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Final Report

## Analysis of VASCAR

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16. Abstract

This study is part of an effort by the National Highway Traffic Safety Administration (NHTSA) to determine the accuracy of the VASCAR-plus speed measurement device. VASCAR-plus is used extensively for speed law enforcement by state and local police. VASCAR-plus calculates average speed using the basic formula: Speed = Distance/Time.

The VASCAR-plus manual claims an overall speed measurement accuracy of $\pm 1 \%$. This accuracy was recently challenged. This study determined the accuracy of VASCAR-plus time, distance, and speed measurements. Two VASCAR-plus units were electronically tripped (no human operator) to determine the timing accuracy, Six VASCAR certified officers participated in a study to determine VASCAR-plus distance measurement accuracy. Eight VASCAR certified officers participated in a series of studies to determine VASCAR-plus speed measurement accuracy. The results of these studies show that VASCAR-plus does not have an overall speed measurement accuracy of $\pm 1 \%$, but that $a+2$ mph upper 90 th percentile tolerance limit ( $95 \%$ of the speed errors are less than +2 mph ) is achievable when the speed measurement is 4 seconds in duration for stationary methods (angular and parking), and is 5 seconds in duration for moving methods (following and approaching from the rear).

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Department of Transportation
National Highway Traffic Safety Administration

## TECHNICAL SUMMARY

## Report Title:

Evaluation of the VASCAR-plus Speed Measurement Device

## Report Author(s):

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Transportation Research Center of Ohio, Inc.
The National Highway Traffic Safety Administration (NHTSA) conducted tests at the Vehicle Research and Test Center (VRTC) to determine the accuracy of the VASCAR-plus speed measurement device. This device is used extensively for speed law enforcement by State and Local Police. VASCAR-plus calculates speed using the basic formula
Speed = Distance/Time.

The process of measuring a motorists speed is called clocking. A successful speed measurement attempt is called a clock. VASCAR-plus can be used with the police cruiser stationary (stationary clocking) or with the police cruiser moving (moving clocking).

The VASCAR-plus manual claims an overall speed measurement accuracy of $\pm 1 \%$. This accuracy was recently challenged. Tests were conducted to determine the accuracy of VASCAR-plus time, distance, and speed measurements.

Two VASCAR-plus units were tested to determine timing accuracy. These units were electronically tripped (no human operator). The VASCAR-plus time measurements were compared to the time measurements of an oscilloscope which had a much higher sampling rate. A negative timing error (i.e. measured time less than true time) produces an overestimate of the target vehicle's speed. It was found that $95 \%$ of the timing errors were above -0.0422 seconds (lower 90 th percentile tolerance limit). This potential timing error results in speed errors that are magnified at higher speeds and are minimized by longer course distances. For example, the potential speed error at 80 mph over a 200 foot course is 2.03 mph , while the potential speed error at 45 mph over a .3 mile course is 0.08 mph .

Six VASCAR certif ied officers participated in a study to determine the accuracy of VASCAR distance measurements. Three distances ( $200 \mathrm{feet}, .1$ mile and .3 mile) were measured. A positive distance error (i.e. measured distance greater than true distance) produces an over estimate of the target vehicle's speed. The distance errors were greater than the 6.3 inch accuracy quoted in the VASCAR manual, but $95 \%$ of the distance errors for each distance were well below $.5 \%$ (upper 90 th percentile tolerance limit).

Eight VASCAR certified officers participated in several different studies to determine the accuracy of VASCAR speed measurements. The variables and variable values examined in these studies are listed in Table 1. Note that not all variables and/or variable values were examined in each study. The variables and variable values were selected based on the VASCAR user manual, the results of a task analysis of VASCAR operation, and the results of a VASCAR user survey.

Table 2 lists the mean and upper 90th percentile tolerance limits for speed error for the overall study, for all of the moving clocks, and for all the stationary clocks. The corresponding values for percent speed error are in Table 3.

TABLE 1 -- Tested Variables and Variable Values

| Variable | Variable Values |
| :--- | :--- |
| Subjects | $1-8$ |
| VASCAR method | Moving <br> Following <br> Approaching from the Rear <br> Stationary <br> Parking <br> Angular |
| Nominal Speed | 45 mph <br> 60 mph <br> 80 mph |
| Course Distance | 200 feet <br> 0.1 mile <br> 0.3 mile |
| Visual Method | Direct <br> Indirect (through mirrors) |
| Elevation | Ground Level <br> Elevated (12. feet) |
| Viewing distance | 200 feet <br> 0.1 mile |
| Gap Distance | 200 feet <br> Between Vehicles |
| I/8 mile |  |

TABLE 2 -- Mean and Upper 90th Percentile Tolerance Limits for Speed Error (mph)

| Portion of <br> Study | Mean | Upper 90th <br> Percentile |
| :---: | :---: | :---: |
| Overall | .426 | 3.134 |
| Moving | .105 | 1.540 |
| Stationary | .644 | 4.074 |

TABLE 3 -- Mean and Upper 90th Percentile Tolerance Limits for Percent Speed Error

| Portion of <br> Study | Mean | Upper 90th <br> Percentite |
| :---: | :---: | :---: |
| Overall | .638 | 4.530 |
| Moving | .164 | 2.230 |
| Stationary | .959 | 5.886 |

For all of the moving clocks greater than 5 seconds in duration, the speed errors were less than +2 mph . The mean and upper 90 th percentile tolerance limits for speed error and percent speed error for the moving clocks greater than 5 seconds in duration are presented in Table 4.

TABLE 4 -- Mean and Upper 90th Percentile Tolerance Limits for Moving Clocks Greater Than 5 Seconds in Duration

| Dependant <br> Variable | Mean | Upper 90th <br> Percentite |
| :---: | :---: | :---: |
| Speed Error | .150 | 1.146 |
| Percent <br> Speed Error | .232 | 1.893 |

The mean and upper 90th percentile tolerance limits for speed error and percent speed error for the stationary clocks greater than or equal to 4 seconds in duration are presented in Table 5.

TABLE 5 -- Mean and Upper 90th Percentile Tolerance Limits for Stationary Clocks Greater Than or Equal to 4 Seconds in Duration

| Dependant <br> Variable | Mean | Upper 90th <br> Percentile |
| :---: | :---: | :---: |
| Speed Error | -.072 | 1.567 |
| Percent <br> Speed Error | -.118 | 2.188 |

From the results presented in Tables 2 through 5, VASCAR-plus does not have an accuracy of $\pm 1$ percent, but an upper 90th percentile tolerance limit ( 95 percent of the values are less than or equal to this limit) of +2 mph is achievable.

It is important to note that no one table or figure in this report can stand alonc. The raw data, the statistics, the laboratory environment, and the officers' opinions of the different test conditions must all by taken into account before any conclusions can be drawn.

There are at least two methods currently used by police officers to measure vehicle speed. One method is to measure the time it takes a vehicle to cover a known distance. The average speed of the vehicle is then computed using the basic formula

```
Speed = Distance/Time.
```

Radar is another way of measuring vehicle speed. Radar is an "instantaneous" speed measurement device. Both systems are used extensively for speed law enforcement by state and local police.

VASCAR-plus, manufactured by Traffic Safety Systems, is a time-distance speed measurement device that is used by many state and local police agencies to enforce traffic laws. VASCAR stands for Visual Average Speed Computer and Recorder. The VASCAR-plus computer calculates an average speed using the basic formula given above. The device allows the user to "drive in" or "dial in" a distance (these two input modes are discussed in greater detail later in this section). The user then "times" a vehicle as it covers the distance. Knowing the distance and the time, the device then calculates the average speed of the vehicle. The process of timing a vehicle over a known distance is called clocking.

Both VASCAR-plus and radar have very distinct advantages as speed measurement devices. One advantage of VASCAR-plus is nondetectability. Radar emits a signal that can be detected by a motorist using a radar detector. The radar detector will warn the motorist to slow down, but the motorist can resume his or her speed when out of the range of the radar. VASCAR-plus does not emit a signal, therefore motorists have no warning that their speed is being monitored. Another advantage of VASCAR-plus is the fact that it calculates average speed. As seen in Figure 1.1, the average speed is always less than or equal to the maximum speed of the vehicle during the distance that the speed is measured. True average speed is equal to the maximum speed only if there is no speed variation during the measured interval. Because it is less than or equal


Figure 1.1 - Comparison of a Hypothetical speed/Time History and
Average speed
to the maximum speed, the average speed benefits the violator. A final advantage of VASCAR-plus is vehicle identification. The user can monitor only one vehicle at a time, so there is no question which motorist's speed is being measured.

The fact that VASCAR-plus can only monitor one vehicle at a time is also a disadvantage. The user has to monitor the vehicle over the entire distance of the clock. Therefore, if there is heavy traffic, the user can only measure the speed of a low percentage of motorists. Radar is an "instantaneous" speed measurement device. The radar unit emits a signal that bounces off a target and returns to the radar. This speed measurement method is much quicker than VASCARplus, so the user can measure a higher percentage of motorists' speed in heavy traffic. Based on the advantages of each, both VASCAR-plus and radar are used extensively as law enforcement tools. From the results of a VASCAR user survey, other perceived advantages of both VASCAR-plus and radar are discussed in Section 3.2.

Each VASCAR-plus unit has a red time toggle switch, a black distance toggle switch, a red time recall button, a black distance recall button, five thumbwheel switches, an LED display, and an odometer module that is driven by the vehicle speedometer cable. A VASCAR-plus unit is displayed in Figure 1.2.


Figure 1.2 - VASCAR-plus Control Panel

When "driving in" a distance, VASCAR-plus uses the pulses produced by the odometer module. A typical car speedometer cable turns 1000 times in a mile and the odometer module creates 10 pulses per turn. This produces 10,000 pulses per mile, hence the VASCAR-plus user manual claims a measurement accuracy of one tenthousandth of a mile, or 6.3 inches in one mile. Not every speedometer cable turns 1000 times per mile, so each car that has a VASCAR-plus unit must be calibrated to read the correct distance (the VASCAR-plus user manual gives a calibration procedure). To "drive in" the distance, the user selects two fixed reference marks. The user then aligns the first fixed reference mark with a reference point on his or her vehicle and switches on the black distance toggle switch. The user then drives to the second fixed reference mark and aligns it with the same reference point on the vehicle he or she used before. The user then switches the black distance toggle switch off. This operation registers the course distance into the VASCAR computer. To dial in the distance, the user enters the known distance on the thumbwheel switches mentioned above.

VASCAR-plus can be used with the police cruiser moving or with the police cruiser stationary. The VASCAR manual describes three moving methods, and three stationary methods.

The three moving methods are:
A. Following - the police cruiser is following the target vehicle
B. Opposite Direction - the police cruiser and target vehicle are approaching each other from opposite directions
C. Approaching from the Rear - the target vehicle approaches the police cruiser from the rear

The three stationary methods are:
A. Parking - the officer sits next to the roadway
B. Angular - the officer sits off to the side of the road and uses two stationary reference points to clock the vehicle
C. T-Intersection - the officer starts the clock from a stationary position, but then follows the target vehicle

For a more detailed explanation of these methods, please see the VASCAR manual and the task analysis in section 3.1 .

The manufacturer claims an overall speed measurement accuracy of $\pm 1$ percent. This stated accuracy was recently challenged. Theoretical presentations have been given to support both the accuracy and the errors of the system.

### 2.0 OBJECTIVE

The objective of this evaluation was to measure the accuracy of the VASCARplus speed measurement device. To accomplish this, a task analysis was performed to determine what variables should be considered in the evaluation of VASCAR. Interviews with VASCAR trained officers were also performed to determine how VASCAR is used by law enforcement officers. Based on the results of both the task analysis and the personal interviews, and based on the VASCAR manual, an experimental design was developed to ascertain how key variables affect speed measurement accuracy. Tests were conducted and the results were statistically analyzed.

### 3.0 DETERMINATION OF VASCAR USE

To determine how VASCAR is used, a task analysis was performed and interviews with VASCAR trained officers were conducted. The task analysis was conducted to determine what an officer has to perform to complete an appropriate VASCAR clock. The task analysis also helped identify variables for evaluation, and potential sources of error and/or distractions that may interfere with the officer's ability to complete a successful clock. The interviews concentrated on how often the officers use the different VASCAR methods and on typical distances they use to make VASCAR clocks. Other topics covered by the interviews were types of training, opinions of VASCAR effectiveness, and the use of VASCAR versus the use of radar. A copy of the personal interview form is in Appendix A.

## Objective

To better understand how police officers use VASCAR in the field and to obtain information for use in designing an evaluation experiment, a task analysis was performed. Essentially, in a task analysis an operator's basic tasks are subdivided into elements so that knowledge and skill requirements, time lines, potential errors, etc. can be examined. Clearly, such an analysis can become quiet complex depending upon the degree of abstraction applied to the problem.

## Participants

The task analysis conducted in this study was based on the observation of four officers from the Columbus, Ohio freeway patrol, who demonstrated VASCAR use during their normal duties. Observations were made both during the day and at night.

Results
The officers demonstrated three of the VASCAR methods described in the operator's training manual. The methods demonstrated were:

| Moving: | Following <br> Approaching from the Rear |
| :--- | :--- |
| Stationary: | Parking |

Due to the constraints imposed by the freeway environment (i.e., limited access divided highway with concrete center divider) the T-Intersection, Angular Clocking and Opposite Direction methods could not be demonstrated.

The results of the task analysis are presented in Table 3.1 and in Appendix B. The tasks involved in the stationary method are illustrated in Table 3.1. For the analysis in Table 3.1, it was assumed that the course distance was previously entered in the VASCAR computer by "driving it in" or "dialing it in" using the thumbwheel switches on the VASCAR control panel. For stationary methods, clocking targets involved activation of only the time toggle switch. See Figure 1.2 for location of switches.

## TABLE 3.1 CLOCR TARGET USING A STATIONARY VASCAR METHOD

## Task: Clock Target Using a stationary VAsCAR Method



## Task: Clock Target Using a stationary VAscar Method (Continued)

| Task Element | SensoryPerceptual Requirements | PsychoMotor Requirements | Cognitive Requirements | Limiting Factors | Potential Sources of Errors | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Track Target to First Reference Marker | Visually monitor target's progress toward VASCAR course <br> Rear view or left side mirror is used when monitoring target in Parked Mode | Estimate arrival time of target at reference marker | Decide when Time switch should be activated | Other traffic could obscure target or reference marker <br> Radio "chatter" |  | Depth cues in road scene (e.g., other vehicles or fixed objects adjacent to highway) aid in arrival time estimation |
| Turn Time Switch ON | Obtain auditory and tactile feedback of switch activation | Push toggle switch into UP position <br> Reaction time | Decide if switch was activated as target passed reference marker | Radio operation requires the same hand used for operating VASCAR controls | Early switch activation could lead to underestimation of true speed <br> Late switch activation could lead to overestimation of true speed | To reduce reaction time delay officers initiate switch activation just prior to the arrival of the target at the reference mark |

# Task: <br> Clock Target Using a stationary VASCAR Method (Continued) 

Task Element

Track Target to
Second Reference
Marker Marker

## Push togile

 switch downReaction time

Visually monitor target's progress through course to second reference marker

Rear view or left side mirror is used when monitoring target in Parked Node
Turn Time Switch

Obtain auditory and tactile feedback of switch activation

Comments

## Early switch activation could lead to overestimation of true speed <br> Late switch activation could lead to underestimation

 of true speedPsycho-
Motor
Requirements

## Estimate arrival time of target at reference marker


Cognitive
Requirements
Note if target
changes lanes
while in course
Decide when Time
switch should be
activated activated

## Requirements

Other traffic could obscure target or reference marker

Radio "chatter"

## Potential <br> Sources of Errors <br> Limiting Factors

Lane changing by target could lead to underestimated true speed

| Decide if switch | Radio operation |
| :--- | :--- |
| was activated as | requires the same |
| the target passed | hand used for |
| the reference | operating VASCAR |
| marker | controls |

To reduce reaction time delay officers initiate switch activation just prior to the arrival of the target at the reference mark

Switch activation errors at both reference markers can either have offsetting effects or additive effects which increase measurement error

Task Element
Read VASCAR Display
Sensory-
Perceptual
Requirements

Read speed value displayed

Viewing distance is approximately 30 inches

Character height
is approximately one-half inch
Psycho-
Motor
Requirements

## Cognitive Requirements

Displayed speed is compared with initial speed judgement made by officer

## Limiting Factors

## Potential <br> Sources of

Errors
Error by officer
in reading
display

Comments
Measured speed must have face validity compared with officer's initial judgement of target speed

Assess Validity
of Speed
■
Measurement

Decide whether or not to pursue

Decide to accept (or reject) speed measurement based on switch activations, lane maintenance by target and displayed reading

Decide to pursue target if
measured speed is greater than speed limit plus an allowance factor for motorist error

Last second requirement to attend to a more critical event (e.g., accident, violent crime, other emergency)

The decision to pursue a violator depends on the measured speed, the officer's ability to safely pursue in traffic, the police department policy for
issuing speeding citations and the need for the officer's services elsewhere

The Following method and the Approaching from the Rear method are illustrated in Appendix B. For these two methods, the officer had to operate both the time and the distance toggle switches. In most circumstances the time switch was operated independently of the distance switch. The descriptions provided in Appendix B also represent a generalized or "typical" sequence of subtasks. Depending on actual conditions on the highway, e.g., target vehicle and police cruiser speeds, course distance, availability of reference marks, etc., officers may use slight variations of the sequence presented.

For this task analysis, the VASCAR control/display panel was located to the right of the officer near the center of the car, close to the height of the seat cushion. Adjustment features on the VASCAR mounting brackets allowed each officer some options in positioning the device to best meet individual needs (e.g., seat location, seated eye height, viewing angle, functional reach envelope, etc.).

Officers used their right hand to operate the VASCAR controls, most frequently with the thumb and index finger. For the moving methods of operation, the officers drove the cruiser with the left hand and simultaneously operated the VASCAR controls with the right hand. Radio communications were also performed with the right hand, when required.

### 3.2 Personal Interview Approach and Results

## Objective

Personal interviews were conducted as an observational study to assist the development of the courses used in the experimental study. The survey concentrated on how often the different VASCAR methods were used, typical course distances used by officers, types of reference markers, and officers' opinions of VASCAR.

## Participants

A sample of twenty-one officers from across the United States was contacted for this survey. All of the officers currently use the VASCAR-plus. Six of the officers were from local police agencies, while the remaining fifteen were from
state police agencies. Twenty officers were trained and certified, while one was currently going through training. The officers were selected as randomly as possible, but the selections did not produce a probability sample.

Results
The officers were asked about the type of training they received. The amount of training each officer received did vary. Not every officer could remember how much training they had received. Of the officers that replied, most had received at least eight hours of classroom training. The amount of supervised and unsupervised training ranged from 12 to 160 hours. The officers that made statements about their certification requirements mentioned the certification test outlined in the VASCAR manual.

The distribution for how often the contacted officers use VASCAR is shown in Figure 3.1. From this figure, over $75 \%$ of the contacted officers used VASCAR on a daily basis.

The distribution of officers based on level of VASCAR experience is shown in Figure 3.2. The level of experience ranged from 1 month to 18 years. The officers were asked to rate their own VASCAR skills on a scale from 1 to 10 , with 1 being a novice and 10 being an expert. Nineteen officers responded. A distribution of the officers based on their self rating is given in Figure 3.3. Self rated skill ranges (mean $\pm$ one standard deviation) for officers with different levels of experience are given in Figure 3.4. The ranges presented in this graph suggest that an officer's opinion of his or her own VASCAR skills would tend to improve during the first one to two years of experience, but may level out after this period. Several officers stated that it takes a certain amount of time to become comfortable with using VASCAR.

A distribution of officers determined by the types of roadways on which they use VASCAR is given in Figure 3.5. From this figure, all of the contacted officers used VASCAR on the freeway and some also used it on other types of roadways.


Figure 3.1-Officer Distribution for the Level of VASCAR Use




Figure 3.4 - Officer Self Rated VASCAR Skills as a Function Experience (mean $\pm$ one std. dev.)


The mean percentage use for each of the VASCAR speed measurement methods for both local and state police is given in Table 3.2. On average, local and state police used each of the VASCAR methods a similar amount of the time (a t-test was performed and the hypothesis that the two means, for each method, were similar could not be rejected at the $5 \%$ level). Based on these comparable percentages, the local and state police responses concerning percentage use were combined as one group.

TABLE 3.2 -- Mean Percentage Use of VASCAR Speed Measurement Methods for Local and State Police Officers

| Method | Local | State |
| :---: | ---: | ---: |
| Moving | 50.8 | 53.0 |
| Following | 30.0 | 30.1 |
| Opposite Direction | 3.1 | 3.3 |
| Approach from Rear | 17.7 | 19.6 |
| Stationary | 49.2 | 47.0 |
| Parking | 29.6 | 26.6 |
| T-Intersection | 0.4 | 5.0 |
| Angular | 19.2 | 15.3 |

After combining the local and state police responses, the mean and standard deviation for the percentage use of each method were calculated. The results are presented in Table 3.3. A range of use for each method is given in Figure 3.6. These ranges represent the mean $\pm$ one standard deviation for the percent use of each method. From this figure, the percentage use of moving and stationary methods were very comparable. Also from this figure, Following, Approaching from the Rear, Parking, and Angular methods were much more prevalent than Opposite Direction and $T$-Intersection methods. For the Opposite Direction method, the officers said they did not use it either because radar was better for this method, or they worked divided highways with concrete barriers which kept them from turning around to chase a vehicle moving in the opposite direction.

The results presented in Figure 3.7 show the distribution of officers as a function of the VASCAR method with which they had the greatest confidence, while the results presented in Figure 3.8 show the distribution for the VASCAR method with which they had the least confidence. From Figure 3.7, most of the contacted officers had the greatest confidence with either the Following or the Parking


Figure 3.6 - Range of Use for Each VASCAR Method (mean $\pm$ one std. dev.)


method. From Figure 3.8, over half of the officers had the least confidence in the Opposite Direction method.

TABLE 3.3 -- Mean and Standard Deviation for the Percentage Use of VASCAR Speed Measurement Methods for all Officers

| Method | Mean | Std. Dev. |
| :--- | ---: | :---: |
| Moving | 52.4 | 32.2 |
| Following | 30.1 | 23.4 |
| Opposite Direction | 3.3 | 6.2 |
| Approach from Rear | 19.0 | 23.1 |
| Stationary | 47.6 | 32.2 |
| Parking | 27.5 | 30.5 |
| T-Intersection | 3.6 | 6.0 |
| Angular | 16.5 | 28.0 |

The results presented in Figure 3.9 show the six most prevalently used references during daylight hours. Other references used during the day (only 1 or 2 officers responded) included a dip in the road, discarded tire treads, trees, light poles, bridge abutments, tape, skid marks, expansion joints, and debris along roadway.

The references used at night were limited to objects on the side of the road like signs, mile markers, guardrails, and poles. Any object that headlights illuminate could be used as a reference marker.

The officers were asked how often they used "dialing in the distance" vs. "driving in the distance" for stationary clocks. On average, the officers drove in the distance more than twice as often as dialing in the distance.

Information concerning course lengths and viewing distances is displayed in Figures 3.10-13. The local and state police officers are grouped together for these figures. The values along the horizontal axis represent distance ranges (. 05 - . 99 represents .05 to .99 mile) From the results presented in Figure 3.10 , the shortest course distances ranged from 200 feet to one half mile. From Figure 3.11, the longest course distances ranged from .19 miles to 4 miles. The




Figure 3.11-Officer Distribution for the Longest VASCAR Course Distance Used
longest stationary course distance was .75 miles. From Figure 3.12, the preferred course distances ranged from 250 feet to 1.9 miles. The range of values for the maximum viewing distance, the distance from the officer's eye to a reference point, is shown in Figure 3.13. The maximum viewing distance ranged from 200 feet to .75 miles.

The mean and median values for the four distances discussed above are listed in Table 3.4.

TABLE 3.4 -- Mean and Median Course and Viewing Distances (miles)

| Distance | Mean | Median |
| :--- | :---: | :---: |
| Shortest Course <br> Longest Course | .093 | .1 |
| Preferred Course <br> Maximum Viewing <br> Distance | .29 | .75 |

The amount of time spent using VASCAR at night is shown in Figure 3.14. From this figure, it appeared that officers either use VASCAR infrequently or quite frequently at night. This was probably a function of the way police departments operate. Some departments have fixed shifts while others have rotating shifts. When asked whether their choice of VASCAR method was in any way determined by day vs. night time use, thirteen of the twenty-one officers said it was not influenced, four officers said VASCAR was easier to operate during the day, and one officer said it was easier to operate at night. Only two officers made comment on how it influenced their VASCAR method choice; one said he mostly used following clocks at night, the other said angular clocking was harder to use at night. One officer said he preferred using it at night because he was less visible to violators.

When asked whether their choice of VASCAR method or references was influenced by weather conditions, 4 officers responded that there was no influence while the other officers had answers ranging from shortening their viewing distances and only using certain methods in bad weather, to not using VASCAR at all in the rain.



Figure 3.13 - Officer Distribution for the Maximum Viewing Distance Used


The frequency of calibration checks of VASGAR units is shown in Figure 3.15. All but two of the officers either calibrated or checked the calibration at least once per day. These responses are based on each individual officer's use. If the officer only used it once a month, he or she calibrated on the day that VASCAR was used.

A distribution of officers based on a self assessment of their speed measurement accuracy is given in Figure 3.16. From this figure, there was a wide range of self assessed speed measurement accuracy. When the officers were asked whether their speed accuracy was a function of course length, target vehicle speed, and/or VASCAR method, 11 of the 21 officers said it was course length dependant, 4 said it depended on the target vehicle speed, and 17 said it was dependant upon VASCAR method.

Of the 21 officers surveyed, 12 had defended a VASCAR based speeding citation in court. These 12 were asked how defendants or defense attorneys attacked their VASCAR speed estimates. Seven responded that they attacked the officers ability (human error of some sort). Only one tried to attack the VASCAR device itself. Other responses to this question were not directly attributable to VASCAR.

When asked what the strengths of VASCAR were, the most common responses were: that VASCAR is accurate, that the officer has a high degree of confidence in which vehicle he or she is clocking, that VASCAR is better for use in high volumes of traffic than radar, and that the calculation of average speed gives the benefit of doubt to the motorist. The number of officers that gave each of the above responses is shown in Figure 3.17.

When asked what the weakness of VASCAR were, the most common responses were: the time it took to set up or to use ( 6 officers) and the potential for human errors (5 officers). Other cited weaknesses (1 or 2 officers) included the length of training, the inability to use without references, the inability to use certain methods under certain conditions, the greater requirements for the operator when compared to radar, and the cost of the VASCAR units.


Figure 3.15 - Officer Distribution for the Frequency of Calibration



Figure 3.17 - strengths of VASCAR

When asked if they had ever experienced a failure in their VASCAR equipment, 8 of the 21 officers responded 'yes'. The failures included shorts in the wiring from the car battery to the VASCAR unit, the VASCAR computer going out, the odometer module breaking, and a lost speed upon fast acceleration (a single officer stated this happened to him one time). No officer stated they had an erroneous speed due to the VASCAR unit itself. Their VASCAR units either gave the correct speed or did not give a speed at all.

All 21 of the surveyed officers also used radar to establish vehicle speeds. The officers were asked "Under what circumstances is VASCAR preferred over radar?", and "Under what circumstances is radar preferred over VASCAR?". The most common responses to these questions are given in Figures 3.18 and 3.19.

The officers were given the statement "It's been said that some officers prefer not to use VASCAR. Why do you think some officers avoid the use of VASCAR?". Some of the officers thought that the training time and the time to set-up certain courses might keep certain officers from wanting to use it. Some of the officers thought if the officer had not spent enough time using VASCAR, he or she might not be familiar enough with it's operation to feel comfortable using it. Some officers stated that an officer's lack of confidence in his or her own ability might be a reason why they may avoid using VASCAR.

To close the survey, the officers were asked if all their opinions on VASCAR had been stated. Most of the officers had favorable things to say about VASCAR. Some officers said they enjoyed having both VASCAR and radar and think they make a good team. Others went as far as saying they would prefer to have VASCAR over radar. The only negative statements made were that radar was easier to use and one officer stated that he wished the distance and time inputs were buttons instead of switches.

### 4.0 EXPERIMENTAL DESIGN AND PROCEDURE

Objectives

1. Determine accuracy of VASCAR-plus timing mechanism.


Figure 3.18 - When VASCAR is Preferred Over Radar


Figure 3.19 - When Radar is Preferred Over VASCAR
2. Determine distance measurement accuracy of VASCAR-plus odometer module.
3. Determine speed measurement accuracy for several VASCAR-plus methods.

### 4.1 Experimental Design of VASCAR Time and Distance Measurements

## VASCAR Timing

According to the manufacturer, VASCAR-plus collects data every 36 milliseconds (i.e., a 36 millisecond resolution). Since this is the case, the VASCAR-plus stored time is in milliseconds ( $1 / 1000$ of a second). VASCAR-plus displays the stored time to $1 / 100$ of a second. To properly assess the accuracy of the VASCAR timing mechanism, the stored time to $1 / 1000$ of a second must be determined.

To determine the stored time to $1 / 1000$ of a second, the manufacturer says to first divide the displayed time by .036 (or 36 milliseconds). This number is then rounded to the next highest integer. This integer value is then multiplied by .036. The resulting value is the stored time. As an example:

VASCAR Displayed Time $=4.60$
To get the number of 36 msec time increments, divide the displayed time by . 036 and then round to the next highest integer.

$$
4.60 / .036=127.77
$$

Number of .036 msec time increments $=128$
To get the VASCAR stored time, multiply this number by .036 .
VASCAR Stored Time $=128 \times .036=4.608$

To determine the validity of the manufacturer's method for determining the stored time, bench tests were performed in which VASCAR displayed speeds were compared to speeds calculated using the VASCAR displayed time and to speeds calculated using the VASCAR "stored" time. If the VASCAR displayed speeds match the speeds calculated using the VASCAR "stored" times, then the manufacturer's
method for determining the stored time would be considered valid. For these bench tests, a . 2500 mile distance was entered on the VASCAR thumbwheels. Then, the VASCAR time switch was toggled to produce times ranging from approximately 3 to 4.5 seconds. These times produced speeds large enough to show the differences between speeds calculated using the VASCAR displayed time and speeds calculated using the VASCAR stored time.

After these tests were completed, additional bench tests were conducted to determine the accuracy of the VASCAR timing device. Two VASCAR units and a Nicolet oscilloscope were simultaneously triggered using two trip switches. The Nicolet oscilloscope's sample rate was set to 1 msec . A total of 58 tests were performed with times ranging from approximately 1 to 4 seconds.

Time error was used to judge the accuracy of the VASCAR-plus timing device:

Time Error $=$ VASCAR time - True Time

## VASCAR Distance

Tests were performed to determine the accuracy of VASCAR distance measurements. Some human error was involved in these tests because vehicle position at each reference mark is estimated by the user. The human error was minimized by having the operators line the vehicle up with reference markers at the beginning and the end of the course. Six subjects participated in this study. Course distances of 200 feet, .1 mile, and .5 mile were each measured 4 times by the subjects.

Distance error was used to judge the accuracy of VASCAR distance measurements:

Distance Error $=$ VASCAR distance - True Distance

Based on the results of the personal interviews and the task analysis, the following were identified as potential variables affecting the accuracy of VASCAR speed measurement:

```
VASCAR method
Target vehicle speed
Course distance
Type of reference marker
Distance of the eye to the course or reference marker
Gap distance - distance between two moving vehicles
Visual method (direct vs. indirect-through use of mirror)
Officer vehicle elevation
Officer differences
Repetition effect - variation from successive trials
Replication effect - variation from different days
Weather conditions
Day vs. night use
```

To investigate the effects of some of these variables, six studies were designed. The six studies were moving, night moving, bridge, parking, angular, and reference marker alignment. Each study focused on one or more of variables listed above. Subject differences were examined in all the studies. Replication of a set of test conditions occurs when the test conditions are repeated in a new randomized order, after a period of time has passed. For the testing conducted in this study, replicates were generally separated by a 24 hour period. Due to time constraints and weather conditions, sometimes 2 replicates were performed on the same day. The replicates were separated by a 4 hour period. Replication effects were examined in all of the studies except the bridge study. Replication effects inciude the possibility of learning and/or fatigue.

### 4.3 Experimental Design and Setup of VASCAR Speed Measurements

In all of the studies mentioned below, the nominal speed represented a speed range. For subjects 1 through 4, the speed range was the nominal speed $\pm 2 \mathrm{mph}$; for subjects 5 through 8, the speed range was the nominal speed $\pm 7 \mathrm{mph}$. These different speed ranges occurred due to concern that the earlier subjects may have known the target vehicle speed (due to repetition) before the clock was finished.

Differences in the results between the two groups are discussed in the test results section of this report.

Another study compared the effect of blind (VASCAR display covered) and normal (display uncovered) speed measurements. This study was not considered to be an appropriate test of VASCAR. The results of the task analysis showed that the displayed speed is compared with the initial speed judgement made by the officer. If the display is hidden, the subject is not able to make this comparison. The results of this study are presented in Appendix $C$.

In all of the following studies, speed error was used to judge the accuracy of VASCAR speed measurements:

Speed Error $=$ VASCAR speed - True Speed

Moving Study
Variables
A. Two VASCAR methods: Following and Approaching from the Rear
B. Course distance at two levels: . 1 and . 3 mile (528 and 1584 feet).
C. Target vehicle speed at three levels: 45,60 , and 80 mph .

This variable list and number of levels resulted in a $2 \times 2 \times 3$ full factorial design, resulting in 12 combinations of conditions. As with all the studies, it was intended that each officer replicate this study four times.

Under ideal conditions it would be best to randomly present the 12 conditions to the officers. Due to the time it takes to set up the different conditions, this was not practical. For this study, a course distance was first randomly selected, then each combination of VASCAR method and speed was randomly selected. The VASCAR method was not completely randomized for each officer. For efficiency, one officer was performing a Following clock, while the other was performing an Approaching from the Rear clock. An example of the order of trials for this study and the other studies is in Appendix D.

The test configuration is detailed in Figure 4.1. In Figure 4.1, and the figures that follow, $T$ is the target vehicle, $S_{1}$ is subject 1 , and $S_{2}$ is subject 2. In Figure 4.1, subject 1 is performing a Following clock while subject 2 is performing an Approaching from the Rear clock in an adjacent lane. Subject 2 uses the side or rear view mirror, depending on the gap distance between vehicles, to maintain visual contact with the target vehicle.

## Night Moving Study

## Variables

A. Target vehicle speed at three levels: 45, 60, and 80 mph

All other variables were held constant. The course distance was .3 mile and the VASCAR Following method was used. These values were chosen to allow a direct comparison between day and night time conditions. Each subject was randomly given each of the speed conditions twice.

The test configuration for the night moving study is detailed in Figure 4. 2. The only differences between following clocks in the moving study and the clocks in the night moving study was the light condition and the reference marker. In the moving study, the subject generally used the photocell reflector plate (see section 4.4 ) as the reference marker. In the night moving study, the subjects used the target vehicle headlights reflecting off the white pole (Figures 4.1 and 4.2).

## Bridge Study

Variables
A. Target vehicle speed at two levels: 60 and 80 mph .
B. Vascar method at two levels: Following and Parking.

C1. For the Following clocks - two gap distances: 250 feet and $1 / 8$ mile


$L=$ Course Lengtin, 528 ft or 1584 ft
O =Orange Cone
$\square$ =Photoce|| Reflector Plate


C2. For the Parking clocks - two viewing methods: direct and indirect (mirror)

This variable list and number of levels gave 8 combinations of conditions. The course distance was held constant at .3 mile ( 1584 feet).

These conditions were presented as randomly as possible. There was only one constraint on the randomization; while one officer was performing a Following clock, the other officer was performing a Parking clock. Figure 4.3 contains details of the test conditions.

For the Following clocks, two gap distances were chosen to study the effect of viewing distance. The shorter gap distance was the same as the gap distance in the moving study. This allowed a direct comparison between the "bridge" shadow and the photocell reflector plate reference markers.

The "bridge shadow" used in this study was not a real bridge shadow. To simulate a bridge shadow, tarps were placed on one side of $4^{\prime} \mathrm{x} 6^{\prime} \mathrm{x} 8^{\prime}$ sections of scaffolding. The shadow cast by each section of scaffolding was $6^{\prime}$ wide. For subjects 1 and 2 there was only one section of scaffolding at each end of the course. For subjects 3 through 6 there were two sections of scaffolding; therefore, the bridge shadow was twice as wide. The shadow was widened because subjects 1 and 2 felt it was unrealistically narrow.

## Parking Study

Variables
A. Target vehicle speed at two levels: 60 and 80 mph .
B. Course distance at two levels: 200 feet and . 1 mile ( 528 feet).

This variable list and number of levels gave a $2 \times 2$ full factorial design resulting in 4 combinations of conditions. The test conditions are detailed in Figure 4.4. As seen in Figure 4.4, this study also used a "bridge" shadow. This bridge shadow was the same bridge shadow used in the bridge study.



=Shadow
$\square=$ Photocel। Reflector Plate

Figure 4.4 - Test Configuration for the Parking study

For this study, the subjects were first randomly assigned a course distance. The target vehicle then drove by twice at the selected speed levels. The order of presentation of the two vehicle speeds was random. The subjects then switched positions and again the target vehicle drove by at the two speed levels.

## Angular Study

## Variables

A. Target vehicle speed at three levels: 45,60 , and 80 mph .
B. Course distance at two levels: 200 feet and .1 mile ( 528 feet).
C. Viewing distance at two levels: 200 feet and .1 mile ( 528 feet).
D. Elevation at two levels: ground level and elevated (12 feet).

This variable list and number of levels gave a $3 \times 2 \times 2 \times 2$ full factorial design resulting in 24 combinations of conditions. Figure 4.5 contains details of the test conditions.

The officers were first randomly assigned a viewing distance. They were then randomly assigned an elevation level; one officer on the ground and the other elevated 12 feet. A course distance was randomly selected, then the three target vehicle speeds were randomly presented to the officers. The course distance was then changed, and again the three speeds were randomly presented. The officers then switched elevation levels and repeated the process. The officers then changed viewing distances and again repeated the process.

## Reference Marker Alignment Study

This study arose due to subjects' 3 - 6 concerns with the angular study. In the angular study, the white pole was not placed in the subjects' line of sight for the 200 foot course distance. The officers said they would not set up a course like this. In this study, the 200 foot viewing distance, 200 foot course distance, and ground level conditions of the angular study were repeated, except for the location of the white pole. In the angular study the white pole
was in line with the photocell reflector plate, while in the reference marker alignment study the white pole was in the subjects' line of sight (Figures 4.5 and 4.6).

Variables
A. Target vehicle speed at three levels: 45,60 , and 80 mph .

For this study the viewing distance and the course distance were both held fixed at 200 feet. The officer was at ground level. The details of this study are shown in Figure 4.6. The three target vehicle speeds were randomly presented to the officers.

This study allowed a direct comparison between having the pole aligned and not aligned for subjects 7 and 8.

### 4.4 Experimental Protocol for Speed Measurement Studies

The experimental protocol consisted of three steps:

1. Give instructions to the subjects
2. Conduct the experimental studies detailed in the previous section
3. Debrief the subjects at the conclusion of all testing

## Subject Instructions

Before any testing was conducted, the subjects were given a statement concerning the testing procedure and protocol. A copy of this statement is given in Appendix E. The testing procedure and protocol statement informed the subjects of the types of clocks they would be making, the risk involved in operating a vehicle at high speeds, the purpose of the study, and their right to discontinue the testing at any time. The subjects were not given details of the particular testing scenarios before testing was conducted.



Immediately prior to conducting each experimental session, the subjects were shown the particular course configuration. They were allowed 2 to 3 practice runs to warm up, then testing began. Prior to any moving tests, the subjects calibrated their VASCAR-plus units. In the stationary studies, the subjects were told the course distance to "dial in". At no time were the officers told the speed of the target vehicle. The subject's speed, time, and distance estimates were recorded by a data collector that rode in the vehicle with each officer. In some of the moving tests, the officers were told when the target vehicle would be "above highway speeds" ( 80 mph nominal speed). This was done due to the short distance available to get the vehicles up to the desired speed. The subjects were not given any results of their performance until weeks after the testing was completed.

It is important to note that in these studies, it was not possible to exactly duplicate real world conditions. The task analysis stated several limiting factors that did not occur during the testing. Other vehicles obscuring objects and radio chatter were two of the limiting factors. The subjects did have to communicate with the control tower and other vehicles by radio, but this communication was probably less than what is heard by an on duty officer. It is also important to note that depth cues, like other vehicles and objects adjacent to the course, were not available in this study, but are available in the real world. Such cues help officers anticipate the arrival of a target vehicle at a reference mark. This permits compensation for reaction time delay.

## Measurement of True Speed

While the subjects measured speed with VASCAR-plus, the target vehicle true speed was measured using a SUNX RS -120 H photocell. The photocell was mounted to the front of the vehicle. The photocell triggered on two reflector plates which were placed at the beginning and end of the course. The photocell signal was monitored by an RTI-815 analog acquisition board. The acquisition board had a 5 megahertz quartz crystal. The sample frequency was scaled to 1000 hertz ( 1 millisecond resolution). An onboard computer collected and stored the signal.

A computer software program used the stored signal to determine the true time. Since all of the clocks were made on courses with known distances, the computer software program calculated the true speed by dividing the known course distance by the true time.

The photocell system timing accuracy was measured by comparing it to the timing of a Nicolet oscilloscope with electronic trip switches. The photocell system was found to be as accurate as the oscilloscope system. Appendix $F$ contains a comparison of the two systems.

## Subject Debriefing

After the testing was completed, the subjects were debriefed. Except for subjects 1 and 2 , the subjects were debriefed separately. During the debriefing the subjects were asked questions concerned with any problems they may have encountered, the realism of the study, and the confidence they had in their VASCAR speed estimates. A sample debriefing guide and the results of the debriefings are in Appendix G. Some of these results are presented in Chapter 5.

### 4.5 Subjects

Two subjects from each of the following departments participated in this study:

1. Columbus Police Department - Columbus, Ohio
2. Arizona Department of Public Safety - Highway Patrol Bureau
3. Indiana State Police Department
4. Wisconsin State Patrol

Each set of subjects had one subject with a low level of VASCAR experience ( $<1.5$ years) and one subject with a high level of VASCAR experience ( $\geq 7$ years). All of the subjects were VASCAR certified, meaning they have passed their departments requirements for operating VASCAR. Selected subject characteristics
and individual subject percentage use and typical course distances for each VASCAR method are in Appendix $H$.

The subjects that participated in each speed measurement study are shown in Table 4.1. All of the subjects did not participate in each of the studies primarily due to weather conditions and due to changes in testing conditions. Weather conditions only affected the studies that required a bridge shadow. When the sun was not shining, the simulated bridge shadow testing could not be performed. There was a wide range of weather conditions for the other studies. The weather conditions included sun, clouds, rain, and snow flurries.

TABLE 4.1 -- Subjects that Participated in Each Study

| Study | Subjects that Participated |
| :---: | :---: |
| Moving | $1-8$ |
| Night Moving | $3-8$ |
| Bridge | $1-6$ |
| Parking | $3-6$ |
| Angular | $3-8$ |
| Align | 788 |

### 5.0 EXPERIMENTAL RESULTS

Several statistical terms are used to present the results. The following definitions will aid in understanding the results:

Mean - the average; the arithmetic sum of all values being considered, divided by the total number of values in the data set.

Variance - is a measure of the variability of the data set; a formula for the variance is given in Appendix E.

Standard Deviation - the square root of the variance; it is also a measure of the variability of the data set.

Type I Error - falsely concluding that something is an effect (the alternative hypothesis) when it is not.
p - the probability of committing a Type I error; $p \leq 0.05$ is used to determine if a variable is a statistically significant effect; $0.05<p \leq$ 1.0 is used as a range for nearly significant effects.

Two Sided Upper 90th Percentile Tolerance Limit with 95 Percent Confidence - 95 percent of the population is less than or equal to this limit with 95 percent confidence.

Two Sided Lower 90th Percentile Tolerance Limit with 95 Percent Confidence - 95 percent of the populations is greater than or equal to this limit with 95 percent confidence.

The upper 90 th percentile tolerance limit with 95 percent confidence (upper 90 th percentile tolerance limit) is used when assessing speed measurement errors. Ninety-five percent of the speed errors will be less than or equal to this limit. The upper 90th percentile tolerance limit is used because it represents the speed error that overestimates the true speed (biased against the violator). The lower 90 th percentile tolerance limit represents the error that underestimates the true speed (biased for the violator).

The lower 90 th percentile tolerance limit is used when assessing time measurement errors. This limit is used because it results in the largest speed errors. The VASCAR timing device produces negative timing errors. Negative timing errors produce estimates of vehicle speed that are higher than the true speed. The largest negative timing errors (lower 90th percentile) produce the largest speed errors that are biased against the violator. Figures 5.1.a and 5.1.b show respectively the locations of the upper and lower 90 th percentile tolerance limits for a normal distribution. The shaded region in these figures represents 95 percent of the population.

To calculate a tolerance limit, two conditions must be met.

1. All assignable causes of variability must be detected and eliminated so the remaining variability may be considered random.
2. Certain assumptions must be made concerning the nature of the statistical population under study - for this study a normal distribution is assumed.


Figure 5.1.a - Upper 90th Percentile Tolerance Limit


Figure 5.1.b - Lower 90th Percentile Tolerance Limit

Definitions for other statistical terms are in Appendix I. All of the raw data and statistical results are also in Appendix $I$. For more thorough statistical definitions, see [1]

In this analysis the variable $p$ is used to determine statistical significance. Also, a 5 mph difference in the upper 90 th percentile tolerance limit is used to determine practical significance.

A second statistical analysis can be found in Appendix J. This analysis considers the lack of complete randomization for the experiment.

