## Bridge Health Monitoring Metrics: Updating the Bridge Deficiency Algorithm

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## Aging Infrastructure Systems Center of Excellence

The University of Alabama and


## University Transportation Center for Alabama

The University of Alabama, The University of Alabama at Birmingham, and The University of Alabama in Huntsville

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## Executive Summary

The Alabama Department of Transportation (ALDOT) contracted The University of Alabama (UA) to update the algorithm that ranks bridges according to deficiency. This project (ALDOT \#930-661) began in August 2006 and finished in April 2008. The goal of this project was to develop a "common sense" algorithm that used simple functions to calculate bridge relative deficiency based on physical bridge characteristics represented in the bridge database. The algorithm's criteria and weight factors were adjusted by comparing the deficiency rankings against the judgment of experienced ALDOT engineers and bridge inspectors.

The contents of this report are as follows. First, the original deficiency algorithm (1991 algorithm) is reviewed since the updated algorithm builds on the original and the lessons learned using it. Next, the updated algorithm is presented: specifically, the functions that compare bridge characteristics in the database against deficiency criteria and assign deficiency points according to the weight factors. The criteria are organized into a matrix, as are the weight factors and adjustment factors to facilitate future adjustment of the algorithm (Figure C-1).

In the third chapter of this report, the new algorithm is evaluated by comparing lists of bridges ranked in order of decreasing deficiency against

- the judgment of experienced division bridge inspectors,
- the 194 bridges selected for replacement in the 2007 through 2011 bridge replacement program, and
- a similar list produced by the 1991 deficiency algorithm.

The lists of deficient bridges produced by the new algorithm showed excellent agreement with each of the above. Where discrepancies occurred, there was almost always a logical explanation.

Chapter 4 explains the process used to develop the algorithm. A graphical interface was developed to quickly adjust the criteria and weight factors and to assess the impact on the deficiency rankings. A detailed list of deficient bridges was also created for spot checking the calculations.

Chapter 5 describes a sensitivity analysis of the weight factors using different scenarios. This analysis was used to determine the range of values that best differentiated each type of deficiency without overshadowing other deficiencies.

And finally, Chapter 6 presents conclusions and recommendations.

Appendix A contains a decision tree of the algorithm that presents the calculation procedures of the algorithm in an easy-to-follow manner. Appendix B contains a flow chart of the algorithm, and Appendix C shows the source code for the algorithm.

### 1.0 1991 Deficiency Algorithm

The original deficiency algorithm was developed in 1991 by Richardson and Turner (1991a, 1991b). The algorithm compared certain characteristics for each bridge recorded in the state bridge database against performance criteria. Bridges not meeting the performance criteria were assigned "deficiency points." The output of the algorithm was a list of bridges ranked from most to least deficient. The bridge deficiency rankings were used to help select bridges for replacement.

In developing the 1991 algorithm, the project team

- reviewed procedures used by other states,
- developed criteria appropriate for Alabama bridges,
- formulated an algorithm to calculate deficiency points, and
- validated the algorithm results against the judgment of experienced ALDOT engineers.

Each of these tasks is reviewed briefly in the following sections.

## Review of Other States' Procedures

Using data in the bridge database, the algorithm compared certain bridge characteristics against goals. These goals, called level of service goals, were set so that bridges meetings these goals would provide highway users with an acceptable level of service. Four categories of goals were developed that were considered to affect the level of service provided to users. A review of level of service goals of other states showed similar goal categories, although the relative importance of the goals varied from state to state. (See Table 1-1.)

Table 1-1. Goal Categories for Calculating Bridge Level of Service (Richardson and Turner, 1991a)

| Goal Category | $\cdots \cdots$ Relative Importance (\% of Total Deficiency) $-\cdots-$ - |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | North Carolina | Virginia | Nebraska | Kansas | Alabama |
| Load Capacity | 70 | 30 | 50 | 17 | 40 |
| Condition | 6 | 46 | 10 | 55 | 40 |
| Width | 12 | 12 | 12 | 28 | 10 |
| Vertical Clearance | 12 | 12 | 28 | 0 | 10 |

## Alabama Deficiency Criteria

The deficiency criteria selected for Alabama are shown in the last column of Table 1-1. A bridge's load capacity and vertical clearance affect the level of service provided to truck traffic. Trucks exceeding the posted load limit or vertical clearance must detour around the bridge. The bridge width affects the level of service provided to both car and truck traffic. Finally, condition ratings indirectly affect the level of service because bridges in very poor condition have an increased likelihood of being closed.

In addition to the four categories described above, another category called special condition points was added to accommodate situations not depicted in the bridge database. For example, if a particular bridge was the only bridge on a route in poor condition, it might be a candidate for special condition points. These points (typically between 30 and 40) were assigned by the State Bridge Maintenance Engineer in consultation with division engineers and bridge inspectors.

The specific goals for three of the four goal categories were assigned in tiers according to the level of service expected from the highway over the bridge. (See Table 1-2.) Bridges carrying routes with higher functional classifications were assigned more stringent goals.

Table 1-2. Goals for Load Capacity, Width, and Vertical Clearance for Each of Five Functional Classifications

| Functional Classification | Load Capacity, tons <br> (Inventory Rating) | Width*, ft <br> $(\mathrm{n}=$ number of lanes) | Vertical Clearance, ft |
| :--- | :---: | :---: | :---: |
| Interstate | 36 | $12 \mathrm{n}+2+2$ | 16 |
| Arterial | 36 | $12 \mathrm{n}+2+2$ | 16 |
| Major Collector | 27 | $11 \mathrm{n}+2+2$ | 15 |
| Minor Collector | 18 | $10 \mathrm{n}+1+1$ | 15 |
| Local | 18 | $10 \mathrm{n}+1+1$ | 14 |

*Width goals are for two-way traffic

Specific goals for the condition goal category can be inferred from the scheme assigning deficiency points for the condition ratings of the major bridge components. (See Table 1-3.) Deficiency points were assigned if the condition rating for the deck, superstructure, or substructure was less than a " 5 ." When a bridge inspector assigns a bridge component a condition rating of " 4 ," he or she must write a letter to the State Maintenance Engineer explaining the situation. Also, the load capacity of the bridge should be re-analyzed and if this is not possible, the load capacity should be set equal to half of the design load. When a condition rating of " 3 " is assigned to a bridge, the bridge should be load posted at three tons and inspected every three months.

Table 1-3. Deficiency Points for Poor Condition Ratings

| Condition Rating | $\cdots \cdots$ Deficiency Points $\cdots-\cdots-$ |  |  |
| :---: | :---: | :---: | :---: |
|  | Deck | Superstructure | Substructure |
| 4 | 5 | 10 | 15 |
| 3 | 10 | 20 | 30 |
| $<=2$ | 20 | 40 | 60 |

Bridge owners occasionally opt to replace a single component of a bridge (e.g. a timber deck in poor condition supported by a superstructure and substructure in good condition). Since a deck is the least costly to replace, it received the fewest deficiency points. (See Table 1-3.)
Replacement of the substructure generally involves complete bridge replacement; therefore, this component was allocated the most deficiency points.

## Algorithm to Calculate Deficiency Points

The load capacity and vertical clearance deficiency points were multiplied by an average daily traffic (ADT) factor and by a detour length factor, and the width deficiency points were multiplied by an ADT factor. The specific functions of the algorithm are presented in a later section of this report as part of a comparison with the new deficiency algorithm.

The 1991 algorithm calculated the total deficiency points of each bridge in the database to form a ranked list of the most-deficient bridges in the state. The total deficiency points were calculated as the sum of the deficiency points in each category. The deficiency points for each category could not exceed the values shown in the last column of Table 1-1, and the total deficiency points could not exceed 100.

## Validation of Algorithm

The 1991 algorithm was validated by comparing the ranked list of deficient bridges against similar lists produced by experienced ALDOT and county engineers and bridge inspectors. Issues raised during the discussions with local engineers and bridge inspectors included:

- the ADT factor should be decreased
- the inventory rating (the measure of load capacity used by the 1991 algorithm) did not reflect the effects of strengthening; perhaps only load-posted bridges should receive deficiency points
- especially narrow bridges should receive more deficiency points
- bridges with scour problems should receive deficiency points
- the ADT numbers for county routes were not always accurate

The ADT factor was decreased, which addressed the first and fifth issue above. The other issues were not addressed in the 1991 algorithm.

## Performance of the 1991 Algorithm

ALDOT engineers and managers used the ranked list of deficient bridges, as calculated by the deficiency algorithm, to help select the state-owned bridges recommended for replacement. The following shortcomings were observed by ALDOT engineers and managers:

- Not enough deficiency points were assigned to very narrow bridges.
- Deficiency points were not assigned to culverts.
- Load capacity was represented by inventory rating, but bridges are posted for load restrictions based on operating ratings.
- The goals for load capacity, width and vertical clearance were not stringent enough.
- The goals and weight factors should be easy to update (without modifying the source code of the program).
- The deficiency equations were not intuitive (i.e. simple and based on a bridge's physical characteristics).


### 2.0 New Algorithm

Each of the issues listed on the preceding page were addressed in the new deficiency algorithm described below. The new algorithm was designed specifically for state-owned bridges, because the population of state-owned bridges differs significantly from county and municipal bridges, and because the processes for selecting bridges for replacement are very different at the state vs. the county level. A follow-on project has been proposed for developing an algorithm specifically for "locally-owned" bridges (county, city, etc.).

The new deficiency algorithm was developed based on the concept of bridge utility. Bridges with characteristics causing loss of utility for the highway user should be assigned deficiency points. The project team reviewed all of the 294 fields in the bridge database and selected four fields as the best measures of bridge utility. (See Table 2-1.) Although these fields represent similar criteria as those used for the 1991 algorithm (Table 1-1), the actual deficiencies are calculated very differently.

Table 2-1. Bridge Database Items and Relative Weight for New Deficiency Algorithm

| Database Item | Relative Weight |
| :--- | :---: |
| Load Capacity Ratings | 40 |
| Condition Ratings | 30 |
| Bridge Width <br> (curb-to-curb) | 20 |
| Vertical Clearance <br> (on and under bridge) | 10 |

Bridges with posted load or height restrictions prevent a certain percentage of truck traffic from using the bridge. Narrow bridges do not prevent use of a bridge, but nonetheless limit the utility of the bridge. For example, if a vehicle breaks down on a narrow bridge, the shoulder is typically not wide enough to allow the motorist to pull completely out of the traffic lane.

Bridges with poor condition ratings are nearing the end of their service lives due to deterioration and loss of structural integrity, and bridge replacement is typically a multi-year process. Therefore, bridges in poor condition should be assigned deficiency points so they can be replaced before their condition deteriorates to the point where they must be closed.

The relative weights of the deficiency categories shown in Table 2-1 are similar to the relative weights used for the 1991 algorithm. (See Table 1-1.) For both algorithms, the load capacity ratings and the condition ratings constitute the bulk of the possible deficiency points. While the other two deficiency categories (width and vertical clearance) involve a measurement of a single bridge feature, load ratings and condition ratings are based on many factors which are
synthesized using engineering judgment to produce a numerical rating. These ratings, while less precise than measured bridge widths or vertical clearances, have greater meaning.

The actual relative weights were selected based on several analyses (described in Chapter 4 of this report) including: a graphical summary of the distribution of bridge deficiencies, a bridge-by-bridge comparison of algorithm results, and a sensitivity study of multiple weighting scenarios.

The specific algorithms for calculating deficiency points and adjustment factors are described in the next five sections:

- Load Capacity Deficiency Points
- Condition Deficiency Points
- Width Deficiency Points
- Vertical Clearance Deficiency Points
- ADT, ADTT, and Detour Length Factors

The corresponding functions from the 1991 algorithm are also shown for comparison purposes.
For the load capacity, width and vertical clearance deficiencies, the functions are all piece-wise linear with four segments, as shown in Figure 2-1. Segments 1 and 4 are always horizontal (constant deficiency): the maximum deficiency points are assigned if the bridge characteristic is below the "minimum acceptable" value, and zero deficiency points are assigned if the bridge characteristic is above the "desirable" value. For bridge characteristics between the minimum acceptable and the desirable, deficiency points are calculated by interpolating on the appropriate segment.


Figure 2-1. Typical deficiency point function.

## Load Capacity Deficiency Points

Truck traffic is only affected by reduced load capacity of a bridge if the bridge is load-posted. Therefore, only bridges posted for load (Posting Status $=$ " P " in the bridge database) are assigned load capacity deficiency points in the new algorithm.

Load restrictions are placed on a bridge if bridge load rating analyses indicate that the operating rating (maximum permissible load) of the bridge is less than the legal load in the state of Alabama. Alabama calculates the maximum safe permissible load of a bridge for eight different vehicle configurations, shown in Figure 2-2 along with the maximum legal gross weight for each vehicle. The load rating factor (RF) is the ratio of the maximum safe load divided by the maximum legal gross vehicle weight. Most state-owned bridges have been load rated, and this information is available in the bridge database.

1. School Bus

12.5 tons
2. H Truck

3. 2 Axle Truck

29.5 tons
4. Concrete Truck


33 tons
5. HS Truck

6. Triaxle Dump Truck

37.5 tons
7. 18 Wheeler


40 tons
8. 6 Axle Truck


Figure 2-2. Maximum legal gross vehicle weights in Alabama.

Bridges that have not been load rated are assigned deficiency points based on the operating rating. The operating rating is specified by the federal government to be the safe permissible load for the HS Truck configuration. The inventory rating, by comparison, is specified to be the HS load that can be applied to a bridge for an indefinite period of time. The inventory rating of a bridge is approximately 0.75 of the operating rating. The inventory rating is used in the formula to calculate the sufficiency rating for a bridge (which controls eligibility for federal replacement funding). The operating rating is used to determine whether a bridge should be load posted, and is therefore the appropriate rating factor to use for assigning load capacity deficiency points.

Deficiency points are assigned to a bridge if the rating factors for certain load rating vehicles are less than one (Table 2-2). Load deficiency points are accumulated for each rating factor less than one, up to a maximum of 40 points.

Table 2-2. Load Deficiency Points, ADTT Factor, and Detour Factor Assigned for Each Load Rating Vehicle

| Load Rating Vehicle | Deficiency Points if <br> $\mathbf{R F}<\mathbf{1}$ | ADTT Factor | Detour Factor |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| School Bus | 30 |  | x |  |  |  |
| H Truck | 0 |  | x |  |  |  |
| Two-Axle Truck | 20 |  | x |  |  |  |
| Concrete Truck | 0 |  | x |  |  |  |
| HS Truck | 0 |  | x |  |  |  |
| Triaxle Dump Truck | 10 |  | x |  |  |  |
| 18-Wheeler | 20 |  |  |  |  |  |
| Six-Axle Truck | 5 |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Max Load Deficiency Points $=40$ |  |  |  |  |  |  |

No deficiency points were assigned for the H Truck and the HS Truck since these are AASHTO design vehicles, and the Two-Axle Truck and 18-Wheeler are similar vehicles (respectively) and are more appropriate for Alabama. Also, no deficiency points were assigned for the Concrete Truck since the rating factor for this truck is usually similar to the rating factor for the Triaxle Dump Truck.

It was assumed that most of the truck traffic on state highways consisted of either Two-Axle Trucks or 18-Wheelers. As a partial justification, weigh-in-motion data for I-20/59 near Bucksville is shown in Figure 2-3. The FHWA vehicle classes are shown in Figure 2-4. The Two-Axle Trucks and 18-Wheelers were each assigned 20 deficiency points. These deficiency points will be multiplied by factors related to the average daily truck traffic (ADTT) and the detour length for the bridge.


Figure 2-3. Distribution of truck types for I-20/59 near Bucksville.


Figure 2-4. FWHA vehicle classification scheme.
The School Bus, the Triaxle Dump Truck, and the Six-Axle Truck were assigned 30, 10, and five deficiency points, respectively. These deficiency points will not be multiplied by the ADTT factor, since these vehicles represent a small percentage of truck traffic, but will be multiplied by the detour factor.

If load ratings for the eight rating vehicles are not available in the bridge database, then up to 40 load capacity deficiency points are assigned using the operating rating as illustrated in Figure 25 , which also shows the 1991 algorithm function for comparison. The deficiency points are then multiplied the ADTT factor and the detour length factor.

Load deficiency points as calculated by the 1991 and by the new algorithm are compared in Table 2-3. The 1991 algorithm assigns deficiency points to many more bridges, due to its use of the more conservative inventory rating and its disregard of the posting status. Also, the 1991
algorithm enforces a maximum of 40 load deficiency points after the ADT and detour factors are applied; whereas the new algorithm applies the maximum of 40 load deficiency points before the ADT and detour factors are applied.


Figure 2-5. Load capacity deficiency points calculation: 1991 algorithm vs. new algorithm.
Table 2-3. Distribution of Bridges with Load Deficiency Points: 1991 Algorithm vs. New Algorithm

| Load Deficiency Points | $\cdots \cdots \cdots$ Number of Bridges $\cdots \cdots \cdots$ |  |
| :---: | :---: | :---: |
|  | $\mathbf{1 9 9 1}$ Algorithm | New Algorithm |
|  | 63 | 0 |
| 10 | 56 | 0 |
| 15 | 91 | 0 |
| 20 | 90 | 0 |
| 25 | 67 | 0 |
| 30 | 79 | 0 |
| 35 | 65 | 0 |
| 40 | 323 | 0 |
| 45 | 0 | 1 |
| 50 | 0 | 0 |
| 55 | 0 | 0 |
| 60 | 0 | 8 |
| Sum | 834 | 9 |

## Condition Deficiency Points

The 1991 algorithm assigned condition deficiency points as discussed earlier (shown again in the left-half of Table 2-4 below for convenience). The new algorithm assigns deficiency points in an apparently similar manner but with three significant differences.

- The new algorithm includes the condition ratings for channel condition in addition to the ratings for deck, superstructure, and substructure.
- The 1991 algorithm assigned a maximum of 40 condition deficiency points while the new algorithm applies no such maximum.
- The 1991 algorithm did not multiply condition deficiency points by ADT or detour length factors, whereas the new algorithm does.

Table 2-4. Deficiency Points for Poor Condition Ratings

| Condition Rating | ------ 1991 Algorithm ----- |  |  | Condition Rating | ------ - New Algorithm ------ - |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Deck | Superstructure | Substructure |  | Lowest Rating* | $2^{\text {nd }}$ Lowest Rating* | $3^{\text {rd }}$ Lowest Rating* |
| 4 | 5 | 10 | 15 | 4 | 20 | 10 | 5 |
| 3 | 10 | 20 | 30 | <=3 | 30 | 20 | 10 |
| $<=2$ | 20 | 40 | 60 |  |  |  |  |

*of deck, superstructure, substructure and channel condition ratings for bridges, or of culvert and channel condition ratings for culverts

Table 2-5 compares the condition deficiency points assigned to state-owned bridges by the 1991 and the new algorithms. The new algorithm assigned condition deficiency points to slightly more bridges ( 148 vs. 123 ), but assigned considerably more deficiency points.

Table 2-5. Distribution of Bridges with Condition Deficiency Points: 1991 Algorithm vs. New Algorithm

| Condition Deficiency Points | ------ Number of Bridges ----- |  |
| :---: | :---: | :---: |
|  | 1991 Algorithm | New Algorithm |
| 5 | 16 | 0 |
| 10 | 40 | 0 |
| 15 | 52 | 0 |
| 20 | 5 | 3 |
| 25 | 4 | 92 |
| 30 | 3 | 25 |
| 35 | 0 | 11 |
| 40 | 3 | 10 |
| 45 | 0 | 3 |
| 50 | 0 | 1 |
| 55 | 0 | 0 |
| 60 | 0 | 3 |
| Sum: | 123 | 148 |

## Width Deficiency Points

Based on experience using the 1991 algorithm as a tool for selecting bridges for replacement, narrow bridges were not assigned enough deficiency points. The possible deficiency points for narrow bridges were therefore increased from 10 to 20 , and the width criteria were made more stringent. Width criteria from the two algorithms are compared in Table 2-6.

The 1991 deficiency algorithm project set "minimum" and "desirable" goals for all criteria, but only the "minimum" goals were used. The bridge width criteria for the new algorithm represent the "desirable" width goals from the 1991 project.

Table 2-6. Comparison of Bridge Width Criteria: 1991 Algorithm vs. New Algorithm

|  | 1991 Algorithm | New Algorithm |
| :--- | :---: | :---: |
| Lane Width, ft | 12 | 12 |
| Shoulder Width, ft |  |  |
| 2-way traffic (both shoulders) | 2 | 10 |
| 1-way traffic, right shoulder | 2 | 10 |
| 1-way traffic, left shoulder | 2 | 6 |

To calculate width deficiency points for a particular bridge, target widths are calculated.
Calculation of target widths is illustrated below for a two-lane bridge carrying two-way traffic.
1991 algorithm: target_width $=\left(12^{\prime} /\right.$ lane $)(2$ lanes $)+2^{\prime}+2^{\prime}=28^{\prime}$
New algorithm: target_width $=\left(12^{\prime} /\right.$ lane $)(2$ lanes $)+10^{\prime}+10^{\prime}=44^{\prime}$
Bridges with widths greater than the above targets would be assigned no deficiency points. Width deficiency points are assigned to each bridge by comparing the curb-to-curb width of the actual bridge against the target widths, as illustrated in Figure 2-6 below. The width deficiency points are multiplied by the ADT and detour length factors to get the total width deficiency.


Figure 2-6. Example width deficiency point calculation for two-lane bridge: 1991 algorithm vs. new algorithm.

The example width deficiency functions shown in Figure 2-6 show that the new algorithm assigns more width deficiency points than the 1991 algorithm. Table 2-7 shows the distributions of width deficiency points assigned by the two algorithms for all state-owned bridges. The new algorithm assigns more width deficiency points due to the following three factors:

- 20 points possible vs. only 10 points possible for the 1991 algorithm
- more stringent criteria
- 1991 algorithm applied ADT and detour factors before enforcing maximum of 10 width deficiency points

Table 2-7. Distribution of Bridges with Width Deficiency Points: 1991 Algorithm vs. New Algorithm

| Width Deficiency Points | $\cdots \cdots$ Number of Bridges $\cdots \cdots$ |  |
| :---: | :---: | :---: |
|  | 1991 Algorithm | New Algorithm |
| 2 | 447 | 563 |
| 4 | 12 | 419 |
| 6 | 38 | 121 |
| 8 | 101 | 121 |
| 10 | 476 | 764 |
| 12 | 0 | 471 |
| 14 | 0 | 166 |
| 16 | 0 | 24 |
| 18 | 0 | 37 |
| 20 | 0 | 22 |
| 22 | 0 | 14 |
| 24 | 0 | 27 |
| 26 | 0 | 5 |
| 28 | 0 | 3 |

## Vertical Clearance Deficiency Points

Vertical clearance deficiency points are calculated similarly for both the 1991 and the new algorithms. Both algorithms assign up to 10 deficiency points. The new algorithm uses more stringent criteria. (See Figure 2-7.) And whereas the 1991 algorithm applied the ADT and detour length factors before enforcing the maximum vertical clearance deficiency of 10 points, the new algorithm does not enforce a maximum.

The vertical clearance deficiency points are multiplied by the appropriate ADTT factor (since this deficiency affects truck traffic only) and detour length factor to get the total vertical clearance deficiency. Clearance deficiencies for the route over the bridge used the ADT, percentage of trucks, and detour length for the "on-bridge" route; and clearance deficiencies for
the route under the bridge used the ADT, percentage of trucks, and detour length for the "underbridge" route. For the rare bridge that has both on-bridge and under-bridge vertical clearance restrictions, the deficiency points for each are added to get the total vertical clearance deficiency for the bridge.


Figure 2-7. Vertical clearance deficiency point calculation: 1991 algorithm vs. new algorithm.

