

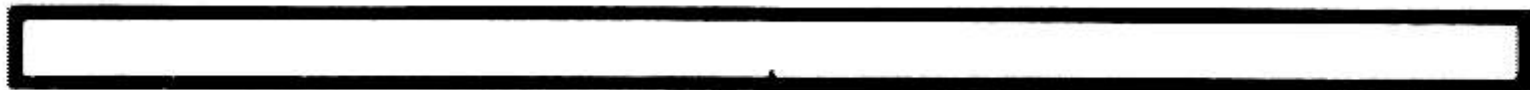
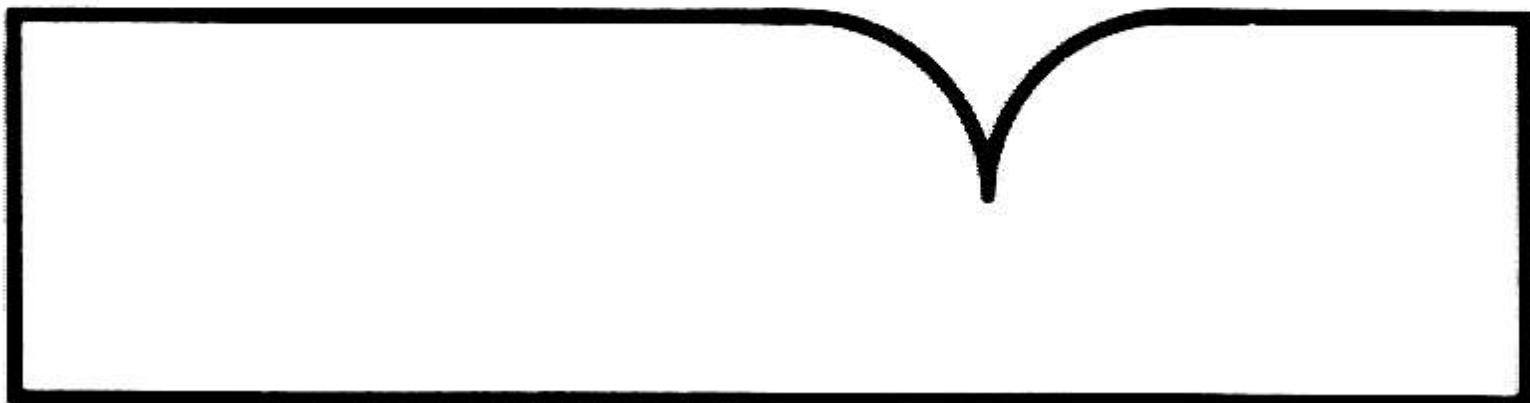
Baseline Fuel Economy and Emissions
Tests of a Chrysler 1978, 225 CID Engine

(U.S.) Transportation Systems Center
Cambridge, MA

Prepared for

National Highway Traffic Safety Administration
Washington, DC

Sep 80



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BASELINE
 FUEL ECONOMY AND EMISSIONS TESTS
 OF A
 CHRYSLER 1978, 225CID ENGINE

G. GAGNE, M. BELL, AND R. WALTER

U.S. DEPARTMENT OF TRANSPORTATION
 RESEARCH AND SPECIAL PROGRAMS ADMINISTRATION
 TRANSPORTATION SYSTEMS CENTER
 CAMBRIDGE MA 02142



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 SEPTEMBER 1980

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16. Abstract This document reports on baseline engine tests of a Chrysler 1978, 225 CID, six-cylinder engine. The tests were conducted in the Automotive Research Laboratory at the Transportation Systems Center. Test results presented herein are also filed on computer-based tapes (9-track ASC II) and are available from the National Technical Information Services (NTIS).					
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PREFACE

This report presents the baseline, steady-state test results of a 1978 Chrysler 225 CID engine. This work was performed in the Automotive Research Laboratory at the Transportation Systems Center of the U.S. Department of Transportation. This work is in support of the Automotive Fuel Economy Research and Analysis Support Program for NHTSA's Technology Assessment Division, Office of Passenger Vehicle Research. The authors gratefully acknowledge the technical support of Ralph Colello, Dr. Thomas Trella, Russell Zub, and Norman Deserres.

METRIC CONVERSION FACTORS

Approximate Conversion to Metric Measures		Approximate Conversion from Metric Measures	
Symbol	When the Given Multiplies by	Symbol	To Find
<u>LENGTH</u>			
1.0	1.0	1.0	1.0
1.0	1.0	1.0	1.0
1.0	1.0	1.0	1.0
<u>AREA</u>			
1.0	1.0	1.0	1.0
1.0	1.0	1.0	1.0
1.0	1.0	1.0	1.0
<u>MASS (weight)</u>			
1.0	1.0	1.0	1.0
1.0	1.0	1.0	1.0
1.0	1.0	1.0	1.0
<u>VOLUME</u>			
1.0	1.0	1.0	1.0
1.0	1.0	1.0	1.0
1.0	1.0	1.0	1.0
<u>TEMPERATURE (centy)</u>			
1.0	1.0	1.0	1.0
1.0	1.0	1.0	1.0
1.0	1.0	1.0	1.0

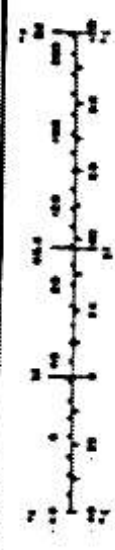
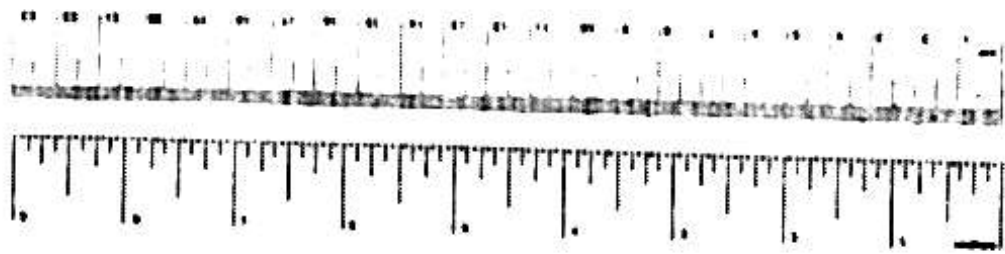


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1. INTRODUCTION

The work reported details the results of baseline, steady-state testing of a 1978 Chrysler, 6-cylinder, 225 CID engine. These tests measured the fuel rate and gaseous emissions while the engine was operated on a dynamometer at 57 speed/load points.

The objectives of this engine test are as follows:

- o Characterize the fuel economy and emissions of present and prototype automotive engines;
- o Provide an independent data base for vehicle performance modeling and fuel economy assessment.

2. EXPERIMENTAL DESIGN

This section briefly reviews the test design and highlights salient features of the Chrysler 225 CID baseline testing.

2.1 ENGINE

The manufacturers specifications for the Chrysler 225 CID engine are given in Table 1.

TABLE 1. ENGINE CHARACTERISTICS

Model Year	1978
Manufacturer	Chrysler Corp.
No. of cylinders	6
Displacement	225 CID (3.7L)
Bore	3.40 inches (86 mm)
Stroke	4.125 inches (105 mm)
Compression ratio	8.4 to 1
Max. Rated HP	109 @ 3600 rpm
Max. Rated Torque	182 @ 2000 rpm
Calibration	49 State, automatic
Transmission type	automatic
Engine weight*	564 lbs (256 kg)

This mean-tolerance engine was broken-in with the test schedule shown in Table 2. The engine came equipped with an oxidation catalyst and Exhaust Gas Recirculation (EGR) for emissions control. The engine was equipped with a manual transmission flywheel for mounting to the dynamometer.

*Includes starter, alternator, fan, manual transmission flywheel, bell housing, wire harness, battery cables, vacuum lines, air inlet system. Does not include radiator, water hoses, exhaust pipes, muffler, engine coolant, oil.

TABLE 2. CHRYSLER 225 CID ENGINE BREAK-IN SCHEDULE

<u>Period</u> <u>(hr)</u>	<u>Speed</u> <u>(rpm)</u>	<u>Torque</u> <u>(lb-ft)</u>
1	1200	64.0
1	1600	94.5
1	2000	108.5
2	2400	122.5
2	2800	133.0
2	3200	136.5
2	3600	138.3(1)
2	4000	WOT (1)
1/2	4400	WOT (2)

- (1) Cycle 4 min. at load, 1 min. at 1600 rpm no load
 (2) Check wide-open throttle (WOT) friction from 4400 rpm down

A single batch of unleaded Indolene test fuel was used for engine break-in and testing. The gasoline specifications are shown in Table 3.

TABLE 3. FUEL SPECIFICATIONS

Amoco Unleaded Indolene
 Specific Gravity ... 0.7455@60°F
 Percent Carbon... 83.39
 Percent Hydrogen... 12.93
 H/C Atomic ratio... 1.85
 Upper heating value... 19,733 BTU/lb

2.2 TEST CONFIGURATION

The engine was installed in the Automotive Research Laboratory test cell No. 2. This cell has a DC, programmable dynamometer for power absorption and motoring tests. Figures 1 and 2 show the electronic and fluid - flow configurations for the engine mounted in the cell for testing. Figure 3 is an illustration of the engine installed in the cell.