### 5.1 Experimental Results of VASCAR Time and Distance Measurements

VASCAR Timing

The first series of bench tests was performed to verify that the VASCAR stored time can be retrieved from the displayed time. The stored time was calculated as described in Section 4.1. A comparison of VASCAR displayed speed, speed calculated using VASCAR displayed time, and speed calculated using VASCAR stored time is shown in Table 5.1

TABLE 5.1 -- Comparison VASCAR Displayed Speed and Speed Calculated Using VASCAR Displayed and Stored Times

|  |  | Speed Calculated Using |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Displayed <br> Time <br> (sec) | Stored <br> Time <br> (sec) | Displayed <br> speed <br> (mph) | Displayed <br> Time <br> (mph) | Stored <br> Time <br> (mph) |
| 3.34 | 3.348 | 268.8 | 269.46 | 268.82 |
| 3.31 | 3.312 | 271.7 | 271.90 | 271.73 |
| 3.70 | 3.708 | 242.7 | 243.24 | 242.72 |
| 4.82 | 4.824 | 186.5 | 186.72 | 186.57 |
| 3.16 | 3.168 | 284.0 | 284.81 | 284.09 |
| 3.45 | 3.456 | 260.4 | 260.87 | 260.41 |
| 3.78 | 3.78 | 238.0 | 238.09 | 238.09 |
| 3.09 | 3.096 | 290.6 | 291.26 | 290.69 |
| 4.64 | 4.644 | 193.7 | 193.96 | 193.79 |
| 3.81 | 3.816 | 235.8 | 236.22 | 235.84 |
| 4.42 | 4.428 | 203.2 | 203.62 | 203.25 |

1 Ostle, B., "Statistics in Research," 2nd Edition, The Iowa State University Press, 1963.

As seen in Table 5.1, the speed calculated using the stored time agreed with the VASCAR displayed speed, while the speed using the displayed time did not. This suggests that the function given in Section 4.1 to calculate the stored time is correct. Since this is the case, the stored time was used to determine the VASCAR timing errors.

A second series of bench tests was performed to determine VASCAR timing errors. Two VASCAR units were tested. The mean and variance for timing errors for each unit were found to be the same. The mean and the lower 90 th percentile tolerance limit for timing error are listed in Table 5.2. Using the value for the lower 90th percentile tolerance limit for timing error, percent speed errors for different speeds and course distances were calculated and are plotted in Figure 5.2. These speed errors were due only to potential VASCAR timing errors. No distance measurement error or human error is included for the errors in Figure 5.2. From section 3.3, the mean value for preferred course distance was .3 mile. The potential percent speed errors due to the timing mechanism for this course distance are below . 5 \%.

## TABLE 5.2-- VASCAR Timing Errors

| Descriptive <br> Statistic | Time <br> Error <br> (sec) |
| :--- | :--- |
| Mean <br> Lower 90th <br> Percentile | -.0223 |

## VASCAR Distance

The following variables were studied to see if they had an effect on VASCAR distance measurements:

> Course Distance
> Subject

Course distance was the only variable found to be significant. The upper 90th percentile tolerance limits for distance errors are plotted in Figure 5.3. The results presented Figure 5.3 show that the tolerance limits for distance


Figure 5.2 - Potential Percent Speed Errors due to the Lower 90 th Percentile Timing Errors for the VASCAR Timing Mechanism


Figure 5.3 - Upper 90th Percentile Tolerance Limits for Distance Error
error tended to increase as distance increased. The upper 90th percentile tolerance limit for percent distance error is plotted in Figure 5.4. The results presented in this figure show that the tolerance limit for percent distance error tended to decrease as distance increased. The tolerance limits presented in these figures show that VASCAR does not have a distance measurement accuracy of 6.3 inches in one mile, as stated by the manufacturer, but the distance measurement error is well below .5 percent.

### 5.2 Experimental Results of VASCAR Speed Measurements <br> Moving Study

The following variables were investigated in the moving study to see if they had a significant effect on the moving clocks:

```
Group - Subjects grouped by nominal speed presentation
                            ranges ( }\pm2\mathrm{ or }\pm7\mathrm{ mph)
Course Distance
Nominal Speed
VASCAR Method
Subject Number
Replications
```

Eight subjects participated in this study. Each subject replicated the different test conditions four times. This resulted in a total of 384 trials.

An analysis of variance indicated the following variables and interactions between variables were statistically significant ( $\mathrm{p} \leq 0.05$ ) :

```
Course Distance
VASCAR Method
Subject Number
Interaction of Course Distance with VASCAR Method
Interaction of Nominal Speed with VASCAR Method
Interaction of Course Distance with Nominal Speed with VASCAR
Method
```

The fact that subject effects were significant in the moving study is not that surprising. This illustrates the variability between subjects often observed in human factors experiments.


A components of variance analysis was performed for this study. The results are presented in Figure 5.5. The differences in subjects accounted for only 3 percent of the variance. There was no replication effect observed. This suggests that little learning or fatigue occurred during the study.

Group (speed range presentation) was not a statistically significant effect. The mean and standard deviation for speed error for each group are presented in Table 5.3.

TABLE 5.3-- Mean and Standard Deviation for Speed Error for (mph) the Moving Study - Grouped by Nominal Speed Range

| Speed <br> Range | Subject <br> Numbers | Speed Error |  |
| :---: | :---: | :---: | :---: |
|  |  | Std. Dev. |  |
| $\pm 2$ | $1-4$ | .090 | .866 |
| $\pm 7$ | $5-8$ | .034 | .880 |

Since VASCAR method and several interactions involving VASCAR method were statistically significant, another analysis was performed on the data after it was separated by VASCAR method. For Following clocks, the following variables and interactions between variables were found to be statistically significant (p $\leq 0.05$ ):

Subject Number
Course Distance
Nominal Speed
Interaction of Course Distance with Nominal Speed

The only statistically significant variable for Approaching from the Rear clocks was:

Nominal Speed

Upper 90th percentile tolerance limits for speed error were calculated for each combination of VASCAR method, course distance, and nominal speed. These values are graphically presented in Figure 5.6. These values and values for the mean, variance, mean square error, and observed 95 th and 99 th percentile speed errors are tabulated in Appendix I.


Day to Day Variance-Due to Replication=0\%

From Figure 5.6, the upper 90th percentile tolerance limits increased as the speed increased and decreased as course distance increased. The tolerance limits for the Following method were slightly lower than those for the Approaching from the Rear method at 45 and 60 mph (. 126 to .319 mph lower), but were slightly higher at 80 mph (. 205 to .351 mph higher). Since the tolerance limits for Following and Approaching from the Rear are within .5 mph of each other, there was no practical difference between the two VASCAR methods.

The speed error for each clock in this study is plotted as function of the clock duration in Figure 5.7. In Figure 5.7, all the clocks that were greater than 5 seconds in duration had less than $a+2$ mph speed error. This figure clearly shows that speed errors decrease as the time in the course increases.

The subjects were asked to indicate the realism of each aspect of the study on scale from 1 to 5,1 being not at all realistic and 5 being very realistic. The range of values and mean values are presented in Table 5.4. On average, the officers felt the .3 mile long clocks were more realistic than the .1 mile clocks.

TABLE 5.4 -- Range and Mean Values for Subject Rating of Realism for the Moving Study

| Conditions | Range | Mean |
| :---: | :---: | :---: |
| Following, .1 mile | $2-5$ | 3.25 |
| Following, . 3 mile | $3.5-5$ | 4.56 |
| Approach from Rear, .1 mile | $2-5$ | 3.88 |
| Approach from Rear, .3 mile | $3-5$ | 4.50 |

When asked what parts of the study were not realistic, one subject stated that the Approaching from the Rear clocks were less difficult than the Following clocks because it was easier to anticipate the target vehicle crossing the reflector plate when it was Approaching from the Rear. Referring to Figure 4.1, the subject following the target vehicle $\left(S_{1}\right)$ had to react to the plate coming underneath the target vehicle. The subject in front of the target vehicle ( $\mathrm{S}_{2}$ ) could maintain visual contact with the reflector plate until the target vehicle passed it. This subject thought the Approaching from the Rear clock was more of an anticipation to the target vehicle crossing the reflector plate, and the



Figure 5.7-speed Error as a Function of Clock Duration for the Moving study

Following clock was more of a reaction to the reflector plate appearing from underneath the target vehicle. At 80 mph , the subjects had less time available to detect the reflector plate and to estimate when the time switch should be turned on and off. This may explain why the upper 90th percentile tolerance limits at 80 mph were lower for the Approaching from the Rear method than those for the Following method.

When asked how they would re-design the study, several officers stated they would improve the reference markers. Instead of using the reflector plate, they would have preferred a line going all the way across the lane of traffic. They thought this would be more realistic and would produce an anticipation of the target vehicle crossing the reference marker instead of a reaction to the reference marker appearing from underneath the car. In the real world, reference markers like tar marks, pavement changes, and expansion joints do run all the way across the road.

Based on their own intuition, the subjects were asked to rank the different types of clocks from the most accurate to the least accurate. All of the subjects felt the .3 mile clocks would be more accurate than the .1 mile clocks. Seven of the eight subjects felt the Following clocks would be more accurate than the Approaching from the Rear clocks. A complete list of the subjects' ratings is in Appendix $G$.

## Night Moving Study

As with the moving study, all of the subjects results were grouped together for the statistical analysis. The following variables were examined in the night moving study:

> Subject Number
> Nominal Speed
> Light Condition - using .3 mile long Following clocks from moving study as a comparison

Six subjects participated in this study. Each subject repeated each test condition twice. This resulted in a total of 36 trials.

The following interaction between variables was found to be statistically significant ( $\mathrm{p} \leq 0.05$ ) :

## Interaction of Light Condition with Nominal Speed

Upper 90th percentile speed errors were calculated for each nominal speed for both day and night time conditions. These values are graphically presented in Figure 5.8. From Figure 5.8, the upper 90th percentile speed error increased as speed increased for both day and night light conditions. The night moving clocks upper 90th percentile speed errors were all less than .35 mph different than the comparable day time clocks. This suggests that there was no practical difference between day and night time Following clocks.

The speed error for each clock in this study is plotted as a function clock duration in Figure 5.9. All of the clocks in this study had errors between $\pm 2$ mph.

The subjects were asked to judge the realism of the night moving study. All of the subjects that participated said this study was very realistic. They each rated this study as a 5 on a scale'l to 5 . The subjects did not suggest any improvements for this study.

## Bridge Study - Moving Portion

The following variables were investigated in the moving portion of the bridge study:

> Subject Number
> Nominal Speed
> Gap Distance

Six subjects participated in this study. Four subjects either repeated or replicated each test condition twice, while the other two replicated each test condition three times. This resulted in a total of 56 trials.


Figure 5.8 - Upper 90 th Percentile Tolerance Limits for speed Error - Day and Night Time Following clocks


The following interaction betweer variables was found to be significant ( $p$ $\leq 0.05$ ):

## Interaction of Subject Number with Nominal Speed

The interaction between Subject Number with Nominal Speed was also significant for the Following clocks in the moving study. Gap distance was not a statistically significant variable. This suggests that as long as the subject could see the bridge shadow cross the vehicle, the gap distance between the vehicles did not influence the accuracy of the VASCAR clock.

Speed error is plotted as a function of clock duration in Figure 5.10. All of the clocks in this study had errors between $\pm 2 \mathrm{mph}$.

The subjects' rankings of the realism of this study are in Table 5.5. The first set of rankings are for subjects 1 and 2 while the second set are for subjects 3 - 6 . As stated in Chapter 4 , subjects 1 and 2 had bridge shadows that were only half as wide as those for subjects $3-6$. Subjects $3-6$ ranking of the moving portion of the study was much higher than subjects 1 and 2 , which suggests that the double width of bridge shadow significantly increased the realism of the moving portion of the bridge study.

TABLE 5.5 -- Range and Mean Values for Subject Rating of the Realism for the Moving Portion of the Bridge Study

| Conditions | Range | Mean |
| :---: | :---: | :---: |
| Subject 1 and 2 |  |  |
| Short Gap Distance | 1 | 1.00 |
| Long Gap Distance | 1 | 1.00 |
| Subjects 3 - 6 |  |  |
| Short Gap Distance | $2-5$ | 4.25 |
| Long Gap Distance | $4-5$ | 4.75 |

Most of the subjects comments on the bridge study were concerned with the stationary portion. The only comments concerning the moving portion of the study was the size of the bridge shadow. They felt it should have been longer and wider.


Figure 5.10-speed Error as a Function of clock Duration for the Moving Portion of the Bridge study

The subjects generally gave similar rankings for the accuracy of these clocks as they gave for the .3 mile following clock of the moving study. Most of the subjects felt there was little difference between the two gap distances. Only one subject (subject 5) did not rank the two gap distances consecutively.

## Bridge Study - Stationary Portion

The following variables were examined in the stationary portion of the bridge study:

```
Subjects
Nominal Speed
Viewing Method - Direct vs. Indirect (mirrors)
```

The stationary portion of the bridge study had the same number of trials as the moving portion (56 trials).

The following variables and interactions between variables were found to be statistically significant (p $\leq 0.05$ ) :

```
Subject Number
Nominal Speed
Interaction of Subject Number with Viewing Method
Interaction of Subject Number with Nominal Speed
Interaction of Subject Number with Viewing Method with Nominal
Speed
```

The variable viewing method was not found to be statistically significant, but several interactions between variables with viewing method were. The upper 90th percentile tolerance limit for each combination of viewing method and nominal speed is presented in Figure 5.11. The upper 90th percentile tolerance limits for the indirect vision method were slightly higher than those for the direct vision method (less than .41 mph higher). This suggests that there is no practical difference for the interaction between nominal speed with viewing method.

Speed error is plotted as a function of clock duration in Figure 5.12. There was one outlier in the data that is marked in this figure. This outlier was probably due to a secondary shadow. During certain parts of the day, the
test center control tower would cast a shadow across the course of the target vehicle. This shadow occurred before the first bridge shadow (see Figure 5.13). The subjects had trouble distinguishing between the two shadows. They would start their clocks using the shadow from the control tower only to realize they had started early. Most of the time this was caught. The clock marked as an outlier in Figure 5.12 was the only one that was not. This outlier was not used in calculating the tolerance limits, nor was it used to determine what variables were significant.

The subjects' ranking of the realism of this portion of the bridge study are in Table 5.6. As with the moving portion, the first set of rankings is for subjects 1 and 2 , while the second set is for subjects 3 - 6 .
$\begin{aligned} \text { TABLE 5.6-- } & \text { Range and Mean Values for Subject } \\ & \text { Rating of the Realism for the } \\ & \text { Stationary Portion of the Bridge Study }\end{aligned}$

| Conditions | Range | Mean |
| :---: | :---: | :---: |
| Subject 1 and 2 |  |  |
| Direct Vision | 1 | 1.00 |
| Indirect Vision | 1 | 1.00 |
| Subjects 3 - 6 |  |  |
| Direct Vision | $2-3$ | 2.25 |
| Indirect Vision | $2-3$ | 2.25 |

The double width of the bridge shadow did not increase the subjects ranking of the realism of this portion of the study as much as in the moving portion of the study. The subjects had very strong comments concerning this portion of the bridge study. They felt the bridge shadows were much to small. The shadow at the beginning of the course was not visible. They said they were reacting to the shadow crossing the vehicle instead of anticipating the vehicle passing through the shadow. This would explain why most of the clocks had positive speed errors. (see Figure 5.12) Since the subjects were reacting to the first bridge shadow, the time of their clocks were likely less than the true time. This shorter time produced a higher estimated speed.


Figure 5.11 - Upper 90th Percentile Tolerance Limits for speed Error - The stationary Portion of the Bridge study
 Portion of the Bridge Study


Figure 5.13-Control Tower shadow

There were several suggestions for improvement of this study. Widening the shadow, elevating the subject, and using a vehicle in front of the target vehicle were suggested as possible ways to produce a test condition that allows more anticipation instead of reaction.

All of the subjects thought their direct vision clocks were more accurate than the indirect vision clocks, but each subject ranked them consecutively among all the different types of clocks performed in this study. This suggests they did not think there was a large difference in the accuracy of the two methods.

## Parking Study

The following variables were studied in the parking study:

Subject Number
Nominal Speed
Course Distance
Replications

Four subjects participated in this study. Each subject replicated the test conditions three times. This resulted in a total of 48 trials.

The only statistically significant variable ( $\mathrm{p} \leq 0.05$ ) was:
Subject Number
Only one interaction between variables was found to be nearly significant ( $0.05 \leq 1.0$ ) :

Interaction of Course Distance with Nominal Speed ( $p=0.07$ )

The upper 90th percentile tolerance limit for each combination of course distance and nominal speed is plotted in Figure 5.14. The upper 90th percentile tolerance limits increased as speed increased and decreased as course length increased. The tolerance limits for the 200 foot course were 1.9 to 2.3 mph higher than those for the $1 / 10$ mile ( 528 foot) course.

Speed error is plotted as a function of clock duration in Figure 5.15. As seen in this figure, there were very few clocks made in this study. This was



Figure 5.15 - Speed Error as a Function of Clock Duration for the Parking study
primarily due to weather conditions. Sunny days were required to produce the bridge shadow used as a reference marker in this study. Because of the small number of trials in this study, some caution is advised when interpreting the results.

The subjects' strongest suggestion for improvement of this study was the elimination of the 200 foot clocks. They felt this distance was too short to produce an accurate clock. They also thought a larger bridge shadow would improve the accuracy of the clocks.

The subjects ranked the accuracy of the 200 foot course distance much lower than the $1 / 10 \mathrm{mile}$ course distance.

## Angular Study

The following variables were investigated in the angular study:

Group - Subjects grouped by nominal speed presentation ranges ( $\pm 2$ or $\pm 7 \mathrm{mph}$ )
Subject Number
Replication
Viewing Distance
Elevation
Course Distance
Nominal Speed

Six subjects participated in this study. Each subject replicated the different test conditions four times. This resulted in a total of 576 trials.

The following variables and interactions between variables were found to be statistically significant ( $\mathrm{p} \leq 0.05$ ) :

[^0]The following interaction between variables was found to be nearly significant ( $0.05 \leq \mathrm{p} \leq 1.0$ ):

Interaction of Viewing Distance with Elevation with Course Distance ( $\mathrm{p}=0.08$ )

A components of variance analysis was performed for this study. The results are presented in Figure 5.16. The differences in subjects accounted for 23 percent of the variance. This number may be artificially high due to the differences between the two nominal speed range groups (these differences are discussed further later in this section). As with the moving study, replication was not an effect. This suggests that neither learning nor fatigue occurred during the study.

Since the alignment of the pole was different for the two course distances (please see Figure 4.5), and because course distance was statistically significant by itself and in combination with other variables, a statistical analysis was performed on each course distance.

For the 528 foot course length, the following variables and interactions between variables were found to be statistically significant ( $\mathrm{P} \leq 0.05$ ) :

Subject Number
Viewing Distance
Nominal Speed
Interaction of Group with Viewing Distance with Elevation

A components of variance analysis was performed for the 528 foot clocks and is presented in Figure 5.17. For these clocks, replication was not significant.

Although the interaction of group with viewing distance with elevation may be statistically significant, from a practical standpoint these differences were very small. The mean speed error for each combination of elevation and viewing distance for the $\pm 2 \mathrm{mph}$ speed range group is plotted in Figure 5.18.a. The same mean speed errors for the $\pm 7 \mathrm{mph}$ speed range group are displayed in Figure 5.18.b. There was only a .4 mph range for all of the mean speed errors for each


Day to Day Variance-Due to Replication=0\%

Figure 5.16-Components of Variance for the Angular study - Overall study


Day to Day Variance-Due to Replication $=0 \%$


Figure 5.18.a - Mean Speed Error as a Function of Viewing Distance and Elevation for the 528 Foot Course Distance - Group 1


Figure 5.18.b - Mean Speed Error as a Function of Viewing Distance and Elevation for the 528 Foot Course Distance - Group 2
group $x$ viewing distance $x$ elevation combination (mean speed errors ranged from -0.51 to -. 11 mph ).

Upper 90th percentile tolerance limits for all the combinations of elevation $x$ viewing distance $x$ nominal speed for the 528 foot course distance are presented in Figure 5.19. These tolerance limits range from . 478 to 1.419 mph . Even though viewing distance and nominal speed were statistically significant, all of the combinations of conditions produced upper 90th percentile tolerance limits that were less than 1.5 mph .

For the 200 foot course distance, the following variables and interactions between variables were found to be significant ( $p \leq 0.05$ ):

```
Subject Number
Replications
Viewing Distance
Nominal Speed
Interaction of Group with Viewing Distance
```

The following variable was found to be nearly significant ( $0.05<\mathrm{p} \leq 1.0$ ):

$$
\text { Group } \quad(p=0.09)
$$

The mean speed error for each group $x$ viewing distance combination is plotted in Figure 5.20. The mean speed errors for the $\pm 2 \mathrm{mph}$ speed range group and the $\pm 7 \mathrm{mph}$ speed range group are significantly different. This suggests that the differences between methods of presenting nominal speed did affect the accuracy of the speed measurements for the 200 foot course distance.

A component of variance analysis was performed on the 200 foot clocks and is presented in Figure 5.21.

This portion of the angulax study was the only occurrence with replication being a significant variable. As seen in Figure 5.21, replication was only 2 percent of the variance. The average speed error for each replication is plotted in Figure 5.22. The average speed was fairly constant until the fourth replication. Since subjects were concerned with the alignment of the pole for


Figure 5.19 - Upper 90th Percentile Tolerance Limits for Speed Error - The Angular study - 528 Foot Course Distance


Figure 5.20-Mean speed Error as a Function of Viewing Distance for the 200 Foot Course Distance



Figure 5.22 - Mean speed Error as a Function of Replication Number for the 200 Foot Course Distance
the 200 foot clock, by the fourth replicate, they may have adjusted to compensate for the alignment problem. As seen in Figure 5.22, the average speed error did improve for the fourth replication.

Upper 90th percentile tolerance limits for all the combinations of elevation, viewing distance, and nominal speed for the 200 foot course distance are presented in Figure 5.23. The upper 90th percentile tolerance linits were lower for the longer viewing distance ( 528 feet). This was not surprising. The differences in the line of sight for the two viewing distances are shown in Figures 5.24.a and 5.24.b. The target vehicle covered a shorter distance when it reached the line of sight for the 200 foot viewing distance (5.24.a) than it did for the 528 foot viewing distance (5.24.b). Since this is the case, the subjects toggled the time switch off sooner for the shorter viewing distance than they did for the longer viewing distance. This resulted in higher estimated speeds for the shorter viewing distance.

Referring to Figure 5.23, at the 200 foot viewing distance, there was very little difference between the ground level and the elevated 90th percentile tolerance limits. The same was true for the 528 foot viewing distance, except at 80 mph . At 80 mph , the upper 90th percentile tolerance limit for grourd level was 2.6 mph lower than it was for the elevated level.

In Figure 5.25, speed error is plotted as a function of clock duration for all of the angular clocks. The clocks above 4 seconds in length were for the 528 foot course distance and those below 4 seconds are for the 200 foot course length. All of the clocks for the 528 foot course distance had less than a +2 mph speed error.

The subjects thought the 528 foot course distance was much more realistic than the 200 foot course distance. They also thought the longer viewing distance was more realistic than the shorter viewing distance. These same results were found when they were asked to rank their accuracy for the different conditions. They thought they were more accurate on the 528 foot course distance and were more accurate for the longer viewing distance.


Figure 5.23 - Upper 90 th Percentile Tolerance Limits for speed Error - the Angular study - 200 Foot Course Distance


200 Foot Viewing Distance


528 Foot Viewing Distance


Figure 5.25 - Speed Error as a Function of clock Duration for the Angular Study

The subjects strongest suggestions for improvement of this study was to align the reference marker for the 200 foot course distance (see Reference Marker Alignment section of Section 4.3). The subjects also thought the 200 foot course distance should be eliminated from the study.

## Reference Marker Alignment Study

The following variables were examined in the reference marker alignment study:

Subjects
Nominal Speed
Replication
Alignment: - Using the comparable unaligned clocks from the angular experiment

Only two subjects participated in this study. They replicated each test condition four times. This resulted in a total of 24 trials.

The following variables were found to be statistically significant ( $\mathrm{p} \leq$ 0.05):

Alignment
Subject Number

The mean speed errors for both aligned and unaligned clocks are presented in Figure 5.26. Aligning the pole with the subjects line of sight resulted in mean speed errors that were very close to zero.

In Figure 5.27, speed error is plotted as a function of clock duration for the aligned clocks. These clocks ranged from $\pm 4 \mathrm{mph}$. The comparable unaligned clocks ranged from -1.3 to +7.4 mph .

The results of this study suggest that it is very important that the reference marker be in the subjects' line of sight. This point is made in the VASCAR manual.


Figure 5.26 - Mean Speed Error for the Aligned and Unaligned Reference Marker


Figure 5.27-speed Error as a Function of clock Duration for the Reference Marker Alignment Study

The subjects thought aligning the reference marker was more realistic, but they still thought the 200 foot course distance was not long enough.

## Reference Marker Comparison

The test conditions for the 250 foot gap distance in the moving portion of the bridge study were very similar to those for the .3 mile long following clocks performed in the moving study. The only difference between the two was the type of reference marker. For the moving study the reference marker was the photocell reflector plate, for the bridge study it was the bridge shadow. An analysis was performed comparing the differences between the two types of reference markers. For this analysis, the following variables were studied:

> Subjects
> Nominal Speed
> Reference Marker Type

None of these variables were found to be statistically significant ( $p \leq$ 0.05). The following variables were found to be nearly significant:

Reference Marker Type ( $p=0.051$ )
Subjects ( $p=0.07$ )
The mean and upper 90th percentile tolerance limits for each reference marker type are given in Table 5.7. The mean speed errors for each reference marker type were less than $1 / 4 \mathrm{mph}$ different, and the upper 90 th percentile speed errors were less than $1 / 2$ mph different. This suggests there was no practical difference between the reference marker types.

TABLE 5.7-- Mean and Upper 90th Percentile Tolerance Limits for Speed Error for Different Reference Marker Types

| Reference Marker <br> Type | Mean <br> Speed <br> Error <br> (mph) | Upper 90th <br> Tolerance <br> Limit <br> (mph) |
| :---: | :---: | :---: |
| Reflector Plate <br> Bridge Shadow | .106 | 0.918 |

## VASCAR Experience Level

Since all 8 subjects participated in the moving study, it was used to examine the effect of VASCAR experience. Four subjects had less than 1.5 years experience and the other four had 7 or more years experience. For the Following method, experience was not statistically significant. For the Approaching from the Rear method, experience was statistically significant. The mean and standard deviation for each group are presented in Table 5.8.

TABLE 5.8-- Mean and Standard Deviation for Speed Error for the Approaching from the Rear Method - Grouped by VASCAR Experience Level

| Vascar <br> Experience <br> Level | Subject <br> Numbers | Speed Error |  |
| :---: | :---: | :---: | :---: |
|  |  | Std. Dev. |  |
| $<1.5$ | $1,4,6,7$ | .094 | .643 |
| $\geq 7$ | $2,3,5,8$ | .394 | .705 |

From the results presented in Table 5.8 , the subjects with less experience performed slightly better than those with more experience. The mean speed error for the subjects with more experience was only .3 mph higher than the mean speed error for the subjects with less experience. This would suggest little practical difference between the two experience levels.

Speed Error as a Function of Clock Time

Table 5.9 lists the mean and upper 90 th percentile tolerance limits for speed error for the overall study, all of the moving clocks performed in this study (moving study, night moving, and moving portion of bridge study), and for all the stationary clocks performed in this study (stationary portion of bridge study, parking study, angular study, and reference marker alignment study). The corresponding values for percent speed error are in Table 5. 10.

TABLE 5.9 -- Mean and Upper 90th Percentile Tolerance Limits for Speed Error (mph)

| Portion of <br> Study | Mean | Upper 90th <br> Percentile |
| :---: | :---: | :---: |
| Overall | .426 | 3.134 |
| Moving | .105 | 1.540 |
| Stationary | .644 | 4.074 |

TABLE 5.10-- Mean and Upper 90th Percentile Tolerance Limits for Percent Speed Error

| Portion of <br> Study | Mean | Upper 90th <br> Percentile |
| :---: | :---: | :---: |
| Overalt | .638 | 4.530 |
| Moving | .164 | 2.230 |
| Stationary | .959 | 5.886 |

Speed error is plotted as a function of clock time for all the moving clocks in Figure 5.28. For all of the moving clocks greater than 5 seconds in duration, the speed errors are less than +2 mph . The mean and upper 90 th percentile tolerance limits for speed error and percent speed error for the moving clocks greater than 5 seconds in duration are presented in Table 5.11

TABLE 5.11 -- Mean and Upper 90th Percentile Tolerance Limits for Moving Clocks Greater Than 5 Seconds in Duration

| Dependant <br> Variable | Mean | Upper 90th <br> Percentile |
| :---: | :---: | :---: |
| Speed Error | .150 | 1.146 |
| Percent <br> Speed Error | .232 | 1.893 |



Figure 5.28 - Speed Error as a Function of Clock Duration for all Moving clocks

Speed error is plotted as a function of clock time for all the stationary clocks in Figure 5.29. For the stationary clocks greater than 4 seconds in duration, the speed errors are less than +4 mph . The mean and upper 90th percentile tolerance limits for speed error and percent speed error for the stationary clocks greater than or equal to 4 seconds in duration are presented in Table 5.12.

TABLE 5.12 -- Mean and Upper 90th Percentile Tolerance Limits for Stationary Clocks Greater Than or Equal to 4 Seconds in Duration

| Dependant <br> Variable | Mean | Upper 90th <br> Percentile |
| :---: | :---: | :---: |
| Speed Error | -.072 | 1.567 |
| Percent <br> Speed Error | -.118 | 2.188 |

From the results presented in Tables 5.9 through 5.12, VASCAR-plus does not have a speed measurement accuracy of $\pm 1$ percent, but an upper 90 th percentile tolerance limit ( 95 percent of the values are less than or equal to this limit) of +2 mph is achievable.

### 6.0 SUMMARY AND RECOMMENDATIONS

In this chapter, a summary of the findings is presented on the accuracy of VASCAR speed measurement capability and recommendations are made for VASCAR operation. These findings are based on the results of the testing and analysis documented in this report. It is very important to note that no one table or figure can stand alone. The raw data, the statistics, the laboratory environment, and the subjects' opinions of the different test conditions must all be taken into account before any conclusions can be drawn.

### 6.1 Summary ,

The results of this study show that VASCAR-plus does not have an overall speed measurement accuracy of $\pm 1$ percent. It does appear that an upper 90 th percentile tolerance limit of +2 mph is achievable. This requires determining


Figure 5.29-Speed Error as a Function of Clock Duration for all stationary clocks
minimum distances or minimum timing durations for the different VASCAR methods.
The following statements support this overall finding:

1. The VASCAR-plus timing mechanism had a lower 90 th percentile tolerance limit of -0.0422 seconds. The speed error resulting from this timing error varies with course length and speed. For courses $1 / 10$ mile or longer, the speed error is less than 1.2 mph (up to 100 mph ). For course lengths greater than the mean preforred course distance (0.29mile - from the personal interview results), the potential speed errors due to the timing mecharism are less than .5 percent.
2. The VASCAR-plus timing mechanism was always biased against the motorist, i.e., the true time was always greater than the VASCAR time, and hence the true speed was less than the VASCAR speed (this is only the timing mechanism, no hunan factors considered)
3. She upper 90th percentile tolerance limits for distance measurement were greater than the 6.3 inches statfd in the VASCAR user manual, but they were well below .5 percent.
4. In general, the upper oth percentile tolerance limits for speed error tended to increase as speed increased, and decrease as course distance increased.
5. For all of the moving clecks in this study, all but one combination of course distance and nominal speed produced upper 90 th percentile tolerance limits lower than +2 mph. The only combination that did not was the .1 mile course distance and the 80 mph nominal speed combination.
6. There was little practical differerce between directly viewing the target vehicle and indirectly viewing the target vehicle using, mirrors. There was less than a .36 mph differerice between Following and Approaching from the Rear upper 90th percentile tolerance limits for every combination of course distance and nominal speed studied. There was less than a .41 mph difference between the upper 90 th percentile tolerance limits for direct and indirect vision parking clocks for each nominal speed studied.
7. There were very small differences between the upper 90 th percentile tolerance limits for day time and night time Following clocks (less than .35 mph ).
8. As long as the officer could observe the vehicle pass the refererice marker, viewing distance was not practically siguificant. For the moving bridge clocks, gap distance was not statistically significant. For the 528 font angular clocks, there was 1 ittle difference between the short and long viewing distances. The upper 95 th percentile tolerance limits for the short and long viewing distances were less than $1 / 4 \mathrm{mph}$ different for each combination of nominal speed and elevation.
9. Except for two cases, the upper 90th percentile tolerance limits for the two elevation levels were less than .5 mph different for each combination of nominal speed, course distance, and viewing distance.
10. It is very important that the reference markers be in the officer's line of sight (see Figures 4.5 and 4.6). For the 200 foot Angular clocks, when the pole was aligned, the mean speed errors were close to zero. When the pole was not aligned, the mean speed errors were as high as 4 mph .
11. For the 528 foot long angular clocks, all of the upper 90 th percentile tolerance limits were less than +1.5 mph .
12. Parking clocks were performed in both the parking study and the stationary portion of the bridge study. In the parking study, most of the upper 90 th percentile tolerance limits were well above +2 mph . Even for the 11 mile course distance, the upper 90 th percentile tolerance limits were as high as 5.82 mph . In the stationary portion of the bridge study, all of the upper 90 th percentile tolerance limits were below +2.4 mph . The upper 90 th percentile tolerance limits in the bridge study were probably lower than those in the parking study due to the longer course distance (. 3 mile vs. 200 feet and .1 mile ). It is important to remember that the subjects had strong opinions about how unrealistic the conditions in these two studies were. Real world Parking clocks may be more accurate and precise.
13. The amount of the speed error variance due to subject differences was dependent on the VASCAR method used. Differences between subjects accounted for only 3 percent of the variance in the moving study. This suggests that there was little difference between subjects for the moving clocks. Subject differences accounted for 23 percent of the variance in the angular study. This suggests that there were differences between subjects for angular clocks. This number may be artificially high due to the group effect (grouped by nominal speed ranges). For the 200 foot course distance, the subjects with the $\pm 2$ mph speed range performed much differently than those subjects with the $\pm 7 \mathrm{mph}$ speed range. Differences between subjects are not that surprising in human factors studies.
14. The group effect (nominal speed ranges) was only found to be practically significant for the 200 foot Angular ciocks performed in this study. The subjects with the $\pm 2 \mathrm{mph}$ speed range performed better than those with the $\pm 7 \mathrm{mph}$ speed range for these clocks. There were not practical or statistical differences between groups for the 528 foot Angular clocks, or for the Moving clocks.
15. VASCAR experience was not practically significant.
16. Replication was only an effect in a portion of the angular study. Replication was not an effect in any other study. This suggests that the subjects did not learn or tire during, the study. In other words, they did not improve as the study progressed. For the 200 foot clocks
in the angular study, the subjects did show a significant improvement on the fourth replication. The subjects did not think the set up for this course was appropriate. By the last day of testing they may have adjusted their technique to compensate for the experimental conditions (see Figure 5.22).
17. For all of the moving clocks greater than 5 seconds in duration, the upper 90 th percentile tolerance limit for speed error was 1.146 mph ( 1.893 \%). For all of the stationary clocks greater than 4 seconds in duration, the upper 90 th percentile tolerance limit for speed error was 1.567 mph ( 2.188 \%).

### 6.2 Recommendations

The following recommendations are given for VASCAR operation and for improvements of the VASCAR-plus manual.

1. When setting up a course for a stationary clock, the officer should choose a course length that will give a time duration of at leasi 4 seconds for the expected maximum speed. For example, in a 25 mph speed zone, an expected maximum speed might be 45 mph. A cai will travel .05 miles (264 ft) in 4 seconds at 45 mph , so we are recommending that the officer use a course length of at least . 05 miles. If a motorist goes through the course faster than 4 seconds, the potential speed error will increase, but it will be obvious that the motorist is well above the posted speed limit.
2. When using VASCAR-plus for moving clocks (Following and Approaching from the Rear), clock durations of at least 5 seconds should be used.
3. The VASCAR-plus manual should be revised to reflect the accuracy when it is used by human operators.

## APPENDIX A

## Personal Interview Form

$\qquad$
Start Time Respondent

Hello my name is $\qquad$ . Is $\qquad$ there?
(Mr., Officer, etc.) $\qquad$ . I represent the Transportation Research Center and I have been assigned as the research engineer on study sponsored by the National Highway Traffic Safety Administration dealing with speed measurement techniques used by police officers. Your department gave me your name as an officer who could help us in our study. I understand that as part of your job as an officer, that you are responsible for enforcing posted speed limits. Is this the case? (if not, end interview)

I'd like to ask you a few questions about this area of law enforcement, if I may. It will take about 20 minutes. The information that you share with me will be completely confidential. No one but our research group will see my notes. We expect to use what we learn from officer interviews to help us develop important features for some field tests of equipment that we have planned.

Is this a good time to talk or can I call you back at a specific time that would be more convenient? (set up a call back if needed) Date, time, and phone \# for call back:

QUESTIONS
A major focus of our research is the use of VASCAR. So most of my questions deal with your experience with and opinions of VASCAR.

1. How familiar are you with VASCAR? (check off the phrase which is most descriptive of the respondent's answer)


1a. Do you currently use VASCAR or VASCAR-plus?
_ VASCAR ___ VASCAR-plus
2. What kind of training have you had on VASCAR?
a. Nature (where and when) and amount (estimate of hours) of FORMAL INCLASS training:
b. Nature and amount of supervised training:
c. Nature and amount of informal training (self study):

2a. How many months (or years) of VASCAR experience do you have?
3. On a scale of $1-10$, where $1=$ Novice and $10=$ Expert, what number would best reflect your VASCAR skills?
4. On what type of roadway (s) do you use VASCAR?
$\qquad$ other
5. What percent of your overall VASCAR use has been at night? $\qquad$
6. I would like to get an idea of how often you use the different methods of operation of VASCAR. I will list some common methods. Please give me an estimate of the percentage of time you use each VASCAR method. If you do not use a method, we will give it a zero value.

Police Car Moving $\qquad$
_ a. Following the Target Vehicle
b O. Opposite Direction
_ c. Target Vehicle Approaching from the Rear
Police Car Stationary $\qquad$
$\qquad$ a. Parking
b. T-Intersection
c. Angular Clocking

6a. Is your choice of VASCAR method in any way determined by day vs. night time use? Explain.
7. For methods with the police car stationary, what percent of the time do you use dial a distance vs. driving in the distance? $\qquad$ Dial $\qquad$ Drive

Ba. Which of the six methods described above do you have the greatest confidence in (i.e. has the best accuracy? Why? $\qquad$
bb. Which do you have the least confidence in (i.e. has the least accuracy)? Why?
9. What is the shortest course distance you typically use to make VASCAR speed measurements? $\qquad$ Feet Miles
10. What is the longest course distance you typically use to make VASCAR speed measurements? Feet $\qquad$ Miles
11. What is your preferred course distance?
12. What is the typical maximum distance (range) from your eye to a reference point? $\qquad$ Feet Miles
13. What objects do you use as stationary reference markers during the day? (could you list in order of preference)? (probe for specifics)
14. What objects do you use as stationary reference markers at night?
15. Do you use a reference marker inside your vehicle in laying out a course? (e.i. tape on window)
16. How is your choice of VASCAR method or references influenced by weather: conditions? Explain.
17. How often do you check the calibration of your VASCAR system? $\qquad$
18a. In using VASCAR, what is the speed accuracy that you believe you can achieve in typical operating conditions ( $\pm$ miles $/ \mathrm{hr}$ )?

18b. Is this accuracy a function of course length? stream speed? VASCAR method? ___ length ___ method

19a. Have you ever had to go to court to defend a VASCAR based speed citation?

19b. If yes, how do defendants or defense attorneys attack your VASCAR speed estimates?
20. What do you feel are the strengths of VASCAR?
21. What do you feel are the weaknesses of VASCAR?
22. Have you ever experienced a failure in VASCAR equipment operation? Explain.
23. Do you use Radar to establish target speeds? How often? $\qquad$
$\qquad$
24. Under what circumstances is VASCAR preferred over Radar? $\qquad$
25. Under what circumstances is Radar preferred over VASCAR? $\qquad$
26. It's been said that some officers prefer not to use VASCAR. Why do you think some officers avoid the use of VASCAR?
27. Did I get all you opinions on VASCAR?

## APPENDIX B

## Task Analysis Results

## table b. 1

clock target using following mode of vascar operation

acuity required in all

Visually search potential tream ahead of police car
stimate the target's speed
riving skill (required in al task elements) potential targ s likely over the posted speed limi

Decide to clock condition if

Officer makes initial speed judgements on an absolute scale and also relative to other vehicles in the traffic stream

In moving modes of VASCAR operation the officer has additional information from the police car speedometer which is not available in stationary clocking modes

As visibility is reduced, the distances over which VASCAR can be used are also reduced


## Task: Clock Target Using Following Mode of VASCAR Operation (Continued)

| Task Element | Sensory- <br> Perceptual <br> Requirements |
| :--- | :--- |
| Turn Time Switch | Obtain auditory <br> and tactile <br> feedback of <br> switch activation |


| Psycho- |  |  |
| :---: | :---: | :---: |
| Motor | Cognitive | Limiting |
| Requirements | Requirements | Factors |

Potential
Sources of
Errors

Radio operation requires the same hand used for VASCAR operation
Early switch
activation could
lead to under-
estimation of
true speed
Late switch
activation could
lead to over-
estimation of
true speed

Distance switch could be activated instead of or in addition to Time switch

Comments
To reduce reaction time delay officers initiate switch activation just prior to arrival of the target at the reference mark

Depth cues in
road scene (e.g.
other vehicles or
fixed objects
adjacent to
highway) aid in
arrival time
estimation



| Task Element | Sensory- <br> Perceptual <br> Requirements | ```Psycho- Motor Requirements``` | Cognitive Requirements | Limiting Factors | Potential Sources of Errors | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Observe Police Car's Approach to Second Reference Mark | Visually monitor location of second reference mark as police car proceeds through course | Estimate arrival time of police car at reference mark | Decide when Distance switch should be activated | Other traffic could obscure reference mark <br> Radio "chatter" |  | Depth cues in road scene (e.g., other vehicles or fixed objects adjacent to highway) aid in arrival time estimation |
| Turn Distance Suitch OFF | Obtain auditory <br> and tactile feedback of switch activation | Push toggle switch into DOWN position <br> Reaction time | Decide if switch was activated as police car passed reference mark | Radio operation requires the same hand as used for VASCAR operation | Early switch activation could lead to underestimation of true speed <br> Late switch activation could lead to overestimation of true speed <br> Time switch could be activated instead of or in addition to Distance switch | To reduce reaction time delay officers initiate switch activation just prior to the arrival of the police car at the reference mark <br> Time switch and Distance switch activation errors at both reference marks can have offsetting effects or additive effects which increase measurement error |

Task: Glock Target Using Following Mode of VASCAR Operation (Continued)


TABLE B. 2
CLOCK TARGET APPROACHING FROM THE REAR


| Task Element | Sensory- <br> Perceptual <br> Requirements | PsychoMotor Requirements | Cognitive Requirements | Limiting <br> Factors | Potential Sources of Errors | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Select First Reference Mark | Visually search road scene for suitable <br> reference mark (e.g., a bridge shadow, pavement color change, sign post, etc.) ahead of police car |  | Decide on the fixed object to use as the first reference mark in the course | Other vehicles can obscure objects <br> Visibility <br> Light levels limit the use of some types of reference marks |  | Depending on the availability of fixed objects ahead, the second reference mark may also be selected at this time; selection of the second reference mark is discussed later |
| Observe Police Car's Approach to First Reference Mark | Visually monitor location of first reference mark as police car proceeds toward course <br> Officers must allocate visual resources to three tasks: tracking the target in the police car mirrors, monitoring the reference mark ahead and driving | Estimate arrival time of police car at reference mark | Decide when Distance switch should be activated | Other traffic could obscure reference mark <br> Radio "chatter" |  | Depth cues in road scene (e.g., other vehicles or fixed objects adjacent to highway) aid in arrival time estimation |


|  | Task Element | SensoryPerceptual Requirements | PsychoMotor Requirements | Cognitive Requirements | Limiting <br> Factors | Potential <br> Sources of Errors | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\stackrel{\oplus}{N}$ | Turn Distance Switch ON | obtain auditory <br> and tactile feedback of switch activation | Push toggle switch into UP position <br> Drive police car with left hand, while operating VASCAR with right hand <br> Reaction time | Decide if switch was activated as police car passed reference mark | Radio operation requires the same hand used for operating VASCAR controls | Early switch activation could lead to overestimation of true speed <br> Late switch activation could lead to underestimation of true speed | To reduce reaction time delay officers initiate switch activation just prior to the arrival of the police car at the reference mark |
|  |  |  |  |  |  | rime switch could be activated instead of or in addition to Distance switch |  |
|  | Track Target to First Reference Mark | Visually monitor via mirrors the target's progress toward VASCAR course | Estimate arrival time of target at reference mark | Decide when Time switch should be activated | Other traffic could obscure target or reference mark |  | Depth cues in road scene aid in arrival time estimation |
|  | . | Officers must allocate visual resources to tracking the target, monitoring the position of the reference mark ahead and driving |  |  | Radio "chatter" |  | On multi-lane divided highways, officers can improve their view of target by positioning themselves in a lane adjacent to target |

Sensory-
Perceptual
Requirements

Obtain auditory
and tactile
feedback of

| Psycho- |  |  |
| :---: | :---: | :---: |
| Motor | Cognitive | Limiting |
| Requirements | Requirements | Factors |
| Push toggle switch into UP position | Decide if switch | Radio operation |
|  | was activated as | requires the same |
|  | target passed | hand used for |
|  | reference mark | VASCAR operation |
| Reaction time |  |  |


| Potential <br> Sources of <br> Errors |  |
| :--- | :--- |
| Early switch | Comments |


| Select Second | Visually search <br> road scene ahead <br> Reference Mark <br> for suitable |
| :--- | :--- |
|  | reference mark |
|  | (e.g., a bridge |
|  | shadow, sign |
|  | post) |


| Decide on the <br> fixed object to <br> use the second <br> reference mark in <br> the course | Other vehicles <br> can obscure <br> objects |
| :--- | :--- |
| Visibility |  |$\quad$| Light levels |
| :--- |
| limit the use of |
| some types of |
| reference marks |


| Task Element | Sensory- <br> Perceptual <br> Requirements |
| :--- | :--- |
| Observe Police | Visually monitor <br> Car's Approach to <br> Second Reference <br> Mark |
| location of <br> second reference <br> mark as police |  |
| car proceeds |  |
| through course |  |


| Psycho- |  |  |
| :---: | :---: | :---: |
| Motor | Cognitive | Limiting |
| Requirements | Requirements | Factors |

Potential
Sources of
Errors

Other traffic
could obscure reference mark

Radio "chatter"

## Turn Distance

 Switch OFF> Obtain auditory and tactile feedback of switch activation

Reaction time

## switch into DOWN position

Estimate arrival time of police car at reference mark

Distance switch should be activated

Decide if switch was activated as police car passed reference mark

Radio operation requires the same hand as used for VASCAR operation

Early switch activation could lead to underestimation of true speed

Late switch activation could lead to overestimation of true speed

Time switch could be activated in addition to or instead of Distance switch

## Comments

Depth cues in road scene aid in arrival time estimation

Officers typically read the police car speedometer several times during a moving clock

To reduce reaction time delay officers delay officers
initiate switch activation just prior to the arrival of the police car at the reference mark

| Task Element | SensoryPerceptual Requirements | ```Psycho- Motor Requirements``` | Cognitive Requirements | Limiting <br> Factors | Potential Sources of Errors | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Track Target Vehicle to Second Reference Mark | Visually monitor target's progress toward second reference mark using mirrors <br> Visual resources must be allocated to tracking the target, monitoring the reference mark and driving | Note if target changes lanes while in course <br> Estimate arrival time of target at reference mark | Decide when Time switch should be activated | Other traffic could obscure target or reference mark <br> Radio "chatter" | Lane changing by target could lead to underestimation of true speed | Depth cues aid in arrival time estimation <br> Target and second reference mark are both to the rear of the police car |
| Turn Time Switch OFF | Obtain auditory and tactile feedback of switch activation | Push toggle switch into DOUN position <br> Reaction time | Decide if switch was activated as target passed the second reference mark | Radio operation requires the same hand as VASCAR operation | Early switch activation could lead to an overestimation of true speed <br> Late switch activation could lead to an underestimation of true speed <br> Distance switch could be activated instead of or in addition to Time switch | To reduce reaction time delay officers initiate switch activation prior to the arrival of the target at the reference mark <br> Time and Distance switch activation errors at both reference marks can have offsetting effects or additive effects that increase error |


|  | Task E1ement | Sensory- <br> Perceptual Requirements | PsychoMotor Requirements | Cognitive Requirements | Limiting <br> Factors | Potential Sources of Errors | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Read VASCAR <br> Display | Read speed value displayed <br> Viewing distance is approximately 30 inches <br> Character height is approximately one-half inch |  | Displayed speed is compared with initial speed judgement made by officer and to speedometer reading(s) obtained during the clocking procedure |  | Error by officer in reading VASCAR display or police car speedometer <br> Officer incorrectly recalls speedometer rezding(s) from memory |  |
| $\stackrel{\otimes}{6}$ | Assess Validity of Speed Measurement |  |  | Decide to accept (or reject) speed measurement based on switch activations, lane maintenance by target, speedometer reading(s) and displayed VASCAR reading |  |  |  |
|  | Decide whether or not to pursue |  |  | Decide to pursue target if measured speed is greater than speed limit plus an allowance factor for motorist error | Last second requirement for officer to attend to a more critical event (e.g., accident, violent crime, other emergency) |  | The decision to pursue a violator depends on the measured speed, the officer's ability to safely pursue, the police department policy for issuing speeding citations and the need for the officer's services elsewhere |

## APPENDIX C

## Results of Tests Conducted with VASCAR Display Covered

Two replicates of the short viewing distance clocks of the angular study were performed by two subjects with the VASCAR LED display covered. The results of these tests were compared to the results of similar tests from the first two replicates of the angular study performed by the same subjects with the VASCAR LED display uncovered. The mean and standard deviation for speed error for each course distance are listed in Table C.l.

