
| P29               | J59           | 3        | 0.273    | 0.360                  | 0.8862                | 0.406                    |                     |                        | Surface |
| P29               | J59           | 3        | -0.177   | 0.171                  | 0.8862                | 0.193                    |                     |                        | Surface |
| P29               | J59           | 3        | 0.280    | 0.469                  | 0.8862                | 0.529                    |                     |                        | Surface |
| P29               | J59           | 3        | -0.020   | 0.148                  | 0.8862                | 0.167                    |                     |                        | Surface |
| P29               | J59           | 4        | -0.113   | 0.427                  | 0.9213                | 0.463                    |                     |                        | Surface |
| P29               | J59           | 3        | -0.200   | 0.061                  | 0.8862                | 0.069                    |                     |                        | Surface |
| P29               | J59           | 3        | -0.303   | 0.153                  | 0.8862                | 0.172                    | -0.027              | 0.25769                | Surface |
| P30               | J65           | 3        | 0.493    | 0.220                  | 0.8862                | 0.248                    |                     |                        | Surface |
| P30               | J65           | 3        | 0.467    | 0.182                  | 0.8862                | 0.206                    |                     |                        | Surface |
| P30               | J65           | 1        | 0.630    | -                      | _                     | _                        |                     |                        | Surface |
| P30               | J65           | 1        | 0.330    | -                      | -                     | _                        | 0.480               | 0.22703                | Surface |
| P32               | J72           | 5        | 0.344    | 0.415                  | 0.9400                | 0.442                    |                     |                        | Surface |
| P32               | J72           | 6        | 0.525    | 0.416                  | 0.9515                | 0.437                    |                     |                        | Surface |
| P32               | J72           | 3        | 0.317    | 0.536                  | 0.8862                | 0.605                    |                     |                        | Surface |
| P32               | J72           | 3        | 0.250    | 0.148                  | 0.8862                | 0.167                    |                     |                        | Surface |
| P32               | J72           | 5        | -0.102   | 0.521                  | 0.9400                | 0.554                    |                     |                        | Surface |
| P32               | J72           | 5        | -0.108   | 0.411                  | 0.9400                | 0.437                    |                     |                        | Surface |
| P32               | J72           | 3        | -0.117   | 0.107                  | 0.8862                | 0.121                    |                     |                        | Surface |
| P32               | J72           | 4        | -0.095   | 0.353                  | 0.9213                | 0.384                    | 0.127               | 0.39329                | Surface |
| P32               | J76           | 4        | -0.095   | 0.560                  | 0.9213                | 0.608                    |                     |                        | Interm  |
| P32               | J76           | 3        | -0.513   | 0.302                  | 0.8862                | 0.341                    |                     |                        | Interm  |
| P32               | J76           | 5        | 0.098    | 0.658                  | 0.9400                | 0.700                    |                     |                        | Interm  |
| P32               | J76           | 4        | -0.060   | 0.354                  | 0.9213                | 0.384                    |                     |                        | Interm  |
| P32               | J76           | 3        | 0.260    | 0.269                  | 0.8862                | 0.303                    |                     |                        | Interm  |
| P32               | J76           | 3        | -0.420   | 0.566                  | 0.8862                | 0.639                    |                     |                        | Interm  |
| P32               | J76           | 3        | -0.173   | 0.169                  | 0.8862                | 0.191                    |                     |                        | Interm  |
| P32               | J76           | 4        | 0.155    | 0.153                  | 0.9213                | 0.166                    |                     |                        | Interm  |
| P32               | J76           | 4        | -0.510   | 0.188                  | 0.9213                | 0.204                    |                     |                        | Interm  |

| Table B.6. Summary of Unbiased Lot Std Dev for | VMA for Each Project (continued) |
|--|----------------------------------|
|--|----------------------------------|

| Project | JMF<br>Number | Lot Size | Lot Mean | Lot St Dev | <i>c</i> <sub>4</sub> | Lot St Dev | Average  | Avg Lot SD | Course  |
|---------|---------------|----------|----------|------------|-----------------------|------------|----------|------------|---------|
| P32     | .176          | 4        | 0.015    | 0.365      | 0 9213                | 0.397      | Lot mean | UliblaSca  | Interm  |
| P32     | .176          | 3        | -0.003   | 0.537      | 0.8862                | 0.606      |          |            | Interm  |
| P32     | J76           | 3        | 0.187    | 0.376      | 0.8862                | 0.424      | -0.088   | 0.41358    | Interm  |
| P32     | J79           | 6        | 0.162    | 0.417      | 0.9515                | 0.438      | 0.000    |            | Surface |
| P32     | J79           | 5        | 0.456    | 0.215      | 0.9400                | 0.229      |          |            | Surface |
| P32     | J79           | 4        | 0.373    | 0.387      | 0.9213                | 0.420      |          |            | Surface |
| P32     | J79           | 3        | -0.060   | 0.410      | 0.8862                | 0.462      |          |            | Surface |
| P32     | J79           | 4        | -0.115   | 0.411      | 0.9213                | 0.446      |          |            | Surface |
| P32     | J79           | 3        | 0.077    | 0.230      | 0.8862                | 0.260      |          |            | Surface |
| P32     | J79           | 3        | 0.307    | 0.497      | 0.8862                | 0.561      |          |            | Surface |
| P32     | J79           | 3        | 0.713    | 0.344      | 0.8862                | 0.388      |          |            | Surface |
| P32     | J79           | 4        | 0.523    | 0.464      | 0.9213                | 0.503      |          |            | Surface |
| P32     | J79           | 5        | 0.276    | 0.632      | 0.9400                | 0.673      |          |            | Surface |
| P32     | J79           | 4        | -0.678   | 1.187      | 0.9213                | 1.288      |          |            | Surface |
| P32     | J79           | 5        | -0.270   | 0.290      | 0.9400                | 0.308      |          |            | Surface |
| P32     | J79           | 3        | 0.017    | 0.032      | 0.8862                | 0.036      |          |            | Surface |
| P32     | J79           | 5        | 0.010    | 0.452      | 0.9400                | 0.481      |          |            | Surface |
| P32     | J79           | 5        | -0.060   | 0.439      | 0.9400                | 0.467      |          |            | Surface |
| P32     | J79           | 5        | -0.680   | 0.322      | 0.9400                | 0.343      |          |            | Surface |
| P32     | J79           | 5        | 0.218    | 0.280      | 0.9400                | 0.298      |          |            | Surface |
| P32     | J79           | 3        | 0.333    | 0.548      | 0.8862                | 0.619      |          |            | Surface |
| P32     | J79           | 5        | 0.388    | 0.459      | 0.9400                | 0.488      |          |            | Surface |
| P32     | J79           | 3        | 0.280    | 0.632      | 0.8862                | 0.713      |          |            | Surface |
| P32     | J79           | 3        | 0.307    | 0.448      | 0.8862                | 0.506      |          |            | Surface |
| P32     | J79           | 4        | -0.233   | 0.351      | 0.9213                | 0.381      |          |            | Surface |
| P32     | J79           | 3        | -0.413   | 0.178      | 0.8862                | 0.201      |          |            | Surface |
| P32     | J79           | 3        | -0.697   | 0.217      | 0.8862                | 0.245      | 0.051    | 0.44816    | Surface |
| P33     | J73           | 1        | 0.420    | _          | -                     | -          |          |            | Interm  |
| P33     | J73           | 3        | 0.277    | 0.220      | 0.8862                | 0.248      |          |            | Interm  |
| P33     | J73           | 3        | -0.590   | 0.488      | 0.8862                | 0.550      |          |            | Interm  |
| P33     | J73           | 5        | 0.070    | 0.143      | 0.9400                | 0.153      |          |            | Interm  |
| P33     | J73           | 4        | 0.258    | 0.506      | 0.9213                | 0.550      |          |            | Interm  |
| P33     | J73           | 3        | 0.093    | 0.045      | 0.8862                | 0.051      |          |            | Interm  |
| P33     | J73           | 3        | 0.647    | 0.212      | 0.8862                | 0.239      |          |            | Interm  |
| P33     | J73           | 3        | 0.197    | 0.236      | 0.8862                | 0.266      | 0.171    | 0.29383    | Interm  |
| P33     | J77           | 4        | -0.210   | 0.492      | 0.9213                | 0.534      |          |            | Surface |
| P33     | J77           | 4        | -0.323   | 0.434      | 0.9213                | 0.471      |          |            | Surface |
| P33     | J77           | 4        | -0.518   | 0.159      | 0.9213                | 0.172      |          |            | Surface |
| P33     | J77           | 4        | 0.660    | 0.518      | 0.9213                | 0.562      |          |            | Surface |
| P33     | J77           | 3        | 0.783    | 0.466      | 0.8862                | 0.526      |          |            | Surface |
| P33     | J77           | 3        | 0.663    | 0.171      | 0.8862                | 0.193      | 0.176    | 0.40976    | Surface |
| P34     | J62           | 4        | 0.170    | 0.284      | 0.9213                | 0.309      |          |            | Surface |
| P34     | J62           | 4        | -0.053   | 0.162      | 0.9213                | 0.176      |          |            | Surface |
| P34     | J62           | 6        | 0.117    | 0.401      | 0.9515                | 0.421      |          |            | Surface |
| P34     | J62           | 4        | 0.450    | 0.615      | 0.9213                | 0.668      |          |            | Surface |
| P34     | J62           | 4        | -0.023   | 0.442      | 0.9213                | 0.480      |          |            | Surface |
| P34     | J62           | 4        | 0.125    | 0.408      | 0.9213                | 0.443      |          |            | Surface |

| Table B.6. Summa | ry of Unbiased Lo | ot Std Dev for VI | MA for Each Proj | ect (continued) |
|------------------|-------------------|-------------------|------------------|-----------------|
|------------------|-------------------|-------------------|------------------|-----------------|

| Project<br>Number | JMF<br>Number | Lot Size | Lot Mean | Lot St Dev<br>(biased) | <i>c</i> <sub>4</sub> | Lot St Dev<br>(unbiased) | Average<br>Lot Mean | Avg Lot SD<br>Unbiased | Course  |
|-------------------|---------------|----------|----------|------------------------|-----------------------|--------------------------|---------------------|------------------------|---------|
| P34               | J62           | 2        | -0.365   | 0.092                  | 0.7979                | 0.115                    | 0.060               | 0.37308                | Surface |
| P34               | J81           | 2        | 0.800    | 0.028                  | 0.7979                | 0.035                    |                     |                        | Surface |
| P34               | J81           | 2        | 0.395    | 0.516                  | 0.7979                | 0.647                    |                     |                        | Surface |
| P34               | J81           | 1        | 0.650    | -                      | _                     | _                        |                     |                        | Surface |
| P34               | J81           | 2        | 0.115    | 0.262                  | 0.7979                | 0.328                    |                     |                        | Surface |
| P34               | J81           | 2        | 0.100    | 0.481                  | 0.7979                | 0.603                    |                     |                        | Surface |
| P34               | J81           | 2        | -0.110   | 0.212                  | 0.7979                | 0.266                    |                     |                        | Surface |
| P34               | J81           | 2        | 0.280    | 0.948                  | 0.7979                | 1.188                    | 0.319               | 0.51105                | Surface |
| P35               | J32           | 3        | -0.103   | 0.530                  | 0.8862                | 0.598                    |                     |                        | Surface |
| P35               | J32           | 1        | -0.270   | -                      | _                     | _                        |                     |                        | Surface |
| P35               | J32           | 3        | 0.280    | 0.243                  | 0.8862                | 0.275                    |                     |                        | Surface |
| P35               | J32           | 3        | 0.013    | 0.216                  | 0.8862                | 0.243                    |                     |                        | Surface |
| P35               | J32           | 3        | 0.650    | 0.139                  | 0.8862                | 0.157                    |                     |                        | Surface |
| P35               | J32           | 1        | 1.010    | _                      | _                     | _                        | 0.263               | 0.31821                | Surface |
| P35               | J38           | 2        | -0.445   | 0.021                  | 0.7979                | 0.027                    |                     |                        | Surface |
| P35               | J38           | 2        | -0.135   | 0.389                  | 0.7979                | 0.487                    |                     |                        | Surface |
| P35               | J38           | 1        | 0.350    | _                      | _                     | _                        |                     |                        | Surface |
| P35               | J38           | 2        | 0.335    | 0.841                  | 0.7979                | 1.055                    |                     |                        | Surface |
| P35               | J38           | 2        | 0.350    | 0.071                  | 0.7979                | 0.089                    |                     |                        | Surface |
| P35               | J38           | 1        | 0.190    | _                      | _                     | _                        |                     |                        | Surface |
| P35               | J38           | 2        | 0.075    | 0.460                  | 0.7979                | 0.576                    |                     |                        | Surface |
| P35               | J38           | 3        | 0.033    | 0.306                  | 0.8862                | 0.345                    |                     |                        | Surface |
| P35               | J38           | 5        | 0.090    | 0.326                  | 0.9400                | 0.346                    |                     |                        | Surface |
| P35               | J38           | 2        | 0.350    | 0.226                  | 0.7979                | 0.284                    |                     |                        | Surface |
| P35               | J38           | 4        | 0.180    | 0.146                  | 0.9213                | 0.158                    |                     |                        | Surface |
| P35               | J38           | 3        | 0.280    | 0.265                  | 0.8862                | 0.299                    |                     |                        | Surface |
| P35               | J38           | 3        | 0.210    | 0.312                  | 0.8862                | 0.353                    |                     |                        | Surface |
| P35               | J38           | 2        | 0.325    | 0.247                  | 0.7979                | 0.310                    |                     |                        | Surface |
| P35               | J38           | 1        | 0.550    | -                      | _                     | —                        |                     |                        | Surface |
| P35               | J38           | 1        | 0.300    | -                      | -                     | _                        | 0.190               | 0.36074                | Surface |
|                   |               |          |          |                        |                       |                          |                     |                        |         |
|                   |               |          |          |                        |                       |                          |                     |                        |         |
|                   |               |          |          |                        |                       |                          |                     |                        |         |
|                   |               |          |          |                        |                       |                          |                     |                        |         |
|                   |               |          |          |                        |                       |                          |                     |                        |         |
|                   |               |          |          |                        |                       |                          |                     |                        |         |
|                   |               |          |          |                        |                       |                          |                     |                        |         |
|                   |               |          |          |                        |                       |                          |                     |                        |         |
|                   |               |          |          |                        |                       |                          |                     |                        |         |
|                   |               |          |          |                        |                       |                          |                     |                        |         |
|                   |               |          |          |                        |                       |                          |                     |                        |         |
|                   |               |          |          |                        |                       |                          |                     |                        |         |
|                   |               |          |          |                        |                       |                          |                     |                        |         |
|                   |               |          |          |                        |                       |                          |                     |                        |         |
|                   |               |          |          |                        |                       |                          |                     |                        |         |
|                   |               |          |          |                        |                       |                          |                     |                        |         |
|                   |               |          |          |                        |                       |                          |                     |                        |         |

| Table B.6. Summary of Unbiased Lot S | td Dev for VMA for | Each Project (continued) |
|--------------------------------------|--------------------|--------------------------|
|--------------------------------------|--------------------|--------------------------|

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# APPENDIX C — PWL VALUES FOR EACH DENSITY LOT FOR EACH PROJECT

One potential point of concern with the Density data is the relatively low value for the average densities on the various projects. These individual project average values ranged from a low of 88.65 to a high of 94.12, and the average for all projects was around 92.4. The specification "target" values for density were 94.0 for Interstate paving and 93.0 for Other paving. To further investigate how well the projects for which data were obtained met the specification requirements, lot PWL values were calculated. For each project, the PWL value for each lot was calculated and the average PWL for all lots on the project was also calculated. These results are shown in the following tables.

| Project<br>Number | JMF<br>Number                                      | Lot<br>Sample<br>Size | Lot Mean | Lot<br>Standard<br>Deviation | Lot PWL | Average<br>Lot PWL | Mix Type |  |  |  |
|-------------------|--|-----------------------|----------|------------------------------|---------|--------------------|----------|--|--|--|
| P01               | J02  | 10                    | 94.37    | 0.821                        | 98.75   |                    | Binder 1 |  |  |  |
| P01               | J02  | 1                     | 92.47    | —                            |         |                    | Binder 1 |  |  |  |
| P01               | J02  | 5                     | 93.81    | 0.746                        | 100.00  |                    | Binder 1 |  |  |  |
| P01               | J02  | 6                     | 93.58    | 0.862                        | 96.76   | 98.50              | Binder 1 |  |  |  |
| P01               | J10  | 3                     | 92.32    | 0.101                        | 100.00  |                    | Interm B |  |  |  |
| P01               | J10  | 4                     | 93.07    | 0.546                        | 100.00  |                    | Interm B |  |  |  |
| P01               | J10  | 4                     | 92.54    | 0.167                        | 100.00  |                    | Interm B |  |  |  |
| P01               | J10  | 5                     | 93.10    | 0.977                        | 81.27   |                    | Interm B |  |  |  |
| P01               | J10  | 3                     | 92.76    | 0.487                        | 97.10   |                    | Interm B |  |  |  |
| P01               | J10  | 5                     | 92.95    | 0.557                        | 92.90   |                    | Interm B |  |  |  |
| P01               | J10  | 6                     | 93.18    | 0.508                        | 99.78   | 96.42              | Interm B |  |  |  |
| P23               | J33  | 3                     | 91.96    | 1.587                        | 45.82   |                    | Interm B |  |  |  |
| P23               | J33  | 3                     | 91.23    | 1.572                        | 32.05   |                    | Interm B |  |  |  |
| P23               | J33  | 5                     | 91.84    | 1.426                        | 41.05   |                    | Interm B |  |  |  |
| P23               | J33  | 5                     | 91.48    | 1.422                        | 32.22   | 37.76              | Interm B |  |  |  |
| P32               | J76  | 9                     | 93.84    | 0.817                        | 99.04   |                    | Interm B |  |  |  |
| P32               | J76  | 6                     | 94.23    | 1.12                         | 95.56   |                    | Interm B |  |  |  |
| P32               | J76  | 10                    | 92.79    | 0.548                        | 85.95   |                    | Interm B |  |  |  |
| P32               | J76  | 10                    | 93.09    | 0.856                        | 85.04   |                    | Interm B |  |  |  |
| P32               | J76  | 10                    | 93.02    | 0.75                         | 86.35   |                    | Interm B |  |  |  |
| P32               | J76  | 6                     | 92.09    | 1.437                        | 47.19   |                    | Interm B |  |  |  |
| P32               | J76  | 7                     | 92.49    | 0.988                        | 60.89   |                    | Interm B |  |  |  |
| P32               | J76  | 6                     | 93.33    | 1.738                        | 68.87   |                    | Interm B |  |  |  |
| P32               | J76  | 9                     | 93.34    | 0.964                        | 88.41   |                    | Interm B |  |  |  |
| P32               | J76  | 9                     | 93.60    | 0.77                         | 97.85   |                    | Interm B |  |  |  |
| P32               | J76  | 10                    | 93.69    | 0.972                        | 94.46   |                    | Interm B |  |  |  |
| P32               | J76  | 7                     | 93.38    | 0.781                        | 94.89   |                    | Interm B |  |  |  |
| P32               | J76  | 6                     | 93.56    | 1.381                        | 82.08   | 83.58              | Interm B |  |  |  |
| P33               | J73  | 5                     | 93.59    | 2.214                        | 58.07   |                    | Interm B |  |  |  |
| P33               | J73  | 7                     | 93.19    | 2.129                        | 58.52   |                    |          |  |  |  |
| P33               | J73  | 5                     | 92.78    | 0.918                        | 72.01   |                    | Interm B |  |  |  |
| P33               | J73  | 10                    | 93.49    | 0.96                         | 91.58   |                    | Interm B |  |  |  |
| P33               | J73  | 7                     | 93.24    | 1.004                        | 84.86   |                    | Interm B |  |  |  |
| P33               | J73  | 9                     | 92.81    | 1.335                        | 66.98   |                    | Interm B |  |  |  |
| P33               | J73  | 7                     | 93.53    | 1.371                        | 81.44   |                    | Interm B |  |  |  |
| P33               | J73  | 6                     | 92.75    | 1.219                        | 66.31   | 72.47              | Interm B |  |  |  |
| <b>T</b>          |  |                       | 00.01    | 4.000                        | 70 7 4  |                    |          |  |  |  |
| Total / /         | Total / Average 229 93.01 1.030 79.54 77.75 Interm |                       |          |                              |         |                    |          |  |  |  |
| Continued         |  |                       |          |                              |         |                    |          |  |  |  |