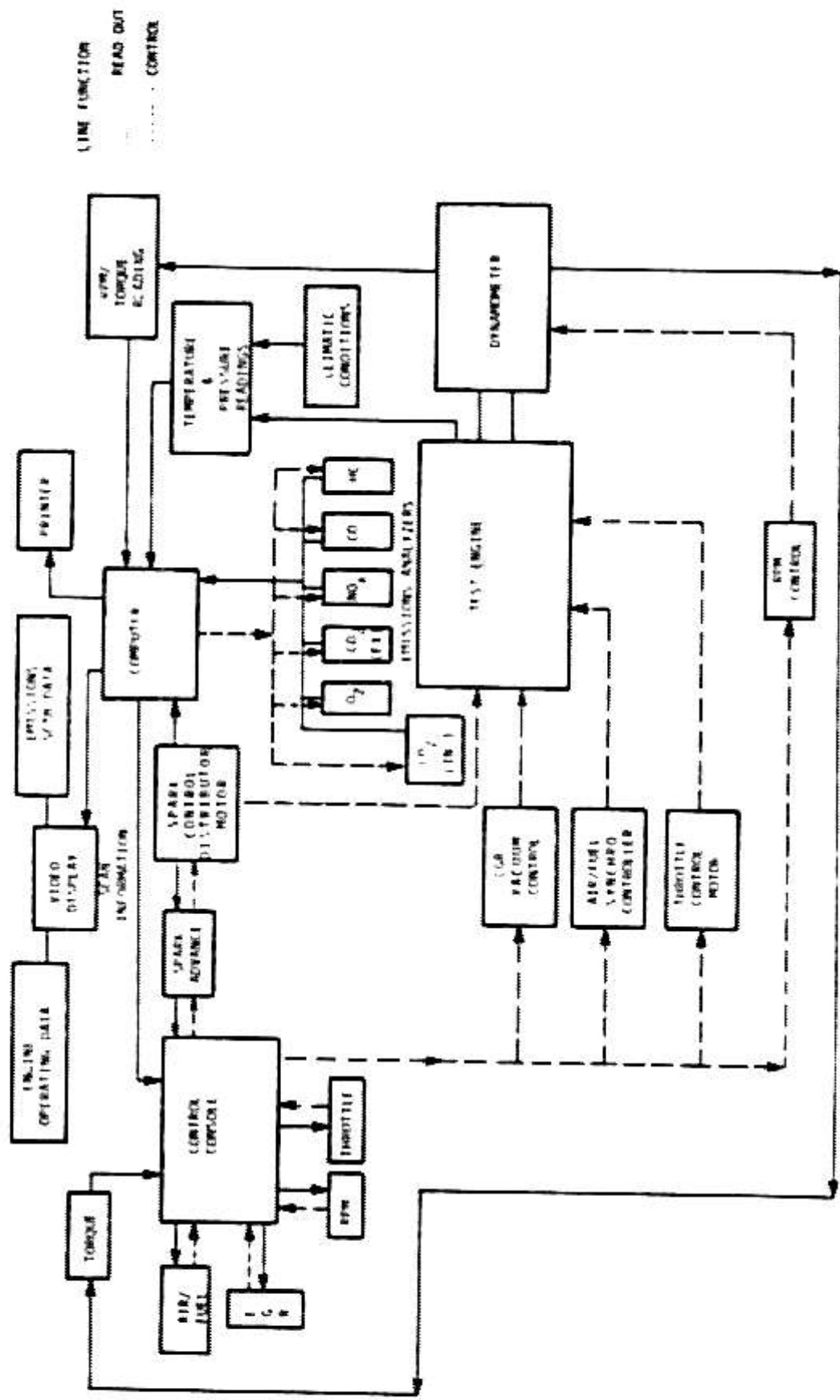


FIGURE 1. ELECTRONIC FLOW DIAGRAM

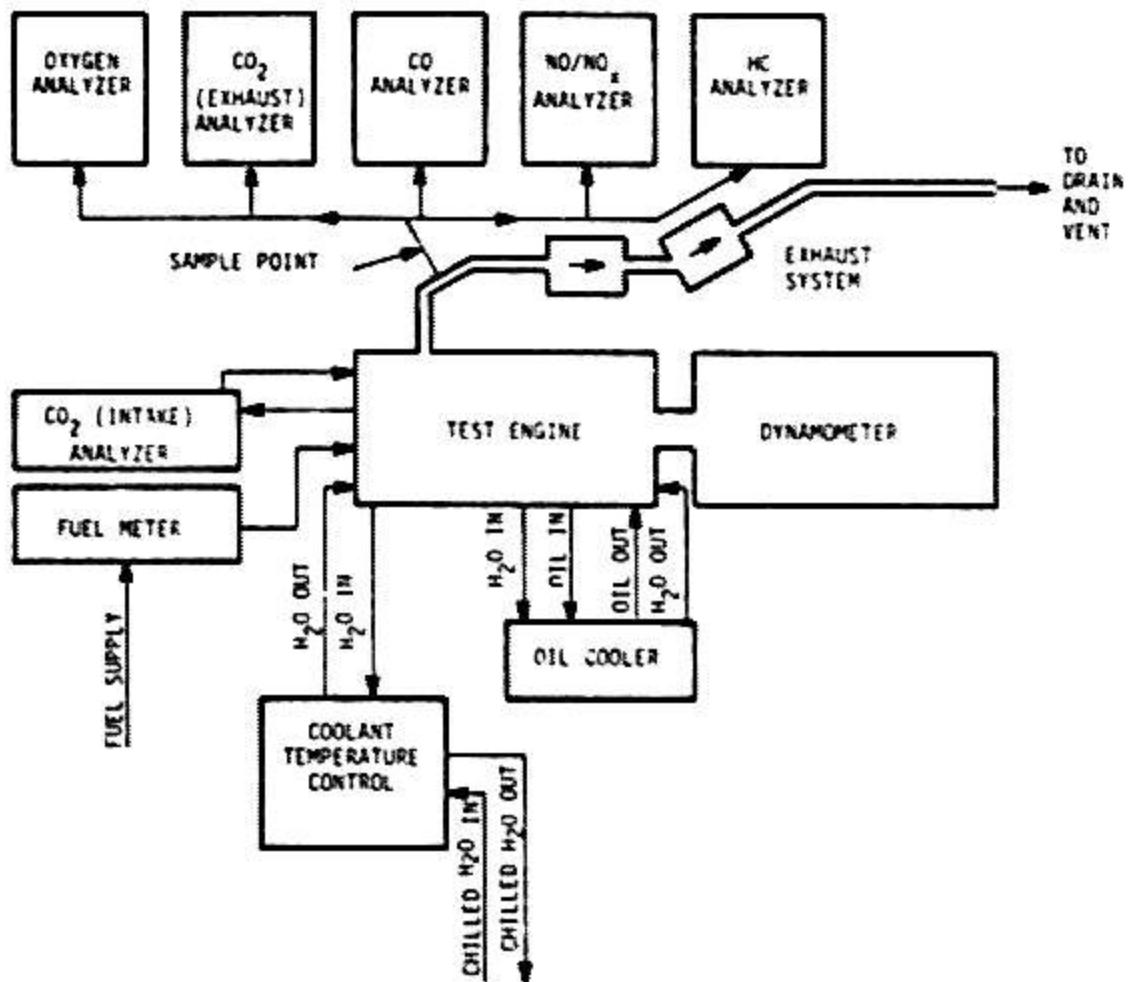


FIGURE 2. CELL NO. 2 TEST ENGINE FLUID FLOW

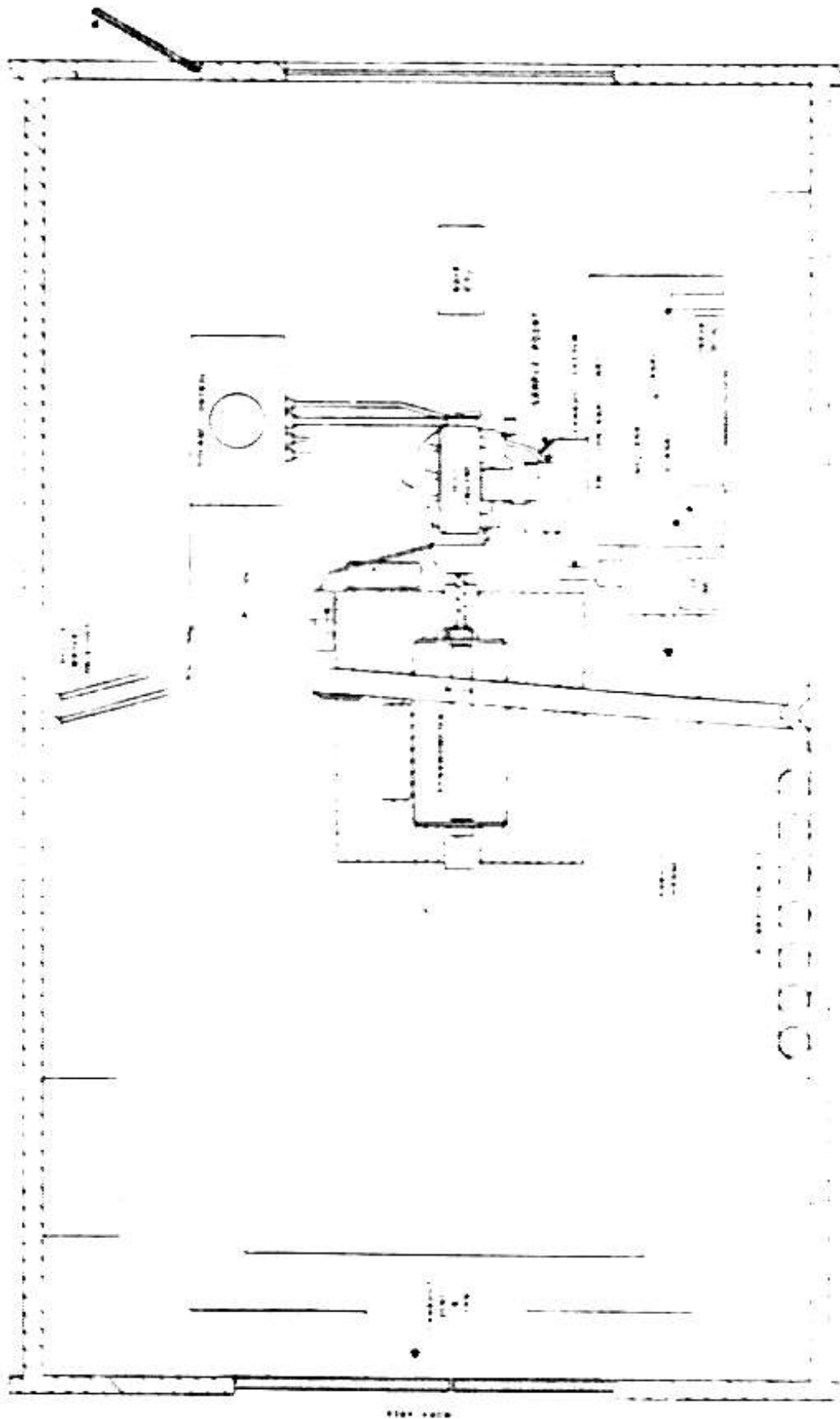


FIGURE 3. TEST CELL NO. 2 LAYOUT

Instead of the standard air cleaner, air induction was directed through a laminar-flow element connected by 4-inch ID plastic tubing to the carburetor. All engine vents (valve cover, carburetor, charcoal canister) were connected to the air-inlet system. Engine coolant and oil temperatures were maintained at $185^{\circ}\text{F} \pm 2^{\circ}\text{F}$ by external heat exchangers. Although all emissions measurements were made before the catalyst, it, as well as a muffler, were installed in the exhaust system in order to duplicate the normal engine back-pressure.