TABLE C.1: Mean and Standard Deviation for Speed Error For Covered and Uncovered VASCAR LED Display

| Course <br> Distance | Uncovered Display |  | Covered Display |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Mean | Std. Dev. | Mean | Std. Dev. |
| 200 ft | 0.107 | 1.212 | 1.145 | 2.296 |
| $1 / 10 \mathrm{mi}$. | -0.449 | 0.587 | -0.582 | 0.663 |

The results presented in Table C. 1 show that there was little difference between the covered and uncovered display results at $1 / 10 \mathrm{mile}$ ( 528 feet), but there was a significant difference at 200 feet. This was the same result found with the group effect of the angular study. In the angular study, the effect of the nominal speed ranges ( $\pm 2 \mathrm{mph}$ and $\pm 7 \mathrm{mph}$ ) was studied. The results showed that the difference between groups was minimal for the 528 foot course distance, but it was significant for the 200 foot course distance.

Means and standard deviations for various test conditions with the 528 foot course distance are presented in Table C.2. The results presented in this table show that there were minimal differences between the results with and without the display covered for the 528 foot course distance.

TABLE C.2: Means and Standard Deviation for Various Test Conditions with the 528 Foot Course Distance

| Test <br> Condition | Uncovered Display |  | Covered Display |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Mean | Std. Dev. | Mean | Std. Dev. |
| ground | -0.358 | 0.741 | -0.489 | 0.426 |
| elevated | -0.539 | 0.392 | -0.674 | 0.889 |
| 45 | -0.272 | 0.348 | -0.330 | 0.588 |
| 60 | -0.125 | 0.398 | -0.470 | 0.517 |
| 80 | -0.948 | 0.642 | -0.944 | 0.771 |

Means and standard deviations for various test conditions with the 200 foot course distance are presented in Table C.3. The results presented in this table show there were significant difference between the results with and without the display covered for the 200 foot course distance.

$$
\begin{aligned}
\text { TABLE C. } 3: & \text { Means and Standard Deviation for } \\
& \text { Various Test Conditions with the } 200 \\
& \text { Foot Course Distance }
\end{aligned}
$$

| Test <br> Condition | Uncovered Display |  | Covered Display |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Mean | Std. Dev. | Mean | Std. Dev. |
| ground | 0.229 | 1.439 | 1.965 | 2.468 |
| elevated | -0.014 | 0.984 | 0.324 | 1.862 |
| 45 | 0.078 | 1.255 | 1.052 | 1.395 |
| 60 | 0.079 | 1.424 | 1.452 | 2.326 |
| 80 | 0.165 | 1.105 | 0.930 | 3.130 |

It is important to note that officers in the real world do not have their displays covered. The results of the task analysis showed that officers compare their initial speed assessment to their VASCAR clock. Using this assessment, and other information, the officers then decide whether or not they have a valid clock.

## APPENDIX D

Order of Trials

SUBJECTS A AND B

DAY 1

| Trial Number | Course Distance | VASCAR Method |  | Target Speed |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Subject A | Subject B |  |
| 1 | 0.3 mile | Leading | Following | 60 |
| 2 | 0.3 mile | Following | Leading | 45 |
| 3 | 0.3 mile | following | Leading | 60 |
| 4 | 0.3 mile | Leading | Following | 80 |
| 5 | 0.3 mile | Following | Leading | 80 |
| 6 | 0.3 mile | Leading | Following | 45 |
| 7 | 0.1 mile | Following | Leading | 45 |
| 8 | 0.1 mile | Following | Leading | 60 |
| 9 | 0.1 mile | Following | Leading | 80 |
| 10 | 0.1 mile | Leading | Following | 80 |
| 11 | 0.1 mile | Leading | Following | 60 |
| 12 | 0.1 mile | Leading | Following | 45 |

ORDER OF TRIALS FOR BRIDGE SESSION
SUBJECTS A AND B
DAY 1

|  |  | Subject A |  | Subject B |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Trial <br> Number | Target <br> Speed | VASCAR <br> Method | Gap/Viewing <br> Method | VASCAR <br> Method | Gap/Viewing <br> Method |
| 1 | 60 | Parking | Direct | Following | 250 ft <br> 2 |
| 3 | 80 | Parking | Indirect | Following | $1 / 8 \mathrm{mile}$ |
| 4 | 60 | Parking | Indirect | Following | $1 / 8$ mile |
| 5 | 80 | Following | 250 ft | Parking | Indirect |
| 5 | 80 | Following | $1 / 8 \mathrm{mile}$ | Parking | Direct |
| 6 | 60 | Following | $1 / 8 \mathrm{mile}$ | Parking | Direct |
| 7 | 60 | Following | 250 ft | Parking | Indirect |
| 8 | 80 | Parking | Direct | Following | 250 ft |

Gap/Viewing Method - Gap distance if a following clock; visual method if parking clock

## SUBJECTS A AND B

DAY 1

| Trial Number | Subject A | Subject B | Course Distance | Target Speed |
| :---: | :---: | :---: | :---: | :---: |
|  | Elev., Viewing Dis. | Elev., Viewing Dis. |  |  |
| 1 | Elevated, 200 ft . | Ground, 200 ft . | 1/10 mile | 60 |
| 2 | Elevated, 200 ft . | Ground, 200 ft . | 1/10 mile | 45 |
| 3 | Elevated, 200 ft . | Ground, 200 ft . | 1/10 mile | 80 |
| 4 | Elevated, 200 ft . | Ground, 200 ft . | 200 ft . | 80 |
| 5 | Elevated, 200 ft . | Ground, 200 ft. | 200 ft . | 45 |
| 6 | Elevated, 200 ft . | Ground, 200 ft . | 200 ft . | 60 |
| 7 | Ground, 200 ft. | Elevated, 200 ft . | 1/10 mile | 45 |
| 8 | Ground, 200 ft. | Elevated, 200 ft. | 1/10 mile | 60 |
| 9 | Ground, 200 ft . | Elevated, 200 ft . | 1/10 mile | 80 |
| 10 | Ground, 200 ft . | Elevated, 200 ft . | 200 ft . | 60 |
| 11 | Ground, 200 ft . | Elevated, 200 ft . | 200 ft . | 45 |
| 12 | Ground, 200 ft . | Elevated, 200 ft . | 200 ft . | 80 |
| 13 | Ground, 528 ft . | Elevated, 528 ft . | 1/10 mile | 45 |
| 14 | Ground, 528 ft . | Elevated, 528 ft . | 1/10 mile | 80 |
| 15 | Ground, 528 ft . | Elevated, 528 ft | 1/10 mile | 60 |
| 16 | Ground, 528 ft . | Elevated, 528 ft . | 200 ft . | 45 |
| 17 | Ground, 528 ft . | Elevated, 528 ft . | 200 ft . | 60 |
| 18 | Ground, 528 ft . | Elevated, $528 \mathrm{ft}$. | 200 ft . | 80 |
| 19 | Elevated, 528 ft . | Ground, 528 ft . |  |  |
| 20 | Elevated, 528 ft . | Ground, 528 ft . | 200 ft. | 60 |
| 21 | Elevated, 528 ft . | Ground, 528 ft . | 200 ft . | 45 |
| 22 | Elevated, 528 ft . | Ground, 528 ft . | 1/10 mile | 45 |
| 23 | Elevated, 528 ft . | Ground, 528 ft . | 1/10 mile | 60 |
| 24 | Elevated, 528 ft . | Ground, 528 ft . | 1/10 mile | 80 |

ORDER OF TRIALS FOR NIGHT MOVING STUDY
SUBJECTS A
!
DAY 1

| Trial <br> Number | Target <br> Speed |
| :---: | :---: |
| 1 | 45 |
| 2 | 60 |
| 3 | 60 |
| 4 | 80 |
| 5 | 45 |
| 6 | 80 |

DAY 1

| Trial <br> Number | Subject A <br> Course Distance | Subject B <br> Course Distance | Target <br> Speed |
| :---: | :---: | :---: | :---: |
| 1 | 200 ft. | $1 / 10$ mile | 60 |
| 2 | 200 ft. | $1 / 10 \mathrm{mile}$ | 80 |
| 3 | $1 / 10 \mathrm{mile}$ | $200 \mathrm{ft}$. | 80 |
| 4 | $1 / 10 \mathrm{mile}$ | 200 ft. | 60 |

ORDER OF TRIALS FOR REFERENCE MARKER ALIGNMENT STUDY
SUBJECT A
DAY 1

| Trial <br> Number | Target <br> Speed |
| :---: | :---: |
| 1 | 60 |
| 2 | 45 |
| 3 | 80 |

## APPENDIX E

## Testing Procedure and Protocol Statement

The Transportation Research Center (TRC) has been contracted by the National Highway Traffic Safety Administration to conduct a study to assess the speed measurement ability of VASCAR under various test conditions including Following, Approaching from the Rear, Angular, and Parking methods. In order to properly test VASCAR, it is very important that professionally trained and certified VASCAR users are a part of this study. The results of this testing may be used to refine or revise the VASCAR manual.

The testing of VASCAR will be performed at TRC test facilities. Other TRC testing will be conducted in close proximity to the testing you will be involved in. All of the personnel involved in testing will be in communication with the control tower and each other using hand held radios. The control tower will give warning if there is any testing being conducted that will interfere with the testing that you will be involved with. Proper protocol involved with the different testing areas will be thoroughly explained before testing begins.

If at any time during the study you do not wish to continue to complete the testing, you have the right to terminate your involvement in the study.

Some of the testing to be conducted will be at higher speeds ( 85 mph maximum). It is important that you are aware that there is some risk involved in testing at high speeds. This risk is minimized by having professional drivers involved in the testing conducted at the TRC.

As stated above, you will be performing Following, Approaching from the Rear, Angular, and Parking methods. If at any time you feel that you have an unacceptable clock (a clock you would not take when out on routine patrol), just mention that you have a bad clock, and the test will be repeated.

The true vehicle speed will be measured using a photocell. The speed from your clock will be compared to this true vehicle speed. During the course of testing we will not be able to provide you with information concerning the accuracy of your clocks. This information can be provided after testing has been completed.

The results of this testing will be kept confidential. The test results will be reported, but your name will never be associated with the data. The data will be labeled as Officer A, Officer B, etc.. You will be given a copy of your data 3 weeks following completion of this testing. These results will be sent directly to you. Your superior officers will not be given copies of individual results unless you chose to share the results provided to you. We will send you a copy of the final report when it is available. This report will contain a more thorough analysis of your results.

Finally, you should know how important your contribution is to this study. Without the dedication of professionals like yourself, this research would not be completed.

I have read and understand the explanation of the testing procedure and protocol. I also understand that I can terminate my involvement in this study at any time.

## APPENDIX F

Determination of Accuracy of Photocell Measurement System

As stated in section 4.4 , the target vehicle true speed was measured using a SUNX-RS-120H photocell, an RTI-815 analog acquisition board, and onboard computer. Several tests were run to determine the accuracy of this system. A Nicolet oscilloscope, triggered by electronic trip switches, was used as the standard. The trip switches were placed next to the photocell reflector plates. The Nicolet's timing resolution was set at 1 msec . The target vehicle covered a 100 foot course at nominal speeds of 45 and 80 mph . Both the Nicolet and the photocell system measured the time for the target vehicle to cover the 100 foot course. The results are presented in Table F.l.

Table F.1: Comparison of Photocell System and
Nicolet Time Measurements

| Trial <br> Number | Photocell <br> Time | Nicolet <br> Time | Time <br> Error |
| :---: | :---: | :---: | :---: |
| 1 | 0.880 | 0.880 | 0.0 |
| 2 | 0.881 | 0.881 | 0.0 |
| 3 | 0.874 | 0.874 | 0.0 |
| 4 | 0.877 | 0.877 | 0.0 |
| 5 | 0.880 | 0.880 | 0.0 |
| 6 | 0.879 | 0.879 | 0.0 |
| 7 | 1.506 | 1.506 | 0.0 |
| 8 | 1.408 | 1.408 | 0.0 |

As seen in Table F.1, the photocell system and the Nicolet oscilloscope gave the same exact times.

APPENDIX G

Debriefing Guide and Results

1. Did you encounter any problems during the experiment? (explain)

Had trouble with eye during one day of the testing - probably would not have run VASCAR on that day if on patrol.
Shadow of guard shack interfered with bridge study.
200 foot clocks - too short ( $n=3$ )
Stationary bridge clock - no anticipation time for the far shadow.
Reflective plates were not enough of a reference mark.
Had some trouble getting use to car. (did not use own vehicle)
Odometer module went out.
2. On the scale below, please indicate how realistic you feel the conditions used in our study wers.

3. What parts of the study were not realistic? (probe for specific situations)

Much of the information gathered from this question is embedded in the table for question 2. From the table, the officers in general felt the 200 foot course distance clocks were not realistic. They felt it was too short. They also did not think the parking portion of the bridge study was realistic. They did not think the bridge shadow was wide enough. They said they were reacting to the bridge shadow instead of anticipating it.

Other comments:
Competing against photocell - little more stressful than the real world; the competition could make you better or worse depending on the individual.
Following clock harder than leading clock - couldn't anticipate the plate.
Angular clocking 200 foot distance - should align post with line of sight of officer.
4. If you were to re-design this study, what would you change to improve it?

Make scaffolding higher and wider for bridge shadow.
Have a car leading target car in bridge study so you can anticipate when the target vehicle is coming through bridge.
Parked portion of moving-stationary study - Place bridge shadows so you could see both shadows, maybe elevate officer.
Lighter colored car would help with bridge shadow.
Moving study - seams in road as reference markers instead of reflector plate and cone.
Do longer clocks in moving study - half mile clocks would be better.
Better reference markers in angular study; white posts were hard to see when you're on the ground.
Minimum clocks should be .1 mile.
Better visibility for first bridge shadow on long clocks.
Do some testing on the highway - more realistic marks.
In the moving study, use more definite references other than reflector plates. : :
Have officers use their own equipment.
Get rid of short clocks.
More night testing - can use long stationary clocks at night.
Put tape all the way across the lane so the following clocks are more anticipation instead of reaction.
White posts were hard to see when the sun was bright, a different color may have been better.
5. For those runs you asked to repeat, what was the usual reason you needed to repeat them?

Missing clock - knew I missed clock ( $\mathrm{n}=5$ )
Time measurement was either early or late; distance measurements were almost always good. ( $\mathrm{n}=2$ )
You know if you've hit the marks right or not.
Forgot to redial distance.
Used wrong marker - didn't activate switch at right marker.

6a. Under what conditions in this study did you have the most confidence in your clocks?

6b. How about the least confidence?
Each subject was asked to rank the confidence level of their clocks
Subjects 1 and 2 participated in the moving and the moving-stationary studies.

Subject 1
Moving
Following
Leading
Moving-Stationary
Following
Short Gap 3
Long Gap 4
Parking
Direct Vision 5 5
Indirect Vision 6

Subjects 3, 4, 5, and 6 participated in the moving, moving-stationary, angular, and parking studies.

Subject 3 Subject 4 Subject 5 Subject 6
Moving
Following

| .1 mile | 5 | 5 | 5 | 9 |
| :--- | :--- | :--- | :--- | ---: |
| .3 mile | 1 | 3 | 1 | 1 |
| .$n$ mile |  |  |  |  |
| .3 mile | 4 | 6 | 6 | 10 |
| .3 | 4 | 2 | 2 |  |

Moving-Stationary
Following

| Short Gap | 2 | 1 | 3 | 5 |
| :--- | :--- | :--- | :--- | :--- |

$\begin{array}{lllll}\text { Long Gap } & 3 & 2 & 11 & 6\end{array}$
Parking
Direct Vision 12
12 五
Indirect Vision 13
$9 \quad 18 \quad 8$

Angular

| Ele. | C.D. | V.D. |  |  |  |  |
| :--- | :--- | :--- | ---: | ---: | ---: | ---: |
| G | S | S | 17 | 18 | 15 | 18 |
| G | L | S | 10 | 13 | 9 | 15 |
| G | S | L | 16 | 17 | 13 | 16 |
| G | L | L | 9 | 12 | 7 | 12 |
| E | S | S | 15 | 15 | 16 | 17 |
| E | L | S | 8 | 11 | 10 | 11 |
| E | S | L | 14 | 14 | 14 | 14 |
| E | L | L | 7 | 10 | 8 | 3 |
| ing |  |  |  |  |  |  |
| 200 Feet |  | 18 | 16 | 12 | 13 |  |
| 1/10 mile |  |  |  |  | 4 | 4 |

Subjects 7 and 8 participated in the moving, angular, and 200 foot aligned post studies.

Subject 7 Subject 8
Moving
Following
$\begin{array}{lll}.1 \text { mile } & 6\end{array}$
.3 mile 5
Leading
.1 mile 8
$\begin{array}{lll}.3 \text { mile } & 7\end{array}$
Angular

| Ele. | C.D. | V.D. |
| :--- | :--- | :--- |
| $G$ | $S$ | $S$ |


| G L | S | 4 | 8 |
| :--- | :--- | :--- | :--- |

$\begin{array}{llll}\text { G } & \text { L } & 11 & 11\end{array}$
$\begin{array}{llll}\text { G L L } & 2 & 7\end{array}$
$\begin{array}{lllll}\text { E S } & 10 & 10\end{array}$
E L S $\quad 3 \quad 6$
$\begin{array}{llll}\text { E } & \text { L } & 9 & 9\end{array}$
$\begin{array}{lllll}\text { E L } & \text { L } & 1 & 5\end{array}$
200 foot aligned post 12
7. What reference markers were you using in each aspect of the stationary study?

200 feet, ground level
post at start, plate at end white posts ( $\mathrm{n}=5$ )
200 feet, elevated
post at start, plate at end
yellow tape
plates ( $\mathrm{n}=2$ )
white posts ( $\mathrm{n}=2$ )
528 feet, ground level
white posts ( $\mathrm{n}=6$ )
528 feet, elevated
white posts ( $n=4$ )
plates ( $\mathrm{n}=2$ )
8. Do you have any other comments?

The tests given were harder than the real world
If officer makes good clocks under these conditions, then the clocks made in real world will be good clocks.
Situations presented force you to be sharper-keener.
In real world situations $I$ give the violator the benefit of the doubt by shutting their time off a little late.

## APPENDIX H

Subject Information

TABLE H.1: Selected Biographic and Anthropometric Characteristics

| Characteristic | Subject Number |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Age | 39 | 50 | 39 | 25 | 40 | 29 | 26 | 36 |
| Years On Force | 11.5 | 27 | 16 | 3 | 10 | 1 | 5 | 10 |
| Years Experience Clocking Vehicles | 11.5 | 27 | 16 | 3 | 9 | 1 | 5 | 7 |
| Years Experience With VASCAR | 1.42 | 11 | 15 | . 83 | 7 | . 5 | 1 | 7 |
| Corrected Visual Acuity | 20/10 | 20/13 | 20/15 | 20/15 | 20/13 | 20/13 | 20/15 | 20/13 |
| Corrective Lenses | yes | yes | yes | no | yes | no | no | no |
| Purpose of Lenses | Reading | Reading | Stigma. | - | Reading | - | - | - |
| Seated Eye Height |  |  | 49 | 49.75 | 46.5 | 47.25 | 46.75 | 48.5 |

TABLE H.2: Percentage Use and Typical Course Distances for VASCAR Methods

| Method | Subject 1 |  | Subject 2 |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Percent Us | Course Dis. | Percent Use | Course Dis. |
| Following Target Vehicle | 2.375 | 300ft-. 25 mile | 37.5 | . 1 - . 3 mile |
| Opposite Direction | . 025 | $300-500 \mathrm{ft}$ | - | - |
| Approaching from Rear | 2.375 | $300 \mathrm{ft}-.25 \mathrm{mile}$ | 12.5 | 1 mile |
| Parking | 95.0 | 99-300 ft | 50.0 | 200-300 ft |
| T-Intersection | - | - | - | - |
| Angular Clocking | - | - | - | - |
|  | Subject 3 |  | Subject 4 |  |
| Method | Percent Us | Course Dis. | Percent Use | Course Dis. |
| Following Target Vehicle | 90.0 | 1-3 miles | 85.0 | $\geq 1$ mile |
| Opposite Direction | - |  | - | - |
| Approaching from Rear | 10.0 | $1-3$ miles | 15.0 | $\geq 1$ mile |
| Parking | - | - | - | - |
| T-Intersection | - | - |  |  |
| Angular Clocking | - | - | - | - |
|  |  |  |  |  |
| Method | Subject 5 <br> Percent Use Course Dis. |  | Subject 6 <br> Percent Use Course Dis. |  |
| Following Target Vehicle | 22.5 | . $2-.4$ mile | 45.0 | . 1 - 2 miles |
| Opposite Direction | 25 | . 2 mile | 2.5 | . 1 mile |
| Approaching from Rear | 2.25 | . 3 mile | 2.5 | . 1 - . 5 mile |
| Parking | 7.5 | . 1 mile | 2.5 | . 1 - . 2 mile |
| T-Intersection | - | - | 2.5 | . 1 - . 2 mile |
| Angular Clocking | 67.5 | . $1-.3 \mathrm{mile}$ | 45.0 | . 1 - 2 mile |
|  |  |  |  |  |
| Method | Subject 7 <br> Percent Use Course Dis. |  | Subject 8 <br> Percent Use Course Dis. |  |
| Following Target Vehicle | 29.7 | $\geq .9 \mathrm{mile}$ | 72.0 | $\geq 1$ mile |
| Opposite Direction | . 3 | . 2 mile | 4.5 | . 25 mile |
| Approaching from Rear | - | - | 13.5 | . 25 mile |
| Parking | - | - | 2.5 | . 1 mile |
| T-Intersection | - | - | - | - |
| Angular Clocking | 70.0 | . 2217 mile | 7.5 | . 1 mile |

APPENDIX I

## Raw Data and Statistical Results

Several statistical terms are used to present the results. The following definitions will aid in understanding the results:

Mean - the mean is nothing more than the average; the arithmetic sum of all values, divided by the total number of values in the data set:

$$
\begin{equation*}
\text { Mean }=\bar{x}=\frac{1}{n} \sum_{i=1}^{c} x_{i} \tag{I.1}
\end{equation*}
$$

Variance - is a measure of the variability of the data set:

$$
\begin{equation*}
S^{2}=\frac{1}{n-1} \sum_{i=1}^{c}\left(x_{1}-\bar{x}\right)^{2} \tag{I.2}
\end{equation*}
$$

Standard Deviation - the square root of the variance; it is also a measure of the variability of the data set.

Type I Error - falsely concluding that something is an effect (the alternative hypothesis) when it is not.
p - the probability of committing a Type I error; $\mathrm{p} \leq 0.05$ is used to determine if a variable is a statistically significant effect.

Mean Square Error - MSE; a measure of the unexplained error

$$
\begin{equation*}
M S E=\frac{\text { Unexplained Variation }}{n-2} \tag{I.3}
\end{equation*}
$$

Two Sided Upper 90th Percentile Tolerance Limit with a 95 Percent Confidence - 95 percent of the population is below this limit; to calculate a tolerance limit, two conditions must be met.

1. All assignable causes of variability must be detected and eliminated so the remaining variability may be considered random.
2. Certain assumptions must be made concerning the nature of the statistical population under study - for this study a normal distribution is assumed.

$$
\begin{equation*}
\text { Upper 95\% T.L }=\text { Mean }+K \times \sqrt{M S E} \tag{I.4}
\end{equation*}
$$

$K$ is dependant on the number of samples ( $n$ )

Observed Upper Nth Percentile - N percent of the data in the sample is equal to or less than this value; if the Nth percentile is not an exact sample point, then the ralue is linearly interpolated between the data points immediately below and immediately above the Nth percentile.

| VASCAR <br> Unit | Nicolet Time | VASCAR Time | VASCAR <br> Calculat <br> Time | Time Error |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 1.521 | 1.51 | 1.512 | -0.009 |
| 1 | 1.296 | 1.26 | 1.26 | -0.036 |
| 1 | 0.99 | 0.97 | 0.972 | -0.018 |
| 1 | 0.91 | 0.9 | 0.9 | -0.01 |
| 1 | 2.01 | 1.98 | 1.98 | -0.03 |
| 1 | 2.662 | 2.66 | 2.664 | 0.002 |
| 1 | 3.108 | 3.09 | 3.096 | -0.012 |
| 1 | 3.082 | 3.06 | 3.06 | -0.022 |
| 1 | 2.696 | 2.66 | 2.664 | -0.032 |
| 1 | 3.223 | 3.2 | 3.204 | -0.019 |
| 1 | 2.586 | 2.55 | 2.556 | -0.03 |
| 1 | 2.881 | 2.84 | 2.844 | -0.037 |
| 1 | 1.405 | 1.36 | 1.368 | -0.037 |
| 1 | 1.671 | 1.65 | 1.656 | -0.015 |
| 1 | 1.118 | 1.11 | 1.116 | -0.002 |
| 1 | 1.346 | 1.33 | 1.332 | -0.014 |
| 1 | 1.137 | 1.11 | 1.116 | -0.021 |
| 1 | 2.412 | 2.37 | 2.376 | -0.036 |
| 1 | 3.484 | 3.45 | 3.456 | -0.028 |
| 1 | 2.436 | 2.41 | 2.412 | -0.024 |
| 1 | 1.689 | 1.65 | 1.656 | -0.033 |
| 1 | 2.599 | 2.59 | 2.592 | -0.007 |
| 1 | 2.807 | 2.77 | 2.772 | -0.035 |
| 1 | 2.072 | 2.05 | 2.052 | -0.02 |
| 1 | 1.679 | 1.65 | 1.656 | -0.023 |
| 1 | 2.134 | 2.12 | 2.124 | -0.01 |
| 1 | 1.984 | 1.94 | 1.944 | -0.04 |
| 1 | 1.936 | 1.9 | 1.908 | -0.028 |
| 1 | 2.532 | 2.52 | 2.52 | -0.012 |
| 1 | 0.882 | 0.86 | 0.864 | -0.018 |
| 1 | 1.386 | 1.36 | 1.368 | -0.018 |
| 1 | 1.709 | 1.69 | 1.692 | -0.017 |
| 1 | 2.098 | 2.08 | 2.088 | -0.01 |
| 1 | 3.444 | 3.42 | 3.42 | -0.024 |
| 1 | 2.18 | 2.16 | 2.16 | -0.02. |
| 1 | 1.919 | 1.9 | 1.908 | -0.011 |
| 1 | 1.451 | 1.44 | 1.44 | -0.011 |
| 1 | 1.332 | 1.29 | 1.296 | -0.036 |
| 1 | 2.806 | 2.77 | 2.772 | -0.034 |


| VASCAR <br> Unit | Nicolet Time | $\begin{aligned} & \text { VASCAR } \\ & \text { Time } \end{aligned}$ | $\begin{aligned} & \text { VASCAR } \\ & \text { Calculat } \\ & \text { Time } \end{aligned}$ | Time ed Error |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 2.251 | 2.23 | 2.232 | -0.019 |
| 1 | 2.523 | 2.48 | 2.484 | -0.039 |
| 1 | 3.843 | 3.81 | 3.816 | -0.027 |
| 1 | 3.539 | 3.52 | 3.528 | -0.011 |
| 1 | 3.48 | 3.45 | 3.456 | -0.024 |
| 1 | 2.083 | 2.05 | 2.052 | -0.031 |
| 1 | 3.829 | 3.81 | 3.816 | -0.013 |
| 1 | 3.617 | 3.6 | 3.6 | -0.017 |
| 1 | 1.161 | 1.15 | 1.152 | -0.009 |
| 1 | 1.739 | 1.72 | 1.728 | -0.011 |
| 1 | 2.911 | 2.88 | 2.88 | -0.031 |
| 1 | 2.231 | 2.19 | 2.196 | -0.035 |
| 1 | 2.487 | 2.44 | 2.448 | -0.039 |
| 1 | 1.535 | 1.51 | 1.512 | -0.023 |
| 1 | 0.999 | 0.97 | 0.972 | -0.027 |
| 1 | 2.748 | 2.73 | 2.736 | -0.012 |
| 1 | 3.302 | 3.27 | 3.276 | -0.026 |
| 1 | 3.641 | 3.6 | 3.6 | -0.041 |
| 1 | 2.503 | 2.48 | 2.484 | -0.019 |
| 2 | 1.521 | 1.51 | 1.512 | -0.009 |
| 2 | 1.296 | 1.29 | 1.296 | -2.2E-16 |
| 2 | 0.99 | 0.97 | 0.972 | -0.018 |
| 2 | 0.91 | 0.9 | 0.9 | -0.01 |
| 2 | 2.01 | 1.98 | 1.98 | -0.03 |
| 2 | 2.662 | 2.66 | 2.664 | 0.002 |
| 2 | 3.108 | 3.09 | 3.096 | -0.012 |
| 2 | 3.082 | 3.06 | 3.06 | -0.022 |
| 2 | 2.696 | 2.66 | 2.664 | -0.032 |
| 2 | 3.223 | 3.2 | 3.204 | -0.019 |
| 2 | 2.586 | 2.55 | 2.556 | -0.03 |
| 2 | 2.881 | 2.84 | 2.844 | -0.037 |
| 2 | 1.405 | 1.36 | 1.368 | -0.037 |
| 2 | 1.671 | 1.65 | 1.656 | -0.015 |
| 2 | 1.118 | 1.08 | 1.08 | -0.038 |
| 2 | 1.346 | 1.33 | 1.332 | -0.014 |
| 2 | 1.137 | 1.11 | 1.116 | -0.021 |
| 2 | 2.412 | 2.37 | 2.376 | -0.036 |
| 2 | 3.484 | 3.45 | 3.456 | -0.028 |
| 2 | 2.436 | 2.41 | 2.412 | -0.024 |
| 2 | 1.689 | 1.65 | 1.656 | -0.033 |
| 2 | 2.599 | 2.59 | 2.592 | -0.007 |


| VASCAR <br> Unit | Nicolet Time | $\begin{aligned} & \text { VASCAR } \\ & \text { Time } \end{aligned}$ | VASCAR Calculated Time | Time Error |
| :---: | :---: | :---: | :---: | :---: |
| 2 | 2.807 | 2.77 | 2.772 | -0.035 |
| 2 | 2.072 | 2.05 | 2.052 | -0.02 |
| 2 | 1.679 | 1.65 | 1.656 | -0.023 |
| 2 | 2.134 | 2.12 | 2.124 | -0.01 |
| 2 | 1.984 | 1.94 | 1.944 | -0.04 |
| 2 | 1.936 | 1.9 | 1.908 | -0.028 |
| 2 | 2.532 | 2.52 | 2.52 | -0.012 |
| 2 | 0.882 | 0.86 | 0.864 | -0.018 |
| 2 | 1.386 | 1.36 | 1.368 | -0.018 |
| 2 | 1.709 | 1.69 | 1.692 | -0.017 |
| 2 | 2.098 | 2.08 | 2.088 | -0.01 |
| 2 | 3.444 | 3.42 | 3.42 | -0.024 |
| 2 | 2.18 | 2.16 | 2.16 | -0.02 |
| 2 | 1.919 | 1.9 | 1.908 | -0.011 |
| 2 | 1.451 | 1.44 | 1.44 | -0.011 |
| 2 | 1.332 | 1.29 | 1.296 | -0.036 |
| 2 | 2.806 | 2.77 | 2.772 | -0.034 |
| 2 | 2.251 | 2.23 | 2.232 | -0.019 |
| 2 | 2.523 | 2.48 | 2.484 | -0.039 |
| 2 | 3.843 | 3.81 | 3.816 | -0.027 |
| 2 | 3.539 | 3.52 | 3.528 | -0.011 |
| 2 | 3.48 | 3.45 | 3.456 | -0.024 |
| 2 | 2.083 | 2.05 | 2.052 | -0.031 |
| 2 | 3.829 | 3.81 | 3.816 | -0.013 |
| 2 | 3.617 | 3.6 | 3.6 | -0.017 |
| 2 | 1.161 | 1.15 | 1.152 | -0.009 |
| 2 | 1.739 | 1.72 | 1.728 | -0.011 |
| 2 | 2.911 | 2.88 | 2.88 | -0.031 |
| 2 | 2.231 | 2.19 | 2.196 | -0.035 |
| 2 | 2.487 | 2.44 | 2.448 | -0.039 |
| 2 | 1.535 | 1.51 | 1.512 | -0.023 |
| 2 | 0.999 | 0.97 | 0.972 | -0.027 |
| 2 | 2.748 | 2.73 | 2.736 | -0.012 |
| 2 | 3.302 | 3.27 | 3:276 | -0.026 |
| 2 | 3.641 | 3.6 | 3.6 | -0.041 |
| 2 | 2.503 | 2.48 | 2.484 | -0.019 |

Subject True True Dist VASCAR Distance \% Distance Number Distance Recoded Distance Error Error

| 1 | 0.5 | 3 | 0.5 | 0 | 0 |
| ---: | ---: | ---: | ---: | ---: | ---: |
| 1 | 0.5 | 3 | 0.5 | 0 | 0 |
| 1 | 0.5 | 3 | 0.5002 | 0.0002 | 0.04 |
| 1 | 0.5 | 3 | 0.5001 | 0.0001 | 0.02 |
| 1 | 0.1 | 2 | 0.1 | 0 | 0 |
| 1 | 0.1 | 2 | 0.1001 | 0.0001 | 0.1 |
| 1 | 0.1 | 2 | 0.1 | 0 | 0 |
| 1 | 0.1 | 2 | 0.1001 | 0.0001 | 0.1 |
| 1 | 0.037878 | 1 | 0.0379 | 0.000021 | 0.056 |
| 1 | 0.037878 | 1 | 0.0378 | -0.00007 | -0.208 |
| 1 | 0.037878 | 1 | 0.0379 | 0.000021 | 0.056 |
| 1 | 0.037878 | 1 | 0.0379 | 0.000021 | 0.056 |
| 2 | 0.5 | 3 | 0.5001 | 0.0001 | 0.02 |
| 2 | 0.5 | 3 | 0.5001 | 0.0001 | 0.02 |
| 2 | 0.5 | 3 | 0.5 | 0 | 0 |
| 2 | 0.5 | 3 | 0.5002 | 0.0002 | 0.04 |
| 2 | 0.1 | 2 | 0.1 | 0 | 0 |
| 2 | 0.1 | 2 | 0.1 | 0 | 0 |
| 2 | 0.1 | 2 | 0.1 | 0 | 0 |
| 2 | 0.1 | 2 | 0.1001 | 0.0001 | 0.1 |
| 2 | 0.037878 | 1 | 0.0378 | -0.00007 | -0.208 |
| 2 | 0.037878 | 1 | 0.0378 | -0.00007 | -0.208 |
| 2 | 0.037878 | 1 | 0.0379 | 0.000021 | 0.056 |
| 2 | 0.037878 | 1 | 0.0378 | -0.00007 | -0.208 |
| 3 | 0.5 | 3 | 0.4998 | -0.0002 | -0.04 |
| 3 | 0.5 | 3 | 0.4998 | -0.0002 | -0.04 |
| 3 | 0.5 | 3 | 0.5001 | 0.0001 | 0.02 |
| 3 | 0.5 | 3 | 0.5002 | 0.0002 | 0.04 |
| 3 | 0.1 | 2 | 0.1 | 0 | 0 |
| 3 | 0.1 | 2 | 0.1001 | 0.0001 | 0.1 |
| 3 | 0.1 | 2 | 0.0999 | -0.0001 | -0.1 |
| 3 | 0.1 | 2 | 0.1 | 0 | 0 |
| 3 | 0.037878 | 1 | 0.0379 | 0.000021 | 0.056 |
| 3 | 0.037878 | 1 | 0.0379 | 0.000021 | 0.056 |
| 3 | 0.037878 | 1 | 0.038 | 0.000121 | 0.32 |
| 3 | 0.037878 | 1 | 0.0379 | 0.000021 | 0.056 |
|  |  |  |  | 0 | 0 |

Subject True True Dist VASCAR Distance of Distance Number Distance Recoded Distance Error Error

| 4 | 0.5 | 3 | 0.5 | 0 | 0 |
| ---: | ---: | ---: | ---: | ---: | ---: |
| 4 | 0.5 | 3 | 0.5 | 0 | 0 |
| 4 | 0.5 | 3 | 0.5001 | 0.0001 | 0.02 |
| 4 | 0.5 | 3 | 0.5001 | 0.0001 | 0.02 |
| 4 | 0.1 | 2 | 0.1 | 0 | 0 |
| 4 | 0.1 | 2 | 0.1 | 0 | 0 |
| 4 | 0.1 | 2 | 0.1001 | 0.0001 | 0.1 |
| 4 | 0.1 | 2 | 0.1 | 0 | 0 |
| 4 | 0.037878 | 1 | 0.0379 | 0.000021 | 0.056 |
| 4 | 0.037878 | 1 | 0.0378 | -0.00007 | -0.208 |
| 4 | 0.037878 | 1 | 0.0379 | 0.000021 | 0.056 |
| 4 | 0.037878 | 1 | 0.0379 | 0.000021 | 0.056 |
| 5 | 0.5 | 3 | 0.4999 | -0.0001 | -0.02 |
| 5 | 0.5 | 3 | 0.5001 | 0.0001 | 0.02 |
| 5 | 0.5 | 3 | 0.5002 | 0.0002 | 0.04 |
| 5 | 0.5 | 3 | 0.5003 | 0.0003 | 0.06 |
| 5 | 0.1 | 2 | 0.1 | 0 | 0 |
| 5 | 0.1 | 2 | 0.1 | 0 | 0 |
| 5 | 0.1 | 2 | 0.1 | 0 | 0 |
| 5 | 0.1 | 2 | 0.1 | 0 | 0 |
| 5 | 0.037878 | 1 | 0.0378 | -0.00007 | -0.208 |
| 5 | 0.037878 | 1 | 0.0379 | 0.000021 | 0.056 |
| 5 | 0.037878 | 1 | 0.0378 | -0.00007 | -0.208 |
| 5 | 0.037878 | 1 | 0.0378 | -0.00007 | -0.208 |
| 6 | 0.5 | 3 | 0.4999 | -0.0001 | -0.02 |
| 6 | 0.5 | 3 | 0.5001 | 0.0001 | 0.02 |
| 6 | 0.5 | 3 | 0.5002 | 0.0002 | 0.04 |
| 6 | 0.5 | 3 | 0.5002 | 0.0002 | 0.04 |
| 6 | 0.1 | 2 | 0.0999 | -0.0001 | -0.1 |
| 6 | 0.1 | 2 | 0.1001 | 0.0001 | 0.1 |
| 6 | 0.1 | 2 | 0.1 | 0 | 0 |
| 6 | 0.1 | 2 | 0.1001 | 0.0001 | 0.1 |
| 6 | 0.037878 | 1 | 0.0378 | -0.00007 | -0.208 |
| 6 | 0.037878 | 1 | 0.0378 | -0.00007 | -0.208 |
| 6 | 0.037878 | 1 | 0.0379 | 0.000021 | 0.056 |
| 6 | 0.037878 | 1 | 0.0379 | 0.000021 | 0.056 |

TABLE I. 3 -- Summary of Speed Measurement Experiments

|  |  | S1 | S2 | S3 | S4 | S5 | S6 | S7 | S8 | All <br> Subjects Combined | Upper 90\% Tolerance Limit | Observ $95 \%-\mathrm{ti}$ | Observed 99\%-tile |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Moving | N | 48 | 48 | 48 | 48 | 48 | 48 | 48 | 48 | 384 |  |  |  |
|  | Mean | -0.291 | 0.377 | 0.092 | 0.183 | 0.206 | 0.014 | -0.137 | 0.054 | 0.062 |  |  |  |
|  | SD | 0.966 | 0.744 | 0.924 | 0.680 | 0.891 | 0.694 | 0.914 | 0.987 | 0.872 | 1.471 | 1.271 | 2.396 |
| Moving - | N | 24 | 24 | 24 | 24 | 2.4 | 24 | 24 | 24 | 192 |  |  |  |
| Following | Mean | -0.657 | 0.431 | -0.253 | 0.217 | -0.077 | -0.036 | -0.362 | -0.218 | -0.119 |  |  |  |
| Method | SD | 1.033 | 0.839 | 0.952 | 0.789 | 0.993 | 0.715 | 1.166 | 1.133 | 0.991 | 1. 550 | 0.943 | 2.407 |
| Moving - | N | 24 | 24 | 24 | 24 | 24 | 24 | 24 | 24 | 192 |  |  |  |
| Leading | Mean | 0.076 | 0.324 | 0.437 | 0.148 | 0.488 | 0.064 | 0.087 | 0.326 | 0.244 |  |  |  |
| Method | SD | 0.749 | 0.649 | 0.768 | 0.566 | 0.685 | 0.684 | 0.598 | 0.742 | 0.690 | 1.291 | 1.418 | 2.106 |
| Night | N |  |  | 6 | 6 | 6 | 6 | 6 | 6 | 36 |  |  |  |
| Moving | Mean |  |  | 0.148 | 0.060 | 0.691 | 0.392 | 0.553 | 0.149 | 0.332 |  |  |  |
|  | SD |  |  | 0.297 | 0.451 | 0.681 | 0.232 | 0.679 | 0.206 | 0.493 | 1.046 | 1.450 | 1.824 |
| Bridge- | N | 8 | 8 | 12 | 12 | 8 | 8 |  |  | 56 |  |  |  |
| Moving | Mean | 0.257 | 0.594 | 0.233 | -0.004 | 0.198 | 0.367 |  |  | 0.251 |  |  |  |
|  | SD | 1.012 | 0.389 | 0.304 | 0.605 | 0.553 | 0.615 |  |  | 0.602 | 1.308 | 1.296 | 1. 544 |
| Bridge- | N | 8 | 8 | 12 | 11 | 8 | 8 |  |  | 55 |  |  |  |
| Station- | Mean | 2.238 | 0.816 | 0.467 | 0.753 | 0.965 | 0.948 |  |  | 0.975 |  |  |  |
| ary | SD | 1.271 | 0.421 | 0.324 | 2.363 | 0.506 | 0.442 |  |  | 0.830 | 1.673 | 2.396 | 3.791 |
| Park | N |  |  | 12 | 12 | 12 | 12 |  |  | 48 |  |  |  |
|  | Mean |  |  | 1.471 | -0.859 | -2.072 | -0.565 |  |  | -0.506 |  |  |  |
|  | SD |  |  | 2.816 | 2.145 | 2.100 | 2.027 |  |  | 2.566 | 1.996 | 3.350 | 4.334 |
| Angular | N |  |  | 96 | 96 | 96 | 96 | 96 | 96 | 576 |  |  |  |
|  | Mean |  |  | -0.089 | 0.163 | 0.372 | 1.667 | 0.524 | 1.791 | 0.738 |  |  |  |
|  | SD |  |  | 0.972 | 1.417 | 2.107 | 2.494 | 1.621 | 2.137 | 1.992 | 3.906 | 4.650 | 7.332 |
| Align | N |  |  |  |  |  |  | 12 | 12 | 24 |  |  |  |
|  | Mean |  |  |  |  |  |  | -0.572 | 0.447 | -0.063 |  |  |  |
|  | SD |  |  |  |  |  |  | 1.601 | 1.877 | 1.784 | 3.999 | 2.698 | 2.877 |
| Entire | N |  |  |  |  |  |  |  |  | 1180 |  |  |  |
| Study | Mean |  |  |  |  |  |  |  |  | 0.426 |  |  |  |
|  | SD |  |  |  |  |  |  |  |  | 1.645 | NA | 3.708 | 6.439 |



| Following | 192 | -0.119 | 1.550 | 0.943 | 2.407 | 0.8577 | 0.983 | 1.802 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Approach from Rear | 192 | 0.244 | 1.291 | 1.418 | 2.106 | 0.3382 | 0.476 | 1.802 |


| Following | 0.1 | 96 | -0.309 | 2.139 | 1.143 | 2.943 | 1.6957 | 1.696 | 1.880 |
| :--- | :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Following | 0.3 | 96 | 0.070 | 0.985 | 0.581 | 0.908 | 0.2371 | 0.207 | 1.880 |
| App. Rear | 0.1 | 96 | 0.236 | 1.596 | 1.678 | 2.566 | 0.5232 | 0.808 | 1.880 |
| App. Rear | 0.3 | 96 | 0.251 | 0.730 | 0.796 | 1.358 | 0.0648 | 0.148 | 1.880 |


| Following | 0.1 | 45 | 32 | -0.067 | 1.113 | 0.725 | 0.974 | 0.3096 | 0.403 | 2.120 |
| :--- | :--- | :--- | :--- | ---: | :--- | :--- | :--- | :--- | :--- | :--- |
| App. Rear | 0.1 | 45 | 32 | 0.222 | 1.334 | 1.135 | 1.249 | 0.2751 | 0.294 | 2.120 |
| Following | 0.1 | 60 | 32 | 0.079 | 1.470 | 1.069 | 1.493 | 0.4302 | 0.543 | 2.120 |
| App. Rear | 0.1 | 60 | 32 | -0.077 | 1.789 | 1.504 | 1.728 | 0.7751 | 0.838 | 2.120 |
| Following | 0.1 | 80 | 32 | -0.939 | 3.138 | 2.584 | 3.183 | 3.6987 | 3.627 | 2.120 |
| App. Rear | 0.1 | 80 | 32 | 0.464 | 2.787 | 2.267 | 2.581 | 1.2010 | 1.132 | 2.120 |
| Following | 0.3 | 45 | 32 | 0.124 | 0.543 | 0.358 | 0.664 | 0.0269 | 0.039 | 2.120 |
| App. Rear | 0.3 | 45 | 32 | 0.209 | 0.669 | 0.575 | 0.586 | 0.0293 | 0.047 | 2.120 |
| Following | 0.3 | 60 | 32 | 0.095 | 0.592 | 0.473 | 0.577 | 0.0549 | 0.080 | 2.120 |
| App. Rear | 0.3 | 60 | 32 | 0.141 | 0.890 | 0.699 | 0.783 | 0.1249 | 0.143 | 2.120 |
| Fcllowing | 0.3 | 80 | 32 | -0.071 | 1.632 | 0.813 | 0.988 | 0.6451 | 0.505 | 2.120 |
| App. Rear | 0.3 | 80 | 32 | 0.404 | 1.427 | 1.169 | 1.467 | 0.2329 | 0.225 | 2.120 |