## Table C.1. Summary of Density Lot PWL Values for Each Interstate Paving Project

| Project<br>Number | JMF<br>Number | Lot<br>Sample<br>Size | Lot Mean | Lot<br>Standard<br>Deviation | Lot PWL | Average<br>Lot PWL | Міх Туре |
|-------------------|---------------|-----------------------|----------|------------------------------|---------|--------------------|----------|
| P01               | J07           | 5                     | 92.50    | 0.217                        | 93.73   |                    | Surf 1C  |
| P01               | J07           | 4                     | 93.55    | 0.396                        | 100.00  |                    | Surf 1C  |
| P01               | J07           | 6                     | 93.19    | 0.346                        | 100.00  |                    | Surf 1C  |
| P01               | J07           | 7                     | 93.70    | 1.101                        | 92.15   | 96.47              | Surf 1C  |
| P26               | J62           | 8                     | 93.39    | 2.154                        | 59.34   |                    | Surf A   |
| P26               | J62           | 4                     | 93.86    | 0.823                        | 100.00  |                    | Surf A   |
| P26               | J62           | 3                     | 92.48    | 0.295                        | 80.71   |                    | Surf A   |
| P26               | J62           | 5                     | 91.70    | 1.538                        | 38.49   |                    | Surf A   |
| P26               | J62           | 5                     | 92.81    | 1.195                        | 67.92   |                    | Surf A   |
| P26               | J62           | 4                     | 92.99    | 0.705                        | 87.35   |                    | Surf A   |
| P26               | J62           | 5                     | 93.07    | 0.878                        | 83.37   |                    | Surf A   |
| P26               | J62           | 3                     | 93.23    | 0.363                        | 100.00  |                    | Surf A   |
| P26               | J62           | 5                     | 92.05    | 0.931                        | 44.27   | 73.49              | Surf A   |
| P26               | J69           | 5                     | 93.27    | 1.226                        | 79.78   |                    | Surf A   |
| P26               | J69           | 6                     | 93.00    | 2.265                        | 54.68   |                    | Surf A   |
| P26               | J69           | 4                     | 92.82    | 2.080                        | 59.94   |                    | Surf A   |
| P26               | J69           | 5                     | 94.13    | 0.564                        | 100.00  |                    | Surf A   |
| P26               | J69           | 4                     | 93.83    | 0.651                        | 100.00  |                    | Surf A   |
| P26               | J69           | 5                     | 94.29    | 0.664                        | 100.00  |                    | Surf A   |
| P26               | J69           | 6                     | 93.37    | 0.994                        | 88.45   |                    | Surf A   |
| P26               | J69           | 5                     | 93.10    | 0.721                        | 90.49   |                    | Surf A   |
| P26               | J69           | 5                     | 93.33    | 0.967                        | 88.40   |                    | Surf A   |
| P26               | J69           | 5                     | 93.26    | 1.282                        | 78.34   |                    | Surf A   |
| P26               | J69           | 5                     | 92.78    | 0.737                        | 77.08   |                    | Surf A   |
| P26               | J69           | 6                     | 92.38    | 1.020                        | 56.47   |                    | Surf A   |
| P26               | J69           | 6                     | 93.79    | 0.782                        | 100.00  |                    | Surf A   |
| P26               | J69           | 6                     | 94.38    | 0.674                        | 100.00  |                    | Surf A   |
| P26               | J69           | 5                     | 93.05    | 1.633                        | 68.26   |                    | Surf A   |
| P26               | J69           | 3                     | 93.54    | 0.650                        | 100.00  | 83.86              | Surf A   |
| P32               | J74           | 6                     | 93.20    | 1.348                        | 76.06   | 76.06              | Surf A   |
|                   |               |                       | Cont     | inued                        |         |                    |          |

## Table C.1. Summary of Density Lot PWL Values for Each Interstate Paving Project (cont)

| Project<br>Number | JMF<br>Number | Lot<br>Sample<br>Size | Lot Mean | Lot<br>Standard<br>Deviation | Lot PWL       | Average<br>Lot PWL | Mix Type |
|-------------------|---------------|-----------------------|----------|------------------------------|---------------|--------------------|----------|
| P32               | J79           | 10                    | 93.03    | 0.817                        | 84.44         |                    | Surf A   |
| P32               | J79           | 8                     | 92.99    | 0.655                        | 88.97         |                    | Surf A   |
| P32               | J79           | 10                    | 92.98    | 1.174                        | 74.17         |                    | Surf A   |
| P32               | J79           | 4                     | 92.80    | 0.896                        | 72.32         |                    | Surf A   |
| P32               | J79           | 10                    | 92.78    | 0.706                        | 79.07         |                    | Surf A   |
| P32               | J79           | 4                     | 93.15    | 0.334                        | 100.00        |                    | Surf A   |
| P32               | J79           | 8                     | 93.03    | 0.520                        | 95.79         |                    | Surf A   |
| P32               | J79           | 4                     | 93.01    | 0.311                        | 100.00        |                    | Surf A   |
| P32               | J79           | 9                     | 92.53    | 1.713                        | 56.45         |                    | Surf A   |
| P32               | J79           | 9                     | 92.93    | 0.609                        | 88.76         |                    | Surf A   |
| P32               | J79           | 11                    | 92.77    | 0.489                        | 87.99         |                    | Surf A   |
| P32               | J79           | 5                     | 93.07    | 0.870                        | 83.64         |                    | Surf A   |
| P32               | J79           | 5                     | 91.26    | 0.663                        | 5.49          |                    | Surf A   |
| P32               | J79           | 10                    | 92.45    | 0.985                        | <u>59.6</u> 8 |                    | Surf A   |
| P32               | J79           | 6                     | 92.21    | 1.104                        | 50.33         |                    | Surf A   |
| P32               | J79           | 8                     | 92.61    | 1.033                        | 64.78         |                    | Surf A   |
| P32               | J79           | 5                     | 92.5     | 0.479                        | 71.82         |                    | Surf A   |
| P32               | J79           | 4                     | 93.49    | 0.645                        | 100.00        |                    | Surf A   |
| P32               | J79           | 7                     | 93.26    | 1.135                        | 82.07         |                    | Surf A   |
| P32               | J79           | 5                     | 92.47    | 0.408                        | 73.00         |                    | Surf A   |
| P32               | J79           | 7                     | 92.97    | 0.617                        | 89.97         |                    | Surf A   |
| P32               | J79           | 8                     | 92.95    | 1.120                        | 74.16         |                    | Surf A   |
| P32               | J79           | 6                     | 92.05    | 1.201                        | 45.42         |                    | Surf A   |
| P32               | J79           | 3                     | 93.19    | 1.344                        | 72.02         | 75.01              | Surf A   |
| P33               | J77           | 8                     | 91.71    | 0.736                        | 25.97         |                    | Surf A   |
| P33               | J77           | 8                     | 93.54    | 1.144                        | 87.94         |                    | Surf A   |
| P33               | J77           | 7                     | 93.78    | 0.594                        | 100.00        |                    | Surf A   |
| P33               | J77           | 7                     | 91.68    | 1.967                        | 40.16         |                    | Surf A   |
| P33               | J77           | 6                     | 92.03    | 1.454                        | 45.71         |                    | Surf A   |
| P33               | J77           | 4                     | 93.55    | 0.756                        | 100.00        | 66.63              | Surf A   |
| P34               | J62           | 5                     | 94.03    | 1.002                        | 100.00        |                    | Surf A   |
| P34               | J62           | 5                     | 92.58    | 1.314                        | 60.25         |                    | Surf A   |
| P34               | J62           | 10                    | 91.67    | 1.927                        | 39.20         |                    | Surf A   |
| P34               | J62           | 5                     | 93.74    | 1.461                        | 82.29         | 70.43              | Surf A   |
| P01               | J07           | 5                     | 92.7     | 0.369                        | 93.10         |                    | Surf B   |
| P01               | J07           | 4                     | 92.99    | 0.648                        | 90.64         |                    | Surf B   |
| P01               | J07           | 3                     | 92.53    | 0.217                        | 100.00        |                    | Surf B   |
| P01               | J07           | 5                     | 92.35    | 0.128                        | 88.49         |                    | Surf B   |
| P01               | J07           | 3                     | 93.28    | 1.109                        | 81.94         | 90.83              | Surf B   |
| P03               | J15           | 4                     | 93.56    | 0.606                        | 100.00        |                    | Surf B   |
| P03               | J15           | 4                     | 92.49    | 0.801                        | 62.07         |                    | Surf B   |
| P03               | J15           | 10                    | 92.8     | 1.583                        | 63.24         |                    | Surf B   |
| P03               | J15           | 4                     | 93.97    | 0.692                        | 100.00        |                    | Surf B   |
| P03               | J15           | 3                     | 94.25    | 0.778                        | 100.00        | 85.06              | Surf B   |
|                   | 1             |                       | Cont     | inued                        |               | 1                  | <u> </u> |

## Table C.1. Summary of Density Lot PWL Values for Each Interstate Paving Project (cont)

| Project<br>Number | JMF<br>Number | Lot<br>Sample<br>Size | Lot Mean | Lot<br>Standard<br>Deviation | Lot PWL | Average<br>Lot PWL | Міх Туре |
|-------------------|---------------|-----------------------|----------|------------------------------|---------|--------------------|----------|
| P23               | J63           | 3                     | 92.76    | 0.487                        | 97.10   |                    | Surf B   |
| P23               | J63           | 3                     | 93.10    | 0.487                        | 100.00  |                    | Surf B   |
| P23               | J63           | 3                     | 92.83    | 0.487                        | 100.00  |                    | Surf B   |
| P23               | J63           | 3                     | 92.87    | 0.487                        | 100.00  |                    | Surf B   |
| P23               | J63           | 3                     | 93.40    | 0.637                        | 100.00  |                    | Surf B   |
| P23               | J63           | 3                     | 93.71    | 0.643                        | 100.00  | 99.52              | Surf B   |
| P32               | J72           | 12                    | 93.05    | 0.726                        | 88.09   |                    | Surf B   |
| P32               | J72           | 14                    | 92.89    | 0.641                        | 85.95   |                    | Surf B   |
| P32               | J72           | 5                     | 92.30    | 0.783                        | 54.54   |                    | Surf B   |
| P32               | J72           | 5                     | 93.40    | 1.298                        | 81.37   |                    | Surf B   |
| P32               | J72           | 10                    | 93.33    | 1.303                        | 79.46   |                    | Surf B   |
| P32               | J72           | 9                     | 93.61    | 0.525                        | 100.00  |                    | Surf B   |
| P32               | J72           | 6                     | 93.01    | 0.647                        | 90.23   |                    | Surf B   |
| P32               | J72           | 9                     | 92.86    | 0.642                        | 84.72   | 83.05              | Surf B   |
|                   |               |                       |          |                              |         |                    |          |
| Total / /         | Average       | 515                   | 93.01    | 0.888                        | 80.55   | 81.06              | Surface  |
|                   |               |                       |          |                              |         |                    |          |
| Total / /         | Average       | 229                   | 93.01    | 1.030                        | 79.54   | 77.75              | Interm   |
| Total / /         | Average       | 744                   | 93.01    | 0.928                        | 80.26   | 80.57              | All      |

 Table C.1. Summary of Density Lot PWL Values for Each Interstate Paving Project (cont)

| Project<br>Number | JMF<br>Number | Lot<br>Sample<br>Size | Lot Mean | Lot<br>Standard<br>Deviation | Lot PWL | Average<br>Lot PWL | Міх Туре |
|-------------------|---------------|-----------------------|----------|------------------------------|---------|--------------------|----------|
| P01               | J23           | 5                     | 93.68    | 0.970                        | 100.00  |                    | Interm B |
| P01               | J23           | 3                     | 93.86    | 1.572                        | 100.00  | 100.00             | Interm B |
| P03               | J04           | 5                     | 93.11    | 1.170                        | 98.47   |                    | Interm B |
| P03               | J04           | 4                     | 94.31    | 1.150                        | 98.99   |                    | Interm B |
| P03               | J04           | 12                    | 94.61    | 0.729                        | 98.05   |                    | Interm B |
| P03               | J04           | 3                     | 93.93    | 0.615                        | 100.00  |                    | Interm B |
| P03               | J04           | 6                     | 91.99    | 1.267                        | 72.20   | 93.54              | Interm B |
| P36               | J09           | 3                     | 93.06    | 0.318                        | 100.00  |                    | Interm B |
| P36               | J09           | 3                     | 93.17    | 1.364                        | 100.00  |                    | Interm B |
| P36               | J09           | 7                     | 92.51    | 1.445                        | 81.29   |                    | Interm B |
| P36               | J09           | 4                     | 92.71    | 1.943                        | 75.90   |                    | Interm B |
| P36               | J09           | 4                     | 92.71    | 1.943                        | 75.90   | 86.62              | Interm B |
| Total / /         | Average       | 59                    | 93.36    | 1.207                        | 91.73   | 93.39              | Interm   |
|                   |               |                       |          |                              |         |                    |          |
| P06               | J26           | 14                    | 90.05    | 1.159                        | 16.11   | 16.11              | Surf 1   |
| P06               | J24           | 6                     | 90.44    | 1.455                        | 31.23   |                    | Surf 1D  |
| P06               | J24           | 6                     | 89.83    | 1.669                        | 21.47   |                    | Surf 1D  |
| P06               | J24           | 5                     | 92.36    | 0.481                        | 100.00  |                    | Surf 1D  |
| P06               | J24           | 4                     | 93.37    | 0.565                        | 100.00  |                    | Surf 1D  |
| P06               | J24           | 4                     | 92.45    | 0.522                        | 100.00  | 70.54              | Surf 1D  |
| P04               | J14           | 8                     | 88.73    | 1.624                        | 5.25    |                    | Surf 1R  |
| P04               | J14           | 8                     | 90.28    | 0.605                        | 5.25    |                    | Surf 1R  |
| P04               | J14           | 6                     | 90.08    | 1.271                        | 19.63   |                    | Surf 1R  |
| P04               | J14           | 9                     | 89.95    | 1.186                        | 14.62   |                    | Surf 1R  |
| P04               | J14           | 5                     | 89.94    | 1.356                        | 18.49   | 12.65              | Surf 1R  |
| P08               | J11           | 8                     | 88.65    | 1.161                        | 0.16    | 0.16               | Surf 1R  |
| P27               | J55           | 5                     | 92.71    | 0.546                        | 100.00  |                    | Surf B   |
| P27               | J55           | 6                     | 91.83    | 0.863                        | 75.68   |                    | Surf B   |
| P27               | J55           | 7                     | 92.50    | 0.504                        | 100.00  |                    | Surf B   |
| P27               | J55           | 6                     | 92.15    | 0.489                        | 99.83   | 93.88              | Surf B   |
| P27               | J70           | 5                     | 93.22    | 1.498                        | 92.95   |                    | Surf B   |
| P27               | J70           | 1                     | 93.36    | 0.949                        | 100.00  |                    | Surf B   |
| P27               | J70           | 4                     | 92.32    | 0.559                        | 100.00  |                    | Surf B   |
| P27               | J/U           | 5                     | 92.75    | 1.001                        | 97.10   |                    | Surf B   |
| P27               | J/0           | 3                     | 93.38    | 0.757                        | 100.00  |                    | Surf B   |
| P27               | J/U           | 6                     | 92.70    | 1.092                        | 92.85   | 07.50              | Surf B   |
| P20               | J/U           | 3<br>E                | 92.72    | 1.222                        | 100.00  | 97.00              | Surf D   |
| P30               | 105<br>165    | 5                     | 93.57    | 3.130                        | 52.85   | 76 40              | Surf D   |
| P30               | 20U           | 3<br>E                | 94.02    | 0.0/5                        | 100.00  | 10.43              | Surf P   |
| P31               | J/1           | 5                     | 94.00    | 0.200                        | 100.00  | 100.00             | Surf D   |
| P12               | J/ I          | 3                     | 94.24    | 0.022                        | 60.70   | 60.70              | Surf C   |
| FIJ               | 303           | Э                     | 92.01    | 1.019                        | 09.70   | 09.70              | Sunc     |

## Table C.2. Summary of Density Lot PWL Values for Each Other Paving Project

| Project<br>Number | JMF<br>Number | Lot<br>Sample<br>Size | Lot Mean | Lot<br>Standard<br>Deviation | Lot PWL | Average<br>Lot PWL | Міх Туре |  |
|-------------------|---------------|-----------------------|----------|------------------------------|---------|--------------------|----------|--|
| P14               | J16           | 6                     | 92.68    | 1.456                        | 84.26   |                    | Surf C   |  |
| P14               | J16           | 7                     | 92.92    | 1.035                        | 96.95   |                    | Surf C   |  |
| P14               | J16           | 6                     | 92.73    | 0.722                        | 100.00  |                    | Surf C   |  |
| P14               | J16           | 10                    | 91.75    | 1.788                        | 61.55   |                    | Surf C   |  |
| P14               | J16           | 5                     | 92.12    | 0.600                        | 96.83   |                    | Surf C   |  |
| P14               | J16           | 4                     | 93.07    | 1.135                        | 100.00  | 89.93              | Surf C   |  |
| P15               | J44           | 3                     | 92.75    | 0.751                        | 100.00  |                    | Surf C   |  |
| P15               | J44           | 3                     | 92.56    | 0.751                        | 100.00  |                    | Surf C   |  |
| P15               | J44           | 4                     | 92.60    | 1.908                        | 74.46   |                    | Surf C   |  |
| P15               | J44           | 4                     | 92.90    | 1.919                        | 79.53   |                    | Surf C   |  |
| P15               | J44           | 4                     | 92.60    | 1.908                        | 74.46   | 85.69              | Surf C   |  |
| P16               | J20           | 4                     | 91.38    | 1.445                        | 54.15   |                    | Surf C   |  |
| P16               | J20           | 4                     | 91.15    | 0.527                        | 46.84   |                    | Surf C   |  |
| P16               | J20           | 4                     | 92.22    | 0.967                        | 85.16   | 62.05              | Surf C   |  |
| P18               | J48           | 7                     | 91.62    | 1.883                        | 58.31   |                    | Surf C   |  |
| P18               | J48           | 3                     | 92.01    | 1.960                        | 61.65   |                    | Surf C   |  |
| P18               | J48           | 8                     | 91.31    | 1.884                        | 52.21   | 57.39              | Surf C   |  |
| P20               | J50           | 11                    | 92.63    | 0.936                        | 94.42   |                    | Surf C   |  |
| P20               | J50           | 12                    | 91.85    | 0.850                        | 77.46   |                    | Surf C   |  |
| P20               | J50           | 11                    | 92.17    | 0.916                        | 85.52   |                    | Surf C   |  |
| P20               | J50           | 7                     | 92.43    | 0.866                        | 93.38   |                    | Surf C   |  |
| P20               | J50           | 8                     | 92.72    | 1.239                        | 89.42   |                    | Surf C   |  |
| P20               | J50           | 8                     | 92.80    | 1.000                        | 95.84   |                    | Surf C   |  |
| P20               | J50           | 10                    | 92.36    | 0.610                        | 98.26   | 90.61              | Surf C   |  |
| P24               | J56           | 11                    | 92.90    | 1.636                        | 83.12   |                    | Surf C   |  |
| P24               | J56           | 4                     | 93.80    | 0.637                        | 100.00  |                    | Surf C   |  |
| P24               | J56           | 6                     | 93.54    | 1.088                        | 100.00  |                    | Surf C   |  |
| P24               | J56           | 8                     | 92.57    | 0.825                        | 96.57   |                    | Surf C   |  |
| P24               | J56           | 9                     | 93.37    | 0.894                        | 99.97   |                    | Surf C   |  |
| P24               | J56           | 9                     | 93.15    | 0.629                        | 100.00  |                    | Surf C   |  |
| P24               | J56           | 9                     | 93.05    | 1.037                        | 97.56   | 96.75              | Surf C   |  |
| P26               | J59           | 6                     | 91.69    | 0.945                        | 68.64   |                    | Surf C   |  |
| P26               | J59           | 8                     | 92.09    | 0.961                        | 81.94   |                    | Surf C   |  |
| P26               | J59           | 7                     | 90.40    | 1.338                        | 28.39   |                    | Surf C   |  |
| P26               | J59           | 11                    | 90.59    | 1.235                        | 31.52   |                    | Surf C   |  |
| P26               | J59           | 6                     | 91.16    | 0.706                        | 47.92   |                    | Surf C   |  |
| P26               | J59           | 7                     | 91.09    | 0.841                        | 45.11   |                    | Surf C   |  |
| P26               | J59           | 8                     | 90.06    | 1.795                        | 26.98   |                    | Surf C   |  |
| P26               | J59           | 2                     | 92.64    | 0.983                        | 100.00  | 53.81              | Surf C   |  |
|                   | Continued     |                       |          |                              |         |                    |          |  |

Table C.2. Summary of Density Lot PWL Values for Each Other Paving Project (continued)

| Project<br>Number | JMF<br>Number | Lot<br>Sample<br>Size | Lot Mean | Lot<br>Standard<br>Deviation | Lot PWL | Average<br>Lot PWL | Міх Туре |
|-------------------|---------------|-----------------------|----------|------------------------------|---------|--------------------|----------|
| P28               | J39           | 7                     | 92.98    | 0.999                        | 98.19   |                    | Surf C   |
| P28               | J39           | 11                    | 93.37    | 1.278                        | 95.40   |                    | Surf C   |
| P28               | J39           | 7                     | 93.27    | 1.861                        | 80.99   |                    | Surf C   |
| P28               | J39           | 3                     | 93.49    | 0.600                        | 100.00  | 93.65              | Surf C   |
|                   |               |                       |          |                              |         |                    |          |
| Total / /         | Average       | 457                   | 92.17    | 1.102                        | 75.44   | 68.64              | Surface  |
|                   |               |                       |          |                              |         |                    |          |
| Total / /         | Average       | 59                    | 93.36    | 1.207                        | 91.73   | 93.39              | Interm   |
|                   |               |                       |          |                              |         |                    |          |
| Total / A         | Average       | 516                   | 92.34    | 1.117                        | 77.96   | 73.36              | All      |

| Table C.2. Summary of Density Lot FWL values for Each Other Paving Project (continued | Table C.2. Summar | y of Density Lot PWL | Values for Each Other | Paving Project (continued |
|---|-------------------|----------------------|-----------------------|---------------------------|
|---|-------------------|----------------------|-----------------------|---------------------------|