The vertical clearance deficiency functions shown in Figure 2-7 show that the new algorithm assigns more width deficiency points than the 1991 algorithm. Table $2-8$ shows the distributions of vertical clearance deficiency points assigned by the two algorithms for all state-owned bridges. The new algorithm assigns more vertical clearance deficiency points due to the following two factors:

- more stringent criteria
- 1991 algorithm applied ADT and detour factors before enforcing maximum of 10 width deficiency points

Table 2-8. Distribution of Bridges with Vertical Clearance Deficiency Points: 1991 Algorithm vs. New Algorithm

| Vertical Clearance <br> Deficiency Points | $\cdots \cdots$ Number of Bridges $-\cdots-\cdots$ |  |
| :---: | :---: | :---: |
|  | 1991 Algorithm | New Algorithm |
| 2 | 4 | 60 |
| 4 | 6 | 80 |
| 6 | 4 | 60 |
| 8 | 2 | 69 |
| 10 | 54 | 86 |
| 12 | 0 | 108 |
| 14 | 0 | 28 |
| 16 | 0 | 2 |
| 18 | 0 | 2 |

## ADT, ADTT, and Detour Length Factors

These factors serve as multipliers to increase deficiency points for bridges with relatively high ADT, ADTT, and/or detour length. The ADT factor for a bridge is based on the percent rank of the bridge ADT out of all bridges and culverts in Alabama. For example, the percent rank of an $\mathrm{ADT}=1200$ (the median ADT ) is 0.50 , and the percent rank of an $\mathrm{ADT}=200,000$ is 1.0 .

The distributions of ADT, ADTT, and detour length are shown in Figures 2-8a, 2-9a, and 2-10a. The ADT factor, the ADTT factor, and the detour length factor are shown in Figures 2-8b, 2-9b, and 2-10b along with the factors from the 1991 algorithm for comparison. The following observations can be made:

- ADT Factor The ADT factor for the 1991 algorithm was unreasonable, nearly tripling the deficiency points for bridges with very high traffic volumes, and reducing to zero the deficiency points for bridges with very low traffic volumes. (See Figure 2-8a.) The ADT factor for the new algorithm increases the deficiency points up to $30 \%$ for bridges with traffic volumes above the median but does not decrease the deficiency points for bridges with traffic volumes below the median. This compromise recognizes the urgency of high traffic volume bridges with serious deficiencies, but keeps low traffic volume bridges with serious deficiencies from being "outranked" by high traffic volume bridges with less serious deficiencies.
- ADTT Factor The 1991 algorithm did not use an average daily truck traffic (ADTT) factor. This factor is more appropriate than the ADT factor for multiplying deficiencies applicable to truck traffic only, such as load capacity and vertical clearance. ADTT is calculated by multiplying two database items as follows: ADTT = ADT x \%_Trucks. In the new algorithm, deficiency points are increased by up to $30 \%$ for bridges with ADTT above the median. (See Figure 2-9b.)
- Detour Length Factor The detour length factor for the 1991 algorithm was not reasonable, increasing by up to $70 \%$ the deficiency points for bridges with greater than the minimum detour length of one mile. (See Figure 2-10b.) The detour length factor for the new algorithm increases by up to $10 \%$ ) the deficiency points for bridges with detour lengths greater than the median detour length (four miles).


Figure 2-8a. Distribution of ADT on Alabama bridges and culverts.


Figure 2-9a. Distribution of ADTT on Alabama bridges and culverts.


Figure 2-8b. ADT Factor: 1991 algorithm vs. new algorithm.


Figure 2-9b. ADTT factor for new algorithm.


Figure 2-10a. Distribution of detour length on Alabama bridges and culverts.


Figure 2-10b. Detour length factor: 1991 algorithm vs. new algorithm.

### 3.0 Evaluation of the New Algorithm

The performance of the new algorithm described in the previous section was assessed by comparing the ranked list of deficient bridges against three other lists:

- Bridges picked for replacement by bridge inspectors from Divisions 6 and 8
- Bridges on the Five-Year Bridge Replacement Program, FY 2007-2011
- Bridges ranked by the 1991 deficiency algorithm


## Comparison with Division Bridge Inspectors

The new algorithm was used to produce a list of deficient bridges for a single ALDOT division. The project team traveled to the division and met individually with the division bridge inspector. During the meeting, the inspector commented on the list of deficient bridges and on the deficiency algorithm in general. A summary of those comments are presented below for Division 8 and Division 6.

For both divisions, most of the 20 most-deficient bridges were scheduled for replacement. Reasonable explanations were provided for almost all of the exceptions.

- Division 8 Bridges The most-deficient bridges for Division 8 are listed in Table 3-1. The first column of the table indicates the replacement status of the bridge, according to the bridge inspector. Of the 20 most-deficient bridges, 18 were either replaced $(\mathrm{R})$ or scheduled to be replaced (S).

No explanation was provided for bridge \#2910 with rank 10 not being scheduled for replacement. Bridge \#9625 with rank 18 is a relief bridge (over a flood plain, normally dry) over a dirt road with an underclearance of 10.4 feet. The bridge inspector commented that since the dirt road has virtually no traffic, the underclearance should possibly be removed from the database.

Bridge \#2319 rank 34 was scheduled for replacement because it is of similar type and near Bridge \#2320 rank 7 which is scheduled for replacement. Bridge \#2670 rank 104 is a culvert scheduled for replacement as part of a road widening project. The culvert was built in 1942 and although it is in good condition, it makes more sense to replace the entire culvert rather than add a new section to lengthen it.

Note that the two bridges already replaced have a posting status of " K " (closed). The bridge inspector recommended that the deficiency algorithm list the closed bridges as
deficient (based on condition, width and vertical clearance) but not move the bridge to the top of the list.

- Division 6 Bridges The most-deficient bridges for Division 6 are listed in Table 3-2. Of the 21 most-deficient bridges, eight were scheduled to be replaced (S). Comments on the 13 of these 21 bridges not scheduled to be replaced are summarized below:

| Rank | Bin | Comment |
| :---: | :---: | :---: |
| 2 | 19618 | has been strengthened by adding false bents |
| 4 | 2853 | no comment |
| 7 | 1911 | channel condition $=4$, but Sufficiency Rating $=62$ (not eligible) |
| 10 | 1695 | channel condition $=4$, but Sufficiency Rating $=62$ |
| 11 | 271 | on historic route (Selma to Montgomery civil rights march) |
| 12 | 11726 | division ranking $=121$ |
| 13 | 10690 | has fatigue-prone pin and hanger connection, but Suf. Rating $=61$ |
| 15 | 8803 | channel cond. $=4$, plan to encase piles in concrete and riprap channel |
| 16 | 5088 | no comment |
| 17 | 12988 | channel cond. $=4$, will be fixed by district |
| 20 | 9542 | underclearance needs to be remeasured (likely error in database) |
| 25 | 9528 | underclearance needs to be remeasured (likely error in database) |
| 78 | 3041 | will be replaced as part of route realignment |
| 79 | 3042 | will be replaced as part of route realignment |
| 125 | 1031 | on same route and similar to BIN 1029 (rank 14) |

Table 3-1. Division 8 Bridges Scheduled to be Replaced (S) or Already Replaced (R)

|  |  | ¢ | 름 |  |  |  |  |  | $\begin{array}{\|c} \hline \stackrel{y}{c} \\ \vdots \\ \vdots \\ y^{\prime} \\ \hline \end{array}$ |  |  |  |  |  |  |  |  |  | $\begin{aligned} & 0 \\ & \vdots \\ & \vdots \\ & 1_{1}^{\prime} \\ & \frac{1}{3} \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \delta_{1} \\ & \frac{1}{4} \\ & \frac{5}{3} \\ & \hline \end{aligned}$ |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S | 1 | 3817 | 8 | S.R. 69 | Jackson Creek | 6 | A | 10 |  |  |  |  |  |  |  | 5 | 5 | 4 | N | 5 | 22 | 2 | 2-way | 99.99 | 0 | 0.0 | 23.4 | 18.5 | 0.0 | 41.9 |
| S | 2 | 3818 | 8 | S.R. 69 | JACkSon Creek relief | 6 | A | 10 |  |  |  |  |  |  |  | 5 | 5 | 4 | N | 6 | 22 | 2 | 2-way | 99.99 | 0 | 0.0 | 23.4 | 18.5 | 0.0 | 41.9 |
| S | 3 | 1268 | 8 | S.R. 69 | KANETUCHE CREEK | 43 | A | 50 |  |  |  |  |  |  |  | 5 | 5 | 4 | N | 5 | 22 | 2 | 2-way | 99.99 | 0 | 0.0 | 23.0 | 18.1 | 0.0 | 41.1 |
| R | 4 | 1739 | 8 | U.S. 43 | BATES CRK. | 6 | к | 10 | 37 | 53 | 49 | 48 | 82 | 80 | 43 | 5 | 5 | 4 | N | 5 | 24 | 2 | 1-way | 99.99 | 0 | 0.0 | 25.6 | 14.1 | 0.0 | 39.7 |
| S | 5 | 1917 | 8 | U.S. 43 | LEWIS CRK. | 6 | A | 10 | 26 | 53 | 49 | 48 | 82 | 82 | 43 | 5 | 5 | 4 | N | 5 | 24 | 2 | 1-way | 99.99 | 0 | 0.0 | 25.5 | 14.0 | 0.0 | 39.5 |
| R | 6 | 1918 | 8 | U.S. 43 | ROBERTS CREEK | 6 | K |  |  |  |  |  |  |  |  | 5 | 5 | 4 | N | 6 | 24 | 2 | 1-way | 99.99 | 0 | 0.0 | 25.5 | 14.0 | 0.0 | 39.5 |
| S | 7 | 2320 | 8 | US. 45 \& S.R. 17 | CREEK | 44 | D | 62 |  |  |  |  |  |  |  | 5 | 6 | 4 | N | 5 | 24 | 2 | 2-way | 99.99 | 0 | 0.0 | 25.1 | 12.5 | 0.0 | 37.6 |
| S | 8 | 5977 | 8 | S.R. 69 | BRANCH | 6 | D | 3 |  |  |  |  |  |  |  | 5 | 5 | 4 | N | 6 | 24 | 2 | 2-way | 99.99 | 0 | 0.0 | 23.9 | 13.2 | 0.0 | 37.1 |
| S | 9 | 3016 | 8 | U.S. 80 | FRENCH CRK. | 33 | A | 49 |  |  |  |  |  |  |  | 6 | 5 | 4 | N | 5 | 26 | 2 | 1-way | 99.99 | 0 | 0.0 | 25.8 | 11.4 | 0.0 | 37.1 |
|  | 10 | 2910 | 8 | U.S. 11 | yellow Creek | 38 | A | 56 |  |  |  |  |  |  |  | 5 | 4 | 5 | N | 6 | 26 | 2 | 2-way | 99.99 | 0 | 0.0 | 25.5 | 11.6 | 0.0 | 37.1 |
| S | 11 | 4797 | 8 | U.S. 80 | SUCARNOOCHEE CRK.REL. | 6 | K |  |  |  |  |  |  |  |  | 5 | 6 | 4 | N | 7 | 28 | 2 | 2-way | 99.99 | 0 | 0.0 | 26.0 | 10.6 | 0.0 | 36.6 |
| S | 12 | 1717 | 8 | S.R. 5 | MUD CRK. | 50 | A | 65 |  |  |  |  |  |  |  | 5 | 5 | 4 | N | 5 | 24 | 2 | 2-way | 99.99 | 0 | 0.0 | 23.4 | 12.9 | 0.0 | 36.3 |
| S | 13 | 3033 | 8 | U.S. 84 | ESCAMBIA CREEK | 44 | A | 55 |  |  |  |  |  |  |  | 5 | 4 | 5 | N | 6 | 26 | 2 | 2-way | 99.99 | 0 | 0.0 | 24.8 | 11.4 | 0.0 | 36.2 |
| S | 14 | 2566 | 8 | S.R. 28 | RELIEF | 6 | A | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 5 | 6 | 4 | N | 5 | 24 | 2 | 2-way | 99.99 | 0 | 0.0 | 23.3 | 12.8 | 0.0 | 36.0 |
| S | 15 | 2567 | 8 | S.R. 28 | CHICKASAW BOGUE CRK. | 6 | A | 10 | 31 | 43 | 46 | 44 | 55 | 78 | 40 | 5 | 5 | 4 | N | 5 | 24 | 2 | 2-way | 99.99 | 0 | 0.0 | 23.3 | 12.8 | 0.0 | 36.0 |
| S | 16 | 843 | 8 | S.R. 156 | BRANCH | 49 | A | 70 |  |  |  |  |  |  |  | 5 | 5 | 4 | N | 6 | 24 | 2 | 2-way | 99.99 | 0 | 0.0 | 22.9 | 11.4 | 0.0 | 34.3 |
| S | 17 | 3024 | 8 | S.R. 10 | SPEARS CRK. | 12 | D | 10 | 28 | 34 | 38 | 33 | 54 | 55 | 34 | 5 | 5 | 4 | N | 5 | 26 | 2 | 2-way | 99.99 | 0 | 0.0 | 21.8 | 10.1 | 0.0 | 31.9 |
|  | 18 | 9625 | 8 | S.R. 10 | COUNTY Road | 63 | A | 53 | 40 | 49 | 47 | 46 | 78 | 78 | 48 | 6 | 6 | 6 | N | 9 | 28 | 2 | 2-way | 99.99 | 10.4 | 0.0 | 0.0 | 10.2 | 13.2 | 23.4 |
| S | 19 | 6201 | 8 | U.S. 84 | TOMBIGBEE RIVER | 44 | A | 34 |  |  |  |  |  |  |  | 5 | 5 | 5 | N | 5 | 26 | 2 | 2-way | 16.17 | 0.00 | 0.0 | 0.0 | 11.1 | 11.6 | 22.7 |
| S | 20 | 4794 | 8 | US 80 | S.R. 17 | 51 | A | 53 |  |  |  |  |  |  |  | 5 | 5 | 6 | N | N | 28 | 2 | 2-way | 99.99 | 16.07 | 0.0 | 0.0 | 10.3 | 9.5 | 19.8 |
|  | 21 | 3300 | 8 | S.R. 69 | SALITPA CRK.REL. | 72 | A | 51 | 32 | 43 | 38 | 38 | 63 | 60 | 39 | 6 | 6 | 6 | N | 5 | 22 | 2 | 2-way | 99.99 | 0 | 0.0 | 0.0 | 18.1 | 0.0 | 18.1 |
|  | 22 | 3301 | 8 | S.R. 69 | SALITPA CRK. | 71 | A | 49 |  |  |  |  |  |  |  | 6 | 6 | 6 | N | 5 | 22 | 2 | 2-way | 99.99 | 0 | 0.0 | 0.0 | 18.1 | 0.0 | 18.1 |
|  | 23 | 3302 | 8 | S.R. 69 | Eberlein mill crk. | 63 | A | 53 |  |  |  |  |  |  |  | 6 | 5 | 6 | N | 5 | 22 | 2 | 2-way | 99.99 | 0 | 0.0 | 0.0 | 17.7 | 0.0 | 17.7 |
|  | 24 | 2547 | 8 | U.S. 43 | FRISCO R.R. OVERPASS | 44 | A | 47 |  |  |  |  |  |  |  | 6 | 5 | 5 | N | N | 24 | 2 | 2-way | 99.99 | 21.75 | 0.0 | 0.0 | 14.3 | 0.0 | 14.3 |
|  | 25 | 1762 | 8 | S.R. 21 | FRISCO R.R. | 55 | A | 48 |  |  |  |  |  |  |  | 5 | 5 | 6 | N | N | 24 | 2 | 2-way | 99.99 | 22.01 | 0.0 | 0.0 | 13.4 | 0.0 | 13.4 |
|  | 26 | 2261 | 8 | S.R. 5 | Cub Creek | 63 | A | 73 | 52 | 46 | 49 | 47 | 60 | 62 | 43 | 5 | 5 | 5 | N | 5 | 24 | 2 | 2-way | 99.99 | 0 | 0.0 | 0.0 | 13.3 | 0.0 | 13.3 |
|  | 27 | 2262 | 8 | S.R. 5 | Moccasin Creek | 63 | A | 66 |  |  |  |  |  |  |  | 5 | 5 | 5 | N | 6 | 24 | 2 | 2-way | 99.99 | 0 | 0.0 | 0.0 | 13.3 | 0.0 | 13.3 |
|  | 28 | 5206 | 8 | S.R. 28 | barton Crk. | 56 | A | 45 |  |  |  |  |  |  |  | 5 | 5 | 5 | N | 5 | 24 | 2 | 2-way | 99.99 | 0 | 0.0 | 0.0 | 12.8 | 0.0 | 12.8 |
|  | 29 | 2555 | 8 | S.R. 17 | SOUWILPA CREEK | 79 | A | 61 |  |  |  |  |  |  |  | 6 | 6 | 6 | N | 6 | 24 | 2 | 2-way | 99.99 | 0 | 0.0 | 0.0 | 12.7 | 0.0 | 12.7 |
|  | 30 | 5205 | 8 | S.R. 28 | double Crk. | 61 | A | 50 |  |  |  |  |  |  |  | 5 | 5 | 5 | N | 6 | 24 | 2 | 2-way | 99.99 | 0 | 0.0 | 0.0 | 12.6 | 0.0 | 12.6 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| S | 34 | 2319 | 8 | US. 45 \& S.R. 17 | BRANCH | 57 | D | 50 |  |  |  |  |  |  |  | 5 | 5 | 5 | N | 5 | 24 | 2 | 2-way | 99.99 | 0 | 0.0 | 0.0 | 12.5 | 0.0 | 12.5 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| S | 104 | 2670 | 8 | U.S. 43 | SPRINGFIELD CRK. | 66 | A | 62 | 30 | 43 | 51 | 42 | 59 | 66 | 27 | N | N | N | 6 | 6 | 29 | 2 | 2-way | 99.99 | 0 | 0.0 | 0.0 | 10.2 | 0.0 | 10.2 |

Table 3-2. Division 6 Bridges Scheduled to be Replaced (S)


## Comparison with the Five-Year Bridge Replacement Program

ALDOT managers selected 191 bridges to be replaced over a five-year period (2007-2011). The distribution of the deficiency rankings of these 191 bridges is shown in Figures 3-1 and 3-2. Of the 191 bridges, 181 were included in the 1700 most-deficient bridges. The other 10 bridges had no deficiency points assigned. Figure 3-2 shows that of the 50 most-deficient bridges, all but nine were selected to be replaced.

Overall, the deficiency algorithm performed satisfactorily, considering many bridges are selected for the replacement program based on information not available in the bridge database.


Figure 3-1. 182 of 191 bridges in five-year bridge replacement program in 1700 most-deficient bridges.


Figure 3-2. 93 of 191 bridges in five-year bridge replacement program in 200 most-deficient bridges.

## Comparison with the 1991 Deficiency Algorithm

The 100 most-deficient bridges according to the new algorithm were compared bridge-by-bridge with the deficiency ranks calculated by the 1991 algorithm. Tables 3-3 and 3-4 present the individual bridge data.

The major cause for the difference in rankings between the two algorithms is the 1991 algorithm over-assigned load deficiency points and under-assigned condition deficiency points. The 1991 algorithm assigned load deficiency points to 834 bridges compared with only 9 for the new algorithm. (See Table 2-3.) And although the two algorithms assigned condition deficiency points to approximately the same number of bridges, the new algorithm assigned approximately three times as many condition deficiency points.

Every one of the bridges in Tables 3-3 and 3-4 with a 1991 ranking greater than 500 had zero load deficiency points from the 1991 algorithm. These bridges are listed below with a comment regarding the cause of the discrepancy. The major cause was under-assignment of condition deficiency points.

| New | 1991 |  |
| :---: | :---: | :---: |
| Rank | Rank | 1991 Algorithm |
| 11 | 2905 | assigned no deficiency points (error?) |
| 25 | 662 | assigned no deficiency points for channel condition $=4$ |
| 30 | 567 | assigned no deficiency points for channel condition $=4$ |
| 32 | 686 | only assigns 5 deficiency points for deck condition $=4$ |
| 35 | 536 | assigned no deficiency points for channel condition $=4$ |
| 40 | 1446 | did not evaluate culverts |
| 49 | 2882 | assigned no deficiency points? |
| 51 | 539 | assigned only 15 deficiency points for substructure condition $=4$ |
| 54 | 831 | assigned no deficiency points for channel condition $=4$, no width points |
| 56 | 1103 | assigned only 5 deficiency points for deck condition $=4$, no width points |
| 58 | 540 | assigned only 15 deficiency points for substructure condition $=4$ |
| 60 | 542 | assigned only 15 deficiency points for substructure condition $=4$ |
| 65 | 759 | assigned only 10 points for superstructure condition $=4$, no width points |
| 72 | 537 | assigned only 15 deficiency points for substructure condition $=4$ |
| 73 | 541 | assigned only 15 deficiency points for substructure condition $=4$ |
| 74 | 790 | assigned no deficiency points for channel condition $=4$ |
| 79 | 656 | assigned only 10 points for superstructure condition $=4$ |
| 81 | 660 | assigned only 10 points for superstructure condition $=4$ |
| 86 | 1182 | assigned no deficiency points for channel condition $=4$ |
| 87 | 815 | assigned no deficiency points for channel condition $=4$ |
| 91 | 931 | assigned only 10 points for narrow deck, no vert. clearance points |
| 92 | 932 | assigned only 10 points for narrow deck, no vert. clearance points |