2.2.1 Instrumentation

Real-time measurements of emissions and engine performance were accomplished by the analog instrumentation shown in Table 4.

2.2.2 Data Acquisition

The data acquisition system was Hewlett-Packard 21MX mini-computer with a 45kHz A/D converter and multiplexer. Analog signals from the instrumentation shown in Table 4 were routed, along with digital speed and torque signals, to this computer. The data was continuously updated on a video display and line printer. Data was stored on a disc for subsequent reduction.

2.3 BASELINE TEXT MATRIX

The baseline data for this engine was collected by operating the engine in the steady-state mode with the factory calibrations of air-to-fuel ratio (A-F), spark advance (SA), and exhaust gas recirculation (EGR). The spark timing, distributor advance characteristics are shown in Figure 4. Figure 5 gives the EGR valve displacement versus actuation pressure. During these baseline tests the A-F varied between 13.2 and 19.8, spark advance from 10° to 24° BTDC, and EGR from 0.6% to 16.8%.

The test matrix consisted of 57 speed/load points from 750 rpm to 3600 rpm, as shown in Table 5. In general, these points correspond to 0%, 25%, 50%, 75%, and 100% of maximum positive torque and 25% and 75% of maximum negative torque. (Negative torque is obtained by motoring the powered engine with the dynamometer, thus simulating deceleration.

TABLE 4. ANALOG INSTRUMENTATION

MEASURED VARIABLE	INSTRUMENT TYPE
Oil temp.	OMEGA type K thermocouple; CJ compensator
Ambient temp.	YSI Model 46T6 Tele-thermometer
Inlet air flow	MERRIAM 50MC2-4 Laminar flow element
Inlet air diff. press.	MKS Baratron type 77
Air inlet temp.	OMEGA type K thermocouple; CJ compensator
Fuel inlet temp.	OMEGA type K thermocouple; CJ compensator
Coolant inlet temp.	OMEGA type K thermocouple; CJ compensator
Relative/Humidity	WEATHERMEASURE Model HM111
Exhaust CO	BECKMAN 864 Infrared Analyzer
Exhaust CO ₂	BECKMAN 864 Infrared Analyzer
Exhaust HC	BECKMAN 402 Hydrocarbon Analyzer
Exhaust NOx	BECKMAN 951 Chemiluminescent Analyzer
Exhaust O ₂	BECKMAN 14330 Paramagnetic Analyzer
Intake CO ₂	BECKMAN 864 Infrared Analyzer
Manifold vacuum	TYCO type AB 15 PSI transducer
Coolant exhaust temp.	OMEGA type K thermocouple; CJ compensator
Spark timing	1.8K precision potentiometer
Peak cylinder press.	KISTLER 538A/601B1 Piezoelectric
Exhaust temp. AC	OMEGA type K thermocouple; CJ compensator
Exhaust temp. BC	OMEGA type K thermocouple; CJ compensator
Exhaust press. AC	TYCO type AB 6 PSI transducer
Exhaust press. BC	TYCO type AB 6 PSI transducer

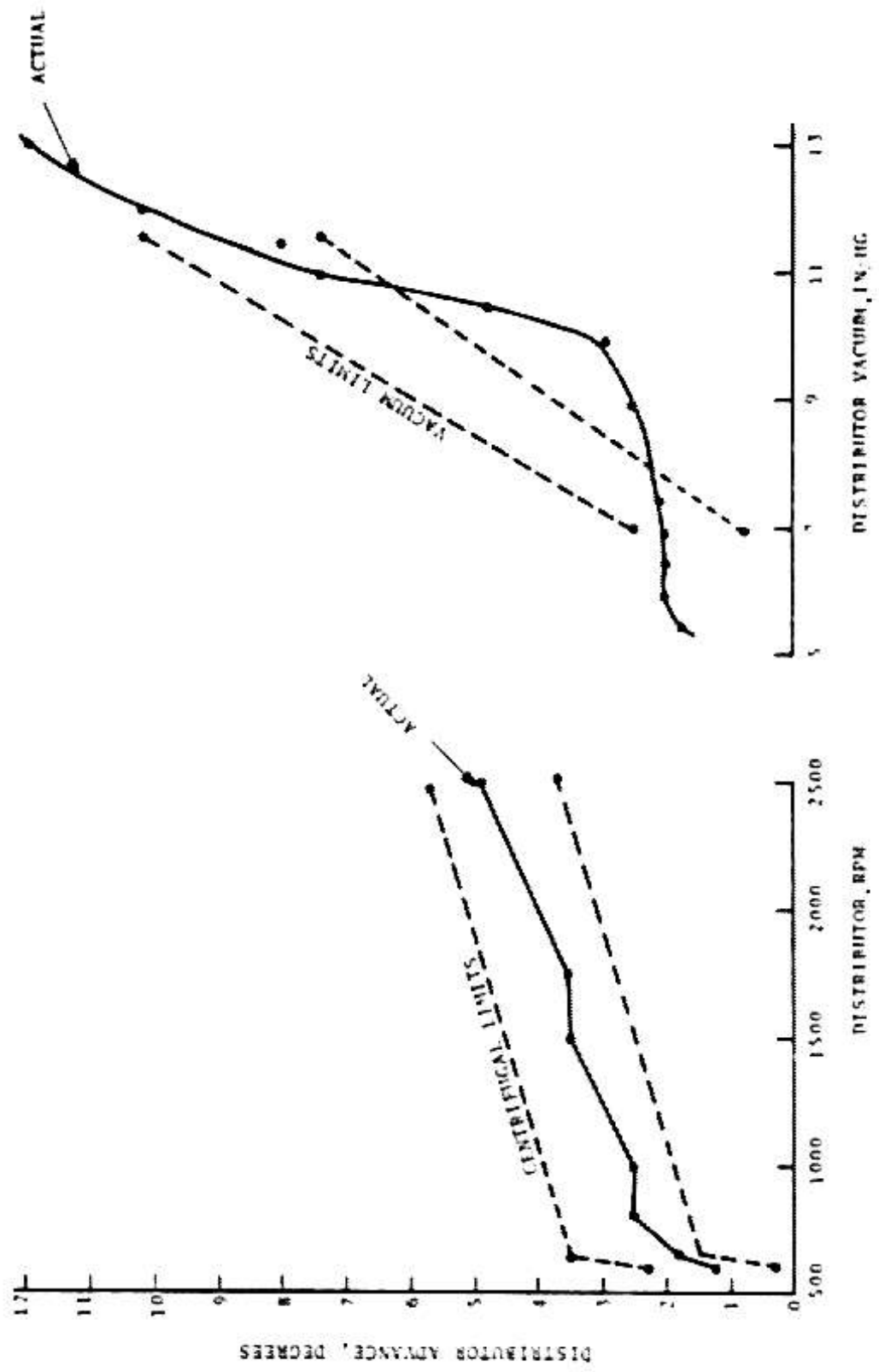


FIGURE 4. DISTRIBUTOR ADVANCE CHARACTERISTICS

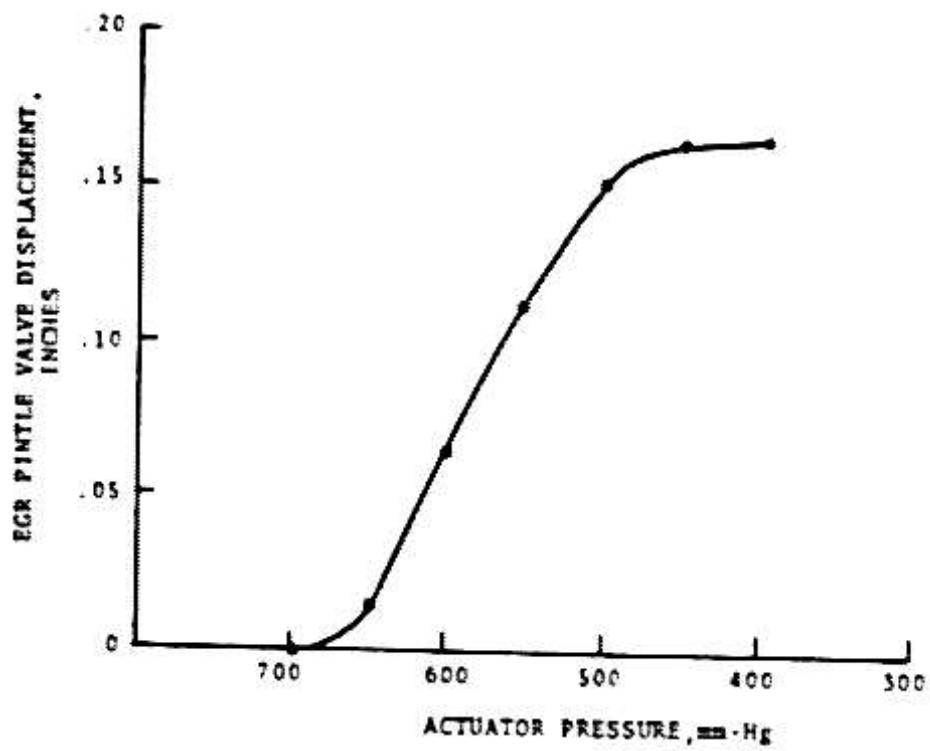


FIGURE 5. MEASURED VACUUM ACTUATOR

TABLE 5. STEADY-STATE BASELINE MAPPING SPEED-TORQUE VALUES

ENGINE SPEED, (RPM)	TORQUE, (LB-FT)									
750	-7,	0,	40							
880	-10,	-2,	0,	40,	80,	120,	160			
1000	-15,	-10,	-5,	0,	40,	80,	120,	160		
1500	-25,	-10,	-5,	0,	40,	80,	120,	160		
2000	-32,	-7,	0,	40,	80,	120,	160			
2500	-30,	-10,	0,	40,	80,	120,	160			
3000	-40,	-30,	-10,	0,	40,	60,	80,	120,	160	
3600	-48,	-36,	-12,	0,	35,	70,	105,	140		

3. TEST PROCEDURES

All instrumentation was periodically checked and calibrated. Emissions instrumentation was calibrated before and after data collection at each power point, or every 30 minutes whichever came first. At each baseline test point, sufficient time was allowed for the operating temperatures and pressures to stabilize (typically 5 to 45 minutes) before data was collected. Each data channel was sampled 30 times in approximately 5 seconds and the data averaged.