#### APPENDIX D — VERIFICATION TEST DATA

The acceptance test results and their corresponding verification test results were provided by SCDOT for 10 projects. Most of these projects were different than those that were analyzed for determining typical process variability values. As such, the verification projects are referred to as V01 to V10. All of the test results along with the *F*-test and *t*-test results are presented in the following tables.

| Proj.<br>No. | Mix<br>Type | Lot<br>No. | Contr. | SCDOT |
|--------------|-------------|------------|--------|-------|
| V01          | Interm B    | 1          | 4.74   | 4.79  |
| V01          | Interm B    | 1          | 4.97   |       |
| V01          | Interm B    | 1          | 4.63   |       |
| V01          | Interm B    | 1          | 4.76   | 4.88  |
| V01          | Interm B    | 1          | 5.00   | 4.68  |
| V01          | Interm B    | 1          | 4.66   |       |
| V01          | Interm B    | 1          | 4.36   |       |
| V01          | Interm B    | 1          | 4.60   |       |
| V01          | Interm B    | 2          | 4.70   |       |
| V01          | Interm B    | 2          | 4.23   | 4.76  |
| V01          | Interm B    | 2          | 4.97   | 4.78  |
| V01          | Interm B    | 2          | 4.38   | 4.54  |
| V01          | Interm B    | 2          | 4.62   |       |
| V01          | Interm B    | 3          | 4.50   |       |
| V01          | Interm B    | 3          | 4.59   |       |
| V01          | Interm B    | 3          | 4.31   |       |
| V01          | Interm B    | 3          | 4.93   |       |
| V01          | Interm B    | 4          | 4.63   | 4.52  |
| V01          | Interm B    | 4          | 4.69   |       |
|              |             |            |        |       |
| V01          | Surf A      | 1          | 4.90   | 4.69  |
| V01          | Surf A      | 1          | 4.83   | 4.84  |
| V01          | Surf A      | 1          | 4.87   | 5.03  |
| V01          | Surf A      | 2          | 4.92   | 4.72  |
| V01          | Surf A      | 3          | 5.08   | 5.22  |
| V01          | Surf A      | 4          | 4.95   |       |
| V01          | Surf A      | 5          | 4.89   | 4.91  |
|              |             |            |        |       |
| V02          | Interm B    | 1          | 4.93   |       |
| V02          | Interm B    | 2          | 4.45   | 4.03  |
| V02          | Interm B    | 2          |        | 4.52  |
| V02          | Interm B    | 3          | 4.36   | 4.14  |
| V02          | Interm B    | 3          | 4.59   |       |
| V02          | Interm B    | 4          | 4.65   |       |
| V02          | Interm B    | 5          | 4.14   | 4.40  |
| V02          | Interm B    | 5          | 4.56   | 3.94  |
|              |             |            |        |       |
| V02          | Surf A      | 1          | 4.83   | 4.88  |
| V02          | Surf A      | 1          | 5.08   | 4.77  |
| V02          | Surf A      | 1          | 4.76   | 4.78  |
| V02          | Surf A      | 1          |        | 4.98  |
| V02          | Surf A      | 2          | 5.10   | 4.66  |
| V02          | Surf A      | 2          | 5.23   | 5.14  |
| V02          | Surf A      | 2          | 4.91   |       |
| V02          | Surf A      | 2          | 5.08   |       |
| V02          | Surf A      | 3          | 4.89   | 4.77  |
| V02          | Surf A      | 3          | 4.98   |       |
| V02          | Surf A      | 3          | 4.81   |       |
| V02          | Surf A      | 4          | 5.35   | 5.13  |
| V02          | Surf A      | 4          | 5.06   |       |

| Table D.1. Asphalt Content | <b>Verification</b> | Test | Results | Data |
|----------------------------|---------------------|------|---------|------|
|----------------------------|---------------------|------|---------|------|

| Proj.<br>No. | Mix<br>Type | Lot<br>No. | Contr. | SCDOT |
|--------------|-------------|------------|--------|-------|
| V02          | Surf A      | 4          | 5.32   |       |
| V02          | Surf A      | 5          | 4.88   |       |
| V02          | Surf A      | 5          | 5.03   |       |
| V02          | Surf A      | 5          | 4.74   |       |
| V02          | Surf A      | 5          | 5.01   |       |
| V02          | Surf A      | 5          | 4.54   | 4.80  |
| V02          | Surf A      | 5          | 5.14   |       |
|              |             |            |        |       |
| V02          | Surf A      | 6          | 4.98   | 5.05  |
| V02          | Surf A      | 6          | 4.93   |       |
| V02          | Surf A      | 6          | 4.96   |       |
| V02          | Surf A      | 6          | 4.77   |       |
| V02          | Surf A      | 7          | 5.06   | 4.86  |
| V02          | Surf A      | 7          | 4.99   |       |
| V02          | Surf A      | 7          | 5.12   |       |
| V02          | Surf A      | 8          | 4.87   | 4.35  |
| V02          | Surf A      | 8          | 4.71   |       |
| V02          | Surf A      | 8          | 5.01   |       |
| V02          | Surf A      | 9          | 5.07   | 4.83  |
| V02          | Surf A      | 9          | 5.08   |       |
| V02          | Surf A      | 9          | 5.01   | 4.79  |
| V02          | Surf A      | 9          | 4.96   |       |
| V02          | Surf A      | 9          | 5.20   |       |
| V02          | Surf A      | 10         | 4.93   | 4.92  |
| V02          | Surf A      | 10         | 5.05   |       |
| V02          | Surf A      | 10         | 5.08   | 5.11  |
|              |             |            |        |       |
| V02          | Surf A      | 11         | 5.01   | 4.86  |
| V02          | Surf A      | 11         | 4.89   |       |
| V02          | Surf A      | 11         | 5.13   | 5.20  |
| V02          | Surf A      | 11         | 5.25   |       |
| V02          | Surf A      | 11         | 4.90   |       |
| V02          | Surf A      | 12         | 4.80   |       |
| V02          | Surf A      | 12         | 4.95   |       |
| V02          | Surf A      | 12         | 5.07   |       |
| V02          | Surf A      | 12         | 4.89   |       |
| V02          | Surf A      | 13         | 5.21   | 5.13  |
| V02          | Surf A      | 13         | 4.88   |       |
| V02          | Surf A      | 13         | 4.93   |       |
| V02          | Surf A      | 13         | 5.02   |       |
| V02          | Surf A      | 14         | 5.23   | 5.08  |
| V02          | Surf A      | 14         | 4.87   |       |
| V02          | Surf A      | 14         | 4.89   |       |
| V02          | Surf A      | 14         | 5.02   | 5.03  |
| V02          | Surf A      | 14         | 5.04   |       |
| V02          | Surf A      | 14         | 4.74   |       |
| V02          | Surf A      | 15         | 5.18   | 5.04  |
| V02          | Surf A      | 15         | 4.73   | 5.25  |
| V02          | Surf A      | 15         | 5.11   |       |
| V02          | Surf A      | 15         | 4.91   |       |

| Proj.<br>No. | Mix<br>Type | Lot<br>No. | Contr.       | SCDOT |
|--------------|-------------|------------|--------------|-------|
|              |             |            |              |       |
| V02          | Surf A      | 16         | 5.12         | 4.97  |
| V02          | Surf A      | 16         | 4.58         | 4.91  |
| V02          | Surf A      | 16         | 5.00         |       |
| V02          | Surf A      | 16         | 5.08         |       |
| V02          | Surf A      | 17         | 4.81         | 5.16  |
| V02          | Surf A      | 17         | 4.81         | 5.10  |
| V02          | Surf A      | 17         | 4.73         |       |
| V02          | Surf A      | 17         | 4.78         |       |
| V02          | Surf A      | 18         | 5.17         | 4.84  |
| V02          | Surf A      | 18         | 4.66         |       |
| V02          | Surf A      | 18         | 5.00         | 4.79  |
| V02          | Surf A      | 18         | 5.17         |       |
| V02          | Surf A      | 19         | 4.86         | 4.94  |
| V02          | Surf A      | 19         | 4.97         |       |
| V02          | Surf A      | 19         | 5.35         | 5.00  |
| V02          | Surf A      | 19         | 4.83         | 0.00  |
| V02          | Surf A      | 20         | 5.03         | 5 19  |
| V02          | Surf A      | 20         | 4 90         | 0.10  |
| V02          | Surf A      | 20         | 4.67         |       |
| V02          | Surf A      | 20         | 4.07         |       |
| V02          | Sull A      | 20         | 4.37         |       |
| V02          | Surf A      | 21         | 5 1 1        | 5.22  |
| V02          | Surf A      | 21         | 5.14         | 0.22  |
| V02          | Surf A      | 21         | 4.89         |       |
| V02          | Surf A      | 21         | 4.00         |       |
| V02          | Surf A      | 22         | 5.16         |       |
| V02          | Surf A      | 22         | 4 79         |       |
| V02          | Surf A      | 18         | 5.17         | 4 84  |
| V02          | Surf A      | 18         | 4.66         | 4.04  |
| V02          |             | 18         | 5.00         | 4 70  |
| V02          |             | 18         | 5.00         | 4.75  |
| V02          |             | 10         | 4.86         | 1 01  |
| V02          | Surf A      | 10         | 4.00         | 4.34  |
| V02          | Surf A      | 10         | 5.35         | 5.00  |
| V02          | Surf A      | 10         | 1.92         | 0.00  |
| V02          | Surf A      | 20         | 4.03<br>5.02 | 5 10  |
| V02          | Surf A      | 20         | 1.00         | 5.19  |
| V02          | Sull A      | 20         | 4.90         |       |
| V02          | Sull A      | 20         | 4.07         |       |
| V02          | Suff A      | 20         | 4.97         |       |
| 1/02         | Curf D      | 4          | 5.07         | E 40  |
| V02          |             | 1          | 5.27         | 5.18  |
| V02          | Surf B      | 1          | 5.19         | 4.70  |
| V02          | Surf B      | 1          | 5.30         | 4.79  |
| V02          | Surf B      | 1          | 4.87         | 4.00  |
| V02          | Surf B      | 2          | 5.27         | 4.82  |
| V02          | Surf B      | 2          | 5.12         | 4.65  |
| V02          | Surf B      | 2          | 5.14         | 4.96  |
| V02          | Surf B      | 2          | 5.04         | 4.56  |
| V02          | Surf B      | 2          | 4.83         |       |

| Proj. | Mix    | Lot | Contr. | SCDOT |
|-------|--------|-----|--------|-------|
| NO.   | Type   | NO. | 5.00   | 1/00  |
| V02   | Surf B | 3   | 5.09   | V02   |
| V02   | Surf B | 3   | 4.75   | V02   |
| V02   | Surf B | 3   | 5.09   | V02   |
| V02   | Surf B | 4   | 5.26   | V02   |
| V02   | Surf B | 4   | 4.98   | V02   |
| V02   | Surf B | 4   | 5.18   | V02   |
| V02   | Surf B | 6   | 4.96   | V02   |
| V02   | Surf B | 6   | 4.98   | V02   |
| V02   | Surf B | 6   | 5.04   | V02   |
|       |        |     |        |       |
| V02   | Surf B | 2   | 5.10   | V02   |
| V02   | Surf B | 2   | 5.07   | V02   |
| V02   | Surf B | 2   | 5.07   | V02   |
| V02   | Surf B | 3   | 4.76   | V02   |
| V02   | Surf B | 3   | 5.16   | V02   |
| V02   | Surf B | 3   | 5.05   | V02   |
| V02   | Surf B | 4   | 5.20   | V02   |
| V02   | Surf B | 4   | 4.74   | V02   |
| V02   | Surf B | 4   | 5.01   | V02   |
| V02   | Surf B | 4   | 5.34   | V02   |
| V02   | Surf B | 5   | 5.23   | V02   |
| V02   | Surf B | 5   | 5.15   | V02   |
| V02   | Surf B | 5   | 5.03   | V02   |
| V02   | Surf B | 6   | 5.21   | V02   |
| V02   | Surf B | 6   | 5.09   | V02   |
| V02   | Surf B | 6   | 4.95   | V02   |
| V02   | Surf B | 6   | 5.12   | V02   |
| V02   | Surf B | 6   | 4.80   | V02   |
|       |        |     |        |       |
| V02   | Surf B | 5   | 4.93   | V02   |
| V02   | Surf B | 5   | 5.03   | V02   |
| V02   | Surf B | 5   | 4.93   | V02   |
| V02   | Surf B | 6   | 5.11   | V02   |
| V02   | Surf B | 6   | 4.76   | V02   |
| V02   | Surf B | 6   | 4.92   | V02   |
| V02   | Surf B | 6   | 5.05   | V02   |
| V02   | Surf B | 6   | 4.83   | V02   |
| V02   | Surf B | 6   | 4.95   | V02   |
| V02   | Surf B | 7   | 4.77   | V02   |
| V02   | Surf B | 7   | 5.20   | V02   |
| V02   | Surf B | 7   | 4.88   | V02   |
| V02   | Surf B | 7   | 4.88   | V02   |
| V02   | Surf B | 8   | 4.96   | V02   |
| V02   | Surf B | 8   | 5.10   | V02   |
| V02   | Surf B | 8   | 5.08   | V02   |
| V02   | Surf B | 9   | 5.07   | V02   |
| V02   | Surf B | 9   | 4.78   | V02   |
| V02   | Surf B | 9   | 4.70   | V02   |
|       |        |     |        |       |
| V02   | Surf B | 10  | 4.98   | V02   |

# Table D.1. Asphalt Content Verification Test Results Data (continued)

| Proj.<br>No. | Mix<br>Type | Lot<br>No. | Contr. | SCDOT |
|--------------|-------------|------------|--------|-------|
| V02          | Surf B      | 10         | 4.83   | 4.89  |
| V02          | Surf B      | 10         | 5.04   |       |
| V02          | Surf B      | 11         | 5.30   |       |
| V02          | Surf B      | 11         | 5.21   |       |
| V02          | Surf B      | 11         | 4.87   |       |
| V02          | Surf B      | 12         | 4.78   | 4.88  |
| V02          | Surf B      | 12         | 4.57   |       |
| V02          | Surf B      | 12         | 5.11   |       |
| V02          | Surf B      | 12         | 5.23   |       |
| V02          | Surf B      | 13         | 4.93   |       |
| V02          | Surf B      | 7          | 5.23   | 5.01  |
| V02          | Surf B      | 7          | 5.06   | 5.18  |
| V02          | Surf B      |            |        | 4.93  |
|              |             |            |        |       |
| V03          | Surf E      | 1          | 6.32   | 6.54  |
| V03          | Surf E      | 2          | 5.99   | 6.08  |
| V03          | Surf E      | 2          | 5.96   |       |
| V03          | Surf E      | 3          | 6.15   | 5.76  |
| V03          | Surf E      | 3          | 6.09   | 5.81  |
| V03          | Surf E      | 3          | 6.21   |       |
| V03          | Surf E      | 4          | 6.13   |       |
| V03          | Surf E      | 4          | 5.65   |       |
| V03          | Surf E      | 4          | 6.10   |       |
| V03          | Surf E      | 5          | 5.87   | 5.68  |
|              |             |            |        |       |
| V03          | Surf E      | 6          | 5.98   | 5.97  |
| V03          | Surf E      | 6          | 6.06   |       |
| V03          | Surf E      | 7          | 6.20   | 6.11  |
| V03          | Surf E      | 7          | 6.18   | 5.37  |
| V03          | Surf E      | 8          | 5.35   |       |
| V03          | Surf E      | 9          | 6.05   |       |
| V03          | Surf E      | 10         | 6.07   | 5.76  |
| V03          | Surf E      |            |        | 6.45  |
|              |             |            |        |       |
| V03          | Surf E      | 11         | 5.99   |       |
| V03          | Surf E      | 12         | 6.11   | 5.27  |
| V03          | Surf E      | 13         | 6.09   | 5.95  |
| V03          | Surf E      | 1          | 5.92   | 5.94  |
| V03          | Surf E      | 2          | 5.98   |       |
| V03          | Surf E      | 2          | 6.14   |       |
|              |             |            |        |       |
| V03          | Surf E      | 14         | 6.09   | 5.77  |
| V03          | Surf E      | 14         | 6.08   |       |
| V03          | Surf E      | 15         | 6.17   | 5.78  |
| V03          | Surf E      | 15         | 6.06   |       |
| V03          | Surf E      | 15         | 6.10   |       |
| V03          | Surf E      | 16         | 5.89   | 5.99  |
| V03          | Surf E      | 16         | 5.84   |       |
| V03          | Surf E      | 16         | 5.93   |       |
| V03          | Surf E      | 17         | 6.00   | 5.83  |

| Proj.<br>No. | Mix<br>Type | Lot No.   | Contr. | SCDOT |
|--------------|-------------|-----------|--------|-------|
| V03          | Surf E      | 17/Sumter | 6.12   | 6.04  |
| V03          | Surf E      | 17/Sumter | 6.18   |       |
| V03          | Surf E      | 18/Sumter | 6.02   | 6.02  |
| V03          | Surf E      | 18/Sumter | 6.06   | 6.01  |
| V03          | Surf E      | 18/Sumter | 6.14   | 6.15  |
|              |             |           |        |       |
| V03          | Surf E      | 19        | 6.12   | 6.18  |
| V03          | Surf E      | 19        | 6.03   | 6.02  |
| V03          | Surf E      | 19        | 6.17   |       |
| V03          | Surf E      | 19        | 6.17   |       |
| V03          | Surf E      | 20        | 5.91   | 6.05  |
| V03          | Surf E      | 20        | 5.88   |       |
| V03          | Surf E      | 20        | 5.93   |       |
| V03          | Surf E      | 21        | 6.29   | 6.06  |
| V03          | Surf E      | 21        | 6.02   |       |
| V03          | Surf E      | 21        | 6.16   |       |
| V03          | Surf E      | 21        | 6.11   |       |
| V03          | Surf E      | 22        | 5.69   | 5.95  |
| V03          | Surf E      | 22        | 6.54   | 6.10  |
| V03          | Surf E      | 22        | 6.29   |       |
| V03          | Surf E      | 22        | 6.04   |       |
| V03          | Surf E      | 23        | 5.91   | 5.91  |
| V03          | Surf F      | 23        | 6.21   | 6.12  |
| V03          | Surf F      | 23        | 6.26   | 02    |
|              | 0011 2      |           | 0.20   |       |
| V03          | Surf E      | 24        | 6.22   | 6.35  |
| V03          | Surf E      | 24        | 6.04   |       |
| V03          | Surf E      | 24        | 5.85   |       |
| V03          | Surf E      | 24        | 6.33   |       |
| V03          | Surf E      | 25        | 6.07   |       |
| V03          | Surf E      | 25        | 6.06   |       |
| V03          | Surf E      | 25        | 6.18   |       |
| V03          | Surf E      | 26        | 6.31   | 6.32  |
| V03          | Surf E      | 26        | 6.32   | 6.65  |
| V03          | Surf E      | 26        | 6.27   |       |
| V03          | Surf E      | 26        | 6.01   |       |
| V03          | Surf E      | 27        | 5.89   | 5.74  |
| V03          | Surf E      | 27        | 5.86   | 5.78  |
| V03          | Surf E      | 28        | 5.93   |       |
|              |             |           |        |       |
| V04          | Surf B      | 1         | 5.25   | 5.48  |
| V04          | Surf B      | 1         | 5.08   | 5.34  |
| V04          | Surf B      | 1         | 4.86   |       |
| V04          | Surf B      | 1         | 5.01   | 5.16  |
| V04          | Surf B      | 1         | 5.00   |       |
| V04          | Surf B      | 2         | 4.96   | 5.42  |
| V04          | Surf B      | 2         | 4.85   |       |
| V04          | Surf B      | 2         | 5.03   |       |
| V04          | Surf B      | 2         | 5.13   |       |
| V04          | Surf B      | 3         | 4.89   | 4.94  |