Table 3-3. Deficiency Points: 1991 Algorithm vs. New Algorithm Bridges Ranked 1 - 50

| \% |  |  |  |  |  |  | $\begin{aligned} & 0 \\ & 0_{0} \\ & \stackrel{1}{1} \\ & \frac{0}{3} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  |  |  | 爰 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1841 | P | 3 | 2 | 3 | 3 | 5 | N | 5 | 40 | 30 | 0 | 0 | 40 | 100 | 3 | 57.2 | 55.9 | 8.2 | 0.0 | 121.4 | 1 |
| 529 | P | 15 | 11 | 4 | 5 | 4 | N | N | 40 | 20 | 10 | 0 | 40 | 100 | 1 | 57.2 | 34.3 | 22.9 | 0.0 | 114.4 | 2 |
| 635 | P | 3 | 2 | 5 | 5 | 3 | N | 7 | 40 | 30 | 1.1 | 0 | 40 | 100 | 2 | 57.2 | 38.0 | 10.3 | 0.0 | 105.6 | 3 |
| 2736 | P | 15 | 11 | 6 | 5 | 2 | N | 5 | 40 | 40 | 8.4 | 0 | 40 | 100 | 4 | 57.2 | 36.4 | 11.0 | 0.0 | 104.6 | 4 |
| 1842 | P | 6 | 4 | 4 | 7 | 5 | N | 4 | 40 | 5 | 0 | 0 | 40 | 85 | 18 | 57.2 | 34.1 | 7.3 | 0.0 | 98.5 | 5 |
| 504 | P | 6.1 | 4 | 5 | 5 | 4 | N | 7 | 40 | 15 | 1 | 0 | 40 | 96 | 6 | 57.2 | 24.8 | 10.1 | 0.0 | 92.1 | 6 |
| 7608 | P | 13 | 10 | 7 | 7 | 4 | N | N | 40 | 15 | 0 | 0 | 0 | 55 | 80 | 57.2 | 22.3 | 9.0 | 0.0 | 88.5 | 7 |
| 2037 | P | 6.9 | 4.1 | 6 | 4 | 5 | N | 7 | 40 | 10 | 0 | 0 | 40 | 90 | 9 | 57.2 | 24.1 | 5.4 | 0.0 | 86.7 | 8 |
| 1765 | P | 6.1 | 4 | 5 | 7 | 4 | N | 7 | 40 | 15 | 0.7 | 0 | 40 | 95.7 | 7 | 42.3 | 24.8 | 10.1 | 0.0 | 77.2 | 9 |
| 4507 | D | 15 | 10 | 4 | 3 | 4 | N | 7 | 40 | 40 | 10 | 0 | 0 | 90 | 11 | 0.0 | 58.3 | 13.0 | 0.0 | 71.3 | 10 |
| 19818 | D | 39.7 | 36 | 3 | 3 | 3 | N | N | 0 | 0 | 0 | 0 | 0 | 0 | 2905 | 0.0 | 60.0 | 10.3 | 0.0 | 70.3 | 11 |
| 503 | D | 3 | 2 | 4 | 3 | 6 | N | 7 | 40 | 25 | 10 | 0 | 0 | 75 | 24 | 0.0 | 43.6 | 21.8 | 0.0 | 65.4 | 12 |
| 1394 | D |  | 0 | 3 | 5 | 6 | N | 5 | 40 | 10 | 10 | 0 | 0 | 60 | 57 | 0.0 | 37.1 | 24.7 | 0.0 | 61.8 | 13 |
| 1798 | D | 10 | 7.5 | 4 | 5 | 4 | N | 3 | 40 | 20 | 6.9 | 0 | 0 | 66.9 | 30 | 0.0 | 49.7 | 11.0 | 0.0 | 60.7 | 14 |
| 784 | E | 10 | 7.5 | 5 | 4 | 5 | N | 6 | 40 | 10 | 10 | 10 | 0 | 70 | 26 | 0.0 | 22.4 | 22.4 | 12.2 | 57.0 | 15 |
| 474 | D | 10 | 7.5 | 6 | 6 | 4 | N | 4 | 40 | 15 | 7.7 | 0 | 0 | 62.7 | 53 | 0.0 | 31.0 | 20.6 | 0.0 | 51.6 | 16 |
| 615 | D | 10 | 7.5 | 4 | 6 | 5 | N | 5 | 40 | 5 | 10 | 0 | 0 | 55 | 77 | 0.0 | 25.1 | 25.1 | 0.0 | 50.3 | 17 |
| 2712 | A | 6 | 4 | 4 | 6 | 4 | N | 5 | 40 | 20 | 10 | 0 | 0 | 70 | 28 | 0.0 | 37.2 | 12.4 | 0.0 | 49.5 | 18 |
| 6588 | A | 24 | 18 | 4 | 4 | 6 | N | 7 | 40 | 15 | 0.4 | 0 | 0 | 55.4 | 75 | 0.0 | 39.2 | 9.9 | 0.0 | 49.1 | 19 |
| 10132 | D | 10 | 7.5 | 5 |  | 4 | N | 4 | 40 | 25 | 0 | 0 | 0 | 65 | 48 | 0.0 | 40.8 | 8.2 | 0.0 | 49.1 | 20 |
| 10102 | A | 35.9 | 21.5 | 4 |  | 5 | N | 5 | 40 | 15 | 0 | 0 | 0 | 55 | 82 | 0.0 | 38.7 | 10.3 | 0.0 | 49.0 | 21 |
| 7365 | A | 24 | 18 | 4 | 4 | 6 | N | 7 | 40 | 15 | 0.4 | 0 | 0 | 55.4 | 76 | 0.0 | 39.1 | 9.8 | 0.0 | 48.9 | 22 |
| 9367 | D | 10 | 7 | 4 | 4 | 4 | N | N | 40 | 30 | 0 | 0 | 30 | 100 | 5 | 0.0 | 41.1 | 7.1 | 0.0 | 48.2 | 23 |
| 5816 | D | 10 | 7 | 4 | 4 | 7 | N |  | 40 | 15 | 0.9 | 0 | 0 | 55.9 | 71 | 0.0 | 37.6 | 10.2 | 0.0 | 47.8 | 24 |
| 12793 | A | 47.9 | 36 | 7 | 7 | 4 | N | 4 | 0 | 15 | 1.7 | 0 | 0 | 16.7 | 662 | 0.0 | 36.7 | 10.0 | 0.0 | 46.7 | 25 |
| 502 | A | 50.1 | 30 | 4 | 4 | 6 | N | 7 | 20.3 | 15 | 10 | 0 | 0 | 45.3 | 195 | 0.0 | 32.6 | 13.6 | 0.0 | 46.1 | 26 |
| 770 | A | 56.9 | 35 | 4 |  | 5 | N | N | 0 | 5 | 10 | 0 | 30 | 45 | 200 | 0.0 | 23.1 | 23.1 | 0.0 | 46.1 | 27 |
| 1665 | D | 10 | 7.5 |  | 5 | 4 | N | 7 | 40 | 20 | 8.3 | 0 | 0 | 68.3 | 29 | 0.0 | 34.0 | 11.3 | 0.0 | 45.4 | 28 |
| 4658 | A | 51.9 | 28.9 | 5 | 5 | 4 | N | 4 | 29.5 | 15 | 7.8 | 0 | 0 | 52.3 | 87 | 0.0 | 34.4 | 10.3 | 0.0 | 44.7 | 29 |
| 1072 | A | 65.9 | 45.9 | 5 | 5 | 4 | N | 4 | 0 | 15 | 7 | 0 | 0 | 22 | 567 | 0.0 | 33.3 | 11.1 | 0.0 | 44.4 | 30 |
| 1368 | A | 40.9 | 24.5 | 4 | 5 | 4 | N | 6 | 40 | 20 | 10 | 0 | 0 | 70 | 27 | 0.0 | 32.7 | 11.7 | 0.0 | 44.4 | 31 |
| 798 | A | 59.4 | 36.9 | 4 | 5 | 5 | N | 5 | 0 | 5 | 10 | 0 | 0 | 15 | 686 | 0.0 | 22.1 | 22.1 | 0.0 | 44.2 | 32 |
| 4994 | A | 25 | 18.9 | 5 | 5 | 4 | N | 4 | 40 | 15 | 0 | 0 | 0 | 55 | 78 | 0.0 | 36.2 | 8.0 | 0.0 | 44.2 | 33 |
| 885 | D | 10 | 7.5 | 5 | 4 | 4 | N | 6 | 40 | 25 | 10 | 0 | 0 | 75 | 25 | 0.0 | 32.7 | 10.9 | 0.0 | 43.5 | 34 |
| 6473 | A | 48 | 36 | 5 | 4 | 4 | N | 6 | 0 | 25 | 0.4 | 0 | 0 | 25.4 | 536 | 0.0 | 34.2 | 8.6 | 0.0 | 42.9 | 35 |
| 3202 | P | 40.7 | 24.4 | 5 | 4 | 6 | N | N | 40 | 10 | 8.4 | 0 | 30 | 88.4 | 16 | 10.0 | 22.1 | 10.0 | 0.0 | 42.1 | 36 |
| 3817 | A | 10 | 7 | 5 | 5 | 4 | N | 5 | 40 | 15 | 10 | 0 | 0 | 65 | 44 | 0.0 | 23.4 | 18.5 | 0.0 | 41.9 | 37 |
| 3818 | A | 10 | 7 | 5 | 5 | 4 | N | 6 | 40 | 15 | 10 | 0 | 0 | 65 | 45 | 0.0 | 23.4 | 18.5 | 0.0 | 41.9 | 38 |
| 2627 | D | 10 | 7.5 | 5 | 5 | 4 | N | 4 | 40 | 15 | 10 | 0 | 0 | 65 | 42 | 0.0 | 30.9 | 10.3 | 0.0 | 41.2 | 39 |
| 617 | D | 10 | 7.5 | N | N | N | 4 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 1446 | 0.0 | 21.9 | 19.2 | 0.0 | 41.1 | 40 |
| 1268 | A | 49.9 | 29.9 | 5 | 5 | 4 | N | 5 | 23.8 | 15 | 10 | 0 | 0 | 48.8 | 144 | 0.0 | 23.0 | 18.1 | 0.0 | 41.1 | 41 |
| 3130 | A | 10 | 7 | 4 | 4 | 5 | N | 6 | 40 | 15 | 8.3 | 0 | 0 | 63.3 | 51 | 0.0 | 30.0 | 10.0 | 0.0 | 40.0 | 42 |
| 2844 | P | 27.2 | 16.1 | 6 | 7 | 6 | N | 5 | 40 | 0 | 0 | 0 | 40 | 80 | 20 | 31.7 | 0.0 | 8.2 | 0.0 | 39.8 | 43 |
| 2550 | D | 13 | 10 | 5 | 4 | 5 | N | 7 | 40 | 10 | 9.3 | 0 | 0 | 59.3 | 66 | 0.0 | 27.3 | 12.4 | 0.0 | 39.7 | 44 |
| 1739 | k | 10 | 7 | 5 | 5 | 4 | N | 5 | 40 | 15 | 10 | 0 | 0 | 65 | 37 | 0.0 | 25.6 | 14.1 | 0.0 | 39.7 | 45 |
| 1917 | A | 10 | 7 | 5 | 5 | 4 | N | 5 | 40 | 15 | 10 | 0 | 0 | 65 | 38 | 0.0 | 25.5 | 14.0 | 0.0 | 39.5 | 46 |
| 1918 | к |  | 0 | 5 | 5 | 4 | N | 6 | 40 | 15 | 10 | 0 | 0 | 65 | 39 | 0.0 | 25.5 | 14.0 | 0.0 | 39.5 | 47 |
| 10493 | A | 47.9 | 36 | 6 | 4 | 6 | N | N | 0 | 10 | 0 | 0 | 0 | 10 | 937 | 0.0 | 22.1 | 5.5 | 11.8 | 39.3 | 48 |
| 18614 | k |  | 0 | 5 | 6 | 2 | N | 7 | 0 | 0 | 0 |  |  | 0 | 2882 | 0.0 | 30.0 | 9.3 | 0.0 | 39.3 | 49 |
| 1897 | A | 46.9 | 29.9 | 6 | 5 | 4 | N | 5 | 31.8 | 15 | 10 | 0 | 0 | 56.8 | 69 | 0.0 | 26.1 | 13.0 | 0.0 | 39.1 | 50 |

Table 3-4. Deficiency Points: 1991 Algorithm vs. New Algorithm Bridges Ranked 51-100

| ¢ |  | $\stackrel{00}{\ldots}$ $\stackrel{0}{0}$ $\stackrel{1}{c}$ 0 0 |  |  |  |  |  |  |  |  |  |  |  | 1991_Algo_Total_Defic_Pts |  |  |  |  |  |  | $\underset{\underset{\sim}{\check{c}}}{\stackrel{\check{c}}{\stackrel{1}{2}}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1898 | A | 52.9 | 36 | 6 | 6 | 4 | N | 5 | 0 | 15 | 10 | 0 | 0 | 25 | 539 | 0.0 | 26.1 | 13.0 | 0.0 | 39.1 | 51 |
| 1664 | D | 10 | 7.5 | 5 | 4 | 6 | N | N | 40 | 10 | 10 | 0 | 0 | 60 | 59 | 0.0 | 25.5 | 12.7 | 0.0 | 38.2 | 52 |
| 1613 | D | 10 | 7 | 5 | 4 | 5 | N | 6 | 40 | 10 | 10 | 0 | 0 | 60 | 58 | 0.0 | 25.5 | 12.7 | 0.0 | 38.2 | 53 |
| 1911 | A | 65.9 | 43.9 | 5 | 5 | 5 | N | 4 | 0 | 0 | 10 | 0 | 0 | 10 | 831 | 0.0 | 24.7 | 13.3 | 0.0 | 38.0 | 54 |
| 8648 | D | 24 | 18 | 6 | 4 | 6 | N | 7 | 40 | 10 | 10 | 0 | 0 | 60 | 64 | 0.0 | 22.9 | 15.1 | 0.0 | 38.0 | 55 |
| 7627 | D | 48 | 36 | 4 | 5 | 6 | N | 6 | 0 | 5 | 0.4 | 0 | 0 | 5.4 | 1103 | 0.0 | 27.4 | 10.4 | 0.0 | 37.8 | 56 |
| 5222 | D | 45.5 | 27.3 | 6 | 4 | 5 | N | 7 | 39.4 | 10 | 10 | 0 | 0 | 59.4 | 65 | 0.0 | 25.2 | 12.6 | 0.0 | 37.8 | 57 |
| 2013 | D | 97.8 | 97.8 | 5 | 5 | 4 | N | 5 | 0 | 15 | 10 | 0 | 0 | 25 | 540 | 0.0 | 25.1 | 12.5 | 0.0 | 37.6 | 58 |
| 1442 | D | 10 | 7.5 | 5 | 5 | 4 | N | 5 | 40 | 15 | 10 | 0 | 0 | 65 | 36 | 0.0 | 25.1 | 12.5 | 0.0 | 37.6 | 59 |
| 2320 | D | 61.8 | 40.9 | 5 | 6 | 4 | N | 5 | 0 | 15 | 10 | 0 | 0 | 25 | 542 | 0.0 | 25.1 | 12.5 | 0.0 | 37.6 | 60 |
| 5430 | D | 24 | 18 | 5 | 4 | 5 | N | 5 | 40 | 10 | 10 | 0 | 0 | 60 | 63 | 0.0 | 22.9 | 14.5 | 0.0 | 37.4 | 61 |
| 2408 | D | 10 | 7.5 | 5 | 4 | 5 | N | 8 | 40 | 10 | 10 | 0 | 0 | 60 | 62 | 0.0 | 24.8 | 12.4 | 0.0 | 37.2 | 62 |
| 5977 | D | 3 | 2 | 5 | 5 | 4 | N | 6 | 40 | 15 | 10 | 0 | 0 | 65 | 46 | 0.0 | 23.9 | 13.2 | 0.0 | 37.1 | 63 |
| 3016 | A | 49 | 27.9 | 6 | 5 | 4 | N | 5 | 40 | 15 | 8 | 0 | 0 | 63 | 52 | 0.0 | 25.8 | 11.4 | 0.0 | 37.1 | 64 |
| 2910 | A | 55.9 | 38 | 5 | 4 | 5 | N | 6 | 0 | 10 | 0.4 | 0 | 0 | 10.4 | 759 | 0.0 | 25.5 | 11.6 | 0.0 | 37.1 | 65 |
| 2866 | D | 3 | 2 | 4 | 5 | 5 | N | 7 | 40 | 5 | 9.2 | 0 | 0 | 54.2 | 85 | 0.0 | 25.5 | 11.5 | 0.0 | 36.9 | 66 |
| 476 | A | 10 | 7.5 | 5 | 4 | 6 | N | 5 | 40 | 10 | 10 | 0 | 0 | 60 | 55 | 0.0 | 23.2 | 13.7 | 0.0 | 36.9 | 67 |
| 2588 | A | 19.9 | 15 | 6 | 5 | 5 | N | 4 | 40 | 0 | 10 | 0 | 0 | 50 | 109 | 0.0 | 24.5 | 12.3 | 0.0 | 36.8 | 68 |
| 2273 | A | 33.9 | 25 | 6 | 5 | 6 | N | 7 | 40 | 0 | 10 | 0 | 0 | 50 | 106 | 0.0 | 0.0 | 21.8 | 14.9 | 36.7 | 69 |
| 4797 | к |  | 0 | 5 | 6 | 4 | N | 7 | 40 | 15 | 1.2 | 0 | 0 | 56.2 | 70 | 0.0 | 26.0 | 10.6 | 0.0 | 36.6 | 70 |
| 6434 | D | 37.7 | 22.6 | 5 | 4 | 5 | N | 6 | 40 | 10 | 1.2 | 0 | 0 | 51.2 | 88 | 0.0 | 25.9 | 10.6 | 0.0 | 36.5 | 71 |
| 1717 | A | 64.9 | 43.9 | 5 | 5 | 4 | N | 5 | 0 | 15 | 10 | 0 | 0 | 25 | 537 | 0.0 | 23.4 | 12.9 | 0.0 | 36.3 | 72 |
| 2253 | A | 61.8 | 41.9 | 7 | 7 | 4 | N | 6 | 0 | 15 | 10 | 0 | 0 | 25 | 541 | 0.0 | 24.2 | 12.1 | 0.0 | 36.3 | 73 |
| 486 | A | 63.9 | 40.9 | 6 | 7 | 6 | N | 4 | 0 | 0 | 10 | 0 | 0 | 10 | 790 | 0.0 | 22.8 | 13.4 | 0.0 | 36.2 | 74 |
| 4202 | A | 17 | 11 | 4 | 5 | 5 | N | 6 | 40 | 5 | 0.4 | 0 | 0 | 45.4 | 193 | 0.0 | 25.8 | 10.4 | 0.0 | 36.2 | 75 |
| 3033 | A | 54.9 | 33.9 | 5 | 4 | 5 | N | 6 | 12.4 | 10 | 9.6 | 0 | 0 | 31.9 | 445 | 0.0 | 24.8 | 11.4 | 0.0 | 36.2 | 76 |
| 2566 | A | 10 | 7 | 5 | 6 | 4 | N | 5 | 40 | 15 | 10 | 0 | 0 | 65 | 40 | 0.0 | 23.3 | 12.8 | 0.0 | 36.0 | 77 |
| 2567 | A | 10 | 7 | 5 | 5 | 4 | N | 5 | 40 | 15 | 10 | 0 | 0 | 65 | 41 | 0.0 | 23.3 | 12.8 | 0.0 | 36.0 | 78 |
| 8466 | A | 49.9 | 29.9 | 6 | 4 | 7 | N | 7 | 0 | 10 | 7 | 0 | 0 | 17 | 656 | 0.0 | 24.0 | 12.0 | 0.0 | 36.0 | 79 |
| 14407 | D | 24 | 18 | 5 | 4 | 6 | N | N | 40 | 10 | 0 | 0 | 0 | 50 | 130 | 0.0 | 23.9 | 0.0 | 11.9 | 35.8 | 80 |
| 8467 | A | 49.9 | 29.9 | 6 | 4 | 7 | N | 6 | 0 | 10 | 6.8 | 0 | 0 | 16.8 | 660 | 0.0 | 23.8 | 11.9 | 0.0 | 35.7 | 81 |
| 2913 | A | 45.5 | 27.3 | 6 | 4 | 6 | N | 6 | 37.4 | 10 | 7.3 | 0 | 0 | 54.6 | 84 | 0.0 | 24.7 | 10.9 | 0.0 | 35.6 | 82 |
| 1273 | D | 10 | 7 | 5 | 6 | 4 | N | 6 | 40 | 15 | 10 | 0 | 0 | 65 | 32 | 0.0 | 23.7 | 11.8 | 0.0 | 35.5 | 83 |
| 1274 | D | 10 | 7 | 5 | 5 | 4 | N | 6 | 40 | 15 | 10 | 0 | 0 | 65 | 33 | 0.0 | 23.7 | 11.8 | 0.0 | 35.5 | 84 |
| 1276 | D | 10 | 7 | 5 | 5 | 4 | N | 7 | 40 | 15 | 10 | 0 | 0 | 65 | 35 | 0.0 | 23.7 | 11.8 | 0.0 | 35.5 | 85 |
| 10083 | P | 38.9 | 27 | 7 | 6 | 5 | N | 4 | 0 | 0 | 1.5 | 0 | 0 | 1.5 | 1182 | 0.0 | 20.0 | 15.5 | 0.0 | 35.5 | 86 |
| 1695 | D | 56.9 | 40.9 | 5 | 5 | 5 | N | 4 | 0 | 0 | 10 | 0 | 0 | 10 | 815 | 0.0 | 23.6 | 11.8 | 0.0 | 35.4 | 87 |
| 7029 | D | 24 | 18 | 5 | 4 | 5 | N | 7 | 40 | 10 | 0 | 0 | 0 | 50 | 123 | 0.0 | 25.2 | 10.1 | 0.0 | 35.3 | 88 |
| 8060 | D | 10 | 7.5 | 5 | 5 | 4 | N | 5 | 40 | 15 | 10 | 0 | 0 | 65 | 47 | 0.0 | 20.1 | 15.1 | 0.0 | 35.2 | 89 |
| 1277 | A | 10 | 7 | 5 | 4 | 5 | N | 6 | 40 | 10 | 10 | 0 | 0 | 60 | 56 | 0.0 | 23.4 | 11.7 | 0.0 | 35.2 | 90 |
| 10033 | A | 47.9 | 36 | 7 | 7 | 7 | N | N | 0 | 0 | 10 | 0 | 0 | 10 | 931 | 0.0 | 0.0 | 23.6 | 11.3 | 34.9 | 91 |
| 10034 | A | 47.9 | 36 | 7 | 7 | 7 | N | N | 0 | 0 | 10 | 0 | 0 | 10 | 932 | 0.0 | 0.0 | 23.6 | 11.3 | 34.9 | 92 |
| 6034 | A | 40.9 | 25 | 6 | 4 | 7 | N | 7 | 40 | 10 | 1.1 | 0 | 0 | 51.1 | 89 | 0.0 | 24.8 | 10.1 | 0.0 | 34.9 | 93 |
| 4274 | A | 48 | 36 | 6 | 6 | 7 | N | 4 | 0 | 0 | 1.1 | 0 | 0 | 1.1 | 1191 | 0.0 | 24.7 | 10.1 | 0.0 | 34.8 | 94 |
| 4677 | A | 56.9 | 33.9 | 5 | 5 | 5 | N | 4 | 12 | 0 | 0.4 | 0 | 0 | 12.4 | 721 | 0.0 | 24.8 | 10.0 | 0.0 | 34.8 | 95 |
| 2695 | A | 53.9 | 35 | N | N | N | N | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 1477 | 0.0 | 22.9 | 11.5 | 0.0 | 34.4 | 96 |
| 2108 | D | 10 | 7 | 5 | 4 | 5 | N | 6 | 40 | 10 | 10 | 0 | 0 | 60 | 61 | 0.0 | 22.9 | 11.5 | 0.0 | 34.4 | 97 |
| 8134 | A | 63.7 | 38.3 | 5 | 4 | 6 | N | N | 0 | 10 | 0 | 0 | 0 | 10 | 918 | 0.0 | 23.6 | 8.8 | 1.9 | 34.4 | 98 |
| 7766 | A | 52.3 | 31.4 | 5 | 6 | 5 | N | 4 | 20.8 | 0 | 0.4 | 0 | 0 | 21.2 | 582 | 0.0 | 24.5 | 9.9 | 0.0 | 34.3 | 99 |
| 843 | A | 69.9 | 49 | 5 | 5 | 4 | N | 6 | 0 | 15 | 7.1 | 0 | 0 | 22.1 | 566 | 0.0 | 22.9 | 11.4 | 0.0 | 34.3 | 100 |

### 4.0 Algorithm Development

The new deficiency algorithm was developed using Excel spreadsheets to facilitate displaying results. The decision tree, flow chart, and source code for the algorithm are presented in Appendices A, B, and C, respectively. In this section, the procedures used to analyze the deficiency algorithm results and determine the optimum deficiency criteria and weight factors are described. Besides documenting the current deficiency algorithm, description of these procedures may be helpful when developing deficiency algorithms for other bridge populations.

In the first section below, the use of a graphical interface is described that enabled quick adjustment of the deficiency criteria and weight factors and provided a global view of the impact on the bridge population. The next section describes spot checking the accuracy of the calculations and reviewing the results for reasonableness using a detailed list of deficient bridges. And finally, a sensitivity analysis of the weight factors is presented that was used to determine the range of values that best differentiated each type of deficiency without overshadowing other deficiencies.

## Graphical Interface

The graphical interface has two pages: an input screen and an output screen.