4. DATA REDUCTION

The data acquisition system sampled the signals from the analog instrumentation shown in Table 4. All samples in each data set (speed/load point) were averaged and stored on the HP-21MX disc. Test variables were also displayed to the operator by video display and line-printer. The stored disc-data was subsequently transferred to magnetic tape for further reduction on a PDP-10 computer. All corrections to the test data and mass emissions and fuel-flow calculations were performed on the PDP-10 using the equations shown in Appendix A.

All corrected data was printed out in the format of Table B-1. The data includes Engine Speed (RPM), Load (torque) (lb-ft), the % EGR, the Air-Fuel Ratio (A/F) from exhaust and fuel-flow calculations, the exhaust concentrations (ppm or %), various temperatures and pressures, measured air flow to the engine (airflo), the humidity (grains/pound), and fuel flow (grams/second).

5. TEST RESULTS

Figure 6 gives the corrected bhp, torque, and BSFC at wide-open throttle (WOT) for this engine. The maximum horsepower and torque are within manufacturer's specifications. The BSFC is at a minimum at 1500 rpm. Figure 7 shows the fuel rate in lb/hr for all speed-load points. Figures 8 and 9 show the A-F ratio and EGR for all positive horsepower points. Distributor advance is shown in Figure 4, while CO, HC, and NOx mass emission rates as a functions of speed and load are given in Figures 10, 11, and 12.

At low power a lean mixture resulted in relatively low levels of CO and HC. At higher speeds and loads, with richer mixtures, CO and HC increased substantially. As expected, NOx increased at higher power points. In general, the results from this engine are typical of those obtained with a modern production engine. Attached as Appendix B is the test and reduced data for all positive and negative speed/load points.