| Proj.<br>No. | Mix<br>Type | Lot<br>No. | Contr. | SCDOT |
|--------------|-------------|------------|--------|-------|
| V04          | Surf B      | 3          | 4.96   | 4.99  |
| V04          | Surf B      | 3          | 4.70   | 4.91  |
| V04          | Surf B      | 3          | 4.82   |       |
| V04          | Surf B      | 4          | 4.55   | 4.43  |
| V04          | Surf B      | 4          | 4.59   |       |
| V04          | Surf B      | 4          | 4.71   |       |
| V04          | Surf B      | 5          | 4.84   | 4.93  |
| V04          | Surf B      | 5          | 4.84   | 4.74  |
| V04          | Surf B      | 5          | 4.79   |       |
| V04          | Surf B      | 5          | 4.79   |       |
| V04          | Surf B      | 6          | 4.80   | 4.62  |
| V04          | Surf B      | 6          | 4.68   |       |
| V04          | Surf B      | 6          | 4.43   |       |
| V04          | Surf B      | 6          | 4.82   |       |
| V04          | Surf B      | 6          | 4.99   |       |
|              |             |            |        |       |
| V05          | Interm B    | 2          | 4.82   | 5.27  |
| V05          | Interm B    | 2          | 4.85   |       |
| V05          | Interm B    | 2          | 5.18   | 5.38  |
| V05          | Interm B    | 2          | 5.15   |       |
| V05          | Interm B    | 3          | 4.74   | 5.28  |
| V05          | Interm B    | 3          | 4.76   |       |
| V05          | Interm B    | 3          | 4.75   |       |
| V05          | Interm B    | 4          | 5.21   |       |
| V05          | Interm B    | 4          | 5.37   | 5.55  |
| V05          | Interm B    | 4          | 4.95   |       |
| V05          | Interm B    | 4          | 4.98   |       |
| V05          | Interm B    | 4          | 4.59   |       |
| V05          | Interm B    | 5          | 5.05   | 5.22  |
| V05          | Interm B    | 5          | 4.93   | 5.25  |
| V05          | Interm B    | 5          | 4.89   |       |
| V05          | Interm B    | 5          | 5.04   |       |
| V05          | Interm B    | 6          | 4.80   |       |
| V05          | Interm B    | 6          | 4.86   |       |
| V05          | Interm B    | 6          | 5.07   |       |
| V05          | Interm B    | 6          | 4.73   |       |
|              |             |            |        |       |
| V05          | Interm B    | 7          | 5.07   |       |
| V05          | Interm B    | 7          | 5.13   |       |
| V05          | Interm B    | 7          | 5.07   |       |
| V05          | Interm B    | 8          | 4.70   | 5.06  |
| V05          | Interm B    | 8          | 4.55   |       |
| V05          | Interm B    | 8          | 5.13   |       |
| V05          | Interm B    | 9          | 4.96   |       |
| V05          | Interm B    | 9          | 4.92   | 5.16  |
| V05          | Interm B    | 9          | 4.90   | 5.49  |
| V05          | Interm B    | 10         | 4.75   | 5.34  |
| V05          | Interm B    | 10         |        | 5.15  |
| V05          | Interm B    | 11         | 4.79   | 5.11  |
| V05          | Interm B    | 11         | 4.82   |       |

| Table D.1. Asphalt Content Verification | <b>Test Results Data</b> | (continued) |
|---|--------------------------|-------------|
|---|--------------------------|-------------|

| Proj.<br>No. | Mix<br>Type | Lot<br>No. | Contr. | SCDOT |
|--------------|-------------|------------|--------|-------|
| V05          | Interm B    | 11         | 4.95   |       |
| V05          | Interm B    | 11         | 4.97   |       |
| 100          |             |            |        |       |
| V05          | Interm B    | 12         | 4.92   | 5.37  |
| V05          | Interm B    | 12         | 5.13   |       |
| V05          | Interm B    | 12         | 5.33   | 5.44  |
| V05          | Interm B    | 12         | 4.98   |       |
| V05          | Interm B    | 13         | 5.42   | 5.20  |
| V05          | Interm B    | 13         | 4.88   |       |
| V05          | Interm B    | 13         | 5.05   |       |
| V05          | Interm B    | 14         | 5.01   | 5.42  |
| V05          | Interm B    | 14         | 4.90   | 5.27  |
| V05          | Interm B    | 14         | 5.13   |       |
| V05          | Interm B    | 15         | 4.48   |       |
| V05          | Interm B    | 11         | 4.79   | 5.11  |
| V05          | Interm B    | 11         | 4.82   |       |
| V05          | Interm B    | 11         | 4.95   |       |
| V05          | Interm B    | 11         | 4.97   |       |
|              |             |            |        |       |
| V05          | Surf A      | 1          | 5.41   |       |
| V05          | Surf A      | 1          | 5.17   |       |
| V05          | Surf A      | 2          | 5.16   | 5.34  |
| V05          | Surf A      | 2          | 5.25   |       |
| V05          | Surf A      | 2          | 5.17   | 5.28  |
| V05          | Surf A      | 2          | 5.28   |       |
| V05          | Surf A      | 2          | 5.33   |       |
| V05          | Surf A      | 2          | 5.16   |       |
| V05          | Surf A      | 3          | 5.29   | 5.34  |
| V05          | Surf A      | 3          | 5.19   |       |
| V05          | Surf A      | 3          | 5.20   |       |
| V05          | Surf A      | 3          | 5.30   |       |
| V05          | Surf A      | 3          | 5.34   |       |
| V05          | Surf A      | 4          | 5.22   | 5.29  |
| V05          | Surf A      | 4          | 5.23   |       |
| V05          | Surf A      | 4          | 5.01   |       |
| V05          | Surf A      | 4          | 5.31   |       |
| V05          | Surf A      | 5          | 5.11   | 5.50  |
| V05          | Surf A      | 5          | 5.36   |       |
| V05          | Surf A      | 5          | 5.19   |       |
|              |             |            |        |       |
| V05          | Surf A      | 6          | 4.77   | 4.72  |
| V05          | Surf A      | 6          | 4.91   |       |
| V05          | Surf A      | 6          | 5.11   | 5.15  |
| V05          | Surf A      | 6          | 5.13   |       |
| V05          | Surf A      | 7          | 5.11   | 5.09  |
| V05          | Surf A      | 7          | 5.08   |       |
| V05          | Surf A      | 7          | 5.22   |       |
| V05          | Surf A      | 8          | 5.06   | 5.13  |
| V05          | Surf A      | 8          | 5.09   |       |
| V05          | Surf A      | 8          | 5.18   |       |

| Proj.<br>No. | Mix<br>Type | Lot<br>No. | Contr. | SCDOT |
|--------------|-------------|------------|--------|-------|
| V05          | Surf A      | 9          | 5.28   | 5.11  |
| V05          | Surf A      | 9          | 5.20   | 5.20  |
| V05          | Surf A      | 9          | 5.17   |       |
| V05          | Surf A      | 10         | 5.22   | 5.18  |
| V05          | Surf A      | 10         | 5.18   | 5.27  |
| V05          | Surf A      | 10         | 5.35   |       |
| V05          | Surf A      | 10         | 5.10   |       |
|              |             | -          |        |       |
| V05          | Surf A      | 11         | 5.01   |       |
| V05          | Surf A      | 11         | 5.07   | 4.94  |
| V05          | Surf A      | 11         | 5.31   | 4.92  |
| V05          | Surf A      | 11         | 4.93   |       |
| V05          | Surf A      | 11         | 5.37   |       |
| V05          | Surf A      | 12         | 5.13   | 5.01  |
| V05          | Surf A      | 12         | 4.86   | 5.03  |
| V05          | Surf A      | 12         | 5.20   |       |
| V05          | Surf A      | 12         | 5.15   |       |
| V05          | Surf A      | 13         | 5.02   | 5.14  |
| V05          | Surf A      | 13         | 4.64   | 4.96  |
| V05          | Surf A      | 13         | 4.69   |       |
| V05          | Surf A      | 13         | 4.93   |       |
| V05          | Surf A      | 13         | 4.90   | 5.27  |
| V05          | Surf A      | 14         | 4.81   |       |
| V05          | Surf A      | 14         | 4.97   |       |
| V05          | Surf A      | 14         | 4.77   | 5.14  |
| V05          | Surf A      | 15         | 5.08   |       |
| V05          | Surf A      | 15         | 5.08   | 5.25  |
| V05          | Surf A      | 15         | 5.28   |       |
| V05          | Surf A      | 15         | 5.19   |       |
| V05          | Surf A      | 15         | 5.25   | 5.32  |
|              |             |            |        |       |
| V05          | Surf A      | 16         | 5.34   |       |
| V05          | Surf A      | 16         | 5.10   | 5.26  |
| V05          | Surf A      | 16         | 5.04   |       |
| V05          | Surf A      | 16         | 5.06   |       |
| V05          | Surf A      | 16         | 5.10   | 5.52  |
| V05          | Surf A      | 17         | 5.20   |       |
| V05          | Surf A      | 17         | 5.03   |       |
| V05          | Surf A      | 17         | 5.10   | 5.42  |
| V05          | Surf A      | 17         | 4.89   |       |
| V05          | Surf A      | 17         | 4.66   |       |
| V05          | Surf A      | 18         | 5.11   |       |
| V05          | Surf A      | 18         | 5.32   |       |
| V05          | Surf A      | 18         | 5.08   | 5.33  |
| V05          | Surf A      | 18         | 5.11   |       |
| V05          | Surf A      | 18         | 5.12   | 5.49  |
| V05          | Surf A      | 19         | 5.17   |       |
| V05          | Surf A      | 19         | 5.32   | 5.58  |
| V05          | Surf A      | 19         | 5.22   | 5.65  |
| V05          | Surf A      | 20         | 5.16   | 5.45  |

| Table D.1. Aspha | It Content | Verification | Test Res | sults Data | (continued) |
|------------------|------------|--------------|----------|------------|-------------|
|------------------|------------|--------------|----------|------------|-------------|

| Proj.<br>No. | Mix<br>Type | Lot<br>No. | Contr. | SCDOT |
|--------------|-------------|------------|--------|-------|
| V05          | Surf A      | 20         | 5.38   |       |
| V05          | Surf A      | 20         | 5.36   | 5.65  |
| V05          | Surf A      | 20         | 5.22   |       |
| V05          | Surf A      | 20         | 4.86   |       |
|              |             |            |        |       |
| V05          | Surf A      | 21         | 5.07   | 5.18  |
| V05          | Surf A      | 21         | 4.94   |       |
| V05          | Surf A      | 21         | 4.93   |       |
| V05          | Surf A      | 22         | 5.25   |       |
| V05          | Surf A      | 22         | 5.02   | 5.17  |
| V05          | Surf A      | 22         | 5.06   | 5.13  |
| V05          | Surf A      | 23         | 5.18   | 5.28  |
| V05          | Surf A      | 23         | 4.98   |       |
| V05          | Surf A      | 23         | 5.06   |       |
| V05          | Surf A      | 23         | 5.17   |       |
| V05          | Surf A      | 24         | 5.14   | 5.15  |
| V05          | Surf A      | 24         | 5.08   |       |
| V05          | Surf A      | 24         | 5.07   |       |
| V05          | Surf A      | 25         | 5.17   |       |
| V05          | Surf A      | 25         | 4.89   |       |
|              |             |            |        |       |
| V05          | Surf B      | 1          | 4.96   |       |
| V05          | Surf B      | 1          | 4.81   |       |
| V05          | Surf B      | 1          | 5.14   | 5.18  |
| V05          | Surf B      | 1          | 5.05   |       |
| V05          | Surf B      | 1          | 5.17   |       |
| V05          | Surf B      | 2          | 5.06   |       |
| V05          | Surf B      | 2          | 5.22   | 5.08  |
| V05          | Surf B      | 2          | 4.85   |       |
| V05          | Surf B      | 2          | 5.11   | 5.10  |
| V05          | Surf B      | 2          | 4.94   |       |
| V05          | Surf B      | 2          | 4.86   | 5.13  |
| V05          | Surf B      | 3          | 4.90   |       |
| V05          | Surf B      | 3          | 5.22   |       |
| V05          | Surf B      | 3          | 4.78   | 5.09  |
| V05          | Surf B      | 4          | 5.13   |       |
| V05          | Surf B      | 4          | 5.29   |       |
| V05          | Surf B      | 4          | 5.22   |       |
| V05          | Surf B      | 5          | 5.08   | 5.23  |
| V05          | Surf B      | 5          | 4.95   | 5.34  |
| V05          | Surf B      | 5          | 5.18   |       |
| V05          | Surf B      | 5          | 4.86   |       |
| V05          | Surf B      | 5          | 5.32   |       |
|              |             |            |        |       |
| V05          | Surf B      | 6          | 5.17   | 5.40  |
| V05          | Surf B      | 6          | 5.19   | 5.36  |
| V05          | Surf B      | 6          | 4.96   | 5.37  |
| V05          | Surf B      | 6          | 5.17   |       |
| V05          | Surf B      | 6          | 5.19   |       |
| V05          | Surf B      | 7          | 5.31   |       |

| Proj.<br>No. | Mix<br>Type | Lot<br>No. | Contr. | SCDOT |
|--------------|-------------|------------|--------|-------|
| V05          | Surf B      | 7          | 5.06   |       |
| V05          | Surf B      | 7          | 5.07   |       |
| V05          | Surf B      | 8          | 5.38   | 5.32  |
| V05          | Surf B      | 8          | 4.64   |       |
| V05          | Surf B      | 8          | 5.16   | 5.39  |
| V05          | Surf B      | 8          | 5.00   |       |
| V05          | Surf B      | 4          | 5.13   |       |
| V05          | Surf B      | 4          | 5.29   |       |
| V05          | Surf B      | 4          | 5.22   |       |
| V05          | Surf B      | 5          | 5.08   | 5.23  |
| V05          | Surf B      | 5          | 4.95   | 5.34  |
| V05          | Surf B      | 5          | 5.18   |       |
| V05          | Surf B      | 5          | 4.86   |       |
| V05          | Surf B      | 5          | 5.32   |       |
|              |             |            |        |       |
| V05          | Surf E      | 1          | 6.22   | 6.72  |
| V05          | Surf E      | 2          | 6.06   | 6.09  |
| V05          | Surf E      | 3          | 5.75   |       |
| V05          | Surf E      | 5          | 5.88   | 6.36  |
| V05          | Surf E      |            |        | 5.91  |
| V05          | Surf E      |            |        | 6.03  |
|              |             |            |        |       |
| V05          | Surf E      | 6          | 5.64   | 5.93  |
| V05          | Surf E      | 6          |        | 5.88  |
| V05          | Surf E      | 7          | 5.71   | 5.91  |
| V05          | Surf E      | 7          | 6.06   | 6.10  |
| V05          | Surf E      | 8          | 5.92   | 6.22  |
| V05          | Surf E      | 8          | 6.12   |       |
| V05          | Surf E      | 9          | 6.12   | 6.18  |
| V05          | Surf E      | 9          | 5.92   | 6.21  |
| V05          | Surf E      | 10         | 5.68   | 6.05  |
| V05          | Surf E      | 10         | 6.01   |       |
| V05          | Surf E      | 10         | 6.31   |       |
|              |             |            |        |       |
| V05          | Surf E      | 11         | 5.92   | 6.17  |
| V05          | Surf E      | 11         |        | 5.99  |
| V05          | Surf E      | 12         | 6.31   | 6.47  |
| V05          | Surf E      | 14         | 6.15   | 6.32  |
|              |             |            |        |       |
| V05          | Surf E      | 21         | 6.08   | 6.40  |
| V05          | Surf E      | 21         |        | 6.38  |
| V05          | Surf E      | 22         | 5.96   | 6.24  |
| V05          | Surf E      | 23         |        | 6.33  |
| V05          | Surf E      | 24         | 6.18   | 6.36  |
| V05          | Surf E      | 25         | 6.04   | 6.39  |
|              |             |            |        |       |
| V05          | Surf E      | 26         | 5.94   | 5.84  |
| V05          | Surf E      | 27         | 6.11   | 6.05  |
| V05          | Surf E      | 28         | 5.93   | 5.96  |
| V05          | Surf E      | 29         |        | 6.11  |

| Table D.1. Asphalt Content Verificatio | n Test Results Data ( <i>continued</i> ) |
|--|--|
|--|--|

| Proj.<br>No. | Mix<br>Type | Lot<br>No. | Contr. | SCDOT |
|--------------|-------------|------------|--------|-------|
| V05          | Surf E      | 30         | 5.96   | 5.94  |
| V05          | Surf E      | 30         | 6.02   | 6.18  |
|              |             |            |        |       |
| V05          | Surf E      | 31         | 6.19   | 5.93  |
| V05          | Surf E      | 31         | 5.95   | 6.03  |
| V05          | Surf E      | 31         |        | 6.06  |
| V05          | Surf E      | 32         | 5.84   | 6.14  |
| V05          | Surf E      | 32         | 5.83   | 6.11  |
| V05          | Surf E      | 33         | 5.59   | 6.20  |
| V05          | Surf E      | 35         | 5.93   |       |
|              |             |            |        |       |
| V05          | Surf E      | 36         | 5.76   | 6.04  |
| V05          | Surf E      | 36         |        | 6.12  |
| V05          | Surf E      | 36         |        | 5.85  |
| V05          | Surf E      | 37         | 6.34   | 5.79  |
| V05          | Surf E      | 38         | 5.95   | 6.02  |
| V05          | Surf E      | 38         | 5.79   | 6.00  |
| V05          | Surf E      | 38         | 5.91   |       |
|              |             |            |        |       |
| V06          | Interm C    | 1          | 5.27   |       |
| V06          | Interm C    | 2          | 5.22   | 4.94  |
| V06          | Interm C    | 3          | 5.16   | 5.17  |
| V06          | Interm C    | 3          |        | 5.41  |
| V06          | Interm C    | 4          | 5.22   | 5.44  |
| V06          | Interm C    | 5          | 5.62   |       |
| V06          | Interm C    | 5          | 5.16   |       |
|              |             |            |        |       |
| V07          | Base A      | 1          | 5.09   | 5.40  |
| V07          | Base A      | 1          | 5.55   |       |
| V07          | Base A      | 2          | 5.13   | 5.13  |
| V07          | Base A      | 2          | 5.29   |       |
| V07          | Base A      | 2          | 5.09   |       |
| V07          | Base A      | 3          | 5.87   | 5.54  |
| V07          | Base A      | 3          | 4.77   |       |
| V07          | Base A      | 3          | 4.52   |       |
| V07          | Base A      | 4          | 4.83   | 5.45  |
| V07          | Base A      | 4          | 5.14   |       |
| V07          | Base A      | 4          | 4.97   |       |
| V07          | Base A      | 4          | 5.15   |       |
| V07          | Base A      | 5          | 5.32   | 5.56  |
| V07          | Base A      | 5          | 4.81   |       |
| V07          | Base A      | 5          | 4.15   |       |
|              |             | 6          |        |       |
| V07          | Base A      | 6          | 4.65   |       |
| V07          | Base A      | 6          | 5.02   |       |
| V07          | Base A      | 6          | 4.96   |       |
| V07          | Base A      | -          | 4.94   | 5.04  |
| V07          | Base A      | 7          | 5.06   | 5.20  |
| V07          | Base A      | 8          | 5.29   | 5.18  |
| V07          | ыase A      | 8          | 4.91   | 5.13  |

| Proj.       | Mix    | Lot      | Contr.       | SCDOT |
|-------------|--------|----------|--------------|-------|
| 140.<br>V07 | Boso A | NO.<br>0 | 4.07         | 4.07  |
| V07         | Base A | 0        | 4.97<br>5.20 | 4.97  |
| V07         | Dase A | 0        | 5.20         |       |
| V07         | Dase A | 0        | 3.00         | E 22  |
| V07         | Dase A | 9        | 4.93         | 0.32  |
| V07         | Dase A | 9        | 5.09         |       |
| V07         | Base A | 9        | 0.00         | 4.02  |
| V07         | Dase A | 10       | 4.00         | 4.92  |
| V07         | Dase A |          |              | 5.26  |
| V07         | Base A | 11       | 5.56         | 4.85  |
| V07         | Base A | 12       | 4.75         | 5.09  |
| V07         | Base A | 13       | 4.75         | 5.39  |
| V07         | Base A | 13       | 4.20         | 0.00  |
| V07         | Base A | 14       | 4.59         | 4.29  |
| V07         | Base A | 14       | 5.02         |       |
| V07         | Base A | 15       | 5.13         |       |
| 101         | Baserr | 10       | 0.10         |       |
| V07         | Base A | 16       | 5.32         | 4.54  |
| V07         | Base A | 17       | 4.80         | 5.30  |
| V07         | Base A | 17       | 1.00         | 5.40  |
| V07         | Base A | 18       | 4.88         | 5.14  |
| V07         | Base A | 18       | 1.00         | 5.41  |
| V07         | Base A | 19       | 5 4 2        | 5 4 9 |
| V07         | Base A | 19       | 0.72         | 574   |
| V07         | Base A | 20       | 4 80         | 0.7 1 |
| V07         | Base A | 20       | 4 95         |       |
|             | Baserr | 20       | 1.00         |       |
| V07         | Base A | 21       | 4.66         | 4.54  |
| V07         | Base A | 1        | 4.57         | 4.98  |
| V07         | Base A | 2        | 4.36         | 4.82  |
| V07         | Base A | 2        |              | 4.64  |
| V07         | Base A | 3        | 5.17         | 5.02  |
| V07         | Base A | 3        |              | 4.79  |
| V07         | Base A | 4        | 4.88         |       |
|             |        |          |              |       |
| V07         | Base A | 5        | 5.40         |       |
| V07         | Base A | 6        | 4.84         | 4.40  |
| V07         | Base A | 6        |              | 4.66  |
| V07         | Base A | 7        | 5.02         | 5.18  |
| V07         | Base A | 8        | 5.07         | 4.72  |
| V07         | Base A | 8        |              | 4.59  |
| V07         | Base A | 9        | 5.06         |       |
|             |        |          |              |       |
| V07         | Base A | 10       | 4.92         |       |
| V07         | Base A | 11       | 5.31         | 4.64  |
| V07         | Base A | 12       | 4.83         | 5.18  |
| V07         | Base A | 13       | 5.13         | 5.41  |
| V07         | Base A | 14       | 4.68         | 4.83  |
|             |        |          |              |       |
| V07         | Base A | 15       | 5.33         | 4.92  |