- Input Screen A ranked list of deficient bridges for a particular population of bridges (Figure 4-1) was calculated by
- Selecting the bridge "owner" and "region"
- Clicking the "Filter Data" button
- Typing in the deficiency criteria (shaded in yellow) for each of the four types of deficiencies. For each deficiency, a minimum, intermediate, and desirable criteria value was specified. (See Figure 4-2.)
- Typing in the deficiency points (shaded in orange) for each minimum and intermediate deficiency criteria. The desirable criteria were automatically assigned zero deficiency points.
- Typing in an "X" under ADT, ADTT, and Detour Length Factors opposite each applicable criteria
- Typing in the ADT and Detour Length Factors
- Checking or unchecking the check-boxes at the bottom regarding closed bridges and ADT/DL factors

bridges selected

| Load-Rating | Rating Factor ---- |  |  | ADT <br> Factor | Truck ADT Factor | Detour Length Factor |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | < | = | > |  |  |  |
|  | 1 | 1 | 1 |  |  |  |
| SCHOOL_BUS | 30 | 0 | 0 |  |  | x |
| H_Truck | 0 | 0 | 0 |  |  |  |
| 2_AXLE_TRUCK | 20 | 0 | 0 |  | x | x |
| CONCRETE_Truck | 0 | 0 | 0 |  |  | x |
| HS_Truck | 0 | 0 | 0 |  |  |  |
| TRIAXLE_DUMP_Truck | 10 | 0 | 0 |  |  | x |
| 18_WHEELER | 20 | 0 | 0 |  | x | x |
| 6_AXLE_Truck | 5 | 0 | 0 |  |  | x |
| Max_Total | 40 | x ADT | x DL Factor |  |  |  |
| - or - ${ }^{\text {a }}$ |  |  |  |  |  |  |
|  | < | = | >= |  |  |  |
| Operating Rating (tons) | 12.5 | 30 | 36 |  |  |  |
| Defic Points: | 40 | 20 | 0 |  | x | x |
| Condition Ratings | <= | = | = |  |  |  |
|  | 3 | 4 | 5 |  |  |  |
| Lowest Condition Rating | 30 | 20 | 0 | x |  | x |
| 2nd Lowest Condition Rating | 20 | 10 | 0 | x |  | x |
| 3rd Lowest Condition Rating | 10 | 5 | 0 | x |  | x |

Bridge Width

|  | $<=$ | $=$ | $>=$ |
| ---: | :---: | :---: | :---: |
| Lane Width (ft): | 10 | 12 | 12 |
| Shoulder Width (ft) | 0 | 0 | 10 |
| Defic Points: | 20 | 10 | 0 |

Vertical Clearance

|  | $<$ | $=$ | $>=$ |
| ---: | :---: | :---: | :---: |
| Height (ft): | 16 | 16.3 | 17 |
| Defic Points: | 10 | 8 | 0 |


ADT Factor: +/- 30\%
Detour Length Factor: +/- 10\%
Set closed bridges (Posting Status $=$ "K") to max. defic. FALSE $\quad \square$ Set factor for ADT \& DL to be a min. of 1 TRUE $\quad \checkmark$

Figure 4-1. Graphical interface screen one: Deficiency criteria and weights.

- Output Screen The distribution of deficient bridges was displayed by
o Clicking the "Calc Defic's" button and waiting 10 to 20 seconds for the algorithm to execute

The order of replacement (e.g. load deficient bridges replaced before vertical clearance deficient bridges) was displayed by

- Moving the slider to the top so that "number of bridges to replace" $=0$
- Clicking in the middle of the slider to display the distribution of replaced bridges, 10 at a time


## Detailed Bridge List

Detailed information about each bridge was shown on another sheet of the spreadsheet (Figure 43). All of the fields are shown in Figure 4-3; however, many fields can be collapsed on the actual spreadsheet to so that all information fits on one screen. All of the fields from the bridge database used to calculate deficiency are displayed. In addition, information derived from the database such as load rating factors, percent rank ADT, minimum condition, and whether the bridge is "underwidth" (less than the desirable bridge width criteria) is also displayed.

The points for each deficiency (load, condition, width, and vertical clearance), total deficiency and deficiency rank are shown on the right-hand side of this sheet (Figure 4-3). On the extreme right-hand side of the sheet the individual bridge deficiencies are indicated in color-coded columns.


Figure 4-2. Graphical interface screen two: Distribution of deficient and "replaced" bridges.

|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 言 | $$ |  | 2 | $\begin{aligned} & \text { त्र } \\ & \text { 亏訁 } \\ & \hline \end{aligned}$ |  |  | $\begin{aligned} & \overleftarrow{O}_{1}^{\prime} \\ & \stackrel{\rightharpoonup}{1} \\ & \stackrel{\rightharpoonup}{\circ} \\ & \hline \end{aligned}$ |  |  |  |  | $\begin{aligned} & \stackrel{\rightharpoonup}{\omega} \\ & \stackrel{1}{\omega} \\ & \stackrel{\rightharpoonup}{\infty} \\ & \hline \end{aligned}$ |  |  | $\begin{aligned} & \stackrel{0}{2} \\ & \stackrel{y}{2} \\ & \stackrel{c}{0} \\ & \stackrel{0}{0} \\ & \hline \end{aligned}$ |  |
| 1841 | 0 | State | 1 | Etowah Co | Hwy | AL 179 | SR 00179 | AL 179 \＆WADE CREEK | Water | WADE CREEK |  | 1938 | Other or 1 | StI | Stringer | 24.9 |
| 529 | 0 | State | 7 | Houston Co | Hwy | SR 52 MP 65 | SR 00052 | ． 8 MI．EAST U．S． 84 | RR | C．S．X．RAILROAD |  | 1928 | H 15 | Conc | T Beam | 2 |
| 635 | 0 | State | 5 | Chilton Co | Hwy | SR 22 | SR 00022 | 2．9 MI E JCT SR 191 | Water | benson Creek |  | 1929 | H 10 | Timber | Stringer | 6 |
| 2736 | 0 | State | 6 | Autauga Co | Hwy | AL 206 | SR 00206 | IN PRATTVILLE | Water | AUTAUGA CREEK |  | 1942 | H 15 | Conc | T Beam | 7 |
| 1842 | 0 | State | 1 | Etowah Co | Hwy | AL 179 | SR 00179 | 6．3 MI N JCT US 278 | Water | BRANCH |  | 1938 | Other or I | StI | Stringer | 29.9 |
| 504 | 0 | State | 5 | Chilton Co | Hwy | SR 22 | SR 00022 | 0．4 MI E JCT SR 191 | Water | MIDDLE MULBERRY CREEK |  | 1928 | H 10 | Timber | Stringer | 6.3 |
| 7608 | 0 | State | 4 | Calhoun Co | Hwy | SUMMERALI | CO 00000 | 0．2 MI W JCT SR 21 | Hwy | US 431 | US 004： | 1962 | HS 20 | Conc | T Beam | 13.7 |
| 2037 | 0 | State | 1 | Etowah Co | Hwy | AL 77 | SR 00077 | AL 77 \＆HORTON CREEK | Water | Horton Creek |  | 1939 | H 15 | StI | Stringer | 26.4 |
| 1765 | 0 | State | 5 | Chilton Co | Hwy | SR 22 | SR 00022 | 0．5 MI E JCT SR 191 | Relief | MULBERRY CREEK RELIEF |  | 1938 | H 10 | Timber | Stringer | 8.5 |
| 4507 | 0 | State | 1 | Etowah Co | Hwy | US 278 | US 00278 | US 278 ＠WALNUT GROVE | Water | BLACK WARRIOR RELIEF |  | 1935 | H 15 | StI | Stringer | 4 |
| 19818 | 0 | State | 6 | Montgomery Co | Hwy | AL0601（OLC | SR 00601 | 1．4MI N．OF JACKSON ST． | RR | CSX RAIL ROAD |  | 1937 | Other or 1 | Conc | Stringer | 28.8 |
| 503 | 0 | State | 2 | Lawrence Co | Hwy | SR 20 | SR 00020 | 9．6 MI E JCT SR 33 | Water | FOX CREEK |  | 1928 | H 15 | Conc | T Beam | 17 |
| 1394 | 0 | State | 3 | Jefferson Co | Hwy－Pec | US 78 | SR 00005 | US 78 \＆VILLAGE CREEK | RR－Water | VILLAGE CK \＆FRISCO RR |  | 1936 | H 20 | StI | Stringer | 2 |
| 1798 | 0 | State | 1 | Cherokee Co | Hwy | AL 68 | SR 00068 | AL 68 \＆MILL CREEK | Water | MILL CREEK |  | 1938 | H 15 | StI Cont | Stringer | 11 |
| 784 | 0 | State | 1 | Jackson Co | Hwy | SR 35 | SR 00035 | 0．5 MI N JCT SR40 \＆SR35 | Water | TENNESSEE RIVER |  | 1930 | H 15 | StI | Truss－Thru | 7.6 |
| 474 | 0 | State | 3 | St．Clair Co | Hwy | US 78 | US 00078 | ． 2 MI E．COOK SPRINGS RD | Water | CANE CREEK |  | 1928 | H 15 | Conc | T Beam | 18.7 |
| 615 | 0 | State | 4 | Chambers Co | Hwy | US 29 | US 00029 | 4 MI N JCT CO 70 | Water | OSANIPPA CREEK |  | 1929 | H 15 | Conc | T Beam | 6.9 |
| 2712 | 0 | State | 3 | Walker Co | Hwy | AL 69 | SR 00069 | AL 69 \＆WARRIOR RIVER | Water | SIPSEY FORK WARIOR RIVER |  | 1942 | H 15 | StI Cont | Stringer | 4 |
| 6588 | 0 | State | 2 | Lawrence Co | Hwy | SR 20 | SR 00020 | 9．6 MI E JCT SR 33 | Water | FOX CREEK |  | 1959 | HS 20 | Conc | T Beam | 15 |
| 10132 | 0 | State | 3 | Blount Co | Hwy | AL 75 | SR 00075 | ． 8 MI．NO CO RD 39 | Water | CHAMPION CREEK |  | 1929 | H 15 | Conc | T Beam | 3 |
| 10102 | 0 | State | 9 | Baldwin Co | Hwy | SR 182 | SR 00182 | 1 MI W SR 59 | Water | LITTLE LAGOON PASS |  | 1969 | HS 20 | Conc | Stringer | 20.9 |
| 7365 | 0 | State | 2 | Lawrence Co | Hwy | SR 20 | SR 00020 | 4．7 MI E JCT SR 33 | Water | MALLARD CREEK |  | 1961 | HS 20 | Conc | T Beam | 15 |
| 9367 | 0 | State | 4 | Talledega Co | Hwy | US 280 | US 00280 | TOWN OF CHILDERSBURG | RR | SOUTHERN RAILROAD |  | 1935 | H 15 | Conc | T Beam | 15 |
| 5816 | 0 | State | 5 | Tuscaloosa Co | Hwy | US 82 | US 00082 | 4．9 MI E TUSC CO LINE | Water | SIPSEY RIVER |  | 1957 | HS 20 | StI Cont | Stringer | 6 |
| 12793 | 0 | State | 9 | Baldwin Co | Hwy | US 98 | US 00098 | 254＇S COUNTY ROAD 24 | Water | TURKEY BRANCH |  | 1982 | HS 20 | Conc | Stringer | 47.5 |
| 502 | 0 | State | 2 | Lawrence Co | Hwy | SR 20 | SR 00020 | 4．7 MI E JCT SR 33 | Water | MALLARD CREEK |  | 1928 | H 15 | Conc | T Beam | 45.1 |
| 770 | 0 | State | 3 | Shelby Co | Hwy | AL 25 | SR 00025 | AL 25 AT VINCENT SCHOOL | RR | ACLC LINE RAILROAD |  | 1930 | H 15 | Conc | T Beam | 63.4 |
| 1665 | 0 | State | 3 | Jefferson Co | Hwy | AL 269 | SR 00269 | ． 1 MI．SO．POWHATAN RD | Water | SHORT CREEK |  | 1937 | H 15 | StI | Stringer | 2 |
| 4658 | 0 | State | 3 | Blount Co | Hwy | AL 79 | SR 00079 | ． 3 MI．NO．LOUUST FK CL | Water | BLACKBURN FK WARR RV |  | 1953 | H 15 | StI Cont | Stringer | 44.6 |
| 1072 | 0 | State | 3 | St．Clair Co | Hwy | US 11 | US 00011 | 3.5 MI ．NO．US 231 | Water | GULF CREEK |  | 1934 | H 15 | StI Cont | Stringer | 52.3 |
| 1368 | 0 | State | 2 | Lauderdale Co | Hwy | US 72 | US 00072 | 2．4 KM W JCT SR 101 | Water | BLUEWATER CREEK |  | 1924 | H 15 | StI | Stringer | 40.4 |

Figure 4－3．Detailed list of deficient bridges．

|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ¢ | $\begin{aligned} & \delta_{1} \\ & \stackrel{\rightharpoonup}{4} \end{aligned}$ |  |  |  |  |  |  | $\begin{aligned} & \stackrel{\infty}{c} \\ & \stackrel{0}{c} \\ & \stackrel{\rightharpoonup}{c} \\ & \stackrel{1}{0} \\ & \hline \end{aligned}$ | $\begin{aligned} & \stackrel{y}{\grave{y}} \\ & \vdots \\ & \vdots \\ & I_{1} \\ & \hline \end{aligned}$ |  |  |  |  | $\begin{aligned} & \text { u } \\ & \underset{<}{4} \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { n } \\ & 0 \\ & \mathbf{o}^{1} \\ & \text { 모 } \\ & \hline \end{aligned}$ |  |  |  |  |  | $\begin{aligned} & \delta_{1} \\ & \frac{1}{4} \\ & \vdots \\ & \hline \end{aligned}$ |  |  |  |  |  |  |  | RF_TRIAXLE_DUMP_Truck_Ratins |  |  |  |
| 1841 | 1910 | 5 | 6 |  |  |  | P | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 5 | N | 5 | 29.3 | 2 | 2-way | 99.99 | 0 | 0.08 | 0.15 | 0.1017 | 0.08 | 0.0909 | 0.075 | 0.0714 |
| 529 | 5360 | 4 | 3 |  |  |  | P | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 4 | 5 | 4 | N | N | 20 | 2 | 2-way | 99.99 | 22.24 | 0.42 | 0.75 | 0.5085 | 0.4 | 0.4545 | 0.375 | 0.3571 |
| 635 | 3500 | 19 | 57 |  |  |  | P | 3 | 15 | 21 | 20 | 18 | 32 | 32 | 18 | 5 | 5 | 3 | N | 7 | 27.7 | 2 | 2-way | 99.99 | 0 | 0.08 | 0.745 | 0.6949 | 0.5333 | 0.5576 | 0.795 | 0.7571 |
| 2736 | 6510 | 6 | 6 |  |  |  | P | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 6 | 5 | 2 | N | 5 | 25.9 | 2 | 2-way | 99.99 | 0 | 0.42 | 0.75 | 0.5085 | 0.4 | 0.4545 | 0.375 | 0.3571 |
| 1842 | 2380 | 5 | 6 |  |  |  | P | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 4 | 7 | 5 | N | 4 | 31.2 | 2 | 2-way | 99.99 | 0 | 0.17 | 0.3 | 0.2034 | 0.16 | 0.1818 | 0.15 | 0.1429 |
| 504 | 2510 | 19 | 57 |  |  |  | P | 6.1 | 15 | 21 | 20 | 18 | 32 | 32 | 18 | 5 | 5 | 4 | N | 7 | 27.7 | 2 | 2-way | 99.99 | 0 | 0.17 | 0.745 | 0.6949 | 0.5333 | 0.5576 | 0.795 | 0.7571 |
| 7608 | 7300 | 5 | 1 | 19580 | 8 | 1 | P | 13 | 13 | 13 | 13 | 13 | 13 | 13 | 13 | 7 | 7 | 4 | N | N | 27.9 | 2 | 2-way | 99.99 | 18.99 | 0.36 | 0.65 | 0.4407 | 0.3467 | 0.3939 | 0.325 | 0.3095 |
| 2037 | 15190 | 9 | 3 |  |  |  | P | 6.9 | 3.8 | 3.4 | 5.1 | 5.1 | 8.7 | 7.9 | 4.5 | 6 | 4 | 5 | N | 7 | 35.1 | 2 | 2-way | 99.99 | 0 | 0.19 | 0.19 | 0.1153 | 0.136 | 0.1545 | 0.2175 | 0.1881 |
| 1765 | 2510 | 19 | 57 |  |  |  | P | 6.1 | 23 | 35 | 32 | 32 | 40 | 41 | 30 | 5 | 7 | 4 | N | 7 | 27.8 | 2 | 2-way | 99.99 | 0 | 0.17 | 1.17 | 1.1932 | 0.8507 | 0.9545 | 0.995 | 0.969 |
| 4507 | 5880 | 25 | 19 |  |  |  | D | 15 | 33 | 42 | 48 | 42 | 66 | 69 | 45 | 4 | 3 | 4 | N | 7 | 24 | 2 | 2-way | 99.99 | 0 | 0.42 | 1.63 | 1.4339 | 1.2693 | 1.2636 | 1.655 | 1.6357 |
| 19818 | 50 | 0 | 199 |  |  |  | D | 40 | 25 | 37 | 40 | 36 | 51 | 53 | 29 | 3 | 3 | 3 | N | N | 23.9 | 2 | 2-way | 99.99 | 22 | 1.1 | 1.24 | 1.2678 | 1.056 | 1.0788 | 1.2725 | 1.25 |
| 503 | 7005 | 15 | 0 |  |  |  | D | 3 | 30 | 43 | 37 | 38 | 62 | 57 | 35 | 4 | 3 | 6 | N | 7 | 20 | 2 | 1-way | 99.99 | 0 | 0.08 | 1.495 | 1.461 | 0.9947 | 1.1424 | 1.55 | 1.3619 |
| 1394 | 37460 | 7 | 3 |  |  |  | D |  | 40 | 52 | 47 | 47 | 78 | 76 | 50 | 3 | 5 | 6 | N | 5 | 40 | 4 | 2-way | 99.99 | 22 |  | 2.02 | 1.7458 | 1.2533 | 1.4121 | 1.9425 | 1.8024 |
| 1798 | 1510 | 11 | 6 |  |  |  | D | 10 |  |  |  |  |  |  |  | 4 | 5 | 4 | N | 3 | 24 | 2 | 2-way | 99.99 | 0 | 0.28 |  |  |  |  |  |  |
| 784 | 7750 | 8 | 1 |  |  |  | E | 10 |  |  |  |  |  |  |  | 5 | 4 | 5 | N | 6 | 19.7 | 2 | 1-way | 14.1 | 0 | 0.28 |  |  |  |  |  |  |
| 474 | 1150 | 5 | 3 |  |  |  | D | 10 | 10 | 10 | 10 | 10 | 10 | 10 |  | 6 | 6 | 4 | N | 4 | 20 | 2 | 2-way | 99.99 | 0 | 0.28 | 0.5 | 0.339 | 0.2667 | 0.303 | 0.25 | 0.2381 |
| 615 | 7940 | 3 | 8 |  |  |  | D | 10 |  |  |  |  |  |  |  | 4 | 6 | 5 | N | 5 | 20 | 2 | 2-way | 99.99 | 0 | 0.28 |  |  |  |  |  |  |
| 2712 | 3530 | 22 | 14 |  |  |  | A | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 4 | 6 | 4 | N | 5 | 24 | 2 | 2-way | 99.99 | 0 | 0.17 | 0.3 | 0.2034 | 0.16 | 0.1818 | 0.15 | 0.1429 |
| 6588 | 7005 | 15 | 18 |  |  |  | A | 24 | 41 | 48 | 53 | 48 | 79 | 76 | 50 | 4 | 4 | 6 | N | 7 | 27.9 | 2 | 1-way | 99.99 | 0 | 0.67 | 2.03 | 1.6271 | 1.4213 | 1.4455 | 1.97 | 1.8119 |
| 10132 | 7590 | 9 | 3 |  |  |  | D | 10 |  |  |  |  |  |  |  | 5 | 4 | 4 | N | 4 | 29.9 | 2 | 2-way | 99.99 | 0 | 0.28 |  |  |  |  |  |  |
| 10102 | 4350 | 2 | 98 |  |  |  | A | 36 | 20 | 37 | 42 | 44 | 67 | 61 | 38 | 4 | 4 | 5 | N | 5 | 28 | 2 | 2-way | 99.99 | 0 | 1 | 0.995 | 1.2644 | 1.1253 | 1.3424 | 1.6825 | 1.4571 |
| 7365 | 6530 | 17 | 18 |  |  |  | A | 24 | 38 | 46 | 52 | 46 | 75 | 71 | 44 | 4 | 4 | 6 | N | 7 | 27.9 | 2 | 1-way | 99.99 | 0 | 0.67 | 1.885 | 1.5559 | 1.384 | 1.4061 | 1.875 | 1.6786 |
| 9367 | 26390 | 12 | 1 |  |  |  | D | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 4 | 4 | 4 | N | N | 67.9 | 5 | 2-way | 99.99 | 21.58 | 0.28 | 0.5 | 0.339 | 0.2667 | 0.303 | 0.25 | 0.2381 |
| 5816 | 12990 | 16 | 6 |  |  |  | D | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 4 | 4 | 7 | N | 6 | 27.8 | 2 | 2-way | 99.99 | 0 | 0.28 | 0.5 | 0.339 | 0.2667 | 0.303 | 0.25 | 0.2381 |
| 12793 | 10680 | 4 | 4 |  |  |  | A | 48 |  |  |  |  |  |  |  | 7 | 7 | 4 | N | 4 | 27.6 | 2 | 2-way | 99.99 | 0 | 1.33 |  |  |  |  |  |  |
| 502 | 6530 | 17 | 0 |  |  |  | A | 50 | 30 | 42 | 37 | 38 | 62 | 57 | 35 | 4 | 4 | 6 | N | 7 | 23 | 2 | 1-way | 99.99 | 0 | 1.39 | 1.5 | 1.4271 | 0.9947 | 1.1424 | 1.55 | 1.3619 |
| 770 | 6150 | 9 | 3 |  |  |  | A | 57 |  |  |  |  |  |  |  | 4 | 5 | 5 | N | N | 18 | 2 | 2-way | 99.99 | 22.57 | 1.58 |  |  |  |  |  |  |
| 1665 | 4700 | 10 | 3 |  |  |  | D | 10 |  |  |  |  |  |  |  | 4 | 5 | 4 | N | 7 | 24 | 2 | 2-way | 99.99 | 0 | 0.28 |  |  |  |  |  |  |
| 4658 | 5520 | 11 | 3 |  |  |  | A | 52 | 20 | 56 | 57 | 51 | 66 | 42 | 60 | 5 | 5 | 4 | N | 4 | 26 | 2 | 2-way | 99.99 | 0 | 1.44 | 1 | 1.8983 | 1.52 | 1.5455 | 1.65 | 1 |
| 1072 | 1690 | 6 | 6 |  |  |  | A | 66 |  |  |  |  |  |  |  | 5 | 5 | 4 | N | 4 | 24 | 2 | 2-way | 99.99 | 0 | 1.83 |  |  |  |  |  |  |
| 1368 | 7055 | 9 | 0 |  |  |  | A | 41 | 33 | 39 | 38 | 38 | 54 | 52 | 39 | 4 | 5 | 4 | N | 6 | 23.7 | 2 | 1-way | 99.99 | 0 | 1.14 | 1.665 | 1.3254 | 1.0187 | 1.1424 | 1.3375 | 1.2381 |

Figure 4-3. Detailed list of deficient bridges (continued).


Figure 4-3. Detailed list of deficient bridges (continued).

## Example

Using the criteria and weights described in the sections above and summarized in Figure 4-1, deficiency points are calculated for all state-owned bridges. The list of deficient bridges is "replaced" 10 bridges at a time by clicking on the slider in Figure 4-2. The bar charts in Figure 4-2 present an overview of the impact on the state bridge population of replacing the 10 mostdeficient bridges; and of replacing the next 10 most-deficient bridges, etc. More detailed information on particular deficiencies is presented in the color-coded column tally sheet (Figure $4-3$ ). Table 4-1 below summarizes the results of incrementally replacing the most-deficient bridges in the population.

