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DT-HS-807-055  
DT-TSC-NHTSA-86-3

# Vehicle Component Characterization

## Vol. II: Data Appendices

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January 1987  
Final Report

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U.S. Department of Transportation  
**National Highway Traffic Safety  
Administration**

Office of Research and Development  
Office of Crashworthiness Research  
Washington DC 20590

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16. Abstract MGA Research Corporation has undertaken a project sponsored by the Transportation Systems Center of the U.S. Department of Transportation which involved the quasi-static and dynamic testing of automobile instrument panels and windshields. During the instrument panel testing phase of this project, the instrument panels of 19 vehicles were tested for their stiffness characteristics using procedures developed under a previous study. (This testing attempted to simulate loadings which occur during frontal collisions and includes contacts of knees to lower instrument panel sections, torso to mid-section and head to upper section.) Also included in the instrument panel testing were parametric tests investigating the effects of different loading geometry. The windshield testing portion of this project included developing a procedure for the testing of windshields as they would be loaded under frontal collision conditions (head/windshield contact) through static and dynamic testing of the windshields of the 19 vehicles used in the instrument panel testing. During the procedural study, it was determined that only dynamic impacts properly duplicate the loading conditions found during an accident. Also carried out during the windshield testing was a parametric study into the effects of different loading and physical conditions. The purpose of this testing was to develop a set of data which could be used in computer crash occupant simulation models in order to study automobile crashworthiness. The data generated by this testing has been used to develop a data base on the National Highway Traffic Safety Administration's VAX 11/780 computer. The data presented in this report are directly available to anyone having access to the NHTSA computer. This report is presented in two volumes: Volume I Project Results Volume II Data Appendices					
17. Key Words Instrument Panel Stiffness Characteristics Windshield Stiffness Characteristics Computer Simulation Computer Database Crashworthiness				18. Distribution Statement DOCUMENT IS AVAILABLE TO THE PUBLIC THROUGH THE NATIONAL TECHNICAL INFORMATION SERVICE, SPRINGFIELD, VIRGINIA 22161	
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## PREFACE

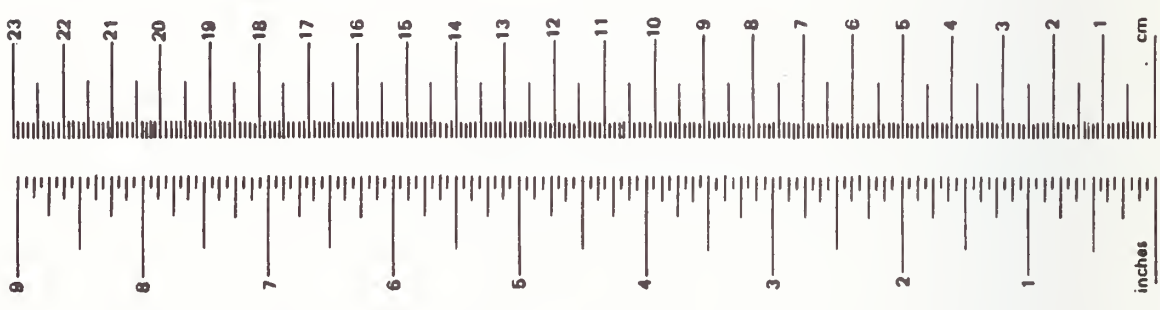
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This report is presented in two volumes: Volume I Project Results  
Volume II Data Appendices

We would like to thank Daniel Cohen of the National Highway Traffic Safety Administration, and Herbert Gould and Lawrence Simeone of the Transportation Systems Center for their support.

# METRIC CONVERSION FACTORS

Approximate Conversions to Metric Measures				Approximate Conversions from Metric Measures			
Symbol	When You Know	Multiply by	To Find	Symbol	When You Know	Multiply by	To Find
<b>LENGTH</b>							
in	inches	2.5	centimeters	mm	millimeters	0.04	inches
ft	feet	30	centimeters	cm	centimeters	0.4	inches
yd	yards	0.9	meters	m	meters	3.3	feet
mi	miles	1.6	kilometers	km	kilometers	1.1	yards
						0.6	miles
<b>AREA</b>							
in <sup>2</sup>	square inches	6.5	square centimeters	cm <sup>2</sup>	square centimeters	0.16	square inches
ft <sup>2</sup>	square feet	0.09	square meters	m <sup>2</sup>	square meters	1.2	square yards
yd <sup>2</sup>	square yards	0.8	square meters	km <sup>2</sup>	square kilometers	0.4	square miles
mi <sup>2</sup>	square miles	2.6	square kilometers	ha	hectares (10,000 m <sup>2</sup> )	2.5	acres
	acres	0.4	hectares				
<b>MASS (weight)</b>							
oz	ounces	28	grams	g	grams	0.035	ounces
lb	pounds (2000 lb)	0.45	kilograms	kg	kilograms	2.2	pounds
		0.9	tonnes	t	tonnes (1000 kg)	1.1	short tons
<b>VOLUME</b>							
tp	teaspoons	5	milliliters	ml	milliliters	0.03	fluid ounces
Tbsp	tablespoons	15	milliliters	l	liters	2.1	pints
fl oz	fluid ounces	30	milliliters	l	liters	1.06	quarts
c	cups	0.24	liters	l	liters	0.26	gallons
pt	pints	0.47	liters	m <sup>3</sup>	cubic meters	36	cubic feet
qt	quarts	0.96	liters	m <sup>3</sup>	cubic meters	1.3	cubic yards
gal	gallons	3.8	liters				
ft <sup>3</sup>	cubic feet	0.03	cubic meters				
yd <sup>3</sup>	cubic yards	0.76	cubic meters				
<b>TEMPERATURE (exact)</b>							
of	Fahrenheit temperature	5/9 (after subtracting 32)	Celsius temperature	of	Celsius temperature	9/5 (then add 32)	Fahrenheit temperature



1 in. = 2.54 cm (exactly). For other exact conversions and more detail tables see NBS Misc. Publ. 286, Units of Weight and Measure, Price \$2.25 SD Catalog No. C13 10 286.

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APPENDIX A

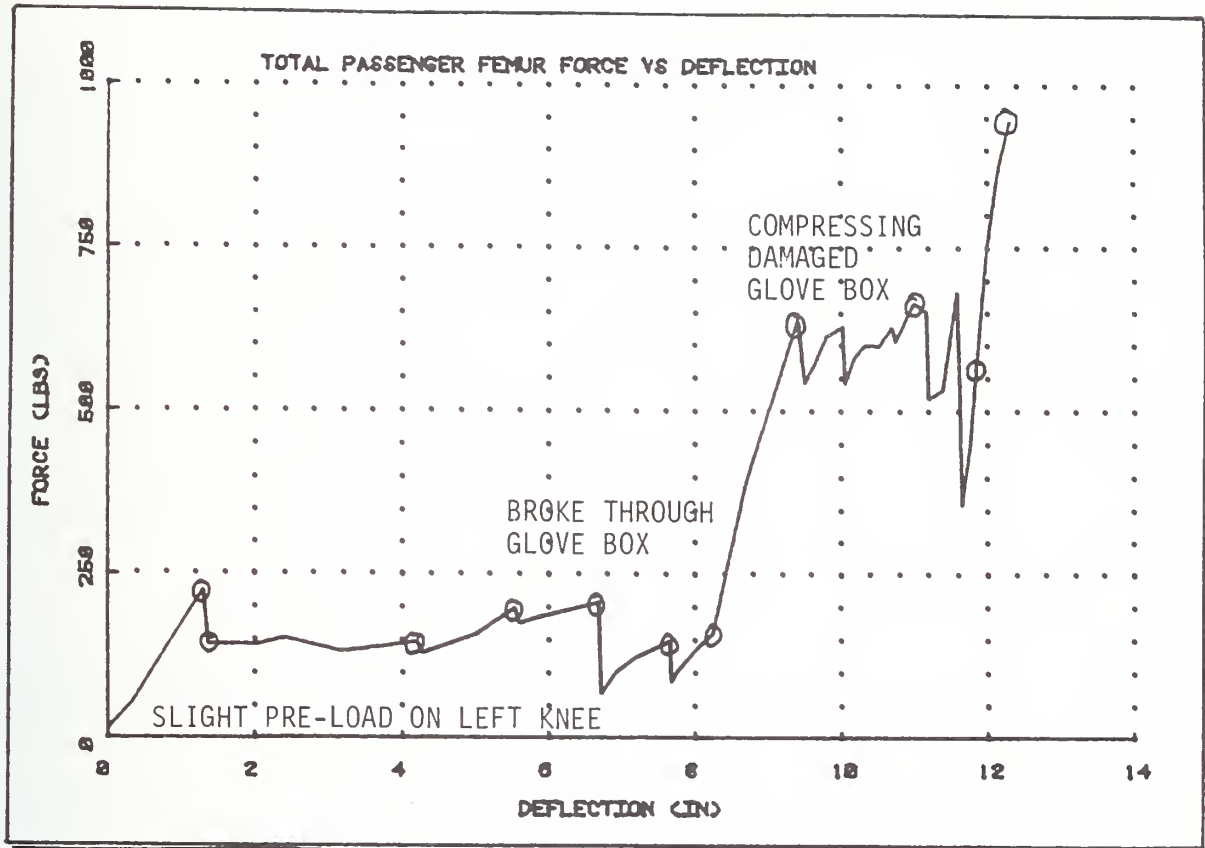
STATIC INSTRUMENT PANEL TEST RESULTS



Test: Passenger Side Femur (static) Date: July 27, 1984

Vehicle: 1977 Plymouth Volare

Options: Metal dash top



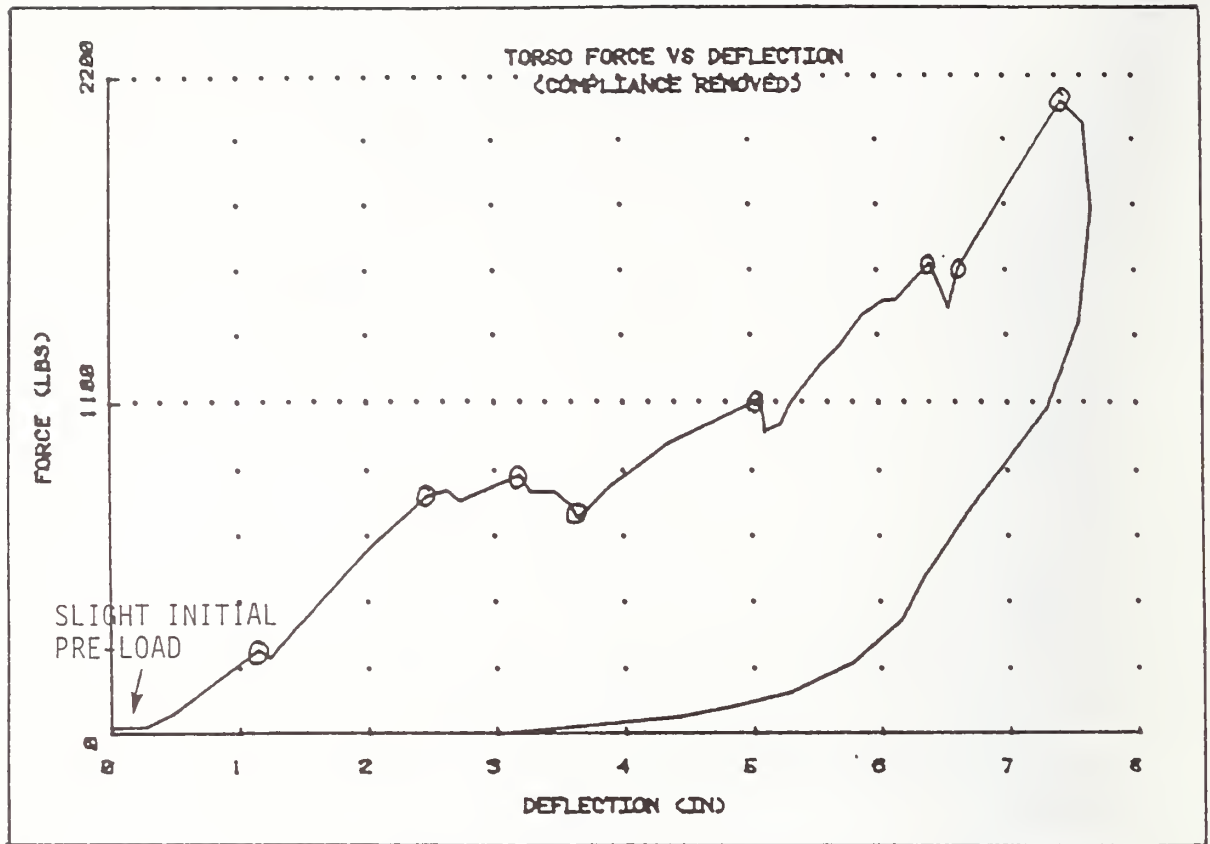
G= 0.920 R= 0.112 K= 1503

c= 1.55  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 18.60  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.00</u>	<u>0.00</u>	<u>11.80</u>	<u>623.36</u>
<u>1.25</u>	<u>221.44</u>	<u>12.28</u>	<u>943.36</u>
<u>1.32</u>	<u>135.68</u>		
<u>4.12</u>	<u>140.80</u>		
<u>5.51</u>	<u>199.68</u>		
<u>6.63</u>	<u>199.68</u>		
<u>7.67</u>	<u>144.64</u>		
<u>8.22</u>	<u>160.00</u>		
<u>9.41</u>	<u>640.00</u>		
<u>11.02</u>	<u>664.32</u>		

Test: Torso (static) Date: July 27, 1984  
 Vehicle: 1977 Plymouth Volare  
 Options: Metal dash top



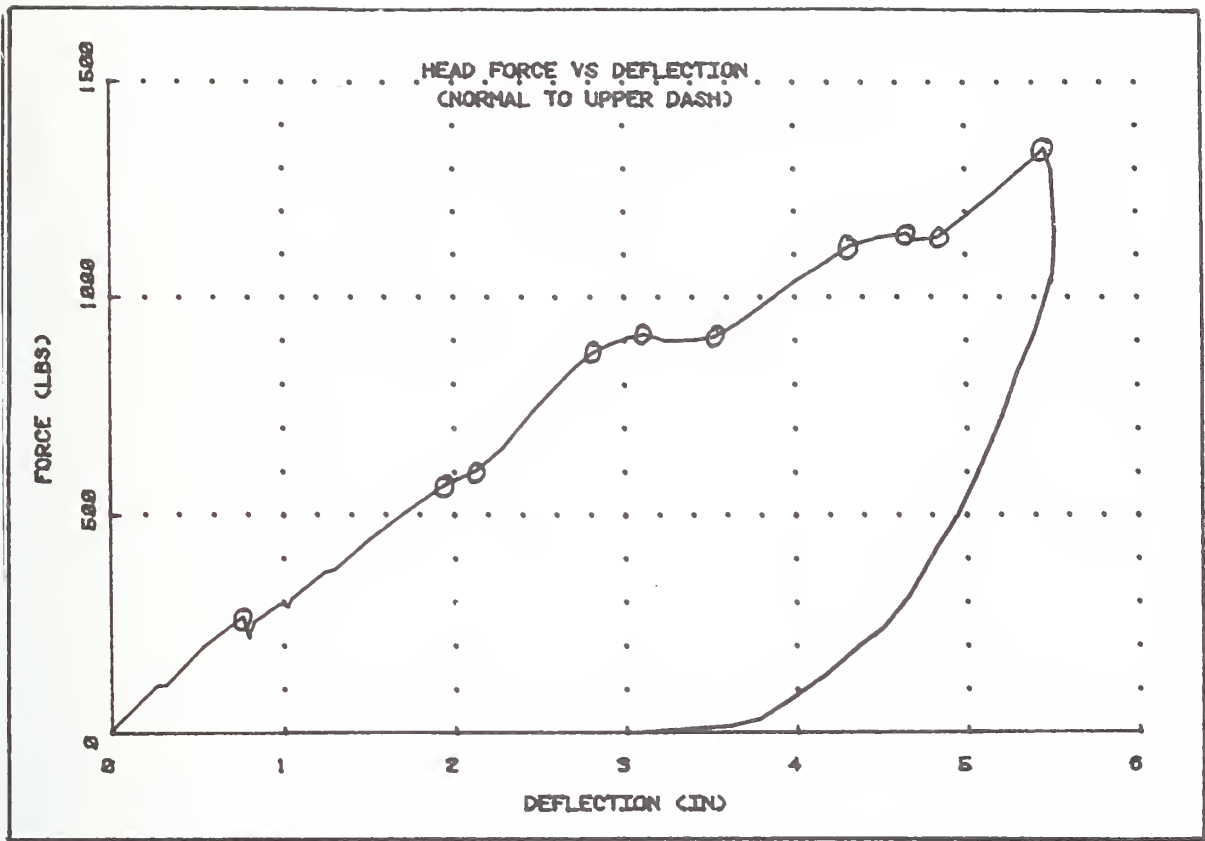
G= 0.408 R= 0.234 K= 2112  
 c= 0.57  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_  
 $\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 6.84  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.00</u>	<u>0.00</u>	_____	_____
<u>1.15</u>	<u>278.78</u>	_____	_____
<u>2.47</u>	<u>794.11</u>	_____	_____
<u>3.19</u>	<u>870.14</u>	_____	_____
<u>3.63</u>	<u>715.26</u>	_____	_____
<u>5.07</u>	<u>1109.50</u>	_____	_____
<u>6.42</u>	<u>1560.06</u>	_____	_____
<u>6.62</u>	<u>1548.80</u>	_____	_____
<u>7.45</u>	<u>2120.44</u>	_____	_____

Test: Head (static) Date: July 27, 1984

Vehicle: 1977 Plymouth Volare

Options: Metal dash top



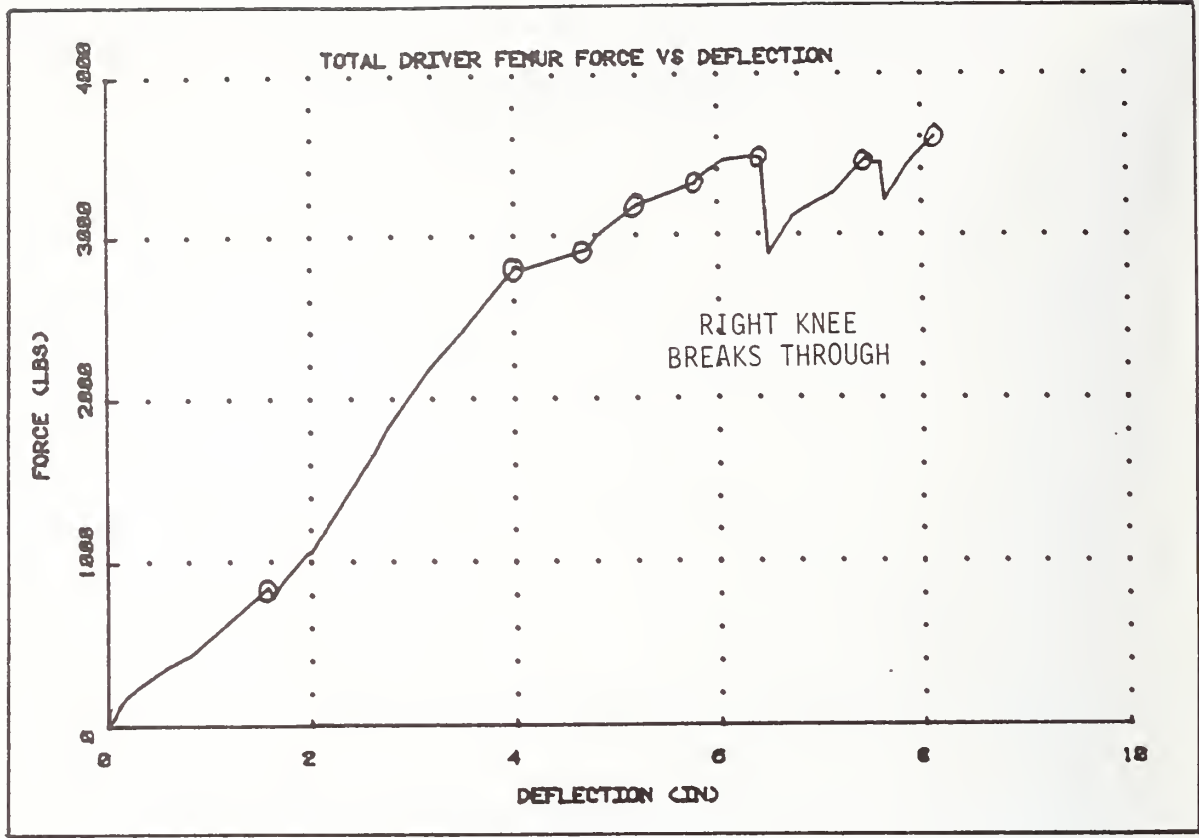
G= 0.563 R= 0.173 K= 973

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.00</u>	<u>0.00</u>	<u>5.45</u>	<u>1345.93</u>
<u>0.75</u>	<u>264.96</u>	_____	_____
<u>1.94</u>	<u>572.16</u>	_____	_____
<u>2.12</u>	<u>600.96</u>	_____	_____
<u>2.81</u>	<u>877.44</u>	_____	_____
<u>3.11</u>	<u>913.92</u>	_____	_____
<u>3.50</u>	<u>906.24</u>	_____	_____
<u>4.31</u>	<u>1123.20</u>	_____	_____
<u>4.64</u>	<u>1144.32</u>	_____	_____
<u>4.85</u>	<u>1144.32</u>	_____	_____

Test: Driver Side Femur (static) Date: July 27, 1984  
 Vehicle: 1977 Plymouth Femur  
 Options: Metal dash top



G= 0.860 R= 0.052 K= 2466  
 c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_  
 $\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

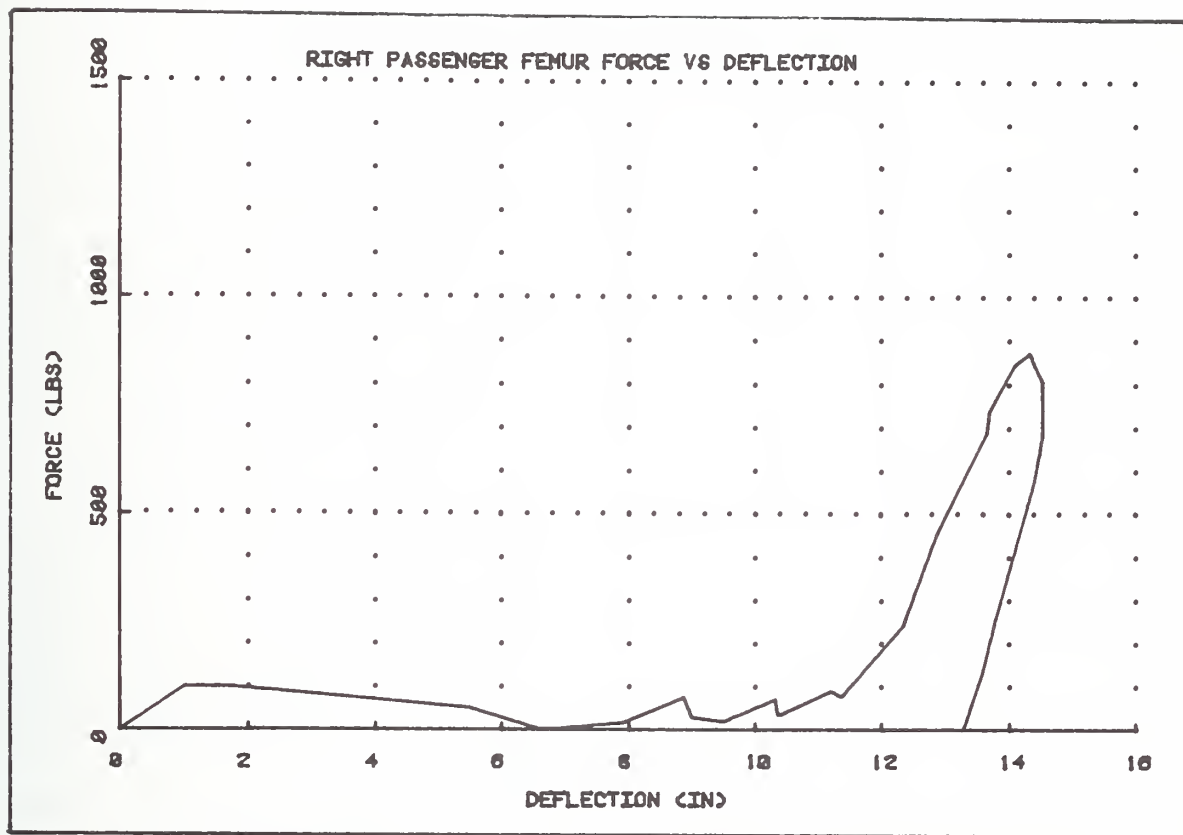
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
0.00	0.00		
1.54	824.32		
3.94	2800.64		
4.69	2997.92		
5.19	3179.52		
5.74	3358.72		
6.44	3476.48		
7.44	3476.48		
8.14	3614.72		

Test Right Passenger Femur

Date: July 27, 1984

Vehicle: 1977 Plymouth Volare

Options: Metal dash top



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

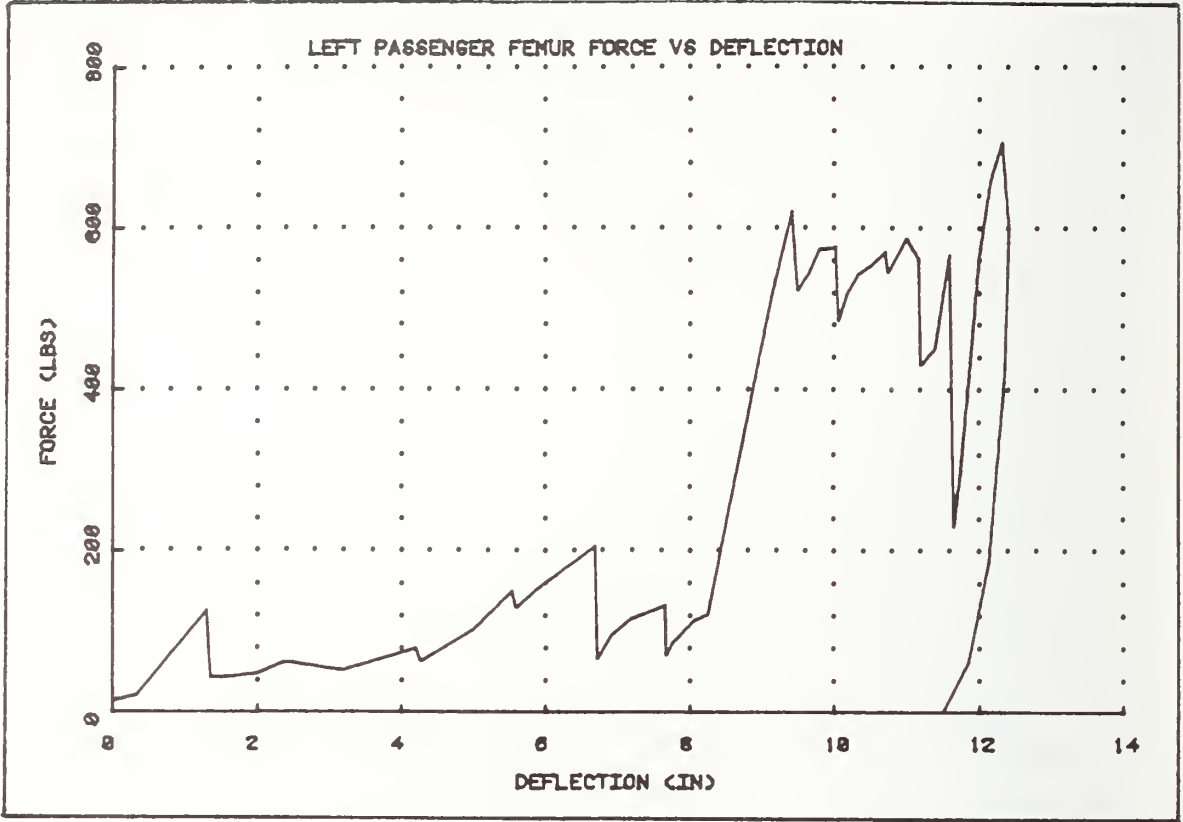
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test Left Passenger Femur