# Table D.1. Asphalt Content Verification Test Results Data (continued)

| Proj.<br>No. | Mix<br>Type | Lot<br>No. | Contr. | SCDOT |
|--------------|-------------|------------|--------|-------|
| V07          | Base A      | 16         | 4.59   | 5.13  |
| V07          | Base A      | 17         | 4.74   |       |
| V07          | Base A      | 18         | 4.81   |       |
| V07          | Base A      | 19         | 4.97   | 4.99  |
| V07          | Base A      | 19         |        | 4.95  |
| V07          | Base A      | 19         |        | 5.35  |
|              |             |            |        |       |
| V08          | Surf E      | 1          | 6.49   | 6.74  |
| V08          | Surf E      | 2          | 6.12   | 6.23  |
| V08          | Surf E      | 2          |        | 6.15  |
| V08          | Surf E      | 3          | 6.26   | 6.01  |
| V08          | Surf E      | 4          | 6.41   | 6.39  |
| V08          | Surf E      | 4          |        | 6.18  |
| V08          | Surf E      | 5          | 6.41   | 6.39  |
| V08          | Surf E      | 5          |        | 6.33  |
|              |             |            |        |       |
| V09          | Surf A      | 1          | 5.06   | 4.76  |
| V09          | Surf A      | 1          | 4.88   |       |
| V09          | Surf A      | 1          | 4.53   |       |
| V09          | Surf A      | 1          | 4.71   |       |
| V09          | Surf A      | 2          | 5.01   | 4.98  |
| V09          | Surf A      | 2          | 5.04   | 4.86  |
| V09          | Surf A      | 2          | 4.91   |       |
| V09          | Surf A      | 2          | 5.06   |       |
| V09          | Surf A      | 3          | 4.82   | 4.69  |
| V09          | Surf A      | 3          | 4.80   | 4.47  |
| V09          | Surf A      | 3          | 4.71   | 4.77  |
| V09          | Surf A      | 3          | 4.71   |       |
| V09          | Surf A      | 3          | 4.48   |       |
| V09          | Surf A      | 3          | 4.68   |       |
| V09          | Surf A      | 4          | 4.79   | 4.79  |
| V09          | Surf A      | 4          | 4.60   |       |
| V09          | Surf A      | 4          | 4.62   | 4.42  |
| V09          | Surf A      | 4          | 4.70   |       |
| V09          | Surf A      | 5          | 4.44   | 4.61  |
| V09          | Surf A      | 5          | 4.91   |       |
| V09          | Surf A      | 5          | 5.01   | 4.04  |
| V09          | Surf A      | 5          | 4.25   |       |
| V09          | Surf A      | 6          | 5.03   | 4.86  |
| V09          | Surf A      | 6          | 4.86   | 4.70  |
| V09          | Surf A      | 6          | 4.86   |       |
| V09          | Surf A      | 6          | 4.86   | 4.80  |
| V09          | Surf A      | 7          | 4.72   |       |
| V09          | Surf A      | 7          | 4.70   |       |
|              |             |            |        |       |
| V09          | Surf E      | 1          | 5.91   | 5.98  |
| V09          | Surf E      | 1          | 6.00   | 5.86  |
| V09          | Surf E      | 2          |        | 6.08  |
| V09          | Surf E      | 2          | 6.13   |       |
| V09          | Surf E      | 3          | 5.96   | 5.97  |

**SCDOT** 4.77

| Proj.<br>No. | Mix<br>Type | Lot<br>No. | Contr. | SCDOT |
|--------------|-------------|------------|--------|-------|
| V09          | Surf E      | 3          | 6.10   | 5.94  |
| V09          | Surf E      | 4          | 5.99   | 5.79  |
| V09          | Surf E      | 5          | 6.03   | 5.95  |
| V09          | Surf E      | 5          | 5.94   |       |
| V09          | Surf E      | 5          | 5.95   |       |
|              |             |            |        |       |
| V10          | Interm B    | 1          | 4.82   | 4.41  |
| V10          | Interm B    | 1          |        | 4.86  |
| V10          | Interm B    | 2          | 4.51   | 4.32  |
| V10          | Interm B    | 2          | 4.34   |       |
| V10          | Interm B    | 2          | 4.80   |       |
| V10          | Interm B    | 3          | 4.28   | 4.73  |
| V10          | Interm B    | 3          | 4.19   |       |
| V10          | Interm B    | 3          | 5.10   | 4.95  |
| V10          | Interm B    | 4          | 4.45   | 5.11  |
| V10          | Interm B    | 4          | 4.38   |       |
| V10          | Interm B    | 4          | 4.84   | 4.79  |
| V10          | Interm B    | 4          | 4.38   |       |
| V10          | Interm B    | 4          | 4.71   |       |
| V10          | Interm B    | 5          | 4.65   |       |
| V10          | Interm B    | 5          | 4.19   |       |
| V10          | Interm B    | 5          | 4.46   |       |
| V10          | Interm B    | 5          | 4.53   |       |
|              |             |            |        |       |
| V10          | Interm B    | 6          | 4.54   |       |
| V10          | Interm B    | 6          | 4.66   |       |
| V10          | Interm B    | 6          | 4.47   |       |
| V10          | Interm B    | 7          | 4.93   | 4.80  |
| V10          | Interm B    | 7          | 4.54   |       |
| V10          | Interm B    | 7          | 4.49   | 4.63  |
| V10          | Interm B    | 7          |        | 5.16  |
| V10          | Interm B    | 8          | 4.38   | 4.63  |
| V10          | Interm B    | 8          |        | 4.56  |
| V10          | Interm B    | 8          | 4.67   |       |
| V10          | Interm B    | 4          | 4.45   | 5.11  |
| V10          | Interm B    | 4          | 4.38   | 170   |
| V10          | Interm B    | 4          | 4.84   | 4.79  |
| V10          | Interm B    | 4          | 4.38   |       |
| V10          | Interm B    | 4<br>F     | 4.71   |       |
| V10          | Interm B    | 5<br>F     | 4.00   |       |
| V10          | Interm B    | ວ<br>      | 4.19   |       |
| V 10         |             | 5<br>5     | 4.40   |       |
| VIU          | Intern B    | 5          | 4.00   |       |
| \/10         | Surf A      | 1          | 4.60   | 4.72  |
| V10          |             | 1          | 4.00   | 4.00  |
| V10          | Surf A      | 1          | 4 73   | 4.30  |
| V10          | Surf A      | 1          | 4.75   | -1.10 |
| V10          | Surf A      | 2          | 4.60   |       |
| V10          | Surf A      | 2          | 4.99   | 4,56  |
|              | Junit       | -          |        | 1.50  |

| Mix<br>ype | Lot<br>No. | Contr. | SCDOT | Proj.<br>No. | Mix<br>Type | Lot<br>No. | Contr. |
|------------|------------|--------|-------|--------------|-------------|------------|--------|
| urf E      | 3          | 6.10   | 5.94  | V10          | Surf A      | 2          | 4.72   |
| urf E      | 4          | 5.99   | 5.79  | V10          | Surf A      | 2          | 4.61   |
| urf E      | 5          | 6.03   | 5.95  | V10          | Surf A      | 3          | 4.84   |
| urf E      | 5          | 5.94   |       | V10          | Surf A      | 3          | 5.05   |
| urf E      | 5          | 5.95   |       | V10          | Surf A      | 3          | 4.89   |
|            |            |        |       | V10          | Surf A      | 3          | 4.92   |
| erm B      | 1          | 4.82   | 4.41  | V10          | Surf A      | 4          | 4.59   |
| erm B      | 1          |        | 4.86  | V10          | Surf A      | 4          | 4.80   |
| erm B      | 2          | 4.51   | 4.32  | V10          | Surf A      | 4          | 4.36   |
| erm B      | 2          | 4.34   |       | V10          | Surf A      | 4          | 4.76   |
| erm B      | 2          | 4.80   |       | V10          | Surf A      | 5          | 4.32   |
| erm B      | 3          | 4.28   | 4.73  | V10          | Surf A      | 5          | 4.71   |
| ≏rm B      | 3          | 4 1 9  |       | V10          | Surf A      | 5          | 4 69   |

| V I U | SULLA  | 3  | 5.05 |      |
|-------|--------|----|------|------|
| V10   | Surf A | 3  | 4.89 | 5.12 |
| V10   | Surf A | 3  | 4.92 | 5.11 |
| V10   | Surf A | 4  | 4.59 |      |
| V10   | Surf A | 4  | 4.80 |      |
| V10   | Surf A | 4  | 4.36 | 5.09 |
| V10   | Surf A | 4  | 4.76 |      |
| V10   | Surf A | 5  | 4.32 | 4.80 |
| V10   | Surf A | 5  | 4.71 |      |
| V10   | Surf A | 5  | 4.69 |      |
|       |        |    |      |      |
| V10   | Surf A | 6  | 4.51 | 4.92 |
| V10   | Surf A | 6  | 4.90 | 5.41 |
| V10   | Surf A | 6  | 5.16 | 5.55 |
| V10   | Surf A | 7  | 4.96 | 4.95 |
| V10   | Surf A | 7  |      | 4.85 |
| V10   | Surf A | 3  | 4.84 |      |
| V10   | Surf A | 3  | 5.05 |      |
| V10   | Surf A | 3  | 4.89 | 5.12 |
| V10   | Surf A | 3  | 4.92 | 5.11 |
| V10   | Surf A | 4  | 4.59 |      |
| V10   | Surf A | 4  | 4.80 |      |
| V10   | Surf A | 4  | 4.36 | 5.09 |
| V10   | Surf A | 4  | 4.76 |      |
| V10   | Surf A | 5  | 4.32 | 4.80 |
| V10   | Surf A | 5  | 4.71 |      |
| V10   | Surf A | 5  | 4.69 |      |
|       |        |    |      |      |
| V10   | Surf E | 1  | 6.40 | 6.58 |
| V10   | Surf E | 2  | 6.35 | 6.52 |
| V10   | Surf E | 2  |      | 6.25 |
| V10   | Surf E | 3  | 6.55 | 6.60 |
| V10   | Surf E | 4  | 6.34 | 6.68 |
| V10   | Surf E | 4  |      | 6.44 |
| V10   | Surf E | 5  | 6.47 |      |
|       |        |    |      |      |
| V10   | Surf E | 6  | 6.87 | 6.50 |
| V10   | Surf E | 7  | 6.33 | 6.44 |
| V10   | Surf E | 8  | 6.40 | 6.51 |
| V10   | Surf E | 9  | 6.40 | 6.54 |
| V10   | Surf E | 10 | 6.74 | 6.71 |
|       |        |    |      |      |
|       |        |    |      |      |
|       |        |    |      |      |
|       |        |    |      |      |
|       |        |    |      |      |
|       |        |    |      |      |

# Table D.1. Asphalt Content Verification Test Results Data (continued)

| Proj. | Mix      | Lot | Contr. | SCDOT |
|-------|----------|-----|--------|-------|
| V01   | Interm B | 1   | 3.07   | 2.56  |
| V01   | Interm B | 1   | 2.06   | 2.30  |
| V01   | Interm B | 1   | 2.90   |       |
| V01   | Interm B | 1   | 2.16   | 2 70  |
| V01   |          | 1   | 3.10   | 2.79  |
| V01   |          | 1   | 3.01   | 4.00  |
| V01   | Interm B | 1   | 4.27   |       |
| V01   | Interm B | 1   | 4.15   |       |
| V01   | Interm B | 1   | 4.38   |       |
| V01   | Interm B | 2   | 3.14   | 4.0.4 |
| V01   | Interm B | 2   | 4.56   | 4.04  |
| V01   | Interm B | 2   | 2.95   | 3.52  |
| V01   | Interm B | 2   | 4.02   | 4.67  |
| V01   | Interm B | 2   | 4.34   |       |
| V01   | Interm B | 3   | 3.98   |       |
| V01   | Interm B | 3   | 3.02   |       |
| V01   | Interm B | 3   | 4.79   |       |
| V01   | Interm B | 3   | 2.72   |       |
| V01   | Interm B | 4   | 3.23   | 4.24  |
| V01   | Interm B | 4   | 3.80   |       |
|       |          |     |        |       |
| V01   | Surf A   | 1   | 3.60   | 3.22  |
| V01   | Surf A   | 1   | 3.74   | 3.02  |
| V01   | Surf A   | 1   | 2.92   | 2.50  |
| V01   | Surf A   | 2   | 2.74   | 2.77  |
| V01   | Surf A   | 3   | 3.10   | 3.20  |
| V01   | Surf A   | 4   | 2.66   |       |
| V01   | Surf A   | 5   | 4.62   | 3.18  |
|       |          |     |        |       |
| V02   | Interm B | 1   | 3.31   |       |
| V02   | Interm B | 2   | 3.52   | 4.73  |
| V02   | Interm B | 2   |        | 2.78  |
| V02   | Interm B | 3   | 3.35   | 4.64  |
| V02   | Interm B | 3   | 4.02   |       |
| V02   | Interm B | 4   | 2.87   |       |
| V02   | Interm B | 5   | 4.33   | 3.44  |
| V02   | Interm B | 5   | 3.05   | 3.47  |
|       |          |     | 0.00   | 0     |
| V02   | Surf A   | 1   | 4.06   | 6.72  |
| V02   | Surf A   | 1   | 2.46   | 3.93  |
| V02   | Surf A   | 1   | 2.40   | 2 14  |
| V02   | Surf A   | 1   | 2.00   | 2.14  |
| \/02  | Surf A   | 2   | 3.07   | 2.37  |
| 1/02  | Surf A   | 2   | 2.07   | 2.00  |
| V02   | Surf A   | 2   | 2.30   | 2.32  |
| V02   | Sull A   | 2   | 2.37   |       |
| V02   | Surf A   | 2   | 2.21   | 2.44  |
| V02   | Surr A   | 3   | 2.52   | 2.41  |
| V02   | Surt A   | 3   | 2.28   |       |
| V02   | Surf A   | 3   | 2.60   |       |
| V02   | Surf A   | 4   | 2.10   | 3.07  |
| V02   | Surf A   | 4   | 2.12   |       |

| Table D.2. Air | Voids | Verification | Test | Results | Data |
|----------------|-------|--------------|------|---------|------|
|----------------|-------|--------------|------|---------|------|

| Proj. | Mix    | Lot | Contr. | SCDOT |
|-------|--------|-----|--------|-------|
| NO.   | Type   | NO. | 0.54   |       |
| V02   | Surf A | 4   | 2.54   |       |
| V02   | Surf A | 5   | 3.12   | -     |
| V02   | Surf A | 5   | 3.34   |       |
| V02   | Surf A | 5   | 3.37   |       |
| V02   | Surf A | 5   | 2.77   | 0.70  |
| V02   | Surf A | 5   | 2.29   | 3.73  |
| V02   | Surf A | 5   | 2.94   |       |
| 1/00  | 0( )   |     | 0.00   | 0.47  |
| V02   | Surf A | 6   | 3.09   | 3.17  |
| V02   | Surf A | 6   | 2.95   |       |
| V02   | Surf A | 6   | 2.78   |       |
| V02   | Surf A | 6   | 2.80   |       |
| V02   | Surf A | 7   | 2.90   | 3.55  |
| V02   | Surf A | 7   | 3.12   |       |
| V02   | Surf A | 7   | 3.01   |       |
| V02   | Surf A | 8   | 3.59   | 5.90  |
| V02   | Surf A | 8   | 3.38   |       |
| V02   | Surf A | 8   | 2.80   |       |
| V02   | Surf A | 9   | 3.54   | 3.60  |
| V02   | Surf A | 9   | 3.73   |       |
| V02   | Surf A | 9   | 3.23   | 3.95  |
| V02   | Surf A | 9   | 3.19   |       |
| V02   | Surf A | 9   | 2.50   |       |
| V02   | Surf A | 10  | 3.29   | 3.62  |
| V02   | Surf A | 10  | 2.59   |       |
| V02   | Surf A | 10  | 2.35   | 2.50  |
|       |        |     |        |       |
| V02   | Surf A | 11  | 2.69   | 4.16  |
| V02   | Surf A | 11  | 3.60   |       |
| V02   | Surf A | 11  | 3.11   | 4.59  |
| V02   | Surf A | 11  | 2.10   |       |
| V02   | Surf A | 11  | 2.65   |       |
| V02   | Surf A | 12  | 2.68   |       |
| V02   | Surf A | 12  | 2.25   |       |
| V02   | Surf A | 12  | 2.32   |       |
| V02   | Surf A | 12  | 2.73   |       |
| V02   | Surf A | 13  | 2.66   | 2.54  |
| V02   | Surf A | 13  | 2.63   |       |
| V02   | Surf A | 13  | 2.71   |       |
| V02   | Surf A | 13  | 2.26   |       |
| V02   | Surf A | 14  | 2.15   | 2.92  |
| V02   | Surf A | 14  | 2.19   |       |
| V02   | Surf A | 14  | 3.00   |       |
| V02   | Surf A | 14  | 2.52   | 2.67  |
| V02   | Surf A | 14  | 2.86   | ļ     |
| V02   | Surf A | 14  | 3.28   | ļ     |
| V02   | Surf A | 15  | 2.14   | 2.34  |
| V02   | Surf A | 15  | 2.79   | 3.19  |
| V02   | Surf A | 15  | 2.97   |       |
| V02   | Surf A | 15  | 2.61   |       |

| Proj.<br>No. | Mix<br>Type | Lot<br>No. | Contr. | SCDOT |
|--------------|-------------|------------|--------|-------|
|              |             |            |        |       |
| V02          | Surf A      | 16         | 2.79   | 2.04  |
| V02          | Surf A      | 16         | 2.69   | 2.39  |
| V02          | Surf A      | 16         | 2.68   |       |
| V02          | Surf A      | 16         | 2.12   |       |
| V02          | Surf A      | 17         | 3.55   | 3.30  |
| V02          | Surf A      | 17         | 3.09   | 3.66  |
| V02          | Surf A      | 17         | 4.02   |       |
| V02          | Surf A      | 17         | 2.98   |       |
| V02          | Surf A      | 18         | 1.34   | 4.21  |
| V02          | Surf A      | 18         | 4.25   |       |
| V02          | Surf A      | 18         | 3.17   | 5.32  |
| V02          | Surf A      | 18         | 2.88   |       |
| V02          | Surf A      | 19         | 3.16   | 3.64  |
| V02          | Surf A      | 19         | 3.39   |       |
| V02          | Surf A      | 19         | 2.95   | 4.10  |
| V02          | Surf A      | 19         | 3.14   |       |
| V02          | Surf A      | 20         | 2.76   | 2.59  |
| V02          | Surf A      | 20         | 2.30   |       |
| V02          | Surf A      | 20         | 2.80   |       |
| V02          | Surf A      | 20         | 3.16   |       |
|              |             |            |        |       |
| V02          | Surf A      | 21         | 2.15   | 2.25  |
| V02          | Surf A      | 21         | 2.77   |       |
| V02          | Surf A      | 21         | 3.38   |       |
| V02          | Surf A      | 21         | 3.31   |       |
| V02          | Surf A      | 22         | 3.40   |       |
| V02          | Surf A      | 22         | 2.45   |       |
| V02          | Surf A      | 18         | 1.34   | 4.21  |
| V02          | Surf A      | 18         | 4.25   |       |
| V02          | Surf A      | 18         | 3.17   | 5.32  |
| V02          | Surf A      | 18         | 2.88   |       |
| V02          | Surf A      | 19         | 3.16   | 3.64  |
| V02          | Surf A      | 19         | 3.39   |       |
| V02          | Surf A      | 19         | 2.95   | 4.10  |
| V02          | Surf A      | 19         | 3.14   |       |
| V02          | Surf A      | 20         | 2.76   | 2.59  |
| V02          | Surf A      | 20         | 2.30   |       |
| V02          | Surf A      | 20         | 2.80   |       |
| V02          | Surf A      | 20         | 3.16   |       |
|              |             |            |        |       |
| V02          | Surf B      | 1          | 3.05   | 3.14  |
| V02          | Surf B      | 1          | 3.33   |       |
| V02          | Surf B      | 1          | 2.14   | 3.75  |
| V02          | Surf B      | 1          | 2.29   |       |
| V02          | Surf B      | 2          | 3.09   | 4.35  |
| V02          | Surf B      | 2          | 3.11   |       |
| V02          | Surf B      | 2          | 2.92   | 4.83  |
| V02          | Surf B      | 2          | 3.45   | 4.44  |
| V02          | Surf B      | 2          | 3.70   |       |