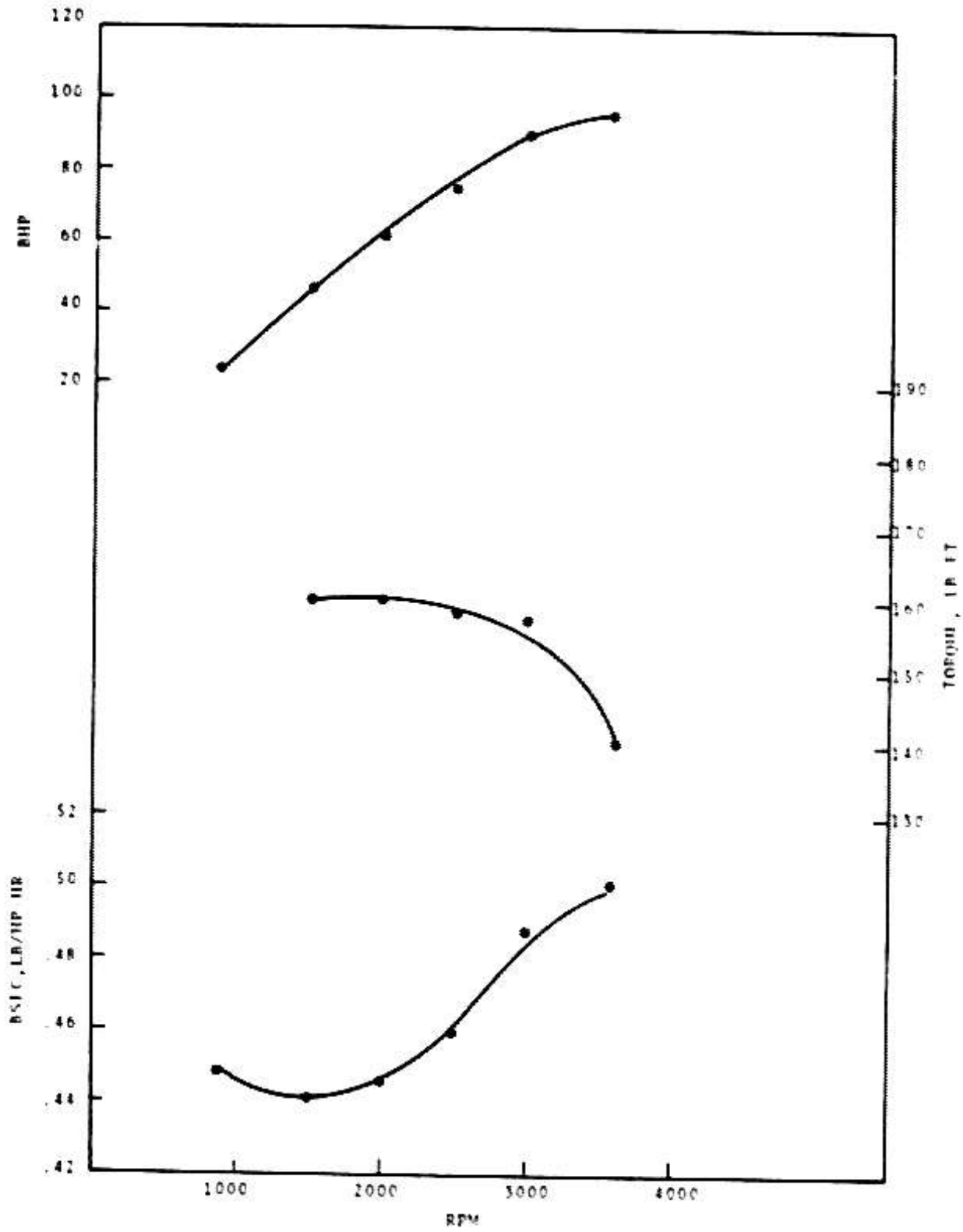


FIGURE 6. CORRECTED BHP, TORQUE, AND BSFC VS WIDE-OPEN THROTTLE

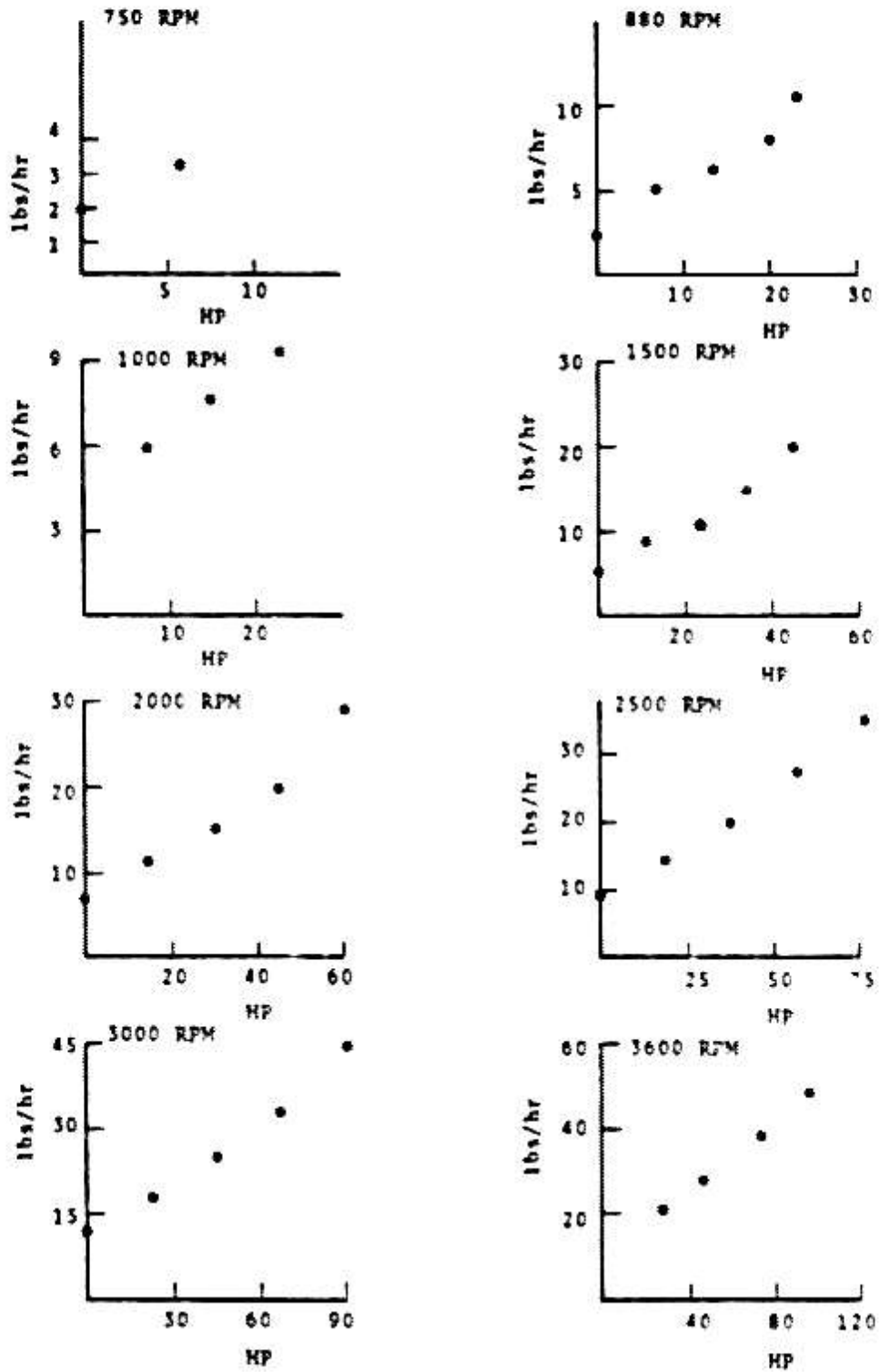


FIGURE 7. FUEL CONSUMPTION VS POWER

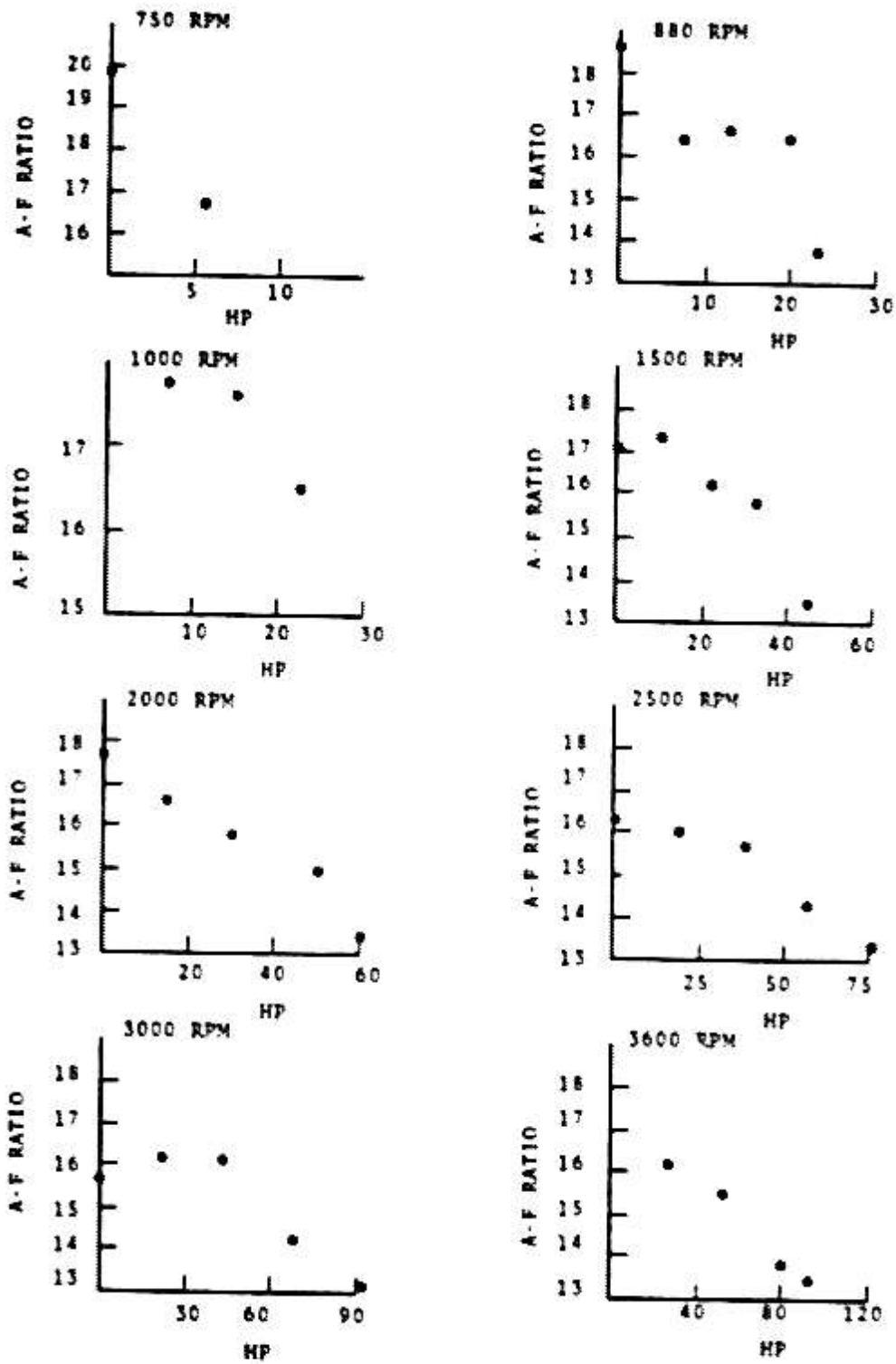


FIGURE 8. AIR-FUEL RATIO VS POWER

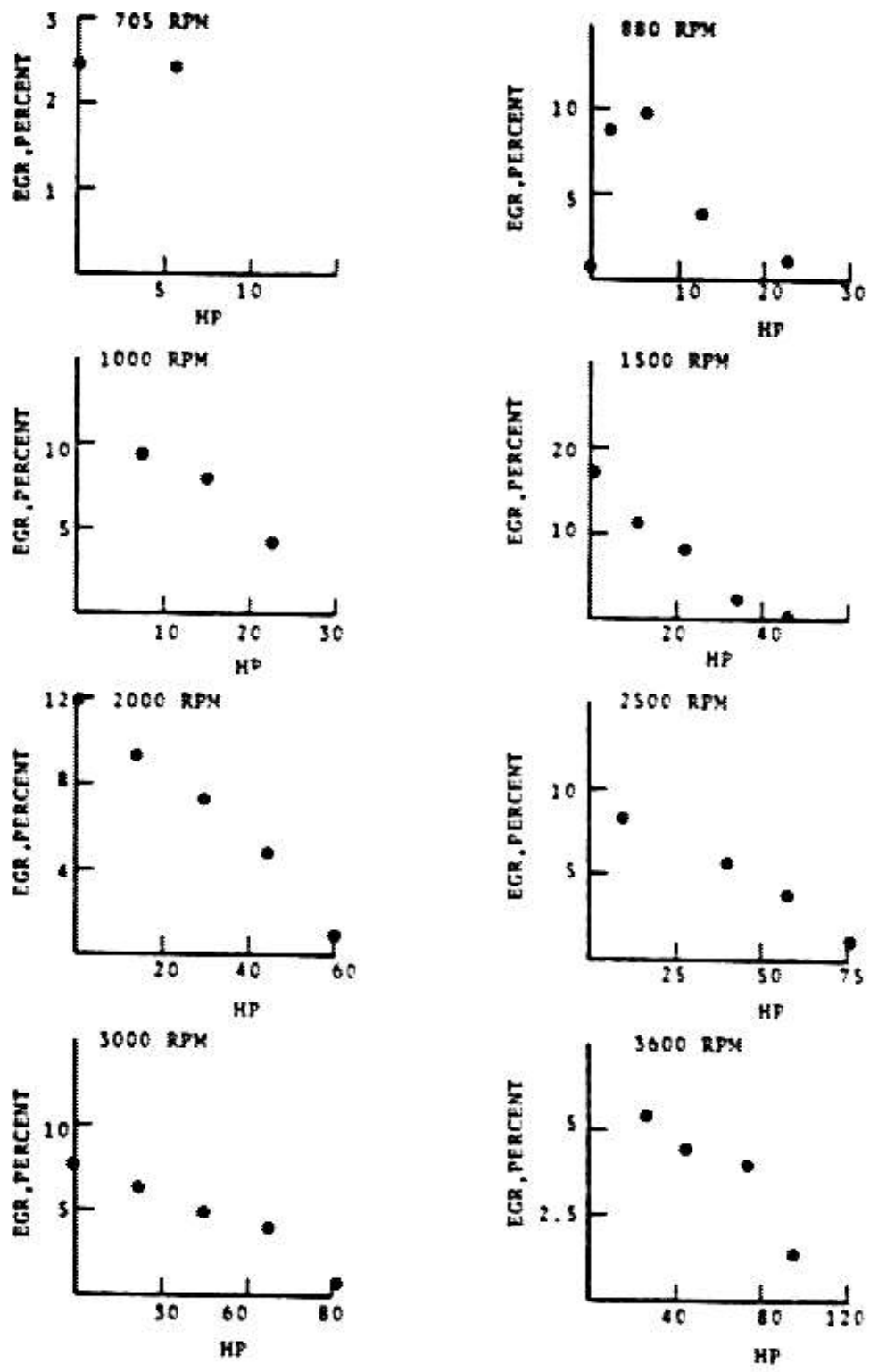


FIGURE 9. EGR VS POWER

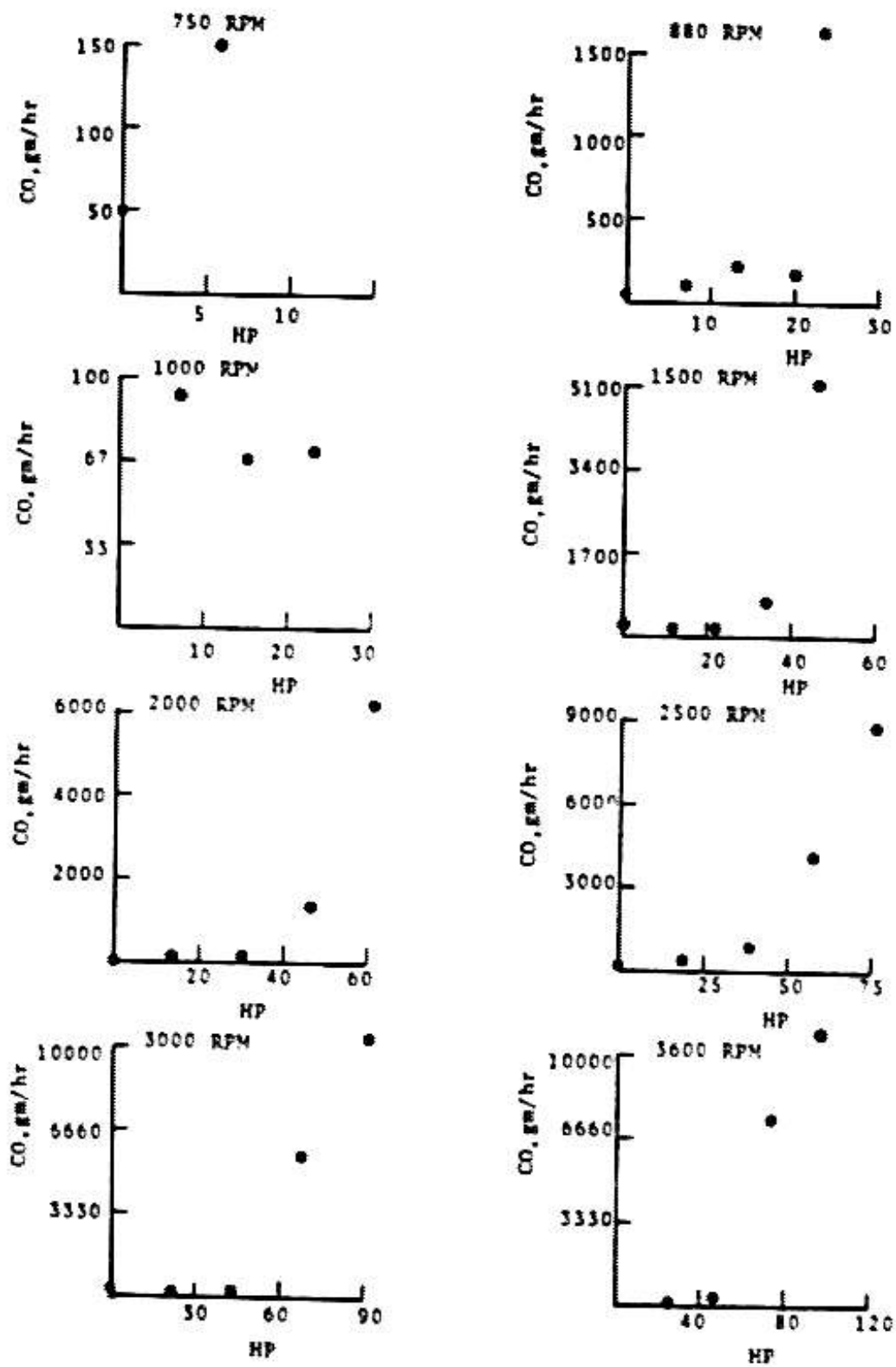


FIGURE 10. CO VS POWER

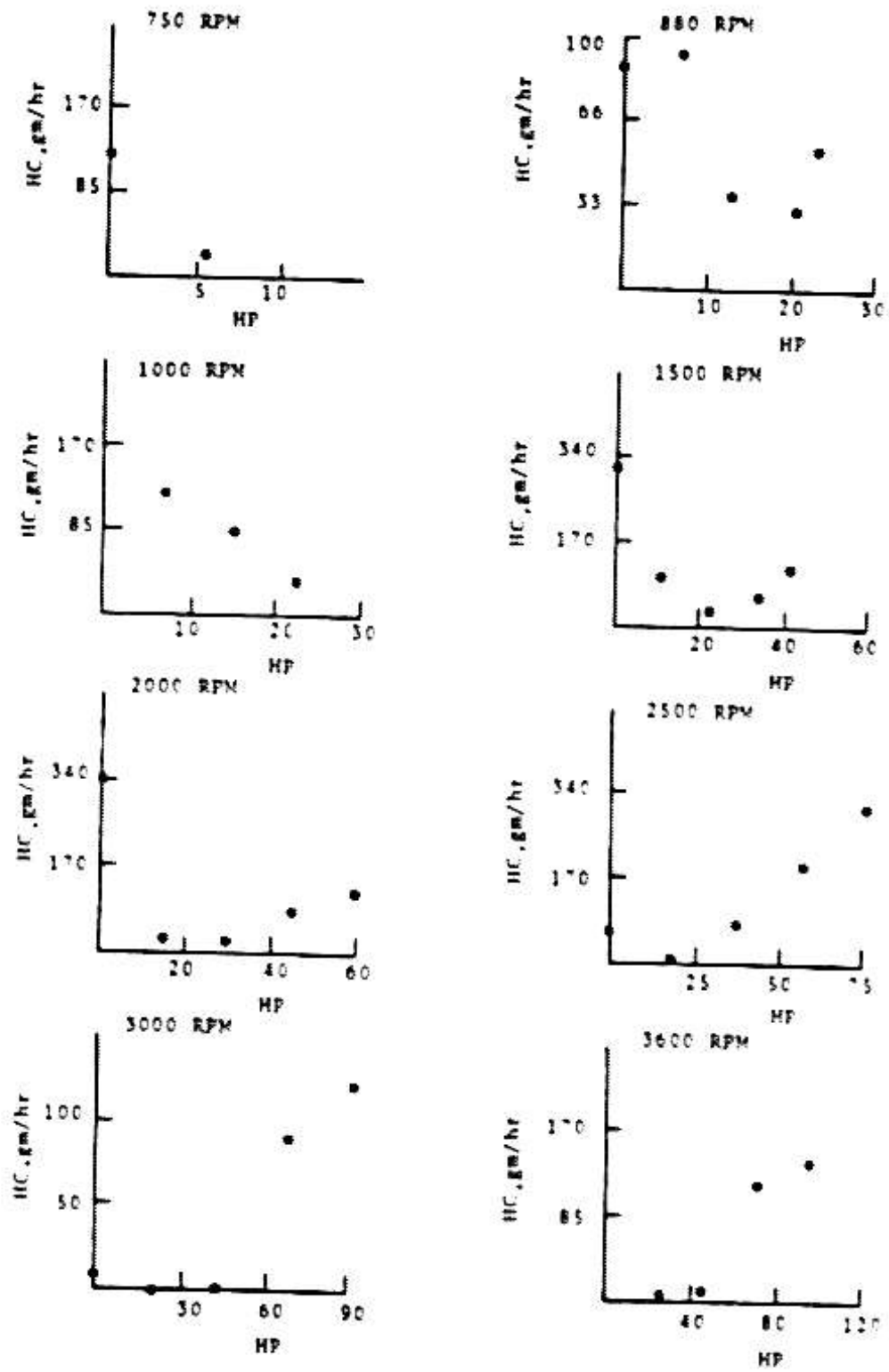


FIGURE 11. HC VS POWER

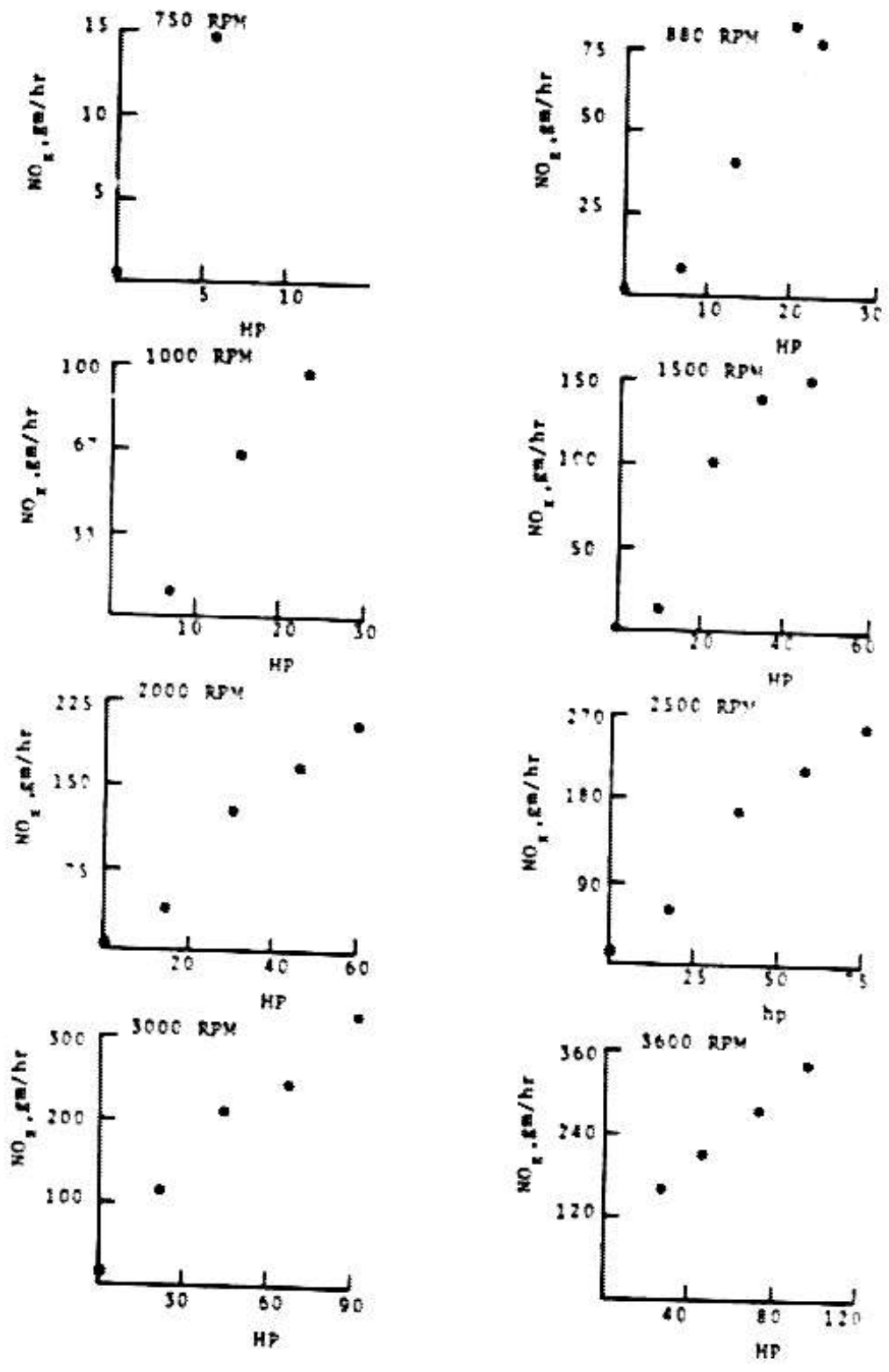


FIGURE 12. NO_x VS POWER

APPENDIX A DATA REDUCTION EQUATIONS

CORRECTED TORQUE, T_c (lb-ft) ⁽¹⁾ From SAE J245, Spark Ignition Engine Rating Code, adjusted to standard SAE ambient conditions

$$T_c = \frac{B_d^*}{B_{dt}} \left(\frac{t_t + A}{t^* + A} \right)^{1/2} T_t$$

where

- B_d^* = Standard Dry Barometric Pressure (29.92 in. Hg, 97.9 kPa)
- B_{dt} = Dry Barometric Pressure at Test Conditions
- t_t = Ambient Air Temperature at Test Conditions
- t^* = Standard Ambient Temperature (85°F, 29.4°C)
- A = Absolute Temperature Constant (460°R, 273°K)
- T_t = Measured Torque at Test Conditions.