Date: July 27, 1984

Vehicle: 1977 Plymouth Volare

Options: Metal dash top



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

Deflection

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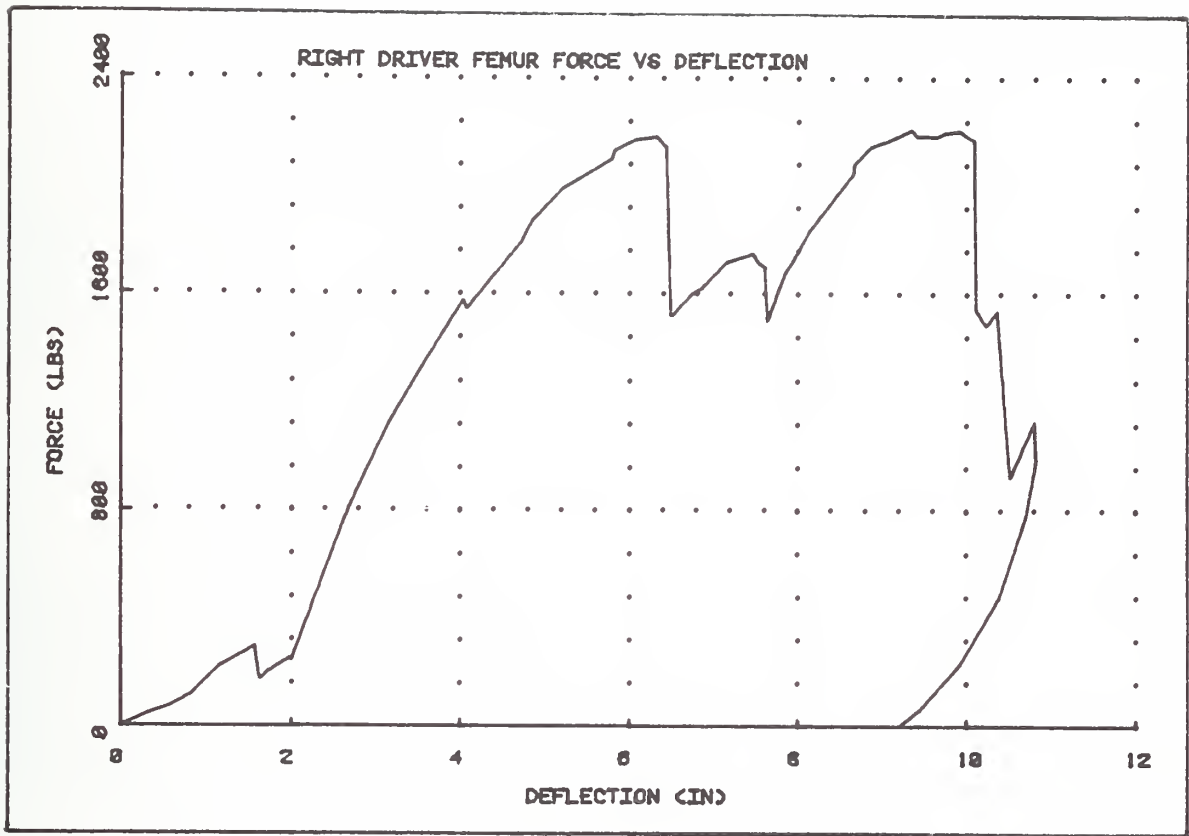


Test Right Driver Femur

Date: July 27, 1984

Vehicle: 1977 Plymouth Volare

Options: Metal dash top



G= \_\_\_\_\_

R= \_\_\_\_\_

K= \_\_\_\_\_

Deflection

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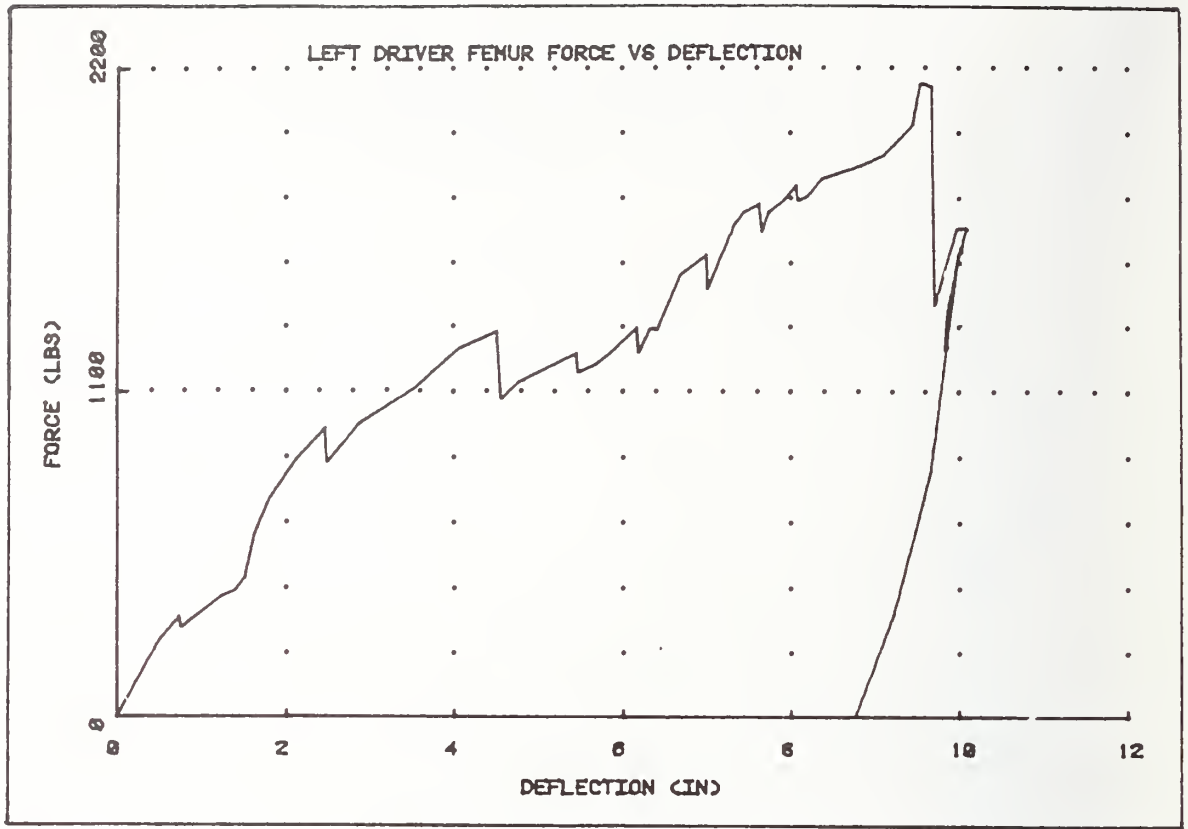
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Test Left Driver Femur

Date: July 27, 1984

Vehicle: 1977 Plymouth Volare

Options: Metal dash top



G= \_\_\_\_\_

R= \_\_\_\_\_

K= \_\_\_\_\_

Deflection

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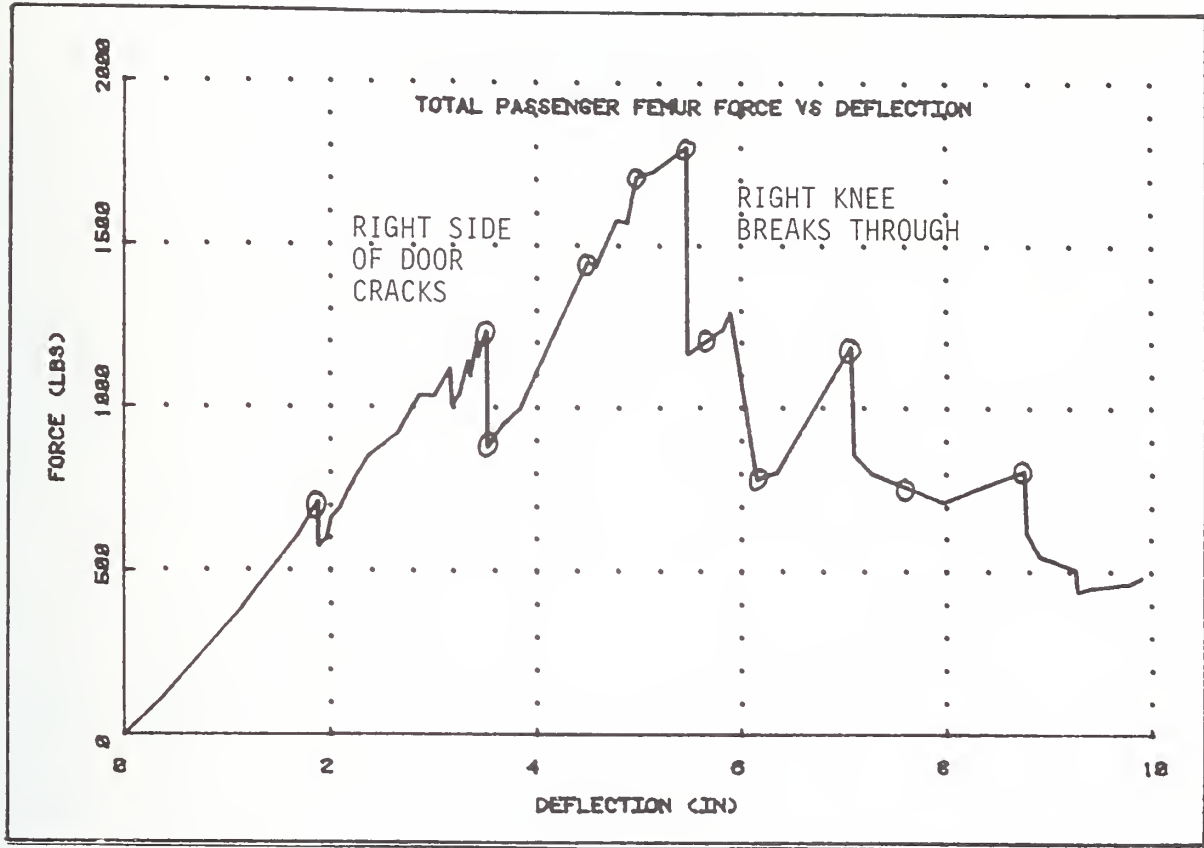
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Test: Passenger Side Femur (static) Date: August 9, 1984

Vehicle: Chevy Chevette

Options: Metal dash with foam crash pad on top and plastic on front,  
no radio



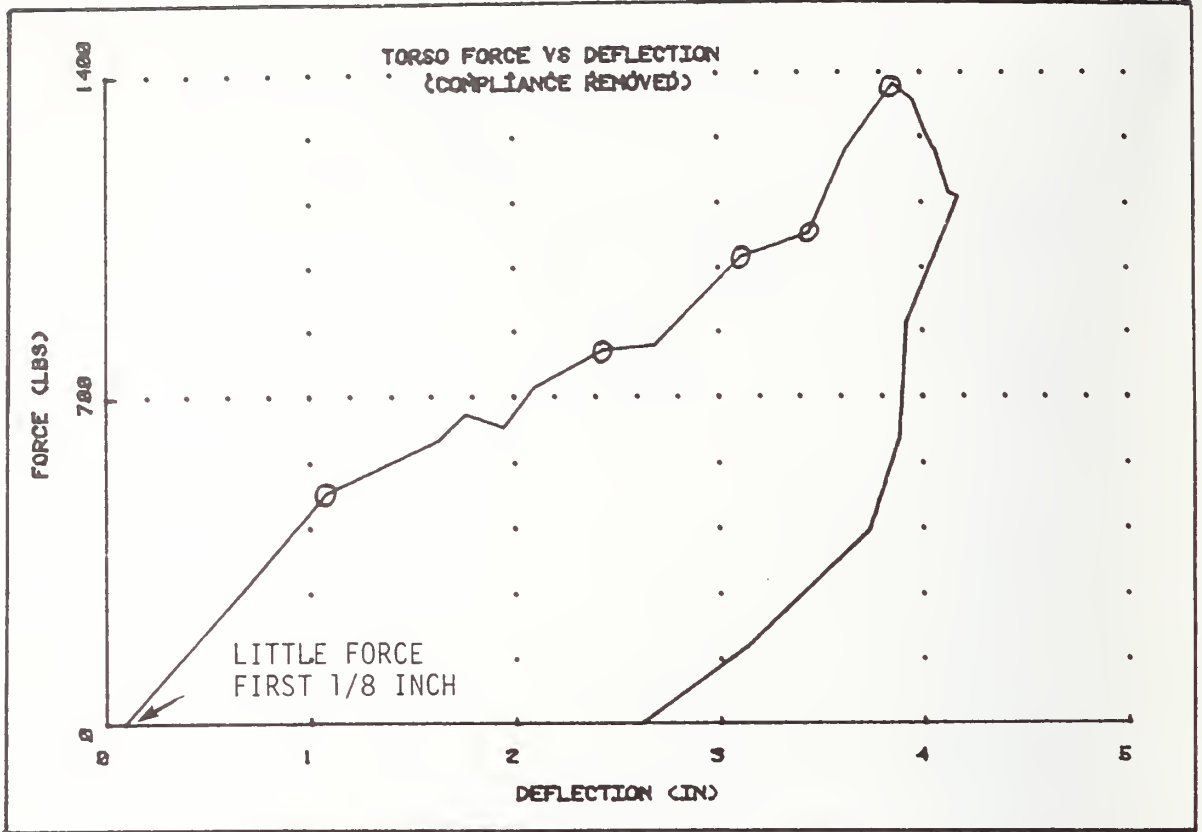
G= 0.935 R= 0.011 K= 900  
 c= 0.0  $\mu_1$ =             $\mu_2$ =             $\mu_3$ =             
 $\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
0.00	0.00	7.54	752.64
1.84	704.00	8.64	793.60
3.49	1233.92		
3.54	872.96		
4.49	1441.28		
4.94	1702.40		
5.44	1802.24		
5.65	1203.20		
6.15	773.12		
7.04	1172.48		

Test: Torso (static) Date: August 9, 1984

Vehicle: Chevy Chevette

Options: Metal dash with foam crash pad on top and plastic on front,  
no radio



G= 0.627 R= 0.195 K= 1279

c= 0.0  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

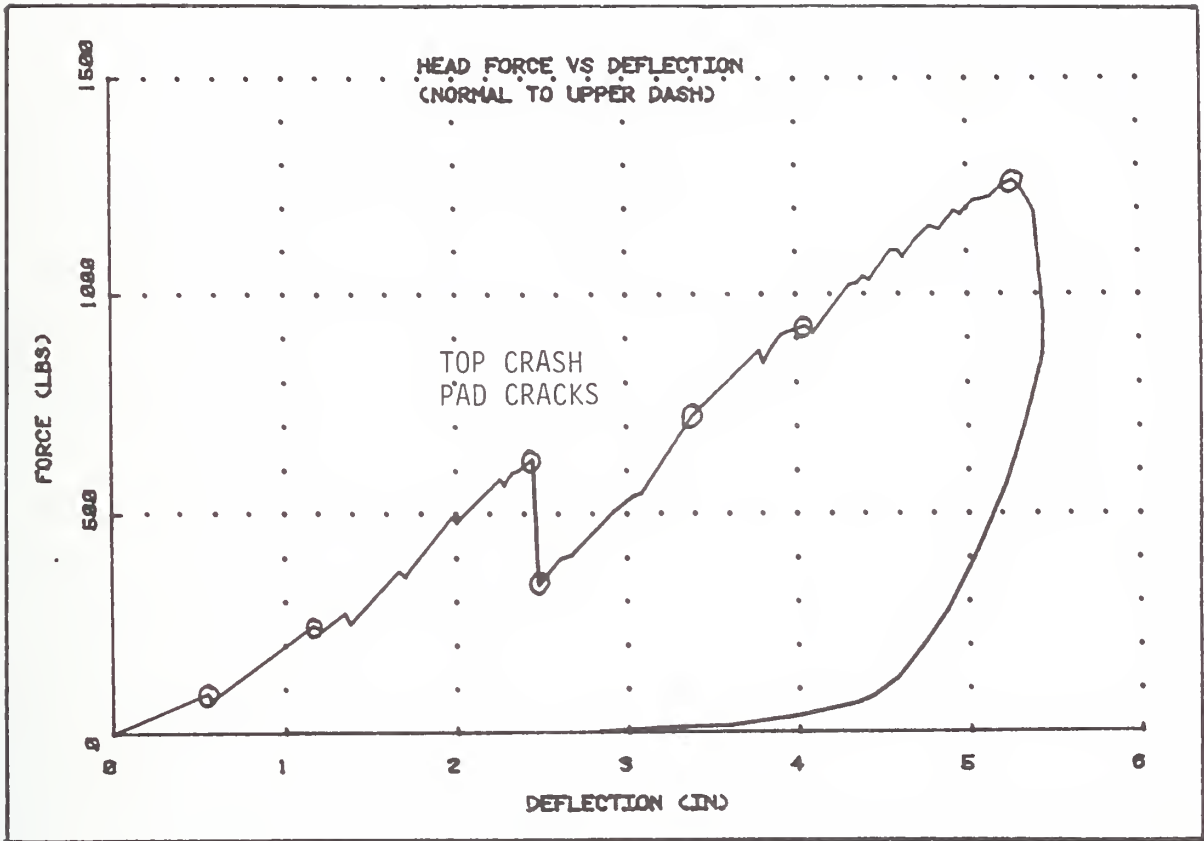
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.00</u>	<u>0.00</u>	_____	_____
<u>1.09</u>	<u>492.80</u>	_____	_____
<u>2.44</u>	<u>801.02</u>	_____	_____
<u>3.12</u>	<u>1003.52</u>	_____	_____
<u>3.44</u>	<u>1051.90</u>	_____	_____
<u>3.86</u>	<u>1379.84</u>	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Head (static) Date: August 9, 1984

Vehicle: Chevy Chevette

Options: Metal dash with foam crash pad on top and plastic on front,  
no radio



G= 0.520 R= 0.129 K= 1271

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

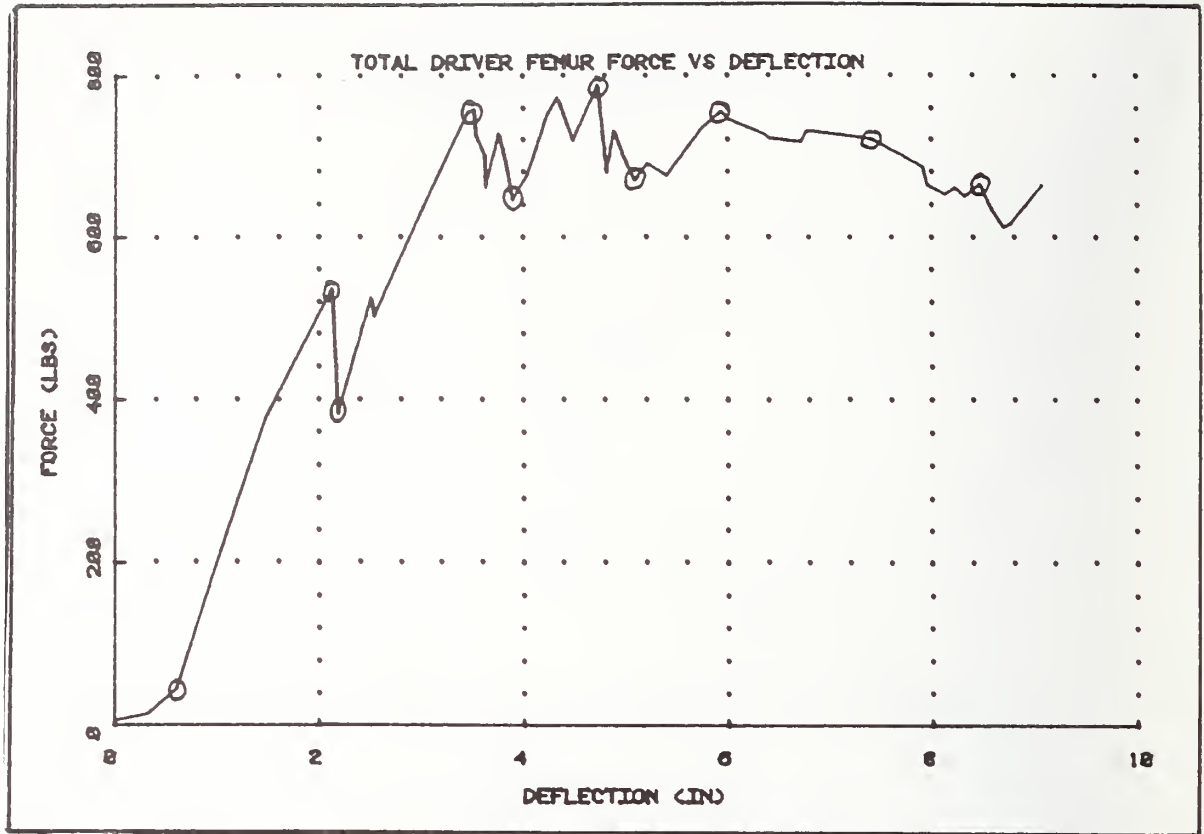
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.00</u>	<u>0.00</u>	_____	_____
<u>0.53</u>	<u>92.16</u>	_____	_____
<u>1.16</u>	<u>241.92</u>	_____	_____
<u>2.45</u>	<u>631.68</u>	_____	_____
<u>2.48</u>	<u>330.24</u>	_____	_____
<u>3.37</u>	<u>727.68</u>	_____	_____
<u>4.04</u>	<u>929.28</u>	_____	_____
<u>5.26</u>	<u>1265.28</u>	_____	_____

Test: Driver Side Femur Date: August 9, 1984

Vehicle: Chevy Chevette

Options: Metal dash with foam crash pad on top and plastic on front,  
no radio



G= 0.869 R= 0.034 K= 309

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.00</u>	<u>0.00</u>	<u>8.46</u>	<u>667.64</u>
<u>0.60</u>	<u>45.05</u>		
<u>2.14</u>	<u>536.57</u>		
<u>2.19</u>	<u>380.92</u>		
<u>3.44</u>	<u>752.64</u>		
<u>3.88</u>	<u>649.09</u>		
<u>4.73</u>	<u>787.45</u>		
<u>5.08</u>	<u>667.64</u>		
<u>5.92</u>	<u>755.71</u>		
<u>7.37</u>	<u>719.87</u>		