A. Variables

Course Distance
Nominal Speed
VASCAR Method
Subject Number Groups
Replication
B. Significant Effects ( $\mathrm{p} \leq 0.05$ )

Subject Number - see summary of experiment
Course Distance

| Course <br> Distance | Mean <br> Error |
| :---: | :---: |
| .1 | -.04 |
| .3 | .16 |

VASCAR Method

| VASCAR <br> Method | Mean <br> Error |
| :---: | :---: |
| Following <br> Leading | .12 <br> .24${ }^{2}$ |

Course Distance x Method

| Course <br> Distance | Mean Error |  |
| :---: | :---: | :---: |
|  | Following | Approach from <br> Rear |
| .1 | -.31 | .24 |
| .3 | .07 | .25 |

Nominal Speed x Method

| Nominal <br> Speed | Mean Error |  |
| :---: | :---: | :---: |
|  | Fol lowing | Approach from <br> Rear |
| 45 | .03 | .22 |
| 60 | .09 | .03 |
| 80 | -.47 | .48 |

Course Distance $x$ Speed $x$ Method - see Moving Summary Statistics on previous page

Moving Study - Analysis by Method
A. Significant Effects for Following Method ( $p \leq 0.05$ )

Course Distance
Nominal Speed
Subject Number
Course Distance x Nominal Speed

| Course <br> Distance | Mean Speed Error |  |  |
| :---: | :---: | :---: | :---: |
|  | 45 | 60 | 80 |
| .1 | -.07 | .08 | -.94 |
| .3 | .12 | .09 | -.01 |

B. Significant Effects for Leading Method ( $\mathrm{p} \leq 0.05$ )

Nominal Speed

The following list of definitions explain the title headings found in the raw data listings:

| SubNum | Subject Number |
| :---: | :---: |
| SessNum | Session Number, the number given to each study (i.e., moving, bridge, etc.) |
| RepNum | Replicate Number |
| Repeat\# | Repeat Number, used only in bridge study, subjects 1 and 2 made repeats instead of replicates |
| TrialNo - | Trial Number |
| CrsDist - | Course Distance |
| CrsDistR- | Course Distance Recoded, represents the course distance - used for statistical analysis |
| Reftype | Reference Type |
| VMethod | VASCAR Method, used in moving study, $1=$ following, $2=$ Approaching from the Rear |
| NomSpd | Nominal Speed, represents the desired speed for statistical analysis |
| DsrdSpd | Desired Speed in mph |
| NoAttemp- | Number of Attempts necessary to complete an acceptable clock acceptability based on subject's assessment of the accuracy of his clock |
| TrueTime - | True Time, measured by photocell system |
| TrueSpd - | True Speed, calculated using known distance and true time |
| VASspeed- | VASCAR displayed speed |
| VAStime - | VASCAR time |
| VASdist | VASCAR Distance |
| VehGap | Vehicle Gap, distance between target vehicle and police cruiser |
| VehGapR | Vehicle Gap Recoded, used for statistical analysis |
| VisMode | Visual Mode, method of viewing target vehicle, direct and indirect (mirrors) |
| VisModeR- | Visual Mode Recoded, used for statistical analysis |
| Elevatn - | Elevation, subject elevation, used in angular study, $1=$ ground, 2 = elevated |

ViewDist- Viewing Distance, used in angular study, $1=200$ feet, $2=528$ feet

TABLE I.5 -- Raw Data for Moving Study

| SubNum | SessNum | RepNum | Trialno | CrsDist | CrsoistR | Reftype | VMethod | NomSpd | DesrdSpd | NoAttempts | TrueTime | Truespd | VASspeed | VAStime | VASdist |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1 | 1 | 1 | 0.1 | 1 | 1 | 1 | 2 | 60 | 2 | 6.158 | 58.461 | 57.9 | 6.22 | 0.1002 |
| 1 | 1 | 1 | 2 | 0.1 | 1 | 1 | 2 | 1 | 45 | 1 | 8.018 | 44.899 | 45.1 | 7.95 | 0.0997 |
| 1 | 1 | 1 | 3 | 0.1 | 1 | 1 | 2 | 2 | 60 | 1 | 6.111 | 58.910 | 59.5 | 6.04 | 0.0999 |
| 1 | 1 | 1 | 4 | 0.1 | 1 | 1 | 1 | 1 | 45 | 1 | 7.873 | 45.726 | 45.6 | 7.84 | 0.0995 |
| 1 | 1 | 1 | 5 | 0.1 | 1 | 1 | 2 | 3 | 80 | 1 | 4.478 | 80.393 | 81.3 | 4.53 | 0.1024 |
| 1 | 1 | 1 | 6 | 0.1 | 1 | 1 | 1 | 3 | 80 | 1 | 4.423 | 81.393 | 78.3 | 4.6 | 0.1002 |
| 1 | 1 | 1 | 7 | 0.3 | 2 | 1 | 1 | 3 | 80 | 1 | 13.286 | 81.289 | 80.9 | 13.32 | 0.2994 |
| 1 | 1 | 1 | 8 | 0.3 | 2 | 1 | 2 | 1 | 45 | 1 | 24.445 | 44.181 | 44.4 | 24.44 | 0.3016 |
| 1 | 1 | 1 | 9 | 0.3 | 2 | 1 | 1 | 2 | 60 | 1 | 18.469 | 58.476 | 57.9 | 18.64 | 0.3004 |
| 1 | 1 | 1 | 10 | 0.3 | 2 | 1 | 2 | 2 | 60 | 1 | 18.263 | 59.136 | 59.2 | 18.21 | 0.2999 |
| 1 | 1 | 1 | 11 | 0.3 | 2 | 1 | 1 | 1 | 45 | 1 | 24.637 | 43.837 | 43.9 | 24.51 | 0.299 |
| 1 | 1 | 1 | 12 | 0.3 | 2 | 1 | 2 | 3 | 80 | 1 | 13.632 | 79.225 | 79 | 13.6 | 0.2988 |
| 1 | 1 | 2 | 1 | 0.3 | 2 | 1 | 1 | 1 | 45 | 1 | 23.743 | 45.487 | 45.7 | 23.58 | 0.2997 |
| 1 | 1 | 2 | 2 | 0.3 | 2 | 1 | 1 | 3 | 80 | 1 | 13.527 | 79.840 | 80 | 13.46 | 0.2994 |
| 1 | 1 | 2 | 3 | 0.3 | 2 | 1 | 1 | 2 | 60 | 1 | 18.28 | 59.081 | 59.1 | 18.28 | 0.3006 |
| 1 | 1 | 2 | 4 | 0.3 | 2 | 1 | 2 | 3 | 80 | 1 | 13.465 | 80.208 | 81 | 13.32 | 0.2999 |
| 1 | 1 | 2 | 5 | 0.3 | 2 | 1 | 2 | 1 | 45 | 1 | 24.524 | 44.038 | 44 | 24.44 | 0.2991 |
| 1 | 1 | 2 | 6 | 0.3 | 2 | 1. | 2 | 2 | 60 | 1 | 18.146 | 59.517 | 59.7 | 18.07 | 0.2998 |
| 1 | 1 | 2 | 7 | 0.1 | 1 | 1 | 1 | 1 | 45 | 1 | 7.85 | 45.860 | 44.9 | 7.99 | 0.0996 |
| 1 | 1 | 2 | 8 | 0.1 | 1 | 1 | 2 | 3 | 80 | 1 | 4.477 | 80.411 | 81.3 | 4.39 | 0.0992 |
| 1 | 1 | 2 | 9 | 0.1 | 1 | 1 | 1 | 2 | 60 | 1 | 6.022 | 59.781 | 59.1 | 6.08 | 0.0998 |
| 1 | 1 | 2 | 10 | 0.1 | 1 | 1 | 2 | 2 | 60 | 1 | 6.092 | 59.094 | 58.9 | 6.12 | 0.1001 |
| 1 | 1 | 2 | 11 | 0.1 | 1 | 9 | 2 | 1 | 45 | 1 | 7.938 | 45.351 | 45.9 | 7.88 | 0.1005 |
| 1 | 1 | 2 | 12 | 0.1 | 1 | 1 | 1 | 3 | 80 | 1 | 4.428 | 81.301 | 78.4 | 4.57 | 0.0096 |
| 1 | 1 | 3 | 1 | 0.3 | 2 | 1 | 1 | 1 | 45 | 1 | 23.657 | 45.652 | 46.1 | 23.42 | 0.3005 |
| 1 | 1 | 3 | 2 | 0.3 | 2 | 1 | 1 | 2 | 60 | 1 | 18.156 | 59.484 | 59 | 18.28 | 0.2999 |
| 1 | 1 | 3 | 3 | 0.3 | 2 | 1 | 2 | 2 | 60 | 1 | 18.185 | 59.390 | 59.5 | 18.07 | 0.299 |
| 1 | 1 | 3 | 4 | 0.3 | 2 | 1 | 2 | 1 | 45 | 1 | 23.646 | 45.674 | 46 | 23.4 | 0.2995 |
| 1 | 1 | 3 | 5 | 0.3 | 2 | 1 | 2 | 3 | 80 | 1 | 13.419 | 80.483 | 80.4 | 13.35 | 0.2985 |
| 1 | 1 | 3 | 6 | 0.3 | 2 | 1 | 1 | 3 | 80 | 1 | 13.304 | 81.179 | 81.5 | 13.21 | 0.2991 |
| 1 | 1 | 3 | 7 | 0.1 | 1 | 1 | 2 | 2 | 60 | 1 | 6.125 | 58.776 | 58.6 | 6.15 | 0.1002 |
| 1 | 1 | 3 | 8 | 0.1 | 1 | 1 | 2 | 3 | 80 | 1 | 4.449 | 80.917 | 79.4 | 4.57 | 0.1008 |
| 1 | 1 | 3 | 9 | 0.1 | 1 | 1 | 1 | 3 | 80 | 1 | 4.457 | 80.772 | 78.1 | 4.6 | 0.1 |
| 1 | 1 | 3 | 10 | 0.1 | 1 | 1 | 1 | 1 | 45 | 1 | 7.993 | 45.039 | 43.3 | 8.28 | 0.0996 |
| 1 | 1 | 3 | 11 | 0.1 | 1 | 1 | 1 | 2 | 60 | 1 | 6.096 | 59.055 | 57.6 | 6.08 | 0.0974 |
| 1 | 1 | 3 | 12 | 0.1 | 1 | 1 | 2 | 1 | 45 | 1 | 8.05 | 44.720 | 44.3 | 8.1 | 0.0997 |
| 1 | 1 | 4 | 1 | 0.1 | 1 | 1 | 1 | 1 | 45 | 1 | 7.894 | 45.604 | 44.3 | 8.1 | 0.0998 |
| 1 | 1 | 4 | 2 | 0.1 | 1 | 1 | 1 | 3 | 80 | 1 | 4.484 | 80.285 | 80 | 4.5 | 0.1004 |
| 1 | 1 | 4 | 3 | 0.1 | 1 | 1 | 2 | 2 | 60 | 1 | 6.028 | 59.721 | 57.4 | 6.26 | 0.1 |
| 1 | 1 | 4 | 4 | 0.1 | 1 | 1 | 2 | 1 | 45 | 1 | 7.877 | 45.703 | 46.9 | 7.7 | 0.1005 |
| 1 | 1 | 4 | 5 | 0.1 | 1 | 1 | 1 | 2 | 60 | 1 | 6.053 | 59.475 | 59.4 | 6.04 | 0.0998 |
| 1 | 1 | 4 | 6 | 0.1 | 1 | 1 | 2 | 3 | 80 | 1 | 4.457 | 80.772 | 80.7 | 4.42 | 0.0993 |
| 1 | 1 | 4 | 7 | 0.3 | 2 | 1 | 2 | 3 | 80 | 1 | 13.317 | 81.099 | 81.7 | 13.21 | 0.3 |
| 1 | 1 | 4 | 8 | 0.3 | 2 | 1 | 1 | 3 | 80 | 1 | 13.341 | 80.953 | 81.2 | 13.28 | 0.2997 |
| 1 | 1 | 4 | 9 | 0.3 | 2 | 1 | 1 | 2 | 60 | 1 | 18.392 | 58.721 | 58.7 | 18.36 | 0.2996 |
| 1 | 1 | 4 | 10 | 0.3 | 2 | 1 | 1 | 1 | 45 | 1 | 24.148 | 44.724 | 44.8 | 24.04 | 0.2997 |
| 1 | 1 | 4 | 11 | 0.3 | 2 | 1 | 2 | 1 | 45 | 1 | 24.178 | 44.669 | 44.6 | 24.12 | 0.2994 |
| 1 | 1 | 4 | 12 | 0.3 | 2 | 1 | 2 | 2 | 60 | 1 | 18.337 | 58.897 | 59.2 | 18.25 | 0.3005 |

TABLE I. 5 -- Raw Data for Moving Study (Continued)

|  | SubNum 2 | SessNum $1$ | RepNum | TrialNo $1$ | $\begin{array}{r} \text { CrsDist } \\ 0.1 \end{array}$ | CrsDistR | Reftype 1 | VMethod 2 | NomSpd 2 | DesrdSpd | NoAttempts | Truetime 6.141 | TrueSpd 58.622 | VASspeed 58 | $\begin{array}{r} \text { VAStime } \\ 6.26 \end{array}$ | $\begin{array}{r} \text { Vasdist } \\ 0.101 \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2 | 1 | 1 | 2 | 0.1 | 1 | 1 | 1 | 1 | 45 | 1 | 8.018 | 44.899 | 44.6 | 8.1 | 0.1003 |
|  | 2 | 1 | 1 | 3 | 0.1 | 1 | 1 | 1 | 2 | 60 | 1 | 6.111 | 58.910 | 59.9 | 6.01 | 0.1001 |
|  | 2 | 1 | 1 | 4 | 0.1 | 1 | 1 | 2 | 1 | 45 | 1 | 7.873 | 45.726 | 47 | 7.63 | 0.0998 |
|  | 2 | 1 | 1 | 5 | 0.1 | 1 | 1 | 1 | 3 | 80 | 2 | 4.466 | 80.609 | 81.9 | 4.35 | 0.0991 |
|  | 2 | 1 | 1 | 6 | 0.1 | 1 | 1 | 2 | 3 | 80 | 2 | 4.494 | 80.107 | 80 | 4.5 | 0.1 |
|  | 2 | 1 | 1 | 7 | 0.3 | 2 | 1 | 2 | 3 | 80 | 2 | 13.452 | 80.285 | 81.1 | 13.35 | 0.301 |
|  | 2 | 1 | 1 | 8 | 0.3 | 2 | 1 | 1 | 1 | 45 | 1 | 24.445 | 44.181 | 44.2 | 24.33 | 0.2989 |
|  | 2 | 1 | 1 | 9 | 0.3 | 2 | 1 | 2 | 2 | 60 | 1 | 18.469 | 58.476 | 58.9 | 18.36 | 0.3005 |
|  | 2 | 1 | 1 | 10 | 0.3 | 2 | 1 | 1 | 2 | 60 | 2 | 18.461 | 58.502 | 58.7 | 18.32 | 0.2991 |
|  | 2 | 1 | 1 | 11 | 0.3 | 2 | 1 | 2 | 1 | 45 | 1 | 24.637 | 43.837 | 44.3 | 24.51 | 0.302 |
|  | 2 | 1 | 1 | 12 | 0.3 | 2 | 1 | 1 | 3 | 80 | 1 | 13.632 | 79.225 | 79.8 | 13.53 | 0.3002 |
|  | 2 | 1 | 2 | 1 | 0.3 | 2 | 1 | 2 | 1 | 45 | 1 | 23.743 | 45.487 | 45.5 | 23.65 | 0.2994 |
|  | 2 | 1 | 2 | 2 | 0.3 | 2 | 1 | 2 | 3 | 80 | 1 | 13.527 | 79.840 | 79.7 | 13.5 | 0.2989 |
|  | 2 | 1 | 2 | 3 | 0.3 | 2 | 1 | 2 | 2 | 60 | 1 | 18.28 | 59.081 | 59.1 | 18.21 | 0.2992 |
|  | 2 | 1 | 2 | 4 | 0.3 | 2 | 1 | 1 | 3 | 80 | 1 | 13.465 | 80.208 | 80.5 | 13.35 | 0.2987 |
|  | 2 | 1 | 2 | 5 | 0.3 | 2 | 1 | 1 | 1 | 45 | 1 | 24.524 | 44.038 | 44.1 | 24.4 | 0.2995 |
|  | 2 | 1 | 2 | 6 | 0.3 | 2 | 1 | 1 | 2 | 60 | 1 | 18.146 | 59.517 | 59.5 | 18.03 | 0.2984 |
|  | 2 | 1 | 2 | 7 | 0.1 | 1 | 1 | 2 | 1 | 45 | 1 | 7.85 | 45.860 | 46.1 | 7.81 | 0.1 |
|  | 2 | 1 | 2 | 8 | 0.1 | 1 | 1 | 1 | 3 | 80 | 1 | 4.477 | 80.411 | 81 | 4.39 | 0.0988 |
|  | 2 | 1 | 2 | 9 | 0.1 | 1 | 1 | 2 | 2 | 60 | 1 | 6.022 | 59.781 | 59.7 | 5.97 | 0.0991 |
|  | 2 | 1 | 2 | 10 | 0.1 | 1 | 1 | 1 | 2 | 60 | 1 | 6.092 | 59.094 | 59.3 | 6.01 | 0.099 |
| $\stackrel{\square}{\square}$ | 2 | 1 | 2 | 11 | 0.1 | 1 | 1 | 1 | 1 | 45 | 1 | 7.938 | 45.351 | 46.1 | 7.81 | 0.1001 |
| W | 2 | 1 | 2 | 12 | 0.1 | 1 | 1 | 2 | 3 | 80 | 1 | 4.477 | 80.411 | 80 | 4.5 | 0.1 |
|  | 2 | 1 | 3 | 1 | 0.3 | 2 | 1 | 2 | 1 | 45 | 1 | 23.657 | 45.652 | 46 | 23.5 | 0.3005 |
|  | 2 | 1 | 3 | 2 | 0.3 | 2 | 1 | 2 | 2 | 60 | 1 | 18.156 | 59.484 | 59.7 | 18.07 | 0.2998 |
|  | 2 | 1 | 3 | 3 | 0.3 | 2 | 1 | 1 | 2 | 60 | 1 | 18.185 | 59.390 | 59.3 | 18.1 | 0.2986 |
|  | 2 | 1 | 3 | 4 | 0.3 | 2 | 1 | 1 | 1 | 45 | 1 | 23.646 | 45.674 | 45.9 | 23.47 | 0.2998 |
|  | 2 | 1 | 3 | 5 | 0.3 | 2 | 1 | 1 | 3 | 80 | 1 | 13.419 | 80.483 | 80.7 | 13.35 | 0.2997 |
|  | 2 | 1 | 3 | 6 | 0.3 | 2 | 1 | 2 | 3 | 80 | 1 | 13.304 | 81.179 | 81.7 | 13.17 | 0.2991 |
|  | 2 | 1 | 3 | 7 | 0.1 | 1 | 1 | 1 | 2 | 60 | 1 | 6.125 | 58.776 | 58.6 | 6.08 | 0.099 |
|  | 2 | 1 | 3 | 8 | 0.1 | 1 | 1 | 1 | 3 | 80 | 2 | 4.4 | 81.818 | 81.1 | 4.42 | 0.998 |
|  | 2 | 1 | 3 | 9 | 0.1 | 1 | 1 | 2 | 3 | 80 | 2 | 4.446 | 80.972 | 81.4 | 4.46 | 0.1009 |
|  | 2 | 1 | 3 | 10 | 0.1 | 1 | 1 | 2 | 1 | 45 | 1 | 7.993 | 45.039 | 44.8 | 7.95 | 0.0991 |
|  | 2 | 1 | 3 | 11 | 0.1 | 1 | 1 | 2 | 2 | 60 | 1 | 6.096 | 59.055 | 59.4 | 6.04 | 0.0999 |
|  | 2 | 1 | 3 | 12 | 0.1 | 1 | 1 | 1 | 1 | 45 | 1 | 8.05 | 44.720 | 45.8 | 7.81 | 0.0995 |
|  | 2 | 1 | 4 | 1 | 0.1 | 1 | 1 | 2 | 1 | 45 | 1 | 7.894 | 45.604 | 46.5 | 7.74 | 0.1 |
|  | 2 | 1 | 4 | 2 | 0.1 | 1 | 1 | 2 | 3 | 80 | 2 | 4.448 | 80.935 | 83.5 | 4.32 | 0.1002 |
|  | 2 | 1 | 4 | 3 | 0.1 | 1 | 1 | 1 | 2 | 60 | 1 | 6.028 | 59.721 | 60.2 | 5.94 | 0.0993 |
|  | 2 | 1 | 4 | 4 | 0.1 | 1 | 1 | 1 | 1 | 45 | 1 | 7.877 | 45.703 | 45.7 | 7.88 | 0.1001 |
|  | 2 | 1 | 4 | 5 | 0.1 | 1 | 1 | 2 | 2 | 60 | 1 | 6.053 | 59.475 | 59.2 | 6.04 | 0.0994 |
|  | 2 | 1 | 4 | 6 | 0.1 | 1 | 1 | 1 | 3 | 80 | 1 | 4.457 | 80.772 | 84.5 | 4.35 | 0.1022 |
|  | 2 | 1 | 4 | 7 | 0.3 | 2 | 1 | 1 | 3 | 80 | 1 | 13.317 | 81.099 | 81.5 | 13.24 | 0.3001 |
|  | 2 | 1 | 4 | 8 | 0.3 | 2 | 1 | 2 | 3 | 80 | 1 | 13.349 | 80.953 | 81.7 | 13.17 | 0.2993 |
|  | 2 | 1 | 4 | 9 | 0.3 | 2 | 1 | 2 | 2 | 60 | 2 | 18.201 | 59.337 | 59.5 | 18.14 | 0.3003 |
|  | 2 | 1 | 4 | 10 | 0.3 | 2 | 1 | 2 | 1 | 45 | 1 | 24.148 | 44.724 | 44.9 | 24.04 | 0.3004 |
|  | 2 | 1 | 4 | 11 | 0.3 | 2 | 1 | 1 | 1 | 45 | 1 | 24.178 | 44.669 | 44.6 | 24.08 | 0.2989 |
|  | 2 | 1 | 4 | 12 | 0.3 | 2 | 1 | 1 | 2 | 60 | 1 | 18.337 | 58.897 | 59.5 | 18.1 | 0.2996 |


|  | SubNum | SessNum | RepNum ${ }_{1}$ | Trialno | CrsDist 0.1 | CrsDistR | Reftype | VMethod | NomSpd | DesrdSpd | NoAt tempts | TrueTime 7.932 | TrueSpd 45.386 | VASspeed 44.3 | VAStime <br> 8.13 | VASdist 0.1001 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 3 | 1 | 1 | 2 | 0.1 | 1 | 1 | 2 | 3 | 80 | 1 | 4.519 | 79.664 | 78.9 | 8.13 | 0.101 |
|  | 3 | 1 | 1 | 3 | 0.1 | 1 | 1 | 2 | 2 | 60 | 1 | 6.053 | 59.475 | 58.9 | 6.15 | 0.1008 |
|  | 3 | 1 | 1 | 4 | 0.1 | 1 | 1 | 1 | 1 | 45 | 1 | 8.006 | 44.966 | 44.8 | 8.02 | 0.0999 |
|  | 3 | 1 | 1 | 5 | 0.1 | 1 | 1 | 1 | 3 | 80 | 1 | 4.532 | 79.435 | 75.8 | 4.75 | 0.1001 |
|  | 3 | 1 | 1 | 6 | 0.1 | 1 | 1 | 1 | 2 | 60 | 1 | 6.085 | 59.162 | 59.9 | 6.01 | 0.0995 |
|  | 3 | 1 | 1 | 7 | 0.3 | 2 | 1 | 2 | 3 | 80 | 1 | 13.265 | 81.417 | 81.3 | 13.24 | 0.2994 |
|  | 3 | 1 | , | 8 | 0.3 | 2 | 1 | 2 | 2 | 60 | 1 | 18.198 | 59.347 | 59.3 | 18.21 | 0.3003 |
|  | 3 | 1 | 1 | 9 | 0.3 | 2 | 1 | 1 | 1 | 45 | 2 | 23.924 | 45.143 | 45.2 | 23.83 | 0.2997 |
|  | 3 | 1 | 1 | 10 | 0.3 | 2 | 1 | 1 | 2 | 60 | 1 | 18.349 | 58.859 | 59.1 | 18.25 | 0.3 |
|  | 3 | 1 | , | 11 | 0.3 | 2 | 1 | 1 | 3 | 80 | 1 | 13.509 | 79.947 | 80 | 13.46 | 0.2994 |
|  | 3 | 1 | 1 | 12 | 0.3 | 2 | 1 | 2 | 1 | 45 | 1 | 24.488 | 44.103 | 44.1 | 24.48 | 0.3003 |
|  | 3 | 1 | 2 | 1 | 0.3 | 2 | 1 | 1 | 3 | 80 | 1 | 13.354 | 80.875 | 81.4 | 13.24 | 0.2998 |
|  | 3 | 1 | 2 | 2 | 0.3 | 2 | 1 | 2 | 3 | 80 | 1 | 13.425 | 80.447 | 81.8 | 13.21 | 0.3003 |
|  | 3 | 1 | 2 | 3 | 0.3 | 2 | 1 | 1 | 1 | 45 | 1 | 23.542 | 45.875 | 46 | 23.5 | 0.3007 |
|  | 3 | 1 | 2 | 4 | 0.3 | 2 | 1 | 2 | 2 | 60 | 1 | 18.095 | 59.685 | 60.4 | 17.89 | 0.3004 |
|  | 3 | 1 | 2 | 5 | 0.3 | 2 | 1 | 2 | 1 | 45 | 1 | 23.469 | 46.018 | 46.3 | 23.36 | 0.3011 |
|  | 3 | 1 | 2 | 6 | 0.3 | 2 | 1 | 1 | 2 | 60 | 1 | 18.168 | 59.445 | 59.5 | 18.14 | 0.3002 |
|  | 3 | 1 | 2 | 7 | 0.1 | 1 | 1 | 1 | 1 | 45 | 1 | 7.894 | 45.604 | 45.9 | 7.88 | 0.1006 |
|  | 3 | 1 | 2 | 8 | 0.1 | 1 | 1 | 1 | 2 | 60 | 1 | 5.994 | 60.060 | 59.6 | 6.01 | 0.0996 |
|  | 3 | 1 | 2 | 9 | 0.1 | 1 | 1 | 2 | 3 | 80 | 1 | 4.448 | 80.935 | 81.4 | 4.46 | 0.101 |
|  | 3 | 1 | 2 | 10 | 0.1 | 1 | 1 | 2 | 2 | 60 | 1 | 6.044 | 59.563 | 60.4 | 5.94 | 0.996 |
| $\stackrel{\text { H }}{ }$ | 3 | 1 | 2 | 11 | 0.1 | 1 | 1 | 1 | 3 | 80 | 2 | 4.489 | 80.196 | 79.9 | 4.46 | 0.991 |
| $\sigma$ | 3 | 1 | 2 | 12 | 0.1 | 1 | 1 | 2 | 1 | 45 | 1 | 7.907 | 45.529 | 45.9 | 7.88 | 0.1007 |
|  | 3 | 1 | 3 | 1 | 0.1 | 1 | 1 | 2 | 3 | 80 | 2 | 4.487 | 80.232 | 82.3 | 4.42 | 0.1013 |
|  | 3 | 1 | 3 | 2 | 0.1 | 1 | 1 | 2 | 1 | 45 | 1 | 7.97 | 45.169 | 44.8 | 8.02 | 0.1001 |
|  | 3 | 1 | 3 | 3 | 0.1 | 1 | 1 | 1 | 2 | 60 | 1 | 6.068 | 59.328 | 58.9 | 6.12 | 0.1002 |
|  | 3 | 1 | 3 | 4 | 0.1 | 1 | 1 | 2 | 2 | 60 | 1 | 6.123 | 58.795 | 60.4 | 6.01 | 0.101 |
|  | 3 | 1 | 3 | 5 | 0.1 | 1 | 1 | 1 | 1 | 45 | 1 | 8.069 | 44.615 | 44.1 | 8.13 | 0.0998 |
|  | 3 | 1 | 3 | 6 | 0.1 | 1 | 1 | 1 | 3 | 80 | 1 | 4.47 | 80.537 | 78.4 | 4.57 | 0.0996 |
|  | 3 | 1 | 3 | 7 | 0.3 | 2 | 1 | 1 | 1 | 45 | 1 | 23.839 | 45.304 | 45.4 | 23.79 | 0.3001 |
|  | 3 | 1 | 3 | 8 | 0.3 | 2 | 1 | 2 | 1 | 45 | 1 | 23.936 | 45.120 | 45.7 | 23.61 | 0.2998 |
|  | 3 | 1 | 3 | 9 | 0.3 | 2 | 1 | 1 | 3 | 80 | 2 | 13.423 | 80.459 | 78.9 | 13.64 | 0.2992 |
|  | 3 | 1 | 3 | 10 | 0.3 | 2 | 1 | 1 | 2 | 60 | 1 | 18.152 | 59.498 | 59.2 | 18.18 | 0.2993 |
|  | 3 | 1 | 3 | 11 | 0.3 | 2 | 1 | 2 | 3 | 80 | 2 | 13.324 | 81.057 | 81.2 | 13.28 | 0.2999 |
|  | 3 | 1 | 3 | 12 | 0.3 | 2 | 1 | 2 | 2 | 60 | 1 | 18.202 | 59.334 | 59.7 | 18.07 | 0.2999 |
|  | 3 | 1 | 4 | 1 | 0.1 | 1 | 1 | 2 | 1 | 45 | 1 | 7.909 | 45.518 | 46.1 | 7.84 | 0.1005 |
|  | 3 | 1 | 4 | 2 | 0.1 | 1 | 1 | 1 | 1 | 45 | 2 | 8.045 | 44.748 | 45 | 8.02 | 0.1003 |
|  | 3 | 1 | 4 | 3 | 0.1 | 1 | 1 | 2 | 2 | 60 | 1 | 6.044 | 59.563 | 61 | 5.94 | 0.1006 |
|  | 3 | 1 | 4 | 4 | 0.1 | 1 | 1 | 1 | 3 | 80 | 1 | 4.451 | 80.881 | 81 | 4.46 | 0.1005 |
|  | 3 | 1 | 4 | 5 | 0.1 | 1 | 1 | 1 | 2 | 60 | 2 | 6.062 | 59.386 | 59.6 | 6.04 | 0.1002 |
|  | 3 | 1 | 4 | 6 | 0.1 | 1 | 1 | 2 | 3 | 80 | 2 | 4.478 | 80.393 | 81.8 | 4.42 | 0.1006 |
|  | 3 | 1 | 4 | 7 | 0.3 | 2 | 1 | 2 | 3 | 80 | 1 | 13.477 | 80.137 | 80.9 | 13.35 | 0.3002 |
|  | 3 | 1 | 4 | 8 | 0.3 | 2 | 1 | 1 | 2 | 60 | 1 | 18.177 | 59.416 | 59.8 | 18.03 | 0.2997 |
|  | 3 | 1 | 4 | 9 | 0.3 | 2 | 1 | 2 | 2 | 60 | 1 | 18.065 | 59.784 | 60.1 | 17.96 | 0.3003 |
|  | 3 | 1 | 4 | 10 | 0.3 | 2 | 1 | 2 | 1 | 45 | 2 | 23.669 | 45.629 | 45.8 | 23.54 | 0.2995 |
|  | 3 | 1 | 4 | 11 | 0.3 | 2 | 1 | 1 | 3 | 80 | 1 | 13.441 | 80.351 | 80.4 | 13.42 | 0.3001 |
|  | 3 | 1 | 4 | 12 | 0.3 | - 2 | 1 | 1 | 1 | 45 | 2 | 23.336 | 46.280 | 46.5 | 23.25 | 0.3005 |

TABLE I. 5 -- Raw Data for Moving Study (Continued)

| SubNum SessNum | RepNum | TrialNo |  |
| :---: | ---: | ---: | ---: |
| 4 | 1 | 1 | 1 |
| 4 | 1 | 1 | 2 |
| 4 | 1 | 1 | 3 |
| 4 | 1 | 1 | 4 |
| 4 | 1 | 1 | 5 |
| 4 | 1 | 1 | 6 |
| 4 | 1 | 1 | 7 |
| 4 | 1 | 1 | 8 |
| 4 | 1 | 1 | 9 |
| 4 | 1 | 1 | 10 |
| 4 | 1 | 1 | 11 |
| 4 | 1 | 1 | 12 |
| 4 | 1 | 2 | 1 |
| 4 | 1 | 2 | 2 |
| 4 | 1 | 2 | 3 |
| 4 | 1 | 2 | 4 |
| 4 | 1 | 2 | 5 |
| 4 | 1 | 2 | 6 |
| 4 | 1 | 2 | 7 |
| 4 | 1 | 2 | 8 |
| 4 | 1 | 2 | 9 |
| 4 | 1 | 2 | 10 |
| 4 | 1 | 2 | 11 |
| 4 | 1 | 2 | 12 |
| 4 | 1 | 3 | 1 |
| 4 | 1 | 3 | 2 |
| 4 | 1 | 3 | 3 |
| 4 | 1 | 3 | 4 |
| 4 | 1 | 3 | 5 |
| 4 | 1 | 3 | 6 |
| 4 | 1 | 3 | 7 |
| 4 | 1 | 3 | 8 |
| 4 | 1 | 3 | 9 |
| 4 | 1 | 3 | 10 |
| 4 | 1 | 3 | 11 |
| 4 | 1 | 3 | 12 |
| 4 | 1 | 4 | 1 |
| 4 | 1 | 4 | 2 |
| 4 | 1 | 4 | 3 |
| 4 | 1 | 4 | 4 |
| 4 | 1 | 4 | 5 |
| 4 | 1 | 4 | 6 |
| 4 | 1 | 4 | 7 |
| 4 | 1 | 4 | 8 |
| 4 | 1 | 4 | 9 |
| 4 | 1 | 4 | 10 |
| 4 | 1 | 4 | 11 |
| 4 | 1 | 4 | 12 |
|  |  |  |  |

CrsDist Crsoistr RefType VMethod
Nomspd DesrdSpd NoAttempts
TrueTime

| $1 e \mathrm{i} m \mathrm{~m}$ |
| ---: |
| 8.128 |
| 4.519 |
| 6.053 |
| 8.006 |
| 4.532 |
| 6.085 |
| 13.265 |
| 18.198 |
| 23.924 |
| 18.349 |
| 13.509 |
| 24.488 |
| 13.354 |
| 13.425 |
| 23.542 |
| 18.095 |
| 23.469 |
| 18.168 |
| 8.013 |
| 5.994 |
| 4.448 |
| 6.044 |
| 4.398 |
| 7.907 |
| 4.46 |
| 7.97 |
| 6.068 |
| 6.123 |
| 8.069 |
| 4.47 |
| 23.839 |
| 23.936 |
| 13.37 |
| 18.182 |
| 13.324 |
| 13.477 |
| 18.177 |
| 18.065 |
| 24.287 |
| 13.441 |
| 23.336 |
| 7.902 |
| 8.117 |
| 6.044 |

TrueSpd VASspeed V
VAStime
time
8.06
4.5
VASdist

| 0.1 | 1 |
| :---: | :---: |
| 0.1 | 1 |
| 0.1 | 1 |
| 0.1 | 1 |
| 0.1 | 1 |
| 0.1 | 1 |
| 0.3 | 2 |
| 0.3 | 2 |
| 0.3 | 2 |
| 0.3 | 2 |
| 0.3 | 2 |
| 0.3 | 2 |
| 0.3 | 2 |
| 0.3 | 2 |
| 0.3 | 2 |
| 0.3 | 2 |
| 0.3 | 2 |
| 0.3 | 2 |
| 0.1 | 1 |
| 0.1 | 1 |
| 0.1 | 1 |
| 0.1 | 1 |
| 0.1 | 1 |
| 0.1 | 1 |
| 0.1 | 1 |
| 0.1 | 1 |
| 0.1 | 1 |
| 0.1 | 1 |
| 0.1 | 1 |
| 0.1 | 1 |
| 0.3 | 2 |
| 0.3 | 2 |
| 0.3 | 2 |
| 0.3 | 2 |
| 0.3 | 2 |
| 0.3 | 2 |
| 0.1 | 1 |
| 0.1 | 1 |
| 0.1 | 1 |
| 0.1 | 1 |
| 0.1 | 1 |
| 0.1 | 1 |
| 0.3 | 2 |
| 0.3 | 2 |
| 0.3 | 2 |
| 0.3 | 2 |
| 0.3 | 2 |
| 0.3 | 2 |


| 1 | 1 |
| :--- | :--- |
| 1 | 1 |
| 1 | 1 |
| 1 | 2 |
| 1 | 2 |
| 1 | 2 |
| 1 | 1 |
| 1 | 1 |
| 1 | 2 |
| 1 | 2 |
| 1 | 2 |
| 1 | 1 |
| 1 | 2 |
| 1 | 1 |
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| 1 | 1 |
| 1 | 2 |
| 1 | 2 |
| 1 | 1 |
| 1 | 1 |
| 1 | 2 |
| 1 | 1 |
| 1 | 1 |
| 1 | 1 |
| 1 | 1 |
| 1 | 2 |
| 1 | 1 |
| 1 | 1 |
| 1 | 2 |
| 1 | 1 |
| 1 | 1 |



| 74.691 | 44.4 80.4 | 4.06 | $\begin{aligned} & 0.0995 \\ & 0.1005 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| 59.475 | 60.1 | 5.97 | 0.0998 |
| 44.966 | 44.9 | 7.99 | 0.0998 |
| 79.435 | 80 | 4.57 | 0.1017 |
| 59.162 | 58.3 | 6.19 | 0.1003 |
| 81.417 | 81.9 | 13.21 | 0.3007 |
| 59.347 | 59.4 | 18.14 | 0.2998 |
| 45.143 | 45.1 | 23.86 | 0.2993 |
| 58.859 | 57.8 | 18.93 | 0.3045 |
| 79.947 | 79.7 | 13.5 | 0.2991 |
| 44.103 | 44.3 | 24.37 | 0.3004 |
| 80.875 | 81.6 | 13.24 | 0.3004 |
| 80.447 | 81.2 | 13.28 | 0.2998 |
| 45.875 | 46.1 | 23.4 | 0.2999 |
| 59.685 | 59.8 | 18 | 0.299 |
| 46.018 | 46.3 | 23.29 | 0.2999 |
| 59.445 | 59.9 | 18.07 | 0.3009 |
| 44.927 | 45.2 | 7.95 | 0.0999 |
| 60.060 | 60 | 5.97 | 0.0996 |
| 80.935 | 83.3 | 4.35 | 0.1008 |
| 59.563 | 59.5 | 6.08 | 0.1005 |
| 81.855 | 81.8 | 4.39 | 0.0999 |
| 45.529 | 45.4 | 7.95 | 0.1003 |
| 80.717 | 79.8 | 4.5 | 0.0997 |
| 45.169 | 45.1 | 7.95 | 0.0997 |
| 59.328 | 59.7 | 6.04 | 0.1003 |
| 58.795 | 59.9 | 6.01 | 0.1001 |
| 44.615 | 45.2 | 7.92 | 0.0994 |
| 80.537 | 81.5 | 4.42 | 0.1003 |
| 45.304 | 45.5 | 23.83 | 0.3014 |
| 45.120 | 45.3 | 23.79 | 0.2995 |
| 80.778 | 81.1 | 13.32 | 0.3 |
| 59.399 | 59.6 | 18.1 | 0.3001 |
| 81.057 | 81.5 | 13.21 | 0.2992 |
| 59.334 | 59.6 | 18.07 | 0.2992 |
| 45.518 | 46.2 | 7.88 | 0.1013 |
| 44.351 | 45.1 | 8.02 | 0.1007 |
| 59.563 | 59.5 | 6.04 | 0.1 |
| 80.881 | 82.2 | 4.35 | 0.0995 |
| 60.050 | 59.5 | 5.97 | 0.0988 |
| 81.246 | 79 | 4.57 | 0.1003 |
| 80.137 | 80.1 | 13.46 | 0.2997 |
| 59.416 | 58.7 | 18.39 | 0.2999 |
| 59.784 | 60 | 17.96 | 0.2997 |
| 44.468 | 44.6 | 24.19 | 0.2997 |
| 80.351 | 80.6 | 13.35 | 0.2993 |
| 46.280 | 46.3 | 23.25 | 0.2995 |