Table 4-1. Effect on Bridge Population of Replacing

| \# Most-Deficient Bridges Replaced | Effect on Bridge Population |
| :---: | :---: |
| first 10 | Half of the 17 load-posted bridges replaced, including <br> all 3 of the bridges posted for school buses, <br> 8 of the 9 bridges posted for two-axle trucks <br> all 9 of the bridges posted for 18 -wheelers <br> Remaining load-deficient bridges are posted for primarily triaxle dump trucks |
| next 10 (total = 20) | 11 of the 12 bridges with condition ratings $=3$ now replaced |
| next 160 (total $=180$ ) | All of the 167 bridges with condition ratings $=4$ replaced 15 of the 17 load-posted bridges now replaced |
| next 80 (total $=260$ ) | All 47 of the narrow bridges (20-foot curb-to-curb decks) now replaced All 17 load-posted bridges now replaced |

The deficiency criteria and weight factors presented in the example therefore implement the following bridge replacement priorities (in order of decreasing importance):

- bridges load-posted for school buses, two-axle, trucks and 18-wheelers and bridges in extremely poor condition (condition ratings $=4$ )
- bridges in poor condition (condition ratings $=4$ )
- narrow bridges and bridges load-posted for less common trucks (triaxle dump truck, concrete, and six-axle)


### 5.0 Sensitivity Study

Utilizing the most recent data from the Alabama Bridge Information Database (ABIMS) database, several iterations of the current ALDOT weights and three scenarios (presented by ALDOT personnel) were generated using increasing levels of ADT and detour factoring.

## Procedure

The current ALDOT weights and the three scenarios are listed in Table 5-1 with respect to the importance placed on each of the four deficiency areas: load, condition, width, and vertical clearance.

Table 5-1. Weight Factors for Each Scenario

|  | Load | Condition | Width | Vertical <br> Clearance |
| :--- | :---: | :---: | :---: | :---: |
| ALDOT | $40 \%$ | $40 \%$ | $10 \%$ | $10 \%$ |
| Scenario I | $40 \%$ | $20 \%$ | $20 \%$ | $20 \%$ |
| Scenario II | $40 \%$ | $30 \%$ | $20 \%$ | $10 \%$ |
| Scenario III | $40 \%$ | $30 \%$ | $15 \%$ | $15 \%$ |

These weights are then used in conjunction with nine different levels of ADT and detour factoring to produce comparisons of the movement of individual bridges within the ranking of each case. This produces 36 different runs to completely saturate all possible outcomes. Table 5-2 presents the nine levels of ADT and detour factoring that were used for this analysis.

Table 5-2. ADT and Detour Length Weights

| Run | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ADT | $0 \%$ | $10 \%$ | $20 \%$ | $30 \%$ | $40 \%$ | $0 \%$ | $30 \%$ | $30 \%$ | $30 \%$ |
| Detour | $0 \%$ | $0 \%$ | $0 \%$ | $0 \%$ | $0 \%$ | $20 \%$ | $10 \%$ | $20 \%$ | $30 \%$ |

## Candidates

The analysis was focused on "state-owned" structures within all divisions of the Alabama Department of Transportation. This database (State-Owned Structures) was populated by more than 5,000 structures. When compared against the parameters used to denote a deficiency in terms of load, condition, width, and vertical clearance, 2906 structures were deficient in one or more of these areas.

The average replacement rate per year in Alabama varies from 20 to 40 structures per year. In order to project out for three years of construction, a base of 30 structures per year will be used
for analysis. This will be further simplified to observing the first 100 structures of the ranking while analyzing the weights and factors when prioritizing replacement policy.

## Deterioration Algorithm

The validation for the deterioration model used for this analysis was developed by Dr. James Richardson, Principal Investigator, as an extension of his previous work with Dr. Daniel Turner (1991a). A prioritized ranking of bridges based on ALDOT's weighting criteria was generated using data from a previous year. This data was then presented to the ALDOT bridge maintenance personnel who validated the result by indicating that structures identified as deficient and with high priority had been replaced or had been scheduled for replacement. This assists in the validation process in that the algorithm is generating the same replacement sequence as the current ALDOT system.

## Analysis

The analysis is a series of observations. The first being the different runs using the nine levels (combinations) of ADT and detour factor. This will assist in determining the proper level to which set the ADT and detour factor within the model. The next step in the analysis process is to graph the individual deficiencies (load, condition, width, and vertical clearance) along with the total deficiency in order to observe each deficiency's behavior. These graphs and their interpretation can be used to convey the results to the Alabama Bridge Management team that will determine the best scenario or a derivation to use as the final model which will be instituted.

## ADT and Detour Factors

A quasi-sensitivity analysis can be conducted by generating the bridge ranking based on ADT and detour factors of zero. This creates a baseline where ADT and detour have no effect on the calculation of total deficiency. ADT is then introduced into the model in increments of $10 \%$ up to a level where the ranking stabilizes and no further changes in a structure's position is observed. Tables 5-3, 5-4, 5-5, and 5-6 display the runs for the first 100 structures for the different scenarios. Through this process, the ADT factor stabilizes between $20 \%$ and $30 \%$. The interpretation is that between $20 \%$ and $30 \%$ the emphasis placed on the amount of ADT has it maximum effect on a structures ranking. ADT factors of $30 \%$ to $40 \%$ are relatively identical indicating that factor is not producing any additional effect that would cause structure to advance in the ranking. This is considered a stable ranking, bridges with large ADT and high deficiency scores will increase toward the front of the ranking and those structures with low ADT and moderate deficiency scores will continue to progress to the end of the ranking. Increasing the ADT factor would only widen this gap and not generate any additional permutations. Additionally, increasing the ADT factor to an immense proportion could have the effect of masking highly deficiency bridges with low ADT scores and focus attention to those structures which may be less deficient but have large ADT levels. Therefore, the ADT factor should be kept to a range where it is a discriminator in like cohort groups.

Detour factor is then applied to an already established ADT level of $30 \%$. Detour is the factor applied when a structure is not capable of carrying a specified load and an alternate route must
be utilized. The greater the amount of distance, "detour" that must be covered the greater the effect of the detour factor will have on the deficiency score. Detour levels of $10 \%, 20 \%$, and $30 \%$ are applied. Tables 5-7, 5-8, 5-9, and 5-10 display the effects of an increasing detour factor. The greatest change in the ranking appears when detour is increased from $0 \%$ to $10 \%$. Factors of $10 \%$ to $20 \%$ are the next greatest change and $20 \%$ to $30 \%$ show signs of stabilization. Increasing the detour factor beyond $30 \%$ would start to have the same effect as mentioned for the ADT factor. Structures with large detour lengths could mask structures that are more deficient.

Table 5-3. Bridge Rankings for Current ALDOT Weights, No Detour Factor, ADT Factor $=0,0.2,0.3,0.4$

|  | $\text { (ınołza ou ' } \perp \square \forall \text { ou) }$ | (no Detour), ADT 20\% | (no Detour) ADT 30\% | (no Detour) ADT 40\% |
| :---: | :---: | :---: | :---: | :---: |
|  | 0 <br> 0 <br> 0 <br> -1 <br> 0 <br> 8 <br> 0 <br>  <br>  <br> 0 <br> 0 | 0 <br> 0 <br> 0 <br> 0 <br> - <br> 0 <br> + <br> 0 <br>  <br>  <br> 0 <br> 0 <br> 4 | 0 <br> 0 <br> - <br> 0 <br> -1 <br> 0 <br> + <br> 0 <br>  <br>  <br> 0 <br> 0 <br> 4 | 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br>  <br>  <br> 0 <br> - |
| Rank | BIN | BIN | BIN | BIN |
| 1 | 1841 | 1841 | 1841 | 1841 |
| 2 | 2736 | 2736 | 2736 | 2736 |
| 3 | 635 | 635 | 635 | 635 |
| 4 | 529 | 529 | 529 | 529 |
| 5 | 981 | 1842 | 1842 | 1842 |
| 6 | 1842 | 981 | 504 | 504 |
| 7 | 504 | 504 | 7608 | 7608 |
| 8 | 7608 | 7608 | 981 | 2037 |
| 9 | 2037 | 2037 | 2037 | 198 |
| 10 | 503 | 503 | 503 | 503 |
| 11 | 1798 | 1798 | 1798 | 1798 |
| 12 | 4507 | 4507 | 4507 | 4507 |
| 13 | 3202 | 3202 | 3202 | 3202 |
| 14 | 1765 | 1765 | 1765 | 1765 |
| 15 | 1394 |  |  |  |
| 16 | 18612 | 1394 | 1394 | 1394 |
| 17 | 18614 | 18612 | 18612 | 18612 |
| 18 |  | 18614 | 18614 | 18614 |
| 19 | 4947 | 4947 | 4947 | 4947 |
| 20 | 5618 | 5618 | 5618 | 5618 |
| 21 | 4975 | 4975 | 4975 | 4975 |
| 22 | 2534 | 2534 | 2534 | 2534 |
| 23 | 474 | 474 | 474 | 474 |
| 24 | 784 | 784 | 784 | 784 |
| 25 | 944 | 944 | 944 | 944 |
| 26 |  |  |  |  |
| 27 | 10132 | 10132 | 10132 | 10132 |
| 28 | 9367 | 9367 | 9367 | 9367 |
| 29 | 502 | 502 | 502 | 502 |
| 30 | 1368 | 1368 | 1368 | 1368 |
| 31 | 885 | 885 | 885 | 885 |
| 32 | $10 / 2$ | 17 | 107 | 101 |
| 33 | 1665 | 1665 | 1665 | 1665 |
| 34 | 2627 | 2627 | 2627 | 2627 |
| 35 | 2712 | 2712 | 2712 | 2712 |
| 36 | 3130 | 3130 | 3130 | 3130 |
| 37 | 4658 | 4658 | 4658 | 4658 |
| 38 | 12793 | 12793 | 12793 | 12793 |
| 39 | 5816 | 5816 | 5816 | 5816 |
| 40 | 10102 | 10102 | 10102 | 10102 |
| 41 | 6473 | 6473 | 6473 | 6473 |
| 42 | 6588 | 6588 | 6588 | 6588 |
| 43 | 7365 | 7365 | 7365 | 7365 |
| 44 | 4994 | 4994 | 4994 | 4994 |
| 45 | 10493 | 10493 | 10493 | 10493 |
| 46 | 615 | 615 | 615 | 615 |
| 47 | 770 | 770 | 770 | 770 |
| 48 | 798 | 798 | 798 | 798 |
| 49 | 14407 | 14407 | 14407 | 14407 |
| 50 | 10083 | 10083 | 10083 | 10083 |


| 51 | 617 | 617 | 617 | 617 |
| :---: | :---: | :---: | :---: | :---: |
| 52 | 1268 | 1268 | 1268 | 1268 |
| 53 | 3817 | 3817 | 3817 | 3817 |
| 54 | 3818 | 3818 | 3818 | 3818 |
| 55 | 8060 | 8060 | 8060 | 8060 |
| 56 | 8648 | 8648 | 8648 | 8648 |
| 57 | 5430 | 5430 | 5430 | 5430 |
| 58 | 10690 | 10690 | 10690 | 10690 |
| 59 | 476 | 476 | 476 | 476 |
| 60 | 486 | 486 | 486 | 486 |
| 61 | 1717 | 1717 | 1717 | 1717 |
| 62 | 1739 | 1739 | 1739 | 1739 |
| 63 | 1917 | 1917 | 1917 | 1917 |
| 64 | 1918 | 1918 | 1918 | 1918 |
| 65 | 2566 | 2566 | 2566 | 2566 |
| 66 | 2567 | 2567 | 2567 | 2567 |
| 67 | 5977 | 5977 | 5977 | 5977 |
| 68 | 1911 | 1911 | 1911 | 1911 |
| 69 | 271 | 271 | 271 | 271 |
| 70 | 843 | 843 | 843 | 843 |
| 71 | 915 | 915 | 915 | 915 |
| 72 | 1029 | 1029 | 1029 | 1029 |
| 73 | 107 | 1072 | 107 | 107 |
| 74 | 1273 | 1273 | 1273 | 1273 |
| 75 | 1274 | 1274 | 1274 | 1274 |
| 76 | 1275 | 1275 | 1275 | 1275 |
| 77 | 1276 | 1276 | 1276 | 1276 |
| 78 | 1277 | 1277 | 1277 | 1277 |
| 79 | 1442 | 1442 | 1442 | 1442 |
| 80 | 1613 | 1613 | 1613 | 1613 |
| 81 | 1664 | 1664 | 1664 | 1664 |
| 82 | 1695 | 1695 | 1695 | 1695 |
| 83 | 1797 | 1797 | 1797 | 1797 |
| 84 | 1897 | 1897 | 1897 | 1897 |
| 85 | 1898 | 1898 | 1898 | 1898 |
| 86 | 2013 | 2013 | 2013 | 2013 |
| 87 | 2108 | 2108 | 2108 | 2108 |
| 88 | 2253 | 2253 | 2253 | 2253 |
| 89 | 2320 | 2320 | 2320 | 2320 |
| 90 | 2408 | 2408 | 2408 | 2408 |
| 91 | 2588 | 2588 | 2588 | 2588 |
| 92 | 2666 | 2666 | 2666 | 2666 |
| 93 | 2695 | 2695 | 2695 | 2695 |
| 94 | 3899 | 3899 | 3899 | 3899 |
| 95 | 4333 | 4333 | 4333 | 4333 |
| 96 | 5222 | 5222 | 5222 | 5222 |
| 97 | 5973 | 5973 | 5973 | 5973 |
| 98 | 6062 | 6062 | 6062 | 6062 |
| 99 | 8466 | 8466 | 8466 | 8466 |
| 100 | 8467 | 8467 | 8467 | 8467 |

Table 5-4. Bridge Rankings for Scenario I, No Detour Factor, ADT Factor $=0,0.2,0.3,0.4$

|  | $\square$ <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> $\vdots$ <br>  <br>  <br> 0 <br> 0 |  | (no Detour) ADT 30\% | (no Detour) ADT 40\% |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Senario I $(40,20,20,20)$ | ( $0 Z^{\prime} 0 Z^{\prime} 0 Z^{\prime} 0 \downarrow$ ) I о!̣меиаS |  |
| Rank | BIN | BIN | BIN | BIN |
| 1 | 1841 | 1841 | 1841 | 1841 |
| 2 | 529 | 529 | 529 | 529 |
| 3 | 2736 | 2736 | 2736 | 2736 |
| 4 | 635 | 635 | 635 | 635 |
| 5 | 1842 | 1842 | 1842 | 1842 |
| 6 | 504 | 504 | 504 | 504 |
| 7 | 7608 | 7608 | 7608 | 7608 |
| 8 | 2037 | 2037 | 2037 | 2037 |
| 9 | 3202 |  | 804 |  |
| 10 | 1765 | 3202 | 3202 | 3202 |
| 11 | 4947 | 1765 | 1765 | 1765 |
| 12 | 5618 | 4947 | 4947 | 4947 |
| 13 | 4975 | 5618 | 5618 | 5618 |
| 14 |  | 784 | 784 | 784 |
| 15 | 2534 | 4975 | 4975 | 4975 |
| 16 | 981 | 2534 | 2534 | 2534 |
| 17 | 503 | 981 | 1981 | 981 |
| 18 | 944 | 503 | 503 | 503 |
| 19 |  | 944 | 944 | 944 |
| 20 | 18612 |  |  |  |
| 21 | 784 | 18612 | 18612 | 18612 |
| 22 | 1394 | 1394 | 1394 | 1394 |
| 23 | 1798 | 2035 | 2035 | 2035 |
| 24 | 4507 | 10033 | 10033 | 10033 |
| 25 | 474 | 10034 | 10034 | 10034 |
| 26 | 615 | 10641 | 10641 | 10641 |
| 27 | 770 | 1798 | 1798 | 1798 |
| 28 | 798 | 4507 | 4507 | 4507 |
| 29 | 2035 | 2273 | 2273 | 2273 |
| 30 | 10033 | 474 | 474 | 474 |
| 31 | 10034 | 10493 | 10493 | 10493 |
| 32 | 10641 | 1901 | 1901 | 1901 |
| 33 | 18614 | 1387 | 1387 | 1387 |
| 34 | 10083 | 1709 | 1709 | 1709 |
| 35 | 502 | 615 | 615 | 615 |
| 36 | 617 | 770 | 770 | 770 |
| 37 | 8323 | 798 | 798 | 798 |
| 38 | 8324 | 6487 | 6487 | 6487 |
| 39 | 2273 | 7544 | 7544 | 7544 |
| 40 | 1268 | 8118 | 8118 | 8118 |
| 41 | 1368 | 8188 | 8188 | 8188 |
| 42 | 3817 | 8327 | 8327 | 8327 |
| 43 | 3818 | 10868 | 10868 | 10868 |
| 44 | 13809 | 14407 | 14407 | 14407 |
| 45 | 885 | 19153 | 19153 | 19153 |
| 46 | 107 | 8326 | 8326 | 8326 |
| 47 | 1665 | 8965 | 8965 | 8965 |
| 48 | 2627 | 10428 | 10428 | 10428 |
| 49 | 2712 | 6229 | 6229 | 6229 |
| 50 | 3130 | 41 | 418 | 415 |


| 51 | 8060 | 18614 | 18614 | 18614 |
| :---: | :---: | :---: | :---: | :---: |
| 52 | 10493 | 6378 | 6378 | 6378 |
| 53 | 10132 | 4850 | 4850 | 4850 |
| 54 | 4658 | 15061 | 15061 | 15061 |
| 55 | 17042 | 5461 | 5461 | 5461 |
| 56 | 6574 | 2648 | 2648 | 2648 |
| 57 | 12793 | 928 | 928 | 928 |
| 58 | 8648 | 9542 | 9542 | 9542 |
| 59 | 5816 | 7638 | 7638 | 7638 |
| 60 | 9367 | 7852 | 7852 | 7852 |
| 61 | 10102 | 8797 | 8797 | 8797 |
| 62 | 5430 | 9528 | 9528 | 9528 |
| 63 | 6473 | 9625 | 9625 | 9625 |
| 64 | 6588 | 10174 | 10174 | 10174 |
| 65 | 7365 | 13682 | 13682 | 13682 |
| 66 | 476 | 6449 | 6449 | 6449 |
| 67 | 486 | 7250 | 7250 | 7250 |
| 68 | 1901 | 10427 | 10427 | 10427 |
| 69 | 4994 | 10083 | 10083 | 10083 |
| 70 | 10690 | 6437 | 6437 | 6437 |
| 71 | 1387 | 6438 | 6438 | 6438 |
| 72 | 1717 | 6495 | 6495 | 6495 |
| 73 | 1739 | 6496 | 6496 | 6496 |
| 74 | 1917 | 6499 | 6499 | 6499 |
| 75 | 1918 | 6500 | 6500 | 6500 |
| 76 | 2566 | 8187 | 8187 | 8187 |
| 77 | 2567 | 9527 | 9527 | 9527 |
| 78 | 5977 | 502 | 502 | 502 |
| 79 | 1911 | 617 | 617 | 617 |
| 80 | 1709 | 7329 | 7329 | 7329 |
| 81 | 226 | 7330 | 7330 | 7330 |
| 82 | 227 | 9902 | 9902 | 9902 |
| 83 | 228 | 8976 | 8976 | 8976 |
| 84 | 249 | 8323 | 8323 | 8323 |
| 85 | 271 | 8324 | 8324 | 8324 |
| 86 | 278 | 7561 | 7561 | 7561 |
| 87 | 280 | 8155 | 8155 | 8155 |
| 88 | 366 | 9543 | 9543 | 9543 |
| 89 | 426 | 9544 | 9544 | 9544 |
| 90 | 429 | 4756 | 4756 | 4756 |
| 91 | 430 | 5068 | 5068 | 5068 |
| 92 | 438 | 7984 | 7984 | 7984 |
| 93 | 469 | 8186 | 8186 | 8186 |
| 94 | 481 | 1268 | 1268 | 1268 |
| 95 | 485 | 1368 | 1368 | 1368 |
| 96 | 517 | 3817 | 3817 | 3817 |
| 97 | 519 | 3818 | 3818 | 3818 |
| 98 | 543 | 7320 | 7320 | 7320 |
| 99 | 556 | 4794 | 4794 | 4794 |
| 100 | 616 | 14647 | 14647 | 14647 |

Table 5-5. Bridge Rankings for Scenario II, No Detour Factor, ADT Factor $=0,0.2,0.3,0.4$

|  | $\square$ <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> $\vdots$ <br> $\vdots$ <br>  <br> 0 <br> 0 | (no Detour), ADT 20\% | (no Detour) ADT 30\% | (no Detour) ADT 40\% |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Senario II $(40,30,20,10)$ |  |  |
| Rank | BIN | BIN | BIN | BIN |
| 1 | 1841 | 1841 | 1841 | 1841 |
| 2 | 529 | 529 | 529 | 529 |
| 3 | 2736 | 2736 | 2736 | 2736 |
| 4 | 635 | 635 | 635 | 635 |
| 5 | 1842 | 1842 | 1842 | 1842 |
| 6 | 504 | 504 | 504 | 504 |
| 7 | 7608 | 7608 | 7608 | 7608 |
| 8 | 981 | 2037 | 2037 | 2037 |
| 9 | 2037 | 9818 | 19818 |  |
| 10 | 3202 | 3202 | 2846 | 1981 |
| 11 | 1765 | 1765 | 3202 | 3202 |
| 12 | 503 | 503 | 1765 | 1765 |
| 13 | 4947 | 844 | 503 | 503 |
| 14 | 5618 | 1798 | 1798 | 1798 |
| 15 | 1394 | 4507 | 4507 | 4507 |
| 16 | 1798 | 4947 | 4947 | 4947 |
| 17 | 4507 | 5618 | 5618 | 5618 |
| 18 | 4975 | 1394 | 1394 | 1394 |
| 19 |  | 4975 | 4975 | 4975 |
| 20 | 2534 | 2534 | 2534 | 2534 |
| 21 | 18612 | 18612 | 18612 | 18612 |
| 22 | 784 | 784 | 784 | 784 |
| 23 | 944 | 944 | 944 | 944 |
| 24 |  |  |  |  |
| 25 | 474 | 474 | 474 | 474 |
| 26 | 18614 | 18614 | 18614 | 18614 |
| 27 | 615 | 615 | 615 | 615 |
| 28 | 770 | 770 | 770 | 770 |
| 29 | 798 | 798 | 798 | 798 |
| 30 | 502 | 502 | 502 | 502 |
| 31 | 1368 | 10132 | 10132 | 10132 |
| 32 | 10083 | 1368 | 1368 | 1368 |
| 33 | 617 | 10083 | 10083 | 10083 |
| 34 | 10132 | 617 | 617 | 617 |
| 35 | 885 | 9367 | 9367 | 9367 |
| 36 | 1072 | 885 | 885 | 885 |
| 37 | 1665 | 107 | 107 | 0 |
| 38 | 2627 | 1665 | 1665 | 1665 |
| 39 | 2712 | 2627 | 2627 | 2627 |
| 40 | 3130 | 2712 | 2712 | 2712 |
| 41 | 9367 | 3130 | 3130 | 3130 |
| 42 | 4658 | 4658 | 4658 | 4658 |
| 43 | 1268 | 1268 | 1268 | 1268 |
| 44 | 3817 | 3817 | 3817 | 3817 |
| 45 | 3818 | 3818 | 3818 | 3818 |
| 46 | 12793 | 12793 | 12793 | 12793 |
| 47 | 5816 | 5816 | 5816 | 5816 |
| 48 | 2035 | 2035 | 2035 | 2035 |
| 49 | 8060 | 8060 | 8060 | 8060 |
| 50 | 10033 | 10033 | 10033 | 10033 |


| 51 | 10034 | 10034 | 10034 | 10034 |
| :---: | :---: | :---: | :---: | :---: |
| 52 | 10102 | 10102 | 10102 | 10102 |
| 53 | 10493 | 10493 | 10493 | 10493 |
| 54 | 10641 | 10641 | 10641 | 10641 |
| 55 | 6473 | 6473 | 6473 | 6473 |
| 56 | 6588 | 6588 | 6588 | 6588 |
| 57 | 7365 | 7365 | 7365 | 7365 |
| 58 | 4994 | 4994 | 4994 | 4994 |
| 59 | 8648 | 8648 | 8648 | 8648 |
| 60 | 5430 | 5430 | 5430 | 5430 |
| 61 | 8323 | 2273 | 2273 | 2273 |
| 62 | 8324 | 476 | 476 | 476 |
| 63 | 2273 | 486 | 486 | 486 |
| 64 | 476 | 1717 | 1717 | 1717 |
| 65 | 486 | 1739 | 1739 | 1739 |
| 66 | 10690 | 1917 | 1917 | 1917 |
| 67 | 1717 | 1918 | 1918 | 1918 |
| 68 | 1739 | 2566 | 2566 | 2566 |
| 69 | 1917 | 2567 | 2567 | 2567 |
| 70 | 1918 | 5977 | 5977 | 5977 |
| 71 | 2566 | 1911 | 1911 | 1911 |
| 72 | 2567 | 271 | 271 | 271 |
| 73 | 5977 | 843 | 843 | 843 |
| 74 | 1911 | 915 | 915 | 915 |
| 75 | 13809 | 1029 | 1029 | 1029 |
| 76 | 271 | 1071 | 107 | 107 |
| 77 | 843 | 1273 | 1273 | 1273 |
| 78 | 915 | 1274 | 1274 | 1274 |
| 79 | 1029 | 1275 | 1275 | 1275 |
| 80 | 107 | 1276 | 1276 | 1276 |
| 81 | 1273 | 1277 | 1277 | 1277 |
| 82 | 1274 | 1442 | 1442 | 1442 |
| 83 | 1275 | 1613 | 1613 | 1613 |
| 84 | 1276 | 1664 | 1664 | 1664 |
| 85 | 1277 | 1695 | 1695 | 1695 |
| 86 | 1442 | 1797 | 1797 | 1797 |
| 87 | 1613 | 1897 | 1897 | 1897 |
| 88 | 1664 | 1898 | 1898 | 1898 |
| 89 | 1695 | 2013 | 2013 | 2013 |
| 90 | 1797 | 2108 | 2108 | 2108 |
| 91 | 1897 | 2253 | 2253 | 2253 |
| 92 | 1898 | 2320 | 2320 | 2320 |
| 93 | 2013 | 2408 | 2408 | 2408 |
| 94 | 2108 | 2588 | 2588 | 2588 |
| 95 | 2253 | 2666 | 2666 | 2666 |
| 96 | 2320 | 2695 | 2695 | 2695 |
| 97 | 2408 | 3899 | 3899 | 3899 |
| 98 | 2588 | 4333 | 4333 | 4333 |
| 99 | 2666 | 5222 | 5222 | 5222 |
| 100 | 2695 | 5973 | 5973 | 5973 |