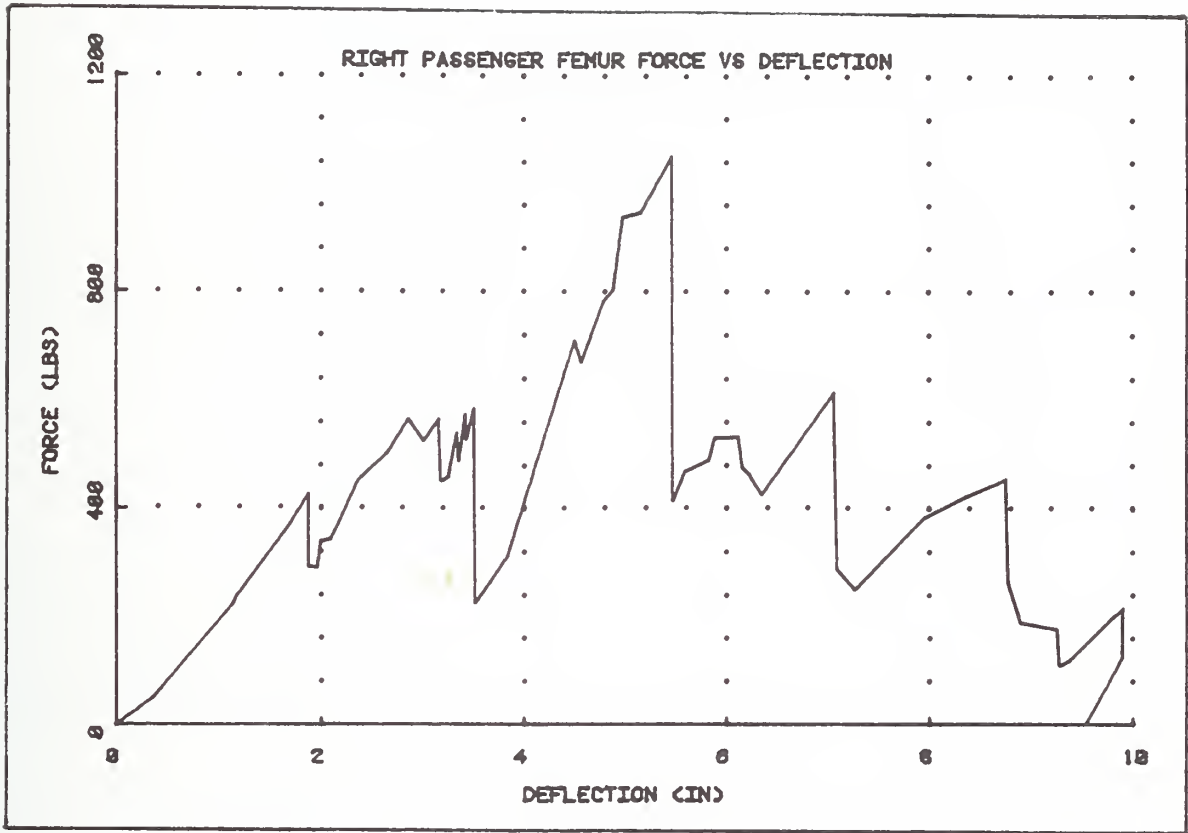
Test Right Passenger Femur

Date: August 9, 1984

Vehicle: Chevy Chevette

Options: Metal dash with foam crash pad on top and plastic on front

Radio missing



G= \_\_\_\_\_

R= \_\_\_\_\_

K= \_\_\_\_\_

Deflection

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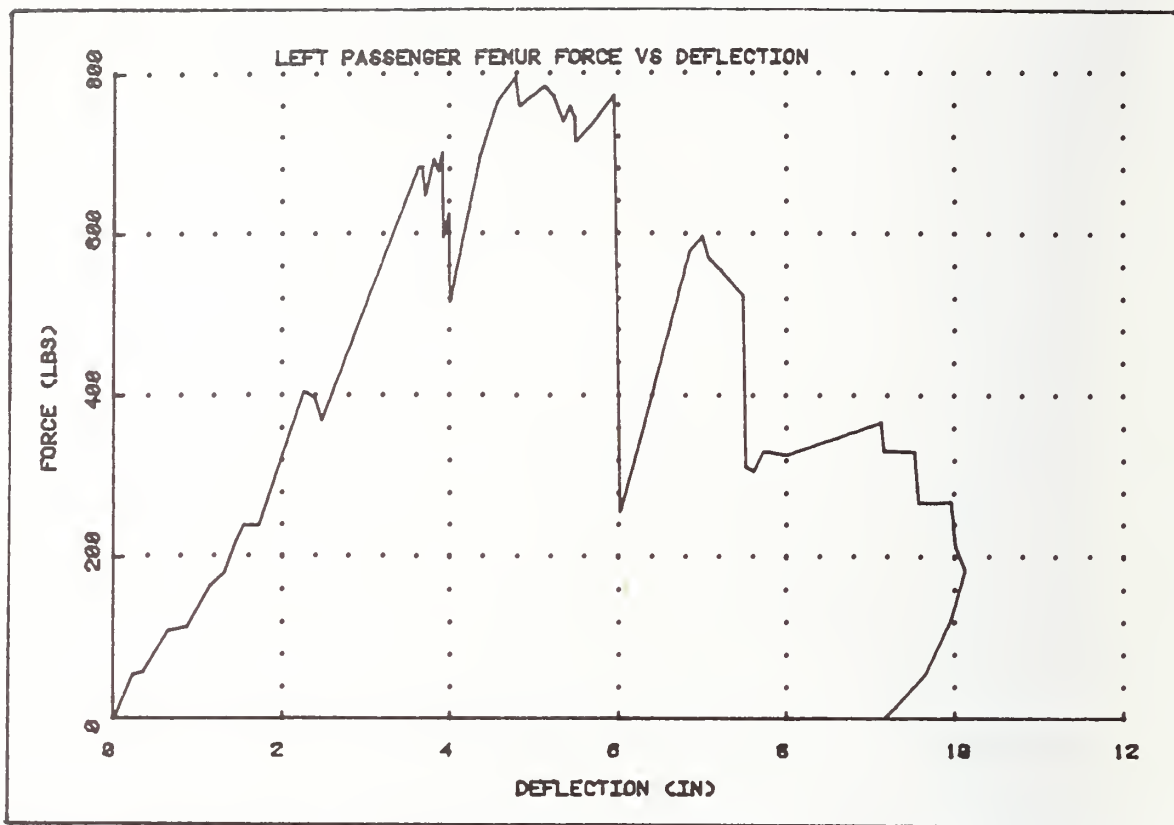
Test Left Passenger Femur

Date: August 9, 1984

Vehicle: Chevy Chevette

Options: Metal dash with foam crash pad on top and plastic on front

Radio missing



G= \_\_\_\_\_

R= \_\_\_\_\_

K= \_\_\_\_\_

Deflection

Force

Deflection

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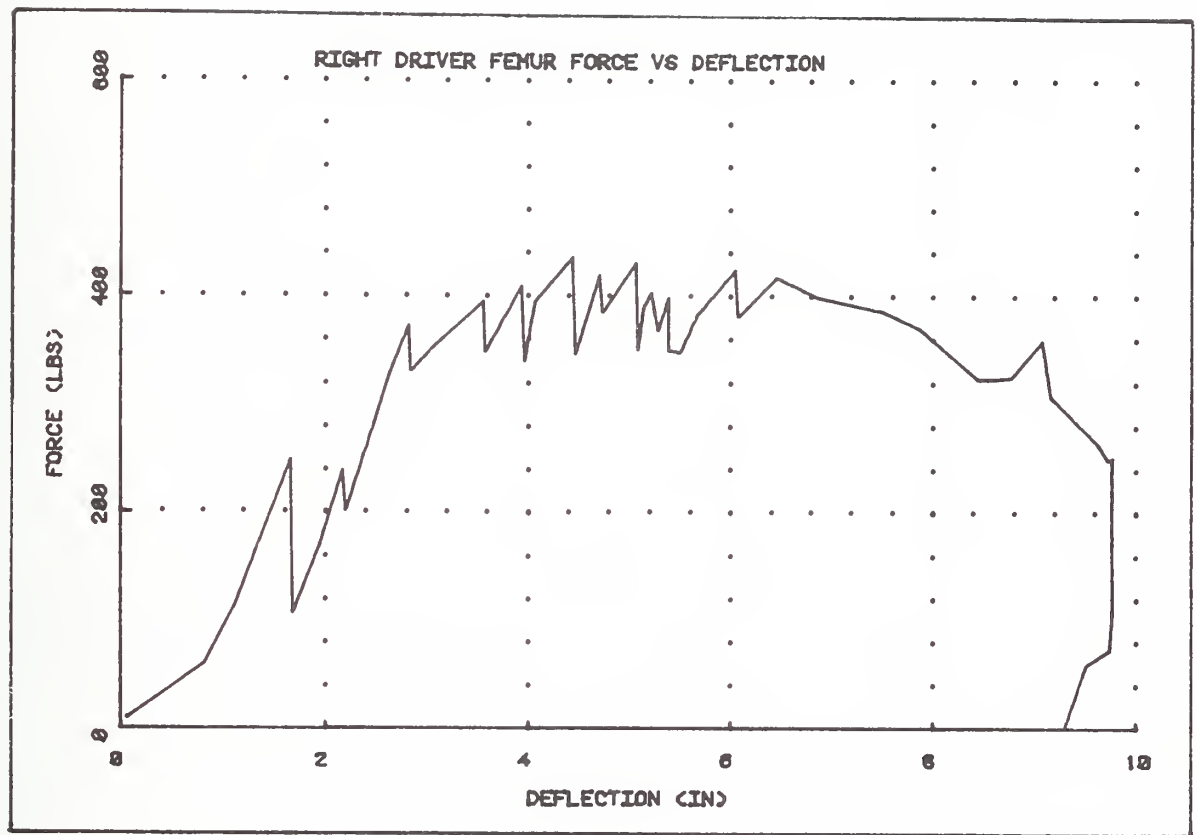
Test Right Driver Femur

Date: August 9, 1984

Vehicle: Chevy Chevette

Options: Metal dash with foam crash pad on top and plastic on front

Radio missing



G= \_\_\_\_\_

R= \_\_\_\_\_

K= \_\_\_\_\_

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

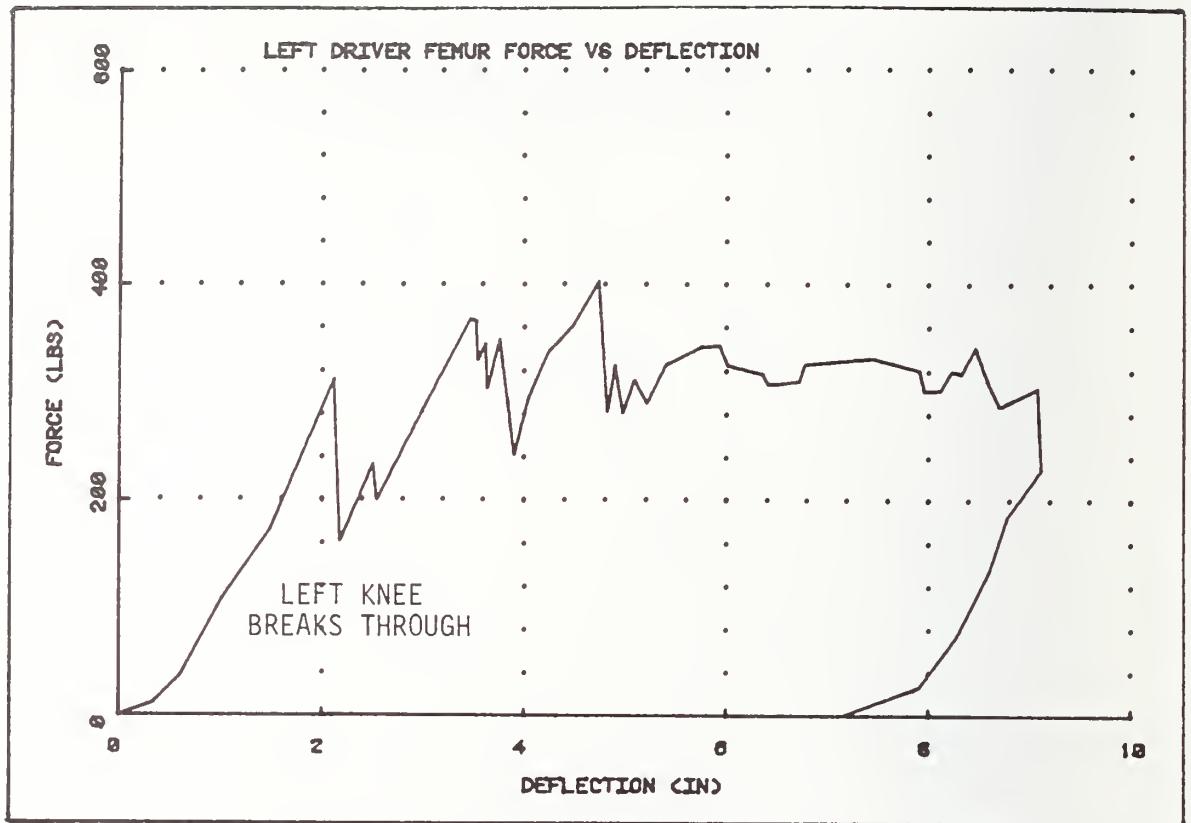
Test Left Driver Femur

Date: August 9, 1984

Vehicle: Chevy Chevette

Options: Metal dash with foam crash pad on top and plastic on front

Radio missing



G= \_\_\_\_\_

R= \_\_\_\_\_

K= \_\_\_\_\_

Deflection

Force

Deflection

Force

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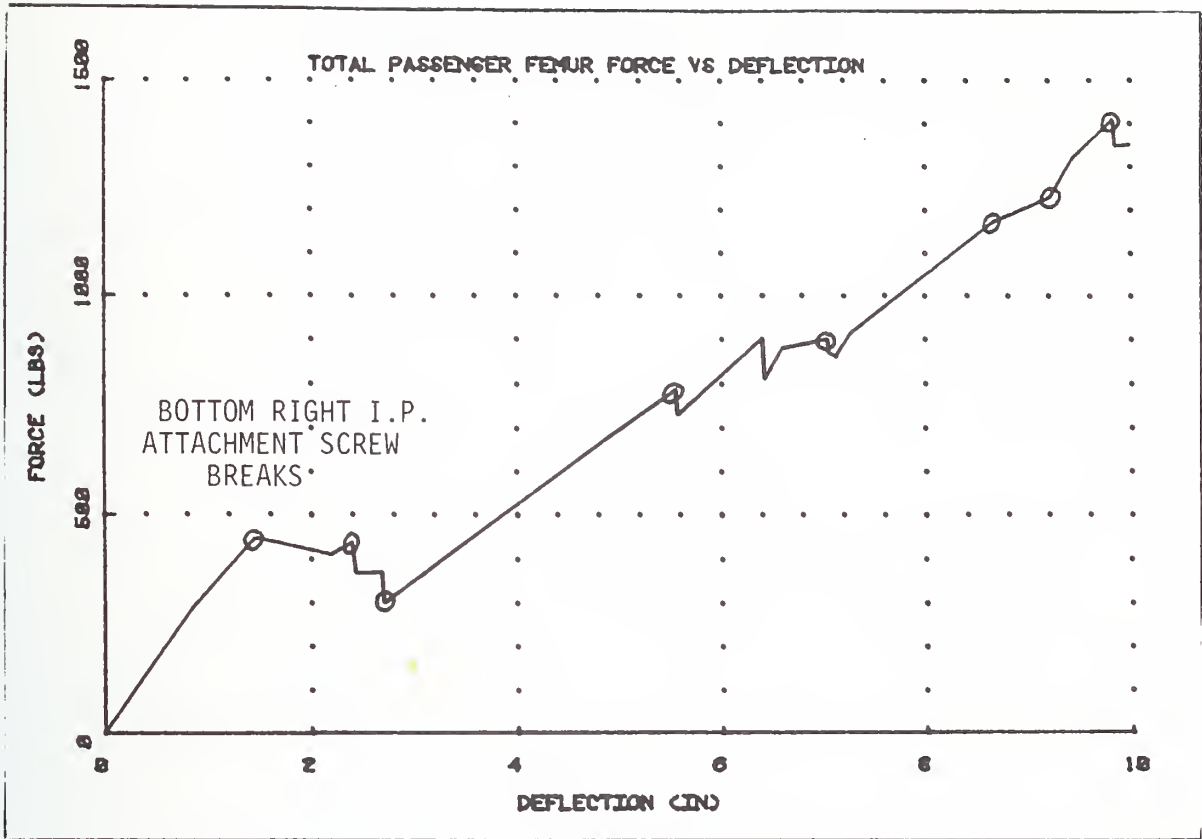
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Test: Passenger Side Femur (static) Date: August 17, 1984

Vehicle: 1976 Chevy Monza

Options: Metal dash with foam crash pad on front



G= 0.902 R= 0.068 K= 1843

c= 0.62  $\mu_1$ =             $\mu_2$ =             $\mu_3$ =           

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 7.44  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

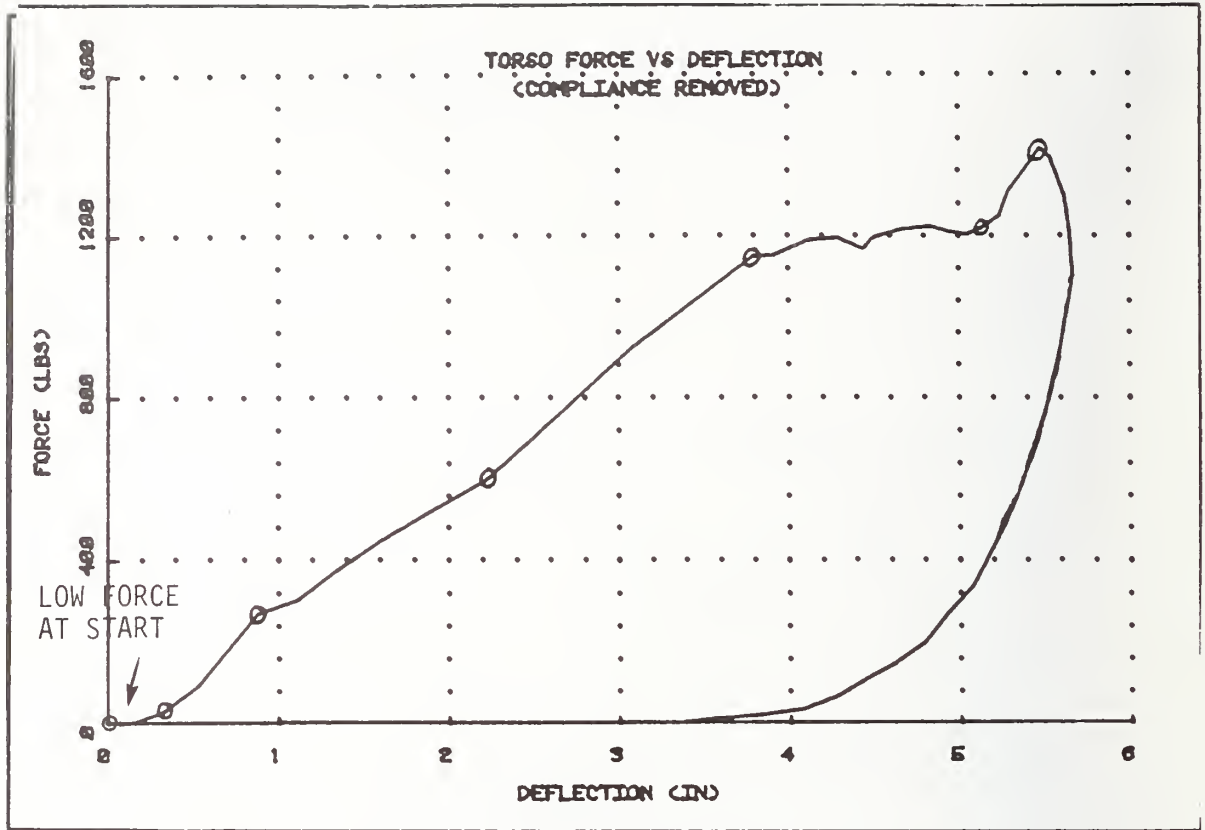
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.00</u>	<u>0.00</u>	<u>          </u>	<u>          </u>
<u>1.44</u>	<u>451.20</u>	<u>          </u>	<u>          </u>
<u>2.39</u>	<u>435.20</u>	<u>          </u>	<u>          </u>
<u>2.68</u>	<u>293.76</u>	<u>          </u>	<u>          </u>
<u>5.58</u>	<u>787.20</u>	<u>          </u>	<u>          </u>
<u>7.07</u>	<u>900.48</u>	<u>          </u>	<u>          </u>
<u>8.67</u>	<u>1176.96</u>	<u>          </u>	<u>          </u>
<u>9.22</u>	<u>1228.80</u>	<u>          </u>	<u>          </u>
<u>9.82</u>	<u>1409.28</u>	<u>          </u>	<u>          </u>

Test: Torso (static)

Date: August 17, 1984

Vehicle: 1976 Chevy Monza

Options: Metal dash with foam crash pad on front



G= 0.597

R= 0.133

K= 2321

c= 2.59

$\mu_1$ =

$\mu_2$ =

$\mu_3$ =

$\delta_A$ = 0.0

$\delta_B$ = 0.0

$\delta_C$ = 4.14

$\delta_D$ = 1000.0

$\delta_F$ = 1000.1

Deflection

Force

Deflection

Force

0.00

0.00

0.36

34.81

0.89

274.43

2.24

602.11

3.80

1153.02

5.15

1224.70

5.48

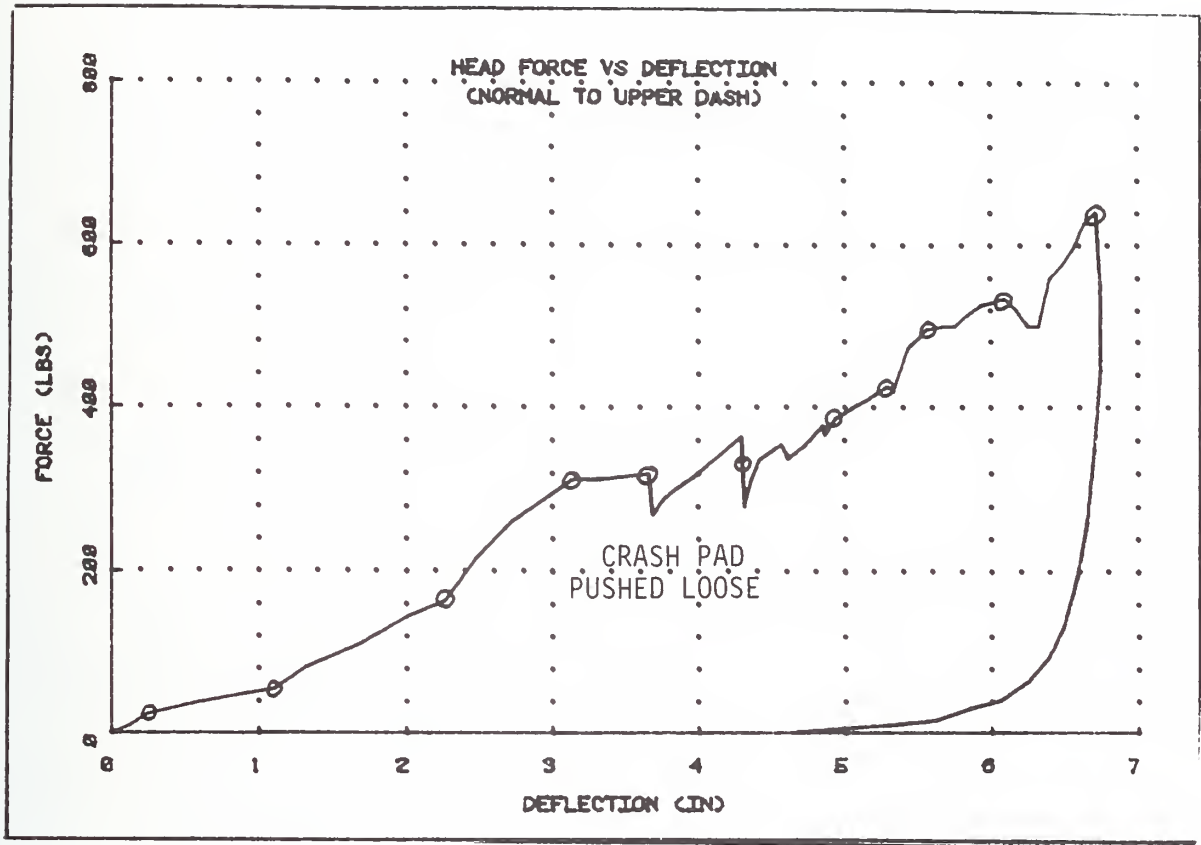
1415.16

Test: Head (static)