TABLE I. 5 -- Raw Data for Moving Study (Contimued)

|  | SubNum | SessNum | RepNum | Trialno | CrsDist | CrsDistr | Reftype | VMethod | NomSpd | DesrdSpd | NoAttempts | TrueTime 8.999 | TrueSpd 40.004 | VASspeed | vastime | VASdist |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 5 | 1 | 1 | 2 | 0.1 | 1 | 1 | 2 | 2 | 60 | 1 | 5.768 | 62.413 | 64.2 | 5.68 | 0.1014 |
|  | 5 | 1 | 1 | 3 | 0.1 | 1 | 1 | 2 | 3 | 80 | 1 | 4.705 | 76.514 | 78.3 | 4.6 | 0.1002 |
|  | 5 | 1 | 1 | 4 | 0.1 | 1 | 1 | 1 | 3 | 80 | 2 | 4.407 | 81.688 | 84.6 | 4.28 | 0.1007 |
|  | 5 | 1 | 1 | 5 | 0.1 | 1 | 1 | 1 | 2 | 60 | 1 | 6.672 | 53.957 | 53.8 | 6.66 | 0.0995 |
|  | 5 | 1 | 1 | 6 | 0.1 | 1 | 1 | 2 | 1 | 45 | 1 | 9.002 | 39.991 | 39.4 | 9.14 | 0.1001 |
|  | 5 | 1 | 1 | 7 | 0.3 | 2 | 1 | 1 | 2 | 60 | 2 | 18.411 | 58.661 | 59.1 | 18.25 | 0.2998 |
|  | 5 | 1 | 1 | 8 | 0.3 | 2 | 1 | 1 | 1 | 45 | 1 | 25.19 | 42.874 | 42.8 | 25.2 | 0.2997 |
|  | 5 | 1 | 1 | 9 | 0.3 | 2 | 1 | 2 | 2 | 60 | 1 | 16.78 | 64.362 | 64.2 | 16.81 | 0.3002 |
|  | 5 | 1 | 1 | 10 | 0.3 | 2 | 1 | 2 | 1 | 45 | 1 | 26.869 | 40.195 | 40.4 | 26.74 | 0.3003 |
|  | 5 | 1 | 1 | 11 | 0.3 | 2 | 1 | 1 | 3 | 80 | 1 | 13.248 | 81.522 | 81.3 | 13.28 | 0.3 |
|  | 5 | 1 | 1 | 12 | 0.3 | 2 |  | 2 | 3 | 80 | 1 | 13.221 | 81.688 | 81.3 | 13.32 | 0.3011 |
|  | 5 | 1 | 2 | 1 | 0.3 | 2 | 1 | 1 | 1 | 45 | 2 | 22.028 | 49.029 | 49.1 | 21.96 | 0.2999 |
|  | 5 | 1 | 2 | 2 | 0.3 | 2 | 1 | 1 | 2 | 60 | 1 | 17.273 | 62.525 | 62.5 | 17.28 | 0.3001 |
|  | 5 | 1 | 2 | 3 | 0.3 | 2 | 1 | 1 | 3 | 80 | 1 | 13.968 | 77.320 | 76.4 | 14 | 0.2974 |
|  | 5 | 1 | 2 | 4 | 0.3 | 2 | 1 | 2 | 1 | 45 | 1 | 22.217 | 48.611 | 49.2 | 21.99 | 0.3007 |
|  | 5 | 1 | 2 | 5 | 0.3 | 2 | 1 | 2 | 3 | 80 | 1 | 13.624 | 79.272 | 79.9 | 13.6 | 0.3021 |
|  | 5 | 1 | 2 | 6 | 0.3 | 2 | 1 | 2 | 2 | 60 | 1 | 16.825 | 64.190 | 64.4 | 16.74 | 0.2998 |
|  | 5 | 1 | 2 | 7 | 0.1 | 1 | 1 | 2 | 2 | 60 | 1 | 6.603 | 54.521 | 53.6 | 6.69 | 0.0998 |
|  | 5 | 1 | 2 | 8 | 0.1 | 1 | 1 | 2 | 1 | 45 | 1 | 8.677 | 41.489 | 41.6 | 8.71 | 0.1007 |
|  | 5 | 1 | 2 | 9 | 0.1 | 1 | 1 | 1 | 3 | 80 | 2 | 4.641 | 77.569 | 75.1 | 4.78 | 0.0999 |
|  | 5 | 1 | 2 | 10 | 0.1 | 1 | 1 | 2 | 3 | 80 | 1 | 4.32 | 83.333 | 83.9 | 4.32 | 0.1007 |
| $\cdots$ | 5 | 1 | 2 | 11 | 0.1 | 1 | 1 | 1 | 2 | 60 | 2 | 6.055 | 59.455 | 60.5 | 5.97 | 0.1005 |
| $\infty$ | 5 | 1 | 2 | 12 | 0.1 | 1 | 1 | 1 | 1 | 45 | 1 | 7.641 | 47.114 | 46.8 | 7.66 | 0.0998 |
|  | 5 | 1 | 3 | 1 | 0.3 | 2 | 1 | 1 | 1 | 45 | 2 | 22.069 | 48.937 | 48.9 | 22.03 | 0.2997 |
|  | 5 | 1 | 3 | 2 | 0.3 | 2 | 1 | 2 | 2 | 60 | 1 | 17.915 | 60.285 | 61.1 | 17.74 | 0.3015 |
|  | 5 | 1 | 3 | 3 | 0.3 | 2 | 1 | 1 | 3 | 80 | 1 | 13.035 | 82.854 | 83 | 12.99 | 0.2996 |
|  | 5 | 1 | 3 | 4 | 0.3 | 2 | 1 | 1 | 2 | 60 | 1 | 17.457 | 61.866 | 62.3 | 17.38 | 0.3009 |
|  | 5 | 1 | 3 | 5 | 0.3 | 2 | 1 | 2 | 3 | 80 | 1 | 12.874 | 83.890 | 84.4 | 12.81 | 0.3006 |
|  | 5 | 1 | 3 | 6 | 0.3 | 2 | 1 | 2 | 1 | 45 | 1 | 24.134 | 44.750 | 45.2 | 23.83 | 0.2997 |
|  | 5 | 1 | 3 | 7 | 0.1 | 1 | 1 | 1 | 3 | 80 | 1 | 4.395 | 81.911 | 79.8 | 4.57 | 0.1014 |
|  | 5 | 1 | 3 | 8 | 0.1 | 1 | , | 2 | 3 | 80 | 1 | 4.202 | 85.673 | 86.7 | 4.14 | 0.0997 |
|  | 5 | 1 | 3 | 9 | 0.1 | 1 | 1 | 1 | 1 | 45 | 1 | 9.002 | 39.991 | 40.3 | 8.92 | 0.1 |
|  | 5 | 1 | 3 | 10 | 0.1 | 1 | 1 | 2 | 2 | 60 | 1 | 5.985 | 60.150 | 61.2 | 5.86 | 0.0997 |
|  | 5 | 1 | 3 | 11 | 0.1 | 1 | 1 | 1 | 2 | 60 | 1 | 5.591 | 64.389 | 65 | 5.58 | 0.1008 |
|  | 5 | 1 | 3 | 12 | 0.1 | 1 | 1 | 2 | 1 | 45 | 1 | 7.491 | 48.058 | 48.1 | 7.48 | 0.1001 |
|  | 5 | 1 | 4 | 1 | 0.1 | 1 | 1 | 1 | 1 | 45 | 1 | 7.794 | 46.189 | 45.9 | 7.81 | 0.0997 |
|  | 5 | 1 | 4 | 2 | 0.1 | 1 | 1 | 2 | 2 | 60 | 1 | 6.21 | 57.971 | 58 | 6.22 | 0.1004 |
|  | 5 | 1 | 4 | 3 | 0.1 | 1 | 1 | 1 | 2 | 60 | 1 | 5.955 | 60.453 | 59.9 | 6.01 | 0.1001 |
|  | 5 | 1 | 4 | 4 | 0.1 | 1 | 1 | 1 | 3 | 80 | 1 | 4.655 | 77.336 | 77.1 | 4.64 | 0.0995 |
|  | 5 | 1 | 4 | 5 | 0.1 | 1 | 1 | 2 | 1 | 45 | 1 | 7.668 | 46.948 | 47.8 | 7.56 | 0.1005 |
|  | 5 | 1 | 4 | 6 | 0.1 | 1 | 1 | 2 | 3 | 80 | 1 | 4.377 | 82.248 | 83.9 | 4.35 | 0.1015 |
|  | 5 | 1 | 4 | 7 | 0.3 | 2 | 1 | 2 | 3 | 80 | 1 | 13.739 | 78.608 | 79.4 | 13.64 | 0.3011 |
|  | 5 | 1 | 4 | 8 | 0.3 | 2 | 1 | 1 | 1 | 45 | 1 | 21.369 | 50.541 | 50.2 | 21.45 | 0.2997 |
|  | 5 | 1 | 4 | 9 | 0.3 | 2 | 1 | 1 | 3 | 80 | 1 | 13.844 | 78.012 | 78.3 | 13.82 | 0.3007 |
|  | 5 | 1 | 4 | 10 | 0.3 | 2 | 1 | 2 | 1 | 45 | 1 | 22.927 | 47.106 | 47.5 | 22.75 | 0.3003 |
|  | 5 | 1 | 4 | 11 | 0.3 | 2 | 1 | 1 | 2 | 60 | 1 | 17.72 | 60.948 | 61 | 17.67 | 0.2995 |
|  | 5 | 1 | 4 | 12 | 0.3 | 2 | 1 | 2 | 2 | 60 | 1 | 17.499 | 61.718 | 62 | 17.46 | 0.3008 |


|  | SubNum | SessNum | RepNum | Trialno | CrsDist | CrsDistR | Reftype | VMethod | NomSpd | DesrdSpd | NoAttempts | Truetime | TrueSpd | VASspeed | Vastime | VASdist |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 6 |  | 1 | 1 | 0.1 | 1 | 1 | 2 | 1 | 45 | 1 | 8.999 | 40.004 | 39.9 | 8.96 | 0.0994 |
|  | 6 | 1 | 1 | 2 | 0.1 | 1 | 1 | 1 | 2 | 60 | 2 | 5.765 | 62.446 | 62.3 | 5.72 | 0.0991 |
|  | 6 | 1 | 1 | 3 | 0.1 | 1 | 1 | 1 | 3 | 80 | 1 | 4.705 | 76.514 | 75.2 | 4.71 | 0.0986 |
|  | 6 | 1 | 1 | 4 | 0.1 | 1 | 1 | 2 | 3 | 80 | 1 | 4.391 | 81.986 | 80.6 | 4.42 | 0.0992 |
|  | 6 | 1 | 1 | 5 | 0.1 | 1 | 1 | 2 | 2 | 60 | 1 | 6.672 | 53.957 | 54.1 | 6.62 | 0.0997 |
|  | 6 | 1 | 1 | 6 | 0.1 | 1 | 1 | 1 | 1 | 45 | 1 | 9.002 | 39.991 | 40.3 | 8.92 | 0.1 |
|  | 6 | 1 | 1 | 7 | 0.3 | 2 | 1 | 2 | 2 | 60 | 1 | 18.603 | 58.055 | 58 | 18.61 | 0.3001 |
|  | 6 | 1 | 1 | 8 | 0.3 | 2 | 1 | 2 | 1 | 45 | 1 | 25.19 | 42.874 | 42.9 | 25.09 | 0.2997 |
|  | 6 | 1 |  | 9 | 0.3 | 2 | 1 | 1 | 2 | 60 | 1 | 16.78 | 64.362 | 64.6 | 16.7 | 0.2998 |
|  | 6 | 1 | 1 | 10 | 0.3 | 2 | 1 | 1 | 1 | 45 | 1 | 26.869 | 40.195 | 40.3 | 26.74 | 0.2998 |
|  | 6 | 1 | 1 | 11 | 0.3 | 2 | 1 | 2 | 3 | 80 | 1 | 13.248 | 81.522 | 81.6 | 13.1 | 0.2971 |
|  | 6 | 1 | 1 | 12 | 0.3 | 2 | 1 | 1 | 3 | 80 | 1 | 13.221 | 81.688 | 81.1 | 13.24 | 0.2986 |
|  | 6 | 1 | 2 | 1 | 0.3 | 2 | 1 | 2 | 1 | 45 | 2 | 22.028 | 49.029 | 49.2 | 21.88 | 0.2994 |
|  | 6 | 1 | 2 | 2 | 0.3 | 2 | 1 | 2 | 2 | 60 | 1 | 17.273 | 62.525 | 62.6 | 17.24 | 0.3003 |
|  | 6 | 1 | 2 | 3 | 0.3 | 2 | 1 | 2 | 3 | 80 | 1 | 13.968 | 77.320 | 77.5 | 13.89 | 0.2993 |
|  | 6 | 1 | 2 | 4 | 0.3 | 2 | 1 | 1 | 1 | 45 | 2 | 22.738 | 47.498 | 47.7 | 22.57 | 0.2995 |
|  | 6 | 1 | 2 | 5 | 0.3 | 2 | 1 | 1 | 3 | 80 | 1 | 13.624 | 79.272 | 80.3 | 13.42 | 0.2996 |
|  | 6 | 1 | 2 | 6 | 0.3 | 2 | 1 | 1 | 2 | 60 | 1 | 16.825 | 64.190 | 64.3 | 16.7 | 0.2987 |
|  | 6 | 1 | 2 | 7 | 0.1 | 1 | 1 | 1 | 2 | 60 | 1 | 6.603 | 54.521 | 54.6 | 6.55 | 0.0994 |
|  | 6 | 1 | 2 | 8 | 0.1 | 1 | 1 | 1 | 1 | 45 | 1 | 8.677 | 41.489 | 42 | 8.53 | 0.0995 |
|  | 6 | 1 | 2 | 9 | 0.1 | 1 | 1 | 2 | 3 | 80 | 1 | 4.645 | 77.503 | 78.4 | 4.6 | 0.1004 |
|  | 6 | 1 | 2 | 10 | 0.1 | 1 | 1 | 1 | 3 | 80 | 2 | 4.359 | 82.588 | 80.9 | 4.39 | 0.0987 |
| $\stackrel{\leftrightarrow}{-}$ | 6 | 1 | 2 | 11 | 0.1 | 1 | 1 | 2 | 2 | 60 | 1 | 6.034 | 59.662 | 58.9 | 6.12 | 0.1001 |
| $\checkmark$ | 6 | 1 | 2 | 12 | 0.1 | 1 | 1 | 2 | 1 | 45 | 1 | 7.641 | 47.114 | 46.6 | 7.7 | 0.0998 |
|  | 6 | 1 | 3 | 1 | 0.3 | 2 | 1 | 2 | 1 | 45 | 1 | 22.209 | 48.629 | 49.2 | 21.92 | 0.3001 |
|  | 6 | 1 | 3 | 2 | 0.3 | 2 | 1 | 1 | 2 | 60 | 2 | 18.037 | 59.877 | 60.4 | 17.85 | 0.3 |
|  | 6 | 1 | 3 | 3 | 0.3 | 2 | 1 | 2 | 3 | 80 | 1 | 13.035 | 82.854 | 83.9 | 12.85 | 0.2998 |
|  | 6 | 1 | 3 | 4 | 0.3 | 2 | 1 | 2 | 2 | 60 | 1 | 17.457 | 61.866 | 62.3 | 17.28 | 0.2992 |
|  | 6 | 1 | 3 | 5 | 0.3 | 2 | 1 | 1 | 3 | 80 | 1 | 12.874 | 83.890 | 84.1 | 12.78 | 0.2988 |
|  | 6 | 1 | 3 | 6 | 0.3 | 2 | 1 | 1 | 1 | 45 | 1 | 24.134 | 44.750 | 45 | 23.9 | 0.299 |
|  | 6 | 1 | 3 | 7 | 0.1 | 1 | 1 | 1 | 3 | 80 | 1 | 4.395 | 81.911 | 80.4 | 4.42 | 0.0989 |
|  | 6 | 1 | 3 | 8 | 0.1 | 1 | 1 | 2 | 3 | 80 | 1 | 4.202 | 85.673 | 84.6 | 4.21 | 0.099 |
|  | 6 | 1 | 3 | 9 | 0.1 | 1 | 1 | 1 | 1 | 45 | 1 | 9.002 | 39.991 | 40.7 | 8.85 | 0.1001 |
|  | 6 | 1 | 3 | 10 | 0.1 | 1 | 1 | 2 | 2 | 60 | 1 | 5.985 | 60.150 | 59.1 | 6.01 | 0.0988 |
|  | 6 | 1 | 3 | 11 | 0.1 | 1 | 1 | 1 | 2 | 60 | 1 | 5.591 | 64.389 | 65.3 | 5.47 | 0.0993 |
|  | 6 | 1 | 3 | 12 | 0.1 | 1 | 1 | 2 | 1 | 45 | 1 | 7.491 | 48.058 | 48.4 | 7.41 | 0.0998 |
|  | 6 | 1 | 4 | 1 | 0.1 | 1 | 1 | 2 | 1 | 45 | 1 | 7.794 | 46.189 | 45.9 | 7.84 | 0.1002 |
|  | 6 | 1 | 4 | 2 | 0.1 | 1 | 1 | 1 | 2 | 60 | 1 | 6.21 | 57.971 | 58 | 6.22 | 0.1003 |
|  | 6 | 1 | 4 | 3 | 0.1 | 1 | 1 | 2 | 2 | 60 | 1 | 5.955 | 60.453 | 61.5 | 5.9 | 0.1008 |
|  | 6 | 1 | 4 | 4 | 0.1 | 1 | 1 | 2 | 3 | 80 | 1 | 4.655 | 77.336 | 78.7 | 4.57 | 0.1 |
|  | 6 | 1 | 4 | 5 | 0.1 | 1 | 1 | 1 | 1 | 45 | 1 | 7.668 | 46.948 | 45.9 | 7.81 | 0.0996 |
|  | 6 | 1 | 4 | 6 | 0.1 | 1 | 1 | 1 | 3 | 80 | 1 | 4.377 | 82.248 | 82.2 | 4.35 | 0.0994 |
|  | 6 | 1 | 4 | 7 | 0.3 | 2 | 1 | 1 | 3 | 80 | 1 | 13.739 | 78.608 | 78.4 | 13.78 | 0.3004 |
|  | 6 | 1 | 4 | 8 | 0.3 | 2 | 1 | 2 | 1 | 45 | 1 | 21.369 | 50.541 | 50.9 | 21.2 | 0.3002 |
|  | 6 | 1 | 4 | 9 | 0.3 | 2 | 1 | 2 | 3 | 80 | 1 | 13.844 | 78.012 | 77.9 | 13.82 | 0.2994 |
|  | 6 | 1 | 4 | 10 | 0.3 | 2 | 1 | 1 | 1 | 45 | 1 | 22.927 | 47.106 | 47.2 | 22.89 | 0.3005 |
|  | 6 | 1 | 4 | 11 | 0.3 | 2 | 1 | 2 | 2 | 60 | 1 | 17.72 | 60.948 | 61.1 | 17.64 | 0.2998 |
|  | 6 | 1 | 4 | 12 | 0.3 | 2 | 1 | 1 | 2 | 60 | 1 | 17.499 | 61.718 | 62.1 | 17.35 | 0.2995 |


| SubNum | SessNum | RepNum | Trialno | CrsDist 0.1 | CrsDistR | Reftype | VMethod | NomSpd | DesrdSpd | NoAt tempts | Truetime 8.281 | TrueSpd 43.473 | VASspeed 43.6 | VAStime 8.24 | VASdist 0.0999 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7 | 1 | 1 | 2 | 0.1 | 1 | 1 | 1 | 3 | 80 | 1 | 4.425 | 81.356 | 80.1 | 4.42 | 0.0985 |
| 7 | 1 | 1 | 3 | 0.1 | 1 | 1 | 1 | 2 | 60 | 1 | 6.659 | 54.062 | 54.2 | 6.62 | 0.0999 |
| 7 | 1 | 1 | 4 | 0.1 | 1 | 1 | 2 | 3 | 80 | 4 | 4.357 | 82.626 | 82.6 | 4.35 | 0.1 |
| 7 | 1 | 1 | 5 | 0.1 | 1 | 1 | 2 | 1 | 45 | 1 | 8.392 | 42.898 | 43.1 | 8.31 | 0.0997 |
| 7 | 1 | 1 | 6 | 0.1 | 1 | 1 | 2 | 2 | 60 | 1 | 5.6 | 64.286 | 64 | 5.58 | 0.0993 |
| 7 | 1 | 1 | 7 | 0.3 | 2 | 1 | 2 | 2 | 60 | 1 | 18.048 | 59.840 | 59.8 | 17.96 | 0.2987 |
| 7 | 1 | 1 | 8 | 0.3 | 2 | 1 | 1 | 3 | 80 | 1 | 14.175 | 76.190 | 76.4 | 14.04 | 0.2982 |
| 7 | 1 | 1 | 9 | 0.3 | 2 | 1 | 1 | 1 | 45 | 1 | 23.477 | 46.002 | 46.3 | 23.29 | 0.3001 |
| 7 | 1 | 1 | 10 | 0.3 | 2 | 1 | 2 | 1 | 45 | 1 | 24.859 | 43.445 | 43.5 | 24.87 | 0.3006 |
| 7 | 1 | 1 | 11 | 0.3 | 2 | 1 | 2 | 3 | 80 | 2 | 12.858 | 83.994 | 84 | 12.78 | 0.2983 |
| 7 | 1 | 1 | 12 | 0.3 | 2 | 1 | 1 | 2 | 60 | 1 | 19.408 | 55.647 | 55.8 | 19.33 | 0.2997 |
| 7 | 1 | 2 | 1 | 0.3 | 2 | 1 | 2 | 3 | 80 | 1 | 13.084 | 82.544 | 82.4 | 12.96 | 0.2969 |
| 7 | 1 | 2 | 2 | 0.3 | 2 | 1 | 2 | 2 | 60 | 2 | 19.417 | 55.621 | 55.5 | 19.36 | 0.299 |
| 7 | 1 | 2 | 3 | 0.3 | 2 | 1 | 2 | 1 | 45 | 1 | 26.253 | 41.138 | 41 | 26.24 | 0.2992 |
| 7 | 1 | 2 | 4 | 0.3 | 2 | 1 | 1 | 3 | 80 | 1 | 12.827 | 84.197 | 85.1 | 12.6 | 0.2981 |
| 7 | 1 | 2 | 5 | 0.3 | 2 | 1 | 1 | 2 | 60 | 1 | 17.793 | 60.698 | 60.8 | 17.71 | 0.2994 |
| 7 | 1 | 2 | 6 | 0.3 | 2 | 1 | 1 | 1 | 45 | 1 | 23.038 | 46.879 | 47 | 22.89 | 0.2991 |
| 7 | 1 | 2 | 7 | 0.1 | 1 | 1 | 2 | 2 | 60 | 1 | 5.829 | 61.760 | 60.4 | 5.9 | 0.0992 |
| 7 | 1 | 2 | 8 | 0.1 | 1 | 1 | 2 | 1 | 45 | 1 | 8.116 | 44.357 | 44.8 | 8.02 | 0.1 |
| 7 | 1 | 2 | 9 | 0.1 | 1 | 1 | 1 | 1 | 45 | 1 | 7.142 | 50.406 | 49.5 | 7.16 | 0.0985 |
| 7 | 1 | 2 | 10 | 0.1 | 1 | 1 | 1 | 3 | 80 | 1 | 4.722 | 76.239 | 75.4 | 4.75 | 0.0996 |
| 7 | 1 | 2 | 11 | 0.1 | 1 | 1 | 2 | 3 | 80 | 2 | 4.387 | 82.061 | 82.2 | 4.39 | 0.1002 |
| 7 | 1 | 2 | 12 | 0.1 |  |  | 1 | 2 | 60 | 1 | 5.589 | 64.412 | 62.6 | 5.65 | 0.0984 |
| 7 | 1 | 3 | 1 | 0.3 | 2 | 1 | 2 | 2 | 60 | 1 | 18.039 | 59.870 | 60.2 | 17.92 | 0.2998 |
| 7 | 1 | 3 | 2 | 0.3 | 2 | 1 | 1 | 1 | 45 | 1 | 26.454 | 40.826 | 41.1 | 26.28 | 0.3004 |
| 7 | 1 | 3 | 3 | 0.3 | 2 | 1 | 1 | 3 | 80 | 2 | 14.006 | 77.110 | 74.6 | 14.43 | 0.2991 |
| 7 | 1 | 3 | 4 | 0.3 | 2 | 1 | 2 | 3 | 80 | 1 | 12.889 | 83.792 | 84.1 | 12.81 | 0.2994 |
| 7 | 1 | 3 | 5 | 0.3 | 2 | 1 | 2 | 1 | 45 | 1 | 21.288 | 50.733 | 51.1 | 21.13 | 0.3002 |
| 7 | 1 | 3 | 6 | 0.3 | 2 | 1 | 1 | 2 | 60 | 1 | 16.893 | 63.932 | 64.3 | 16.77 | 0.2997 |
| 7 | 1 | 3 | 7 | 0.1 | 1 | 1 | 1 | 1 | 45 | 1 | 7.779 | 46.278 | 46.6 | 7.7 | 0.0998 |
| 7 | 1 | 3 | 8 | 0.1 | 1 | 1 | 1 | 2 | 60 | 1 | 6.157 | 58.470 | 59.3 | 6.08 | 0.1002 |
| 7 | 1 | 3 | 9 | 0.1 | 1 | 1 | 1 | 3 | 80 | 1 | 4.377 | 82.248 | 81.6 | 4.35 | 0.0987 |
| 7 | 1 | 3 | 10 | 0.1 | 1 | 1 | 2 | 3 | 80 | 1 | 4.599 | 78.278 | 77.3 | 4.57 | 0.0982 |
| 7 | 1 | 3 | 11 | 0.1 | 1 | 1 | 2 | 2 | 60 | 1 | 6.449 | 55.823 | 54.9 | 6.44 | 0.0983 |
| 7 | 1 | 3 | 12 | 0.1 | 1 | 1 | 2 | 1 | 45 | 1 | 8.241 | 43.684 | 43.8 | 8.17 | 0.0994 |
| 7 | 1 | 4 | 1 | 0.3 | 2 | 1 | 2 | 3 | 80 | 1 | 14.096 | 76.617 | 77.4 | 13.89 | 0.2988 |
| 7 | 1 | 4 | 2 | 0.3 | 2 | 1 | 1 | 3 | 80 | 1 | 13.101 | 82.436 | 82.3 | 13.03 | 0.2981 |
| 7 | 1 | 4 | 3 | 0.3 | 2 | 1 | 2 | 1 | 45 | 1 | 22.322 | 48.383 | 48.8 | 22.14 | 0.3001 |
| 7 | 1 | 4 | 4 | 0.3 | 2 | 1 | 1 | 2 | 60 | 1 | 17.409 | 62.037 | 61.7 | 17.46 | 0.2992 |
| 7 | 1 | 4 | 5 | 0.3 | 2 | 1 | 2 | 2 | 60 | 1 | 16.536 | 65.312 | 66 | 16.34 | 0.3 |
| 7 | 1 | 4 | 6 | 0.3 | 2 | 1 | 1 | 1 | 45 | 1 | 21.079 | 51.236 | 51.3 | 20.98 | 0.2996 |
| 7 | 1 | 4 | 7 | 0.1 | 1 | 1 | 1 | 3 | 80 | 1 | 4.348 | 82.797 | 78.8 | 4.5 | 0.0986 |
| 7 | 1 | 4 | 8 | 0.1 | 1 | 1 | 2 | 3 | 80 | 1 | 4.178 | 86.166 | 87.6 | 4.1 | 0.0998 |
| 7 | 1 | 4 | 9 |  | an 1 | 1 | 2 | 2 | 60 | 1 | 6.341 | 56.773 | 57.6 | 6.26 | 0.1002 |
| 7 | 1 | 4 | 10 | 0.1 | 1 | 1 | 1 | 2 | 60 | 1 | 5.611 | 64.160 | 64.6 | 5.54 | 0.0995 |
| 7 | 1 | 4 | 11 | 0.1 | 1 | 1 | 1 | 1 | 45 | 1 | 7.661 | 46.991 | 46.4 | 7.63 | 0.0985 |
| 7 | 1 | 4 | 12 | 0.1 | 1 | 1 | 2 | 1 | 45 | 1 | 7.1 | 50.704 | 50.7 | 7.05 | 0.0994 |

TABLE 1.5 -- Raw Data for Moving Study (Continued)

| SubNum | SessNum | RepNum | Trialno | CrsDist | Crsoistr | Reftype | VMethoo' | NomSpd | DesrdSpd | NoAttempts | TrueTime | TrueSpd | VASspeed | VAStime | VASdist |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 8 | 1 | 1 | 1 | 0.1 | 1 | 1 | 2 | 1 | 45 | 3 | 8.281 | 43.473 | 44 | 8.2 | 0.1003 |
| 8 | 1 | 1 | 2 | 0.1 | 1 | 1 | 2 | 3 | 80 | 2 | 4.395 | 81.911 | 84.5 | 4.24 | 0.0997 |
| 8 | 1 | 1 | 3 | 0.1 | 1 | 1 | 2 | 2 | 60 | 1 | 6.659 | 54.062 | 54 | 6.66 | 0.0999 |
| 8 | 1 | 1 | 4 | 0.1 | 1 | 1 | 1 | 3 | 80 | 1 | 4.374 | 82.305 | 77.5 | 4.57 | 0.0984 |
| 8 | 1 | 1 | 5 | 0.1 | 1 | 1 | 1 | 1 | 45 | 1 | 8.392 | 42.898 | 43 | 8.35 | 0.0998 |
| 8 | 1 | 1 | 6 | 0.1 | 1 | 1 | 1 | 2 | 60 | 1 | 5.6 | 64.286 | 64.4 | 5.54 | 0.0992 |
| 8 | 1 | 1 | 7 | 0.3 | 2 | 1 | 1 | 2 | 60 | 2 | 18.048 | 59.840 | 60.1 | 17.96 | 0.2999 |
| 8 | 1 | 1 | 8 | 0.3 | 2 | 1 | 2 | 3 | 80 | 1 | 14.175 | 76.190 | 76.7 | 14.07 | 0.3002 |
| 8 | 1 | 1 | 9 | 0.3 | 2 | 1 | 2 | 1 | 45 | 2 | 24.161 | 44.700 | 44.4 | 24.26 | 0.2994 |
| 8 | 1 | 1 | 10 | 0.3 | 2 | 1 | 1 | 1 | 45 | 1 | 24.859 | 43.445 | 43.6 | 24.66 | 0.2993 |
| 8 | 1 | 1 | 11 | 0.3 | 2 | 1 | 1 | 3 | 80 | 2 | 12.858 | 83.994 | 83.7 | 12.85 | 0.2989 |
| 8 | 1 | 1 | 12 | 0.3 | 2 | 1 | 2 | 2 | 60 | 1 | 19.408 | 55.647 | 55.5 | 19.4 | 0.2996 |
| 8 | 1 | 2 | 1 | 0.3 | 2 | 1 | 1 | 3 | 80 | 1 | 13.084 | 82.544 | 81.5 | 13.14 | 0.2976 |
| 8 | 1 | 2 | 2 | 0.3 | 2 | 1 | 1 | 2 | 60 | 1 | 19.27 | 56.046 | 56.1 | 19.22 | 0.2999 |
| 8 | 1 | 2 | 3 | 0.3 | 2 | 1 | 1 | 1 | 45 | 1 | 26.253 | 41.138 | 41.1 | 26.24 | 0.3001 |
| 8 | 1 | 2 | 4 | 0.3 | 2 | 1 | 2 | 3 | 80 | 2 | 12.995 | 83.109 | 84.6 | 12.81 | 0.3013 |
| 8 | 1 | 2 | 5 | 0.3 | 2 | 1 | 2 | 2 | 60 | 1 | 17.793 | 60.698 | 61.2 | 17.6 | 0.2994 |
| 8 | 1 | 2 | 6 | 0.3 | 2 | 1 | 2 | 1 | 45 | 1 | 23.038 | 46.879 | 47.1 | 22.89 | 0.2999 |
| 8 | 1 | 2 | 7 | 0.1 | 1 | 1 | 1 | 2 | 60 | 2 | 5.844 | 61.602 | 61.1 | 5.94 | 0.1009 |
| 8 | 1 | 2 | 8 | 0.1 | 1 | 1 | 1 | 1 | 45 | 1 | 8.116 | 44.357 | 44.7 | 7.99 | 0.0994 |
| 8 | 1 | 2 | 9 | 0.1 | 1 | 1 | 2 | 1 | 45 | 1 | 7.142 | 50.406 | 51.5 | 7.02 | 0.1006 |
| 8 | 1 | 2 | 10 | 0.1 | 1 | 1 | 2 | 3 | 80 | 1 | 4.722 | 76.239 | 77.5 | 4.64 | 0.1 |
| 8 | 1 | 2 | 11 | 0.1 | 1 | 1 | 1 | 3 | 80 | 1 | 4.378 | 82.229 | 81.4 | 4.42 | 0.1002 |
| 8 | 1 | 2 | 12 | 0.1 | 1 | 1 | 2 | 2 | 60 | 1 | 5.589 | 64.412 | 64.5 | 5.58 | 0.1001 |
| 8 | 1 | 3 | 1 | 0.3 | 2 | 1 | 1 | 2 | 60 | 1 | 18.039 | 59.870 | 59.5 | 18.1 | 0.2996 |
| 8 | 1 | 3 | 2 | 0.3 | 2 | 1 | 2 | 1 | 45 | 1 | 26.454 | 40.826 | 41.1 | 26.24 | 0.3 |
| 8 | 1 | 3 | 3 | 0.3 | 2 | 1 | 2 | 3 | 80 | 1 | 14.001 | 77.137 | 77.9 | 13.86 | 0.3002 |
| 8 | 1 | 3 | 4 | 0.3 | 2 | 1 | 1 | 3 | 80 | 2 | 12.887 | 83.805 | 83.8 | 12.85 | 0.2993 |
| 8 | 1 | 3 | 5 | 0.3 | 2 | 1 | 1 | 1 | 45 | 1 | 21.288 | 50.733 | 51.5 | 20.98 | 0.3006 |
| 8 | 1 | 3 | 6 | 0.3 | 2 | 1 | 2 | 2 | 60 | 1 | 16.893 | 63.932 | 64.1 | 16.88 | 0.3008 |
| 8 | 1 | 3 | 7 | 0.1 | 1 | 1 | 2 | 1 | 45 | 1 | 7.779 | 46.278 | 46.6 | 7.74 | 0.1002 |
| 8 | 1 | 3 | 8 | 0.1 | 1 | 1 | 2 | 2 | 60 | 1 | 6.157 | 58.470 | 58.1 | 6.15 | 0.0995 |
| 8 | 1 | 3 | 9 | 0.1 | 1 | 1 | 2 | 3 | 80 | 1 | 4.377 | 82.248 | 82.4 | 4.35 | 0.0998 |
| 8 | 1 | 3 | 10 | 0.1 | 1 | 1 | 1 | 3 | 80 | 1 | 4.599 | 78.278 | 77.5 | 4.6 | 0.0992 |
| 8 | 1 | 3 | 11 | 0.1 | 1 | 1 | 1 | 2 | 60 | 1 | 6.449 | 55.823 | 57.5 | 6.26 | 0.1002 |
| 8 | 1 | 3 | 12 | 0.1 | 1 | 1 |  |  | 45 | 1 | 8.241 | 43.684 | 43.9 | 8.13 | 0.0992 |
| 8 | 1 | 4 | 1 | 0.3 | 2 | 1 | 1 | 3 | 80 | 1 | 14.096 | 76.617 | 77 | 14 | 0.2995 |
| 8 | 1 | 4 | 2 | 0.3 | 2 | 1 | 2 | 3 | 80 | 1 | 13.101 | 82.436 | 82.7 | 13.06 | 0.3004 |
| 8 | 1 | 4 | 3 | 0.3 | 2 | 1 | 1 | 9 | 45 | 1 | 22.322 | 48.383 | 48.1 | 22.39 | 0.2995 |
| 8 | 1 | 4 | 4 | 0.3 | 2 | 1 | 2 | 2 | 60 | 1 | 17.409 | 62.037 | 61.7 | 17.42 | 0.2986 |
| 8 | 1 | 4 | 5 | 0.3 | 2 | 1 | 1 | 2 | 60 | 1 | 16.536 | 65.312 | 65.3 | 16.48 | 0.2993 |
| 8 | 1 | 4 | 6 | 0.3 | 2 | 1 | 2 | 1 | 45 | 1 | 21.079 | 51.236 | 51.4 | 20.98 | 0.3001 |
| 8 | 1 | 4 | 7 | 0.1 | 1 | 1 | 2 | 3 | 80 | 1 | 4.348 | 82.797 | 82.8 | 4.32 | 0.0993 |
| 8 | 1 | 4 | 8 | 0.1 | 1 | 1 | 1 | 3 | 80 | 1 | 4.178 | 86.166 | 85.8 | 4.14 | 0.0987 |
| 8 | 1 | 4 | 9 | 0.1 | 1 | 1 | 1 | 2 | 60 | 1 | 6.341 | 56.773 | 56.2 | 6.37 | 0.0995 |
| 8 | 1 | 4 | 10 | 0.1 | 1 | 1 | 2 | 2 | 60 | 1 | 5.611 | 64.160 | 63 | 5.68 | 0.0995 |
| 8 | 1 | 4 | 11 | 0.1 | 1 | 1 | 2 | 1 | 45 | 1 | 7.661 | 46.991 | 46.8 | 7.66 | 0.0998 |
| 8 | 1 | 4 | 412 | 0.1 | 1 | 1 | 1 | 1 | 45 | 1 | 7.1 | 50.704 | 51.3 | 6.98 | 0.0995 |

TABLE I. $6-$ Night Moving Summary Statistics
Upper
VASCAR Course Nominal
Method Distance Speed $N$ Mean Limit $95 \%$-tile $99 \%$-tile MSE Variance $K$

| Night Moving - Overall | 36 | 0.322 | 1.046 | 1.450 | 1.824 | 0.1176 | 0.243 | 2.082 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Following | 0.3 | 45 | 12 | 0.128 | 0.477 | 0.412 | 0.466 | 0.0173 | 0.055 | 2.655 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Following | 0.3 | 60 | 12 | 0.120 | 1.020 | 0.391 | 0.397 | 0.1148 | 0.102 | 2.655 |
| Following | 0.3 | 80 | 12 | 0.748 | 1.994 | 1.784 | 1.862 | 0.2204 | 0.331 | 2.655 |

Similar Day Clocks - Subjects, Distance, Speeds

|  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |


| Day Moving - Overall | 72 | 0.059 | 0.987 | 0.696 | 0.953 | 0.2325 | 0.248 | 1.924 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Following | 0.3 | 45 | 24 | 0.122 | 0.584 | 0.295 | 0.655 | 0.0432 | 0.044 | 2.225 |
| :--- | :--- | :--- | :--- | ---: | :--- | :--- | :--- | :--- | :--- | :--- |
| Following | 0.3 | 60 | 24 | 0.142 | 0.676 | 0.438 | 0.503 | 0.0575 | 0.057 | 2.225 |
| Following | 0.3 | 80 | 24 | -0.085 | 1.793 | 0.874 | 0.998 | 0.7121 | 0.632 | 2.225 |

Nighttime Moving Study
A. Variables

Subject Number
Nominal Speed
Light Condition
B. Significant Effects (p $\leq 0.05$ )

Light Condition

| Light <br> Condition | Mean <br> Error |
| :---: | :---: |
| Day <br> Night | .059 |

Light Condition $x$ Nominal Speed

| Light <br> Condition | Mean Speed Error |  |  |
| :---: | :---: | :---: | :---: |
|  | -.044 | 60 | 80 |

C. Nearly Significant Effects

Nominal Speed $(p=.07)$

| Nominal <br> Speed | Mean <br> Error |
| :---: | :---: |
| 45 | .066 |
| 60 | .134 |
| 80 | .193 |

TABLE I. 7 -- Raw Data for the Night Moving Study

| SubNum | SessNum | RepNum | TrialNo | CrsDist 0.3 | CrsDistR | Reftype | VMethod | NomSpd | DesrdSpd | NoAt tempts | Truerime 22.39 | TrueSpd 48.236 | VASspeed 46 | VAStime 23.4 | VASdist 0.2995 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | 4 | 1 | 4 | 0.3 | 1 | 4 | 1 | 1 | 45 | 9 | 23.419 | 46.116 | 46 | 23.5 | 0.3006 |
| 3 | 4 | 1 | 6 | 0.3 | 1 | 4 | 1 | 2 | 60 | 1 | 18.314 | 58.971 | 59.1 | 18.18 | 0.2988 |
| 3 | 4 | 1 | 3 | 0.3 | 1 | 4 | 1 | 2 | 60 | 1 | 18.194 | 59.360 | 59.4 | 18.18 | 0.2999 |
| 3 | 4 | 1 | 2 | 0.3 | 1 | 4 | 1 | 3 | 80 | 2 | 13.45 | 80.297 | 80.8 | 13.35 | 0.2997 |
| 3 | 4 | 1 | 5 | 0.3 | 1 | 4 | 1 | 3 | 80 | 1 | 13.586 | 79.494 | 80 | 13.5 | 0.3002 |
| 4 | 4 | 1 | 6 | 0.3 | 1 | 4 | 1 | 1 | 45 | 1 | 23.393 | 46.168 | 46.2 | 23.25 | 0.2984 |
| 4 | 4 | 1 | 3 | 0.3 | 1 | 4 | 1 | 1 | 45 | 1 | 23.432 | 46.091 | 46.1 | 23.36 | 0.2992 |
| 4 | 4 | 1 | 2 | 0.3 | 1 | 4 | 1 | 2 | 60 | 1 | 18.355 | 58.840 | 59.1 | 18.25 | 0.2998 |
| 4 | 4 | 1 | 4 | 0.3 | 1 | 4 | 1 | 2 | 60 | 1 | 18.218 | 59.282 | 58.5 | 18.5 | 0.3009 |
| 4 | 4 | 1 | 5 | 0.3 | 1 | 4 | 1 | 3 | 80 | 1 | 13.51 | 79.941 | 80.4 | 13.42 | 0.3 |
| 4 | 4 | 1 | 1 | 0.3 | 1 | 4 | 1 | 3 | 80 | 1 | 13.43 | 80.417 | 80.8 | 13.39 | 0.3008 |
| 5 | 4 | 1 | 6 | 0.3 | 1 | 4 | 1 | 1 | 45 | 1 | 26.256 | 41.133 | 41.5 | 25.99 | 0.2999 |
| 5 | 4 | 1 | 1 | 0.3 | 1 | 4 | 1 | 1 | 45 | 1 | 26.443 | 40.843 | 41.2 | 26.24 | 0.3003 |
| 5 | 4 | 1 | 5 | 0.3 | 1 | 4 | 1 | 2 | 60 | 1 | 19.034 | 56.741 | 57 | 18.86 | 0.2991 |
| 5 | 4 | 1 | 2 | 0.3 | 1 | 4 | 1 | 2 | 60 | 1 | 16.972 | 63.634 | 63.7 | 16.92 | 0.2997 |
| 5 | 4 | 1 | 4 | 0.3 | 1 | 4 | 1 | 3 | 80 | 1 | 13.015 | 82.981 | 84.7 | 12.7 | 0.299 |
| 5 | 4 | 1 | 3 | 0.3 | 1 | 4 | 1 | 3 | 80 | 1 | 13.789 | 78.323 | 79.7 | 13.53 | 0.2999 |
| 6 | 4 | 1 | 4 | 0.3 | 1 | 4 | 1 | 1 | 45 | 1 | 26.466 | 40.807 | 40.9 | 26.35 | 0.2996 |
| 6 | 4 | 1 | 2 | 0.3 | 1 | 4 | 1 | 1 | 45 | 1 | 23.552 | 45.856 | 46.1 | 23.36 | 0.2995 |
| 6 | 4 |  | 1 | 0.3 | 1 | 4 | 1 | 2 | 60 | 1 | 18.398 | 58.702 | 59.1 | 18.21 | 0.2992 |
| 6 | 4 | 1 | 3 | 0.3 | 1 | 4 | 1 | 2 | 60 | 1 | 17.313 | 62.381 | 62.7 | 17.2 | 0.2997 |
| 6 | 4 | 1 | 5 | 0.3 | 1 | 4 | 1 | 3 | 80 | 2 | 12.911 | 83.650 | 84.4 | 12.78 | 0.2996 |
| 6 | 4 | , | 6 | 0.3 | 1 | 4 | 1 | 3 | 80 | 1 | 13.146 | 82.154 | 82.7 | 13.06 | 0.3005 |
| 7 | 4 | , | 5 | 0.3 | 1 | 4 | 1 | 1 | 45 | 1 | 21.591 | 50.021 | 50.5 | 21.27 | 0.2987 |
| 7 | 4 | 1 | 1 | 0.3 | 1 | 4 | 1 | 1 | 45 | 1 | 25.435 | 42.461 | 42.8 | 25.16 | 0.2997 |
| 7 | 4 | 1 | 6 | 0.3 | 1 | 4 | 1 | 2 | 60 | 1 | 16.394 | 65.878 | 65.8 | 16.38 | 0.2993 |
| 7 | 4 | 1 | 3 | 0.3 | 1 | 4 | 1 | 2 | 60 | 1 | 17.672 | 61.114 | 61.5 | 17.49 | 0.2989 |
| 7 | 4 | 1 | 2 | 0.3 | 1 | 4 | 1 | 3 | 80 | 1 | 13.79 | 78.318 | 80.2 | 13.39 | 0.2987 |
| 7 | 4 | 1 | 4 | 0.3 | 1 | 4 | 1 | 3 | 80 | 1 | 14.212 | 75.992 | 76.3 | 14.11 | 0.2994 |
| 8 | 4 | 1 | 3 | 0.3 | 1 | 4 | 1 | 1 | 45 | 1 | 21.841 | 49.448 | 49.2 | 21.85 | 0.2992 |
| 8 | 4 | 1 | 4 | 0.3 | 1 | 4 | 1 | 1 | 45 | 1 | 25.089 | 43.047 | 43.2 | 24.49 | 0.2994 |
| 8 | 4 | 1 | 1 | 0.3 | 1 | 4 | 1 | 2 | 60 | 1 | 17.573 | 61.458 | 61.6 | 17.56 | 0.3007 |
| 8 | 4 | 1 | 6 | 0.3 | 1 | 4 | 1 | 2 | 60 | 1 | 17.618 | 61.301 | 61.6 | 17.49 | 0.2995 |
| 8 | 4 | 1 | 2 | 0.3 | 1 | 4 | 1 | 3 | 80 | 1 | 13.723 | 78.700 | 79 | 13.64 | 0.2996 |
| 8 | 4 | 1 | 5 | 0.3 | 1 | 4 | 1 | 3 | 80 | 2 | 13.051 | 82.752 | 83 | 12.96 | 0.2991 |



Bridge Moving - Overall | 56 | 0.251 | 1.308 | 1.296 | 1.544 | 0.2874 | 0.362 | 1.972 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

| Following 60 | both | 28 | 0.158 | 1.353 | 0.942 | 1.179 | 0.3046 | 0.349 | 2.165 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Following 80 | both | 28 | 0.344 | 1.469 | 1.486 | 1.577 | 0.2702 | 0.371 | 2.165 |


| Following 60 | short | 14 | 0.265 | 1.354 | 0.902 | 0.976 | 0.1854 | 0.392 | 2.529 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Following 60 | long | 14 | 0.051 | 1.697 | 0.899 | 1.180 | 0.4237 | 0.372 | 2.529 |
| Following 80 | short | 14 | 0.404 | 1.932 | 1.315 | 1.457 | 0.3651 | 0.262 | 2.529 |
| Following 80 | long | 14 | 0.285 | 1.344 | 1.516 | 1.591 | 0.1753 | 0.500 | 2.529 |

## Bridge Study - Moving Portion

A. Variables

Subject Number
Nominal Speed
Vehicle Gap
B. Significant Effects ( $\mathrm{p} \leq 0.05$ )

Subject x Nominal Speed

| Subject Number | Mean Error |  |
| :---: | :---: | :---: |
|  | 60 mph | 80 mph |
| 1 | -. 412 | . 925 |
| 2 | . 662 | . 525 |
| 3 | . 203 | . 262 |
| 4 | -. 074 | . 066 |
| 5 | . 040 | . 356 |
| 6 | . 096 | . 637 |