Table 5-6. Bridge Rankings for Scenario III, No Detour Factor, ADT Factor $=0,0.2,0.3,0.4$

|  | ( ınozəg ou ' $\lrcorner \square \forall$ ou) | no Detour), ADT 20\% |  | (no Detour) ADT 40\% |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| Rank | BIN | BIN | BIN | BIN |
| 1 | 1841 | 1841 | 1841 | 1841 |
| 2 | 529 | 529 | 529 | 529 |
| 3 | 2736 | 2736 | 2736 | 2736 |
| 4 | 635 | 635 | 635 | 635 |
| 5 | 1842 | 1842 | 1842 | 1842 |
| 6 | 504 | 504 | 504 | 504 |
| 7 | 7608 | 7608 | 7608 | 7608 |
| 8 | 981 | 2037 | 2037 | 2037 |
| 9 | 2037 | 9818 | 9818 |  |
| 10 | 3202 | 3202 |  | 981 |
| 11 | 1765 | 1765 | 3202 | 3202 |
| 12 | 503 |  | 1765 | 1765 |
| 13 | 4507 | 503 | 503 | 503 |
| 14 | 1798 | 1798 | 1798 | 1798 |
| 15 | 4947 | 4507 | 4507 | 4507 |
| 16 | 5618 | 4947 | 4947 | 4947 |
| 17 | 4975 | 5618 | 5618 | 5618 |
| 18 | 284 | 4975 | 4975 | 4975 |
| 19 | 1394 | 784 | 784 | 784 |
| 20 | 784 | 1394 | 1394 | 1394 |
| 21 | 18612 | 18612 | 18612 | 18612 |
| 22 | 2534 | 2534 | 2534 | 2534 |
| 23 | 944 | 944 | 944 | 944 |
| 24 |  |  |  |  |
| 25 | 474 | 474 | Sea | 474 |
| 26 | 18614 | 18614 | 18614 | 18614 |
| 27 | 10493 | 10493 | 10493 | 10493 |
| 28 | 502 | 502 | 502 | 502 |
| 29 | 14407 | 10132 | 10132 | 10132 |
| 30 | 10641 | 9367 | 9367 | 9367 |
| 31 | 10034 | 615 | 615 | 615 |
| 32 | 10033 | 770 | 770 | 770 |
| 33 | 2035 | 798 | 798 | 798 |
| 34 | 798 | 2035 | 2035 | 2035 |
| 35 | 770 | 10033 | 10033 | 10033 |
| 36 | 615 | 10034 | 10034 | 10034 |
| 37 | 10132 | 10641 | 10641 | 10641 |
| 38 | 1368 | 14407 | 14407 | 14407 |
| 39 | 9367 | 1368 | 1368 | 1368 |
| 40 | 3130 | 885 | 885 | 885 |
| 41 | 2712 | 107 | 107 | 107 |
| 42 | 2627 | 1665 | 1665 | 1665 |
| 43 | 1665 | 2627 | 2627 | 2627 |
| 44 | $10 / 2$ | 2712 | 2712 | 2712 |
| 45 | 885 | 3130 | 3130 | 3130 |
| 46 | 10083 | 10083 | 10083 | 10083 |
| 47 | 4658 | 4658 | 4658 | 4658 |
| 48 | 617 | 617 | 617 | 617 |
| 49 | 12793 | 12793 | 12793 | 12793 |
| 50 | 2273 | 2273 | 2273 | 2273 |


| 51 | 5816 | 5816 | 5816 | 5816 |
| :---: | :---: | :---: | :---: | :---: |
| 52 | 10102 | 10102 | 10102 | 10102 |
| 53 | 7365 | 6473 | 6473 | 6473 |
| 54 | 6588 | 6588 | 6588 | 6588 |
| 55 | 6473 | 7365 | 7365 | 7365 |
| 56 | 4994 | 4994 | 4994 | 4994 |
| 57 | 3818 | 1268 | 1268 | 1268 |
| 58 | 3817 | 3817 | 3817 | 3817 |
| 59 | 1268 | 3818 | 3818 | 3818 |
| 60 | 8060 | 8060 | 8060 | 8060 |
| 61 | 8648 | 8648 | 8648 | 8648 |
| 62 | 5430 | 5430 | 5430 | 5430 |
| 63 | 10690 | 10690 | 10690 | 10690 |
| 64 | 1901 | 476 | 476 | 476 |
| 65 | 486 | 486 | 486 | 486 |
| 66 | 476 | 1901 | 1901 | 1901 |
| 67 | 5977 | 1387 | 1387 | 1387 |
| 68 | 2567 | 1717 | 1717 | 1717 |
| 69 | 2566 | 1739 | 1739 | 1739 |
| 70 | 1918 | 1917 | 1917 | 1917 |
| 71 | 1917 | 1918 | 1918 | 1918 |
| 72 | 1739 | 2566 | 2566 | 2566 |
| 73 | 1717 | 2567 | 2567 | 2567 |
| 74 | 1387 | 5977 | 5977 | 5977 |
| 75 | 1911 | 1911 | 1911 | 1911 |
| 76 | 1709 | 1709 | 1709 | 1709 |
| 77 | 19153 | 271 | 271 | 271 |
| 78 | 10868 | 843 | 843 | 843 |
| 79 | 8467 | 915 | 915 | 915 |
| 80 | 8466 | 1029 | 1029 | 1029 |
| 81 | 8327 | 107 | 107 | 107 |
| 82 | 8188 | 1273 | 1273 | 1273 |
| 83 | 8118 | 1274 | 1274 | 1274 |
| 84 | 7544 | 1275 | 1275 | 1275 |
| 85 | 6487 | 1276 | 1276 | 1276 |
| 86 | 6062 | 1277 | 1277 | 1277 |
| 87 | 5973 | 1442 | 1442 | 1442 |
| 88 | 5222 | 1613 | 1613 | 1613 |
| 89 | 4333 | 1664 | 1664 | 1664 |
| 90 | 3899 | 1695 | 1695 | 1695 |
| 91 | 2695 | 1797 | 1797 | 1797 |
| 92 | 2666 | 1897 | 1897 | 1897 |
| 93 | 2588 | 1898 | 1898 | 1898 |
| 94 | 2408 | 2013 | 2013 | 2013 |
| 95 | 2320 | 2108 | 2108 | 2108 |
| 96 | 2253 | 2253 | 2253 | 2253 |
| 97 | 2108 | 2320 | 2320 | 2320 |
| 98 | 2013 | 2408 | 2408 | 2408 |
| 99 | 1898 | 2588 | 2588 | 2588 |
| 100 | 1897 | 2666 | 2666 | 2666 |

Table 5-7. Bridge Rankings for Current ALDOT Weights, ADT Factor $=0.3$, Detour Factor $=0,0.1,0.2,0.3$

|  | (no Detour) ADT 30\% |  | \%0Z inolag '\%0ع 1 IG |  |
| :---: | :---: | :---: | :---: | :---: |
|  | $\operatorname{ALDOT}(40,40,10,10)$ | $\operatorname{ALDOT}(40,40,10,10)$ | 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br>  <br> 0 <br> 0 | $\operatorname{ALDOT}(40,40,10,10)$ |
| Rank | BIN | BIN | BIN | BIN |
| 1 | 1841 | 1841 | 1841 | 1841 |
| 2 | 2736 | 2736 | 2736 | 2736 |
| 3 | 635 | 635 | 635 | 635 |
| 4 | 529 | 529 | 529 | 529 |
| 5 | 1842 | 1842 | 1842 | 1842 |
| 6 | 504 | 7608 | 7608 | 7608 |
| 7 | 7608 | 504 | 2037 | 2037 |
| 8 | 19818 | 2037 | 504 | 504 |
| 9 | 2037 | 1981 | 503 | 503 |
| 10 | 503 | 503 | 4507 | 4507 |
| 11 | 1798 | 4507 | 3202 | 3202 |
| 12 | 4507 | 3202 |  |  |
| 13 | 3202 | 1798 | 1765 | 1765 |
| 14 | 1765 | 1765 | 1798 | 1798 |
| 15 |  | 2892 | 1981 | 1394 |
| 16 | 1394 | 1394 | 1394 | 981 |
| 17 | 18612 | 18612 | 784 | 784 |
| 18 | 18614 | 4975 | 4975 | 9367 |
| 19 | 4947 | 784 | 9367 | 4975 |
| 20 | 5618 | 4947 | 2534 | 10132 |
| 21 | 4975 | 5618 | 4947 | 2534 |
| 22 | 2534 | 18614 | 10132 | 4947 |
| 23 | 474 | 2534 | 18612 | 944 |
| 24 | 784 | 944 | 944 | 502 |
| 25 | 944 | 9367 | 5618 |  |
| 26 |  | 10132 |  | 5618 |
| 27 | 10132 | 474 | 474 | 474 |
| 28 | 9367 | 285 | 502 | 1368 |
| 29 | 502 | 502 | 18614 | 10493 |
| 30 | 1368 | 1368 | 1368 | 5816 |
| 31 | 885 | 885 | 5816 | 12793 |
| 32 | 107 | 1665 | 12793 | 6473 |
| 33 | 1665 | 5816 | 885 | 18612 |
| 34 | 2627 | 2712 | 1665 | 885 |
| 35 | 2712 | 12793 | 6473 | 1665 |
| 36 | 3130 | 4658 | 10493 | 4658 |
| 37 | 4658 | 6473 | 4658 | 6588 |
| 38 | 12793 | 2627 | 2712 | 7365 |
| 39 | 5816 | 107 | 6588 | 14407 |
| 40 | 10102 | 6588 | 7365 | 2712 |
| 41 | 6473 | 7365 | 10102 | 10102 |
| 42 | 6588 | 10102 | 2627 | 4994 |
| 43 | 7365 | 10493 | 4994 | 2627 |
| 44 | 4994 | 4994 | 107 | 18614 |
| 45 | 10493 | 3130 | 14407 | 07 |
| 46 | 615 | 14407 | 615 | 615 |
| 47 | 770 | 615 | 770 | 770 |
| 48 | 798 | 770 | 3130 | 8648 |
| 49 | 14407 | 798 | 798 | 798 |
| 50 | 10083 | 617 | 617 | 617 |


| 51 | 617 | 8648 | 8648 | 5430 |
| :---: | :---: | :---: | :---: | :---: |
| 52 | 1268 | 3817 | 5430 | 3130 |
| 53 | 3817 | 3818 | 476 | 8134 |
| 54 | 3818 | 5430 | 8134 | 476 |
| 55 | 8060 | 1268 | 3817 | 861 |
| 56 | 8648 | 8060 | 3818 | 486 |
| 57 | 5430 | 476 | 486 | 1695 |
| 58 | 10690 | 10690 | 10690 | 2550 |
| 59 | 476 | 486 | 1268 | 9044 |
| 60 | 486 | 10083 | 86 | 2253 |
| 61 | 1717 | 8134 | 1695 | 10690 |
| 62 | 1739 | 1739 | 2253 | 8133 |
| 63 | 1917 | 1695 | 1739 | 2013 |
| 64 | 1918 | 1917 | 2013 | 5006 |
| 65 | 2566 | 1918 | 2550 | 1739 |
| 66 | 2567 | 2253 | 1897 | 3817 |
| 67 | 5977 | 2013 | 1898 | 3818 |
| 68 | 1911 | 1911 | 1664 | 1897 |
| 69 | 271 | 1897 | 8060 | 1898 |
| 70 | 843 | 1898 | 1917 | 1664 |
| 71 | 915 | 1664 | 1918 | 9229 |
| 72 | 1029 | 886 | 9044 | 2682 |
| 73 | 107 | 1613 | 8133 | 5603 |
| 74 | 1273 | 2666 | 2682 | 7630 |
| 75 | 1274 | 271 | 1613 | 7631 |
| 76 | 1275 | 2550 | 2666 | 9444 |
| 77 | 1276 | 915 | 5006 | 1613 |
| 78 | 1277 | 1717 | 271 | 7627 |
| 79 | 1442 | 1273 | 1911 | 2666 |
| 80 | 1613 | 1274 | 915 | 1917 |
| 81 | 1664 | 1275 | 9229 | 1918 |
| 82 | 1695 | 1276 | 1273 | 7766 |
| 83 | 1797 | 6062 | 1274 | 271 |
| 84 | 1897 | 2320 | 1275 | 4754 |
| 85 | 1898 | 5977 | 1276 | 915 |
| 86 | 2013 | 1277 | 6062 | 3033 |
| 87 | 2108 | 2682 | 2320 | 6470 |
| 88 | 2253 | 2588 | 5603 | 6471 |
| 89 | 2320 | 1442 | 3033 | 140 |
| 90 | 2408 | 2408 | 9444 | 7232 |
| 91 | 2588 | 5222 | 7766 | 1911 |
| 92 | 2666 | 3033 | 7630 | 1273 |
| 93 | 2695 | 2695 | 7631 | 1274 |
| 94 | 3899 | 3024 | 1277 | 1275 |
| 95 | 4333 | 2566 | 7627 | 1276 |
| 96 | 5222 | 2567 | 3024 | 7238 |
| 97 | 5973 | 1029 | 2588 | 6062 |
| 98 | 6062 | 9044 | 1442 | 5992 |
| 99 | 8466 | 8133 | 314 | 6355 |
| 100 | 8467 | 5006 | 2408 | 2320 |

Table 5－8．Bridge Rankings for Scenario I，ADT Factor $=0.3$ ，Detour Factor $=0,0.1,0.2,0.3$

|  | （no Detour）ADT 30\％ | ADT 30\％，Detour 10\％ | ADT 30\％，Detour 20\％ | \％0と ユnotag＇\％0と 1 OV |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| Rank | BIN | BIN | BIN | BIN |
| 1 | 1841 | 1841 | 1841 | 1841 |
| 2 | 529 | 529 | 529 | 529 |
| 3 | 2736 | 2736 | 2736 | 2736 |
| 4 | 635 | 635 | 635 | 635 |
| 5 | 1842 | 1842 | 1842 | 1842 |
| 6 | 504 | 7608 | 7608 | 7608 |
| 7 | 7608 | 504 | 504 | 2037 |
| 8 | 2037 | 2037 | 2037 | 504 |
| 9 |  |  |  |  |
| 10 | 3202 | 3202 | 3202 | 784 |
| 11 | 1765 | 1765 | 784 | 3202 |
| 12 | 4947 | 784 | 1765 | 1765 |
| 13 | 5618 | 4975 | 4975 | 2035 |
| 14 | 784 | 4947 | 4947 | 4975 |
| 15 | 4975 | 5618 | 503 | 503 |
| 16 | 2534 | 2534 | 5618 | 2273 |
| 17 | 81 | 503 | 2534 | 4947 |
| 18 | 503 | 944 | 2035 | 2534 |
| 19 | 944 |  | 944 | 10641 |
| 20 |  | 2035 | 10641 | 1394 |
| 21 | 18612 | 10641 | 2273 | 5618 |
| 22 | 1394 | 1394 | 1394 | 944 |
| 23 | 2035 | 2273 |  | 10493 |
| 24 | 10033 | 1981 | 10493 |  |
| 25 | 10034 | 10033 | 4507 | 1901 |
| 26 | 10641 | 10034 | 10033 | 4507 |
| 27 | 1798 | 4507 | 10034 | 10428 |
| 28 | 4507 | 10493 | 1901 | 10033 |
| 29 | 2273 | 18612 | 1798 | 10034 |
| 30 | 474 | 1798 | 10428 | 14407 |
| 31 | 10493 | 1901 | 1981 | 8327 |
| 32 | 1901 | 474 | 1387 | 9542 |
| 33 | 1387 | 1387 | 14407 | 1387 |
| 34 | 1709 | 10428 | 8327 | 1798 |
| 35 | 615 | 14407 | 18612 | 10427 |
| 36 | 770 | 8327 | 9542 | 2648 |
| 37 | 798 | 1709 | 474 | 928 |
| 38 | 6487 | 6487 | 2648 | 9543 |
| 39 | 7544 | 2648 | 10427 | 9544 |
| 40 | 8118 | 928 | 928 | 15061 |
| 41 | 8188 | 9542 | 6487 | 6487 |
| 42 | 8327 | 8118 | 15061 | 474 |
| 43 | 10868 | 615 | 1709 | 1709 |
| 44 | 14407 | 15061 | 8118 | 6378 |
| 45 | 19153 | 10427 | 6378 | 8118 |
| 46 | 8326 | 770 | 9543 | 615 |
| 47 | 8965 | 19153 | 9544 | 9902 |
| 48 | 10428 | 6378 | 615 | 770 |
| 49 | 6229 | 8326 | 770 | 18612 |
| 50 | 4159 | 8188 | 19153 | 19153 |


| 51 | 18614 | 10868 | 8326 | 6437 |
| :---: | :---: | :---: | :---: | :---: |
| 52 | 6378 | 798 | 9902 | 6438 |
| 53 | 4850 | 7544 | 8188 | 8326 |
| 54 | 15061 | 6229 | 6437 | 19812 |
| 55 | 5461 | 8965 | 6438 | 8797 |
| 56 | 2648 | 9543 | 7638 | 6449 |
| 57 | 928 | 9544 | 8797 | 7638 |
| 58 | 9542 | 9902 | 6449 | 8188 |
| 59 | 7638 | 7638 | 10868 | 5068 |
| 60 | 7852 | 8797 | 798 | 10868 |
| 61 | 8797 | 6449 | 6229 | 8976 |
| 62 | 9528 | 6437 | 7544 | 502 |
| 63 | 9625 | 6438 | 8976 | 7852 |
| 64 | 10174 | 4850 | 7852 | 798 |
| 65 | 13682 | 7852 | 5068 | 6229 |
| 66 | 6449 | 14159 | 502 | 7320 |
| 67 | 7250 | 5461 | 8965 | 7544 |
| 68 | 10427 | 8976 | 7329 | 13809 |
| 69 | 10083 | 502 | 7330 | 7329 |
| 70 | 6437 | 10174 | 10174 | 7330 |
| 71 | 6438 | 7329 | 4850 | 8142 |
| 72 | 6495 | 7330 | 7320 | 10174 |
| 73 | 6496 | 6499 | 617 | 8965 |
| 74 | 6499 | 6500 | 6499 | 9926 |
| 75 | 6500 | 617 | 6500 | 617 |
| 76 | 8187 | 8187 | 5461 | 1368 |
| 77 | 9527 | 7250 | 8187 | 7984 |
| 78 | 502 | 6495 | 13809 | 7561 |
| 79 | 617 | 6496 | 4158 | 6499 |
| 80 | 7329 | 5068 | 6495 | 6500 |
| 81 | 7330 | 9527 | 6496 | 9050 |
| 82 | 9902 | 9528 | 7561 | 8971 |
| 83 | 8976 | 7561 | 7250 | 4850 |
| 84 | 8323 | 18614 | 1368 | 8187 |
| 85 | 8324 | 7320 | 7984 | 9367 |
| 86 | 7561 | 13682 | 9527 | 5461 |
| 87 | 8155 | 8155 | 8155 | 10132 |
| 88 | 9543 | 8323 | 8971 | 7250 |
| 89 | 9544 | 8324 | 9050 | 10573 |
| 90 | 4756 | 7984 | 10132 | 6495 |
| 91 | 5068 | 9625 | 11672 | 6496 |
| 92 | 7984 | 13809 | 9367 | 11672 |
| 93 | 8186 | 1368 | 9528 | 9286 |
| 94 | 1268 | 9905 | 8323 | 8155 |
| 95 | 1368 | 9906 | 8324 | 9270 |
| 96 | 3817 | 10132 | 8142 | 885 |
| 97 | 3818 | 8971 | 9286 | 1665 |
| 98 | 7320 | 11672 | 9905 | 9527 |
| 99 | 4794 | 4756 | 9906 | 6574 |
| 100 | 14647 | 885 | 9270 | 418 |