Date: August 17, 1984

Vehicle: 1976 Chevy Monza

Options: Metal dash with foam crash pad on front



G= 0.691

R= 0.062

K= 1278

c= \_\_\_\_\_

$\mu_1$ = \_\_\_\_\_

$\mu_2$ = \_\_\_\_\_

$\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0

$\delta_B$ = 0.0

$\delta_C$ = 0.0

$\delta_D$ = 1000.0

$\delta_F$ = 1000.1

Deflection

Force

Deflection

Force

0.00

0.00

6.07

534.52

0.27

25.60

6.73

646.14

1.11

53.24

2.26

164.86

3.14

312.32

3.66

319.48

4.29

327.68

4.92

387.07

5.27

422.91

5.54

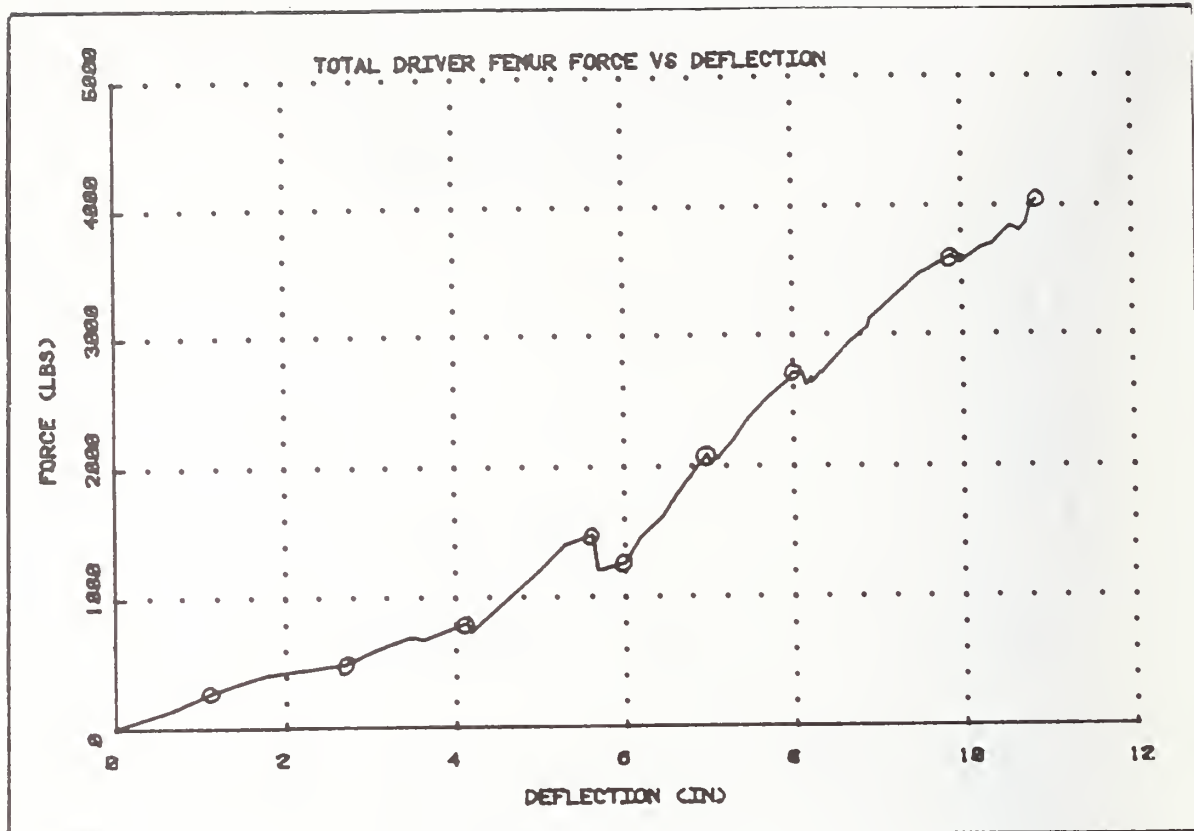
494.59

Test: Driver Side Femur

Date: August 17, 1984

Vehicle: 1976 Chevy Monza

Options: Metal dash with foam crash pad on front



G= 0.809

R= 0.124

K= 1989

c= \_\_\_\_\_

$\mu_1$ = \_\_\_\_\_

$\mu_2$ = \_\_\_\_\_

$\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0

$\delta_B$ = 0.0

$\delta_C$ = 0.0

$\delta_D$ = 1000.0

$\delta_F$ = 1000.1

Deflection

Force

Deflection

Force

0.00

0.00

1.13

281.60

2.75

505.60

4.12

800.00

5.62

1497.60

5.97

1273.60

6.93

2073.60

8.01

2720.00

9.86

3616.00

10.88

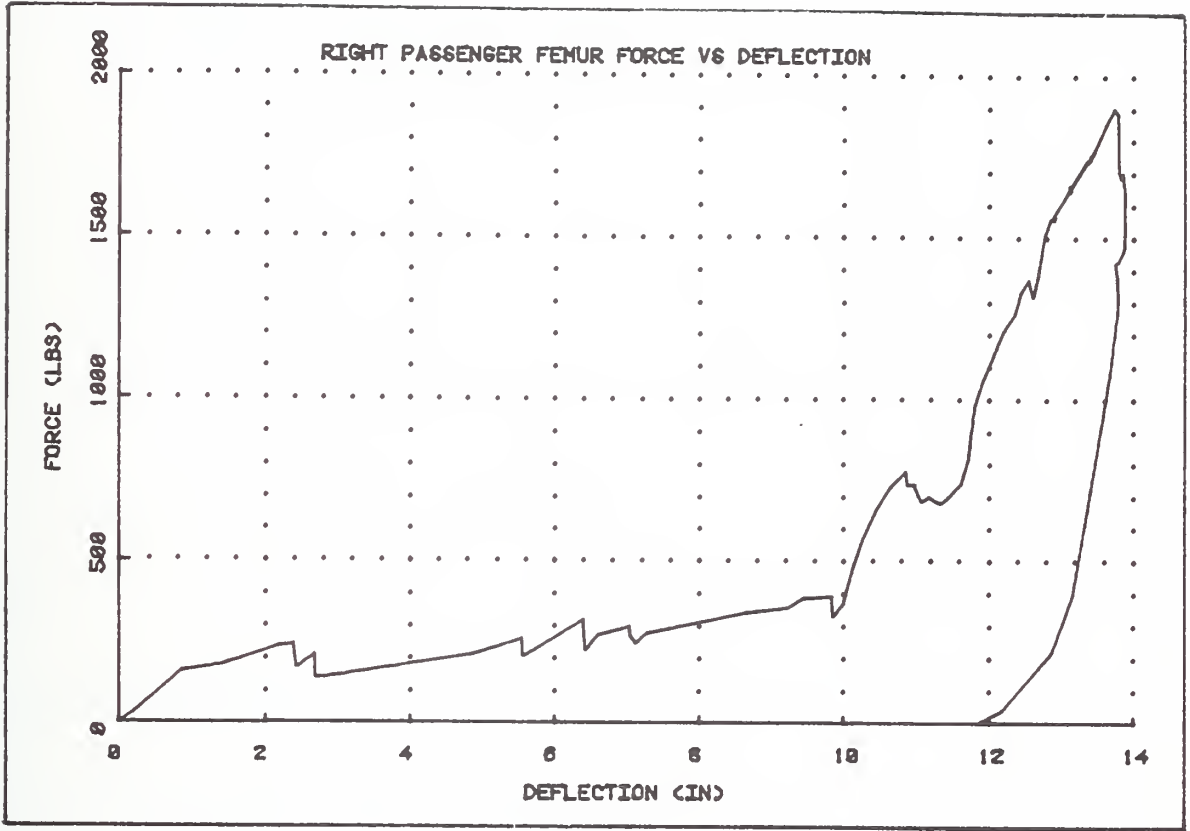
4038.40

Test Right Passenger Femur

Date: August 17, 1984

Vehicle: 1976 Chevy Monza

Options: Metal dash with foam crash pad on front



G= \_\_\_\_\_

R= \_\_\_\_\_

K= \_\_\_\_\_

Deflection

Force

Deflection

Force

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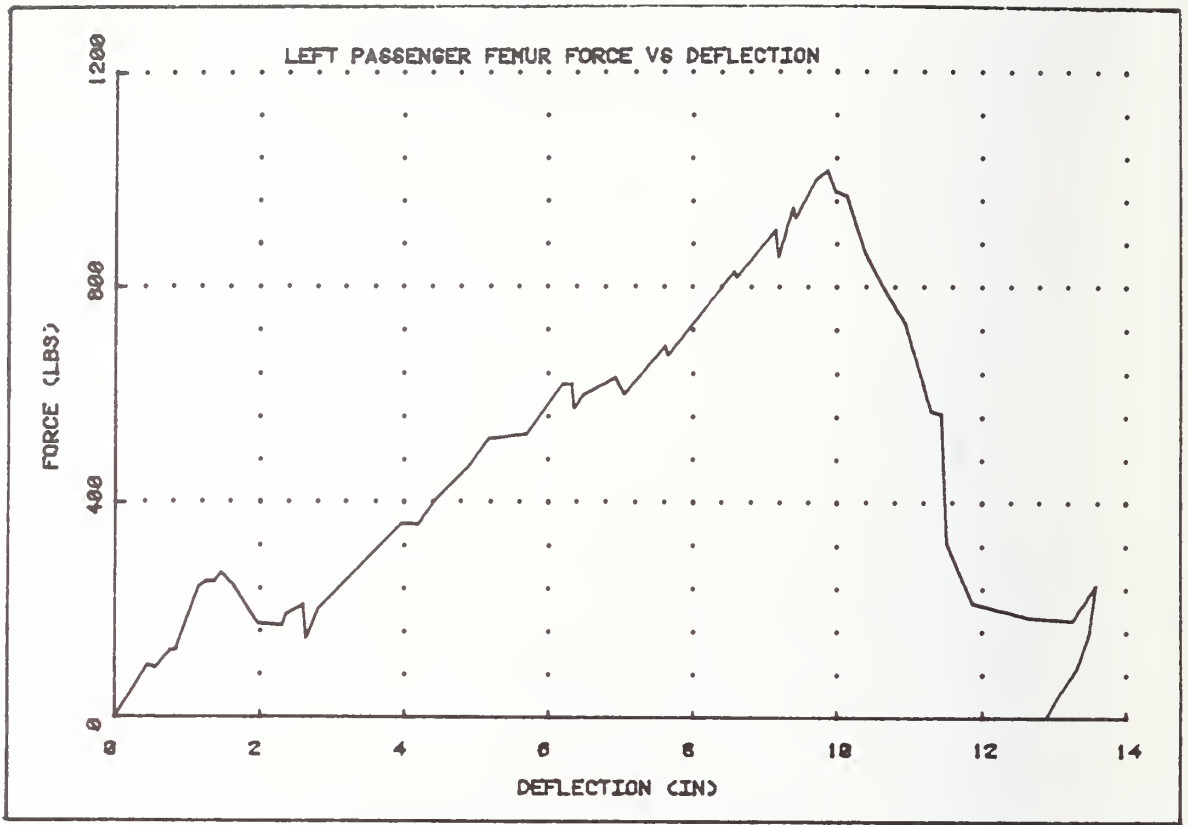
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Test Left Passenger Femur

Date: August 17, 1984

Vehicle: 1976 Chevy Monza

Options: Metal dash with foam crash pad on top



G= \_\_\_\_\_

R= \_\_\_\_\_

K= \_\_\_\_\_

Deflection

Force

Deflection

Force

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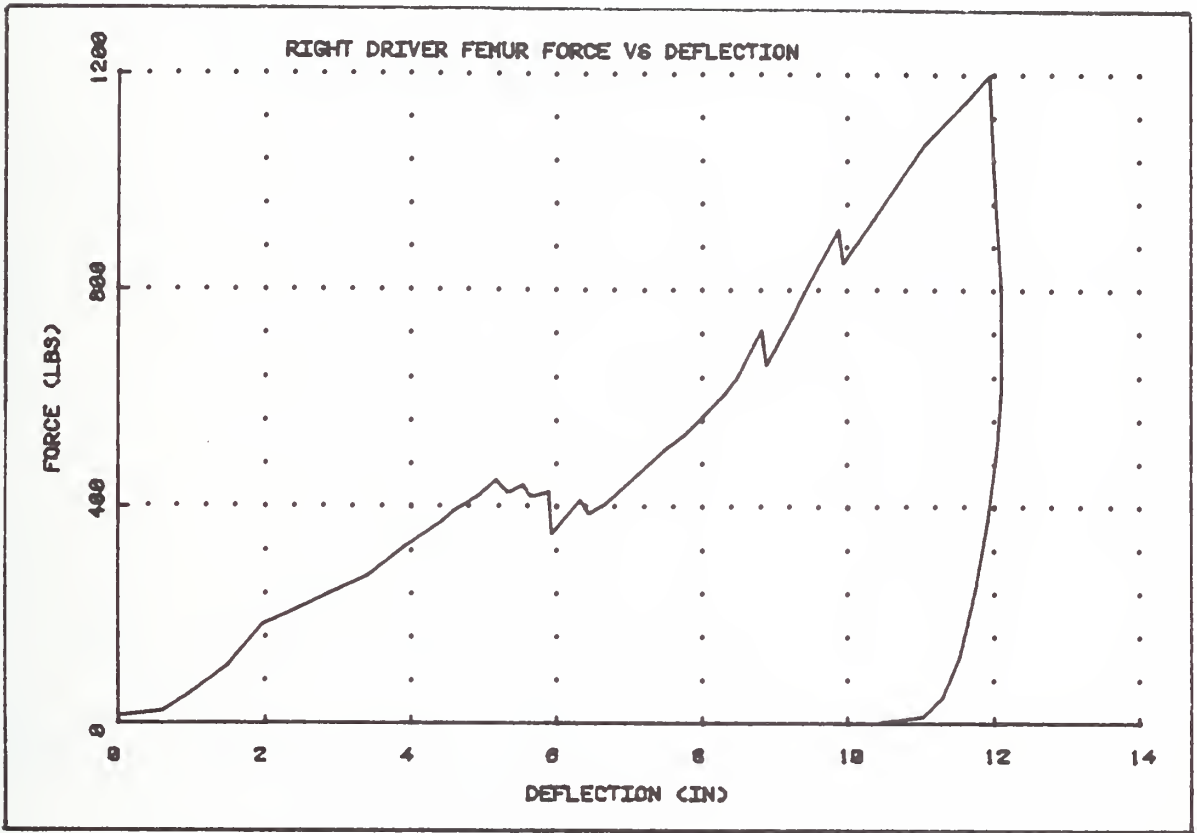


Test Right Driver Femur

Date: August 17, 1984

Vehicle: 1976 Chevy Monza

Options: Metal dash with foam crash pad on front



G= \_\_\_\_\_

R= \_\_\_\_\_

K= \_\_\_\_\_

Deflection

Force

Deflection

Force

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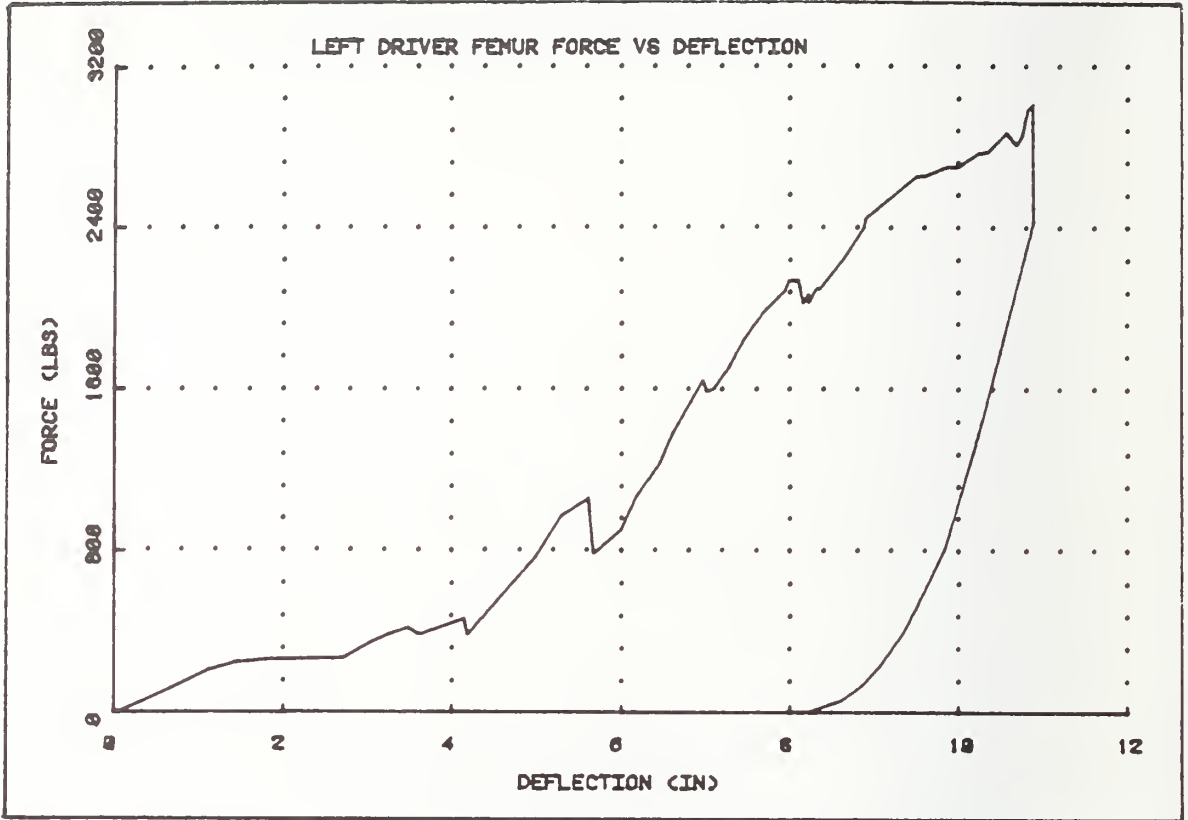
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Test Left Driver Femur

Date: August 17, 1984

Vehicle: 1976 Chevy Monza

Options: Metal dash with foam crash pad on front



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

Deflection

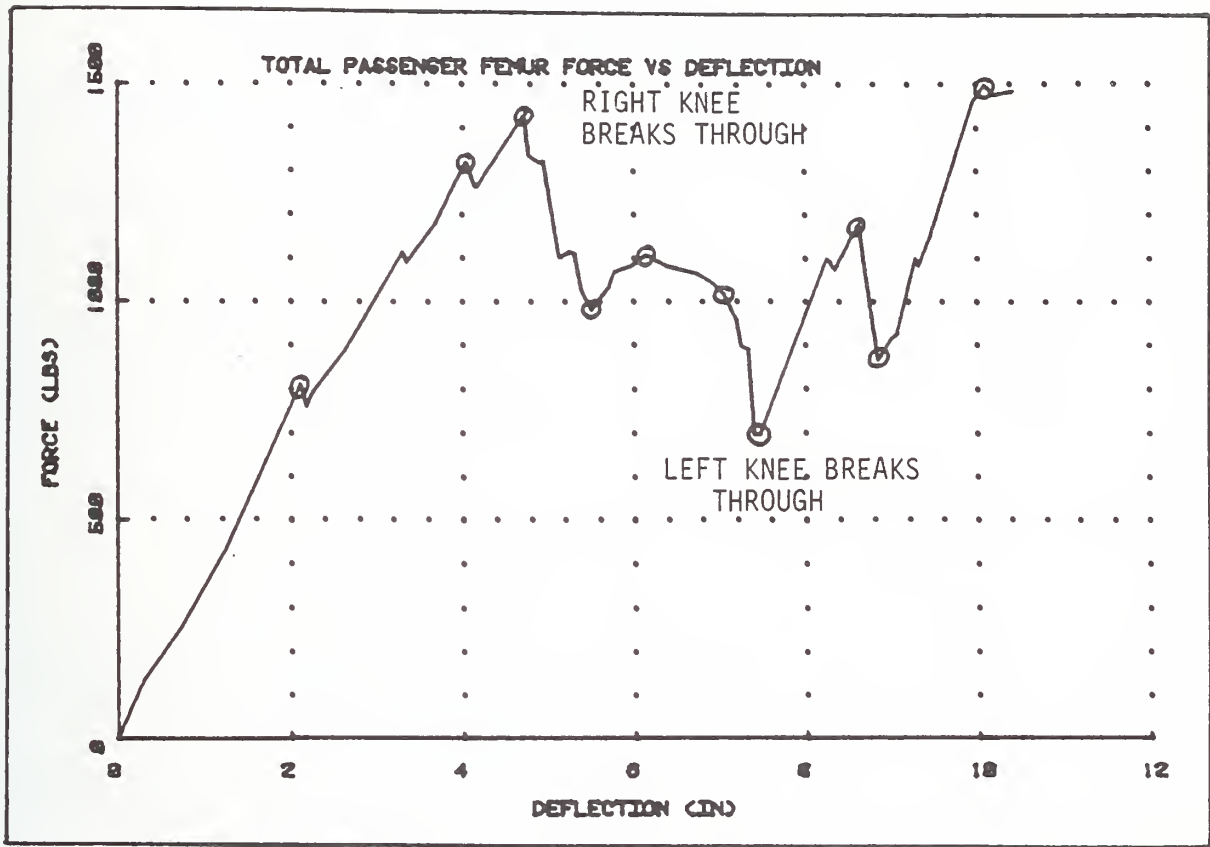
Force

Deflection

Force

_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Passenger Side Femur (static) Date: August 21, 1984  
 Vehicle: Honda Civic CVCC  
 Options: No radio



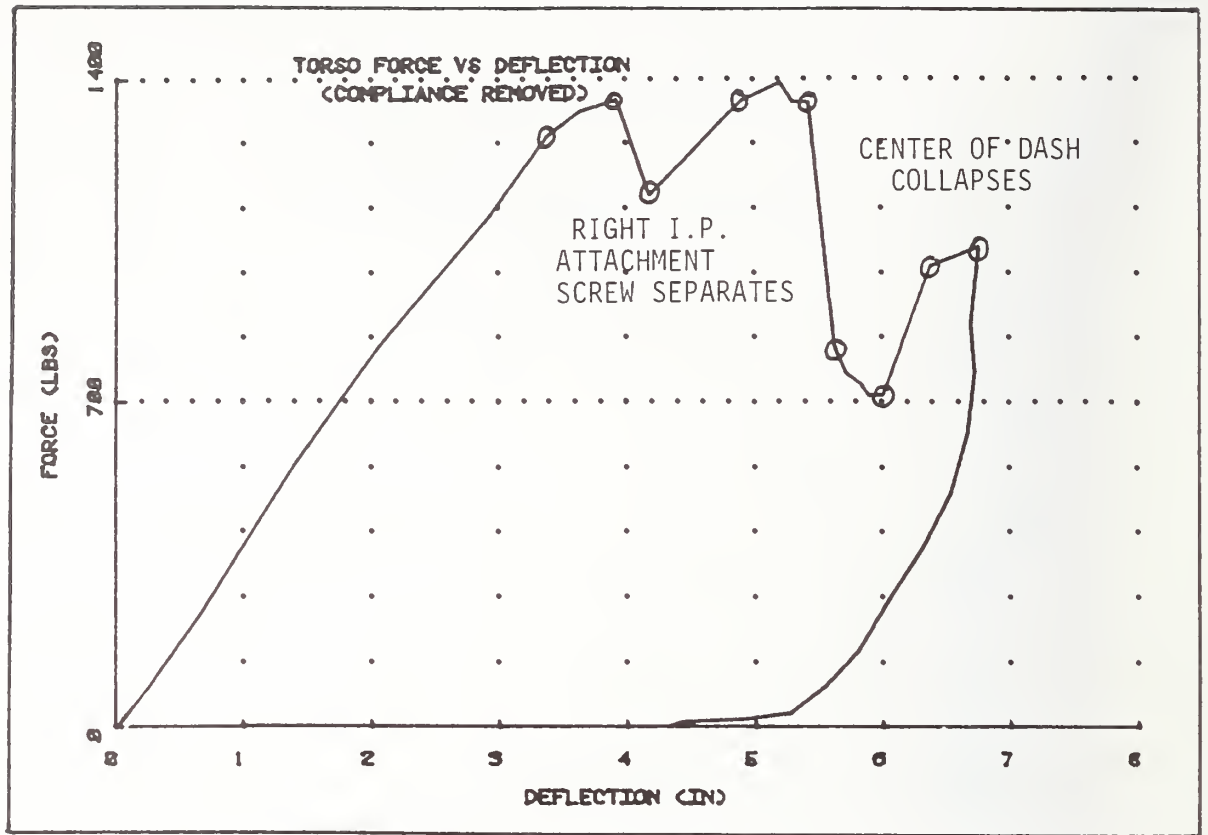
G= 0.793 R= 0.065 K= 1170  
 c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_  
 $\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

Deflection	Force	Deflection	Force
0.00	0.00	10.10	1499.52
2.16	819.84		
4.07	1328.64		
4.73	1434.24		
5.51	983.04		
6.10	1109.76		
7.06	1019.52		
7.42	689.28		
8.67	1184.64		
8.84	862.08		

Test: Torso (static) Date: August 21, 1984

Vehicle: Honda Civic CVCC

Options: No radio



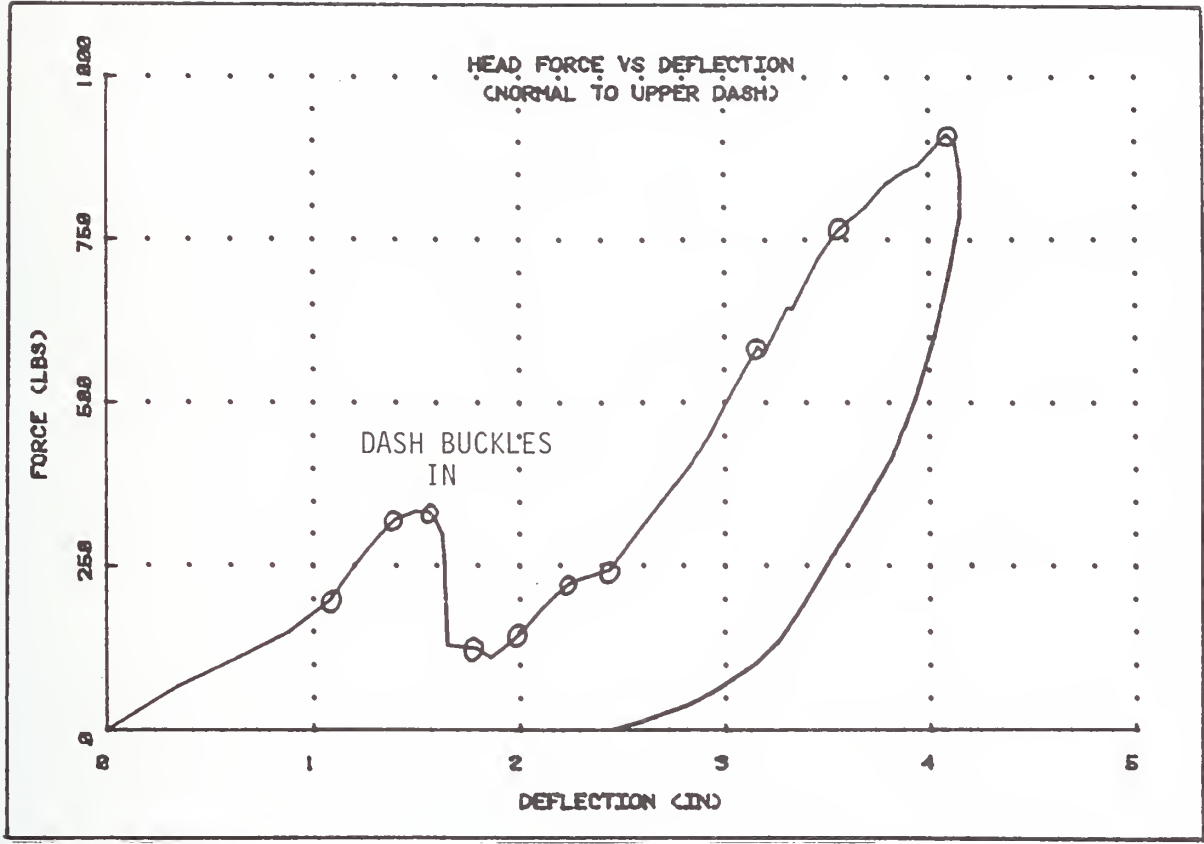
G= 0.641 R= 0.074 K= 1624

c= 2.60  $\mu_1$ =             $\mu_2$ =             $\mu_3$ =           

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 31.20  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
0.00	0.00		
3.40	1275.90		
3.92	1352.96		
4.19	1148.67		
4.91	1351.16		
5.43	1351.16		
5.63	818.94		
6.02	713.21		
6.38	992.76		
6.78	1033.98		

Test: Head (static) Date: August 21, 1984  
 Vehicle: Honda Civic CVCC  
 Options: No radio



G= 0.591 R= 0.266 K= 965  
 c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_  
 $\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

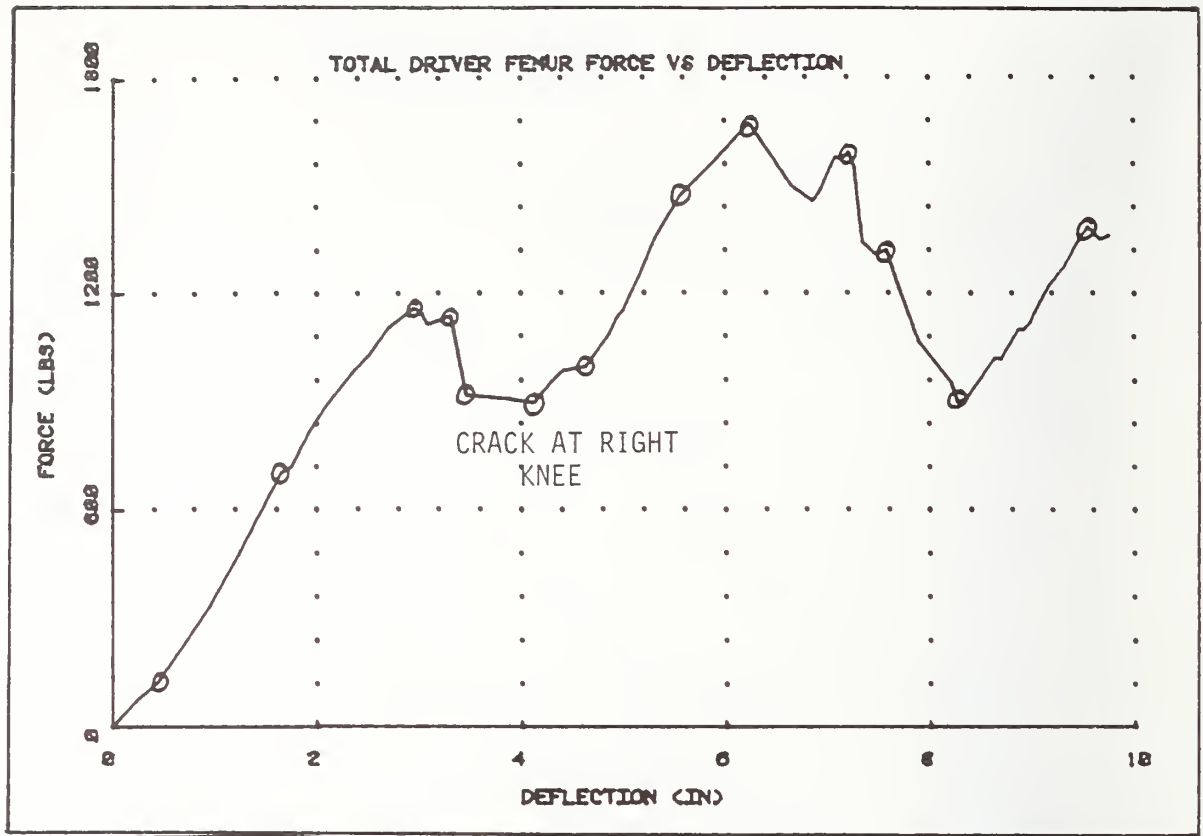
Deflection	Force	Deflection	Force
0.00	0.00	4.09	913.93
1.07	197.12		
1.39	326.40		
1.54	336.64		
1.79	126.72		
1.96	136.96		
2.24	226.56		
2.44	245.76		
3.17	590.08		
3.56	764.16		