C. Nearly Significant Effects

Subject $x$ Vehicle Gap $p=0.09$

TABLE I. 9 -- Raw Data for the Moving Portion of the Bridge Study

|  | SubNum | Sessnum | Replum |  | Repeat\# | Trialno | crsdist | CrsDistr VehGap | VehGapR | Reftype | Nomspd | DesrdSpd | NoAttempt | Truet ime | Truespd | VASspeed | VAStime | VASdist |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 |  | 1 | 1 | 1 | 0.3 | $21 / 8 \mathrm{mile}$ | 2 | 2 | 2 | 80 | 1 | 13.119 | 82.323 | 83.8 | 12.81 | 0.2986 |
|  | 1 | 2 |  | 1 | 2 | 1 | 0.3 | $21 / 8 \mathrm{mile}$ | 2 | 2 | 2 | 80 | 1 | 13.256 | 81.473 | 82.5 | 13.14 | 0.3012 |
|  | 1 | 2 |  | 1 | 1 | 4 | 0.3 | $21 / 8$ mile | 2 | 2 | 1 | 60 | 1 | 18.305 | 59.000 | 58.8 | 18.32 | 0.2997 |
|  | 1 | 2 |  | 1 | 2 | 4 | 0.3 | $21 / 8$ mile | 2 | 2 | 1 | 60 | 1 | 18.311 | 58.981 | 59 | 18.28 | 0.2997 |
|  | 1 | 2 |  | 1 | 1 | 6 | 0.3 | 2250 feet | 1 | 2 | 1 | 60 | 1 | 18.197 | 59.350 | 57.9 | 18.5 | 0.2977 |
|  | 1 | 2 |  | 1 | 2 | 6 | 0.3 | 2250 feet | 1 | 2 | 1 | 60 | 1 | 18.116 | 59.616 | 59.6 | 18.07 | 0.2996 |
|  | 1 | 2 |  | 1 | 1 | 7 | 0.3 | 2250 feet | 1 | 2 | 2 | 80 | 1 | 13.285 | 81.295 | 81 | 13.24 | 0.2981 |
|  | 1 | 2 |  | 1 | 2 | 7 | 0.3 | 2250 feet | 1 | 2 | 2 | 80 | 1 | 13.234 | 81.608 | 83.1 | 12.99 | 0.3003 |
|  | 2 | 2 |  | 1 | 1 | 2 | 0.3 | $21 / 8$ mile | 2 | 2 | 1 | 60 | 1 | 18.573 | 58.149 | 58.9 | 18.39 | 0.301 |
|  | 2 | 2 |  | 1 | 2 | 2 | 0.3 | $21 / 8$ mile | 2 | 2 | 1 | 60 | 1 | 18.174 | 59.426 | 59.7 | 18.07 | 0.2997 |
|  | 2 | 2 |  | 1 | 1 | 3 | 0.3 | 2250 feet | 1 | 2 | 2 | 80 | 1 | 13.242 | 81.559 | 82.8 | 13.06 | 0.3006 |
|  | 2 | 2 |  | 1 | 2 | 3 | 0.3 | 2250 feet | 1 | 2 | 2 | 80 | 1 | 13.333 | 81.002 | 81.3 | 13.21 | 0.2985 |
|  | 2 | 2 |  | 1 | 1 | 5 | 0.3 | $21 / 8 \mathrm{mile}$ | 2 | 2 | 2 | 80 | 1 | 13.278 | 81.338 | 81.8 | 13.21 | 0.3003 |
|  | 2 | 2 |  | 1 | 2 | 5 | 0.3 | $21 / 8$ mile | 2 | 2 | 2 | 80 | 2 | 13.235 | 81.602 | 81.7 | 13.21 | 0.3000 |
|  | 2 | 2 |  | 1 | 1 | 8 | 0.3 | 2250 feet | 1 | 2 | 1 | 60 | 1 | 18.283 | 59.071 | 59.7 | 18.1 | 0.3006 |
|  | 2 | 2 |  | 1 | 2 | 8 | 0.3 | 2250 feet | 1 | 2 | 1 | 60 | 1 | 18.089 | 59.705 | 60.7 | 17.74 | 0.2993 |
|  | 3 | 2 |  | 1 | 1 | 1 | 0.3 | $21 / 8$ mile | 2 | 2 | 2 | 80 | 2 | 13.448 | 80.309 | 80.2 | 13.46 | 0.3001 |
|  | 3 | 2 |  | 1 | 1 | 3 | 0.3 | 2250 feet | 1 | 2 | 1 | 60 | 1 | 18.086 | 59.715 | 60.4 | 17.89 | 0.3003 |
|  | 3 | 2 |  | 1 | 1 | 4 | 0.3 | 2250 feet | 1 | 2 | 2 | 80 | 1 | 13.422 | 80.465 | 80.7 | 13.39 | 0.3003 |
|  | 3 | 2 |  | 1 | 1 | 8 | 0.3 | 2 1/8 mile | 2 | 2 | 1 | 60 | 1 | 18.238 | 59.217 | 59.7 | 18.1 | 0.3003 |
|  | 3 | 2 |  | 2 | 1 | 1 | 0.3 | 2250 feet | 1 | 2 | 1 | 60 | 1 | 17.86 | 60.470 | 60.8 | 17.74 | 0.3001 |
|  | 3 | 2 |  | 2 | 1 | 3 | 0.3 | 2 1/8 mile | 2 | 2 | 1 | 60 | 1 | 18.242 | 59.204 | 59.1 | 18.14 | 0.2982 |
| H | 3 | 2 |  | 2 | 1 | 5 | 0.3 | 2250 feet | 1 | 2 | 2 | 80 | 1 | 13.471 | 80.172 | 80.4 | 13.35 | 0.2985 |
| $N$ | 3 | 2 |  | 2 | 1 | 6 | 0.3 | $21 / 8 \mathrm{mile}$ | 2 | 2 | 2 | 80 | 1 | 13.385 | 80.687 | 80.9 | 13.35 | 0.3001 |
|  | 3 | 2 |  | 3 | 1 | 2 | 0.3 | $21 / 8 \mathrm{mile}$ | 2 | 2 | 1 | 60 | 1 | 17.923 | 60.258 | 59.9 | 17.96 | 0.2991 |
|  | 3 | 2 |  | 3 | 1 | 4 | 0.3 | $21 / 8 \mathrm{mile}$ | 2 | 2 | 2 | 80 | 1 | 13.555 | 79.675 | 80.1 | 13.42 | 0.2990 |
|  | 3 | 2 |  | 3 | 1 | 6 | 0.3 | 2250 feet | 1 | 2 | 2 | 80 | 1 | 13.514 | 79.917 | 80.5 | 13.35 | 0.2989 |
|  | 3 | 2 |  | 3 | 1 | 7 | 0.3 - | - 2250 feet | 1 | 2 | 1 | 60 | 2 | 18.147 | 59.514 | 59.7 | 18.07 | 0.2998 |

SubNum Sessnum RepNum Repeat\#TrialNo crsdist CrsDistr VehGap VehGapR RefTy

| ubNum | Sessnum | RepNum |  | Repeat\#Trialno | crsdist | Crsoistr VehGap | VehGapR | RefType | NomSpd | DesrdSpd | NoA t temp | otTrueTime | Truespd | VASspeed | VAStime | VASdist |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4 | 2 |  | 1 | 12 | 0.3 | $21 / 8 \mathrm{mile}$ | 2 | 2 | 2 | 80 | 1 | 13.43 | 80.417 | 79.8 | 13.42 | 0.2979 |
| 4 | 2 |  | 1 | 15 | 0.3 | 2250 feet | 1 | 2 | 2 | 80 | 1 | 13.387 | 80.675 | 81.3 | 13.35 | 0.3017 |
| 4 | 2 |  | 1 | 16 | 0.3 | $21 / 8 \mathrm{mile}$ | 2 | 2 | 1 | 60 | 1 | 18.101 | 59.665 | 58.4 | 18.43 | 0.2993 |
| 4 | 2 |  | 1 | 17 | 0.3 | 2250 feet | 1 | 2 | 1 | 60 | 1 | 18.019 | 59.937 | 60.8 | 17.96 | 0.3035 |
| 4 | 2 |  | 2 | 12 | 0.3 | 2250 feet | 1 | 2 | 2 | 80 | 1 | 13.371 | 80.772 | 80.5 | 13.42 | 0.3003 |
| 4 | 2 |  | 2 | 14 | 0.3 | $21 / 8 \mathrm{mile}$ | 2 | 2 | 2 | 80 | 1 | 13.325 | 81.051 | 80.4 | 13.32 | 0.2977 |
| 4 | 2 |  | 2 | 17 | 0.3 | 2250 feet | 1 | 2 | 1 | 60 | 1 | 18.229 | 59.246 | 59.5 | 18.1 | 0.2993 |
| 4 | 2 |  | 2 | 18 | 0.3 | $21 / 8 \mathrm{mile}$ | 2 | 2 | 1 | 60 | 1 | 18.099 | 59.672 | 59.7 | 18 | 0.2986 |
| 4 | 2 |  | 3 | 19 | 0.3 | $21 / 8 \mathrm{mile}$ | 2 | 2 | 1 | 60 | 1 | 17.885 | 60.386 | 60.6 | 17.78 | 0.2997 |
| 4 | 2 |  | 3 | 13 | 0.3 | $21 / 8 \mathrm{mile}$ | 2 | 2 | 2 | 80 | 1 | 13.484 | 80.095 | 80.1 | 13.46 | 0.2996 |
| 4 | 2 |  | 3 | 15 | 0.3 | 2250 feet | 1 | 2 | 1 | 60 | 1 | 18 | 60.000 | 60.3 | 17.89 | 0.3000 |
| 4 | 2 |  | 3 | 18 | 0.3 | 2250 feet | 1 | 2 | 2 | 80 | 1 | 13.41 | 80.537 | 81 | 13.28 | 0.2991 |
| 5 | 2 |  | 1 | 13 | 0.3 | $21 / 8 \mathrm{mile}$ | 2 | 2 | 2 | 80 | 1 | 12.944 | 83.436 | 82.9 | 12.99 | 0.2995 |
| 5 | 2 |  | 1 | 15 | 0.3 | 2250 feet | 1 | 2 | 1 | 60 | 1 | 18.268 | 59.120 | 59.4 | 18.18 | 0.3001 |
| 5 | 2 |  | 1 | 16 | 0.3 | 2 1/8 mile | 2 | 2 | 1 | 60 | 1 | 18.281 | 59.078 | 58.9 | 18.28 | 0.2992 |
| 5 | 2 |  | 1 | 18 | 0.3 | 2250 feet | 1 | 2 | 2 | 80 | 1 | 12.829 | 84.184 | 84.1 | 12.78 | 0.2987 |
| 5 | 2 |  | 2 | 11 | 0.3 | 2250 feet | 1 | 2 | 2 | 80 | 1 | 12.933 | 83.507 | 84.2 | 12.78 | 0.2991 |
| 5 | 2 |  | 2 | 12 | 0.3 | 2250 feet | 1 | 2 | 1 | 60 | 1 | 17.843 | 60.528 | 60.6 | 17.78 | 0.2994 |
| 5 | 2 |  | 2 | 15 | 0.3 | $21 / 8$ mile | 2 | 2 | 2 | 80 | 1 | 13.617 | 79.313 | 79.4 | 13.64 | 0.3011 |
| 5 | 2 |  | 2 | 18 | 0.3 | $21 / 8 \mathrm{mile}$ | 2 | 2 | 1 | 60 | 1 | 19.132 | 56.450 | 57.7 | 18.72 | 0.3004 |
| 6 | 2 |  | 1 | $1 \quad 1$ | 0.3 | 2250 feet | 1 | 2 | 2 | 80 | 1 | 13.664 | 79.040 | 79.4 | 13.6 | 0.3003 |
| 6 | 2 |  | 1 | 12 | 0.3 | 2250 feet | 1 | 2 | 1 | 60 | 2 | 19.615 | 55.060 | 55.4 | 19.47 | 0.3000 |
| 6 | 2 |  | 1 | 14 | 0.3 | $21 / 8 \mathrm{mile}$ | 2 | 2 | 1 | 60 | 1 | 17.485 | 61.767 | 62.2 | 17.38 | 0.3004 |
| 6 | 2 |  | 1 | 17 | 0.3 | $21 / 8 \mathrm{mile}$ | 2 | 2 | 2 | 80 | 2 | 13.368 | 80.790 | 82.4 | 13.06 | 0.2991 |
| 6 | 2 |  | 2 | 13 | 0.3 | 2250 feet | 1 | 2 | 1 | 60 | 1 | 18.256 | 59.159 | 59.4 | 18.18 | 0.3001 |
| 6 | 2 |  | 2 | 14 | 0.3 | $21 / 8 \mathrm{mile}$ | 2 | 2 | 1 | 60 | 1 | 17.468 | 61.827 | 61.2 | 17.67 | 0.3005 |
| 6 | 2 |  | 2 | 16 | 0.3 | 2250 feet | 1 | 2 | 2 | 80 | 1 | 12.556 | 86.015 | 86.1 | 12.56 | 0.3005 |
| 6 | 2 |  | 2 | 17 | 0.3 | $21 / 8 \mathrm{mile}$ | 2 | 2 | 2 | 80 | 1 | 13.415 | 80.507 | 81 | 13.28 | 0.2991 |

TABLE I. 10 -- Bridge - Stationary Portion Summary Statistics Upper
VASCAR Nominal Visual 90\% Observed Observed
Method Speed Method $N$ Mean Limit 95\%-tile 99\%-tile MSE Variance $K$

| Bridge Stationary-All | 55 | 0.975 | 1.673 | 2.396 | 3.791 | 0.1246 | 0.691 | 1.976 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Parking | 60 | Direct | 14 | 0.521 | 1.308 | 1.109 | 1.429 | 0.0969 | 0.184 | 2.529 |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Parking | 60 | Indirect | 13 | 0.717 | 1.713 | 1.259 | 1.973 | 0.1481 | 0.224 | 2.587 |
| Parking | 80 | Direct | 14 | 1.288 | 2.094 | 3.715 | 3.993 | 0.1017 | 1.419 | 2.529 |
| Parking | 80 | Indirect | 14 | 1.355 | 2.349 | 2.406 | 2.994 | 0.1545 | 0.494 | 2.529 |

## Bridge Study - Stationary Portion

A. Variables

Subject Number
Visual Mode
Nominal Speed
B. Significant Effects

Subject Number - see summary of experiment
Nominal Speed

| Nominal <br> Speed | Mean <br> Error |
| :---: | :---: |
| 60 | .616 |
| 80 | 1.322 |

Subject Number x Visual Mode
Subject Number x Nominal Speed
Subject Number x Visual Mode x Nominal Speed

## TABLE I. 11 -- Raw Data for the Stationary Portion of the Bridge Study

| SubNum | Sessnum | RepNum | Repeat\#TrialNo | Crsoist | Crsoistr | Vismode $V$ | VisModeR | Reftype | NomSpd | DesrdSpd | NoRepeat | Truetime | Truespd | VASspeed | VASt ime |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2 | 1 | 12 | 0.3 | 2 | 2 Indirect | $t 2$ | 2 | 1 | 60 | 1 | 18.573 | 58.149 | 60.3 | 17.89 |
| 1 | 2 | 1 | 22 | 0.3 | 2 | 2 Indirect | 2 | 2 | 1 | 60 | 1 | 18.174 | 59.426 | 60.2 | 17.92 |
| 1 | 2 | 1 | 13 | 0.3 | 2 | 2 Indirect | 2 | 2 | 2 | 80 | 1 | 13.242 | 81.559 | 84.7 | 12.74 |
| 1 | 2 | 1 | 23 | 0.3 |  | 2 Indirect | 2 | 2 | 2 | 80 | 1 | 13.333 | 81.002 | 83.1 | 12.99 |
| 1 | 2 | 1 | 15 | 0.3 |  | 2 Direct | 1 | 2 | 2 | 80 | 1 | 13.278 | 81.338 | 85.4 | 12.63 |
| 1 | 2 | 1 | 25 | 0.3 | 2 | 2 Direct | 1 | 2 | 2 | 80 | 1 | 13.198 | 81.831 | 85.4 | 12.63 |
| 1 | 2 | 1 | 18 | 0.3 | 2 | 2 Direct | 1 | 2 | 1 | 60 | 2 | 18.089 | 59.705 | 60.3 | 17.89 |
| 1 | 2 | 1 | 28 | 0.3 | 2 | 2 Direct | 1 | 2 | 1 | 60 | 1 | 18.063 | 59.791 | 61.3 | 17.6 |
| 2 | 2 | 1 | $1 \quad 1$ | 0.3 |  | 2 Direct | 1 | 2 | 2 | 80 | 1 | 13.119 | 82.323 | 82.8 | 13.03 |
| 2 | 2 | 1 | 21 | 0.3 | 2 | 2 Direct | 1 | 2 | 2 | 80 | 1 | 13.256 | 81.473 | 82.8 | 13.03 |
| 2 | 2 | 1 | 14 | 0.3 | 2 | 2 Direct | 1 | 2 | 1 | 60 | 1 | 18.305 | 59.000 | 59.2 | 18.14 |
| 2 | 2 | 1 | 24 | 0.3 |  | 2 Direct | 1 | 2 | 1 | 60 | 1 | 18.311 | 58.981 | 59.5 | 18.03 |
| 2 | 2 | 1 | 16 | 0.3 |  | 2 Indirect | $t 2$ | 2 | 1 | 60 | 1 | 18.197 | 59.350 | 60.1 | 17.96 |
| 2 | 2 | 1 | 26 | 0.3 |  | 2 Indirect | $t 2$ | 2 | 1 | 60 | 1 | 18.116 | 59.616 | 60.4 | 17.85 |
| 2 | 2 | 1 | 17 | 0.3 | 2 | 2 Indirect | $t 2$ | 2 | 2 | 80 | 1 | 13.285 | 81.295 | 82.4 | 13.1 |
| 2 | 2 | 1 | 27 | 0.3 |  | 2 Indirect | $t 2$ | 2 | 2 | 80 | 3 | 13.214 | 81.731 | 83.1 | 12.99 |
| 3 | 2 | 1 | 12 | 0.3 |  | 2 Direct | 1 | 2 | 2 | 80 | 1 | 13.411 | 80.531 | 80.8 | 13.35 |
| 3 | 2 | 1 | 15 | 0.3 |  | 2 Indirect | $t 2$ | 2 | 2 | 80 | 1 | 13.387 | 80.675 | 81.7 | 13.21 |
| 3 | 2 | 1 | 16 | 0.3 |  | 2 Indirect | $t \quad 2$ | 2 | 1 | 60 | 1 | 18.101 | 59.665 | 59.8 | 18.03 |
| 3 | 2 | 1 | 17 | 0.3 |  | 2 Direct | 1 | 2 | 1 | 60 | 1 | 18.019 | 59.937 | 60.3 | 17.89 |
| 3 | 2 | 2 | 12 | 0.3 |  | 2 Indirect | $t 2$ | 2 | 2 | 80 | 1 | 13.371 | 80.772 | 81.7 | 13.21 |
| 3 | 2 | 2 | 14 | 0.3 |  | 2 Direct | 1 | 2 | 2 | 80 | 1 | 13.325 | 81.051 | 81.7 | 13.21 |
| 3 | 2 | 2 | 17 | 0.3 |  | 2 Indirect | $t 2$ | 2 | 1 | 60 | 1 | 18.229 | 59.246 | 59.7 | 18.07 |
| 3 | 2 | 2 | 18 | 0.3 |  | 2 Direct | 1 | 2 | 1 | 60 | 3 | 18.194 | 59.360 | 59.6 | 18.1 |
| 3 | 2 | 3 | 11 | 0.3 |  | 2 Direct | 1 | 2 | 1 | 60 | 1 | 17.885 | 60.386 | 61.2 | 17.64 |
| 3 | 2 | 3 | 13 | 0.3 |  | 2 Indirect | $t \quad 2$ | 2 | 2 | 80 | 1 | 13.484 | 80.095 | 80.6 | 13.39 |
| 3 | 2 | 3 | 15 | 0.3 |  | 2 Indirect | $t 2$ | 2 | 1 | 60 |  | 18 | 60.000 | 60.2 | 17.92 |
| 3 | 2 | 3 | 18 | 0.3 |  | 2 Oirect | 1 | 2 | 2 | 80 | 9 | 13.337 | 80.978 | 81 | 13.32 |


| SubNum | Sessnum | RepNum | Repeat\#TrialNo | CrsDist | CrsDistR | VisMode | VisModer | Reftype | NomSpd | DesrdSpd | NoRepeat | TrueTime | Truespd | VASspeed | VAStime |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4 | 2 | 1 | 11 | 0.3 | 2 | Direct | 1 | 2 | 2 | 80 | 2 | 13.448 | 80.309 | 80.8 | 13.35 |
| 4 | 2 | 1 | 13 | 0.3 | 2 | Indirect | 2 | 2 | 1 | 60 | 1 | 18.086 | 59.715 | 60.6 | 17.82 |
| 4 | 2 | 1 | 14 | 0.3 | 2 | Indirect | - 2 | 2 | 2 | 80 | 1 | 13.422 | 80.465 | 81.9 | 13.17 |
| 4 | 2 | 1 | 18 | 0.3 | 2 | Direct | 1 | 2 | 1 | 60 | 1 | 18.238 | 59.217 | 59 | 18.28 |
| 4 | 2 | 2 | 11 | 0.3 | 2 | Indirect | - 2 | 2 | 1 | 60 | 1 | 17.86 | 60.470 | 53.3 | 20.23 |
| 4 | 2 | 2 | 13 | 0.3 | 2 | Direct | 1 | 2 | 1 | 60 | 2 | 18.161 | 59.468 | 59.7 | 18.07 |
| 4 | 2 | 2 | 15 | 0.3 | 2 | 2 Indirect | $t 2$ | 2 | 2 | 80 | 1 | 13.471 | 80.172 | 81.5 | 13.24 |
| 4 | 2 | 2 | 16 | 0.3 | 2 | Direct | 1 | 2 | 2 | 80 | 3 | 13.433 | 80.399 | 81.3 | 13.28 |
| 4 | 2 | 3 | 12 | 0.3 | 2 | 2 Direct | 1 | 2 | 1 | 60 | 1 | 17.923 | 60.258 | 60.3 | 17.89 |
| 4 | 2 | 3 | 14 | 0.3 | 2 | 2 Indirect | $t 2$ | 2 | 2 | 80 | 1 | 13.555 | 79.675 | 81.5 | 13.24 |
| 4 | 2 | 3 | 16 | 0.3 | 2 | 2 Direct | 1 | 2 | 2 | 80 | 1 | 13.514 | 79.917 | 80.4 | 13.42 |
| 4 | 2 | 3 | 17 | 0.3 | 2 | 2 Indirect | $t \quad 2$ | 2 | 1 | 60 | 1 | 18.207 | 59.318 | 60.2 | 17.92 |
| 5 | 2 | 1 | 11 | 0.3 | 2 | 2 Indirect | $t \quad 2$ | 2 | 2 | 80 | 2 | 13.778 | 78.386 | 73.7 | 13.71 |
| 5 | 2 | 1 | 12 | 0.3 | 2 | 2 Indirect | $t 2$ | 2 | 1 | 60 | 1 | 19.615 | 55.060 | 55.7 | 19.36 |
| 5 | 2 | 1 | 14 | 0.3 | 2 | 2 Direct | 1 | 2 | 1 | 60 | 1 | 17.428 | 61.969 | 62.7 | 17.2 |
| 5 | 2 | 1 | 17 | 0.3 | 2 | 2 Direct | 1 | 2 | 2 | 80 | 9 | 13.324 | 81.057 | 82.8 | 13.03 |
| 5 | 2 | 2 | 13 | 0.3 | 2 | 2 Direct | 1 | 2 | 1 | 60 | 2 | 18.256 | 59.159 | 60.1 | 17.96 |
| 5 | 2 | 2 | 14 | 0.3 | 2 | 2 Indirect | $t 2$ | 2 | 1 | 60 | 1 | 17.468 | 61.827 | 62.5 | 17.28 |
| 5 | 2 | 2 | 16 | 0.3 |  | 2 Direct | 1 | 2 | 2 | 80 | 2 | 12.556 | 86.015 | 87.7 | 12.31 |
| 5 | 2 | 2 | 17 | 0.3 | 2 | 2 Indirect | $t 2$ | 2 | 2 | 80 | 1 | 13.415 | 80.507 | 81.5 | 13.24 |
| 6 | 2 | 1 | 13 | 0.3 | 2 | 2 Direct | 1 | 2 | 2 | 80 | ? | 12.944 | 83.436 | 84.7 | 12.74 |
| 6 | 2 | 1 | 15 | 0.3 | 2 | 2 Direct | 1 | 2 | 1 | 60 | 1 | 18.268 | 59.120 | 59.8 | 18.03 |
| 6 | 2 | 1 | 16 | 0.3 |  | 2 Indirect | $t$ | 2 | 1 | 60 | 1 | 18.281 | 59.078 | 59.7 | 18.07 |
| 6 | 2 | 1 | 18 | 0.3 | 2 | 2 Indirect | t | 2 | 2 | 80 |  | 12.829 | 84.184 | 85.9 | 12.56 |
| 6 | 2 | 2 | 11 | 0.3 | 2 | 2 Indirect | $t \quad 2$ | 2 | 2 | 80 | 1 | 12.933 | 83.507 | 84.7 | 12.74 |
| 6 | 2 | 2 | 12 | 0.3 | 2 | 2 Indirect | $t \quad 2$ | 2 | 1 | 60 | 2 | 17.843 | 60.528 | 60.9 | 17.71 |
| 6 | 2 | 2 | 15 | 0.3 |  | 2 girect | 1 | 2 | 2 | 80 | 1 | 13.617 | 79.313 | 80.4 | 13.42 |
| 6 | 2 | 2 | 18 | 0.3 | 2 | 2 Direct | 1 | 2 | 1 | 60 | 1 | 19.132 | 56.450 | 57.1 | 18.9 |

TABLE I. 12 -- Park - Summary Statistics
Upper
VASCAR Course Nominal $90 \%$ Observed Observed
Method Distance Speed $N$ Mean Limit 95\%-tile 99\%-tile MSE Variance K

| Parked - Overall | 48 | -0.506 | 1.996 | 3.350 | 4.334 | 1.5554 | 6.583 | 2.006 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Parked | 200 ft | 24 | -1.403 | 4.229 | 3.358 | 4.739 | 6.4079 | 9.454 | 2.225 |
| :--- | :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Parked | 528 ft | 24 | 0.391 | 3.875 | 2.706 | 3.264 | 2.4516 | 2.318 | 2.225 |


| Parked | 200 ft | 60 | 12 | -0.522 | 3.909 | 4.061 | 4.947 | 2.7859 | 8.296 | 2.655 |  |
| :--- | :--- | :--- | :--- | :--- | ---: | :--- | :--- | :--- | :--- | :--- | :--- |
| Parked | 200 | ft | 80 | 12 | -2.285 | 8.076 | 1.939 | 3.083 | 15.2304 | 9.777 | 2.655 |
| Parked | 528 | ft | 60 | 12 | 0.123 | 1.955 | 1.378 | 1.740 | 0.4761 | 1.131 | 2.655 |
| Parked | 528 | ft | 80 | 12 | 0.659 | 5.821 | 3.008 | 3.350 | 3.7801 | 3.379 | 2.655 |

A. Variables

Subject Number Replications
Course Distance
Nominal Speed
B. Significant Effects ( $\mathrm{p} \leq 0.05$ )

Subject Number - see summary of experiment
C. Nearly Significant Effects

Course Distance $x$ Nominal Speed ( $p=.07$ )

TABLE I. 13 -- Raw Data for the Park Study

|  | SubNum | SessNum | RepNum | Trialno | CrsDist | CrsDistR | Reftype | NomSpd | DesrdSpd | NoAttempt | $\begin{array}{r} \text { TrueTime } \\ 2.24 \end{array}$ | $\begin{aligned} & \text { TrueSpd } \\ & 60.877 \end{aligned}$ | VASspeed 64.2 | VAStime $2.12$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 3 | 5 | 1 | 2 | 200 | 1 | 5 | 2 | 80 | 1 | 1.677 | 81.314 | 82.3 | 1.65 |
|  | 3 | 5 | 1 | 3 | 528 | 2 | 5 | 2 | 80 | 2 | 4.507 | 79.876 | 82.6 | 4.35 |
|  | 3 | 5 | 1 | 4 | 528 | 2 | 5 | 1 | 60 | 1 | 6.089 | 59.123 | 60.2 | 5.97 |
|  | 3 | 5 | 2 | 1 | 200 | 1 | 5 | 1 | 60 | 2 | 2.296 | 59.392 | 61.1 | 2.23 |
|  | 3 | 5 | 2 | 2 | 200 | 1 | 5 | 2 | 80 | 3 | 1.687 | 80.832 | 84.2 | 1.62 |
|  | 3 | 5 | 2 | 3 | 528 | 2 | 5 | 2 | 80 | 1 | 4.392 | 81.967 | 85.4 | 4.21 |
|  | 3 | 5 | 2 | 4 | 528 | 2 | 5 | 1 | 60 | 1 | 6.109 | 58.929 | 59.8 | 6.01 |
|  | 3 | 5 | 3 | 1 | 528 | 2 | 5 | 2 | 80 | 2 | 4.487 | 80.232 | 79.3 | 4.53 |
|  | 3 | 5 | 3 | 2 | 528 | 2 | 5 | 1 | 60 | 1 | 6.013 | 59.870 | 61.7 | 5.83 |
|  | 3 | 5 | 3 | 3 | 200 | 1 | 5 | 2 | 80 | 2 | 1.669 | 81.704 | 75.8 | 1.8 |
|  | 3 | 5 | 3 | 4 | 200 | 1 | 5 | 1 | 60 | 2 | 2.31 | 59.032 | 64.2 | 2.12 |
|  | 4 | 5 | 1 | 1 | 528 | 2 | 5 | 1 | 60 | 1 | 5.926 | 60.749 | 60.6 | 5.94 |
|  | 4 | 5 | 1 | 2 | 528 | 2 | 5 | 2 | 80 | 1 | 4.425 | 81.356 | 81.9 | 4.39 |
|  | 4 | 5 | 1 | 3 | 200 | 1 | 5 | 2 | 80 | 1 | 1.682 | 81.072 | 74.3 | 1.83 |
|  | 4 | 5 | 1 | 4 | 200 | 1 | 5 | 1 | 60 | 1 | 2.304 | 59.186 | 57.4 | 2.37 |
|  | 4 | 5 | 2 | 1 | 528 | 2 | 5 | 1 | 60 | 1 | 6.107 | 58.949 | 59.8 | 6.01 |
|  | 4 | 5 | 2 | 2 | 528 | 2 | 5 | 2 | 80 | 1 | 4.39 | 82.005 | 81.9 | 4.39 |
|  | 4 | 5 | 2 | 3 | 200 | 1 | 5 | 2 | 80 | 1 | 1.665 | 81.900 | 80.6 | 1.69 |
|  | 4 | 5 | 2 | 4 | 200 | 1 | 5 | 1 | 60 | 1 | 2.317 | 58.854 | 56.5 | 2.41 |
|  | 4 | 5 | 3 | 1 | 200 | 1 | 5 | 2 | 80 | 1 | 1.682 | 81.072 | 80.6 | 1.69 |
|  | 4 | 5 | 3 | 2 | 200 | 1 | 5 | 1 | 60 | 1 | 2.279 | 59.835 | 60.1 | 2.26 |
| H | 4 | 5 | 3 | 3 | 528 | 2 | 5 | 2 | 80 | 1 | 4.467 | 80.591 | 81.9 | 4.39 |
| 心 | 4 | 5 | 3 | 4 | 528 | 2 | 5 | 1 | 60 | 2 | 6.057 | 59.435 | 59.1 | 6.08 |
|  | 5 | 5 | 1 | 1 | 528 | 2 | 5 | 1 | 60 | 1 | 5.982 | 60.181 | 59.8 | 6.01 |
|  | 5 | 5 | 1 | 2 | 528 | 2 | 5 | 2 | 80 | 1 | 4.407 | 81.688 | 80.6 | 4.46 |
|  | 5 | 5 | 1 | 3 | 200 | 1 | 5 | 2 | 80 | 1 | 1.679 | 81.217 | 74.3 | 1.83 |
|  | 5 | 5 | 1 | 4 | 200 | 1 | 5 | 1 | 60 | 1 | 2.313 | 58.955 | 54.9 | 2.48 |
|  | 5 | 5 | 2 | 21 | 528 | 2 | 5 | 2 | 80 | 1 | 4.599 | 78.278 | 76.9 | 4.68 |
|  | 5 | 5 | 2 | 22 | 528 | 2 | 5 | 1 | 60 | 1 | 6.388 | 56.356 | 54 | 6.66 |
|  | 5 | 5 | 2 | 23 | 200 | 1 | 5 | 2 | 80 | 1 | 1.663 | 81.999 | 80.6 | 1.69 |
|  | 5 | 5 | 2 | 24 | 200 | 1 | 5 | 1 | 60 | 1 | 2.45 | 55.659 | 55.7 | 2.44 |
|  | 5 | 5 | 3 | 31 | 200 | 1 | 5 | 2 | 80 | 1 | 1.661 | 82.097 | 80.6 | 1.69 |
|  | 5 | 5 | 3 | 32 | 200 | 1 | 5 | 1 | 60 | 1 | 2.445 | 55.772 | 51.2 | 2.66 |
|  | 5 | 5 | 3 | 3 | 528 | 2 | 5 | 1 | 60 | 1 | 6.433 | 55.961 | 54.6 | 6.58 |
|  | 5 | 5 | 3 | 34 | 528 | 2 | 5 | 2 | 80 | 1 | 4.762 | 75.598 | 75.7 | 4.75 |
|  | 6 | 5 | 1 | 11 | 200 | 1 | 5 | 1 | 60 | 1 | 2.265 | 60.205 | 60.1 | 2.26 |
|  | 6 | 5 | 1 | 12 | 200 | - 1 | 5 | 2 | 80 | 1 | 1.679 | 81.217 | 78.9 | 1.72 |
|  | 6 | 5 |  | 13 | 528 | 2 | 5 | 2 | 80 | 2 | 4.433 | 81.209 | 79.3 | 4.53 |
|  | 6 | 5 | 1 | 14 | 528 | 2 | 5 | 1 | 60 | 1 | 6.106 | 58.958 | 59.8 | 6.01 |
|  | 6 | 5 | 2 | 21 | 200 | 1 | 5 | 2 | 80 | 9 | 1.74 | 78.370 | 74.3 | 1.83 |
|  | 6 | 6 | 2 | 22 | 200 | 1 | 5 | 1 | 60 | 1 | 2.423 | 56.279 | 54.1 | 2.52 |
|  | 6 | 5 | 2 | 23 | 528 | 3 | 5 | 2 | 80 | 1 | 4.383 | 82.136 | 84.7 | 4.24 |
|  | 6 | - 5 |  | 24 | 528 | - 2 | 5 | 1 | 60 | 1 | 6.472 | 55.624 | 56.1 | 6.4 |
|  | 6 | 6 |  | 31 | 528 | 3 | 5 | 2 | 80 | 1 | 4.387 | 82.061 | 84.7 | 4.24 |
|  | 6 | 65 |  | 32 | 228 | 2 | 5 | 1 | 60 | 1 | 6.465 | 55.684 | 55.8 | 6.44 |
|  | 6 | 65 |  | 3 3 | 3200 | 1 | 5 | 1 | 60 | 1 | 2.443 | 55.818 | 54.1 | 2.52 |
|  | 6 | 65 | 3 | 34 | 200 | - 1 | 5 | 2 | 80 | 1 | 1.808 | 75.422 | 74.3 | 1.83 |

View Eleva- Course Nom. 90\% Observed Observed
Dist. tion Dist. Speed $N$ Mean Limit 95\%-tile 99\%-tile MSE Variance K

| Angular - Overall | 576 | 0.738 | 3.906 | 4.650 | 7.332 | 3.3501 | 3.967 | 1.731 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| 200 | 288 | 1.787 | 3.775 | 6.230 | 7.954 | 1.2617 | 5.227 | 1.770 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 528 | 288 | -0.311 | 0.853 | 0.667 | 1.209 | 0.4326 | 0.511 | 1.770 |


| 200 | 45 | 96 | 1.134 | 3.142 | 3.742 | 4.178 | 1.1403 | 2.250 | 1.880 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 200 | 60 | 96 | 1.904 | 4.600 | 4.925 | 5.955 | 2.0566 | 3.885 | 1.880 |
| 200 | 80 | 96 | 2.323 | 6.586 | 7.376 | 8.333 | 5.1401 | 8.922 | 1.880 |
| 528 | 45 | 96 | -0.064 | 0.683 | 0.600 | 1.076 | 0.1578 | 0.170 | 1.880 |
| 528 | 60 | 96 | -0.169 | 0.756 | 0.677 | 0.938 | 0.2419 | 0.305 | 1.880 |
| 528 | 80 | 96 | -0.700 | 0.798 | 0.730 | 1.264 | 0.6353 | 0.835 | 1.880 |

200 Ground 200 200 Elevated 200 528 Ground 200 528 Elevated 200 200 Ground 200 200 Elevated 200 528 Ground 200 528 Elevated 200 200 Ground 200 200 Elevated 200 528 Ground 200 528 Elevated 200 200 Ground 528 200 Elevated 528 528 Ground 528 528 Elevated 528 200 Ground 528 200 Elevated 528 528 Ground 528 528 Elevated 528 200 Ground 528 200 Elevated 528 528 Ground 528 528 Elevated 528

| 45 | 24 | 1.805 | 4.186 | 3.982 | 4.148 | 1.1458 | 2.465 | 2.225 |
| :--- | :--- | ---: | :--- | :--- | :--- | :--- | :--- | :--- |
| 45 | 24 | 1.346 | 4.685 | 4.035 | 4.563 | 2.2516 | 3.538 | 2.225 |
| 45 | 24 | 1.002 | 2.823 | 2.634 | 2.944 | 0.6718 | 1.128 | 2.225 |
| 45 | 24 | 1.019 | 2.681 | 1.678 | 1.790 | 0.5585 | 1.038 | 2.225 |
| 60 | 24 | 2.768 | 5.850 | 5.672 | 6.792 | 1.9185 | 5.211 | 2.225 |
| 60 | 24 | 1.782 | 5.941 | 4.748 | 5.682 | 3.4932 | 5.502 | 2.225 |
| 60 | 24 | 1.277 | 3.784 | 3.550 | 4.736 | 1.2698 | 2.469 | 2.225 |
| 60 | 24 | 1.790 | 4.082 | 3.636 | 4.629 | 1.0609 | 1.646 | 2.225 |
| 80 | 24 | 3.260 | 8.692 | 7.981 | 9.652 | 5.9597 | 10.460 | 2.225 |
| 80 | 24 | 2.591 | 8.482 | 7.768 | 8.243 | 7.0091 | 13.165 | 2.225 |
| 80 | 24 | 1.646 | 4.532 | 4.637 | 5.182 | 1.6819 | 4.664 | 2.225 |
| 80 | 24 | 1.796 | 7.399 | 6.721 | 7.492 | 6.3419 | 6.806 | 2.225 |
| 45 | 24 | -0.123 | 0.872 | 0.593 | 0.790 | 0.2401 | 0.239 | 2.225 |
| 45 | 24 | -0.127 | 0.715 | 0.529 | 0.980 | 0.1433 | 0.204 | 2.225 |
| 45 | 24 | -0.030 | 0.872 | 0.560 | 0.959 | 0.1433 | 0.143 | 2.225 |
| 45 | 24 | -0.035 | 0.478 | 0.513 | 0.733 | 0.0531 | 0.097 | 2.225 |
| 60 | 24 | -0.130 | 0.871 | 0.590 | 0.689 | 0.2023 | 0.194 | 2.225 |
| 60 | 24 | -0.243 | 0.992 | 0.840 | 1.682 | 0.3081 | 0.459 | 2.225 |
| 60 | 24 | -0.167 | 1.056 | 0.744 | 0.896 | 0.3023 | 0.356 | 2.225 |
| 60 | 24 | -0.136 | 0.943 | 0.425 | 0.567 | 0.2351 | 0.241 | 2.225 |
| 80 | 24 | -0.881 | 1.318 | 1.035 | 1.319 | 0.9766 | 1.135 | 2.225 |
| 80 | 24 | -0.834 | 0.819 | 0.310 | 0.525 | 0.5520 | 0.597 | 2.225 |
| 80 | 24 | -0.437 | 1.419 | 0.512 | 1.090 | 0.5879 | 0.696 | 2.225 |
| 80 | 24 | -0.649 | 0.839 | 0.930 | 1.119 | 0.4472 | 0.895 | 2.225 |

A. Variables

Group
Subjects
Replicates
Course Distance
Nominal. Speed
Viewing Distance
Elevation
B. Significant Effects ( $\mathrm{p} \leq 0.05$ )

Subject Number
Viewing Distance
Course Distance
Group x Viewing Distance
Group x Course Distance
Viewing Distance $x$ Course Distance
Course Distance x Nominal Speed
Group x Viewing Distance x Course Distance
C. Nearly Significant Effects

Viewing Distance x Elevation x Course Distance ( $\mathrm{p}=0.08$ )
A. Significant Effects for 200 Foot Course Distance

Subject Number - see summary of experiment
Replications

| Repl icate <br> Number | Mean Speed <br> Error |
| :---: | :---: |
| 1 | 2.119 |
| 2 | 1.883 |
| 3 | 2.042 |
| 4 | 1.104 |

Viewing Distance

| Viewing <br> Distance | Mean Speed <br> Error |
| :---: | :---: |
| 200 ft | 2.258 |
| 528 ft | 1.316 |

Group x Viewing Distance

| Viewing <br> Distance | Mean Speed Error |  |
| :---: | :---: | :---: |
|  | Group 1 | Group 2 |
| 200 ft | .406 | 3.185 |
| 528 ft | .475 | 1.736 |

Nominal Speed

| Nominal <br> Speed | Mean Speed <br> Error |
| :---: | :---: |
| 45 | 1.134 |
| 60 | 1.904 |
| 80 | 2.323 |

B. Significant Effects for 528 Foot Course Distance

Subject Number - see summary of experiment
Viewing Distance

| Viewing <br> Distance | Mean Speed <br> Error |
| :---: | :---: |
| 200 ft | -0.390 |
| 528 ft | -0.233 |

Nominal Speed

| Nominal <br> Speed | Mean Speed <br> Error |
| :---: | :---: |
| 45 | -0.064 |
| 60 | -0.169 |
| 80 | -0.700 |