Table 5-9. Bridge Rankings for Scenario II, ADT Factor $=0.3$, Detour Factor $=0,0.1,0.2,0.3$

|  | (no Detour) ADT 30\% | ADT 30\%, Detour 10\% | ADT 30\%, Detour 20\% | ADT 30\%, Detour 30\% |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Senario II $(40,30,20,10)$ | (0エ'0て'0 $\varepsilon^{\prime} 0 t$ ) ІІ оฺฺеuәs |  |
| Rank | BIN | BIN | BIN | BIN |
| 1 | 1841 | 1841 | 1841 | 1841 |
| 2 | 529 | 529 | 529 | 529 |
| 3 | 2736 | 2736 | 2736 | 2736 |
| 4 | 635 | 635 | 635 | 1842 |
| 5 | 1842 | 1842 | 1842 | 635 |
| 6 | 504 | 7608 | 7608 | 7608 |
| 7 | 7608 | 504 | 2037 | 2037 |
| 8 | 2037 | 2037 | 504 | 504 |
| 9 | 981 | 3202 | 3202 | 3202 |
| 10 | 34 | 1765 | 89 |  |
| 11 | 3202 | 89 | 1765 | 503 |
| 12 | 1765 | 9818 | 503 | 1765 |
| 13 | 503 | 503 | 4507 | 4507 |
| 14 | 1798 | 4507 | 1394 | 1394 |
| 15 | 4507 | 1798 | 19818 | 784 |
| 16 | 4947 | 1394 | 784 | 1798 |
| 17 | 5618 | 784 | 1798 | 4975 |
| 18 | 1394 | 4975 | 4975 | 19812 |
| 19 | 4975 | 4947 | 474 | 474 |
| 20 | 2534 | 474 | 4947 | 4947 |
| 21 | 18612 | 5618 | 5618 | 2534 |
| 22 | 784 | 18612 | 2534 | 9367 |
| 23 | 944 | 2534 | 944 | 502 |
| 24 |  | 944 | 9367 | 5618 |
| 25 | 474 |  | 502 | 10132 |
| 26 | 18614 | 502 | 10132 | 944 |
| 27 | 615 | 10132 |  | 1368 |
| 28 | 770 | 9367 | 18612 | 615 |
| 29 | 798 | 1368 | 1368 |  |
| 30 | 502 | 615 | 615 | 770 |
| 31 | 10132 | 770 | 770 | 5816 |
| 32 | 1368 | 885 | 885 | 885 |
| 33 | 10083 | 1665 | 1665 | 1665 |
| 34 | 617 | 2712 | 5816 | 12793 |
| 35 | 9367 | 2627 | 2712 | 6473 |
| 36 | 885 | 4658 | 12793 | 4658 |
| 37 | 107 | 107 | 4658 | 2712 |
| 38 | 1665 | 798 | 6473 | 10493 |
| 39 | 2627 | 5816 | 2627 | 6588 |
| 40 | 2712 | 12793 | 6588 | 7365 |
| 41 | 3130 | 6473 | 107 | 2627 |
| 42 | 4658 | 10102 | 7365 | 10102 |
| 43 | 1268 | 6588 | 798 | 18612 |
| 44 | 3817 | 7365 | 10102 | 07 |
| 45 | 3818 | 617 | 10493 | 798 |
| 46 | 12793 | 4994 | 4994 | 4994 |
| 47 | 5816 | 3130 | 617 | 617 |
| 48 | 2035 | 10493 | 8648 | 8648 |
| 49 | 8060 | 18614 | 5430 | 5430 |
| 50 | 10033 | 3817 | 3817 | 14407 |


| 51 | 10034 | 3818 | 3818 | 2035 |
| :---: | :---: | :---: | :---: | :---: |
| 52 | 10102 | 1268 | 3130 | 3817 |
| 53 | 10493 | 8648 | 1268 | 3818 |
| 54 | 10641 | 8060 | 14407 | 476 |
| 55 | 6473 | 5430 | 2035 | 10641 |
| 56 | 6588 | 10083 | 476 | 486 |
| 57 | 7365 | 476 | 8060 | 2273 |
| 58 | 4994 | 486 | 18614 | 1268 |
| 59 | 8648 | 14407 | 486 | 1695 |
| 60 | 5430 | 2035 | 10641 | 1739 |
| 61 | 2273 | 1739 | 1739 | 880 |
| 62 | 476 | 1917 | 1695 | 8060 |
| 63 | 486 | 1918 | 2253 | 2253 |
| 64 | 1717 | 10641 | 1917 | 8134 |
| 65 | 1739 | 1911 | 1918 | 3130 |
| 66 | 1917 | 1695 | 2013 | 2013 |
| 67 | 1918 | 1717 | 2868 | 2550 |
| 68 | 2566 | 2253 | 1897 | 1897 |
| 69 | 2567 | 2013 | 1898 | 1898 |
| 70 | 5977 | 5977 | 1664 | 1664 |
| 71 | 1911 | 1897 | 1911 | 1917 |
| 72 | 271 | 1898 | 2273 | 1918 |
| 73 | 843 | 1664 | 8134 | 1613 |
| 74 | 915 | 1613 | 2550 | 2666 |
| 75 | 1029 | 2666 | 1613 | 1911 |
| 76 | $107 / 2$ | 271 | 2666 | 271 |
| 77 | 1273 | 915 | 271 | 2682 |
| 78 | 1274 | 1273 | 915 | 915 |
| 79 | 1275 | 1274 | 1273 | 9044 |
| 80 | 1276 | 1275 | 1274 | 1273 |
| 81 | 1277 | 1276 | 1275 | 1274 |
| 82 | 1442 | 2566 | 1276 | 1275 |
| 83 | 1613 | 2567 | 6062 | 1276 |
| 84 | 1664 | 6062 | 2320 | 6062 |
| 85 | 1695 | 2320 | 1717 | 8133 |
| 86 | 1797 | 10033 | 2682 | 2320 |
| 87 | 1897 | 10034 | 1277 | 5006 |
| 88 | 1898 | 1277 | 10033 | 3033 |
| 89 | 2013 | 2588 | 10034 | 1277 |
| 90 | 2108 | 1442 | 5977 | 9229 |
| 91 | 2253 | 2408 | 2588 | 2588 |
| 92 | 2320 | 2861 | 1442 | 1442 |
| 93 | 2408 | 5222 | 2408 | 2408 |
| 94 | 2588 | 2550 | 3033 | 5603 |
| 95 | 2666 | 2695 | 5222 | 3024 |
| 96 | 2695 | 8134 | 3024 | 7766 |
| 97 | 3899 | 1029 | 2695 | 9444 |
| 98 | 4333 | 2682 | 9044 | 1717 |
| 99 | 5222 | 3033 | 8133 | 10033 |
| 100 | 5973 | 2108 | 5006 | 10034 |

Table 5-10. Bridge Rankings for Scenario III, ADT Factor $=0.3$, Detour Factor $=0,0.1,0.2,0.3$

|  | (no Detour) ADT 30\% | ADT 30\%, Detour 10\% | ADT 30\%, Detour 20\% |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | $\text { Senario III }(40,30,15,15)$ | (ST'ST'0 $\varepsilon^{\prime} 0 \downarrow$ ) III O!меuas | Senario III $(40,30,15,15)$ |
| Rank | BIN | BIN | BIN | BIN |
| 1 | 1841 | 1841 | 1841 | 1841 |
| 2 | 529 | 529 | 529 | 529 |
| 3 | 2736 | 2736 | 2736 | 2736 |
| 4 | 635 | 635 | 635 | 1842 |
| 5 | 1842 | 1842 | 1842 | 635 |
| 6 | 504 | 7608 | 7608 | 7608 |
| 7 | 7608 | 504 | 2037 | 2037 |
| 8 | 2037 | 2037 | 504 | 504 |
| 9 | 9818 | 3202 | 3202 | 3202 |
| 10 |  | 1765 |  |  |
| 11 | 3202 | 20n | 1765 | 1765 |
| 12 | 1765 | 981 | 503 | 503 |
| 13 | 503 | 503 | 784 | 784 |
| 14 | 1798 | 4507 | 4507 | 4507 |
| 15 | 4507 | 784 | 1981 | 1394 |
| 16 | 4947 | 1798 | 1798 | 1798 |
| 17 | 5618 | 1394 | 1394 | 10493 |
| 18 | 4975 | 4975 | 4975 | 981 |
| 19 | 784 | 4947 | 4947 | 4975 |
| 20 | 1394 | 18612 | 474 | 9367 |
| 21 | 18612 | 5618 | 10493 | 4947 |
| 22 | 2534 | 474 | 2534 | 2534 |
| 23 | 944 | 2534 | 5618 | 10132 |
| 24 |  | 944 | 9367 | 474 |
| 25 | Sea | 9367 | 10132 | 14407 |
| 26 | 18614 | 10132 | 944 | 944 |
| 27 | 10493 |  | 18612 | 502 |
| 28 | 502 | 10493 | 502 | 5618 |
| 29 | 10132 | 502 |  | 1368 |
| 30 | 9367 | 1368 | 14407 |  |
| 31 | 615 | 885 | 1368 | 5816 |
| 32 | 770 | 1665 | 885 | 12793 |
| 33 | 798 | 14407 | 5816 | 885 |
| 34 | 2035 | 2712 | 1665 | 6473 |
| 35 | 10033 | 4658 | 12793 | 1665 |
| 36 | 10034 | 5816 | 4658 | 4658 |
| 37 | 10641 | 12793 | 6473 | 18612 |
| 38 | 14407 | 2627 | 2712 | 2712 |
| 39 | 1368 | 107 | 6588 | 6588 |
| 40 | 885 | 6473 | 7365 | 615 |
| 41 | - | 6588 | 615 | 7365 |
| 42 | 1665 | 7365 | 2627 | 770 |
| 43 | 2627 | 10102 | 10102 | 2035 |
| 44 | 2712 | 615 | 770 | 10102 |
| 45 | 3130 | 770 | 101 | 4994 |
| 46 | 10083 | 4994 | 4994 | 2627 |
| 47 | 4658 | 798 | 2035 | 10 |
| 48 | 617 | 3130 | 798 | 2273 |
| 49 | 12793 | 18614 | 617 | 10641 |
| 50 | 2273 | 617 | 10641 | 798 |


| 51 | 5816 | 2035 | 2273 | 617 |
| :---: | :---: | :---: | :---: | :---: |
| 52 | 10102 | 10641 | 3130 | 8648 |
| 53 | 6473 | 3817 | 8648 | 5430 |
| 54 | 6588 | 3818 | 5430 | 1901 |
| 55 | 7365 | 1268 | 18614 | 476 |
| 56 | 4994 | 8648 | 3817 | 3817 |
| 57 | 1268 | 2273 | 3818 | 3818 |
| 58 | 3817 | 5430 | 1268 | 8134 |
| 59 | 3818 | 8060 | 476 | 486 |
| 60 | 8060 | 10033 | 10033 | 3130 |
| 61 | 8648 | 10034 | 10034 | 288 |
| 62 | 5430 | 10083 | 8060 | 1268 |
| 63 | 10690 | 476 | 486 | 1695 |
| 64 | 476 | 486 | 8134 | 10690 |
| 65 | 486 | 10690 | 10690 | 2253 |
| 66 | 1901 | 1739 | 1901 | 1739 |
| 67 | 1387 | 8134 | 1739 | 2550 |
| 68 | 1717 | 1917 | 1695 | 2013 |
| 69 | 1739 | 1918 | 2253 | 10033 |
| 70 | 1917 | 1911 | 86 | 10034 |
| 71 | 1918 | 1695 | 2013 | 1897 |
| 72 | 2566 | 2253 | 1917 | 1898 |
| 73 | 2567 | 2013 | 1918 | 1664 |
| 74 | 5977 | 1717 | 1897 | 9044 |
| 75 | 1911 | 1897 | 1898 | 8060 |
| 76 | 1709 | 1898 | 2550 | 1917 |
| 77 | 271 | 1664 | 1664 | 1918 |
| 78 | 843 | 5977 | 1911 | 8133 |
| 79 | 915 | 1613 | 1613 | 5006 |
| 80 | 1029 | 2666 | 2666 | 2682 |
| 81 | 107 | 271 | 271 | 10428 |
| 82 | 1273 | 915 | 2682 | 1613 |
| 83 | 1274 | 88 | 915 | 2666 |
| 84 | 1275 | 1273 | 1273 | 271 |
| 85 | 1276 | 1274 | 1274 | 1911 |
| 86 | 1277 | 1275 | 1275 | 9229 |
| 87 | 1442 | 1276 | 1276 | 915 |
| 88 | 1613 | 6062 | 6062 | 18614 |
| 89 | 1664 | 2320 | 2320 | 5603 |
| 90 | 1695 | 2550 | 9044 | 1273 |
| 91 | 1797 | 1277 | 8133 | 1274 |
| 92 | 1897 | 2566 | 1277 | 1275 |
| 93 | 1898 | 2567 | 1717 | 1276 |
| 94 | 2013 | 2588 | 3033 | 6062 |
| 95 | 2108 | 1442 | 5006 | 9444 |
| 96 | 2253 | 2408 | 2588 | 3033 |
| 97 | 2320 | 5222 | 1442 | 2320 |
| 98 | 2408 | 2682 | 2408 | 7766 |
| 99 | 2588 | 2695 | 5977 | 7630 |
| 100 | 2666 | 3033 | 9229 | 7631 |

## Descriptive Results (Scenarios)

The next step in the analysis will employ ADT and detour at $30 \%$ and $20 \%$ respectively to describe the behavior of the individual deficiencies (load, condition, width, and vertical clearance). This behavior makes use of three dimensional graphs to visually observe the performance of the individual deficiencies from the first structure to structure 100. All four runs (ALDOT, Scenario I, Scenario II, Scenario III) are displayed as Figures 5-1, 5-2, 5-3, and 5-4.

Viewing Figures 5-1, 5-2, 5-3, and 5-4, the first observation is that based on a 100 point scale (without ADT or detour factor applied) the total deficiency points decrease to less than $50 \%$ of the possible value within 15 structures. The majority of this behavior is due to the elimination of load deficient structures early in the process. Load deficiency possesses $40 \%$ of the weight in all the scenarios; therefore, the behavior is the same for all iterations.

ALDOT Load and condition deficiency are the drivers for the first 30 structures. The first 10 structures are near or at the maximum number of possible deficiency points for load with the discriminator being the condition deficiency (decreases with every structure for the first 10 bridges). An important observation is the relationship with load and condition; the two measures appear to have a negative correlation. The relationship, with the exception of a few structures, either has a high load deficiency or a high condition deficiency but rarely have both present (which may indicate a bridge with a poor condition and has been posted to preserve its state).

Structures 30 to 100 have condition as the main contributor to the total deficiency since all load deficient structures have been identified in the initial set of 30 bridges. Width contributes to all 100 structures with varying levels of deficiency.

The width deficiency is a much more strenuous calculation compared to previous formulas and appears in most bridge deficiencies with few zero entries. The result of this adjusted calculation appears to have increased the baseline of the width deficiency. By observing the ALDOT graph and the subsequent scenarios, the width deficiency line is averaging 10 deficiency points with a few spikes to the maximum value ( 10 points coupled with an ADT factor). This negates some of the influence of the width deficiency since its average is has an almost uniform increase in all the structures scores.

Vertical clearance has little effect on the model, the instances of vertical are few and therefore the majority of the entries are zero.

Scenario I (40, 20, 20, 20) This scenario deviates the greatest amount from the contemporary ALDOT weighting. The behavior of load remains the same at $40 \%$ and allows load to drive the model again in the first 30 structures. Condition is at $20 \%$ weight and reduces its emphasis in the model (allowing width, vertical clearance, and condition to have equal influence). The result is a more balanced model when comparing the three variables. Width has a more uniform presence, while condition and vertical clearance compete for position (a negative correlation type behavior). This method also generates the most diverse raking when compared to ALDOT and the remaining two scenarios. This variety is due to the structures with vertical clearance are
allowed to vie against condition equally and therefore brings more vertical clearance deficient structure to the foreground.

One limitation to this scenario is the equal impact of the three variables (condition, width, and vertical clearance). The actual priority of these variables may be skewed as a structure with a high vertical clearance and width deficiency (an older structure for example) may mask a structure with a poor condition.

Scenario II (40, 30, 20, 10) The step weighting approach for Scenario II can be viewed as a priority scale. Load and condition takes $40 \%$ and $30 \%$ of the total deficiency score, respectively. This portion of the bridge deficiency can be considered the "health" of the structure and therefore takes the majority of the weight.

Width is the next highest weighting with $20 \%$ of the total deficiency. Width has been discussed as a safety concern and a possible contributor to accidents in and around bridges when it is less than accommodating to present standards. The safety aspect and new building standards, while important to safety and meeting current construction goals, are not as detrimental to the structure (when compared to load and condition). This weighting allows width to have more influence in this model but not overshadow the importance of load and condition.

Vertical clearance has few instances throughout the population and therefore allowing it to remain at $10 \%$ will allow it to have influence and discriminate tie within like structures.

Scenario III $(\mathbf{4 0}, \mathbf{3 0}, \mathbf{1 5}, \mathbf{1 5})$ Scenario III is a derivation of Scenario II. The difference is width and vertical clearance split the remaining $30 \%$ of the weight evenly. This approach allows vertical clearance (which has few instances) to have the same amount of influence as the width deficiency. The results are similar to Scenario II. The major difference is the level which width and vertical clearance can maximize when an extreme condition is present. Width is confined to a lower maximum score but is still uniform in nature and a few of the vertical clearance deficiencies meet the higher threshold.


Figure 5-1. Deficiency points for each of 100 most-deficient bridges: ALDOT current weights.


Figure 5-2. Deficiency points for each of 100 most-deficient bridges: Scenario I.


Figure 5-3. Deficiency points for each of 100 most-deficient bridges: Scenario II.


Figure 5-4. Deficiency points for each of 100 most-deficient bridges: Scenario III.

## Research Recommendations

Based on the results discussed above, specific values for the ADT and detour factors and for the load, condition, width, and vertical clearance weights are presented in the following section. And finally, a recommendation to update these factors and weights as the bridge population changes is discussed.

## Recommended Factors and Weights

ADT and detour factors can be set at $30 \%$ and $20 \%$ respectively. (See ADT and Detour Factors in Chapter 5 for a thorough explanation.) Scenario II gives a best fit, where the major factors to a structure's "health" (load and condition) are given the majority of the weight. Load is given a $10 \%$ gain over condition, accommodating the impact of certain vehicles types having to divert to another structure. (This can be viewed as an economic impact.) This difference is important with the calculation that is used to compute the condition deficiency.

Condition deficiency is given $30 \%$ total points with the caveat that as more components (deck, superstructure, substructure) reach threshold values this score can exceed the 30 points (prior to ADT factoring). Condition has $30 \%$ of the weight; it becomes the next most important driver after the load deficient structures are eliminated in approximately the first year. Condition deficient structures can lead to postings and closures; therefore, the priority placed on condition is commensurate to its weighting.

Width is increased from its current $10 \%$ contribution to $20 \%$. The increase allows width to take into effect the more stringent criteria to determine width deficiency, which is becoming a priority within ALDOT. The benefit of using $20 \%$ as opposed to a higher and more equal rating with load and condition is to prevent a width deficient structure from becoming an equal priority with other structures with a load or condition deficiency. The concept to replace a bridge that is only exhibiting a width deficiency is rare, and therefore should be considered a "multiplier" to the total deficiency to elevate a structure that may be tied with other structures.

The instances of vertical clearance deficient structures in the inventory are low. The calculation also presents structures that are not a clearance constraint to themselves but may create a clearance constraint to a structure below the crossing (a bridge crossing over a road may cause a clearance restriction on that road while the bridge is otherwise fully functional). This may present a false representation if the route being crossed by the structure is not under the same constraints that are being used to calculate the current ranking. Leaving the vertical clearance weighting low will not convolute the ranking but will allow recognition of a possible vertical clearance deficiency.

## Dynamic Adjustment

The situation that all the scenarios and the current ALDOT model display is the removal of the load deficient structures early in the process. This adjusted weighting from the 1991 research should not be considered a static weighting. As the load deficient structures are eliminated from the pool of possible candidates, this process should be repeated to best accommodate and reflect
the demographics of the remaining inventory. Additionally, the current ADT numbers within the database may not reflect the true "possible" ADT numbers if a structure were not posted. The ADT measure is the current number of vehicles utilizing the structure, not taking into account the amount of traffic that is being diverted due to its limited capacity.

### 6.0 Conclusions and Recommendations

## Objective and Scope of this Project

During validation of the 1991 ALDOT deficiency algorithm, the following comments were made by division bridge inspectors and county engineers:

- The ADT factor should be decreased.
- The inventory rating (the measure of load capacity used by the 1991 algorithm) does not reflect the effects of strengthening; perhaps only load-posted bridges should receive deficiency points.
- Especially narrow bridges should receive more deficiency points.
- Bridges with scour problems should receive deficiency points.
- The ADT numbers for county routes were not always accurate.

The deficiency algorithm developed in 1991 was used by ALDOT managers to select bridges for the bridge replacement program. Comments from these managers regarding the algorithm include:

- Not enough deficiency points were assigned to very narrow bridges.
- Deficiency points were not assigned to culverts.
- Load capacity was represented by inventory rating, but bridges are posted for load restrictions based on operating ratings.
- The goals for load capacity, width, and vertical clearance were not stringent enough.
- The goals and weight factors should be easy to update (without modifying the source code of the program).
- The deficiency equations were not intuitive (i.e. simple and based on a bridge's physical characteristics).

Every one of the "shortcomings" pointed out in the comments from the division bridge inspectors, the county engineers, and the ALDOT managers has been addressed in the revised algorithm presented in this report.

It is important to mention that this project only updated the deficiency algorithm for state-owned bridges. The population of state-owned bridges is very different from the population of locallyowned bridges (county, municipal, etc.), and the procedures for replacing state-owned bridges are different than the procedures for replacing locally-owned bridges. This is significant because the primary use of the deficiency algorithm is to help select bridges for replacement. This report was written to provide information useful for developing a similar algorithm for locally-owned bridges.

## Principles of Algorithm Development

The preceding sections describe the mechanics of the new algorithm and document its validation. Lacking is a discussion of the bridge deficiency principles that evolved during algorithm development.

- Principle: One major deficiency should outweigh several minor deficiencies.
o Rational: Major deficiencies have an urgency that minor deficiencies do not. Therefore, a bridge with one major deficiency should be ranked higher than a bridge with several minor deficiencies.
o Implementation: Deficiency points are assigned aggressively for the major deficiencies to create a "gap" between the major and the intermediate deficiencies. For example, a bridge with a posted maximum load of 10 tons (restricted to all bus and truck traffic) is assigned 40 deficiency points while a bridge with a condition rating of 4 , no shoulders, and a vertical clearance of only 16.5 feet is assigned 35 deficiency points.
- Principle: Load ratings and condition ratings are the most meaningful indicators of bridge deficiency.
- Rational: Both of these data items are based on a synthesis of many pieces of information by an experienced load rating engineer or bridge inspector. And both data items can trigger ALDOT actions: low load ratings lead to bridge posting, and low condition ratings (condition rating of three or four) lead to notification of superiors and other actions.
- Implementation: Deficiency points are only assigned to bridges with load ratings and condition ratings that trigger ALDOT actions: i.e. for posted bridges and for condition ratings equal to three or four. The majority of the possible deficiency points are assigned to these two data items (up to 40 points for load ratings and up to 60 points (rare) for poor condition ratings).
- Principle: ADT should affect deficiency points in moderation.
- Rational: Take the case of two bridges with identical characteristics and therefore equal deficiency points. One bridge has very high traffic and the other only average traffic. Replacement of the high-traffic bridge is more urgent than replacement of the moderate traffic bridge, so the high-traffic bridge should therefore be assigned more deficiency points.

But, the ADT factor should not be so large that it causes a high-traffic bridge with a minor deficiency to outrank a low-traffic bridge with a major deficiency.

More controversial is the assertion that a low-traffic bridge should not be penalized, i.e. be assigned fewer deficiency points than an identical moderate-traffic bridge. Part of the argument supporting this assertion is that bridges on the state highway system should provide a minimum level of service, no matter what their traffic volume. Another part of the argument is that ADT does not reflect the type of traffic. For example a low-traffic bridge could carry school buses or log trucks, both important to the local community.

Implementation: The ADT factor is rather small, increasing the deficiency points for high-traffic bridges by a maximum of $30 \%$. The ADT factor is based on the percent rank of a bridge's ADT in the population of all state-owned bridges. Using percent rank as the basis for the ADT factor serves two purposes: (1) bridge deficiency rankings are adjusted based on traffic volume relative to the population under consideration and (2) there is no need to update the factor as the bridge population changes. (See Dynamic Adjustment in Chapter 5.)