Test: Driver Side Femur (static)

Date: August 21, 1984

Vehicle: Honda Civic CVCC

Options: No radio



G= 0.824

R= 0.072

K= 767

c= \_\_\_\_\_

$\mu_1$ = \_\_\_\_\_

$\mu_2$ = \_\_\_\_\_

$\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0

$\delta_B$ = 0.0

$\delta_C$ = 0.0

$\delta_D$ = 1000.0

$\delta_F$ = 1000.1

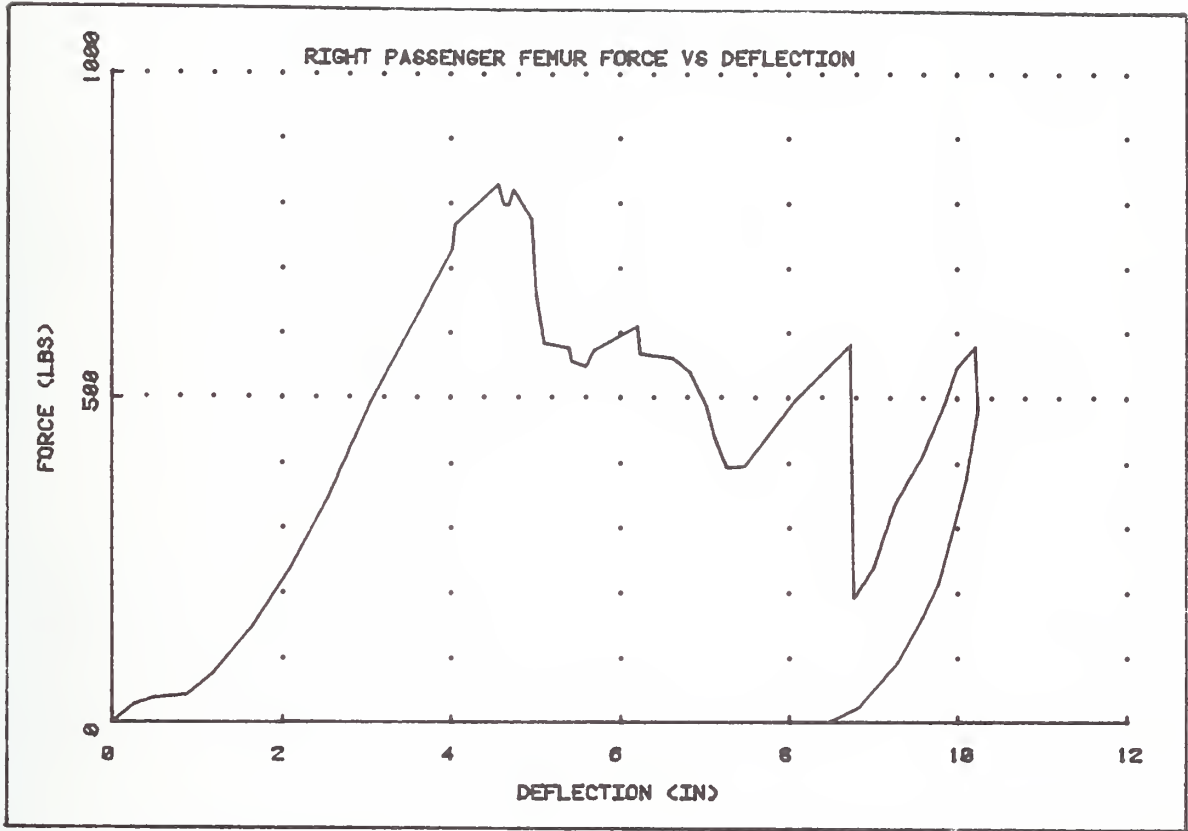
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.00</u>	<u>0.00</u>	<u>7.22</u>	<u>1592.06</u>
<u>0.45</u>	<u>129.02</u>	<u>7.57</u>	<u>1322.44</u>
<u>1.65</u>	<u>705.02</u>	<u>8.27</u>	<u>898.56</u>
<u>2.95</u>	<u>1154.30</u>	<u>9.57</u>	<u>1384.70</u>
<u>3.29</u>	<u>1135.87</u>		
<u>3.44</u>	<u>910.08</u>		
<u>4.44</u>	<u>891.64</u>		
<u>4.63</u>	<u>999.93</u>		
<u>5.58</u>	<u>1476.86</u>		
<u>6.23</u>	<u>1675.00</u>		

Test Right Passenger Femur

Date: August 21, 1984

Vehicle: Honda Civic CVCC

Options: No radio



G= \_\_\_\_\_

R= \_\_\_\_\_

K= \_\_\_\_\_

Deflection

Force

Deflection

Force

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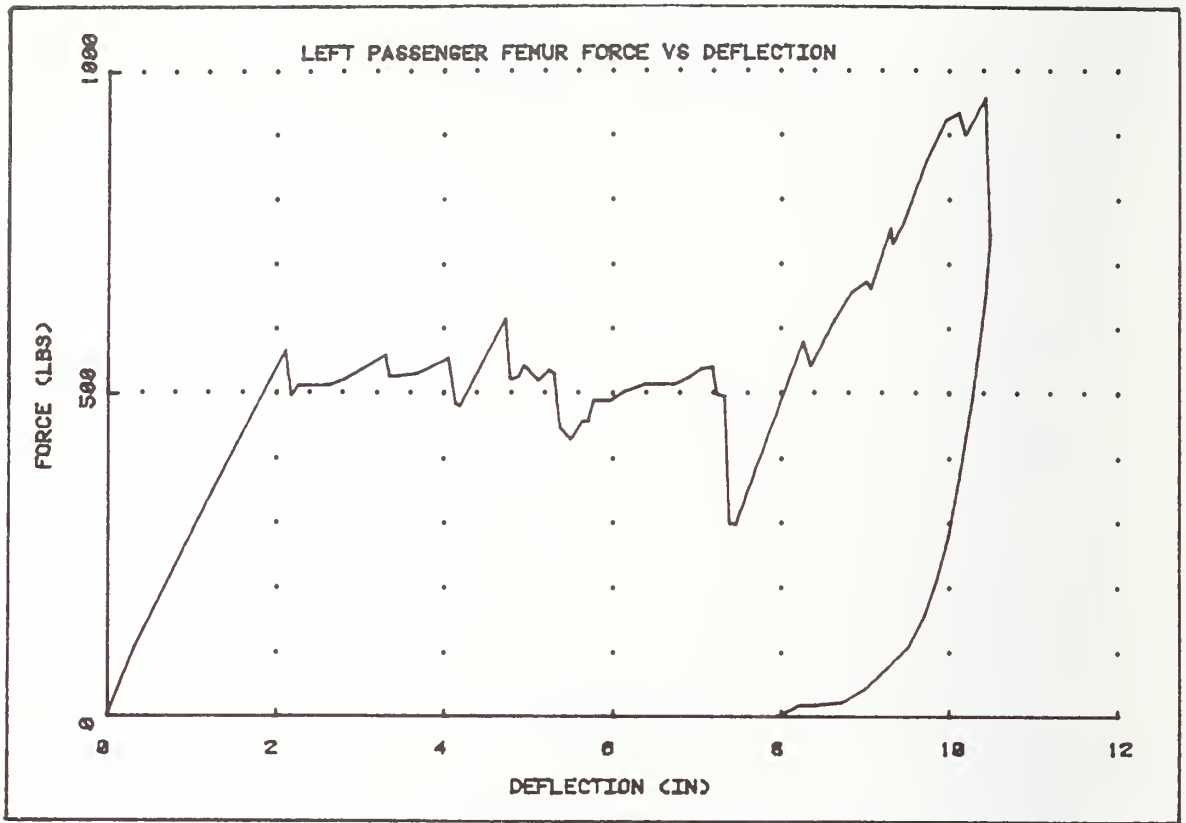
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Test Left Passenger Femur

Date: August 21, 1984

Vehicle: Honda Civic CVCC

Options: No radio



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

Deflection

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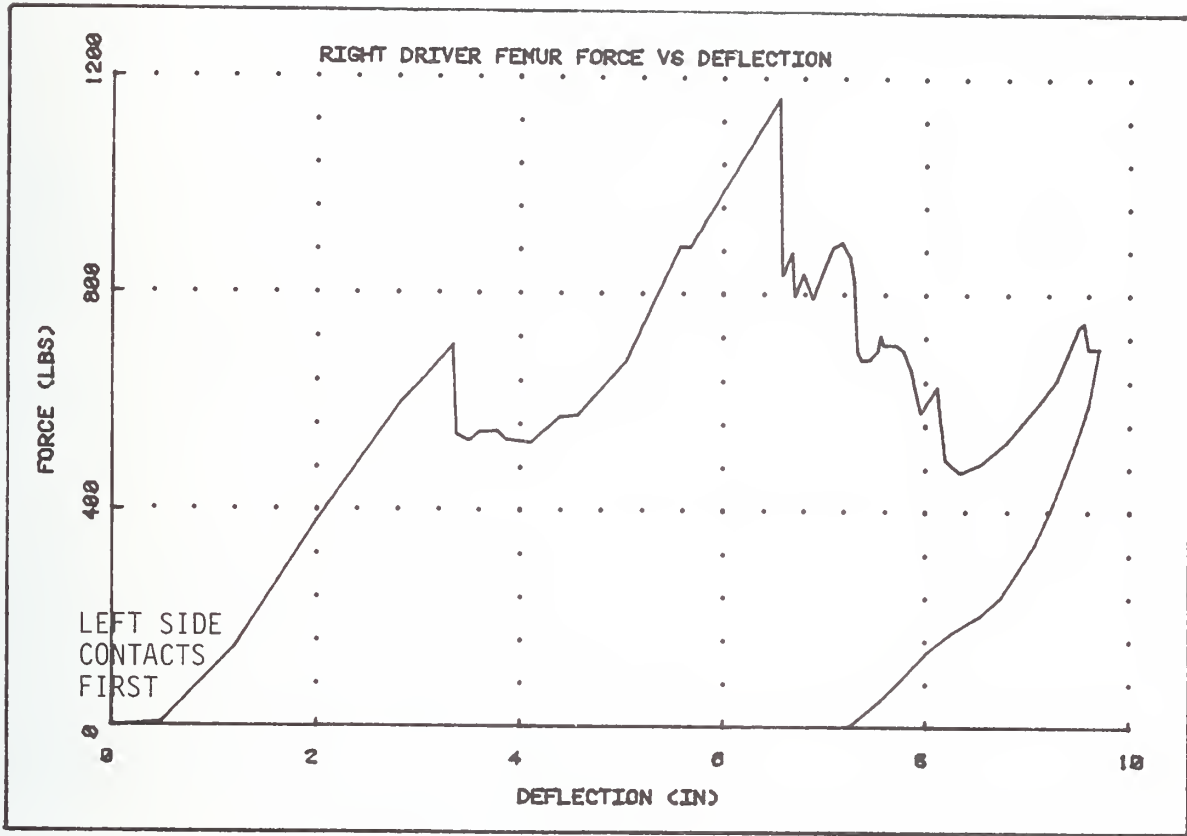


Test Right Driver Femur

Date: August 21, 1984

Vehicle: Honda Civic CVCC

Options: No radio



G= \_\_\_\_\_

R= \_\_\_\_\_

K= \_\_\_\_\_

Deflection

Force

Deflection

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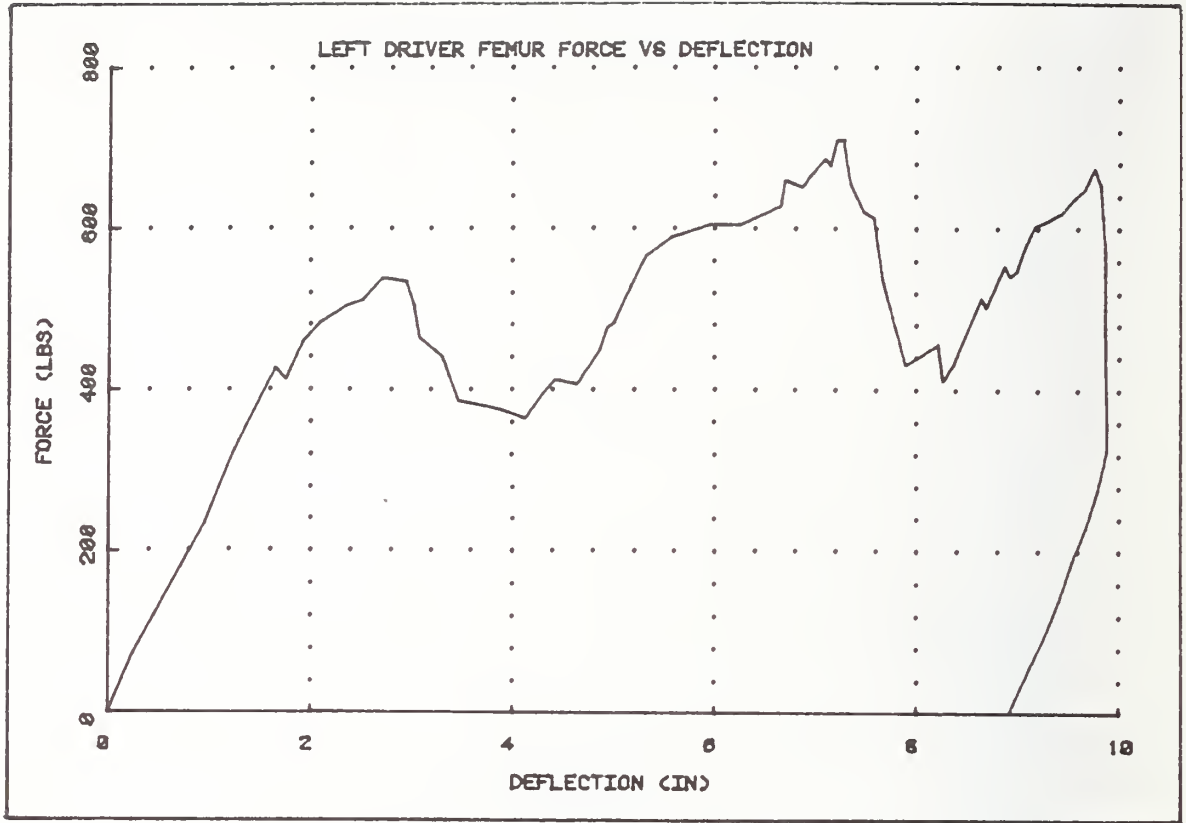
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Test Left Driver Femur

Date: August 21, 1984

Vehicle: Honda Civic CVCC

Options: No radio



G= \_\_\_\_\_

R= \_\_\_\_\_

K= \_\_\_\_\_

Deflection

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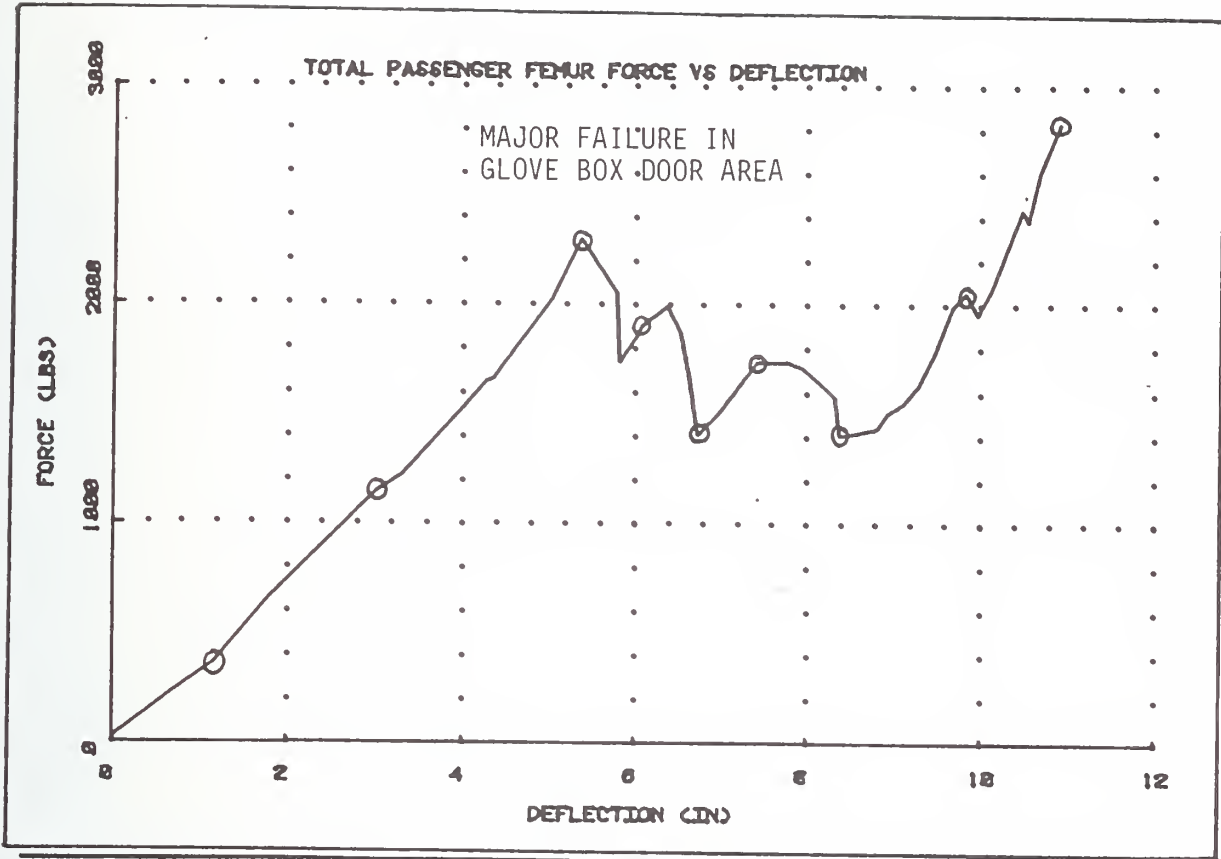
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Test: Passenger Side Femur (static)

Date: August 28, 1984

Vehicle: Ford LTD

Options: Air conditioning, radio missing



G= 0.814 R= 0.094 K= 1792

c= 0.0  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

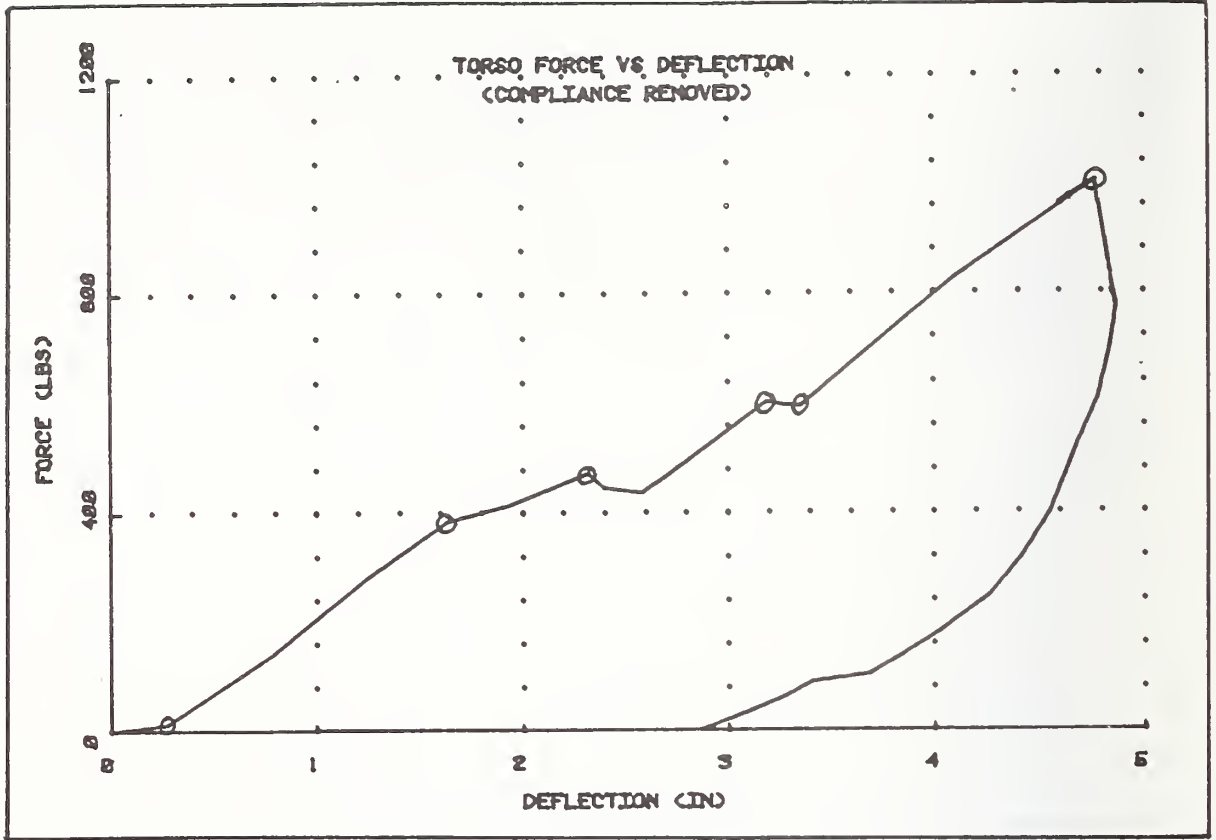
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
0.00	0.00		
1.17	366.42		
3.02	1149.33		
5.36	2298.48		
6.07	1905.88		
6.72	1404.66		
7.75	1740.31		
8.38	1401.95		
9.83	2059.63		
10.91	2836.35		

Test: Torso (static)

Date: August 28, 1984

Vehicle: Ford LTD

Options: Air conditioning, radio missing



G= 0.588

R= -0.179

K= 636

c= 0.66

$\mu_1 =$

$\mu_2 =$

$\mu_3 =$

$\delta_A = 0.0$

$\delta_B = 0.0$

$\delta_C = 7.92$

$\delta_D = 1000.0$

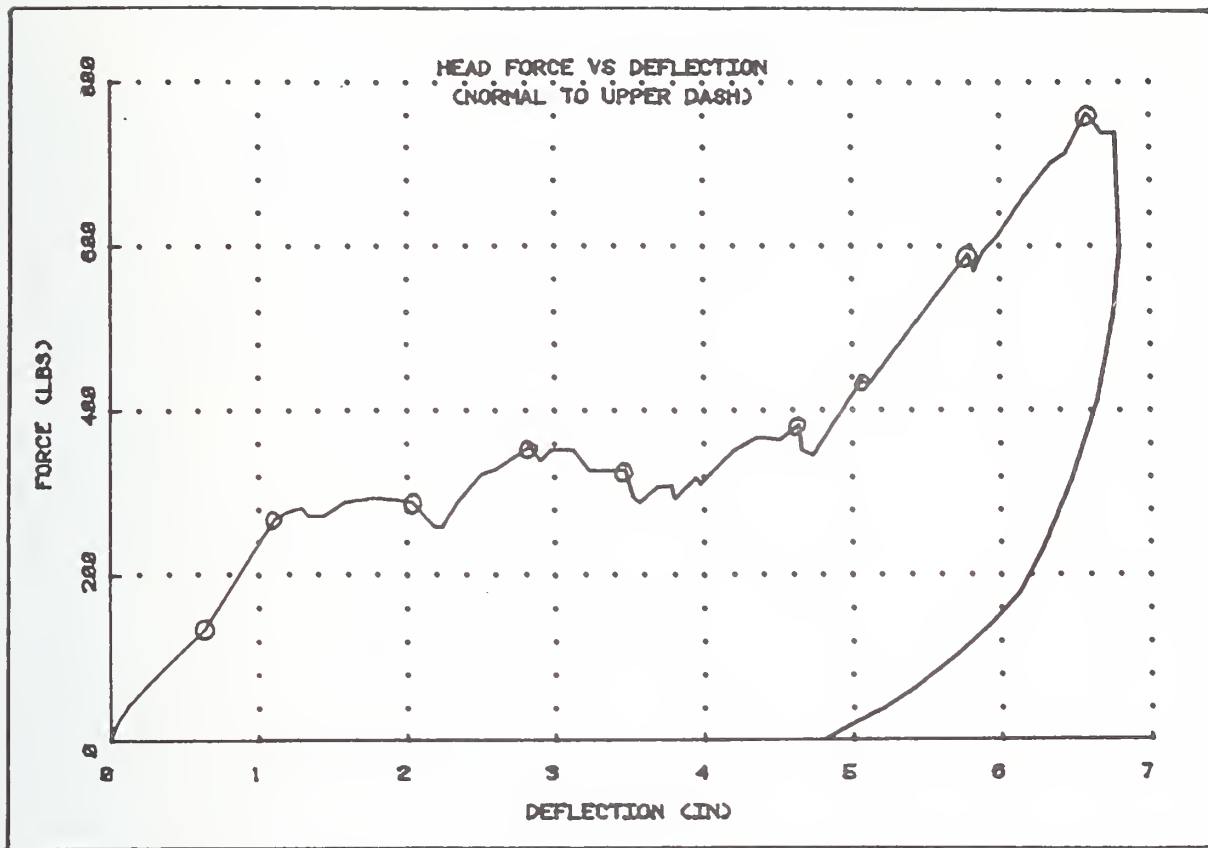
$\delta_F = 1000.1$

Deflection	Force	Deflection	Force
0.00	0.00		
0.27	13.27		
1.63	384.98		
2.31	472.01		
3.18	602.81		
3.26	594.03		
4.77	1005.11		