Group x Viewing Distance x Elevation

| Viewing <br> Distance | Mean Speed Error |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Group 1 |  | Group 2 |  |
|  | ground | elevated | ground | elevated |
| 200 ft | -0.510 | -0.116 | -0.312 | -0.230 |
| 528 ft | -0.355 | -0.488 | -0.424 | -0.166 |


| SubNum | SessNum | RepNum | TrialNo | CrsDist | CrsDistR | Reftype | NomSpd | DesrdSpd | Elevatn | Viewdist | NoAttempt | Truetime | TrueSpd | VASspeed | VAStime |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | 3 | 1 | 1 | 200 | 1 | 3 | 1 | 45 | 2 | 1 | 1 | 2.962 | 46.038 | 46.2 | 2.95 |
| 3 | 3 | 1 | 2 | 200 | 1 | 3 | 3 | 80 | 2 | 1 | 2 | 1.701 | 80.167 | 78.9 | 1.72 |
| 3 | 3 | 1 | 3 | 200 | 1 | 3 | 2 | 60 | 2 | 1 | 1 | 2.278 | 59.861 | 58.3 | 2.34 |
| 3 | 3 | 1 | 4 | 528 | 2 | 3 | 2 | 60 | 2 | 1 | 2 | 6.049 | 59.514 | 59.1 | 6.08 |
| 3 | 3 | 1 | 5 | 528 | 2 | 3 | 3 | 80 | 2 | 1 | 1 | 4.458 | 80.754 | 80.6 | 4.46 |
| 3 | 3 | 1 | 6 | 528 | 2 | 3 | 1 | 45 | 2 | 1 | 1 | 7.948 | 45.294 | 45.2 | 7.95 |
| 3 | 3 | 1 | 7 | 528 | 2 | 3 | 3 | 80 | 1 | 1 | 1 | 4.475 | 80.447 | 79.3 | 4.53 |
| 3 | 3 | 1 | 8 | 528 | 2 | 3 | 2 | 60 | 1 | 1 | 1 | 6.156 | 58.480 | 59.1 | 6.08 |
| 3 | 3 | 1 | 9 | 528 | 2 | 3 | 1 | 45 | 1 | 1 | 1 | 7.793 | 46.195 | 46.5 | 7.74 |
| 3 | 3 | 1 | 10 | 200 | 1 | 3 | 1 | 45 | 1 | 1 | 2 | 2.997 | 45.500 | 44 | 3.09 |
| 3 | 3 | 1 | 11 | 200 | 1 | 3 | 3 | 80 | 1 | 1 | 1 | 1.69 | 80.689 | 82.3 | 1.65 |
| 3 | 3 | 1 | 12 | 200 | 1 | 3 | 2 | 60 | 1 | 1 | 1 | 2.341 | 58.250 | 55.7 | 2.44 |
| 3 | 3 | 1 | 13 | 528 | 2 | 3 | 2 | 60 | 1 | 2 | 2 | 6.047 | 59.534 | 59.1 | 6.08 |
| 3 | 3 | 1 | 14 | 528 | 2 | 3 | 1 | 45 | 1 | 2 | 1 | 7.753 | 46.434 | 46.5 | 7.74 |
| 3 | 3 | 1 | 15 | 528 | 2 | 3 | 3 | 80 | 1 | 2 | 1 | 4.485 | 80.268 | 80 | 4.5 |
| 3 | 3 | 1 | 16 | 200 | 1 | 3 | 1 | 45 | 1 | 2 | 1 | 2.969 | 45.929 | 45.1 | 3.02 |
| 3 | 3 | 1 | 17 | 200 | 1 | 3 | 3 | 80 | 1 | 2 | 2 | 1.691 | 80.641 | 82.3 | 1.65 |
| 3 | 3 | 1 | 18 | 200 | 1 | 3 | 2 | 60 | 1 | 2 | 1 | 2.282 | 59.756 | 59.2 | 2.3 |
| 3 | 3 | 1 | 19 | 528 | 2 | 3 | 1 | 45 | 2 | 2 | 1 | 7.883 | 45.668 | 45.4 | 7.92 |
| 3 | 3 | 1 | 20 | 528 | 2 | 3 | 3 | 80 | 2 | 2 | 1 | 4.496 | 80.071 | 79.3 | 4.53 |
| 3 | 3 | 1 | 21 | 528 | 2 | 3 | 2 | 60 | 2 | 2 | 1 | 6.059 | 59.416 | 59.5 | 6.04 |
| 3 | 3 | 1 | 22 | 200 | 1 | 3 | 1 | 45 | 2 | 2 | 1 | 2.947 | 46.272 | 46.7 | 2.91 |
| 3 | 3 | 1 | 23 | 200 | 1 | 3 | 3 | 80 | 2 | 2 | 1 | 1.71 | 79.745 | 82.3 | 1.65 |
| 3 | 3 | 1 | 24 | 200 | 1 | 3 | 2 | 60 | 2 | 2 | 1 | 2.291 | 59.521 | 59.2 | 2.3 |
| 3 | 3 | 2 | 1 | 528 | 2 | 3 | 1 | 45 | 1 | 2 | 1 | 7.822 | 46.024 | 46 | 7.81 |
| 3 | 3 | 2 | 2 | 528 | 2 | 3 | 3 | 80 | 1 | 2 | 1 | 4.513 | 79.770 | 79.3 | 4.53 |
| 3 | 3 | 2 | 3 | 528 | 2 | 3 | 2 | 60 | 1 | 2 | 1 | 6.063 | 59.377 | 59.8 | 6.01 |
| 3 | 3 | 2 | 4 | 200 | 1 | 3 | 2 | 60 | 1 | 2 | 2 | 2.293 | 59.470 | 60.1 | 2.26 |
| 3 | 3 | 2 | 5 | 200 | 1 | 3 | 1 | 45 | 1 | 2 | 1 | 2.98 | 45.760 | 47.3 | 2.88 |
| 3 | 3 | 2 | 6 | 200 | 1 | 3 | 3 | 80 | 1 | 2 | 1 | 1.688 | 80.784 | 84.2 | 1.62 |
| 3 | 3 | 2 | 7 | 528 | 2 | 3 | 1 | 45 | 2 | 2 | 2 | 7.882 | 45.674 | 45.6 | 7.88 |
| 3 | 3 | 2 | 8 | 528 | 2 | 3 | 3 | 80 | 2 | 2 | 1 | 4.498 | 80.036 | 78.7 | 4.57 |
| 3 | 3 | 2 | 9 | 528 | 2 | 3 | 2 | 60 | 2 | 2 | 3 | 6.135 | 58.680 | 58.4 | 6.15 |
| 3 | 3 | 2 | 10 | 200 | 1 | 3 | 3 | 80 | 2 | 2 | 2 | 1.708 | 79.838 | 82.3 | 1.65 |
| 3 | 3 | 2 | 11 | 200 | 1 | 3 | 2 | 60 | 2 | 2 | 1 | 2.311 | 59.006 | 60.1 | 2.26 |
| 3 | 3 | 2 | 12 | 200 | 1 | 3 | 1 | 45 | 2 | 2 | 2 | 2.974 | 45.852 | 47.3 | 2.88 |
| 3 | 3 | 2 | 13 | 200 | 1 | 3 | 2 | 60 | 1 | 1 | 1 | 2.359 | 57.806 | 59.2 | 2.3 |
| 3 | 3 | 2 | 14 | 200 | 1 | 3 | 1 | 45 | 1 | 1 | 1 | 2.933 | 46.493 | 45.1 | 3.02 |
| 3 | 3 | 2 | 15 | 200 | 1 | 3 | 3 | 80 | 1 | 1 | 1 | 1.735 | 78.596 | 78.9 | 1.72 |
| 3 | 3 | 2 | 16 | 528 | 2 | 3 | 2 | 60 | 1 | 1 | 2 | 6.064 | 59.367 | 59.5 | 6.04 |
| 3 | 3 | 2 | 17 | 528 | 2 | 3 | 3 | 80 | 1 | 1 | 1 | 4.482 | 80.321 | 80 | 4.5 |
| 3 | 3 | 2 | 18 | 528 | 2 | 3 | 1 | 45 | 1 | 1 | 1 | 7.768 | 46.344 | 46 | 7.81 |
| 3 | 3 | 2 | 19 | 528 | 2 | 3 | 3 | 80 | 2 | 1 | 1 | 4.482 | 80.321 | 79.3 | 4.53 |
| 3 | 3 | 2 | 20 | 528 | 2 | 3 | 2 | 60 | 2 | 1 | 2 | 6.064 | 59.367 | 58.8 | 6.12 |
| 3 | 3 | 2 | 21 | 528 | 2 | 3 | 1 | 45 | 2 | 1 | 1 | 7.929 | 45.403 | 45.2 | 7.95 |
| 3 | 3 | 2 | 22 | 200 | 1 | 3 | 1 | 45 | 2 | 1 | 2 | 3.003 | 45.409 | 45.6 | 2.98 |
| 3 | 3 | 2 | 23 | 200 | 1 | 3 | 3 | 80 | 2 | 1 | 2 | 1.691 | 80.641 | 80.6 | 1.69 |
| 3 | 3 | 2 | 24 | 200 | 1 | 3 | 2 | 60 | 2 | 1 | 1 | 2.311 | 59.006 | 60.1 | 2.26 |

TABLE 1. 15 -- Rau Data For Angular Study (Continued)

| SubNum SessNum |  |
| ---: | ---: |
| 3 | 3 |
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| 3 | 3 |
| 3 | 3 |
| 3 | 3 |


| RepNum | TrialNo | Crsoist | CrsDistR |
| :---: | :---: | :---: | :---: |
| 3 | 1 | 200 | 1 |
| 3 | 2 | 200 | 1 |
| 3 | 3 | 200 | 1 |
| 3 | 4 | 528 | 2 |
| 3 | 5 | 528 | 2 |
| 3 | 6 | 528 | 2 |
| 3 | 7 | 528 | 2 |
| 3 | 8 | 528 | 2 |
| 3 | 9 | 528 | 2 |
| 3 | 10 | 200 | 1 |
| 3 | 11 | 200 | 1 |
| 3 | 12 | 200 | 1 |
| 3 | 13 | 200 | 1 |
| 3 | 14 | 200 | 1 |
| 3 | 15 | 200 | 1 |
| 3 | 16 | 528 | 2 |
| 3 | 17 | 528 | 2 |
| 3 | 18 | 528 | 2 |
| 3 | 19 | 200 | 1 |
| 3 | 20 | 200 | 1 |
| 3 | 21 | 200 | 1 |
| 3 | 22 | 528 | 2 |
| 3 | 23 | 528 | 2 |
| 3 | 24 | 528 | 2 |
| 4 | 1 | 528 | 2 |
| 4 | 2 | 528 | 2 |
| 4 | 3 | 528 | 2 |
| 4 | 4 | 200 | 1 |
| 4 | 5 | 200 | 1 |
| 4 | 6 | 200 | 1 |
| 4 | 7 | 200 | 1 |
| 4 | 8 | 200 | 1 |
| 4 | 9 | 200 | 1 |
| 4 | 10 | 528 | - 2 |
| 4 | 11 | 528 | - 2 |
| 4 | 12 | 528 | - 2 |
| 4 | 13 | 528 | - 2 |
| 4 | 14 | 528 | - 2 |
| 4 | 15 | 528 | - 2 |
| 4 | 16 | 290 | - 1 |
| 4 | 17 | 200 | -1 |
| 4 | 18 | 200 | - 1 |
| 4 | 19 | 528 | - 2 |
| 4 | 20 | 528 | - 2 |
| 4 | 21 | 528 | - 2 |
| 4 | 22 | 200 | - 1 |
| 4 | 23 | 200 | - 1 |
| 4 | 24 | 200 | - 1 |



Elevatn ViewDist NoAttempt
TrueTim
TrueSpd VASspeed
Vastime
2.98
1.699
2.29
7.839
6.028
4.509
4.487
6.058
7.821
2.297
1.702
2.936
2.908
1.705
2.311
5.915
4.481
7.821
1.68
2.267
2.951
6.084
7.709
4.455
7.784
6.034
4.478
2.952
2.338
1.689
1.69
2.964
2.302
7.796
6.132
4.477
6.013
4.518
7.79
1.691
3.034
2.276
4.475
7.839
6.023
2.303
2.999
1.689
145.760
80.261
59.547
45.924
59.721
79.840
80.232
59.426
46.030
59.366
80.120
46.445
46.893
79.979
59.006
60.862
80.339
46.030
81.169
60.152
46.209
59.172
46.699
80.808
46.249
59.662
80.393
46.194
58.325
80.736
80.689
46.007
59.237
46.178
58.708
80.411
59.870
79.681
46.213
80.641
44.945
59.914
80.447
45.924
59.771
59.211
45.470
80.736
45.1
78.9
61.1
45.6
59.5
79.3
79.3
59.5
46
59.2
80.6
46.7
46.7
80.6
60.1
60.2
79.3
46.2
80.6
59.2
46.7
58.8
46.9
80
46
59.5
80
46.2
59.2
78.9
78.9
45.6
59.2
45.4
58.4
79.3
59.1
80
45.6
80.6
45.1
59.2
78.7
59.5
59.2
45.6
82.3
3.02
1.72
2.23
7.88
6.04
4.53
4.53
6.04
7.81
2.3
1.69
2.91
2.91
1.69
2.26
5.97
4.53
7.77
1.69
2.3
2.91
6.12
7.66
4.5
7.81
6.04
4.5
2.95
2.3

| SubNum <br> 4 | SessNum <br> 3 | RepNum | TrialNo 1 | Crsoist 200 | CrsDistR | Reftype | Nomspd | DesrdSpod | Elevatn | ViewDist | NoAttempt | TrueT ime 2.962 | TrueSpd 46.038 | VASspeed 46.7 | VAStime 2.91 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4 | 3 | 1 | 2 | 200 | 1 | 3 | 3 | 80 | 1 | 1 | 2 | 1.701 | 80.167 | 80.6 | 1.69 |
| 4 | 3 | 1 | 3 | 200 | 1 | 3 | 2 | 60 | 1 | 1 | 1 | 2.278 | 59.861 | 60.1 | 2.26 |
| 4 | 3 | 1 | 4 | 528 | 2 | 3 | 2 | 60 | 1 | 1 | 1 | 6.01 | 59.900 | 59.5 | 6.04 |
| 4 | 3 | 1 | 5 | 528 | 2 | 3 | 3 | 80 | 1 | 1 | 2 | 4.469 | 80.555 | 80 | 4.5 |
| 4 | 3 | 1 | 6 | 528 | 2 | 3 | 1 | 45 | 1 | 1 | 1 | 7.948 | 45.294 | 45 | 7.99 |
| 4 | 3 | 1 | 7 | 528 | 2 | 3 | 3 | 80 | 2 | 1 | 1 | 4.475 | 80.447 | 79.3 | 4.53 |
| 4 | 3 | 1 | 8 | 528 | 2 | 3 | 2 | 60 | 2 | 1 | 1 | 6.156 | 58.480 | 58.1 | 6.19 |
| 4 | 3 | 1 | 9 | 528 | 2 | 3 | 1 | 45 | 2 | 1 | 1 | 7.793 | 46.195 | 45.8 | 7.84 |
| 4 | 3 | 1 | 10 | 200 | 1 | 3 | 1 | 45 | 2 | 1 | 1 | 2.971 | 45.898 | 46.2 | 2.95 |
| 4 | 3 | 1 | 11 | 200 | 1 | 3 | 3 | 80 | 2 | 1 | 1 | 1.69 | 80.689 | 82.3 | 1.65 |
| 4 | 3 | 1 | 12 | 200 | 1 | 3 | 2 | 60 | 2 | 1 | 1 | 2.341 | 58.250 | 59.2 | 2.3 |
| 4 | 3 | 1 | 13 | 528 | 2 | 3 | 2 | 60 | 2 | 2 | 2 | 6.047 | 59.534 | 59.1 | 6.08 |
| 4 | 3 | 1 | 14 | 528 | 2 | 3 | 1 | 45 | 2 | 2 | 1 | 7.753 | 46.434 | 46.2 | 7.77 |
| 4 | 3 | 1 | 15 | 528 | 2 | 3 | 3 | 80 | 2 | 2 | 1 | 4.485 | 80.268 | 80 | 4.5 |
| 4 | 3 | 1 | 16 | 200 | 1 | 3 | 1 | 45 | 2 | 2 | 1 | 2.969 | 45.929 | 44.5 | 3.06 |
| 4 | 3 | 1 | 17 | 200 | 1 | 3 | 3 | 80 | 2 | 2 | 2 | 1.691 | 80.641 | 88.1 | 1.54 |
| 4 | 3 | 1 | 18 | 200 | 1 | 3 | 2 | 60 | 2 | 2 | 1 | 2.282 | 59.756 | 59.2 | 2.3 |
| 4 | 3 | 1 | 19 | 528 | 2 | 3 | 1 | 45 | 1 | 2 | 1 | 7.883 | 45.668 | 46 | 7.81 |
| 4 | 3 | 1 | 20 | 528 | 2 | 3 | 3 | 80 | 1 | 2 | 1 | 4.496 | 80.071 | 79.3 | 4.53 |
| 4 | 3 | 1 | 21 | 528 | 2 | 3 | 2 | 60 | 1 | 2 | 1 | 6.059 | 59.416 | 58.4 | 6.15 |
| 4 | 3 | 1 | 22 | 200 | 1 | 3 | 1 | 45 | 1 | 2 | 1 | 2.947 | 46.272 | 46.7 | 2.91 |
| 4 | 3 | 1 | 23 | 200 | 1 | 3 | 3 | 80 | 1 | 2 | 1 | 1.71 | 79.745 | 82.3 | 1.65 |
| 4 | 3 | 1 | 24 | 200 | 1 | 3 | 2 | 60 | 1 | 2 | 1 | 2.291 | 59.521 | 58.3 | 2.34 |
| 4 | 3 | 2 | 1 | 528 | 2 | 3 | 1 | 45 | 2 | 2 | 1 | 7.822 | 46.024 | 45.6 | 7.88 |
| 4 | 3 | 2 | 2 | 528 | 2 | 3 | 3 | 80 | 2 | 2 | 1 | 4.513 | 79.770 | 79.3 | 4.53 |
| 4 | 3 | 2 | 3 | 528 | 2 | 3 | 2 | 60 | 2 | 2 | 1 | 6.063 | 59.377 | 59.1 | 6.08 |
| 4 | 3 | 2 | 4 | 200 | 1 | 3 | 2 | 60 | 2 | 2 | 2 | 2.293 | 59.470 | 61.1 | 2.23 |
| 4 | 3 | 2 | 5 | 200 | 1 | 3 | 1 | 45 | 2 | 2 | 1 | 2.98 | 45.760 | 44.5 | 3.06 |
| 4 | 3 | 2 | 6 | 200 | 1 | 3 | 3 | 80 | 2 | 2 | 1 | 1.688 | 80.784 | 80.6 | 1.69 |
| 4 | 3 | 2 | 7 | 528 | 2 | 3 | 1 | 45 | 1 | 2 | 1 | 7.672 | 46.924 | 48 | 7.48 |
| 4 | 3 | 2 | 8 | 528 | 2 | 3 | 3 | 80 | 1 | 2 | 1 | 4.498 | 80.036 | 81.3 | 4.42 |
| 4 | 3 | 2 | 9 | 528 | 2 | 3 | 2 | 60 | 1 | 2 | 1 | 6.09 | 59.113 | 59.1 | 6.08 |
| 4 | 3 | 2 | 10 | 200 | 1 | 3 | 3 | 80 | 1 | 2 | 2 | 1.691 | 80.641 | 78.9 | 1.72 |
| 4 | 3 | 2 | 11 | 200 | 1 | 3 | 2 | 60 | 1 | 2 | 1 | 2.311 | 59.006 | 60.1 | 2.26 |
| 4 | 3 | 2 | 12 | 200 | 1 | 3 | 1 | 45 | 1 | 2 | 1 | 2.987 | 45.652 | 46.2 | 2.95 |
| 4 | 3 | 2 | 13 | 200 | 1 | 3 | 2 | 60 | 2 | 1 | 2 | 2.338 | 58.325 | 58.3 | 2.34 |
| 4 | 3 | 2 | 14 | 200 | 1 | 3 | 1 | 45 | 2 | 1 | 1 | 2.933 | 46.493 | 46.2 | 2.95 |
| 4 | 3 | 2 | 15 | 200 | 1 | 3 | 3 | 80 | 2 | 1 | 1 | 1.735 | 78.596 | 77.3 | 1.76 |
| 4 | 3 | 2 | 16 | 528 | 2 | 3 | 2 | 60 | 2 | 1 | 1 | 6.078 | 59.230 | 59.1 | 6.08 |
| 4 | 3 | 2 | 17 | 528 | 2 | 3 | 3 | 80 | 2 | 1 | 1 | 4.482 | 80.321 | 79.3 | 4.53 |
| 4 | 3 | 2 | 18 | 528 | 2 | 3 | 1 | 45 | 2 | 1 | 1 | 7.768 | 46.344 | 45.4 | 7.92 |
| 4 | 3 | 2 | 19 | 528 | 2 | 3 | 3 | 80 | 1 | 1 | 1 | 4.482 | 80.321 | 78.1 | 4.6 |
| 4 | 3 | 2 | 20 | 528 | 2 | 3 | 2 | 60 | 1 | 1 | 2 | 6.064 | 59.367 | 59.5 | 6.04 |
| 4 | 3 | 2 | 21 | 528 | 2 | 3 | 1 | 45 | 1 | 1 | 1 | 7.929 | 45.403 | 45.2 | 7.95 |
| 4 | 3 | 2 | 22 | 200 | 1 | 3 | 1 | 45 | 1 | 1 | 1 | 3.003 | 45.409 | 47.9 | 2.84 |
| 4 | 3 | 2 | 23 | 200 | 1 | 3 | 3 | 80 | 1 | 1 | 2 | 1.691 | 80.641 | 80.6 | 1.69 |
| 4 | 3 | 2 | 24 | 200 | 1 | 3 | 2 | 60 | 1 | 1 | 1 | 2.311 | 59.006 | 60.1 | 2.26 |


| SubNum | SessNum | RepNum | TrialNo | CrsDist 200 | CrsDistr | Reftype | NomSpl | DesrdSpd 45 | Elevatn | viewDist | NoAt tempt | Truet ime 2.98 | TrueSpd 45.760 | VASspeed 47.9 | $\begin{array}{r} \text { VAStime } \\ 2.84 \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4 | 3 | 3 | 2 | 200 | 1 | 3 | 3 | 80 | 1 | 2 | 1 | 1.699 | 80.261 | 80.6 | 1.69 |
| 4 | 3 | 3 | 3 | 200 | 1 | 3 | 2 | 60 | 1 | 2 | 1 | 2.332 | 58.475 | 60.1 | 2.26 |
| 4 | 3 | 3 | 4 | 528 | 2 | 3 | 1 | 45 | 1 | 2 | 1 | 7.682 | 46.863 | 46.5 | 7.74 |
| 4 | 3 | 3 | 5 | 528 | 2 | 3 | 2 | 60 | 1 | 2 | 1 | 6.148 | 58.556 | 59.1 | 6.08 |
| 4 | 3 | 3 | 6 | 528 | 2 | 3 | 3 | 80 | 1 | 2 | 1 | 4.509 | 79.840 | 80 | 4.5 |
| 4 | 3 | 3 | 7 | 528 | 2 | 3 | 3 | 80 | 2 | 2 | 1 | 4.487 | 80.232 | 78.7 | 4.57 |
| 4 | 3 | 3 | 8 | 528 | 2 | 3 | 2 | 60 | 2 | 2 | 1 | 6.058 | 59.426 | 59.1 | 6.08 |
| 4 | 3 | 3 | 9 | 528 | 2 | 3 | 1 | 45 | 2 | 2 | 1 | 7.821 | 46.030 | 46 | 7.81 |
| 4 | 3 | 3 | 10 | 200 | 1 | 3 | 2 | 60 | 2 | 2 | 2 | 2.283 | 59.730 | 60.1 | 2.26 |
| 4 | 3 | 3 | 11 | 200 | 1 | 3 | 3 | 80 | 2 | 2 | 1 | 1.702 | 80.120 | 78.9 | 1.72 |
| 4 | 3 | 3 | 12 | 200 | 1 | 3 | 1 | 45 | 2 | 2 | 1 | 2.936 | 46.445 | 46.2 | 2.95 |
| 4 | 3 | 3 | 13 | 200 | 1 | 3 | 1 | 45 | 1 | 1 | 1 | 3.039 | 44.871 | 47.3 | 2.88 |
| 4 | 3 | 3 | 14 | 200 | 1 | 3 | 3 | 80 | 1 | 1 | 1 | 1.705 | 79.979 | 82.3 | 1.65 |
| 4 | 3 | 3 | 15 | 200 | 1 | 3 | 2 | 60 | 1 | 1 | 1 | 2.311 | 59.006 | 63.1 | 2.16 |
| 4 | 3 | 3 | 16 | 528 | 2 | 3 | 2 | 60 | 1 | 1 | 1 | 5.943 | 60.575 | 60.6 | 5.94 |
| 4 | 3 | 3 | 17 | 528 | 2 | 3 | 3 | 80 | 1 | 1 | 1 | 4.496 | 80.071 | 79.3 | 4.53 |
| 4 | 3 | 3 | 18 | 528 | 2 | 3 | 1 | 45 | 1 | 1 | 1 | 7.786 | 46.237 | 46.9 | 7.66 |
| 4 | 3 | 3 | 19 | 200 | 1 | 3 | 3 | 80 | 2 | 1 | 1 | 1.698 | 80.308 | 82.3 | 1.65 |
| 4 | 3 | 3 | 20 | 200 | 1 | 3 | 2 | 60 | 2 | 1 | 1 | 2.267 | 60.152 | 60.1 | 2.26 |
| 4 | 3 | 3 | 21 | 200 | 1 | 3 | 1 | 45 | 2 | 1 | 1 | 2.951 | 46.209 | 46.2 | 2.95 |
| 4 | 3 | 3 | 22 | 528 | 2 | 3 | 2 | 60 | 2 | 1 | 2 | 6.084 | 59.172 | 59.8 | 6.01 |
| 4 | 3 | 3 | 23 | 528 | 2 | 3 | 1 | 45 | 2 | 1 | 1 | 7.709 | 46.699 | 46.7 | 7.7 |
| 4 | 3 | 3 | 24 | 528 | 2 | 3 | 3 | 380 | 2 | 1 | 1 | 4.455 | 80.808 | 80 | 4.5 |
| 4 | 3 | 4 | 1 | 528 | 2 | 3 | 1 | 45 | 1 | 2 | 1 | 7.784 | 46.249 | 46.2 | 7.77 |
| 4 | 3 | 4 | 2 | 528 | 2 | 3 | 2 | 60 | 1 | 2 | 1 | 6.034 | 59.662 | 60.6 | 5.94 |
| 4 | 3 | 4 | 3 | 528 | 2 | 3 | 3 | 80 | 1 | 2 | 1 | 4.478 | 80.393 | 79.3 | 4.53 |
| 4 | 3 | 4 | 4 | 200 | 1 | 3 | 1 | 45 | 1 | 2 | 1 | 2.952 | 46.194 | 45.6 | 2.98 |
| 4 | 3 | 4 | 5 | 200 | 1 | 3 | 2 | 260 | 1 | 2 | 1 | 2.338 | 58.325 | 59.2 | 2.3 |
| 4 | 3 | 4 | 6 | 200 | 1 | 3 | 3 | 80 | 1 | 2 | 1 | 1.689 | 80.736 | 80.6 | 1.69 |
| 4 | 3 | 4 | 7 | 200 | 1 | 3 | 3 | 30 | 2 | 2 | 1 | 1.69 | 80.689 | 84.2 | 1.62 |
| 4 | 3 | 4 | 8 | 200 | 1 | 3 | 1 | 45 | 2 | 2 | 1 | 2.922 | 46.668 | 45.1 | 3.02 |
| 4 | 3 | 4 | 9 | 200 | 1 | 3 | 2 | 260 | 2 | 2 | 1 | 2.302 | 59.237 | 59.2 | 2.3 |
| 4 | 3 | 4 | 10 | 528 | 2 | 3 | 1 | 45 | 2 | 2 | 1 | 7.796 | 46.178 | 45.6 | 7.88 |
| 4 | 3 | 4 | 11 | 528 | 2 | 3 | 2 | - 60 | 2 | 2 | 1 | 6.132 | 58.708 | 58.4 | 6.15 |
| 4 | 3 | 4 | 12 | 528 | 2 | 3 | 3 | 3.80 | 2 | 2 | 2 | 4.477 | 80.411 | 78.1 | 4.06 |
| 4 | 3 | 4 | 13 | 528 | 2 | 3 | 2 | 260 | 1 | 1 | 1 | 6.013 | 59.870 | 58.8 | 6.12 |
| 4 | 3 | 4 | 14 | 528 | 2 | 3 | 3 | 30 | 1 | 1 | 1 | 4.502 | 79.964 | 77.5 | 4.64 |
| 4 | $?$ | 4 | 15 | 528 | 2 | 3 | 1 | 45 | 1 | 1 | 1 | 7.79 | 46.213 | 44.8 | 8.02 |
| 4 | 3 | 4 | 16 | 200 | 1 | 3 | 3 | 380 | 1 | 1 | 1 | 1.688 | 80.784 | 82.3 | 1.65 |
| 4 | 3 | 4 | 17 | 200 | - 1 | 3 | 1 | 145 | 1 | 1 | 1 | 3.034 | 44.945 | 45.6 | 2.98 |
| 4 | 3 | 4 | 18 | 200 | - 1 | 3 | 2 | 260 | 1 | 1 | 1 | 2.288 | 59.599 | 60.1 | 2.26 |
| 4 | 3 | 4 | 19 | 528 | 2 | 3 | 3 | 380 | 2 | 1 | 1 | 4.479 | 80.375 | 79.3 | 4.53 |
| 4 | 3 | 4 | 20 | 528 | 2 | 3 | 1 | 145 | 2 | 1 | 1 | 7.839 | 45.924 | 45.8 | 7.84 |
| 4 | 3 | 4 | 21 | 528 | 2 | 3 | 2 | 260 | 2 | 1 | 1 | 6.023 | 59.771 | 61.7 | 5.83 |
| 4 | 3 | 4 | 22 | 200 | 1 | 3 | 2 | 260 | 2 | 1 | 1 | 2.303 | 59.211 | 61.1 | 2.23 |
| 4 | 3 | 4 | 23 | 200 | 1 | 3 | 1 | 145 | 2 | 1 | 1 | 2.999 | 45.470 | 45.6 | 2.98 |
| 4 | 3 | 4 | 24 | 200 | 1 | 3 | 3 | 380 | 2 | 1 | 1 | 1.689 | 80.736 | 80.6 | 1.69 |

TABLE I. 15 -- Raw Data For Angular Study (Contimued)

SubNum Sessilum
RepNum TrialNo Cr ist
528
528
528
200
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TABLE I. 15 -- Raw Data For Angular Study (Continued)

SubNum SessNum | 6 | 3 |
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| 6 | 3 |
| 6 | 3 |

RepNum TrialNo | 1 |
| :---: |
| 1 |
| 1 |
| 1 |

| Crsoist CrsDistR | RefType | NomSpd DesrdSpd |  |  |
| ---: | ---: | ---: | ---: | ---: |
| 200 | 1 | 3 | 1 | 45 |
| 200 | 1 | 3 | 2 | 60 |
| 200 | 1 | 3 | 3 | 80 |
| 528 | 2 | 3 | 1 | 45 |
| 528 | 2 | 3 | 3 | 80 |
| 528 | 2 | 3 | 2 | 60 |
| 200 | 1 | 3 | 1 | 45 |
| 200 | 1 | 3 | 3 | 80 |
| 200 | 1 | 3 | 2 | 60 |
| 528 | 2 | 3 | 3 | 80 |
| 528 | 2 | 3 | 1 | 45 |
| 528 | 2 | 3 | 2 | 60 |
| 200 | 1 | 3 | 2 | 60 |
| 200 | 1 | 3 | 3 | 80 |
| 200 | 1 | 3 | 1 | 45 |
| 528 | 2 | 3 | 1 | 45 |
| 528 | 2 | 3 | 3 | 80 |
| 528 | 2 | 3 | 2 | 60 |
| 528 | 2 | 3 | 1 | 45 |
| 528 | 2 | 3 | 3 | 80 |
| 528 | 2 | 3 | 2 | 60 |
| 200 | 1 | 3 | 2 | 60 |
| 200 | 1 | 3 | 3 | 3 |

Elevatn Viewdist NoAttemp
Tr

| rueTime |
| ---: |
| 2.85 |
| 2.388 |
| 1.703 |
| 8.13 |
| 4.394 |
| 6.043 |
| 3.5 |
| 1.667 |
| 2.497 |
| 4.784 |
| 8.745 |
| 6.059 |
| 2.267 |
| 1.746 |
| 2.679 |
| 7.287 |
| 4.649 |
| 5.845 |
| 7.881 |
| 4.344 |
| 6.419 |
| 2.357 |
| 1.566 |
| 2.986 |
| 3.282 |
| 1.733 |
| 2.38 |
| 4.432 |
| 5.997 |
| 8.34 |
| 4.143 |
| 4.645 |
| 7.508 |
| 5.855 |
| 2.547 |
| 2.279 |
| 1.645 |
| 1.626 |
| 2.842 |
| 1.595 |
| 2.991 |
| 2.318 |
| 4.73 |


| TrueSpd | VASspeed | VAStime |
| :---: | :---: | :---: |
| 47.847 | 51.9 | 2.62 |
| 57.104 | 64.2 | 2.12 |
| 80.073 | 90.2 | 1.51 |
| 44.280 | 44 | 8.17 |
| 81.930 | 81.3 | 4.42 |
| 59.573 | 59.8 | 6.01 |
| 38.961 | 41.1 | 3.31 |
| 81.802 | 86.1 | 1.58 |
| 54.611 | 58.3 | 2.34 |
| 75.251 | 74.6 | 4.82 |
| 41.166 | 40.9 | 8.78 |
| 59.416 | 59.5 | 6.04 |
| 60.152 | 62.1 | 2.19 |
| 78.101 | 82.3 | 1.65 |
| 50.901 | 52.6 | 2.59 |
| 49.403 | 50.2 | 7.16 |
| 77.436 | 78.1 | 4.6 |
| 61.591 | 61.3 | 5.86 |
| 45.679 | 45.8 | 7.84 |
| 82.873 | 83.3 | 4.32 |
| 56.084 | 55.8 | 6.44 |
| 57.855 | 61.1 | 2.23 |
| 87.078 | 92.4 | 1.47 |
| 45.668 | 46.7 | 2.91 |
| 41.549 | 43 | 3.16 |
| 78.686 | 80.6 | 1.69 |
| 57.296 | 60.1 | 2.26 |
| 81.227 | 81.3 | 4.42 |
| 60.030 | 59.5 | 6.04 |
| 43.165 | 43.2 | 8.31 |
| 87.083 | 85.4 | 4.21 |
| 47.949 | 48 | 7.48 |
| 61.486 | 60.9 | 5.9 |
| 59.835 | 62.1 | 2.19 |
| 83.864 | 88.1 | 1.54 |
| 47.982 | 50.5 | 2.7 |
| 85.494 | 92.4 | 1.47 |
| 45.591 | 47.3 | 2.88 |
| 58.828 | 63.1 | 2.16 |
| 76.110 | 74.6 | 4.82 |
| 54.987 | 54.6 | 6.58 |
| 45.995 | 45.8 | 7.84 |
| 82.896 | 90.2 | 1.51 |
| 41.842 | 43.5 | 3.13 |
| 61.342 | 66.4 | 2.05 |
| 77.503 | 76.9 | 4.68 |
| 47.164 | 46.9 | 7.66 |
| 58.575 | 58.1 | 6.19 |

TABLE I. 15 -- Raw Data For Angular Study (Continued)
SubNum SessNum


TrueTime


TrueSpd
$59.045 \quad 58.8$
speed
58.8
47.1
Vastime
64.62
81.26
1.266 $\qquad$

TABLE I. 15 -- Raw Data For Angular Study (Contirued)


TABLE 1. 15 -- Raw Data For Angular Study (Continued)

|  | SubNum <br> 7 | SessNum | RepNum | TrialNo | CrsDist 528 | CrsDistR | Reftype 3 | NomSpd 2 | DesrdSpd | Elevatn | ViewDist | NoAttempt | TrueTime 5.879 | Truespd 61.235 | VASspeed 60.6 | VAStime 5.94 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 7 | 3 | 3 | 2 | 528 | 2 | 3 | 1 | 45 | 2 | 1 | 1 | 7.247 | 49.676 | 50.2 | 7.16 |
|  | 7 | 3 | 3 | 3 | 528 | 2 | 3 | 3 | 80 | 2 | 1 | 1 | 4.823 | 74.642 | 74 | 4.86 |
|  | 7 | 3 | 3 | 4 | 200 | 1 | 3 | 3 | 80 | 2 | 1 | 1 | 1.909 | 71.432 | 68.9 | 1.98 |
|  | 7 | 3 | 3 | 5 | 200 | 1 | 3 | 1 | 45 | 2 | 1 | 1 | 2.934 | 46.477 | 46.7 | 2.91 |
|  | 7 | 3 | 3 | 6 | 200 | 1 | 3 | 2 | 60 | 2 | 1 | 1 | 2.423 | 56.279 | 57.4 | 2.37 |
|  | 7 | 3 | 3 | 7 | 528 | 2 | 3 | 1 | 45 | 1 | 1 | 1 | 7.272 | 49.505 | 49.7 | 7.23 |
|  | 7 | 3 | 3 | 8 | 528 | 2 | 3 | 2 | 60 | 1 | 1 | 1 | 6.41 | 56.162 | 55.5 | 6.48 |
|  | 7 | 3 | 3 | 9 | 528 | 2 | 3 | 3 | 80 | 1 | 1 | 1 | 4.755 | 75.710 | 74.6 | 4.82 |
|  | 7 | 3 | 3 | 10 | 200 | 1 | 3 | 2 | 60 | 1 | 1 | 1 | 2.304 | 59.186 | 62.1 | 2.19 |
|  | 7 | 3 | 3 | 11 | 200 | 1 | 3 | 1 | 45 | 1 | 1 | 1 | 2.975 | 45.837 | 48.5 | 2.8 |
|  | 7 | 3 | 3 | 12 | 200 | 1 | 3 | 3 | 80 | 1 | 1 | 1 | 1.678 | 81.266 | 86.1 | 1.58 |
|  | 7 | 3 | 3 | 13 | 528 | 2 | 3 | 1 | 45 | 2 | 2 | 1 | 7.73 | 46.572 | 47.1 | 7.63 |
|  | 7 | 3 | 3 | 14 | 528 | 2 | 3 | 3 | 80 | 2 | 2 | 1 | 4.242 | 84.866 | 82.6 | 4.35 |
|  | 7 | 3 | 3 | 15 | 528 | 2 | 3 | 2 | 60 | 2 | 2 | 1 | 6.586 | 54.661 | 54.9 | 6.55 |
|  | 7 | 3 | 3 | 16 | 200 | 1 | 3 | 1 | 45 | 2 | 2 | 1 | 2.831 | 48.168 | 49.2 | 2.77 |
|  | 7 | 3 | 3 | 17 | 200 | 1 | 3 | 2 | 60 | 2 | 2 | 1 | 2.217 | 61.508 | 66.4 | 2.05 |
|  | 7 | 3 | 3 | 18 | 200 | 1 | 3 | 3 | 80 | 2 | 2 | 1 | 1.672 | 81.557 | 82.3 | 1.65 |
|  | 7 | 3 | 3 | 19 | 528 | 2 | 3 | 3 | 80 | 1 | 2 | 1 | 4.402 | 81.781 | 81.9 | 4.39 |
|  | 7 | 3 | 3 | 20 | 528 | 2 | 3 | 2 | 60 | 1 | 2 | 1 | 6.39 | 56.338 | 55.5 | 6.48 |
|  | 7 | 3 | 3 | 21 | 528 | 2 | 3 | 1 | 45 | 1 | 2 | 1 | 7.76 | 46.392 | 46.5 | 7.74 |
|  | 7 | 3 | 3 | 22 | 200 | 1 | 3 | 1 | 45 | 1 | 2 | 1 | 2.788 | 48.911 | 50.5 | 2.7 |
| $\mapsto$ | 7 | 3 | 3 | 23 | 200 | 1 | 3 | 2 | 60 | 1 | 2 | 1 | 2.182 | 62.495 | 63.1 | 2.16 |
| $\stackrel{\sim}{+}$ | 7 | 3 | 3 | 24 | 200 | 1 | 3 | 3 | 80 | 1 | 2 | 1 | 1.577 | 86.470 | 90.2 | 1.51 |
| 0 | 7 | 3 | 4 | 1 | 528 | 2 | 3 | 2 | 60 | 2 | 1 | 1 | 5.798 | 62.090 | 62.1 | 5.79 |
|  | 7 | 3 | 4 | 2 | 528 | 2 | 3 | 3 | 80 | 2 | 1 | 1 | 4.484 | 80.285 | 80 | 4.5 |
|  | 7 | 3 | 4 | 3 | 528 | 2 | 3 | 1 | 45 | 2 | 1 | 1 | 7.463 | 48.238 | 48 | 7.48 |
|  | 7 | 3 | 4 | 4 | 200 | 1 | 3 | 2 | 60 | 2 | 1 | 1 | 2.333 | 58.450 | 57.4 | 2.37 |
|  | 7 | 3 | 4 | 5 | 200 | 1 | 3 | 3 | 80 | 2 | 1 | 1 | 1.58 | 86.306 | 84.2 | 1.62 |
|  | 7 | 3 | 4 | 6 | 200 | 1 | 3 | 1 | 45 | 2 | 1 | 1 | 2.9 | 47.022 | 46.7 | 2.91 |
|  | 7 | 3 | 4 | 7 | 200 | 1 | 3 | 2 | 60 | 1 | 1 | 1 | 2.296 | 59.392 | 63.1 | 2.16 |
|  | 7 | 3 | 4 | 8 | 200 | 1 | 3 | 1 | 45 | 1 | 1 | 1 | 2.926 | 46.604 | 46.2 | 2.95 |
|  | 7 | 3 | 4 | 9 | 200 | 1 | 3 | 3 | 80 | 1 | 1 | 1 | 1.724 | 79.097 | 77.3 | 1.76 |
|  | 7 | 3 | 4 | 10 | 528 | 2 | 3 | 1 | 45 | 1 | 1 | 1 | 7.991 | 45.051 | 44.8 | 8.02 |
|  | 7 | 3 | 4 | 11 | 528 | 2 | 3 | 2 | 60 | 1 | 1 | 1 | 5.815 | 61.909 | 62.1 | 5.79 |
|  | 7 | 3 | 4 | 12 | 528 | 2 | 3 | 3 | 80 | 1 | 1 | 1 | 4.439 | 84.099 | 80 | 4.5 |
|  | 7 | 3 | 4 | 13 | 200 | 1 | 3 | 2 | 60 | 2 | 2 | 1 | 2.28 | 59.809 | 61.1 | 2.23 |
|  | 7 | 3 | 4 | 14 | 200 | 1 | 3 | 3 | 80 | 2 | 2 | 1 | 1.675 | 81.411 | 80.6 | 1.69 |
|  | 7 | 3 | 4 | 15 | 200 | 1 | 3 | 1 | 45 | 2 | 2 | 1 | 2.762 | 49.371 | 49.8 | 2.73 |
|  | 7 | 3 | 4 | 16 | 528 | 2 | 3 | 3 | 80 | 2 | 2 | 1 | 4.834 | 74.472 | 72.9 | 4.93 |
|  | 7 | 3 | 4 | 17 | 528 | 2 | 3 | 2 | 60 | 2 | 2 | 1 | 5.977 | 60.231 | 60.6 | 5.94 |
|  | 7 | 3 | 4 | 18 | 528 | 2 | 3 | 1 | 45 | 2 | 2 | 1 | 7.892 | 45.616 | 45.8 | 7.84 |
|  | 7 | 3 | 4 | 19 | 200 | 1 | 3 | 3 | 80 | 1 | 2 | 1 | 1.718 | 79.373 | 80.6 | 1.69 |
|  | 7 | 3 | 4 | 20 | 200 | 1 | 3 | 2 | 60 | 1 | 2 | 1 | 2.152 | 63.366 | 63.1 | 2.16 |
|  | 7 | 3 | 4 | 21 | 200 | 1 | 3 | 1 | 45 | 1 | 2 | 1 | 2.851 | 47.830 | 47.9 | 2.84 |
|  | 7 | 3 | 4 | 22 | 528 | 2 | 3 | 2 | 60 | 1 | 2 | 1 | 5.579 | 64.528 | 63.2 | 5.68 |
|  | 7 | 3 | 4 | 23 | 528 | 2 | 3 | 1 | 45 | 1 | 2 | 1 | 6.94 | 51.873 | 52 | 6.91 |
|  | 7 | 3 | 4 | 24 | 528 | 2 | 3 | 3 | 80 | 1 | 2 | 1 | 4.714 | 76.368 | 76.9 | 4.68 |


| SubNum $8$ | SessNum <br> 3 | RepNum | TrialNo | $\begin{array}{r} \text { CrsDist } \\ 200 \end{array}$ | CrsDistR 1 | Reftype 3 | NomSpd 1 | DesrdSpd 45 | Elevatn 2 | ViewDist 2 | NoAt tempt 1 | Truet ime 3.195 | TrueSpd 42.680 | VASspeed 44 | VAStime 3.09 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 8 | 3 | 1 | 2 | 200 | 1 | 3 | 3 | 80 | 2 | 2 | 1 | 1.698 | 80.308 | 84.2 | 1.62 |
| 8 | 3 | 1 | 3 | 200 | 1 | 3 | 2 | 60 | 2 | 2 | 1 | 2.347 | 58.101 | 60.1 | 2.26 |
| 8 | 3 | 1 | 4 | 528 | 2 | 3 | 2 | 60 | 2 | 2 | 1 | 6.372 | 56.497 | 56.8 | 6.33 |
| 8 | 3 | 1 | 5 | 528 | 2 | 3 | 1 | 45 | 2 | 2 | 1 | 7.189 | 50.077 | 50 | 7.2 |
| 8 | 3 | 1 | 6 | 528 | 2 | 3 | 3 | 80 | 2 | 2 | 1 | 4.753 | 75.742 | 76.9 | 4.68 |
| 8 | 3 | 1 | 7 | 200 | 1 | 3 | 2 | 60 | 1 | 2 | 1 | 2.292 | 59.495 | 63.1 | 2.16 |
| 8 | 3 | 1 | 8 | 200 | 1 | 3 | 3 | 80 | 1 | 2 | 1 | 1.714 | 79.559 | 82.3 | 1.65 |
| 8 | 3 | 1 | 9 | 200 | 1 | 3 | 1 | 45 | 1 | 2 | 1 | 3.122 | 43.678 | 46.2 | 2.95 |
| 8 | 3 | 1 | 10 | 528 | 2 | 3 | 2 | 60 | 1 | 2 | 2 | 6.39 | 56.338 | 57.1 | 6.3 |
| 8 | 3 | 1 | 11 | 528 | 2 | 3 | 3 | 80 | 1 | 2 | 1 | 4.432 | 81.227 | 81.3 | 4.42 |
| 8 | 3 | 1 | 12 | 528 | 2 | 3 | 1 | 45 | 1 | 2 | 1 | 7.928 | 45.409 | 45.4 | 7.92 |
| 8 | 3 | 1 | 13 | 528 | 2 | 3 | 3 | 80 | 2 | 1 | 1 | 4.503 | 79.947 | 78.1 | 4.6 |
| 8 | 3 | 1 | 14 | 528 | 2 | 3 | 2 | 60 | 2 | 1 | 1 | 6.462 | 55.710 | 55.8 | 6.44 |
| 8 | 3 | 1 | 15 | 528 | 2 | 3 | 1 | 45 | 2 | 1 | 1 | 7.644 | 47.096 | 47.3 | 7.59 |
| 8 | 3 | 1 | 16 | 200 | 1 | 3 | 3 | 80 | 2 | 1 | 1 | 1.658 | 82.246 | 90.2 | 1.51 |
| 8 | 3 | 1 | 17 | 200 | 1 | 3 | 2 | 60 | 2 | 1 | 1 | 2.256 | 60.445 | 66.4 | 2.05 |
| 8 | 3 | 1 | 18 | 200 | 1 | 3 | 1 | 45 | 2 | 1 | 9 | 2.93 | 46.540 | 50.5 | 2.7 |
| 8 | 3 | 1 | 19 | 528 | 2 | 3 | 2 | 60 | 1 | 1 | 1 | 6.471 | 55.633 | 56.1 | 6.4 |
| 8 | 3 | 1 | 20 | 528 | 2 | 3 | 1 | 45 | 1 | 1 | 1 | 8.599 | 41.865 | 41.8 | 8.6 |
| 8 | 3 | 1 | 21 | 528 | 2 | 3 | 3 | 80 | 1 | 1 | 1 | 4.276 | 84.191 | 85.4 | 4.21 |
| 8 | 3 | 1 | 22 | 200 | 1 | 3 | 3 | 80 | 1 | 1 | 2 | 1.646 | 82.845 | 90.2 | 1.51 |
| 8 | 3 | 1 | 23 | 200 | 1 | 3 | 2 | 60 | 1 | 1 | 1 | 2.249 | 60.633 | 65.3 | 2.08 |
| 8 | 3 | 1 | 24 | 200 | 1 | 3 | 1 | 45 | 1 |  | 1 | 3.153 | 43.249 | 46.7 | 2.91 |
| 8 | 3 | 2 | 1 | 200 | 1 | 3 | 3 | 80 | 1 | 2 | 1 | 1.75 | 77.922 | 80.6 | 1.69 |
| 8 | 3 | 2 | 2 | 200 | 1 | 3 | 1 | 45 | 1 | 2 | 1 | 2.651 | 51.439 | 54.1 | 2.52 |
| 8 | 3 | 2 | 3 | 200 | 1 | 3 | 2 | 60 | 1 | 2 | 1 | 2.184 | 62.438 | 65.3 | 2.08 |
| 8 | 3 | 2 | 4 | 528 | 2 | 3 | 1 | 45 | 1 | 2 | 1 | 7.134 | 50.463 | 50.7 | 7.09 |
| 8 | 3 | 2 | 5 | 528 | 2 | 3 | 3 | 80 | 4 | 2 | 1 | 4.704 | 76.531 | 76.9 | 4.68 |
| 8 | 3 | 2 | 6 | 528 | 2 | 3 | 2 | 60 | 1 | 2 | 1 | 6.247 | 57.628 | 57.8 | 6.22 |
| 8 | 3 | 2 | 7 | 528 | 2 | 3 | 3 | 80 | 2 | 2 | 1 | 4.807 | 74.891 | 75.1 | 4.78 |
| 8 | 3 | 2 | 8 | 528 | 2 | 3 | 2 | 60 | 2 | 2 | 1 | 5.67 | 63.492 | 64.1 | 5.61 |
| 8 | 3 | 2 | 9 | 528 | 2 | 3 | , | 45 | 2 | 2 | 1 | 8.013 | 44.927 | 44.8 | 8.02 |
| 8 | 3 | 2 | 10 | 200 | , | 3 | 2 | 60 | 2 | 2 | 2 | 2.259 | 60.365 | 63.1 | 2.16 |
| 8 | 3 | 2 | 11 | 200 | 1 | 3 | 1 | 45 | 2 | 2 | 2 | 2.709 | 50.337 | 51.2 | 2.66 |
| 8 | 3 | 2 | 12 | 200 | 1 | 3 | 3 | 80 | 2 | 2 | 1 | 1.659 | 82.196 | 80.6 | 1.69 |
| 8 | 3 | 2 | 13 | 528 | 2 | 3 | 1 | 45 | $\because 2$ | 1 | 1 | 8.095 | 44.472 | 44.4 | 8.1 |
| 8 | 3 | 2 | 14 | 528 | 2 | 3 | 3 | 80 | 2 | 1 | 1 | 4.264 | 84.428 | 84.7 | 4.24 |
| 8 | 3 | 2 | 15 | 528 | 2 | 3 | 2 | 60 | 2 | 1 | 1 | 5.929 | 60.719 | 60.6 | 5.94 |
| 8 | 3 | 2 | 16 | 200 | 1 | 3 | 2 | 60 | 2 | 1 | 1 | 2.224 | 61.315 | 65.3 | 2.08 |
| 8 | 3 | 2 | 17 | 200 | 1 | 3 | 1 | 45 | 2 | 1 | 1 | 3.068 | 44.447 | 48.5 | 2.8 |
| 8 | 3 | 2 | 18 | 200 | 1 | 3 | 3 | 80 | 2 | 1 | 1 | 1.87 | 72.922 | 77.3 | 1.76 |
| 8 | 3 | 2 | 19 | 200 | 1 | 3 | 1 | 45 | 1 | 1 | 1 | 3.218 | 42.375 | 44.5 | 3.06 |
| 8 | 3 | 2 | 20 | 200 | 1 | 3 | 2 | 60 | 1 | 1 | 1 | 2.176 | 62.667 | 66.4 | 2.05 |
| 8 | 3 | 2 | 21 | 200 | 1 | 3 | 3 | 80 | 1 |  | 1 | 1.628 | 83.761 | 90.2 | 1.51 |
| 8 | 3 | 2 | 22 | 528 | 2 | 3 | 2 | 60 | 1 |  | 1 | 5.694 | 63.224 | 63.2 | 5.68 |
| 8 | 3 | 2 | 23 | 528 | 2 | 3 | 1 | 45 | 1 | 1 | 1 | 8.723 | 41.270 | 42.1 | 8.53 |
| 8 | 3 | 2 | 24 | 528 | 2 | 3 | 3 | 80 | 1 | 1 | 1 | 4.636 | 77.653 | 76.9 | 4.68 |