| Proj. | Mix    | Lot | Contr. | SCDOT |
|-------|--------|-----|--------|-------|
| NO.   | Type   | NO. | 0.00   | 0.04  |
| V02   | Surf B | 3   | 2.93   | 3.04  |
| V02   | Surf B | 3   | 3.79   | 4.68  |
| V02   | Surf B | 3   | 3.69   | 3.60  |
| V02   | Surf B | 4   | 2.62   | 2.80  |
| V02   | Surf B | 4   | 3.28   |       |
| V02   | Surf B | 4   | 2.58   |       |
| V02   | Surf B | 6   | 2.21   | 2.27  |
| V02   | Surf B | 6   | 3.41   | 2.92  |
| V02   | Surf B | 6   | 2.05   |       |
|       |        |     |        |       |
| V02   | Surf B | 2   | 2.43   |       |
| V02   | Surf B | 2   | 3.51   |       |
| V02   | Surf B | 2   | 3.18   |       |
| V02   | Surf B | 3   | 3.44   | 4.60  |
| V02   | Surf B | 3   | 2.88   | 4.37  |
| V02   | Surf B | 3   | 3.23   | 3.63  |
| V02   | Surf B | 4   | 2.58   | 2.79  |
| V02   | Surf B | 4   | 3.29   |       |
| V02   | Surf B | 4   | 3.03   |       |
| V02   | Surf B | 4   | 2.27   |       |
| V02   | Surf B | 5   | 3.06   | 2.70  |
| V02   | Surf B | 5   | 3.21   |       |
| V02   | Surf B | 5   | 3.04   |       |
| V02   | Surf B | 6   | 2.37   | 2.85  |
| V02   | Surf B | 6   | 2.84   | 2.54  |
| V02   | Surf B | 6   | 2.94   |       |
| V02   | Surf B | 6   | 3.01   |       |
| V02   | Surf B | 6   | 3.15   |       |
|       |        |     |        |       |
| V02   | Surf B | 5   | 3.74   | 3.57  |
| V02   | Surf B | 5   | 3.15   |       |
| V02   | Surf B | 5   | 2.96   |       |
| V02   | Surf B | 6   | 2.63   |       |
| V02   | Surf B | 6   | 2.84   | 4.01  |
| V02   | Surf B | 6   | 3.25   | 4.10  |
| V02   | Surf B | 6   | 3.09   |       |
| V02   | Surf B | 6   | 2.94   |       |
| V02   | Surf B | 6   | 2.53   |       |
| V02   | Surf B | 7   | 3.82   |       |
| V02   | Surf B | 7   | 2.42   |       |
| V02   | Surf B | 7   | 2.33   |       |
| V02   | Surf B | 7   | 2.92   |       |
| V02   | Surf B | 8   | 3.46   | 3.31  |
| V02   | Surf B | 8   | 2.99   | 3.48  |
| V02   | Surf B | 8   | 2.39   |       |
| V02   | Surf B | 9   | 3.50   | 3,58  |
| V02   | Surf B | 9   | 3.44   | 3.34  |
| V02   | Surf B | 9   | 2.95   |       |
|       |        |     |        |       |
| V02   | Surf B | 10  | 3.66   | 4.70  |

# Table D.2. Air Voids Verification Test Results Data (continued)

| Proj.<br>No | Mix<br>Type | Lot<br>No | Contr.   | SCDOT |
|-------------|-------------|-----------|----------|-------|
| V02         | Surf B      | 10        | 311      | 5.09  |
| V02         | Surf B      | 10        | 3.12     | 0.00  |
| V02         | Surf B      | 11        | 2.65     |       |
| V02         | Surf B      | 11        | 3.54     |       |
| V02         | Surf B      | 11        | 3.74     |       |
| V02         | Surf B      | 12        | 3.79     | 5 4 4 |
| V02<br>V02  | Surf B      | 12        | 5.70     | 5.44  |
| V02         | Surf B      | 12        | 3.86     |       |
| V02         | Surf B      | 12        | 3.00     |       |
| V02         | Surf B      | 12        | 3.85     |       |
| V02         | Surf B      | 7         | 3 32     | 3.80  |
| V02         | Surf B      | 7         | 2.54     | 3.81  |
| V02         | Surf B      | 1         | 2.04     | 3.96  |
| V 02        | Our D       |           |          | 0.00  |
| V04         | Surf B      | 1         | 2 79     | 2.62  |
| V04         | Surf B      | 1         | 2.75     | 3 55  |
| V04         | Surf B      | 1         | 3 31     | 0.00  |
| V04         | Surf B      | 1         | 3 15     | 2.05  |
| V04         | Surf B      | 1         | 3.01     | 2.00  |
| V04<br>V04  | Surf B      | 2         | 3.05     | 3 30  |
| V04         | Surf B      | 2         | 2.84     | 0.00  |
| V04         | Surf B      | 2         | 3.44     |       |
| V04         | Surf B      | 2         | 2.00     |       |
| V04<br>V04  | Surf B      | 2         | 2.78     | 3 / 1 |
| V04         | Surf B      | 3         | 2.70     | 3.41  |
| V04<br>V04  | Surf B      | 3         | 3.07     | 3.10  |
| V04<br>V04  | Surf B      | 3         | 3.03     | 5.50  |
| V04         | Surf B      | 1         | 3.45     | / 18  |
| V04         | Surf B      | 4         | 3.94     | 4.10  |
| V04         | Surf B      | 4         | 3.14     |       |
| V04<br>V04  | Surf B      | 5         | 3.17     | 3.52  |
| V04<br>V04  | Surf B      | 5         | 2.83     | 2.40  |
| V04         | Surf B      | 5         | 2.00     | 2.43  |
| V04         | Surf B      | 5         | 3.50     |       |
| V04         | Surf B      | 6         | 4 32     | 5 50  |
| V04         | Surf B      | 6         | 3.85     | 5.59  |
| V04         | Surf B      | 6         | <u> </u> |       |
| V04         | Surf B      | 6         | 3 35     |       |
| V04         | Surf B      | 6         | 3.00     |       |
| v 04        | Juir D      | 0         | 5.92     |       |
| V05         | Interm R    | 2         | 2.69     | 3.97  |
| V05         | Interm P    | 2         | 2.00     | 5.07  |
| V05         | Interm P    | 2         | 2.50     | 3 50  |
| V05         |             | 2         | 2.10     | 3.39  |
|             |             | 2         | 2.04     | 2 5 5 |
| VUD         |             | 3<br>2    | 2.70     | 3.55  |
| VUD         |             | 3<br>2    | 2.19     |       |
| V05         |             | 3         | 3.02     |       |
| VOF         |             | 4         | 3.02     | A 4 E |
| 207         | Interm B    | 4         | 2.48     | 4.15  |
| VUD         |             | . //      |          |       |

| Proj.<br>No | Mix<br>Type | Lot    | Contr. | SCDOT |
|-------------|-------------|--------|--------|-------|
| V05         | Interm B    | 4      | 2.92   |       |
| V05         | Interm B    | 4      | 2.87   |       |
| V05         | Interm B    | 5      | 3.29   | 2.57  |
| V05         | Interm B    | 5      | 2.84   | 3.01  |
| V05         | Interm B    | 5      | 2.04   | 0.01  |
| V05         | Interm B    | 5      | 2.58   |       |
| V05         | Interm B    | 6      | 3.08   |       |
| V05         | Interm B    | 6      | 3.12   |       |
| V05         | Interm B    | 6      | 2.82   |       |
| V05         | Interm B    | 6      | 2.02   |       |
| 100         | Internet    | 0      | 2.72   |       |
| V05         | Interm B    | 7      | 2.78   |       |
| V05         | Interm B    | 7      | 3.17   |       |
| V05         | Interm B    | 7      | 3.01   |       |
| V05         | Interm B    | 8      | 3.12   | 4.65  |
| V05         | Interm R    | 8      | 3.12   | 4.00  |
| V05         | Interm B    | 8      | 2.85   |       |
| V05         | Interm B    | 0<br>0 | 2.00   |       |
| V05         | Interm B    | 9      | 2.00   | 4.10  |
| V05         | Interm B    | 9      | 2.30   | 4.10  |
| V05         | Interm B    | 10     | 2.00   | 4.13  |
| V05         | Interm B    | 10     | 5.71   | 3.40  |
| V05         | Interm B    | 11     | 2.06   | 3.40  |
| V05         | Interm B    | 11     | 2.50   | 5.75  |
| V05         | Interm B    | 11     | 2.52   |       |
| V05         | Interm B    | 11     | 2.00   |       |
| V05         | Interni D   | 11     | 2.50   |       |
| V05         | Intorm B    | 12     | 2.02   | 2.41  |
| V05         | Interm B    | 12     | 2.54   | 5.41  |
| V05         | Interm B    | 12     | 2.54   | 2.60  |
| V05         | Interm B    | 12     | 2.00   | 2.00  |
| V05         | Interm B    | 12     | 2.00   | 3.56  |
| V05         | Interm B    | 13     | 2.44   | 0.00  |
| V05         | Interm B    | 13     | 2.00   |       |
| V05         | Interm B    | 14     | 2.74   | 3.28  |
| V05         | Interm B    | 14     | 2 92   | 4 20  |
| V05         | Interm B    | 14     | 2.02   | 4.20  |
| V05         | Interm B    | 14     | 4.07   |       |
| V05         | Interm B    | 11     | 2.06   | 373   |
| V05         | Interm B    | 11     | 2.50   | 0.70  |
| V05         | Interm B    | 11     | 2.02   |       |
| V05<br>V05  | Interm R    | 11     | 2.00   |       |
| 000         |             | 11     | 2.00   |       |
| V05         | Surf A      | 1      | 2.53   |       |
| V05         | Surf A      | 1      | 2.00   |       |
| V05         | Surf A      | 2      | 2.70   | 5.02  |
| V05         | Surf A      | 2      | 4.01   | 5.03  |
| V05         | Surf A      | 2      | 3.70   | 264   |
| V05         | Surf A      | 2      | 2.89   | 3.04  |
| V05         | Surf A      | 2      | 2.00   |       |
| V05         | Suff A      | 2      | 3.09   |       |

| Proj.<br>No. | Mix<br>Type | Lot<br>No. | Contr. | SCDOT |
|--------------|-------------|------------|--------|-------|
| V05          | Surf A      | 2          | 3.30   |       |
| V05          | Surf A      | 3          | 3.71   | 4.21  |
| V05          | Surf A      | 3          | 3.58   |       |
| V05          | Surf A      | 3          | 3.72   |       |
| V05          | Surf A      | 3          | 3.07   |       |
| V05          | Surf A      | 3          | 3.16   |       |
| V05          | Surf A      | 4          | 3.80   | 4.39  |
| V05          | Surf A      | 4          | 3.85   |       |
| V05          | Surf A      | 4          | 3.60   |       |
| V05          | Surf A      | 4          | 2.93   |       |
| V05          | Surf A      | 5          | 2.84   | 3.54  |
| V05          | Surf A      | 5          | 2.57   |       |
| V05          | Surf A      | 5          | 3.58   |       |
|              |             |            |        |       |
| V05          | Surf A      | 6          | 3.44   | 4.34  |
| V05          | Surf A      | 6          | 3.80   |       |
| V05          | Surf A      | 6          | 3.55   | 4.37  |
| V05          | Surf A      | 6          | 3.40   |       |
| V05          | Surf A      | 7          | 3.41   | 4.21  |
| V05          | Surf A      | 7          | 3.22   |       |
| V05          | Surf A      | 7          | 3.38   |       |
| V05          | Surf A      | 8          | 4.21   | 4.80  |
| V05          | Surf A      | 8          | 3.96   |       |
| V05          | Surf A      | 8          | 2.89   |       |
| V05          | Surf A      | 9          | 4.16   | 5.23  |
| V05          | Surf A      | 9          | 3.68   | 5.09  |
| V05          | Surf A      | 9          | 3.83   |       |
| V05          | Surf A      | 10         | 3.48   | 4.61  |
| V05          | Surf A      | 10         | 3.86   | 4.65  |
| V05          | Surf A      | 10         | 3.94   |       |
| V05          | Surf A      | 10         | 3.37   |       |
|              |             |            |        |       |
| V05          | Surf A      | 11         | 4.01   |       |
| V05          | Surf A      | 11         | 4.61   | 4.04  |
| V05          | Surf A      | 11         | 3.24   | 4.77  |
| V05          | Surf A      | 11         | 3.09   |       |
| V05          | Surf A      | 11         | 3.03   |       |
| V05          | Surf A      | 12         | 3.68   | 5.21  |
| V05          | Surf A      | 12         | 3.20   | 5.06  |
| V05          | Surf A      | 12         | 3.83   |       |
| V05          | Surf A      | 12         | 3.27   |       |
| V05          | Surf A      | 13         | 3.69   | 4.88  |
| V05          | Surf A      | 13         | 3.95   | 6.03  |
| V05          | Surf A      | 13         | 4.04   |       |
| V05          | Surf A      | 13         | 3.18   |       |
| V05          | Surf A      | 13         | 3.80   | 4.33  |
| V05          | Surf A      | 14         | 4.15   |       |
| V05          | Surf A      | 14         | 3.68   |       |
| V05          | Surf A      | 14         | 4.13   | 4.37  |
| V05          | Surf A      | 15         | 3.24   |       |

| Table D.2. Air Voids Verification | n Test Results Data | (continued) |
|-----------------------------------|---------------------|-------------|
|-----------------------------------|---------------------|-------------|

| Proj.<br>No. | Mix<br>Type | Lot<br>No. | Contr. | SCDOT |  |
|--------------|-------------|------------|--------|-------|--|
| V05          | Surf A      | 15         | 3.35   | 4.00  |  |
| V05          | Surf A      | 15         | 3.70   |       |  |
| V05          | Surf A      | 15         | 2.77   |       |  |
| V05          | Surf A      | 15         | 2.72   | 3.41  |  |
|              | Curre       |            |        | 0111  |  |
| V05          | Surf A      | 16         | 2.47   |       |  |
| V05          | Surf A      | 16         | 2.72   | 3.06  |  |
| V05          | Surf A      | 16         | 3.43   |       |  |
| V05          | Surf A      | 16         | 3.39   |       |  |
| V05          | Surf A      | 16         | 3.98   | 3.65  |  |
| V05          | Surf A      | 17         | 2.81   |       |  |
| V05          | Surf A      | 17         | 2.62   |       |  |
| V05          | Surf A      | 17         | 3.00   | 3.51  |  |
| V05          | Surf A      | 17         | 2.80   |       |  |
| V05          | Surf A      | 17         | 3.40   |       |  |
| V05          | Surf A      | 18         | 3.13   |       |  |
| V05          | Surf A      | 18         | 3.43   |       |  |
| V05          | Surf A      | 18         | 3.47   | 3.38  |  |
| V05          | Surf A      | 18         | 3.55   |       |  |
| V05          | Surf A      | 18         | 3.65   | 2.98  |  |
| V05          | Surf A      | 19         | 3.96   |       |  |
| V05          | Surf A      | 19         | 3.42   | 3.09  |  |
| V05          | Surf A      | 19         | 2.72   | 1.97  |  |
| V05          | Surf A      | 20         | 3.43   | 3.79  |  |
| V05          | Surf A      | 20         | 3.83   |       |  |
| V05          | Surf A      | 20         | 3.44   | 2.51  |  |
| V05          | Surf A      | 20         | 3.20   |       |  |
| V05          | Surf A      | 20         | 3.90   |       |  |
|              |             |            |        |       |  |
| V05          | Surf A      | 21         | 4.51   | 4.35  |  |
| V05          | Surf A      | 21         | 3.44   |       |  |
| V05          | Surf A      | 21         | 4.00   |       |  |
| V05          | Surf A      | 22         | 3.75   |       |  |
| V05          | Surf A      | 22         | 3.94   | 4.15  |  |
| V05          | Surf A      | 22         | 3.25   | 3.49  |  |
| V05          | Surf A      | 23         | 2.57   | 3.72  |  |
| V05          | Surf A      | 23         | 3.67   |       |  |
| V05          | Surf A      | 23         | 3.58   |       |  |
| V05          | Surf A      | 23         | 2.68   |       |  |
| V05          | Surf A      | 24         | 2.58   | 3.61  |  |
| V05          | Surf A      | 24         | 3.16   |       |  |
| V05          | Surf A      | 24         | 2.97   |       |  |
| V05          | Surf A      | 25         | 2.22   |       |  |
| V05          | Surf A      | 25         | 3.04   |       |  |
|              |             |            |        |       |  |
| V05          | Surf B      | 1          | 4.02   |       |  |
| V05          | Surf B      | 1          | 3.59   |       |  |
| V05          | Surf B      | 1          | 3.76   | 5.30  |  |
| V05          | Surf B      | 1          | 3.92   |       |  |
| V05          | Surf B      | 1          | 3.87   |       |  |

| Proj.<br>No. | Mix<br>Type | Lot<br>No. | Contr. | SCDOT |
|--------------|-------------|------------|--------|-------|
| V05          | Surf B      | 2          | 4.53   |       |
| V05          | Surf B      | 2          | 3.70   | 5.77  |
| V05          | Surf B      | 2          | 4.55   |       |
| V05          | Surf B      | 2          | 4.26   | 4.79  |
| V05          | Surf B      | 2          | 3.84   |       |
| V05          | Surf B      | 2          | 3.77   | 5.06  |
| V05          | Surf B      | 3          | 3.88   |       |
| V05          | Surf B      | 3          | 4.00   |       |
| V05          | Surf B      | 3          | 4.02   | 5.25  |
| V05          | Surf B      | 4          | 3.25   |       |
| V05          | Surf B      | 4          | 3.14   |       |
| V05          | Surf B      | 4          | 3.27   |       |
| V05          | Surf B      | 5          | 3.13   | 4.72  |
| V05          | Surf B      | 5          | 3.15   | 3.95  |
| V05          | Surf B      | 5          | 3.08   |       |
| V05          | Surf B      | 5          | 3.11   |       |
| V05          | Surf B      | 5          | 3.46   |       |
|              |             |            |        |       |
| V05          | Surf B      | 6          | 3.03   | 3.60  |
| V05          | Surf B      | 6          | 3.33   | 3.05  |
| V05          | Surf B      | 6          | 2.71   | 3.54  |
| V05          | Surf B      | 6          | 2.98   |       |
| V05          | Surf B      | 6          | 3.05   |       |
| V05          | Surf B      | 7          | 2.70   |       |
| V05          | Surf B      | 7          | 3.19   |       |
| V05          | Surf B      | 7          | 3.10   |       |
| V05          | Surf B      | 8          | 2.73   | 3.71  |
| V05          | Surf B      | 8          | 3.78   |       |
| V05          | Surf B      | 8          | 3.21   | 3.49  |
| V05          | Surf B      | 8          | 3.30   |       |
| V05          | Surf B      | 4          | 3.25   |       |
| V05          | Surf B      | 4          | 3.14   |       |
| V05          | Surf B      | 4          | 3.27   |       |
| V05          | Surf B      | 5          | 3.13   | 4.72  |
| V05          | Surf B      | 5          | 3.15   | 3.95  |
| V05          | Surf B      | 5          | 3.08   |       |
| V05          | Surf B      | 5          | 3.11   |       |
| V05          | Surf B      | 5          | 3.46   |       |
|              |             |            |        |       |
| V06          | Interm C    | 1          | 5.04   |       |
| V06          | Interm C    | 2          | 5.01   | 5.21  |
| V06          | Interm C    | 3          | 4.41   | 5.54  |
| V06          | Interm C    | 3          |        | 4.13  |
| V06          | Interm C    | 4          | 4.83   | 4.29  |
| V06          | Interm C    | 5          | 4.26   |       |
| V06          | Interm C    | 5          | 5.25   |       |
|              |             |            |        |       |
| V09          | Surf A      | 1          | 2.85   | 4.46  |
| V09          | Surf A      | 1          | 3.45   |       |
| V/09         | Surf A      | 1          | 3.89   |       |

| Table D.2. Air Voids Verificatio | n Test Results Data | (continued) |
|----------------------------------|---------------------|-------------|
|----------------------------------|---------------------|-------------|