Test: Head (static) Date: August 28, 1984

Vehicle: Ford LTD

Options: Air conditioning, radio missing



G= 0.707 R= 0.132 K= 335

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

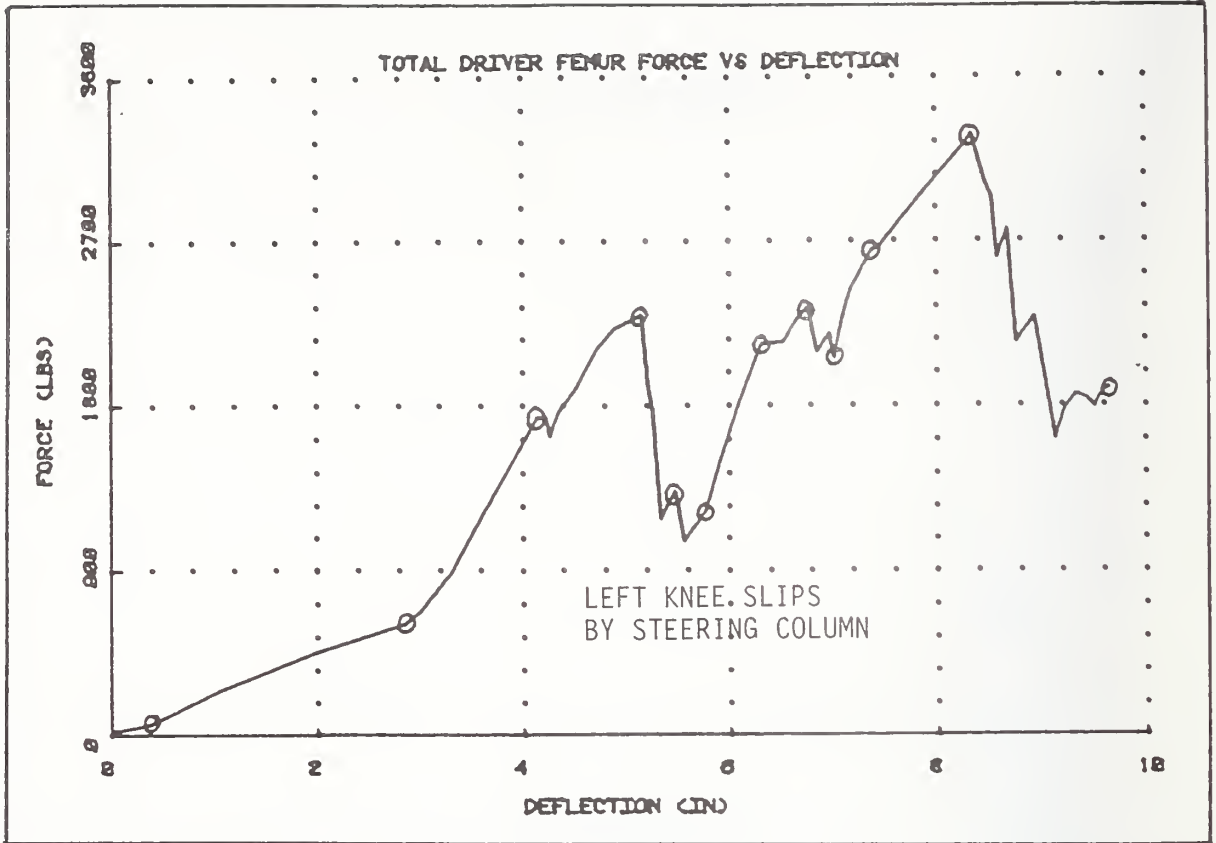
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
0.00	0.00	_____	_____
0.64	135.23	_____	_____
1.10	268.59	_____	_____
2.04	288.25	_____	_____
2.82	356.34	_____	_____
3.47	327.73	_____	_____
4.63	384.13	_____	_____
5.06	434.88	_____	_____
5.79	590.72	_____	_____
6.58	762.03	_____	_____

Test: Driver Side Femur (static)

Date: August 28, 1984

Vehicle: Ford LTD

Options: Air conditioning, radio missing



G= 0.769

R= 0.066

K= 1987

C=

$\mu_1$ =

$\mu_2$ =

$\mu_3$ =

$\delta_A$ = 0.0

$\delta_B$ = 0.0

$\delta_C$ = 0.0

$\delta_D$ = 1000.0

$\delta_F$ = 1000.1

Deflection

Force

Deflection

Force

0.00

0.00

7.39

2646.47

0.38

62.33

8.34

3280.81

2.86

611.75

9.64

1891.25

4.14

1734.33

5.15

2293.73

5.47

1339.26

5.77

1228.56

6.32

2138.37

6.77

2331.81

7.02

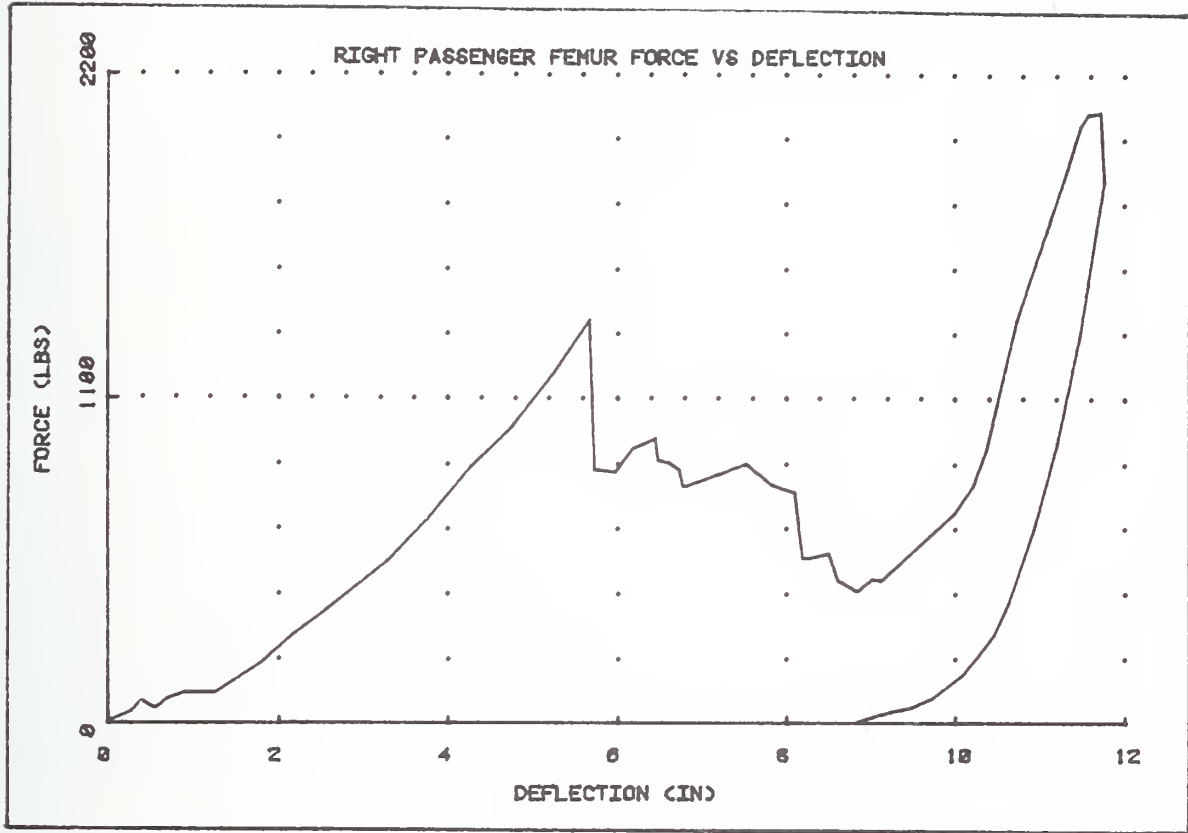
2048.00

Test Right Passenger Femur

Date: August 28, 1984

Vehicle: Ford LTD

Options: Air Conditioning, Radio missing



G= \_\_\_\_\_

R= \_\_\_\_\_

K= \_\_\_\_\_

Deflection

Force

Deflection

Force

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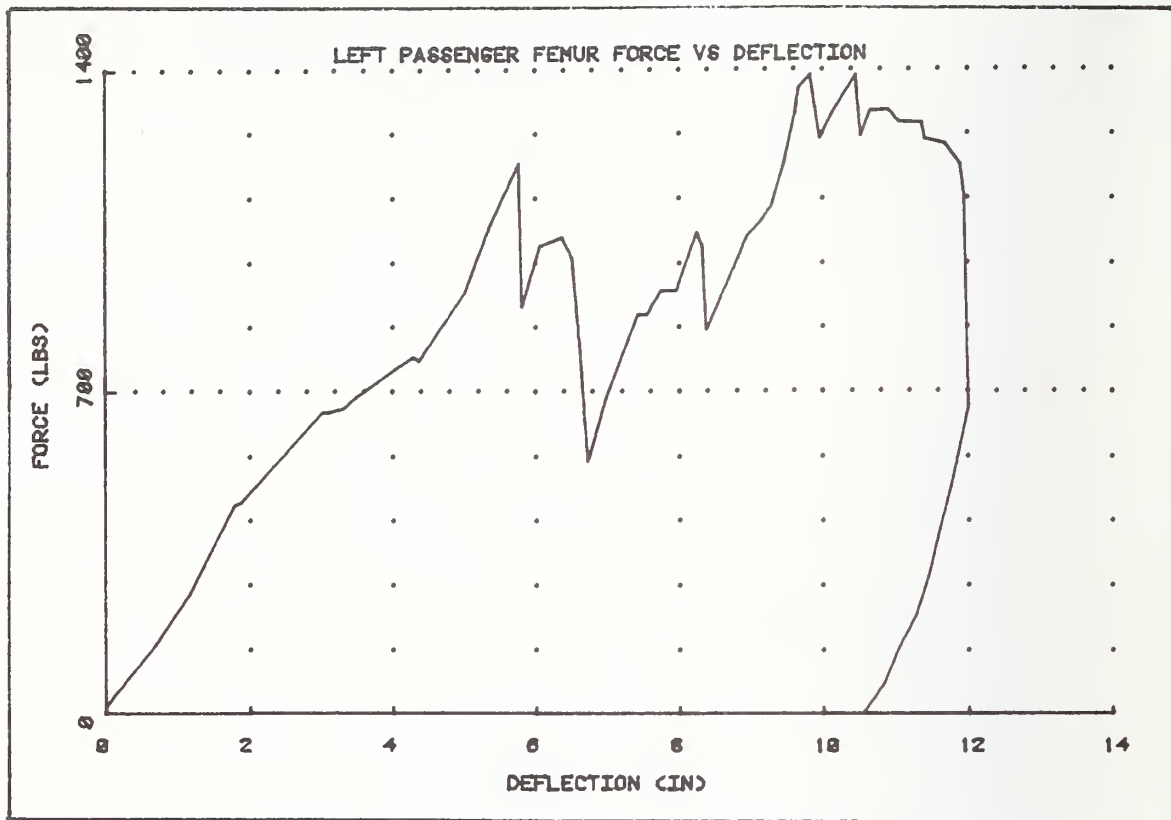
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Test Left Passenger Femur

Date: August 28, 1984

Vehicle: Ford LTD

Options: Air conditioning, Radio missing



G= \_\_\_\_\_

R= \_\_\_\_\_

K= \_\_\_\_\_

Deflection

Force

Deflection

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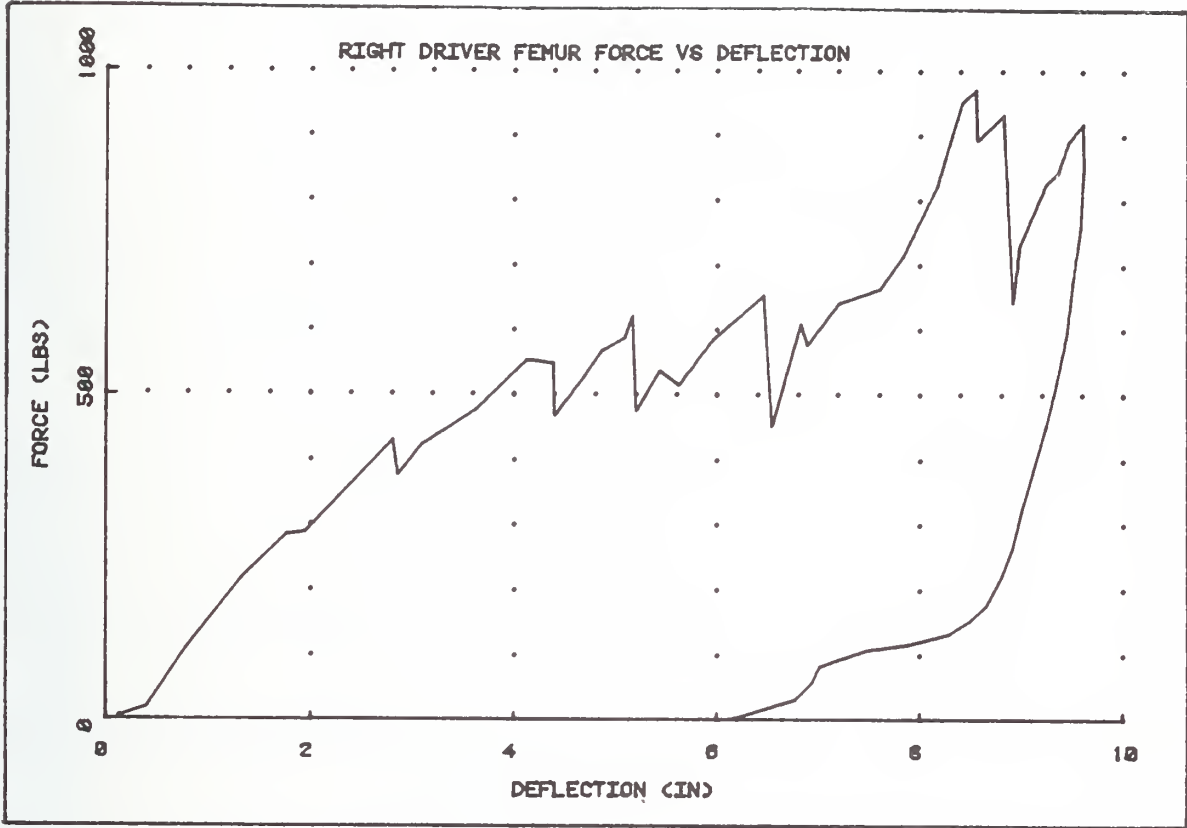


Test Right Driver Femur

Date: August 28, 1984

Vehicle: Ford LTD

Options: Air conditioning, Radio missing



G= \_\_\_\_\_

R= \_\_\_\_\_

K= \_\_\_\_\_

Deflection

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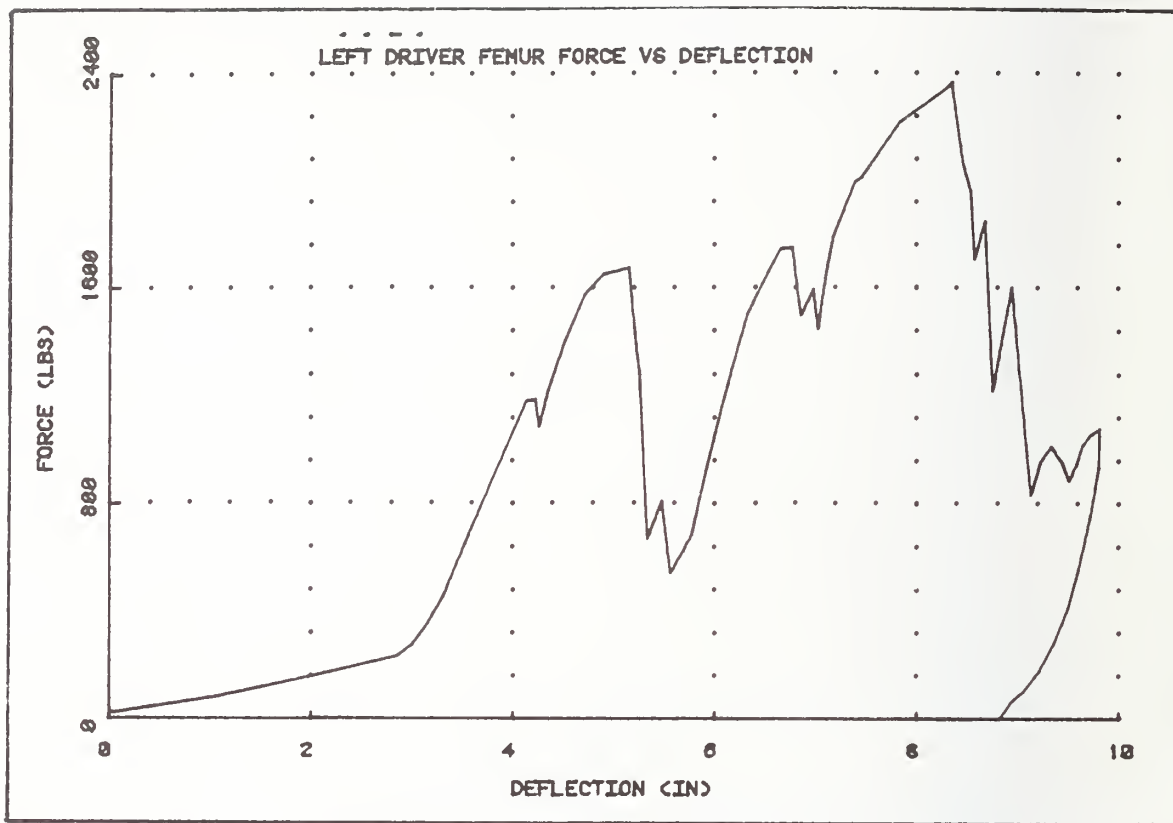
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Test Left Driver Femur

Date: August 28, 1984

Vehicle: Ford LTD

Options: Air conditioning, Radio missing



G= \_\_\_\_\_

R= \_\_\_\_\_

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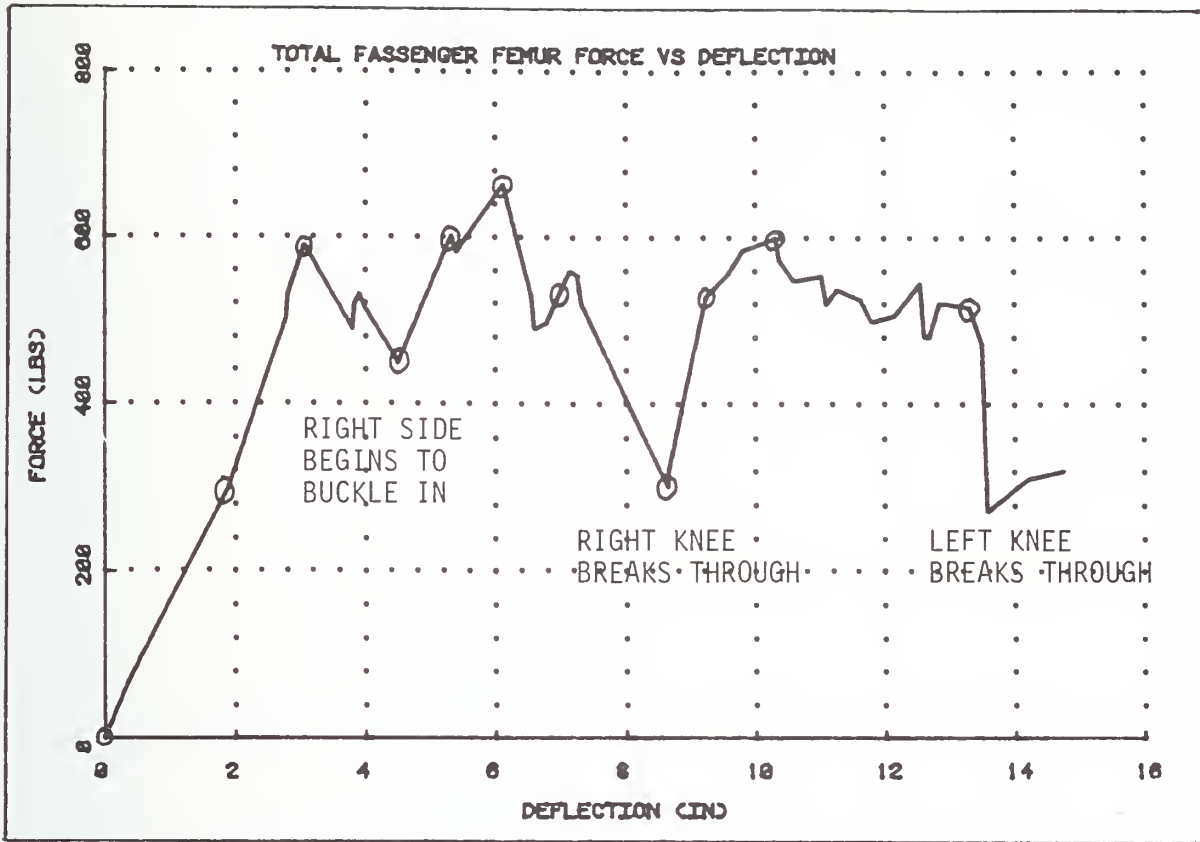
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Test: Passenger Side Femur (static) Date: August 31, 1984

Vehicle: Dodge Omni

Options: Metal dash top, no radio



G= 0.900 R= 0.016 K= 356

c= 0.16  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 1.92  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

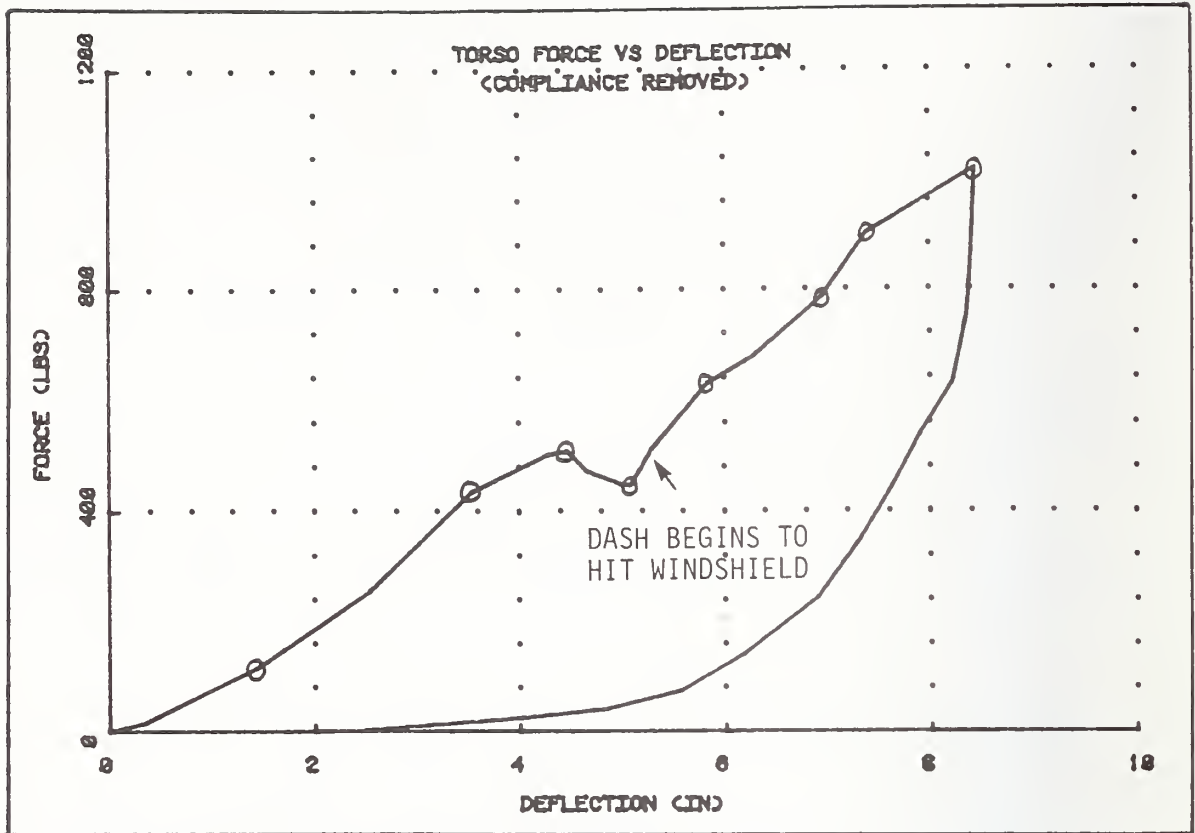
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
0.00	0.00	13.30	514.78
1.88	298.40		
3.05	589.33		
4.49	447.56		
5.32	601.65		
6.12	663.21		
7.13	558.43		
8.64	301.21		
9.23	527.81		
10.32	599.50		

Test: Torso (static)

Date: August 31, 1984

Vehicle: Dodge Omni

Options: Metal dash top, no radio



G= 0.292 R= 0.260 K= 294

c= 2.94  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

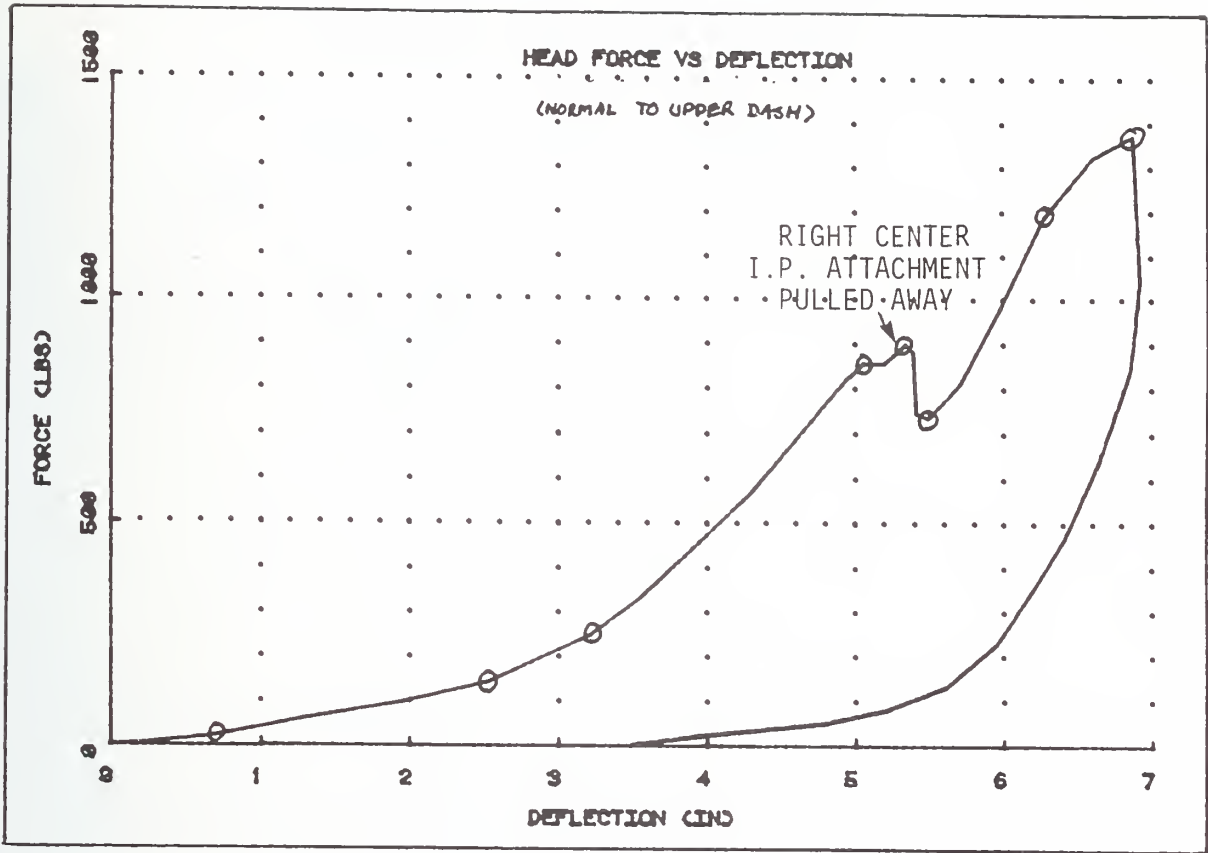
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 35.28  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
0.00	0.00		
1.44	116.80		
3.53	435.18		
4.46	509.37		
5.08	445.61		
5.84	629.89		
6.97	784.92		
7.40	901.70		
8.44	1017.52		