| SubNum 8 | SessNum <br> 3 | RepNum | TrialNo | $\begin{array}{r} \text { CrsDist } \\ 528 \end{array}$ | CrsDistR 2 | Reftype | NomSpd | $\begin{array}{r} \text { DesrdSpd } \\ 60 \end{array}$ | Elevatn | Viewoist | NoAt tempt | $\begin{array}{r} \text { TrueTime } \\ 5.98 \end{array}$ | TrueSpd 60.201 | VASspeed 59.8 | $\begin{array}{r} \text { VASt ime } \\ 6.01 \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 8 | 3 | 3 | 2 | 528 | 2 | 3 | 1 | 45 | 1 | 1 | 1 | 7.247 | 49.676 | 49.7 | 7.23 |
| 8 | 3 | 3 | 3 | 528 | 2 | 3 | 3 | 80 | 1 | 1 | 1 | 4.823 | 74.642 | 74.6 | 4.82 |
| 8 | 3 | 3 | 4 | 200 | 1 | 3 | 3 | 80 | 1 | 1 | 1 | 1.909 | 71.432 | 74.3 | 1.83 |
| 8 | 3 | 3 | 5 | 200 | 1 | 3 | 1 | 45 | 1 | 1 | 1 | 2.934 | 46.477 | 49.8 | 2.73 |
| 8 | 3 | 3 | 6 | 200 | 1 | 3 | 2 | 60 | 1 | 1 | 1 | 2.423 | 56.279 | 62.1 | 2.19 |
| 8 | 3 | 3 | 7 | 528 | 2 | 3 | 1 | 45 | 2 | 1 | 1 | 6.993 | 51.480 | 52.6 | 6.84 |
| 8 | 3 | 3 | 8 | 528 | 2 | 3 | 2 | 60 | 2 | 1 | 1 | 6.41 | 56.162 | 56.4 | 6.37 |
| 8 | 3 | 3 | 9 | 528 | 2 | 3 | 3 | 80 | 2 | 1 | 1 | 4.755 | 75.710 | 76.3 | 4.71 |
| 8 | 3 | 3 | 10 | 200 | 1 | 3 | 2 | 60 | 2 | 1 | 1 | 2.304 | 59.186 | 62.1 | 2.19 |
| 8 | 3 | 3 | 11 | 200 | 1 | 3 | 1 | 45 | 2 | 1 | 1 | 2.975 | 45.837 | 49.2 | 2.77 |
| 8 | 3 | 3 | 12 | 200 | 1 | 3 | 3 | 80 | 2 | 1 | 1 | 1.678 | 81.266 | 88.1 | 1.54 |
| 8 | 3 | 3 | 13 | 528 | 2 | 3 | 1 | 45 | 1 | 2 | 1 | 8.091 | 44.494 | 44.6 | 8.06 |
| 8 | 3 | 3 | 14 | 528 | 2 | 3 | 3 | 80 | 1 | 2 | 1 | 4.242 | 84.866 | 84.7 | 4.24 |
| 8 | 3 | 3 | 15 | 528 | 2 | 3 | 2 | 60 | 1 | 2 | 1 | 6.586 | 54.661 | 54.3 | 6.62 |
| 8 | 3 | 3 | 16 | 200 | 1 | 3 | 1 | 45 | 1 | 2 | 1 | 2.831 | 48.168 | 51.2 | 2.66 |
| 8 | 3 | 3 | 17 | 200 | 1 | 3 | 2 | 60 | 1 | 2 | 1 | 2.217 | 61.508 | 62.1 | 2.19 |
| 8 | 3 | 3 | 18 | 200 | 1 | 3 | 3 | 80 | 1 | 2 | 1 | 1.672 | 81.557 | 84.2 | 1.62 |
| 8 | 3 | 3 | 19 | 528 | 2 | 3 | 3 | 80 | 2 | 2 | 9 | 4.374 | 82.305 | 83.3 | 4.32 |
| 8 | 3 | 3 | 20 | 528 | 2 | 3 | 2 | 60 | 2 | 2 | 1 | 6.39 | 56.338 | 56.4 | 6.37 |
| 8 | 3 | 3 | 21 | 528 | 2 | 3 | 1 | 45 | 2 | 2 | 1 | 7.76 | 46.392 | 46.2 | 7.77 |
| 8 | 3 | 3 | 22 | 200 | 1 | 3 | 1 | 45 | 2 | 2 | 1 | 2.788 | 48.911 | 50.5 | 2.7 |
| 8 | 3 | 3 | 23 | 200 | 1 | 3 | 2 | 60 | 2 | 2 | 1 | 2.182 | 62.495 | 65.3 | 2.08 |
| 8 | 3 | 3 | 24 | 200 | 1 | 3 | 3 | 80 | 2 | 2 | 1 | 1.577 | 86.470 | 90.2 | 1.51 |
| 8 | 3 | 4 | 1 | 528 | 2 | 3 | 2 | 60 | 1 | 1 | 1 | 5.798 | 62.090 | 62.8 | 5.72 |
| 8 | 3 | 4 | 2 | 528 | 2 | 3 | 3 | 80 | 1 | 1 | 1 | 4.484 | 80.285 | 80.6 | 4.46 |
| 8 | 3 | 4 | 3 | 528 | 2 | 3 | 1 | 45 | 1 | 1 | 1 | 7.463 | 48.238 | 48.5 | 7.41 |
| 8 | 3 | 4 | 4 | 200 | 1 | 3 | 2 | 60 | 1 | 1 | 1 | 2.333 | 58.450 | 63.1 | 2.16 |
| 8 | 3 | 4 | 5 | 200 | 1 | 3 | 3 | 80 | , | 1 | 1 | 1.58 | 86.306 | 92.4 | 1.47 |
| 8 | 3 | 4 | 6 | 200 | 1 | 3 | 1 | 45 | 1 | 1 | 1 | 2.9 | 47.022 | 51.2 | 2.66 |
| 8 | 3 | 4 | 7 | 200 | 1 | 3 | 2 | 60 | 2 | 1 | 1 | 2.296 | 59.392 | 64.2 | 2.12 |
| 8 | 3 | 4 | 8 | 200 | 1 | 3 | 1 | 45 | 2 | 1 | 1 | 2.926 | 46.604 | 49.8 | 2.73 |
| 8 | 3 | 4 | 9 | 200 | 1 | 3 | 3 | 80 | 2 | 1 | 1 | 1.724 | 79.097 | 86.1 | 1.58 |
| 8 | 3 | 4 | 10 | 528 | 2 | 3 | 1 | 45 | 2 | 1 | 1 | 7.991 | 45.051 | 45.2 | 7.95 |
| 8 | 3 | 4 | 11 | 528 | 2 | 3 | 2 | 60 | 2 | 1 | 1 | 5.815 | 61.909 | 62.8 | 5.72 |
| 8 | 3 | 4 | 12 | 528 | 2 | 3 | 3 | 80 | 2 | 1 | 1 | 4.439 | 81.099 | 81.3 | 4.42 |
| 8 | 3 | 4 | 13 | 200 | 1 | 3 | 2 | 60 | 1 | 2 | 1 | 2.28 | 59.809 | 61.1 | 2.23 |
| 8 | 3 | 4 | 14 | 200 | 1 | 3 | 3 | 80 | 1 | 2 | 1 | 1.675 | 81.411 | 84.2 | 1.62 |
| 8 | 3 | 4 | 15 | 200 | 1 | 3 | 1 | 45 | 1 | 2 | 1 | 2.762 | 49.371 | 50.5 | 2.7 |
| 8 | 3 | 4 | 16 | 528 | 2 | 3 | 3 | 80 | 1 | 2 | 1 | 4.834 | 74.472 | 74.6 | 4.82 |
| 8 | 3 | 4 | 17 | 528 | 2 | 3 | 2 | 60 | 1 | 2 | 1 | 5.977 | 60.231 | 60.9 | 5.9 |
| 8 | 3 | 4 | 18 | 528 | 2 | 3 | 1 | 45 | 1 | 2 | 1 | 7.892 | 45.616 | 46.2 | 7.77 |
| 8 | 3 | 4 | 19 | 200 | 1 | 3 | 3 | 80 | 2 | 2 | 1 | 1.718 | 79.373 | 80.6 | 1.69 |
| 8 | 3 | 4 | 20 | 200 | 1 | 3 | 2 | 60 | 2 | 2 | 1 | 2.152 | 63.366 | 64.2 | 2.12 |
| 8 | 3 | 4 | 21 | 200 | 1 | 3 | 1 | 45 | 2 | 2 | 1 | 2.851 | 47.830 | 48.5 | 2.8 |
| 8 | 3 | 4 | 22 | 528 | 2 | 3 | 2 | 60 | 2 | 2 | 1 | 5.695 | 63.213 | 63.6 | 5.65 |
| 8 | 3 | 4 | 23 | 528 | 2 | 3 | 1 | 45 | 2 | 2 | 1 | 6.94 | 51.873 | 52 | 6.91 |
| 8 | 3 | 4 | 24 | 528 | 2 | 3 | 3 | 80 | 2 | 2 | 1 | 4.714 | 76.368 | 76.3 | 4.71 |

TABLE I. 16 -- Reference Marker Alignment - Summary Statistics Upper
View Eleva- Course Nom.
Dist. tion Dist. Speed N Mean Limit $95 \%$-tile $99 \%$-tile MSE Variance $\quad$ K

| Align - Overall | 24 | -0.063 | 3.999 | 2.698 | 2.877 | 3.3320 | 3.182 | 2.225 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| 200 | Ground | 200 | 45 | 8 | -0.346 | 5.181 | 0.901 | 0.954 | 3.1064 | 1.629 | 3.136 |
| :--- | :--- | :--- | :--- | :--- | ---: | :--- | :--- | :--- | :--- | :--- | :--- |
| 200 | Ground | 200 | 60 | 8 | 0.199 | 4.953 | 2.169 | 2.373 | 2.3753 | 1.797 | 3.136 |
| 200 | Ground | 200 | 80 | 8 | 0.040 | 4.276 | 3.442 | 3.802 | 1.8244 | 6.887 | 3.136 |



| Angular | Comparable | 24 | 3.479 | 8.492 | 6.372 | 7.137 | 5.0754 | 4.183 | 2.225 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Conditions |  |  |  |  |  |  |  |  |


| 200 | Ground | 200 | 45 | 8 | 2.444 | 7.472 | 3.887 | 4.120 | 2.5710 | 2.057 | 3.136 |
| :--- | :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 200 | Ground | 200 | 60 | 8 | 3.886 | 6.027 | 5.359 | 5.729 | 0.4661 | 1.480 | 3.136 |
| 200 | Ground | 200 | 80 | 8 | 4.109 | 13.054 | 6.989 | 7.282 | 8.1365 | 8.339 | 3.136 |

Reference Marker Alignment Study - Aligned vs. Unaligned Reference Marks
A. Variables

Subject Number
Nominal Speed
Replication
Alignment
B. Significant Effects (p $\leq 0.05$ )

Alignment

| Al ignmert | Mean <br> Error |
| :---: | :---: |
| Not Al igned <br> Al igned | 3.479 |

Subject Number- see summary of experiment

| SubNum 7 | SessNum 6 | RepNum | TrialNo 1 | $\begin{array}{r} \text { CrsDist } \\ 200 \end{array}$ | CrsDistR 1 | Reftype 3 | NomSpd | $\begin{array}{r} \text { DesrdSpd } \\ 60 \end{array}$ | Elevatn Viewdist $1 \quad 1$ | NoAttempt | TrueTime 2.49 | TrueSpd 54.765 | VASspeed 54.1 | VAStime 2.52 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7 | 6 | 1 | 2 | 200 | 1 | 3 | 3 | 80 | 11 | 1 | 1.649 | 82.695 | 80.6 | 1.69 |
| 7 | 6 | 1 | 3 | 200 | 1 | 3 | 1 | 45 | 11 | 1 | 3.356 | 40.633 | 41.6 | 3.27 |
| 7 | 6 | 2 | 1 | 200 | 1 | 3 | 2 | 60 | 11 | 1 | 2.392 | 57.008 | 57.4 | 2.37 |
| 7 | 6 | 2 | 2 | 200 | 1 | 3 | 3 | 80 | 11 | 1 | 1.841 | 74.070 | 70.1 | 1.94 |
| 7 | 6 | 2 | 3 | 200 | 1 | 3 | 1 | 45 | 11 | 1 | 2.913 | 46.812 | 45.6 | 2.98 |
| 7 | 6 | 3 | 1 | 200 | 1 | 3 | 2 | 60 | 11 | 1 | 2.324 | 58.676 | 61.1 | 2.23 |
| 7 | 6 | 3 | 2 | 200 | 1 | 3 | 1 | 45 | $1 \quad 1$ | 1 | 2.7 | 50.505 | 50.5 | 2.7 |
| 7 | 6 | 3 | 3 | 200 | 1 | 3 | 3 | 80 | 11 | 1 | 1.804 | 75.590 | 74.3 | 1.83 |
| 7 | 6 | 4 | 1 | 200 | 1 | 3 | 1 | 45 | $1 \quad 1$ | 1 | 3.082 | 44.245 | 43.5 | 3.13 |
| 7 | 6 | 4 | 2 | 200 | 1 | 3 | 2 | 60 | $1 \quad 1$ | 1 | 2.199 | 62.012 | 61.1 | 2.23 |
| 7 | 6 | 4 | 3 | 200 | 1 | 3 | 3 | 80 | 11 | 1 | 1.697 | 80.356 | 80.6 | 1.69 |
| 8 | 6 | 1 | 1 | 200 | 1 | 3 | 2 | 60 | 11 | 1 | 2.449 | 55.681 | 55.7 | 2.44 |
| 8 | 6 | 1 | 2 | 200 | 1 | 3 | 3 | 80 | $1 \quad 1$ | 1 | 1.698 | 80.308 | 84.2 | 1.62 |
| 8 | 6 | 1 | 3 | 200 | 1 | 3 | 1 | 45 | $1 \quad 1$ | 1 | 3.19 | 42.747 | 39.8 | 3.42 |
| 8 | 6 | 2 | 1 | 200 | 1 | 3 | 2 | 60 | 11 | 1 | 2.299 | 59.314 | 61.1 | 2.23 |
| 8 | 6 | 2 | 2 | 200 | 1 | 3 | 3 | 80 | 11 | 1 | 1.744 | 78.190 | 77.3 | 1.76 |
| 8 | 6 | 2 | 3 | 200 | 1 | 3 | 1 | 45 | 11 | 1 | 2.894 | 47.119 | 47.3 | 2.88 |
| 8 | 6 | 3 | 1 | 200 | 1 | 3 | 2 | 60 | 11 | 1 | 2.331 | 58.500 | 57.4 | 2.37 |
| 8 | 6 | 3 | 2 | 200 | 1 | 3 | 1 | 45 | 11 | 1 | 2.783 | 48.999 | 49.8 | 2.73 |
| 8 | 6 | 3 | 3 | 200 | 1 | 3 | 3 | 80 | 11 | 1 | 1.752 | 77.833 | 80.6 | 1.69 |
| 8 | 6 | 4 | 1 | 200 | 1 | 3 | 1 | 45 | 11 | 1 | 2.964 | 46.007 | 46.2 | 2.95 |
| 8 | 6 | 4 | 2 | 200 | 1 | 3 | 2 | 60 | 11 | 1 | 2.196 | 62.096 | 61.1 | 2.23 |
| 8 | 6 | 4 | 3 | 200 | 1 | 3 | 3 | 80 | 11 | 1 | 1.691 | 80.641 | 82.3 | 1.65 |

## APPENDIX J

A Second Statistical Analysis

A second statistical analysis was performed to determine statistically significant variables. This analysis took into account the lack of complete randomization for the different studies. The lack of complete randomization created what is called a split-plot experimental design. The statistical analysis in the body of the report did not examine the effect of the split-plot design. The results of this second analysis (w/ split-plot) is compared to the results of the first analysis (w/o split-plot) in Table J. 1.

Table J. 1 -- Comparison of Statistical Analyses With and With Out Split-Plot

| Study | Statistically significant Variables |  |
| :---: | :---: | :---: |
|  | w/ split-plot | w/o split-plot |
| Moving | Subjects <br> Distance $x$ Method <br> Speed x Distance x Method | Subjects Method Distance Speed $\times$ Method Distance $\times$ Method Speed $\times$ Distance $\times$ Method |
| Reference Marker Alignment | Alignment | Alignment Subjects |
| Parking | Subjects Speed x Distance | $\begin{gathered} \text { Subjects } \\ \text { Speed } \times \text { Distance }- \text { nearly } \\ \text { significant } \end{gathered}$ |
| $\begin{aligned} & \text { Angular - } \\ & \text { (see note) } \end{aligned}$ | ```Subjects ReplicateNone``` | Subjects <br> Distance <br> Subject $\times$ Distance Distance x Speed |

Note - The analyses for the angular study presented in Table J. 1 do not include group effects.

The results presented in Table J. 1 show that the two analyses are very similar. Since this was the case, it was decided not to pursue the split-plot analysis further.

## APPENDIX K

## Preliminary Study Results

The main objective of this preliminary evaluation was to determine the accuracy of the VASCAR-plus hardware, without including the human factors involved with typical usage. A secondary objective was to compare user operated VASCAR speed measurements to "true" average speed measurements. The results of these tests must be considered preliminary.

## TEST PROCEDURE

To check the accuracy of the drive in distance method, officers $A$ and $B$ were asked to drive in distances between two sets of reference points. The first set of reference points were 240 feet apart, the second set were 440 feet apart. The accuracy of these distances is $+/-1 / 2$ inch. Each officer was asked to drive in the distance 5 times. The officers set the VASCAR units to display the measured distance to the nearest foot. [It was later discovered that this set up for the display was not the highest resolution VASCAR can achieve. It has a higher resolution when the distance is displayed in miles.]

To test the accuracy of the timing mechanism of the VASCAR-plus, a vehicle was driven repeatedly over a known distance (in this case a separate course which was measured to be 439 feet $8-9 / 16$ inches) at three different nominal speeds ( 35 , 55 , and 65 mph ). A separate VASCAR-plus unit and a Nicolet oscilloscope were wired to two electronic trip switches; one at the beginning of the course, and one at the end. The trip switches were tripped by the vehicle tires rolling over them. Since both the front and rear tires will cause the trip switches to trip, a "flip-flop" circuit was used to insure that only the front tire of the vehicle would trip the Nicolet and the VASCAR-plus timing mechanism. [It was later discovered that the flip-flop circuit and the VASCAR-plus timing mechanism were incompatible. The flip flop circuit induced inconsistent timing delays in the VASCAR timing mechanism that were not found in later bench tests conducted without the flip-flop circuit. The flip-flop circuit did not affect the Nicolet timing mechanism.]

The VASCAR-plus manual states that the device collects data every 36 milliseconds (msec). The Nicolet can collect data at user selected time increments. For the 35 mph tests, the Nicolet sample interval was set at 2 msec ,
and for the 55 and 65 mph tests, a sample interval of 1 msec was chosen. These Nicolet sample rates yield a speed measurement resolution of .014 mph or better, so the Nicolet times were taken as the true times and the VASCAR-plus times were compared to them. The trip switches and the flip-flop board reaction times were at least 100 times less than the Nicolet sample intervals used, so they did not introduce significant error for the Nicolet time measurements. The flip-flop circuit measured reaction times are given in the attachment to this appendix.

Officers A and B also measured the vehicle speed during the above tests, as well as others. The officers first entered the course distance using the "drivein" method. They then were positioned approximately 300 feet away from the center of the course (see Figure K.1). Officer A was in a squad car elevated approximately 7 feet above the ground, while officer B was in a car at ground level. Poles were positioned at the beginning and the end of the course, so the officers had good reference markers. The officers watched the vehicle pass the poles. As the vehicle passed the first pole, the officers switched on the red time toggle switch, and as it passed the second pole, they switched it off. The VASCAR-plus computer then calculated the speed based on the entered distance and the time the red time switch was on. These speeds were recorded and compared to the Nicolet calculated speeds which were based on dividing the distance of the course by the Nicolet recorded time.

The officers also recorded speeds on a 200 foot course. The officers were again positioned near the center of the course, but officer A was positioned right next to the course and officer $B$ was positioned approximately 150 feet away (see Figure K.2). The officers objected to these conditions. The reference markers for this course were yellow strips of tape that were placed on the ground at the beginning and end of the course. The officer measured the speed the same way as described before. Nominal speeds of 35 and 60 mph were used on this course. The Nicolet and trip switches were also used on this course to measure the true speed. The Nicolet sample interval was 1 msec for the 35 mph tests and .5 msec for the 60 mph tests. Again, the officers' speeds were recorded and compared to the Nicolet's calculated speed.




The results of the distance measurements performed by officers A and B are shown in Table K.l. The left half of the table is for the 240 foot distance, while the right half is for the 440 foot distance. The mean and standard deviation for each distance and for each officer are presented at the bottom of the table.

Mean
Standard Deviation
Distance Measurement Using VASCAR-plus

|  | $\begin{gathered} \text { Officer Measurement } \\ \text { of } 240 \text { Foot } \\ \text { Distance Using VASCAR-plus } \end{gathered}$ |  | Officer Measurement of 440 Foot <br> Distance Using VASCAR-plus |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Officer A | Officer B | Officer A | Officer B |
|  | 239 | 239 | 441 | 440 |
|  | 240 | 239 | 440 | 440 |
|  | 240 | 240 | 442 | 441 |
|  | 241 | 239 | 440 | 439 |
|  | 241 | 239 | 441 | 440 |
| Mean | 240.2 | 239.2 | 440.8 | 440 |
| Standard Deviation | 0.84 | 0.45 | 0.84 | 0.71 |

The Nicolet and VASCAR-plus time measurements for the 35 mph tests on the 439 feet $8-9 / 16$ inch ( 439.71 feet) course are compared in Table K.2. Both the Nicolet and VASCAR were triggered with the same electronic switches, so no human factors were involved in the time measurements. The Nicolet times are presented in the first column and the VASCAR-plus times are in the second column. Time error (VASCAR time - Nicolet Time) is presented in the third column and the percent time error is presented in the fourth column.

Nicolet and VASCAR velocities that were calculated using the time values in Table K. 2 and the course distance ( 439.71 feet) are compared in Table K.3. Tables for the 55 and 65 mph tests are in the attachment to this appendix.

Comparison of NICOLET and VASCAR Time Measurements

```
NOMINAL SPEED \(=35 \mathrm{mph}\)
DISTANCE \(=439.71 \mathrm{ft}\)
```

|  | Nicolet $2 \mathrm{~ms}$ | VASCAR Tripped | Time Error. | Percent Time Error |
| :---: | :---: | :---: | :---: | :---: |
|  | 8.282 | 8.24 | -0.042 | -0.51 |
|  | 8.566 | 8.53 | -0.036 | -0.42 |
|  | 8.552 | 8.49 | -0.062 | -0.72 |
|  | 8.316 | 8.28 | -0.036 | -0.43 |
|  | 8.490 | 8.46 | -0.030 | -0.35 |
|  | 8.408 | 8.35 | -0.058 | -0.69 |
|  | 8.400 | 8.35 | -0.050 | -0.60 |
|  | 8.244 | 8.20 | -0.044 | -0.53 |
|  | 8.246 | 8.20 | -0.046 | -0.56 |
|  | 8.340 | 8.31 | -0.030 | -0.36 |
| Mean | 8.384 | 8.34 | -0.043 | -0.52 |
| Standard Deviation | 0.120 | 0.119 | 0.011 | 0.129 |

TABLE K. 3
Comparison of NICOLET and VASCAR Velocity Calculations

> NOMINAL SPEED $=35 \mathrm{mph}$
> DISTANCE $=439.71 \mathrm{ft}$

|  | Nicolet <br> Calculation | VASCAR <br> Calculation |  | Speed <br> Error |
| :--- | :---: | :---: | :---: | :---: |

The mean absolute and percent differences between the Nicolet and VASCAR computed velocities for the 35,55 , and 65 mph tests are listed in Table K. 4 .

TABLE K. 4
Mean Errors and Mean Percent Errors for VASCAR Computed Velocities

| Test Condition <br> (nominal <br> speed/course length) <br> $($ mph/feet) | Mean <br> Error <br> (mph) | Mean Percent <br> Error <br> $(\%)$ |
| :---: | :---: | :---: |
| $35 / 439.71$ | .186 | 0.52 |
| $55 / 439.71$ | .404 | 0.74 |
| $65 / 439.7$ | .535 | 0.83 |

Comparisons of officer $A^{\prime} s$ and $B^{\prime}$ 's measured velocities to the "true" velocities for the 35 mph tests on the 200 foot course are shown in Tables K. 5 K.7. The true velocities are calculated using the Nicolet times and the course distance. The true velocities and officer A's and B's velocities are listed in Table K.5. For these tests, officer A was next to the course (distance=0) and officer B was 150 feet away from the course (distance=150).

TABLE K. 5
Comparison of True and Officer Measured Velocities
Using VASCAR-plus
NOMINAL SPEED $=35 \mathrm{mph}$ DISTANCE $=200 \mathrm{ft}$

Mean
Standard Deviation
*Distance $=$ Distance From Target Vehicle Path in Feet

The percent speed errors are listed in Table K.6. The mean and standard deviation for each officers percent speed error are presented at the bottom of the table.

TABLE K. 6
Officers' Percent Speed Error
NOMINAL SPEED $=35 \mathrm{mph}$ DISTANCE $=200 \mathrm{ft}$

Officer A
Distance $=0$
3.30
1.97
1.57
0.20
0.58
3.12
2.39
2.91
2.68
$\frac{3.99}{2.27}$
1.204

Officer B
$\underline{\text { Distance }=150}$ 0.18
-0.14
0.12
-1.96
1.13
-0.05
0.92
0.90
-0.49
Mean
Standard Deviation
$\frac{-1.04}{-0.04}$
0.951

The speed errors are listed in Table K.7. The mean and standard deviation for speed error are at the bottom of the table. Similar tables for the other test conditions are in the attachment to this appendix.

|  | TABLE K. 7 |  |
| :---: | :---: | :---: |
|  | Officers' Speed Error |  |
|  | NOMINAL SPEED $=35 \mathrm{mph}$ DISTANCE $=200 \mathrm{ft}$ |  |
|  | $\begin{gathered} \text { Officer A } \\ \underline{\text { Distance }=0} \end{gathered}$ | $\begin{gathered} \text { Officer B } \\ \text { Distance }=150 \end{gathered}$ |
|  | 1.16 | 0.06 |
|  | 0.65 | -0.05 |
|  | 0.54 | 0.04 |
|  | 0.07 | -0.73 |
|  | 0.21 | 0.41 |
|  | 1.08 | -0.02 |
|  | 0.81 | 0.31 |
|  | 1.01 | 0.31 |
|  | 0.93 | -0.17 |
|  | 1.35 | -0.35 |
| Mean | 0.78 | -0.02 |
| Standard Deviation | 0.412 | 0.341 |

Each officers' mean percent speed error for each test condition is listed in Table K. 8.

TABLE K. 8
Officer A and B Mean Percent Speed Error

| Test Condition <br> (nominal <br> speed/course length) <br> (mph/feet) | Officer A <br> (8) | Officer B <br> $(8)$ |
| :---: | :---: | :---: |
| $35 / 200$ | 2.27 | -0.04 |
| $60 / 200$ | 5.41 | 1.11 |
| $35 / 439.71$ | 0.55 | 1.08 |
| $55 / 439.71$ | 0.67 | 1.37 |
| $65 / 439.71$ | 1 | 0.71 |
|  |  | 1.25 |

Tables K. 9 and K. 10 list the mean and standard deviation for speed error for each test condition for officers $A$ and $B$ respectively.

TABLE K. 9
Officer A's Mean and Standard Deviation for Speed Error

| Test Condition <br> (nominal <br> speed/course length) <br> (mph/feet) | Mean <br> $(\mathrm{mph})$ | Standard Deviation <br> (mph) |
| :---: | :---: | :---: |
| $35 / 200$ | 0.78 | 0.412 |
| $60 / 200$ | 3.26 |  |
| $35 / 439.71$ | 0.20 | 1.602 |
|  | $55 / 439.71$ | 0.37 |
| $65 / 439.71$ | 0.45 | 0.261 |
|  |  | 0.392 |
|  |  |  |

TABLE K. 10
Officer B's Mean and Standard Deviation for Speed Error


The upper 90 th percentile tolerance limit (with $95 \%$ confidence) for each test condition and each officer is listed in Table K. 11 . The following formala is used to calculate these tolerance limits:

K for ten samples is 2.839.

TABLE K. 11
Upper 90th Percentile Tolerance Limits for Speed Error


The upper 90th percentile tolerance limits for the 200 foot course distance are plotted in Figure K.3. From Figure K.3, the upper 90th percentile tolerance limits for officer $B$ were less than those for officer A. This probably was primarily due to officer location. Referring to Figure K.2, officer A was right next to the course, while officer B was 150 feet away. This probably gave officer $B$ a better vantage point. The tolerance limits increased as speed increased. The officers strongly objected to the set up of the test conditions. They said they would never set up a course like this.

The upper 90th percentile tolerance limits for the 439.71 foot course distance are plotted in Figure K.4. From this figure, the upper tolerance limits for both officers were fairly comparable. The tolerance limits increased as speed increased.

Upper 90th percentile tolerance limits for the VASCAR distance measurements and the VASCAR timing mechanism were not appropriate due to complications with the testing. As stated earlier, the VASCAR timing errcrs for these tests were incorrect due to complications with the flip-flop circuit. The VASCAR distance


errors were incorrect because the VASCAR was set up to display in feet instead of miles.

## SUMMARY

Since this study was considered preliminary, and since it was limited to only two officers, no definitive conclusions were drawn. The following statements summarize the results of this study:

1. The mean speed errors were less than 1 mph for 9 of the 10 combinations of officer, speed, and course distance. The errors increased as speed increased and as course distance decreased.
2. The upper 90th percentile tolerance limits for speed error were less than 2.5 mph for 8 of the 10 combinations of officer, speed, and course distance. The two conditions which produced higher tolerance limits were the $60 \mathrm{mph} / 200$ foot course distance combination for each officer. This combination of speed and course distance gave the shortest timing interval for the study.
3. The two officers that participated in this study objected to some of the viewing distance/course distance combinations. Their strongest objections were for the officer adjacent to the roadway/200 foot course distance combination.
4. The errors in the distance measurements taken with the VASCAR-plus device were not representative, since the device was not set at its highest resolution. This was not learned until after the completion of the testing for this study.
5. The error in the timing mechanism of the VASCAR-plus device were not accurate due to an incompatibility between the VASCAR-plus timing mechanism and the flip-flop circuit. This incompatibility was not discovered until after the completion of the testing for this study.

## ATTACHMENT TO APPENDIX K

Raw Data from VASCAR-plus Testing


TABLE K. 13

Comparison of NICOLET and VASCAR Time Measurements
NOMINAL SPEED $=55 \mathrm{mph}$ DISTANCE $=439.71 \mathrm{ft}$

|  | Nicolet <br> I ms. | VASCAR <br> Tripped | Absolute <br> Diff | of diff <br> (\%) |
| :--- | :---: | :---: | :---: | :---: |
|  | 5.531 | 5.50 | -0.031 | -0.56 |
|  | 5.376 | 5.32 | -0.056 | -1.04 |
|  | 5.463 | 5.43 | -0.033 | -0.60 |
|  | 5.553 | 5.50 | -0.053 | -0.95 |
|  | 5.470 | 5.43 | -0.040 | -0.73 |
|  | 5.399 | 5.36 | -0.039 | -0.72 |
|  | 5.412 | 5.36 | -0.052 | -0.96 |
|  | 5.565 | 5.54 | -0.025 | -0.45 |
|  | 5.434 | 5.40 | -0.034 | -0.63 |
|  | 5.395 | 5.36 | -0.035 | -0.65 |
| Mean | 5.460 | 5.42 | -0.040 | -0.73 |
| Std. Dev. | 0.069 | 0.073 | 0.010 | 0.195 |

TABLE K. 14

Comparison of NICOLET and VASCAR Velocity Calculations

> NOMINAL SPEED $=55 \mathrm{mph}$ DISTANCE $=439.71 \mathrm{ft}$

|  | Nicolet <br> Calc. | VASCAR <br> Calc. | Absolute <br> Diff. | q diff. <br> (q) |
| :--- | :---: | :---: | :---: | :---: |
|  | 54.20 | 54.51 | 0.306 | 0.56 |
|  | 55.77 | 56.35 | 0.587 | 1.05 |
|  | 54.88 | 55.21 | 0.334 | 0.61 |
|  | 53.99 | 54.51 | 0.520 | 0.96 |
|  | 54.81 | 55.21 | 0.404 | 0.74 |
|  | 55.53 | 55.93 | 0.404 | 0.73 |
|  | 55.40 | 55.93 | 0.537 | 0.97 |
|  | 53.87 | 54.12 | 0.243 | 0.45 |
|  | 55.17 | 55.52 | 0.347 | 0.63 |
|  | 55.57 | 55.93 | 0.363 | 0.65 |
| Mean | 54.92 | 55.32 | 0.404 | 0.74 |
| Std. Dev. | 0.690 | 0.747 | 0.111 | 0.198 |

Comparison of Nicolet and VASCAR Time Measurements
NOMINAL SPEED $=65 \mathrm{mph}$
DISTANCE $=439.71 \mathrm{ft}$

|  | $\begin{gathered} \text { Nicolet } \\ 1 \mathrm{~ms} . \end{gathered}$ | VASCAR Tripped | Absolute Diff. | $\begin{gathered} \% \text { diff } \\ (\%) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: |
|  | 4.735 | 4.71 | -0.025 | -0.53 |
|  | 4.564 | 4.53 | -0.034 | -0.74 |
|  | 4.546 | 4.50 | -0.046 | -1.01 |
|  | 4.609 | 4.57 | -0.039 | -0.85 |
|  | 4.671 | 4.64 | -0.031 | -0.66 |
|  | 4.657 | 4.60 | -0.057 | -1.22 |
|  | 4.686 | 4.64 | -0.046 | -0.98 |
|  | 4.655 | 4.60 | -0.055 | -1.18 |
|  | 4.705 | 4.68 | -0.025 | -0.53 |
|  | 4.663 | 4.64 | -0.023 | -0,49 |
| Mean | 4.649 | 4.61 | -0.038 | -0.82 |
| Std. Dev. | 0.060 | 0.065 | 0.013 | 0.271 |

TABLE K. 16
Comparison of NICOLET and VASCAR Velocity Calculations

> NOMINAL SPEED $=65 \mathrm{mph}$
> DISTANCE $=439.71 \mathrm{ft}$

|  | Nicolet <br> Calc. | VASCAR <br> Calc. | Absolute <br> Diff. | o diff. <br> (\%) |
| :--- | ---: | :---: | :---: | :---: |
|  | 63.32 | 63.65 | 0.336 | 0.53 |
|  | 65.69 | 66.18 | 0.493 | 0.75 |
|  | 65.95 | 66.62 | 0.674 | 1.02 |
|  | 65.05 | 65.60 | 0.555 | 0.85 |
|  | 64.18 | 64.61 | 0.429 | 0.67 |
|  | 64.38 | 65.17 | 0.798 | 1.24 |
|  | 63.98 | 64.61 | 0.634 | 0.99 |
|  | 64.40 | 65.17 | 0.770 | 1.20 |
|  | 63.72 | 64.06 | 0.340 | 0.53 |
|  | 64.29 | 64.61 | 0.319 | 0.50 |
| Mean | 64.50 | 65.03 | 0.535 | 0.83 |
| Std. Dev. | 0.834 | 0.919 | 0.180 | 0.276 |

TABLE K. 17

## Comparison of True and Officer Measured Velocities Using VASCAR-plus

NOMINAL SPEED $=60 \mathrm{mph}$
DISTANCE $=200 \mathrm{ft}$
True
Officer A
Officer B Velocity $\quad$ Distance $=0 \quad$ Distance $=150$

|  | 64.23 | 66.5 | 65.1 |
| :--- | :--- | ---: | ---: |
|  | 58.98 | 62.1 | 58.1 |
|  | 60.90 | 62.1 | 61.9 |
|  | 62.18 | 64.3 | 63.0 |
|  | 58.09 | 60.2 | 59.0 |
|  | 59.61 | 65.4 | 60.9 |
|  | 58.39 | 61.1 | 59.0 |
|  | 61.56 | 67.7 | 63.0 |
|  | 60.57 | 64.3 | 61.9 |
|  | $\underline{58.68}$ | $\boxed{62.1}$ | 58.1 |
| Mean |  | 63.58 | 61.00 |
| Standard Deviation | 1.954 | 2.449 | 2.387 |

Distance $=$ Distance from Target Vehicle Path in Feet

TABLE K. 18

Officers Percent Speed Error
NOMINAL SPEED $=60 \mathrm{mph}$ DISTANCE $=200 \mathrm{ft}$

Officer A Officer B
Distance $=0 \quad$ Distance $=150$
$3.53 \quad 1.35$
$5.29 \quad-1.49$
$1.97 \quad 1.64$
$3.41 \quad 1.32$
3.631 .57
$9.71 \quad 2.16$
$4.64 \quad 1.04$
$9.97 \quad 2.34$
$6.16 \quad 2.20$
$\frac{5.83}{5.41} \quad \frac{-0.98}{1.11}$
Standard
Deviation 2.6491 .313

TABLE K. 19

Officers' Speed Error
NOMINAL SPEED $=60 \mathrm{mph}$ DISTANCE $=200 \mathrm{ft}$

Officer A
Officer B
$\underline{\text { Distance }=0 \quad \text { Distance }=150}$
$2.27 \quad 0.87$
$3.12-0.88$
1.20
1.00
$2.12 \quad 0.82$
$2.11 \quad 0.91$
$5.79 \quad 1.29$
$2.71 \quad 0.61$
$6.14 \quad 1.44$
$3.73 \quad 1.33$
$\begin{array}{ll}\text { Mean } & \frac{1.02}{3.26} \quad \frac{-2.98}{0.68}\end{array}$
Standard
Deviation 1.6020 .789


TABLE K. 23
Comparison of True and Officer Measured Velocities Using VASCAR-plus

NOMINAL SPEED $=55 \mathrm{mph}$ DISTANCE $=439.71 \mathrm{ft}$

|  | True <br> Velocity | Officer A <br> Distance $=300$ | Officer B <br> Distance $=300$ |
| :--- | :---: | :---: | :---: |
| 54.20 | 54.2 | 55.0 |  |
|  | 55.77 | 56.4 | 56.4 |
|  | 54.88 | 55.3 | 56.1 |
|  | 53.99 | 54.2 | 55.0 |
|  | 54.81 | 55.0 | 55.0 |
|  | 55.53 | 55.3 | 56.8 |
|  | 55.40 | 56.1 | 55.3 |
|  | 53.87 | 53.9 | 55.0 |
|  | 55.17 | 56.1 | 55.7 |
| Mean | 55.57 | 56.4 |  |
| Standard Deviation | 54.92 | 55.29 | 55.67 |
|  | 0.690 | 0.953 | 0.704 |

TABLE K. 24
Officers' Percent Speed Error
NOMINAL SPEED $=55 \mathrm{mph}$ DISTANCE $=439.71 \mathrm{ft}$

Officer A Officer B Distance $=300$ Distance $=300$

|  | -0.01 | 1.47 |
| :--- | ---: | ---: |
|  | 1.14 | 1.14 |
|  | 0.77 | 2.23 |
|  | 0.39 | 1.87 |
|  | 0.35 | 0.35 |
|  | -0.41 | 2.29 |
|  | 1.27 | -0.17 |
|  | 0.05 | 2.09 |
|  | 1.68 | 0.96 |
|  | 1.49 |  |
|  | 0.67 |  |
| Mean |  | 1.37 |
| Standard |  |  |
| Deviation | 0.706 |  |
|  |  |  |

TABLE K. 25
Officers' Speed Error
NOMINAL SPEED $=55 \mathrm{mph}$
: DISTANCE $=439.71 \mathrm{ft}$

|  | Officer A <br> Distance $=300$ | $\begin{aligned} \text { Officer } & \mathrm{B} \\ \text { Distance } & =300 \end{aligned}$ |
| :---: | :---: | :---: |
|  | -0.00 | 0.80 |
|  | 0.63 | 0.63 |
|  | 0.42 | 1.22 |
|  | 0.21 | 1.01 |
|  | 0.19 | 0.19 |
|  | -0.23 | 1.27 |
|  | 0.70 | -0.10 |
|  | 0.03 | 1.13 |
|  | 0.93 | 0.53 |
|  | 0.83 | 0.83 |
| Mean | 0.37 | 0.75 |
| Standard |  |  |
| Deviation | on 0.392 | 0.447 |

## Comparison of True and Officer Measured Velocities

 Using VASCAR-plusNOMINAL SPEED $=65 \mathrm{mph}$ DISTANCE $=439.71 \mathrm{ft}$

|  | True <br> Velocity | Officer A <br> Distance $=300$ | Officer B <br> Distance $=300$ |
| :--- | :---: | :---: | :---: |
| 63.32 | 63.8 | 64.8 |  |
| 65.69 | 66.3 | 66.8 |  |
| 65.95 | 64.8 | 66.8 |  |
|  | 65.05 | 65.8 | 65.8 |
|  | 64.18 | 64.8 | 64.8 |
|  | 64.38 | 65.3 | 65.3 |
|  | 63.98 | 64.3 | 65.3 |
|  | 64.40 | 65.3 | 65.3 |
|  | 63.72 | 63.8 | 64.3 |
|  | 64.29 | 65.3 | 63.8 |
| Mean | 64.50 | 64.95 | 65.30 |
| Standard Deviation | 0.834 | 0.818 | 0.972 |

TABLE K. 27
TABLE K. 28

Officers' Percent Speed Error
NOMINAL SPEED $=65 \mathrm{mph}$ DISTANGE $=439.71 \mathrm{ft}$

Officer A Officer B
Distance $=300$ Distance $=300$

### 0.76 <br> 2.34

$0.93 \quad 1.69$
$-1.74 \quad 1.29$
$1.16 \quad 1.16$
$0.96 \quad 0.96$
$1.43 \quad 1.43$
$0.50 \quad 2.07$
$1.39 \quad 1.39$
$0.13 \quad 0.91$
$\begin{array}{ll}\frac{1.56}{0.71} & -0.77 \\ 1.25\end{array}$
Standard
Deviation $0.968 \quad 0.843$

Officers' Speed Error
NOMINAL SPEED $=65 \mathrm{mph}$ DISTANCE $=439.71 \mathrm{ft}$

Officer A Officer B Distance $=300$ Distance $=300$ $0.48 \quad 1.48$
$0.61 \quad 1.11$
$-1.15 \quad 0.85$
$0.75 \quad 0.75$
$0.62 \quad 0.62$
$0.92 \quad 0.92$
$0.32 \quad 1.32$
$0.90 \quad 0.90$
$0.08 \quad 0.58$
$-1.01$
$\frac{-0.49}{0.80}$
Standard
Deviation 0.631
0.540


[^0]:    Subject Number
    Viewing Distance
    Course Distance
    Interaction of Group with Viewing Distance
    Interaction of Group with Course Distance
    Interaction of Viewing Distance with Course Distance
    Interaction of Course Distance with Nominal Speed
    Interaction of Group with Viewing Distance with Course Distance