CORRECTED HORSEPOWER, hp_c ⁽¹⁾ From SAE J245, Spark Ignition Engine Rating Code, adjusted to standard SAE ambient conditions:

$$hp_c = \frac{T_c N}{C}$$

where

- T_c = Corrected Torque (See above.)
- N = Engine Speed (RPM)
- C = Power Constant (3252 English, 955 SI).

(1) Engines with manifold preheated air inlet systems are designed to control carburetor air inlet temperature to a specific temperature. Excursions in ambient temperature below this value do not appreciably affect the controlled temperature. The engine performance correction factor as described in SAE J245 Engine Rating Code for Spark Ignition Engines has therefore been updated as follows: If ambient temperature is less than or equal to the manufacturer's stated controlled temperatures, no correction component involving carburetor inlet temperature is made. If ambient temperature exceeds the targeted controlled temperature, the normal J245 correction factor is applied with the targeted controlled temperature used in place of the standard ambient temperature.

MASS FUEL FLOW RATE (lb/hr) From volumetric measurement (corrected to 60°F per ASTM petroleum tables) and fuel specific gravity:

$$\dot{m}_f = \frac{(\text{SpG})_f \left(\frac{\text{lb H}_2\text{O}}{\text{vol}} \right) (\text{vol})_f}{\Delta t_T}$$

where

- \dot{m}_f = Fuel Flow Rate lb/hr
- $(\text{SpG})_f$ = Specific Gravity of Fuel
- $(\text{lb H}_2\text{O}/\text{vol})$ = Pounds of Water per Unit Volume
- $(\text{vol})_f$ = Volume of Fuel Measured, corrected to 60°F per ASTM petroleum tables
- Δt_T = Time interval of volume measurement (hrs.)

CORRECTED BRAKE SPECIFIC FUEL CONSUMPTION (BSFC) (lb/HP-hr)

$$\text{BSFC}_c = \frac{\dot{m}_f}{\text{HP}_c}$$

where

- BSFC_c = Corrected Brake Specific Fuel Consumption
- HP_c = Corrected Horsepower
- \dot{m}_f = Mass Fuel Flow Rate (lb/hr).

AIR/FUEL RATIO (A/F) Based on emissions measurements from SPINDT, SAE #650507:

$$A/F = F_b \left[11.49 F_c \left(\frac{1+R/2+Q}{1+K} \right) + \left(\frac{120(1-FC)}{3.5+K} \right) \right]$$

where

- $R = \frac{\% \text{CO}}{\% \text{CO}_2} = \frac{\text{Percent CO Concentration}}{\text{Percent CO}_2 \text{ Concentration}}$
- F_c = Mass Fraction of Carbon in Fuel
- $F_b = \frac{\% \text{CO} + \% \text{CO}_2}{\% \text{CO} + \% \text{CO}_2 + \% \text{CH}}$
- $Q = \frac{\% \text{O}_2}{\% \text{CO}_2} = \frac{\text{Percent O}_2 \text{ Concentration}}{\text{Percent CO}_2 \text{ Concentration}}$

CARBON MONOXIDE (CO) MASS EMISSION RATE (Grams/Hr)

$$\text{MASS CO} = (4.383) (\dot{m}_f) (A/F+1) (\% \text{CO}) \left[\frac{1}{1 + 0.03148 (\% \text{CO}_2) \left(\frac{\% \text{CO} + \text{CO}_2}{\% \text{CO} + 31 \text{CO}_2} \right)} \right]$$

where

- \dot{m}_f = Mass Fuel Flow Rate
- A/F = Air-to-Fuel Ratio
- % CO = Percent CO, Concentration
- % CO₂ = Percent CO₂, Concentration.

HYDROCARBON (HC) MASS EMISSION RATE (Grams/Hr)

$$\text{Mass HC} = (0.0002207) (\dot{m}_f) (A/F+1) (\text{ppm HC})$$

where

- \dot{m}_f = Mass Fuel Flow Rate
- A/F = Air-to-Fuel Ratio
- ppm HC = Parts per Million, HC Concentration.

OXIDES OF NITROGEN (NOx) MASS EMISSION RATE (Grams/Hr)

$$\text{Mass NOx} = 0.007201 (\dot{m}_f) (A/F+1) (\text{ppm NOx}) \left[\frac{1}{1 + .03148 (\% \text{CO}_2) \left(\frac{\% \text{CO} + \% \text{CO}_2}{\% \text{CO} + 31 \text{CO}_2} \right)} \right]$$

where

- \dot{m}_f = Mass Fuel Flow Rate
- A/F = Air-to-Fuel Ratio
- ppm NOx = Parts per Million, NOx Concentration
- % CO = Percent CO, Concentration
- % CO₂ = Percent CO₂, Concentration
- K_H = Humidity Correction Factor.

HUMIDITY CORRECTION FACTOR

$$K_H = \frac{1}{1 + 0.0047 (\text{Absolute Humidity} - 75)}$$

where absolute humidity is in grains/pound of dry air.

ABSOLUTE HUMIDITY (AH) (Grains/Lb. Dry Air):

$$AH = \frac{(RH) P_{SU}}{1.608 (P_{AMB} - RH \cdot P_{SU})}$$

where

- RH = Measured Relative Humidity
- P_{SU} = Saturated Vapor Pressure (from Keenan and Keyes Steam Tables)
- P_{AMB} = Ambient Barometric Pressure.

APPENDIX B
CHRYSLER 225 CID TEST DATA AND REDUCED TEST DATA

EXPLANATION OF DATA COLUMN HEADINGS

RPM	
CTORQ LB-FT	Torque corrected to standard conditions, SAE, J245
EGR	
A/FEX	Air-to-Fuel ratio Calculated using Spindt method
A/FTC LB/HR	Air-to-Fuel ratio Calculated using total carbon method
CNOX PPM	Oxides of nitrogen corrected for relative humidity
HC PPM	Hydrocarbons, parts per million
CO	Carbon monoxide, percent
CO2	Carbon dioxide, percent
O2	Oxygen, percent
COOLE DEG-F	Exit engine coolant to heat exchanger
EXOIL DEG-F	Exit engine oil to heat exchanger
AIRDP INH2O	Pressure differential across Merriam airflow sensor
AIRFLO LB/MIN	Engine inlet airflow
ABSHUM GR/LB	Grains per pound
FLO G/S	Measured fuel flow, grams per second

Note: Runs 1-85 were taken during warm-up.

TABLE B-1. CHRYSLER 225 CID TEST DATA (CONTD)

TEST RUN	MINIMUM LOAD (PSI)	ENGINE SPEED (RPM)	COOLANT TEMP (°F)	CRANK POSITION (°)	CRANK SPEED (RPM)	NO. OF TESTS	MAX. LOAD (PSI)	ENGINE SPEED (RPM)	COOLANT TEMP (°F)	CRANK POSITION (°)	CRANK SPEED (RPM)	NO. OF TESTS
414	1000	1800	165	3	198	105	1210	1800	175	3	216	105
415	1000	1800	165	3	198	105	1210	1800	175	3	216	105
416	1000	1800	165	3	198	105	1210	1800	175	3	216	105
417	1000	1800	165	3	198	105	1210	1800	175	3	216	105
418	1000	1800	165	3	198	105	1210	1800	175	3	216	105
419	1000	1800	165	3	198	105	1210	1800	175	3	216	105
420	1000	1800	165	3	198	105	1210	1800	175	3	216	105
421	1000	1800	165	3	198	105	1210	1800	175	3	216	105
422	1000	1800	165	3	198	105	1210	1800	175	3	216	105
423	1000	1800	165	3	198	105	1210	1800	175	3	216	105
424	1000	1800	165	3	198	105	1210	1800	175	3	216	105
425	1000	1800	165	3	198	105	1210	1800	175	3	216	105
426	1000	1800	165	3	198	105	1210	1800	175	3	216	105
427	1000	1800	165	3	198	105	1210	1800	175	3	216	105
428	1000	1800	165	3	198	105	1210	1800	175	3	216	105
429	1000	1800	165	3	198	105	1210	1800	175	3	216	105
430	1000	1800	165	3	198	105	1210	1800	175	3	216	105
431	1000	1800	165	3	198	105	1210	1800	175	3	216	105
432	1000	1800	165	3	198	105	1210	1800	175	3	216	105
433	1000	1800	165	3	198	105	1210	1800	175	3	216	105
434	1000	1800	165	3	198	105	1210	1800	175	3	216	105
435	1000	1800	165	3	198	105	1210	1800	175	3	216	105
436	1000	1800	165	3	198	105	1210	1800	175	3	216	105
437	1000	1800	165	3	198	105	1210	1800	175	3	216	105
438	1000	1800	165	3	198	105	1210	1800	175	3	216	105
439	1000	1800	165	3	198	105	1210	1800	175	3	216	105
440	1000	1800	165	3	198	105	1210	1800	175	3	216	105
441	1000	1800	165	3	198	105	1210	1800	175	3	216	105
442	1000	1800	165	3	198	105	1210	1800	175	3	216	105
443	1000	1800	165	3	198	105	1210	1800	175	3	216	105
444	1000	1800	165	3	198	105	1210	1800	175	3	216	105
445	1000	1800	165	3	198	105	1210	1800	175	3	216	105
446	1000	1800	165	3	198	105	1210	1800	175	3	216	105
447	1000	1800	165	3	198	105	1210	1800	175	3	216	105
448	1000	1800	165	3	198	105	1210	1800	175	3	216	105
449	1000	1800	165	3	198	105	1210	1800	175	3	216	105
450	1000	1800	165	3	198	105	1210	1800	175	3	216	105