Test: Head (static) Date: August 31, 1984

Vehicle: Dodge Omni

Options: Metal dash top, no radio



G= 0.503 R= 0.210 K= 736

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

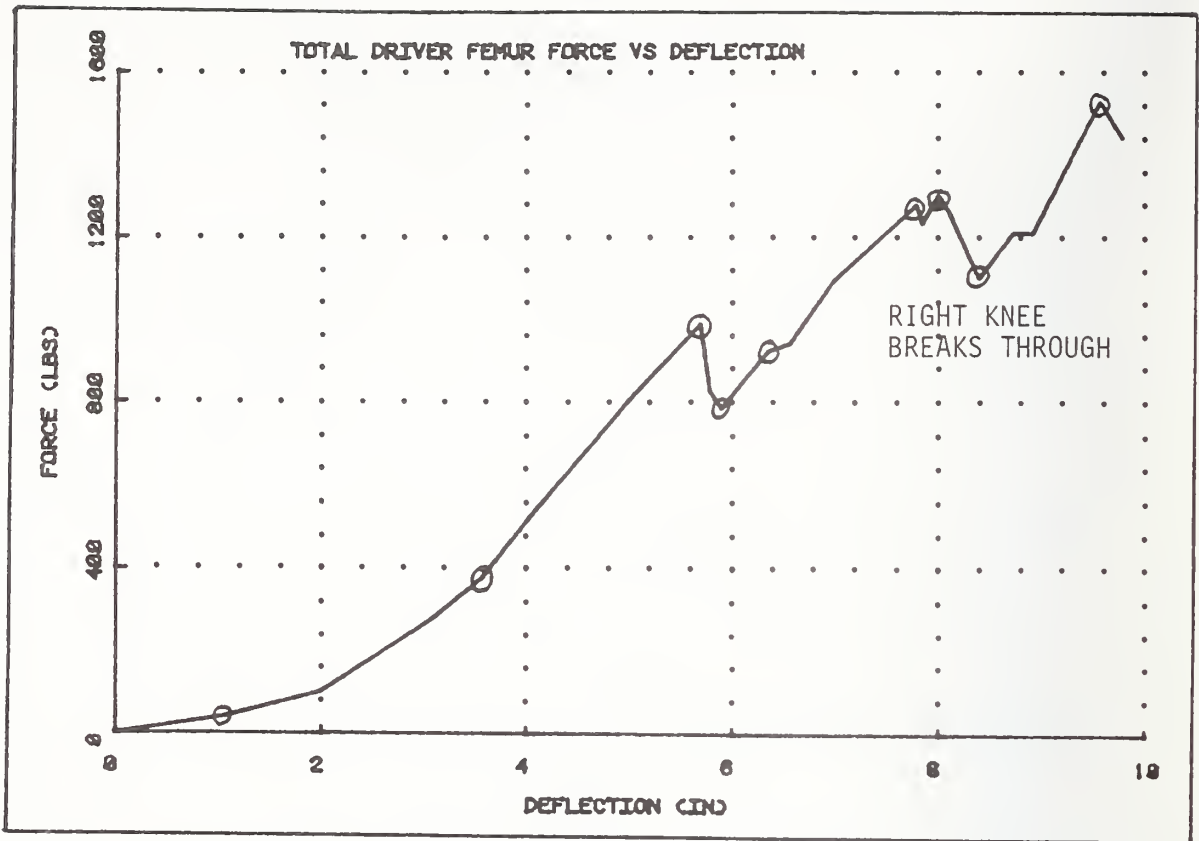
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
0.00	0.00		
0.69	21.23		
2.52	142.02		
3.21	246.65		
5.06	856.13		
5.34	898.81		
5.49	731.79		
6.27	1187.00		
6.88	1373.32		

Test: Driver Side Femur (static) Date: August 31, 1984

Vehicle: Dodge Omni

Options: Metal dash top, no radio



G= 0.706 R= 0.115 K= 961

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

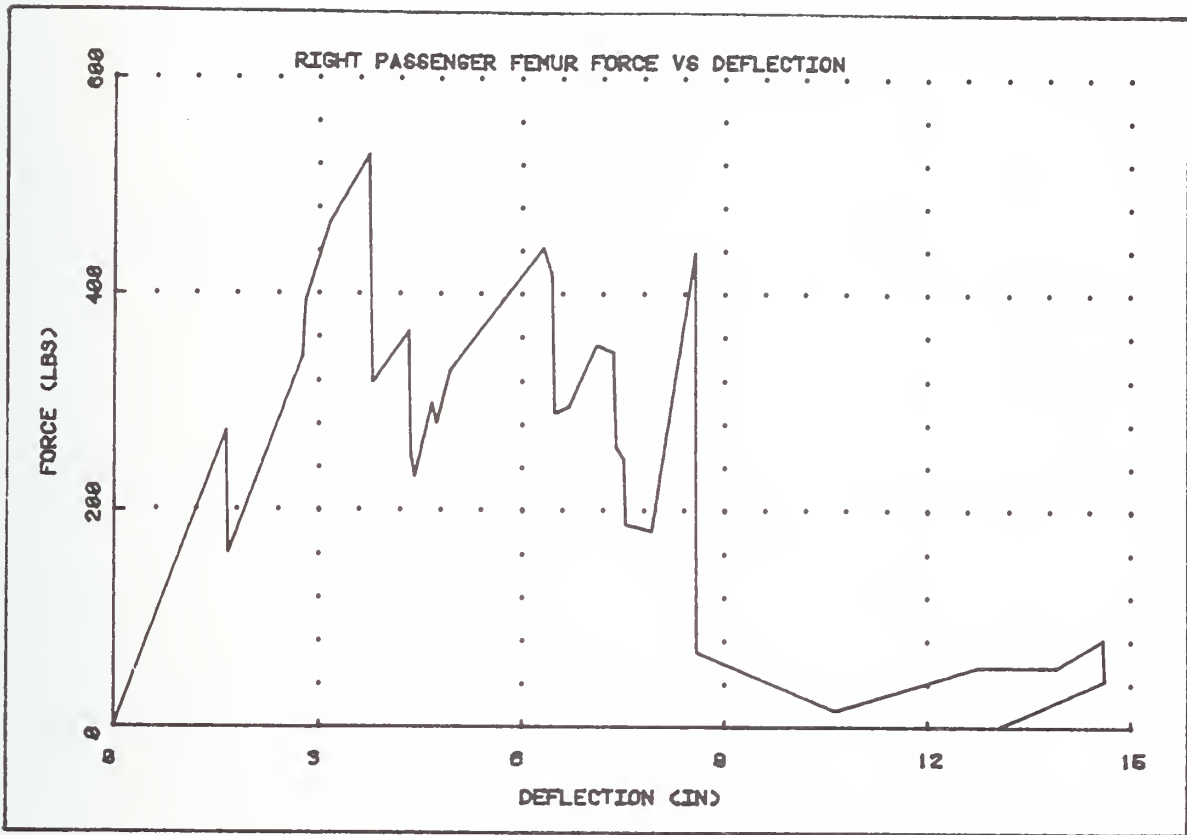
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
0.00	0.00		
1.08	41.93		
3.57	379.45		
5.69	986.46		
5.89	783.39		
6.36	923.12		
7.79	1278.67		
8.00	1302.37		
8.39	1097.80		
9.57	1527.42		

Test Right Passenger Femur

Date: August 31, 1984

Vehicle: Dodge Omni

Options: Metal dash top, No radio



G= \_\_\_\_\_

R= \_\_\_\_\_

K= \_\_\_\_\_

Deflection

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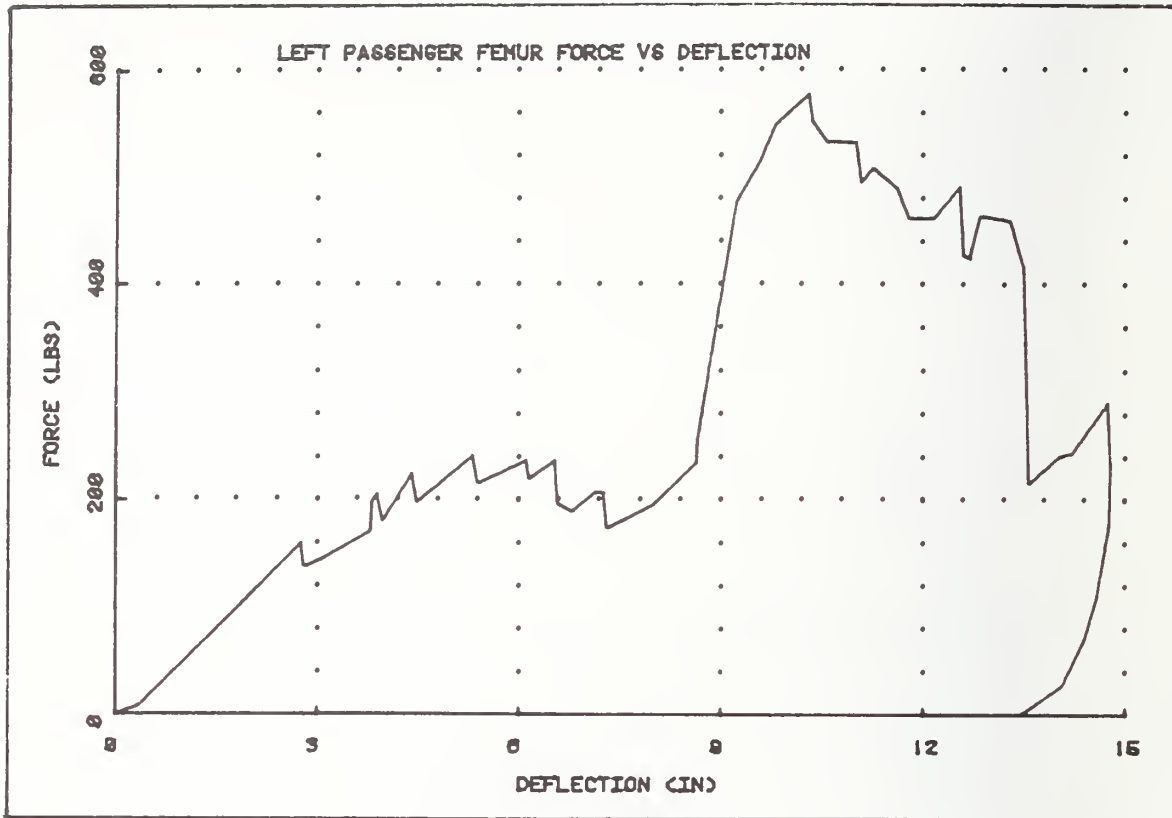
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Test Left Passenger Femur

Date: August 31, 1984

Vehicle: Dodge Omni

Options: Metal Dash top, No radio



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

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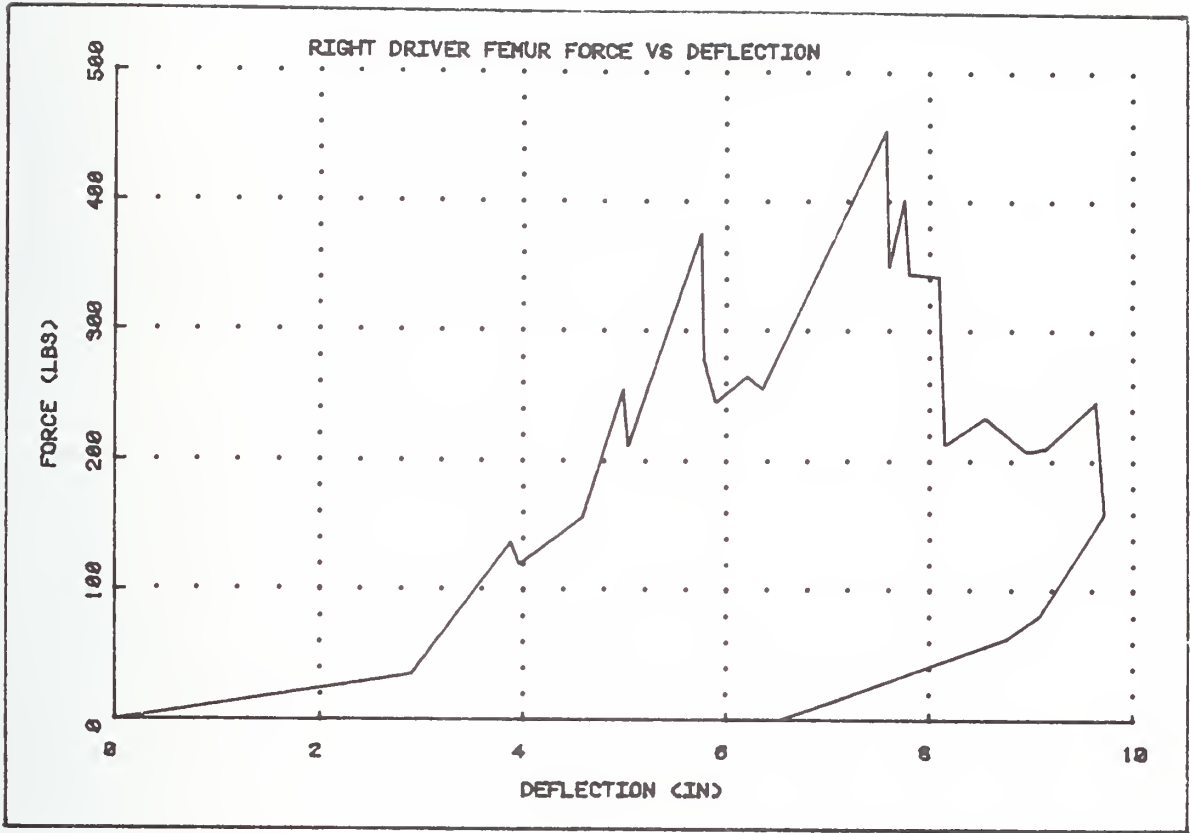


Test Right Driver Femur

Date: August 31, 1984

Vehicle: Dodge Omni

Options: Metal dash top, No radio



G= \_\_\_\_\_

R= \_\_\_\_\_

K= \_\_\_\_\_

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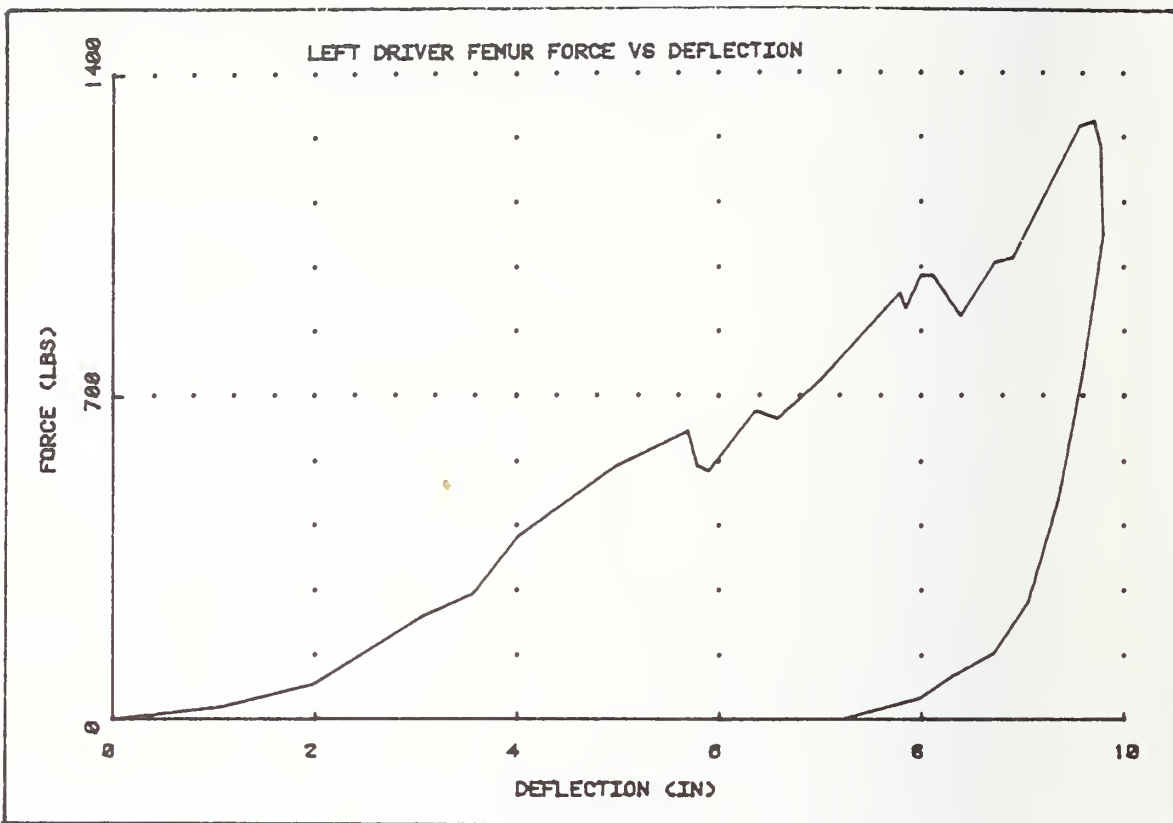
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Test Left Driver Femur

Date: August 31, 1984

Vehicle: Dodge Omni

Options: Metal dash top, No radio



G= \_\_\_\_\_

R= \_\_\_\_\_

K= \_\_\_\_\_

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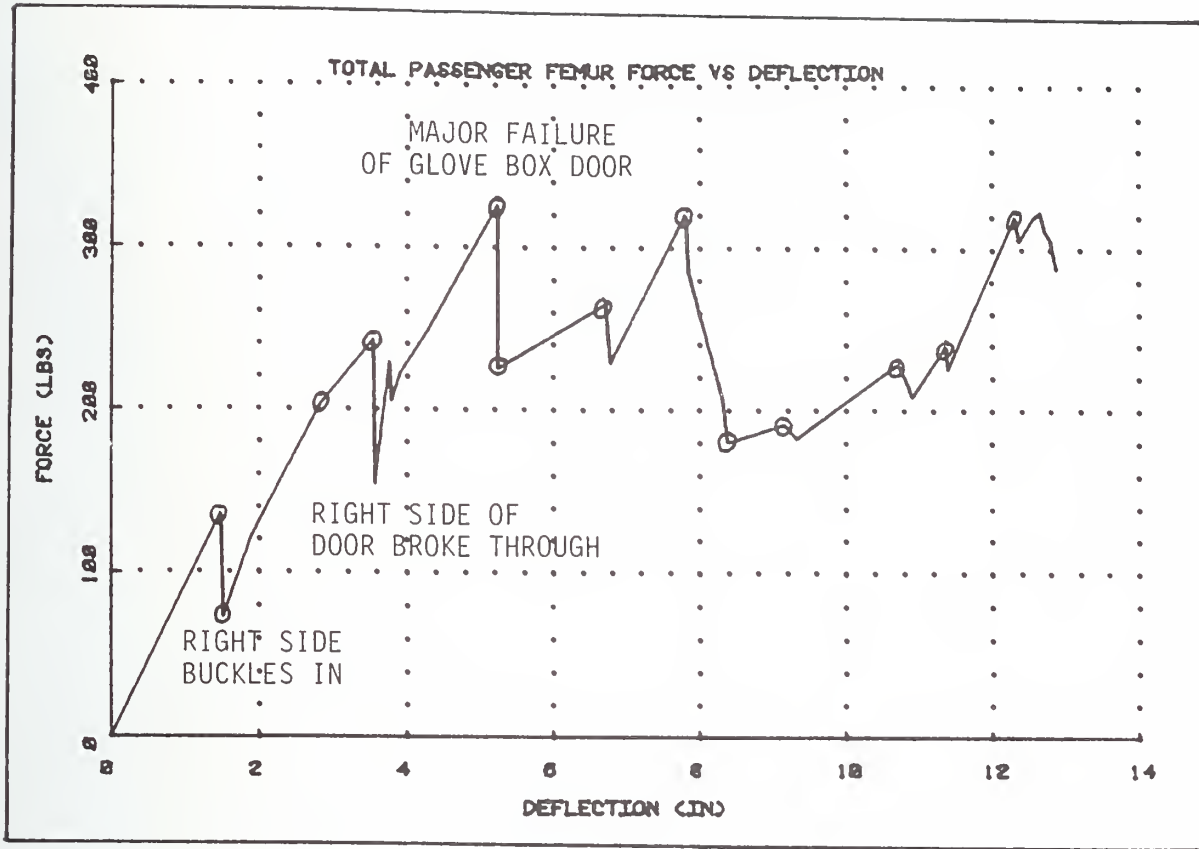
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Test: Passenger Side Femur (static) Date: September 5, 1984

Vehicle: Ford Mustang

Options: \_\_\_\_\_



G= 0.957 R= 0.012 K= 1131

c= 1.01  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

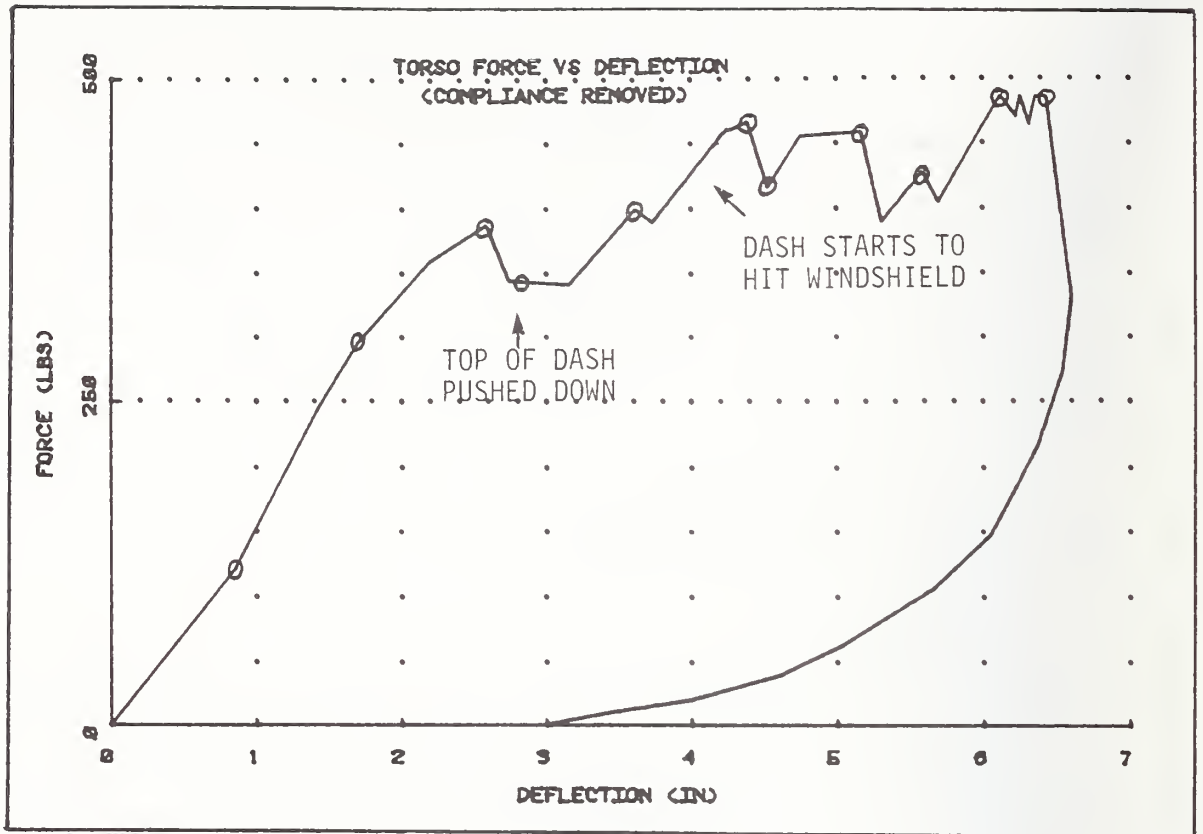
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 12.12  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
0.00	0.00	9.15	191.19
1.48	136.11	10.71	228.18
1.51	72.30	11.37	239.48
2.82	202.13	12.31	320.27
3.53	242.49		
5.23	326.06		
5.231	224.99		
6.71	265.11		
7.79	320.87		
8.37	179.81		