## Algorithm Implementation

Once ALDOT managers approve the deficiency criteria and weights, the deficiency algorithm can be implemented on the Department's central computer. One of the comments made by a user of the 1991 algorithm, and a recommendation of this report, is to implement the deficiency algorithm so that the deficiency criteria, weights (deficiency points), and adjustment factors can be easily changed by an ALDOT manager, say the Bridge Maintenance Engineer. One method is to place the criteria, deficiency points, and adjustment factors in matrices, such as those shown in Figure 6-1 below.

|  |  | ---- - Criteria----- |  |  | ---- - Points ---- |  |  | ---- - Factors ---- |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Max. Defic. | Intermed. Defic. | No Defic. | Max. Defic. | Intermed. Defic. | No Defic. | ADT | ADTT | DL |
| SCHOOL_BUS | 1 | 1 | 0 | 0 | 30 | 0 | 0 | 0 | 0 | 0.1 |
| H_Truck | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2_AXLE_TRUCK | 3 | 1 | 0 | 0 | 20 | 0 | 0 | 0 | 0.3 | 0.1 |
| CONCRETE_Truck | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.1 |
| HS_Truck | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TRIAXLE_DUMP_Truck | 6 | 1 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0.1 |
| 18_WHEELER_Truck | 7 | 1 | 0 | 0 | 20 | 0 | 0 | 0 | 0.3 | 0.1 |
| 6_AXLE_Truck | 8 | 1 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0.1 |
| Operating Rating (tons) | 9 | 12.5 | 30 | 36 | 40 | 20 | 0 | 0 | 0.3 | 0.1 |
| Lowest Condition Rating | 10 | 3 | 4 | 5 | 30 | 20 | 0 | 0.3 | 0 | 0.1 |
| 2nd Lowest Condition Rating | 11 | 3 | 4 | 5 | 20 | 10 | 0 | 0.3 | 0 | 0.1 |
| 3rd Lowest Condition Rating | 12 | 3 | 4 | 5 | 10 | 5 | 0 | 0.3 | 0 | 0.1 |
| Lane Width | 13 | 10 | 12 | 12 | 20 | 10 | 0 | 0.3 | 0 | 0.1 |
| Shoulder Width | 14 | 0 | 0 | 10 |  |  |  |  |  |  |
| Height | 15 | 16 | 16.3 | 17 | 10 | 8 | 0 | 0 | 0.3 | 0.1 |

Figure 6-1. Criteria, deficiency points, and ADT/detour factor matrices for deficiency algorithm.

### 7.0 References

Richardson, J. and Turner, D., Development of Deficiency Point Algorithms for the Alabama Bridge Information Management System, Bureau of Engineering Research Report \#547-39, University of Alabama College of Engineering, 1991a, 49 pp.

Richardson, J. and Turner, D., Development of Deficiency Point Algorithms for the Alabama Bridge Information Management System (Executive Summary), Bureau of Engineering Research Report \#557-39, University of Alabama College of Engineering, 1991b, 16 pp.

## Appendix A: Decision Tree of Deficiency Algorithm

## INITIAL CALCULATIONS



Max_Load_Defic $=\operatorname{Pts}(9,1)^{*}(1+$ adt_factor $) *(1+$ DL_Factor $)$

LOAD DEFICIENCY
Function Interp $(y 1, y 2, x 1, x 2, x)$
Interp $=(y 2-y 1)(x 2-x 1) *(x-x 1)+y$
Function ADT_Mult (i_bridge, j_crit, ADT_Fac, perc_rank
ADT_Mult = 1
For K=1 to 3
ADT_Mult = ADT_Mult*(interp(1-ADT_Fac(j_crit,k), 1+ADT_Fac(j_crit, k), ,0,1,perc_rank(i_bridge, k))
Next K


ADT_Mult $\{2\}=\{i, j$, ADT_Fac, perc_rank_on) where $j=1$ to 8 respectfully
$\operatorname{Interp}\{1\}=\operatorname{Interp}(\operatorname{Pts}(9,-1), \operatorname{Pts}(9,2), \operatorname{Crit}(9,1), \operatorname{Crit}(9,2)$, op_rating(i))
$\operatorname{Interp}\{2\}=\operatorname{Interp}(\operatorname{Pts}(9,2), \operatorname{Pts}(9,3), \operatorname{Crit}(9,2), \operatorname{Crit}(9,3)$, op_rating(i))

Function $\operatorname{Interp}(y 1, y 2, x 1, x 2, x)$
Interp $=(y 2-y 1) /(x 2-x 1) *(x-x 1)+y 1$
Function ADT_Mult (i_bridge, i_crit, ADT_Fac, perc_rank)
ADT_Mult $=1$
For K=1 to 3
 Next K


ADT_Mult $\{1\}=\{i, 13$, ADT_Fac, perc_rank_on)
Interp\{1\} = Interp(Pts(13,1), Pts(13,2), Target_Width(1), Target_Width(2), Width_on(i))
$\operatorname{Interp}\{2\}=\operatorname{Interp}(\operatorname{Pts}(13,2), \operatorname{Pts}(13,3)$, Target_Width(2), Target_Width(3), Width_on(i))


CLEARANCE DEFICIENCY
Function Interp ( $\mathbf{y 1}, \mathrm{y} 2, \mathrm{x} 1, \mathrm{x} 2, \mathrm{x})$
nterp $=(y 2-y 1) /(x 2-x 1)^{*}(x-x 1)+y$
Function ADT_Mult (i ibridge, i_crit, ADT_Fac, perc_rank)
ADT_Mult $=1$
For $\mathrm{K}=1$ to 3
 Next K


ADT_Mult\{1\} = \{i,15, ADT_Fac, perc_rank_on)
ADT Mult 2 ? $=\left\{1,15\right.$ ADT ${ }^{-}$Fac perc
Interp\{1\} $=\operatorname{Interp}(\operatorname{Pts}(15,1), \operatorname{Pts}(15,2), \operatorname{Crit}(15,1), \operatorname{Crit}(15,2)$, Overclearance(i) $)$
$\operatorname{Interp}\{2\}=\operatorname{Interp}(\operatorname{Pts}(15,2), \operatorname{Pts}(15,3), \operatorname{Crit}(15,2), \operatorname{Crit}(15,3)$, Overclearance(i))

TOTAL DEFICIENCY


## Appendix B: Flow Chart of Deficiency Algorithm

## CALCULATE INITIALIZATION SCORES

These calculations are used throughout the program to determine deficiency values


## CALCULATE LOAD DEFICIENCY

HWY ON : calculated from INITIALIZATION
Posting_status: ABIMS variable
Op_rating: ABIMS variable
Crit(A,B): TABLE value
Load RF (A,B): TABLE value for bridge I
Pts(A,B): TABLE value
Function Interp(y1, y2, x1, x2, x)
Interp $=(y 2-y 1) /(x 2-x 1)^{*}(x-x 1)+y 1$
Function ADT_Mult (i_bridge, j_crit, ADT_Fac, perc_rank) ADT_Mult = 1 For $\bar{K}=1$ to 3 ADT_Mult = ADT_Mult*(interp(1-ADT_Fac(j_crit,k)
$1+A D T$ Fac(j_crit, k), 0,1 , perc rank(i bridge, $k)$ )) Next K


ADT Mult $\}=\{i, 9$, ADT Fac, perc rank on) where $i=$ Bridge ADT_Mult $\{2\}=\{i, j$, ADT_Fac, perc_rank_on) where $j=1$ to 8 respectfully Interp\{1\} $=\operatorname{Interp}(\operatorname{Pts}(9,1), \operatorname{Pts}(9,2), \operatorname{Crit}(9,1), \operatorname{Crit}(9,2)$, op_rating(i)) $\operatorname{Interp}\{2\}=\operatorname{Interp}(\operatorname{Pts}(9,2), \operatorname{Pts}(9,3), \operatorname{Crit}(9,2), \operatorname{Crit}(9,3)$, op_rating(i))

## CALCULATE LOAD (Subroutine for LOAD RF for 7 vehicles) called by

 LOAD DEFICIENCY$\operatorname{Crit}(A, B)$ : TABLE value

Function Interp( $\mathrm{y} 1, \mathrm{y} 2, \mathrm{x} 1, \mathrm{x} 2, \mathrm{x}$ )
Interp $=(y 2-y 1) /(x 2-x 1) *(x-x 1)+y 1$


## CALCULATE TOTAL CLEARANCE DEFICIENCY

## Calls SUBROUTINE CLEARANCE DEFICIENCY

Clearance: ABIMS variable
Span_type: ABIMS variable
HWY_ON: Calculated in INITIALIZATION
HWY_UNDER: Calculated in INITIALIZATION


CALCULATE CLEARANCE DEFICIENCY (Subroutine for "On" and "Under") called by TOTAL CLEARANCE DEFICIENCY
Clearance: ABIMS variable
Crit(A,B): TABLE value


## CALCULATE WIDTH DEFICIENCY

Lane_width: ABIMS variable or basic calculation
$\operatorname{Crit}(A, B)$ : TABLE value

Function Interp(y1, y2, x1, x2, x) Interp $=(y 2-y 1) /(x 2-x 1)^{*}(x-x 1)+y 1$

Function ADT_Mult (i_bridge, j_crit, ADT_Fac, perc_rank) ADT_Mult = 1
For $\bar{K}=1$ to 3
ADT_Mult = ADT_Mult* $($ interp(1-ADT_Fac(j_crit,k),
$1+$ ADT_Fac(j_crit, $k$ ), 0,1 , perc_rank(i_bridge, $k$ )) Next K


ADT_Mult\{1\} = \{i,13, ADT_Fac, perc_rank_on)
Interp $\{1\}=\operatorname{Interp}(\operatorname{Pts}(13,1), \operatorname{Pts}(13,2)$, Target_Width(1), Target_Width(2), Width_on(i)) Interp $\{2\}=\operatorname{Interp}(\operatorname{Pts}(13,2), \operatorname{Pts}(13,3)$, Target_Width(2), Target_Width(3), Width_on(i))

## CALCULATE CONDITION DEFICIENCY

Deck: ABIMS variable
Superstructure: ABIMS variable
Substructure: ABIMS variable
Culvert Condition: ABIMS variable
Crit(A,B): TABLE value
Function Interp( $\mathrm{y} 1, \mathrm{y} 2, \mathrm{x} 1, \mathrm{x} 2, \mathrm{x}$ ) Interp $=(y 2-y 1) /(x 2-x 1)^{*}(x-x 1)+y$


ADT_Mult\{1\} = \{i,j, ADT_Fac, perc_rank_on)
Where j represents (min condition 1,2,3 respectfully)

## CALCULATE TOTAL DEFICIENCY

Calculation Module Condition Deficiency
Calculation Module Clearance Deficiency
Calculation Module Load Deficiency
Calculation Module Width Deficiency


## Appendix C: Source Code for Deficiency Algorithm

The deficiency algorithm compares information in the bridge database against the appropriate criteria in the 15 -row by 3 -column "Criteria" matrix, assigns the points specified in the 15 -row by 3 -column "Pts" matrix, and multiplies by the factors in the 15 -row by 3 -column "Factors" matrix. (See Figure C-1.)

- Rational: Major deficiencies have an urgency that minor deficiencies do not. Therefore a bridge with one major deficiency should be ranked higher than a bridge with several minor deficiencies.

|  |  | Criteria |  |  | Pts |  |  | Factors |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ADT | ADTT | DL |  |  |  |
| SCHOOL_BUS | 1 |  |  |  | 1 | 0 | 0 | 30 | 0 | 0 | 0 | 0 | 0.1 |
| H_Truck | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2_AXLE_TRUCK | 3 | 1 | 0 | 0 | 20 | 0 | 0 | 0 | 0.3 | 0.1 |
| CONCRETE_Truck | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.1 |
| HS_Truck | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TRIAXLE_DUMP_Truck | 6 | 1 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0.1 |
| 18_WHEELER_Truck | 7 | 1 | 0 | 0 | 20 | 0 | 0 | 0 | 0.3 | 0.1 |
| 6_AXLE_Truck | 8 | 1 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0.1 |
| Operating Rating (tons) | 9 | 12.5 | 30 | 36 | 40 | 20 | 0 | 0 | 0.3 | 0.1 |
| Lowest Condition Rating | 10 | 3 | 4 | 5 | 30 | 20 | 0 | 0.3 | 0 | 0.1 |
| 2nd Lowest Condition Rating | 11 | 3 | 4 | 5 | 20 | 10 | 0 | 0.3 | 0 | 0.1 |
| 3rd Lowest Condition Rating | 12 | 3 | 4 | 5 | 10 | 5 | 0 | 0.3 | 0 | 0.1 |
| Lane Width | 13 | 10 | 12 | 12 | 20 | 10 | 0 | 0.3 | 0 | 0.1 |
| Shoulder Width | 14 | 0 | 0 | 10 |  |  |  |  |  |  |
| Height | 15 | 16 | 16.3 | 17 | 10 | 8 | 0 | 0 | 0.3 | 0.1 |

"ADT_Fac"
"Crit"
"Pts"
Figure C-1. Matrices used by deficiency algorithm.
The matrix names used in the source code are written at the bottom of the figure.

## Source Code:

Sub Calc_Defic()
Dim Target_Width(3)
max_Load_Defic $=\operatorname{Pts}(9,1) *(1+$ adt_factor $) *(1+$ DL_Factor $)$
For $\mathrm{i}=1$ To num_bridges
Select Case Service_On(i)
Case "Hwy", "Hwy-RR", "Hwy-Ped", "Overpass", "3rd level Overpass", "4th level Overpass" is_highway_on = True
Case Else is_highway_on = False
End Select

```
    Select Case Service_Under(i)
    Case "Hwy", "Hwy-RR", "Hwy-Water", "Hwy-Water-RR"
        is_highway_under = True
    Case Else
        is_highway_under = False
    End Select
'Calc Load Defic
Load_Defic \((\mathrm{i})=0\)
If is_highway_on And Posting_Status(i) = "P" Then
    If Load_RFs(i, 2) > 0 Then 'If Load Ratings exist for 8 std veh
        For \(\mathrm{j}=1\) To 8
        j_veh = veh_dir(j)
        If Load_RFs(i, j_veh) < Crit( \(\mathrm{j}, 1\) ) Then
            Load_Defic(i) \(=\) Load_Defic(i) \(+\operatorname{Pts}(\mathrm{j}, 1) *\) ADT_Mult(i, j, ADT_Fac, perc_rank_on,
ADT_Factor_gt_1)
            Select Case j
            Case Is = 1
                Bridge_Count(i, 6) \(=1\)
            Case Is = 3
                    Bridge_Count(i, 7) \(=1\)
            Case Is = 7
                Bridge_Count(i, 8 ) = 1
            Case Else
                Bridge_Count(i, 9) = 1
            End Select
            End If
        Next j
    Else
        Select Case op_rating(i)
            Case Is < Crit \((9,1)\)
            Load_Defic(i) \(=\operatorname{Pts}(9,1)\)
            Bridge_Count(i, 2) = 1
            Case Is <= Crit( 9,2 )
                Load_Defic(i) \(=\operatorname{interp}(\operatorname{Pts}(9,1), \operatorname{Pts}(9,2), \operatorname{Crit}(9,1), \operatorname{Crit}(9,2)\), op_rating(i))
                Bridge_Count \((\mathrm{i}, 3)=1\)
            Case Is < Crit \((9,3)\)
            Load_Defic(i) \(=\operatorname{interp}(\operatorname{Pts}(9,2), \operatorname{Pts}(9,3), \operatorname{Crit}(9,2), \operatorname{Crit}(9,3)\), op_rating(i))
            Bridge_Count(i, 4) = 1
            End Select
            Load_Defic(i) = Load_Defic(i) * ADT_Mult(i, 9, ADT_Fac, perc_rank_on,
ADT_Factor_gt_1)
    End If
    If Load_Defic(i) > max_Load_Defic Then Load_Defic(i) = max_Load_Defic
End If
```

```
'Calc Condition Defic
    min_con = 0
    Cond_Defic(i) \(=0\)
    For \(\mathrm{j}=10\) To 12
    min_con = min_con +1
    Select Case Min_Conds(i, min_con)
    Case Is <= Crit(j, 1)
        Cond_Defic(i) \(=\) Cond_Defic(i) \(+\operatorname{Pts}(\mathrm{j}, 1) *\) ADT_Mult(i, j, ADT_Fac, perc_rank_on,
ADT_Factor_gt_1)
        Bridge_Count \((\mathrm{i}, 11)=\) Bridge_Count \((\mathrm{i}, 11)+1\)
        Case Is = Crit( \(\mathrm{j}, 2\) )
        Cond_Defic(i) = Cond_Defic(i) + Pts(j, 2) * ADT_Mult(i, j, ADT_Fac, perc_rank_on,
ADT_Factor_gt_1)
            Bridge_Count(i, 12) = Bridge_Count(i, 12) + 1
            Case Is = Crit( \(\mathrm{j}, 3\) )
                Cond_Defic(i) = Cond_Defic(i) + Pts(j, 3) * ADT_Mult(i, j, ADT_Fac, perc_rank_on,
ADT_Factor_gt_1)
            Bridge_Count(i, 13) \(=\) Bridge_Count(i, 13) +1
        End Select
    Next j
'Calc Bridge Width Defic
Width_Defic(i) \(=0\)
If is_highway_on And num_lanes(i) >0 Then
    Select Case Direc_Traffic(i)
    Case Is = "1-lane"
        shoulder_multiplier = 1
    Case Is = "2-way"
        shoulder_multiplier \(=2\)
    Case Is = "1-way"
        shoulder_multiplier \(=1+0.6\)
End Select
For \(\mathrm{j}=1\) To 3
    Target_Width \((\mathrm{j})=\operatorname{Crit}(13, \mathrm{j}) *\) num_lanes \((\mathrm{i})+\operatorname{Crit}(14, \mathrm{j}) *\) shoulder_multiplier
Next j
Select Case Width_on(i)
    Case Is =0 'Error in Database
        Width_Defic(i) = 0
    Case Is <= Target_Width(1)
        Width_Defic(i) \(=\operatorname{Pts}(13,1)\)
        Bridge_Count(i, 15) = 1
    Case Is <= Target_Width(2)
```

Width_Defic(i) $=\operatorname{interp}(\operatorname{Pts}(13,1), \operatorname{Pts}(13,2)$, Target_Width(1), Target_Width(2), Width_on(i))

Bridge_Count $(\mathrm{i}, 16)=1$
Case Is < Target_Width(3)
Width_Defic(i) $=\operatorname{interp}(\operatorname{Pts}(13,2), \operatorname{Pts}(13,3)$, Target_Width(2), Target_Width(3), Width_on(i))

Bridge_Count(i, 17) = 1
End Select
Width_Defic(i) = Width_Defic(i) * ADT_Mult(i, 13, ADT_Fac, perc_rank_on, ADT_Factor_gt_1)
End If
If Direc_Traffic(i) = "1-lane" And num_lanes(i) <> 1 Then Width_Defic(i) = 0 'Error in Database
'Calc Vertical Clearance Defic
Vert_Clear_Defic(i) = 0
'Check OverClearance
Select Case Span_Type(i)
Case "Truss -Thru", "Arch -Thru", "Movable -Lift", "Movable -Bascule", "Movable -Swing", "Tunnel"
is_poss_overclearance_restricted_structure = True
Case Else
is_poss_overclearance_restricted_structure $=$ False
End Select
If Overclearance(i) <> 0 And is_highway_on And is_poss_overclearance_restricted_structure Then

Select Case Overclearance(i)
Case Is < Crit $(15,1)$
temp $=\operatorname{Pts}(15,1) *$ ADT_Mult(i, 15, ADT_Fac, perc_rank_on, ADT_Factor_gt_1)
Bridge_Count(i, 19) = 1
Case Is <= Crit(15, 2)
temp $=\operatorname{interp}(\operatorname{Pts}(15,1), \operatorname{Pts}(15,2), \operatorname{Crit}(15,1), \operatorname{Crit}(15,2)$, Overclearance(i))
Bridge_Count(i, 20) = 1
Case Is < Crit(15, 3)
temp $=\operatorname{interp}(\operatorname{Pts}(15,2), \operatorname{Pts}(15,3), \operatorname{Crit}(15,2), \operatorname{Crit}(15,3)$, Overclearance(i))
Bridge_Count(i, 21) = 1
Case Else
temp $=0$
End Select
Vert_Clear_Defic(i) = temp * ADT_Mult(i, 15, ADT_Fac, perc_rank_on, ADT_Factor_gt_1)
End If
'Check UnderClearance
If Span_Type(i) <> "Tunnel" And Span_Type(i) <> "Culvert" Then
is_poss_underclearance_restricted_structure = True
Else

```
    is_poss_underclearance_restricted_structure = False
    End If
    If Underclearance(i) <> 0 And is_highway_under And
is_poss_underclearance_restricted_structure Then
    Select Case Underclearance(i)
        Case Is < Crit \((15,1)\)
        temp \(=\operatorname{Pts}(15,1)\) * ADT_Mult(i, 15, ADT_Fac, perc_rank_on, ADT_Factor_gt_1)
        Bridge_Count \((\mathrm{i}, 19)=\) Bridge_Count \((\mathrm{i}, 18)+1\)
        Case Is <= Crit \((15,2)\)
        temp \(=\operatorname{interp}(\operatorname{Pts}(15,1), \operatorname{Pts}(15,2), \operatorname{Crit}(15,1), \operatorname{Crit}(15,2)\), Underclearance(i))
        Bridge_Count(i, 20) \(=\) Bridge_Count(i, 19) +1
    Case Is < Crit \((15,3)\)
        temp \(=\operatorname{interp}(\operatorname{Pts}(15,2), \operatorname{Pts}(15,3), \operatorname{Crit}(15,2), \operatorname{Crit}(15,3)\), Underclearance(i))
        Bridge_Count( \(\mathrm{i}, 21\) ) \(=\) Bridge_Count \((\mathrm{i}, 20)+1\)
        Case Else
        temp \(=0\)
    End Select
    Vert_Clear_Defic(i) = Vert_Clear_Defic(i) + temp * ADT_Mult(i, 15, ADT_Fac,
perc_rank_under, ADT_Factor_gt_1)
    End If
    Total_Defic(i).Value = Load_Defic(i) + Cond_Defic(i) + Width_Defic(i) + Vert_Clear_Defic(i)
Next i
'Set closed bridges to max defic
If Range("Set_Closed_to_Max_Defic") Then
    max_defic = WorksheetFunction.Max(Total_Defic)
    For \(\mathrm{i}=1\) To num_bridges
    If Posting_Status(i) = "K" Then
        Bridge_Count(i, 1) = 1
        Select Case Service_On(i)
        Case "Hwy", "Hwy-RR", "Hwy-Ped", "Overpass", "3rd level Overpass", "4th level
Overpass"
            Total_Defic(i) = max_defic
        End Select
        End If
    Next i
End If
col_num = WorksheetFunction.Match("Total_Defic", Range("Headings"), 0)
All_Defic_Data.sort , Key1:=All_Defic_Data.Columns(col_num), Order1:=xlDescending
'Find last bridge with deficiencies
i = num_bridges
Do While Total_Defic \((\mathbf{i})=0\)
```

$$
\mathrm{i}=\mathrm{i}-1
$$

Loop
num_defic_bridges.Value = i
For $\mathrm{i}=1$ To num_defic_bridges
$\operatorname{Rank}(\mathrm{i})$. Value $=\mathrm{i}$
Next i
End Sub

Function ADT_Mult(i_bridge, j_Crit, ADT_Fac, perc_rank, ADT_Factor_gt_1)
ADT_Mult $=1$
Fork $=1$ To 3
ADT_Mult = ADT_Mult * (interp(1-ADT_Fac(j_Crit, k), $1+$ ADT_Fac(j_Crit, k), 0, 1, perc_rank(i_bridge, k)))
Next k

If ADT_Factor_gt_1 Then
If ADT_Mult < 1 Then ADT_Mult = 1
End If
End Function
Function interp $(\mathrm{y} 1, \mathrm{y} 2, \mathrm{x} 1, \mathrm{x} 2, \mathrm{x})$
interp $=(y 2-y 1) /(x 2-x 1) *(x-x 1)+y 1$
End Function