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TABLE B-1. CHRYSLER 225 CID TEST DATA (CONTD)

ALL	ORIGINAL	TIME	RPM	EVAP	FCM	R/DIR	WT	CO	NOX	OZ	COALS	COALS	MIN	MIN	RANGE	MIN	MIN	MIN	DATE
NO	NO	MIN	PPM	PPM	(G/G)	(G/G)	PPM	%	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM
000	000304	0	181300	740	0	1.7	1.8	0	0	0	100	102	-	10	003	16	340	227	79
001	000305	0	181270	740	1	1.3	1.7	0	0	0	100	103	-	10	002	16	330	227	79
002	000306	0	181400	740	1	1.5	1.7	0	0	0	100	103	-	10	006	16	330	227	79
003	000307	0	181310	740	0	1.2	1.7	0	0	0	100	102	-	10	008	16	330	227	79
004	000308	0	181400	740	0	1.5	1.7	0	0	0	100	102	-	10	001	16	330	227	79
005	000309	0	181410	740	0	1.3	1.7	0	0	0	100	102	-	10	006	16	330	227	79

TABLE B-1. CHRYSLER 225 CID TEST DATA (CONTD)

NEGATIVE TORQUES

rpm	torque lb-ft	n/s in	meqnc rpm	accnt rpm	cofmc %	carcom %	aircom %	cool temp SEC F	coil temp SEC F	massflow LBS/MIN	BSMOR GPH
1500	-25.26	17.47	21.35	13381-05	6831	5.190	3.261	186.7	192.1	1623	49.24
1500	-16.22	14.22	21.56	61161-05	1818	8.718	8.615	186.7	196.4	2001	44.58
1500	-4.958	17.13	53.25	8886	1354	11.22	4.568	187.3	197.8	2268E-01	44.37
1000 0	-14.55	16.04	19.11	1193E-05	1.768	5.489	3.761	187.7	191.8	1107	65.26
1000 0	-5.626	18.77	77.98	9189	2.158	11.87	7.822	187.7	188.6	1238	45.63
850.7	-3.385	18.11	68.88	2534	3227	11.16	8.638	186.3	186.7	2254	45.18
2000	-22.24	17.94	15.84	13071-05	5378	3.385	3.899	187.1	212.3	1881	49.11
2000	-2.988	17.18	24.51	6041	3126	16.55	3.892	186.5	211.3	2.197	28.83
2500	-28.79	18.89	14.68	1249E-05	3781	8.148	7.452	187.8	223.8	1.878	28.85
2500	-18.88	17.87	38.88	4781	3858	11.88	8.938	187.4	226.4	2.613	49.74
3000	-68.81	19.19	11.85	12881-05	2127	8.852	6.374	188.8	235.8	3152	31.78
3000	-28.75	18.32	15.88	1161E-05	5194	8.288	5.971	188.8	238.2	1.748	18.82
3000	-8.737	15.78	65.81	359.8	1582	12.51	1.818	181.8	238.7	3.824	37.16
3500	-1559	15.34	137.1	13.42	887E-01	19.84	7.854	187.8	287.8	1.198	37.85
3600	-47.55	16.88	14.88	12781-05	2978	7.213	1.813	182.1	237.1	4.827	28.74
3500	-35.78	17.73	17.17	3337E-05	4372	9.531	13.37	182.3	238.1	2.884	37.81
3500	-11.88	18.84	84.45	1117	8761	12.55	1.855	183.8	268.5	3.288	68.43
410.8	-16.65	18.74	22.42	1881E-05	1.784	5.222	3.196	183.8	181.3	8828	19.89
410.7	-1.914	18.18	48.45	9381	3394	5.752	3.373	184.2	174.8	5384	67.41
3500 0	-7.872	18.23	15.74	1051E-05	3782	8.312	3.742	184.8	178.8	8884	33.18
178.8	-1.887	15.88	21.45	9.714	2816	8.198	6.114	182.5	177.7	5181	82.18

TABLE B-2. CHRYSLER 225 CID REDUCED TEST DATA.

RPM	CORRECTED TORQUE (LB-FT)	EGR (PERCENT)	AIR-FUEL RATIO	FUEL FLOW (LB/HR)	NO _x (GM/HR)	HC (GM/HR)	CO (GM/HR)
1133.3333	71.1100	6.2383	18.7700	8.4285	17.1817	15.2248	187.3754
1145.3333	61.1100	7.1333	18.7800	17.7333	17.9888	18.8107	116.3157
1157.3333	78.8933	7.5873	17.9333	17.1333	17.8188	28.8388	177.1343
1169.3333	74.1100	7.5600	18.5200	14.5585	123.8870	23.1936	186.3713
1181.3333	71.1100	7.1870	18.9933	17.3771	128.6213	23.1100	176.4883
1193.3333	81.2700	6.3573	18.7333	11.3133	37.2701	27.1287	177.3746
1205.3333	1.1863	12.0800	17.5600	7.3231	3.7751	337.8570	151.3885
1217.3333	117.1100	6.9200	17.9333	17.4200	167.7338	75.1788	1865.7213
1229.3333	143.1100	6.8974	17.8333	27.1871	238.1813	198.7837	8238.5333
1241.3333	178.1100	1.0470	17.3633	17.3833	75.5578	137.5217	8933.4883
1253.3333	121.1100	1.4340	18.7833	27.3633	711.5837	82.7813	9152.3200
1265.3333	67.1100	5.6271	18.8700	23.1833	168.5770	71.2828	854.8100
1277.3333	81.1100	8.2210	17.1100	17.8457	89.2957	72.1810	377.8081
1289.3333	1.1100	13.1833	18.1100	4.7333	11.8117	26.1173	288.4201
1301.3333	141.3133	3.8004	17.7633	20.1851	187.8971	177.3168	5238.3883
1313.3333	170.8133	3.8134	17.1100	23.2888	153.1007	131.2788	5387.8883
1325.3333	171.1100	0.8818	17.5633	13.3333	168.8813	132.3207	8138.3213
1337.3333	67.3133	8.7303	18.3333	17.4153	133.5888	27.2810	187.5138
1349.3333	87.7100	19.3100	17.8300	6.3731	11.8371	135.7131	187.8811
1361.3333	7.1100	16.8000	17.3100	7.6287	1.7888	137.1881	237.8701
1373.3333	177.1100	3.8864	17.3100	17.1888	124.1817	127.3733	1016.8113
1385.3333	157.8300	1.8873	18.3733	12.8857	227.3818	88.7888	8977.8883
1397.3333	78.1100	6.6733	17.1100	18.8933	72.3833	7.7781	81.1133
1409.3333	11.8800	6.3888	18.7833	18.7887	131.1370	1.7887	77.7818
1421.3333	71.3300	8.8688	17.1100	17.8888	157.3817	1.7887	132.1331
1433.3333	7.1100	7.1700	17.7800	18.7133	18.8810	7.1158	277.1100
1445.3333	187.1100	1.8183	17.8700	18.8881	181.1100	182.8137	13846.1133
1457.3333	157.1100	3.8010	17.8300	17.2178	278.8374	198.7788	7178.8813
1469.3333	67.1100	6.8273	17.7333	27.1113	223.7700	6.3887	372.3788
1481.3333	77.7800	7.3710	17.3500	22.7037	184.3718	1.7887	87.7813
1493.3333	123.1100	1.8220	18.7833	12.2757	231.7817	177.1233	1818.7883
1505.3333	121.1100	3.8893	18.4700	12.8351	238.1817	138.8188	3667.2113
1517.3333	177.1100	8.2743	17.5333	18.8733	132.8370	52.8011	732.8733
1529.3333	117.3100	3.1880	18.8833	7.8818	87.8888	72.1187	67.8873
1541.3333	77.1100	6.7887	17.4133	1.1287	83.2887	77.2887	73.8817
1553.3333	177.1100	1.8750	18.8500	17.1813	187.3771	87.8813	378.1100
1565.3333	121.1100	8.1810	18.7333	7.1233	91.2887	77.1887	73.1100
1577.3333	87.2833	7.1210	17.8100	7.1788	62.8138	77.2771	76.3788
1589.3333	37.1100	6.3733	17.2100	5.8731	3.8817	117.7457	6.8888
1601.3333	37.1100	8.8733	18.8133	7.1168	8.8733	81.3888	138.8718
1613.3333	111.1100	1.0180	17.7100	17.8788	76.7817	82.3771	1411.3771
1625.3333	7.1100	3.1581	18.7133	1.8881	3.1818	17.1188	81.1817
1637.3333	7.1100	3.8384	18.8633	7.8788	1.7217	77.1788	81.1788
1649.3333	87.1100	3.1323	18.7800	7.7768	1.8887	81.8771	81.1788
1661.3333	87.1100	3.8374	18.3100	7.8821	2.1788	87.7817	87.0771
1673.3333	11.1100	3.8137	18.7333	2.1788	1.8771	78.1817	87.8817
1685.3333	11.1100	3.8110	17.7833	2.1878	18.7217	72.1187	187.3817
1697.3333	17.1100	2.8870	18.8733	7.8871	11.7317	27.1817	182.2887
1709.3333	1.1100	2.8720	17.8500	17.5731	3.6818	118.8100	81.1100

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