| Proj.<br>No. | Mix<br>Type | Lot<br>No. | Contr. | SCDOT |
|--------------|-------------|------------|--------|-------|
| V09          | Surf A      | 1          | 4.22   |       |
| V09          | Surf A      | 2          | 2.98   | 3.67  |
| V09          | Surf A      | 2          | 2.71   | 3.19  |
| V09          | Surf A      | 2          | 2.84   |       |
| V09          | Surf A      | 2          | 2.81   |       |
| V09          | Surf A      | 3          | 3.52   | 2.81  |
| V09          | Surf A      | 3          | 3.66   | 4.93  |
| V09          | Surf A      | 3          | 3.78   | 3.93  |
| V09          | Surf A      | 3          | 4.08   |       |
| V09          | Surf A      | 3          | 3.52   |       |
| V09          | Surf A      | 3          | 4.19   |       |
| V09          | Surf A      | 4          | 3.04   | 3.84  |
| V09          | Surf A      | 4          | 4.25   |       |
| V09          | Surf A      | 4          | 5.02   | 4.57  |
| V09          | Surf A      | 4          | 4.39   |       |
| V09          | Surf A      | 5          | 4.37   | 4.25  |
| V09          | Surf A      | 5          | 3.66   |       |
| V09          | Surf A      | 5          | 2.24   | 4.62  |
| V09          | Surf A      | 5          | 4.66   |       |
| V09          | Surf A      | 6          | 2.69   | 2.56  |
| V09          | Surf A      | 6          | 4.11   | 4.02  |
| V09          | Surf A      | 6          | 3.56   |       |
| V09          | Surf A      | 6          | 3.20   | 3.42  |
| V09          | Surf A      | 7          | 3.22   |       |
| V09          | Surf A      | 7          | 3.39   |       |
|              |             |            |        |       |
| V10          | Interm B    | 1          | 3.77   | 3.86  |
| V10          | Interm B    | 1          |        | 4.21  |
| V10          | Interm B    | 2          | 4.34   | 4.90  |
| V10          | Interm B    | 2          | 4.55   |       |
| V10          | Interm B    | 2          | 3.91   |       |
| V10          | Interm B    | 3          | 3.63   | 3.74  |
| V10          | Interm B    | 3          | 3.99   |       |
| V10          | Interm B    | 3          | 2.54   | 2.66  |
| V10          | Interm B    | 4          | 4.14   | 3.71  |
| V10          | Interm B    | 4          | 4.58   |       |
| V10          | Interm B    | 4          | 3.43   | 3.23  |
| V10          | Interm B    | 4          | 4.69   |       |
| V10          | Interm B    | 4          | 3.50   |       |
| V10          | Interm B    | 5          | 4.37   |       |
| V10          | Interm B    | 5          | 4.38   |       |
| V10          | Interm B    | 5          | 4.66   |       |
| V10          | Interm B    | 5          | 4.55   |       |
|              |             |            |        |       |
| V10          | Interm B    | 6          | 4.06   |       |
| V10          | Interm B    | 6          | 3.74   |       |
| V10          | Interm B    | 6          | 4.30   |       |
| V10          | Interm B    | 7          | 3.76   | 3.40  |
| V10          | Interm B    | 7          | 4.92   |       |
| V10          | Interm B    | 7          | 4.55   | 4.55  |

| Proj.<br>No. | Mix<br>Type | Lot<br>No. | Contr. | SCDOT |
|--------------|-------------|------------|--------|-------|
| V10          | Interm B    | 7          |        | 3.08  |
| V10          | Interm B    | 8          | 4.35   | 3.49  |
| V10          | Interm B    | 8          |        | 5.15  |
| V10          | Interm B    | 8          | 3.89   |       |
| V10          | Interm B    | 4          | 4.14   | 3.71  |
| V10          | Interm B    | 4          | 4.58   |       |
| V10          | Interm B    | 4          | 3.43   | 3.23  |
| V10          | Interm B    | 4          | 4.69   |       |
| V10          | Interm B    | 4          | 3.50   |       |
| V10          | Interm B    | 5          | 4.37   |       |
| V10          | Interm B    | 5          | 4.38   |       |
| V10          | Interm B    | 5          | 4.66   |       |
| V10          | Interm B    | 5          | 4.55   |       |
|              |             |            |        |       |
| V10          | Surf A      | 1          | 5.30   | 5.72  |
| V10          | Surf A      | 1          | 5.42   | 5.58  |
| V10          | Surf A      | 1          | 4.63   | 4.52  |
| V10          | Surf A      | 1          | 4.67   |       |
| V10          | Surf A      | 2          | 3.91   |       |
| V10          | Surf A      | 2          | 4.09   | 4.44  |
| V10          | Surf A      | 2          | 4.24   | 4.59  |
| V10          | Surf A      | 2          | 4.68   |       |
| V10          | Surf A      | 3          | 3.82   |       |
| V10          | Surf A      | 3          | 3.50   |       |
| V10          | Surf A      | 3          | 3.56   | 3.52  |
| V10          | Surf A      | 3          | 3.37   | 2.86  |
| V10          | Surf A      | 4          | 5.01   |       |
| V10          | Surf A      | 4          | 4.61   |       |
| V10          | Surf A      | 4          | 4.47   | 3.51  |
| V10          | Surf A      | 4          | 3.97   |       |
| V10          | Surf A      | 5          | 4.83   | 5.03  |
| V10          | Surf A      | 5          | 4.66   |       |
| V10          | Surf A      | 5          | 4.83   |       |
|              |             | -          |        |       |
| V10          | Surf A      | 6          | 4.65   | 3.34  |
| V10          | Surf A      | 6          | 4.05   | 3.01  |
| V10          | Surf A      | 6          | 3.03   | 3.08  |
| V10          | Surf A      | 7          | 3.80   | 3.80  |
| V10          | Surf A      | 7          |        | 3,37  |
| V10          | Surf A      | 3          | 3.82   |       |
| V10          | Surf A      | .3         | 3.50   |       |
| V10          | Surf A      | 3          | 3.56   | 3,52  |
| V10          | Surf A      | 3          | 3.37   | 2.86  |
| V10          | Surf A      | 4          | 5.01   |       |
| V10          | Surf A      | 4          | 4.61   |       |
| V10          | Surf A      | 4          | 4.47   | 3.51  |
| V10          | Surf A      | 4          | 3.97   |       |
| V10          | Surf A      | 5          | 4.83   | 5.03  |
| V10          | Surf A      | 5          | 4.66   | 0.00  |
| V10          | Surf A      | 5          | 4.83   |       |
| V 10         | Juli A      | 5          | 7.00   |       |

| Proj.<br>No. | Mix<br>Type | Lot<br>No. | Contr. | SCDOT |
|--------------|-------------|------------|--------|-------|
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|              | 1           | 1          | 1      |       |

# Table D.2. Air Voids Verification Test Results Data (continued)

| Proj.<br>No | Mix<br>Type | Lot<br>No | Contr. | SCDOT |
|-------------|-------------|-----------|--------|-------|
| V01         | Interm B    | 1         | 14 30  | 13.03 |
| V01         | Interm B    | 1         | 14.60  | 10.00 |
| V01         | Interm B    | 1         | 15 29  |       |
| V01         | Interm B    | 1         | 14.45  | 14.40 |
| V01         | Interm B    | 1         | 15.36  | 15.12 |
| V01         | Interm B    | 1         | 15.30  | 10.12 |
| V01         | Interm B    | 1         | 1/ /3  |       |
| V01         | Interm B    | 1         | 15 21  |       |
| V01         | Interm B    | 2         | 1/ 28  |       |
| V01         | Interm B    | 2         | 14.20  | 15.24 |
| V01         | Interm B    | 2         | 14.45  | 14.82 |
| V01         | Interm B    | 2         | 1/ 3/  | 15.33 |
| V01         | Interm B    | 2         | 15 10  | 10.00 |
| V01         | Interm B    | 2         | 14.50  |       |
| V01         | Interm B    | 3         | 12.97  |       |
| V01         | Interm P    | 2         | 14.04  |       |
| V01         | Interm P    | 2         | 14.94  |       |
| V01         | Interm P    | 3         | 14.41  | 14.96 |
| V01         | Interm P    | 4         | 14.23  | 14.00 |
| V01         |             | 4         | 14.09  |       |
| V/01        | Surf A      | 1         | 1/ 80  | 14 15 |
| V01         |             | 1         | 14.03  | 14.13 |
| V01         |             | 1         | 14.32  | 14.30 |
| V01         |             | 2         | 14.23  | 13.85 |
| V01         |             | 2         | 14.86  | 15.00 |
| V01         | Surf A      | 1         | 14.00  | 10.00 |
| V01         | Surf A      | 5         | 15.75  | 14.66 |
| 101         | Guilin      | 0         | 10.70  | 14.00 |
| V02         | Interm B    | 1         | 14 67  |       |
| V02         | Interm B    | 2         | 13.78  | 13.96 |
| V02         | Interm B    | 2         | 10.70  | 13.29 |
| V02         | Interm B    | 3         | 13.46  | 14 17 |
| V02         | Interm B    | 3         | 14 52  | 17.17 |
| V02         | Interm B    | 4         | 13.62  |       |
| V02         | Interm B    | 5         | 13.80  | 13 65 |
| V02         | Interm B    | 5         | 13.57  | 12.58 |
| 102         |             |           | 10.07  | 12.00 |
| V02         | Surf A      | 1         | 15.05  | 17.54 |
| V02         | Surf A      | 1         | 14.17  | 14.82 |
| V02         | Surf A      | 1         | 13.56  | 13.26 |
| V02         | Surf A      | 1         |        | 14.07 |
| V02         | Surf A      | 2         | 14.74  | 13.72 |
| V02         | Surf A      | 2         | 14.35  | 14.15 |
| V02         | Surf A      | 2         | 13.72  |       |
| V02         | Surf A      | 2         | 13.98  |       |
| V02         | Surf A      | 3         | 13.79  | 13.43 |
| V02         | Surf A      | 3         | 13.75  |       |
| V02         | Surf A      | 3         | 13.68  |       |
| V02         | Surf A      | 4         | 14.40  | 14.83 |
| V02         | Surf A      | 4         | 13 77  |       |

| Table D.3. | VMA | Verification | Test | Results | Data |
|------------|-----|--------------|------|---------|------|
|------------|-----|--------------|------|---------|------|

| Proj.<br>No. | Mix<br>Type | Lot<br>No. | Contr. | SCDOT |
|--------------|-------------|------------|--------|-------|
| V02          | Surf A      | 4          | 14.70  |       |
| V02          | Surf A      | 5          | 14.27  |       |
| V02          | Surf A      | 5          | 14.83  |       |
| V02          | Surf A      | 5          | 14.22  |       |
| V02          | Surf A      | 5          | 14.25  |       |
| V02          | Surf A      | 5          | 12.78  | 14.69 |
| V02          | Surf A      | 5          | 14.69  |       |
|              |             |            |        |       |
| V02          | Surf A      | 6          | 14.51  | 14.81 |
| V02          | Surf A      | 6          | 14.25  |       |
| V02          | Surf A      | 6          | 14.11  |       |
| V02          | Surf A      | 6          | 13.78  |       |
| V02          | Surf A      | 7          | 14.55  | 14.68 |
| V02          | Surf A      | 7          | 14.58  |       |
| V02          | Surf A      | 7          | 14.74  |       |
| V02          | Surf A      | 8          | 14.73  | 15.67 |
| V02          | Surf A      | 8          | 14.14  |       |
| V02          | Surf A      | 8          | 14.33  |       |
| V02          | Surf A      | 9          | 15.11  | 14.62 |
| V02          | Surf A      | 9          | 15.34  |       |
| V02          | Surf A      | 9          | 14.70  | 14.84 |
| V02          | Surf A      | 9          | 14.57  |       |
| V02          | Surf A      | 9          | 14.48  |       |
| V02          | Surf A      | 10         | 14.57  | 14.83 |
| V02          | Surf A      | 10         | 14.16  |       |
| V02          | Surf A      | 10         | 14.07  | 14.27 |
|              |             |            |        |       |
| V02          | Surf A      | 11         | 14.18  | 15.21 |
| V02          | Surf A      | 11         | 14.75  |       |
| V02          | Surf A      | 11         | 14.79  | 16.63 |
| V02          | Surf A      | 11         | 14.18  |       |
| V02          | Surf A      | 11         | 13.91  |       |
| V02          | Surf A      | 12         | 13.71  |       |
| V02          | Surf A      | 12         | 13.73  |       |
| V02          | Surf A      | 12         | 14.01  |       |
| V02          | Surf A      | 12         | 13.96  |       |
| V02          | Surf A      | 13         | 14.58  | 14.34 |
| V02          | Surf A      | 13         | 13.82  |       |
| V02          | Surf A      | 13         | 14.01  |       |
| V02          | Surf A      | 13         | 13.80  |       |
| V02          | Surf A      | 14         | 14.24  | 14.60 |
| V02          | Surf A      | 14         | 13.45  |       |
| V02          | Surf A      | 14         | 14.23  |       |
| V02          | Surf A      | 14         | 14.07  | 14.27 |
| V02          | Surf A      | 14         | 14.39  |       |
| V02          | Surf A      | 14         | 14.11  |       |
| V02          | Surf A      | 15         | 14.08  | 13.94 |
| V02          | Surf A      | 15         | 13.65  | 15.21 |
| V02          | Surf A      | 15         | 14.68  |       |
| V02          | Surf A      | 15         | 13.88  |       |

| Proj.<br>No. | Mix<br>Type      | Lot<br>No. | Contr. | SCDOT |
|--------------|------------------|------------|--------|-------|
|              |                  |            |        |       |
| V02          | Surf A           | 16         | 14.55  | 13.60 |
| V02          | Surf A           | 16         | 13.27  | 13.76 |
| V02          | Surf A           | 16         | 14.19  |       |
| V02          | Surf A           | 16         | 13.91  |       |
| V02          | Surf A           | 17         | 14.55  | 15.14 |
| V02          | Surf A           | 17         | 14.12  | 15.35 |
| V02          | Surf A           | 17         | 14.75  |       |
| V02          | Surf A           | 17         | 13.96  |       |
| V02          | Surf A           | 18         | 13.35  | 15.23 |
| V02          | Surf A           | 18         | 14.82  |       |
| V02          | Surf A           | 18         | 14.62  | 16.13 |
| V02          | Surf A           | 18         | 14.71  |       |
| V02          | Surf A           | 19         | 14.27  | 14.91 |
| V02          | Surf A           | 19         | 14.71  |       |
| V02          | Surf A           | 19         | 15.20  | 15.47 |
| V02          | Surf A           | 19         | 14.18  |       |
| V02          | Surf A           | 20         | 14.33  | 14.59 |
| V02          | Surf A           | 20         | 13.58  |       |
| V02          | Surf A           | 20         | 13.55  |       |
| V02          | Surf A           | 20         | 14 52  |       |
| 102          | Curry            | 20         | 11.02  |       |
| V02          | Surf A           | 21         | 13.95  | 14.34 |
| V02          | Surf A           | 21         | 14.55  | 11.01 |
| V02          | Surf A           | 21         | 14.54  |       |
| V02          | Surf A           | 21         | 14.54  |       |
| V02          | Surf A           | 22         | 15.18  |       |
| V02          | Surf A           | 22         | 13.51  |       |
| V02          | Surf A           | 18         | 13.35  | 15.23 |
| V02          | Surf A           | 18         | 14.82  | .0.20 |
| V02          | Surf A           | 18         | 14.62  | 16.13 |
| V02          | Surf A           | 18         | 14 71  |       |
| V02          | Surf A           | 19         | 14.27  | 14 91 |
| V02          | Surf A           | 19         | 14 71  | 11.01 |
| V02          |                  | 19         | 15 20  | 15 47 |
| V02          |                  | 10         | 14 18  | 10.71 |
| V02          | Surf A           | 20         | 14 33  | 14 59 |
| V02          |                  | 20         | 13 58  | 14.00 |
| V02          | Surf A           | 20         | 13 55  |       |
| V02          | Surf A           | 20         | 14.52  |       |
| v 02         |                  | 20         | 17.02  |       |
| V02          | Surf B           | 1          | 15 12  | 15.03 |
| V02          | Surf R           | 1          | 15.72  | 10.00 |
| V02          | Surf R           | 1          | 14 34  | 14 71 |
| V02          | Surf R           | 1          | 13.54  | (4./) |
| V02          |                  | ו<br>ר     | 15 10  | 15.22 |
| V UZ         | Sull D           | 2          | 14.00  | 10.02 |
| \//\?        | Quirf D          | ,          |        |       |
| V02          | Surf B           | 2          | 14.03  | 16.04 |
| V02<br>V02   | Surf B<br>Surf B | 2          | 14.66  | 16.04 |

| Proi | Mix    | Lot |        |       |
|------|--------|-----|--------|-------|
| No.  | Туре   | No. | Contr. | SCDOT |
| V02  | Surf B | 3   | 14.61  | 14.58 |
| V02  | Surf B | 3   | 14.62  | 15.20 |
| V02  | Surf B | 3   | 15.27  | 15.36 |
| V02  | Surf B | 4   | 14.74  | 14.20 |
| V02  | Surf B | 4   | 14.70  |       |
| V02  | Surf B | 4   | 14.51  |       |
| V02  | Surf B | 6   | 13.67  | 13.79 |
| V02  | Surf B | 6   | 14.80  | 14.66 |
| V02  | Surf B | 6   | 13.74  |       |
|      |        |     |        |       |
| V02  | Surf B | 2   | 14.14  |       |
| V02  | Surf B | 2   | 15.12  |       |
| V02  | Surf B | 2   | 14.76  |       |
| V02  | Surf B | 3   | 14.37  | 15.97 |
| V02  | Surf B | 3   | 14.74  | 15.93 |
| V02  | Surf B | 3   | 14.80  | 14.21 |
| V02  | Surf B | 4   | 14.54  | 13.50 |
| V02  | Surf B | 4   | 14.15  |       |
| V02  | Surf B | 4   | 14.53  |       |
| V02  | Surf B | 4   | 14.63  |       |
| V02  | Surf B | 5   | 15.07  | 14.55 |
| V02  | Surf B | 5   | 15.01  |       |
| V02  | Surf B | 5   | 14.59  |       |
| V02  | Surf B | 6   | 14.40  | 14.70 |
| V02  | Surf B | 6   | 14.56  | 14.32 |
| V02  | Surf B | 6   | 14.31  |       |
| V02  | Surf B | 6   | 14.74  |       |
| V02  | Surf B | 6   | 14.16  |       |
|      |        |     |        |       |
| V02  | Surf B | 5   | 14.98  | 16.24 |
| V02  | Surf B | 5   | 14.69  |       |
| V02  | Surf B | 5   | 14.31  |       |
| V02  | Surf B | 6   | 14.43  |       |
| V02  | Surf B | 6   | 13.80  | 15.20 |
| V02  | Surf B | 6   | 14.53  | 14.33 |
| V02  | Surf B | 6   | 14.65  |       |
| V02  | Surf B | 6   | 14.04  |       |
| V02  | Surf B | 6   | 13.96  |       |
| V02  | Surf B | 7   | 14.69  |       |
| V02  | Surf B | 7   | 14.39  |       |
| V02  | Surf B | 7   | 13.62  |       |
| V02  | Surf B | 7   | 14.13  |       |
| V02  | Surf B | 8   | 14.77  | 15.13 |
| V02  | Surf B | 8   | 14.67  | 15.00 |
| V02  | Surf B | 8   | 14.15  |       |
| V02  | Surf B | 9   | 15.08  | 14.59 |
| V02  | Surf B | 9   | 14.34  | 14.28 |
| V02  | Surf B | 9   | 13.74  |       |
|      |        |     |        |       |
| V02  | Surf B | 10  | 15.02  | 16.08 |

# Table D.3. VMA Verification Test Results Data (continued)

| Table D.3. VMA Verification | Test Results Data ( | (continued) |
|-----------------------------|---------------------|-------------|
|-----------------------------|---------------------|-------------|

| Proj.<br>No. | Mix<br>Type | Lot<br>No. | Contr. | SCDOT |
|--------------|-------------|------------|--------|-------|
| V02          | Surf B      | 10         | 14.18  | 16.17 |
| V02          | Surf B      | 10         | 14.63  |       |
| V02          | Surf B      | 11         | 14.81  |       |
| V02          | Surf B      | 11         | 15.42  |       |
| V02          | Surf B      | 11         | 14.83  |       |
| V02          | Surf B      | 12         | 14.63  | 16.47 |
| V02          | Surf B      | 12         | 15.37  |       |
| V02          | Surf B      | 12         | 15.43  |       |
| V02          | Surf B      | 12         | 15.38  |       |
| V02          | Surf B      | 13         | 15.10  |       |
| V02          | Surf B      | 7          | 15.27  | 15.16 |
| V02          | Surf B      | 7          | 14.20  | 15.58 |
| V02          | Surf B      |            |        | 15.23 |
|              |             |            |        |       |
| V04          | Surf B      | 1          | 14.96  | 15.36 |
| V04          | Surf B      | 1          | 14.61  | 15.87 |
| V04          | Surf B      | 1          | 14.54  |       |
| V04          | Surf B      | 1          | 14.73  | 14.15 |
| V04          | Surf B      | 1          | 14.58  |       |
| V04          | Surf B      | 2          | 14.54  | 15.90 |
| V04          | Surf B      | 2          | 14.12  |       |
| V04          | Surf B      | 2          | 15.02  |       |
| V04          | Surf B      | 2          | 14.95  |       |
| V04          | Surf B      | 3          | 14.15  | 14.89 |
| V04          | Surf B      | 3          | 14.55  | 14.77 |
| V04          | Surf B      | 3          | 13.99  | 14.69 |
| V04          | Surf B      | 3          | 14.58  |       |
| V04          | Surf B      | 4          | 14.40  | 14.39 |
| V04          | Surf B      | 4          | 14.30  |       |
| V04          | Surf B      | 4          | 14.06  |       |
| V04          | Surf B      | 5          | 14.27  | 14.94 |
| V04          | Surf B      | 5          | 14.06  | 13.59 |
| V04          | Surf B      | 5          | 14.36  |       |
| V04          | Surf B      | 5          | 14.55  |       |
| V04          | Surf B      | 6          | 15.27  | 16.12 |
| V04          | Surf B      | 6          | 14.59  |       |
| V04          | Surf B      | 6          | 14.37  |       |
| V04          | Surf B      | 6          | 14.48  |       |
| V04          | Surf B      | 6          | 15.38  |       |
| 1/05         | 1 / D       |            | 44.07  | 40.04 |
| V05          | Interm B    | 2          | 14.07  | 16.21 |
| V05          | Interm B    | 2          | 14.39  | 40.00 |
| V05          | Interm B    | 2          | 15.34  | 16.22 |
| V05          | Interm B    | 2          | 14.75  | 15.00 |
| V05          | Interm B    | 3          | 14.00  | 15.90 |
| V05          |             | <u>১</u>   | 14.00  |       |
| V05          |             | 3          | 14.04  |       |
| V05          |             | 4          | 15.20  | 17 10 |
| V05          |             | 4          | 15.19  | 17.10 |
| 000          |             | 4          | 10.20  |       |

| Proj.<br>No. | Mix<br>Type | Lot<br>No. | Contr. | SCDOT |
|--------------|-------------|------------|--------|-------|
| V05          | Interm B    | 4          | 14.65  |       |
| V05          | Interm B    | 4          | 13.72  |       |
| V05          | Interm B    | 5          | 15.18  | 14.89 |
| V05          | Interm B    | 5          | 14.46  | 15.34 |
| V05          | Interm B    | 5          | 14.47  |       |
| V05          | Interm B    | 5          | 14.49  |       |
| V05          | Interm B    | 6          | 14.37  |       |
| V05          | Interm B    | 6          | 14.53  |       |
| V05          | Interm B    | 6          | 14.77  |       |
| V05          | Interm B    | 6          | 13.90  |       |
|              |             |            |        |       |
| V05          | Interm B    | 7          | 14.73  |       |
| V05          | Interm B    | 7          | 15.26  |       |
| V05          | Interm B    | 7          | 14.92  |       |
| V05          | Interm B    | 8          | 14.16  | 16.43 |
| V05          | Interm B    | 8          | 13.80  |       |
| V05          | Interm B    | 8          | 14.91  |       |
| V05          | Interm B    | 9          | 14.68  |       |
| V05          | Interm B    | 9          | 14.58  | 16.17 |
| V05          | Interm B    | 9          | 14.35  | 16.95 |
| V05          | Interm B    | 10         | 14.84  | 17.15 |
| V05          | Interm B    | 10         |        | 15.48 |
| V05          | Interm B    | 11         | 14.26  | 15.70 |
| V05          | Interm B    | 11         | 13.92  |       |
| V05          | Interm B    | 11         | 14.30  |       |
| V05          | Interm B    | 11         | 14.32  |       |
|              |             |            |        |       |
| V05          | Interm B    | 12         | 14.61  | 16.05 |
| V05          | Interm B    | 12         | 14.67  |       |
| V05          | Interm B    | 12         | 15.24  | 15.46 |
| V05          | Interm B    | 12         | 14.38  |       |
| V05          | Interm B    | 13         | 15.27  | 15.73 |
| V05          | Interm B    | 13         | 14.20  |       |
| V05          | Interm B    | 13         | 14.65  |       |
| V05          | Interm B    | 14         | 15.18  | 16.01 |
| V05          | Interm B    | 14         | 14.47  | 16.52 |
| V05          | Interm B    | 14         | 15.04  |       |
| V05          | Interm B    | 15         | 14.63  |       |
| V05          | Interm B    | 11         | 14.26  | 15.70 |
| V05          | Interm B    | 11         | 13.92  |       |
| V05          | Interm B    | 11         | 14.30  |       |
| V05          | Interm B    | 11         | 14.32  |       |
|              |             |            |        |       |
| V05          | Surf A      | 1          | 15.29  |       |
| V05          | Surf A      | 1          | 14.98  |       |
| V05          | Surf A      | 2          | 16.00  | 17.31 |
| V05          | Surf A      | 2          | 15.90  |       |
| V05          | Surf A      | 2          | 15.05  | 15.99 |
| V05          | Surf A      | 2          | 15.01  |       |
| V05          | Surf A      | 2          | 15.59  |       |

| Proj.<br>No. | Mix<br>Type | Lot<br>No. | Contr. | SCDOT |
|--------------|-------------|------------|--------|-------|
| V05          | Surf A      | 2          | 15.40  |       |
| V05          | Surf A      | 3          | 16.10  | 16.66 |
| V05          | Surf A      | 3          | 15.71  |       |
| V05          | Surf A      | 3          | 15.87  |       |
| V05          | Surf A      | 3          | 15.52  |       |
| V05          | Surf A      | 3          | 15.73  |       |
| V05          | Surf A      | 4          | 15.99  | 16.70 |
| V05          | Surf A      | 4          | 16.08  |       |
| V05          | Surf A      | 4          | 15.33  |       |
| V05          | Surf A      | 4          | 15.41  |       |
| V05          | Surf A      | 5          | 14.90  | 16.44 |
| V05          | Surf A      | 5          | 15.20  |       |
| V05          | Surf A      | 5          | 15.71  |       |
|              |             |            |        |       |
| V05          | Surf A      | 6          | 14.62  | 15.36 |
| V05          | Surf A      | 6          | 15.28  |       |
| V05          | Surf A      | 6          | 15.54  | 16.36 |
| V05          | Surf A      | 6          | 15.42  |       |
| V05          | Surf A      | 7          | 15.42  | 16.14 |
| V05          | Surf A      | 7          | 15.17  |       |
| V05          | Surf A      | 7          | 15.63  |       |
| V05          | Surf A      | 8          | 16.00  | 16.71 |
| V05          | Surf A      | 8          | 15.84  |       |
| V05          | Surf A      | 8          | 15.07  |       |
| V05          | Surf A      | 9          | 16.44  | 17.06 |
| V05          | Surf A      | 9          | 15.83  | 17.15 |
| V05          | Surf A      | 9          | 15.86  |       |
| V05          | Surf A      | 10         | 15.72  | 16.69 |
| V05          | Surf A      | 10         | 15.96  | 16.93 |
| V05          | Surf A      | 10         | 16.42  |       |
| V05          | Surf A      | 10         | 15.31  |       |
|              |             |            |        |       |
| V05          | Surf A      | 11         | 15.67  |       |
| V05          | Surf A      | 11         | 16.43  | 15.59 |
| V05          | Surf A      | 11         | 15.66  | 16.22 |
| V05          | Surf A      | 11         | 14.65  |       |
| V05          | Surf A      | 11         | 15.62  |       |
| V05          | Surf A      | 12         | 15.67  | 16.84 |
| V05          | Surf A      | 12         | 14.81  | 16.75 |
| V05          | Surf A      | 12         | 16.00  |       |
| V05          | Surf A      | 12         | 15.33  |       |
| V05          | Surf A      | 13         | 15.45  | 16.83 |
| V05          | Surf A      | 13         | 14.80  | 17.44 |
| V05          | Surf A      | 13         | 15.02  |       |
| V05          | Surf A      | 13         | 14.78  |       |
| V05          | Surf A      | 13         | 15.25  | 16.65 |
| V05          | Surf A      | 14         | 15.37  |       |
| V05          | Surf A      | 14         | 15.36  |       |
| V05          | Surf A      | 14         | 15.31  | 16.34 |
| V05          | Surf A      | 15         | 15 19  |       |

| Table D.3. VMA | Verification | <b>Test Results</b> | Data | (continued) |
|----------------|--------------|---------------------|------|-------------|
|----------------|--------------|---------------------|------|-------------|

| Proj.<br>No. | Mix<br>Type | Lot<br>No. | Contr. | SCDOT |
|--------------|-------------|------------|--------|-------|
| V05          | Surf A      | 15         | 15.30  | 16.30 |
| V05          | Surf A      | 15         | 16.12  |       |
| V05          | Surf A      | 15         | 14.97  |       |
| V05          | Surf A      | 15         | 15.12  | 15.91 |
|              |             |            |        |       |
| V05          | Surf A      | 16         | 15.07  |       |
| V05          | Surf A      | 16         | 14.74  | 15.45 |
| V05          | Surf A      | 16         | 15.30  |       |
| V05          | Surf A      | 16         | 15.30  |       |
| V05          | Surf A      | 16         | 15.94  | 16.59 |
| V05          | Surf A      | 17         | 14.98  |       |
| V05          | Surf A      | 17         | 14.53  |       |
| V05          | Surf A      | 17         | 15.01  | 16.22 |
| V05          | Surf A      | 17         | 14.35  |       |
| V05          | Surf A      | 17         | 14.38  |       |
| V05          | Surf A      | 18         | 15.19  |       |
| V05          | Surf A      | 18         | 15.95  |       |
| V05          | Surf A      | 18         | 15.42  | 15.90 |
| V05          | Surf A      | 18         | 15.54  |       |
| V05          | Surf A      | 18         | 15.64  | 15.89 |
| V05          | Surf A      | 19         | 16.07  |       |
| V05          | Surf A      | 19         | 15.88  | 16.16 |
| V05          | Surf A      | 19         | 15.04  | 15.38 |
| V05          | Surf A      | 20         | 15.51  | 16.50 |
| V05          | Surf A      | 20         | 16.36  |       |
| V05          | Surf A      | 20         | 16.02  | 15.82 |
| V05          | Surf A      | 20         | 15.46  |       |
| V05          | Surf A      | 20         | 15.24  |       |
|              |             |            |        |       |
| V05          | Surf A      | 21         | 16.29  | 16.42 |
| V05          | Surf A      | 21         | 15.04  |       |
| V05          | Surf A      | 21         | 15.50  |       |
| V05          | Surf A      | 22         | 16.05  |       |
| V05          | Surf A      | 22         | 15.70  | 16.21 |
| V05          | Surf A      | 22         | 15.16  | 15.54 |
| V05          | Surf A      | 23         | 14.77  | 16.07 |
| V05          | Surf A      | 23         | 15.34  |       |
| V05          | Surf A      | 23         | 15.44  |       |
| V05          | Surf A      | 23         | 14.91  |       |
| V05          | Surf A      | 24         | 14.76  | 15.69 |
| V05          | Surf A      | 24         | 15.11  |       |
| V05          | Surf A      | 24         | 14.88  |       |
| V05          | Surf A      | 25         | 14.47  |       |
| V05          | Surf A      | 25         | 14.55  |       |
|              |             |            |        |       |
| V05          | Surf B      | 1          | 15.52  |       |
| V05          | Surf B      | 1          | 14.81  |       |
| V05          | Surf B      | 1          | 15.70  | 17.25 |
| V05          | Surf B      | 1          | 15.65  |       |
| V05          | Surf B      | 1          | 15.89  |       |

## Table D.3. VMA Verification Test Results Data (continued)

| Proj.<br>No. | Mix<br>Type | Lot<br>No. | Contr. | SCDOT |
|--------------|-------------|------------|--------|-------|
| V05          | Surf B      | 2          | 16.16  |       |
| V05          | Surf B      | 2          | 15.83  | 17.40 |
| V05          | Surf B      | 2          | 15.73  |       |
| V05          | Surf B      | 2          | 16.04  | 16.59 |
| V05          | Surf B      | 2          | 15.33  | 10100 |
| V05          | Surf B      | 2          | 15.08  | 16.89 |
| V05          | Surf B      | 3          | 15.25  |       |
| V05          | Surf B      | 3          | 16.10  |       |
| V05          | Surf B      | 3          | 15.11  | 16.95 |
| V05          | Surf B      | 4          | 15.25  |       |
| V05          | Surf B      | 4          | 15.52  |       |
| V05          | Surf B      | 4          | 15.49  |       |
| V05          | Surf B      | 5          | 15.05  | 16.86 |
| V05          | Surf B      | 5          | 14.74  | 16.44 |
| V05          | Surf B      | 5          | 15.18  |       |
| V05          | Surf B      | 5          | 14.50  |       |
| V05          | Surf B      | 5          | 15.87  |       |
|              |             |            |        |       |
| V05          | Surf B      | 6          | 15.17  | 16.22 |
| V05          | Surf B      | 6          | 15.46  | 15.63 |
| V05          | Surf B      | 6          | 14.37  | 16.11 |
| V05          | Surf B      | 6          | 15.09  |       |
| V05          | Surf B      | 6          | 15.22  |       |
| V05          | Surf B      | 7          | 15.17  |       |
| V05          | Surf B      | 7          | 15.03  |       |
| V05          | Surf B      | 7          | 14.96  |       |
| V05          | Surf B      | 8          | 15.41  | 16.11 |
| V05          | Surf B      | 8          | 14.62  |       |
| V05          | Surf B      | 8          | 15.29  | 16.07 |
| V05          | Surf B      | 8          | 14.98  |       |
| V05          | Surf B      | 4          | 15.25  |       |
| V05          | Surf B      | 4          | 15.52  |       |
| V05          | Surf B      | 4          | 15.49  |       |
| V05          | Surf B      | 5          | 15.05  | 16.86 |
| V05          | Surf B      | 5          | 14.74  | 16.44 |
| V05          | Surf B      | 5          | 15.18  |       |
| V05          | Surf B      | 5          | 14.50  |       |
| V05          | Surf B      | 5          | 15.87  |       |
|              |             |            |        |       |
| V06          | Interm C    | 1          | 17.08  |       |
| V06          | Interm C    | 2          | 16.94  | 16.43 |
| V06          | Interm C    | 3          | 16.20  | 17.28 |
| V06          | Interm C    | 3          |        | 16.52 |
| V06          | Interm C    | 4          | 16.72  | 16.72 |
| V06          | Interm C    | 5          | 17.14  |       |
| V06          | Interm C    | 5          | 17.00  |       |
|              |             |            |        |       |
| V09          | Surf A      | 1          | 14.62  | 15.45 |
| V09          | Surf A      | 1          | 14.76  |       |
| V09          | Surf A      | 1          | 14.39  |       |

| Proj.<br>No. | Mix<br>Type | Lot<br>No. | Contr. | SCDOT |
|--------------|-------------|------------|--------|-------|
| V09          | Surf A      | 1          | 15.07  |       |
| V09          | Surf A      | 2          | 14.64  | 15.25 |
| V09          | Surf A      | 2          | 14.44  | 14.55 |
| V09          | Surf A      | 2          | 14.28  |       |
| V09          | Surf A      | 2          | 14.59  |       |
| V09          | Surf A      | 3          | 14.71  | 13.79 |
| V09          | Surf A      | 3          | 14.83  | 15.23 |
| V09          | Surf A      | 3          | 14.67  | 14.97 |
| V09          | Surf A      | 3          | 14.95  |       |
| V09          | Surf A      | 3          | 13.87  |       |
| V09          | Surf A      | 3          | 14.91  |       |
| V09          | Surf A      | 4          | 14.19  | 14.94 |
| V09          | Surf A      | 4          | 14.89  |       |
| V09          | Surf A      | 4          | 15.64  | 14.74 |
| V09          | Surf A      | 4          | 15.24  |       |
| V09          | Surf A      | 5          | 14.62  | 14.91 |
| V09          | Surf A      | 5          | 15.03  |       |
| V09          | Surf A      | 5          | 13.96  | 13.94 |
| V09          | Surf A      | 5          | 14.46  |       |
| V09          | Surf A      | 6          | 14.31  | 13.93 |
| V09          | Surf A      | 6          | 15.21  | 14.88 |
| V09          | Surf A      | 6          | 14.74  |       |
| V09          | Surf A      | 6          | 14.40  | 14.57 |
| V09          | Surf A      | 7          | 14.11  |       |
| V09          | Surf A      | 7          | 14.24  |       |
|              |             |            |        |       |
| V10          | Interm B    | 1          | 15.07  | 14.15 |
| V10          | Interm B    | 1          |        | 15.55 |
| V10          | Interm B    | 2          | 14.92  | 15.00 |
| V10          | Interm B    | 2          | 14.71  |       |
| V10          | Interm B    | 2          | 15.15  |       |
| V10          | Interm B    | 3          | 13.73  | 14.85 |
| V10          | Interm B    | 3          | 13.83  |       |
| V10          | Interm B    | 3          | 14.62  | 14.36 |
| V10          | Interm B    | 4          | 14.60  | 15.69 |
| V10          | Interm B    | 4          | 14.76  |       |
| V10          | Interm B    | 4          | 14.79  | 14.46 |
| V10          | Interm B    | 4          | 14.90  |       |
| V10          | Interm B    | 4          | 14.55  |       |
| V10          | Interm B    | 5          | 15.28  |       |
| V10          | Interm B    | 5          | 14.16  |       |
| V10          | Interm B    | 5          | 15.07  |       |
| V10          | Interm B    | 5          | 15.12  |       |
|              |             |            |        |       |
| V10          | Interm B    | 6          | 14.74  |       |
| V10          | Interm B    | 6          | 14.70  |       |
| V10          | Interm B    | 6          | 14.79  |       |
| V10          | Interm B    | 7          | 15.33  | 14.66 |
| V10          | Interm B    | 7          | 15.49  |       |
| V10          | Interm B    | 7          | 15.07  | 15.36 |

| Proj.<br>No. | Mix<br>Type | Lot<br>No. | Contr. | SCDOT |
|--------------|-------------|------------|--------|-------|
| V10          | Interm B    | 7          |        | 15.21 |
| V10          | Interm B    | 8          | 14.60  | 14.43 |
| V10          | Interm B    | 8          |        | 15.72 |
| V10          | Interm B    | 8          | 14.87  |       |
| V10          | Interm B    | 4          | 14.60  | 15.69 |
| V10          | Interm B    | 4          | 14.76  |       |
| V10          | Interm B    | 4          | 14.79  | 14.46 |
| V10          | Interm B    | 4          | 14.90  |       |
| V10          | Interm B    | 4          | 14.55  |       |
| V10          | Interm B    | 5          | 15.28  |       |
| V10          | Interm B    | 5          | 14.16  |       |
| V10          | Interm B    | 5          | 15.07  |       |
| V10          | Interm B    | 5          | 15.12  |       |
|              |             |            |        |       |
| V10          | Surf A      | 1          | 15.92  | 16.55 |
| V10          | Surf A      | 1          | 15.14  | 16.84 |
| V10          | Surf A      | 1          | 15.61  | 15.41 |
| V10          | Surf A      | 1          | 14.81  |       |
| V10          | Surf A      | 2          | 14.66  |       |
| V10          | Surf A      | 2          | 15.69  | 15.06 |
| V10          | Surf A      | 2          | 15.28  | 15.67 |
| V10          | Surf A      | 2          | 15.40  |       |
| V10          | Surf A      | 3          | 15.12  |       |
| V10          | Surf A      | 3          | 15.25  |       |
| V10          | Surf A      | 3          | 15.00  | 15.44 |
| V10          | Surf A      | 3          | 14.88  | 14.83 |
| V10          | Surf A      | 4          | 15.62  |       |
| V10          | Surf A      | 4          | 15.70  |       |
| V10          | Surf A      | 4          | 14.60  | 15.34 |
| V10          | Surf A      | 4          | 15.04  |       |
| V10          | Surf A      | 5          | 14.83  | 16.12 |
| V10          | Surf A      | 5          | 15.57  |       |
| V10          | Surf A      | 5          | 15.69  |       |
|              |             |            |        |       |
| V10          | Surf A      | 6          | 15.16  | 14.83 |
| V10          | Surf A      | 6          | 15.44  | 15.63 |
| V10          | Surf A      | 6          | 15.13  | 15.98 |
| V10          | Surf A      | 7          | 15.37  | 15.30 |
| V10          | Surf A      | 7          |        | 14.69 |
| V10          | Surf A      | 3          | 15.12  |       |
| V10          | Surf A      | 3          | 15.25  |       |
| V10          | Surf A      | 3          | 15.00  | 15.44 |
| V10          | Surf A      | 3          | 14.88  | 14.83 |
| V10          | Surf A      | 4          | 15.62  |       |
| V10          | Surf A      | 4          | 15.70  |       |
| V10          | Surf A      | 4          | 14.60  | 15.34 |
| <u>V</u> 10  | Surf A      | 4          | 15.04  |       |
| V10          | Surf A      | 5          | 14.83  | 16.12 |
| V10          | Surf A      | 5          | 15.57  |       |
| V10          | Surf A      | 5          | 15.69  |       |

| Table D.3. | VMA | Verification | <b>Test Results</b> | Data | (continued) |
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| Proj.<br>No. | Mix<br>Type | Lot<br>No. | Contr. | SCDOT |
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| Total Printing Cost       | \$544.26 |
|---------------------------|----------|
| Total Number of Documents | 30       |
| Cost per Unit             | \$18.14  |