Test: Torso (static) Date: September 5, 1984

Vehicle: Ford Mustang

Options: \_\_\_\_\_



G= 0.454 R= 0.122 K= 273

c= 0.69  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

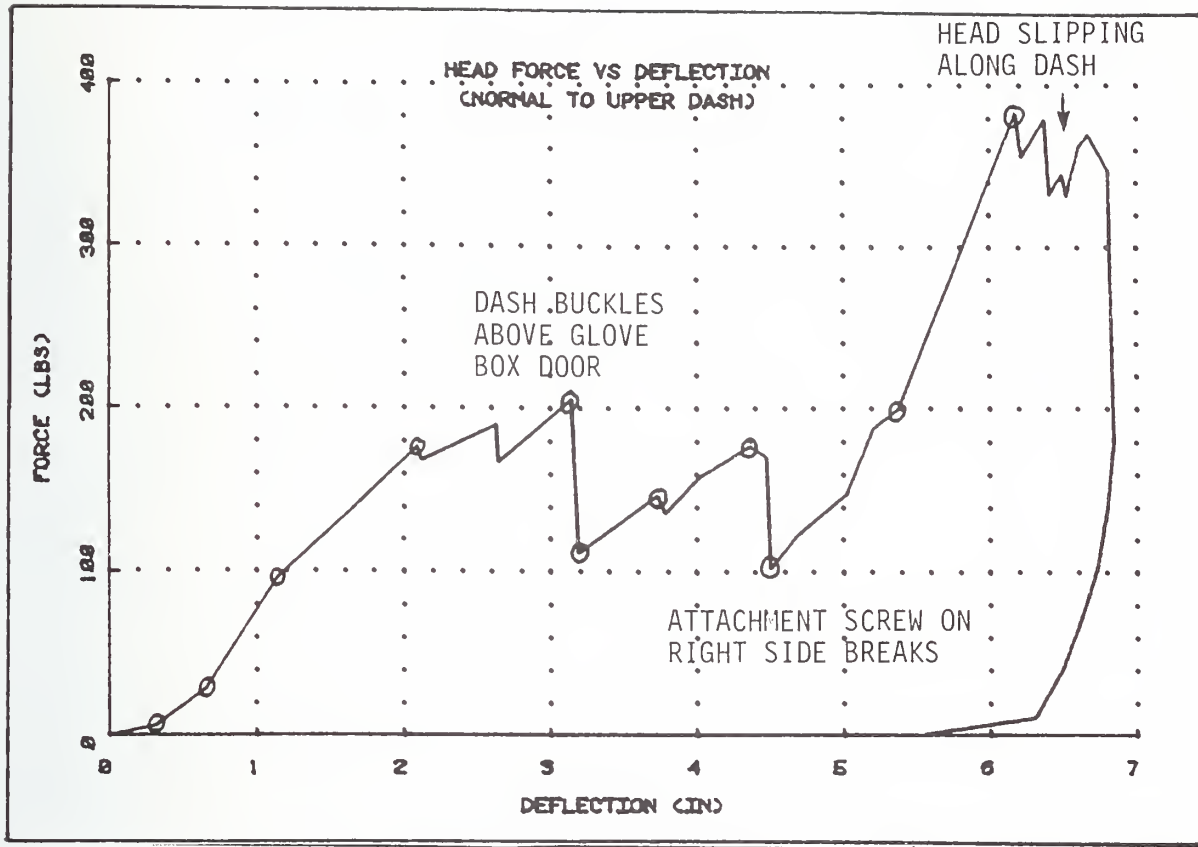
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 8.28  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
0.00	0.00	6.12	486.05
0.85	121.69	6.44	484.70
1.69	295.72		
2.58	387.64		
2.74	343.55		
3.60	399.08		
4.39	466.80		
4.53	415.87		
5.17	458.53		
5.59	427.14		

Test: Head (static) Date: September 5, 1984

Vehicle: Ford Mustang

Options: \_\_\_\_\_



G= 0.811 R= 0.036 K= 232

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

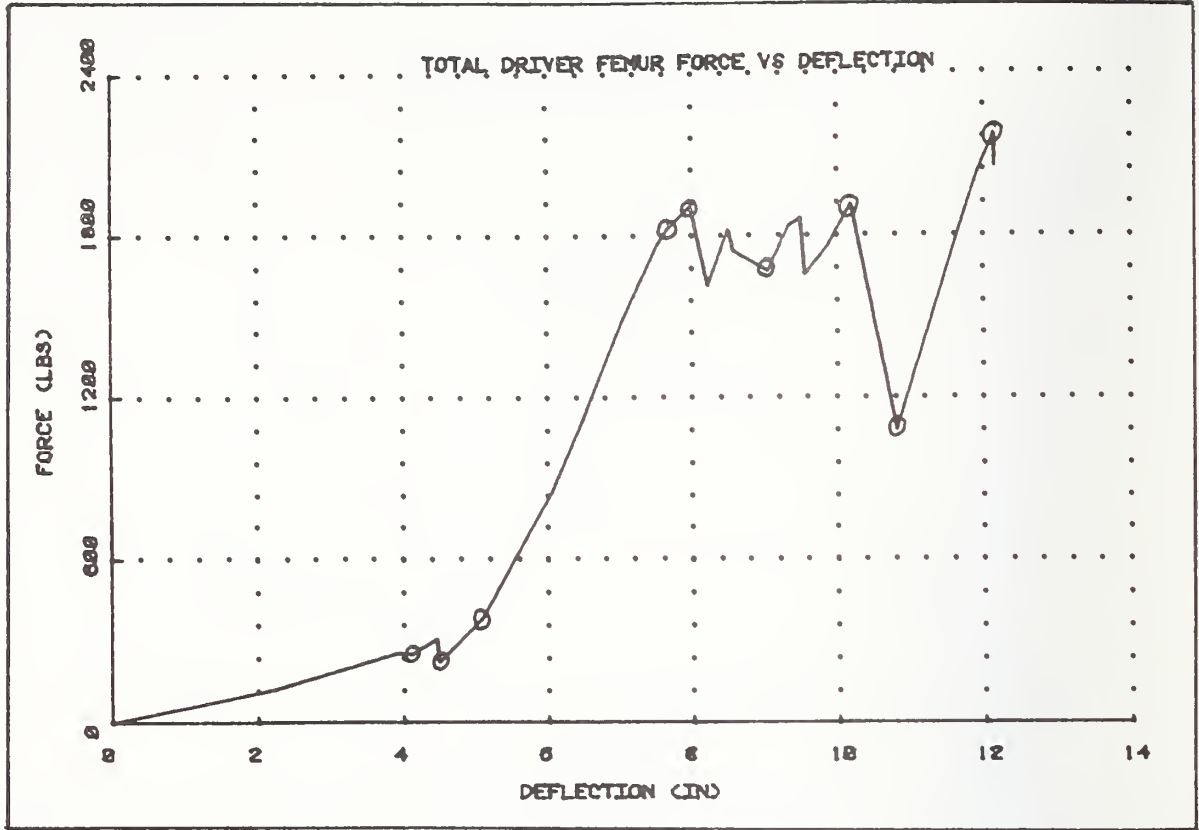
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
0.00	0.00	5.38	200.00
0.31	6.11	6.18	383.34
0.65	28.33		
1.14	96.66		
2.09	176.11		
3.14	205.56		
3.19	111.66		
3.72	146.67		
4.35	177.22		
4.50	101.66		

Test: Driver Side Femur (static) Date: September 5, 1984

Vehicle: Ford Mustang

Options: \_\_\_\_\_



G= 0.801 R= 0.105 K= 1519

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

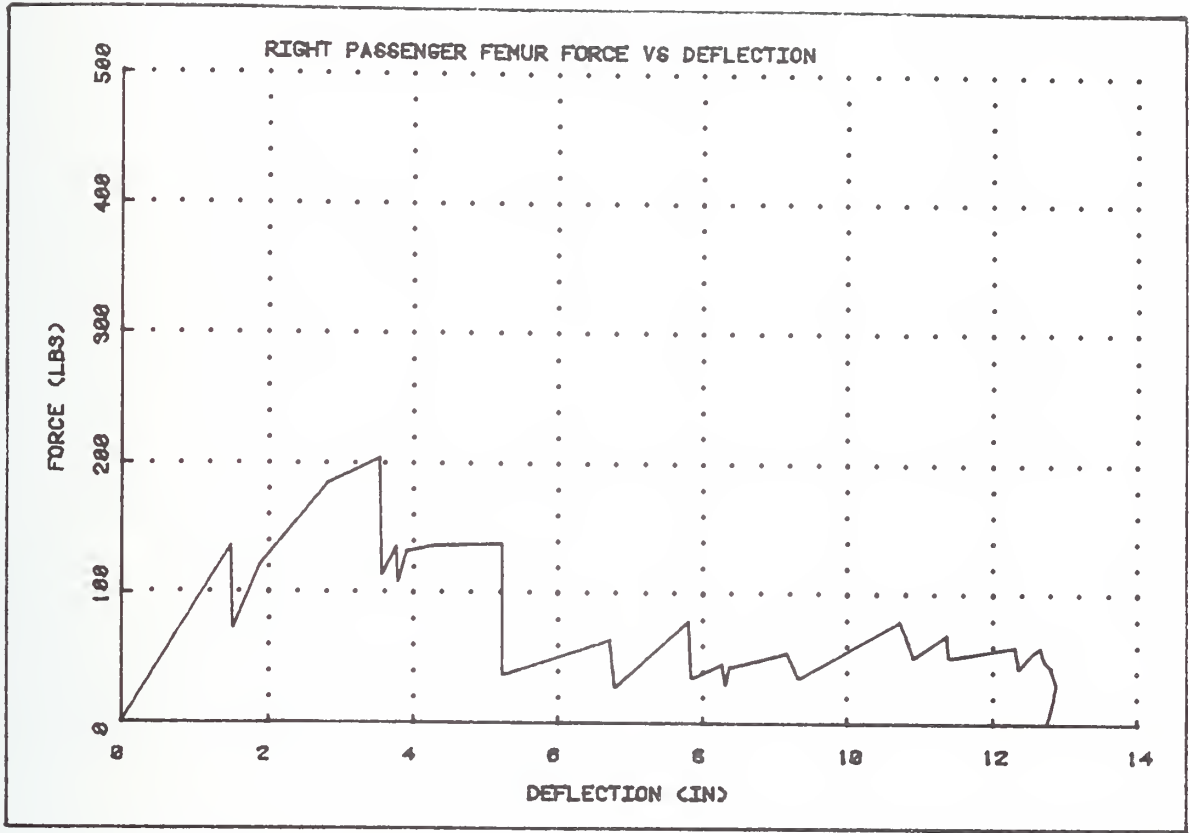
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
0.00	0.00		
4.09	250.57		
4.48	221.54		
5.10	388.52		
7.66	1824.67		
7.98	1907.46		
9.03	1665.69		
10.20	1912.52		
10.81	1076.28		
12.15	2171.27		

Test Right Passenger Femur

Date: September 5, 1984

Vehicle: Ford Mustang

Options: \_\_\_\_\_  
\_\_\_\_\_



G= \_\_\_\_\_

R= \_\_\_\_\_

K= \_\_\_\_\_

Deflection

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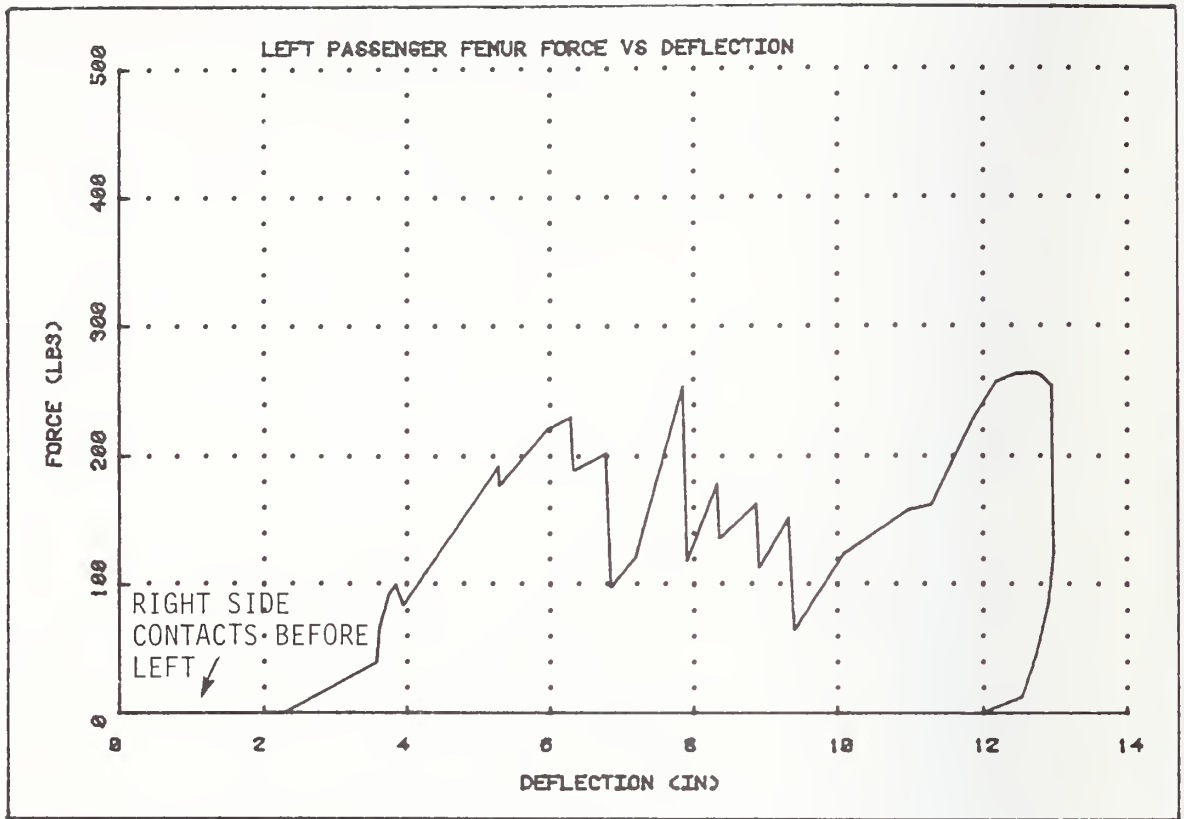
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Test Left Passenger Femur

Date: September 5, 1984

Vehicle: Ford Mustang

Options: \_\_\_\_\_



G= \_\_\_\_\_

R= \_\_\_\_\_

K= \_\_\_\_\_

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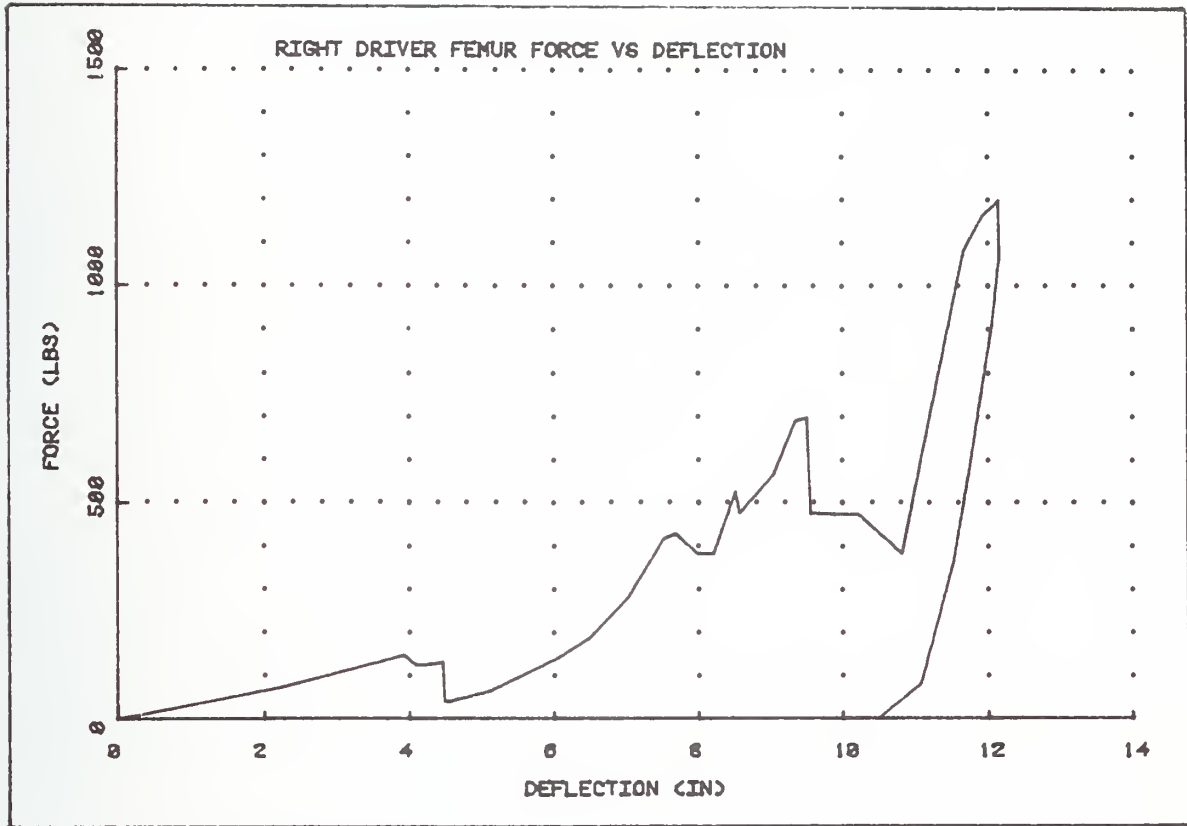
Test Right Driver Femur

Date: September 5, 1984

Vehicle: Ford Mustang

Options: \_\_\_\_\_

\_\_\_\_\_



G= \_\_\_\_\_

R= \_\_\_\_\_

K= \_\_\_\_\_

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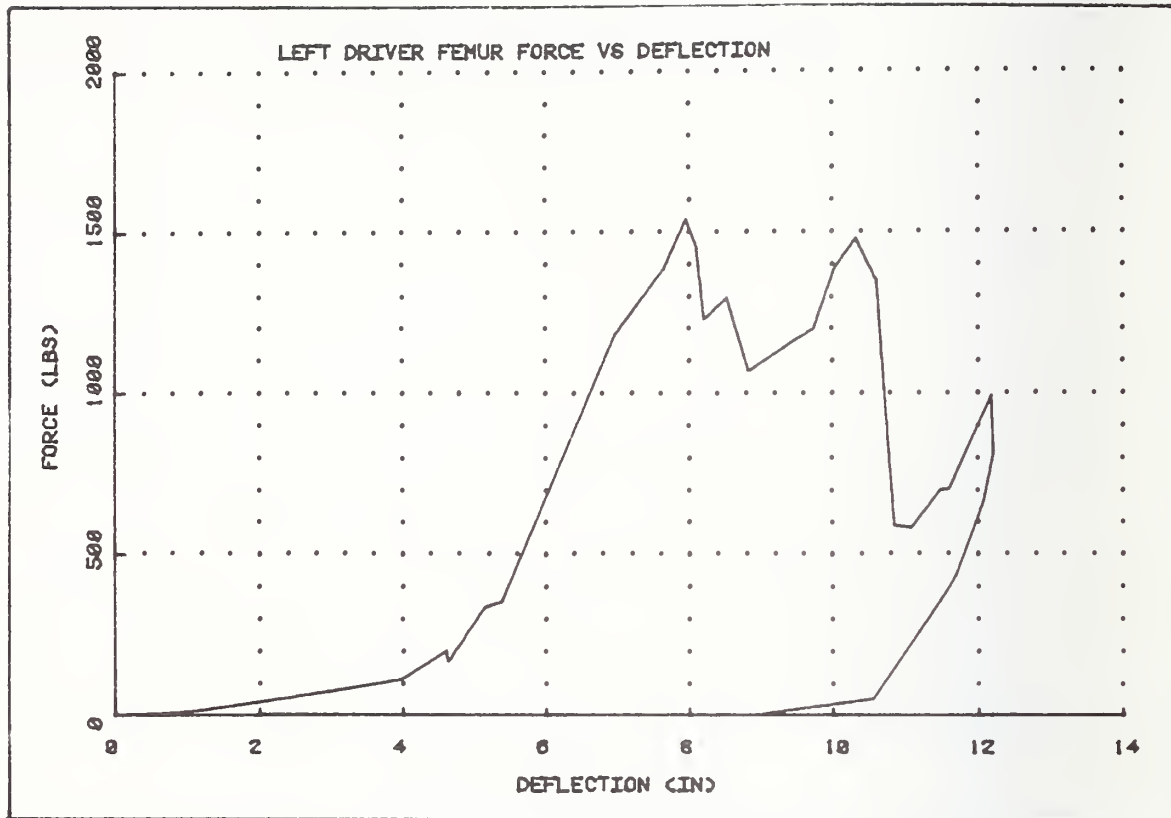
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Test Left Driver Femur

Date: September 5, 1984

Vehicle: Ford Mustang

Options: \_\_\_\_\_



G= \_\_\_\_\_

R= \_\_\_\_\_

K= \_\_\_\_\_

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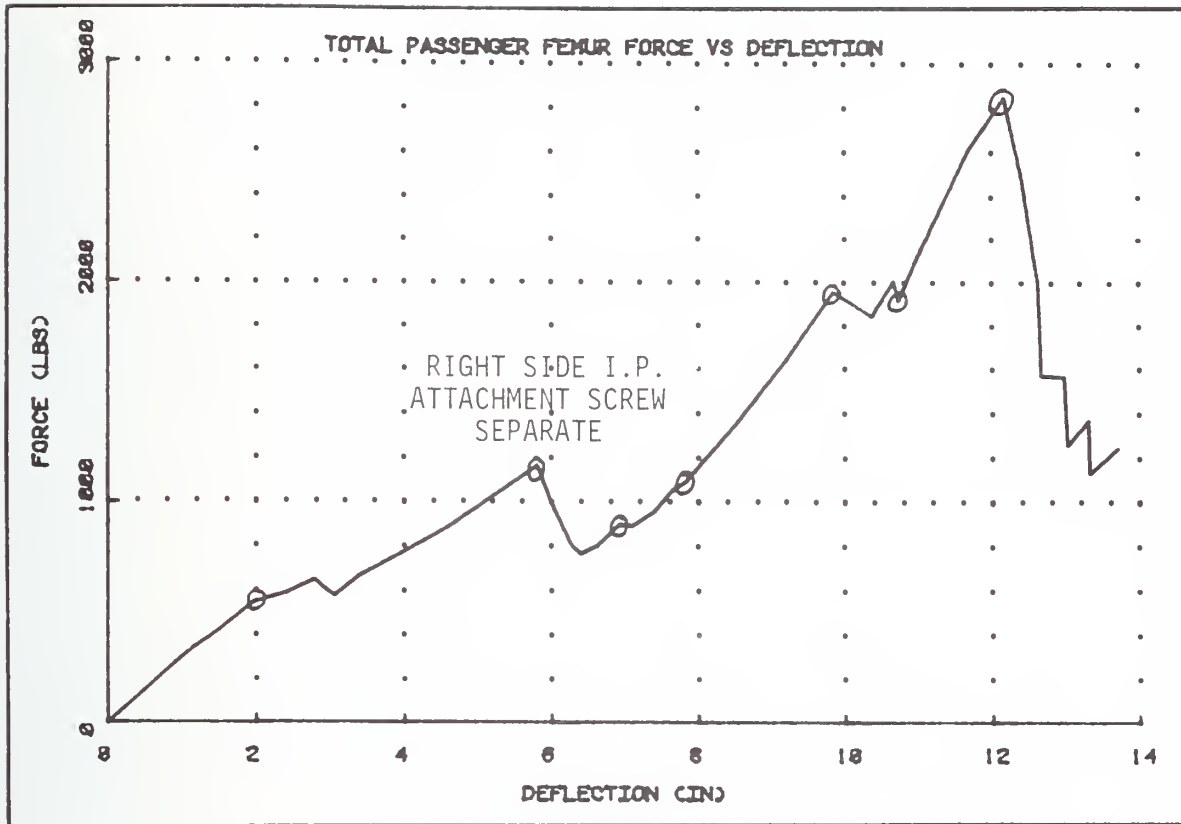
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Test: Passenger Side Femur (static) Date: September 11, 1984

Vehicle: Ford Pinto

Options: Metal dash with foam crash pad on top,  
heat control and radio missing



G= 0.871 R= 0.034 K= 1030

c= 0.64  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

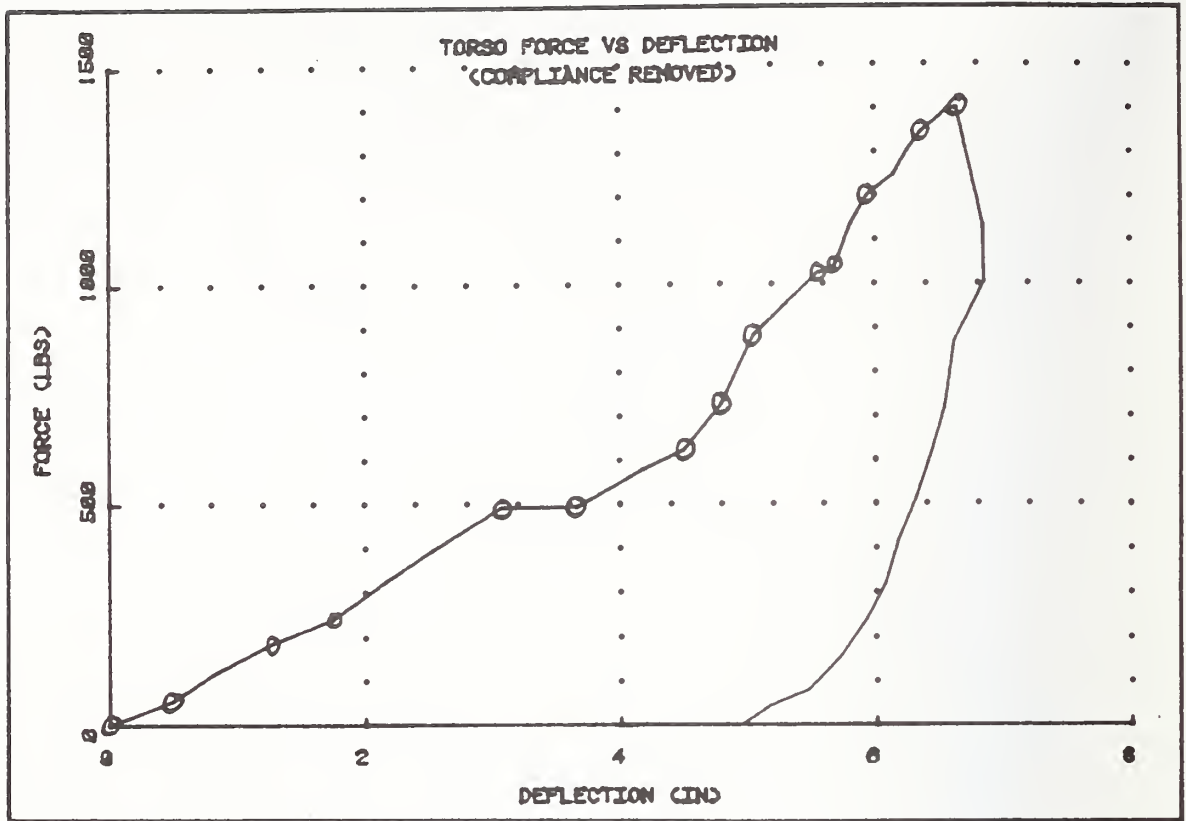
$\delta_A$ = \_\_\_\_\_  $\delta_B$ = \_\_\_\_\_  $\delta_C$ = 7.68  $\delta_D$ = \_\_\_\_\_  $\delta_F$ = \_\_\_\_\_

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
0.00	0.00		
2.02	560.64		
5.80	1175.04		
6.91	890.88		
7.82	1082.88		
9.85	1950.72		
10.76	1904.64		
12.15	2849.28		

Test: Torso Date: September 11, 1984

Vehicle: Ford Pinto

Options: Metal dash with foam crash pad on top,  
Heat control and radio missing.



G= 0.723 R= 0.165 K= 786.46

C= 2.51  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

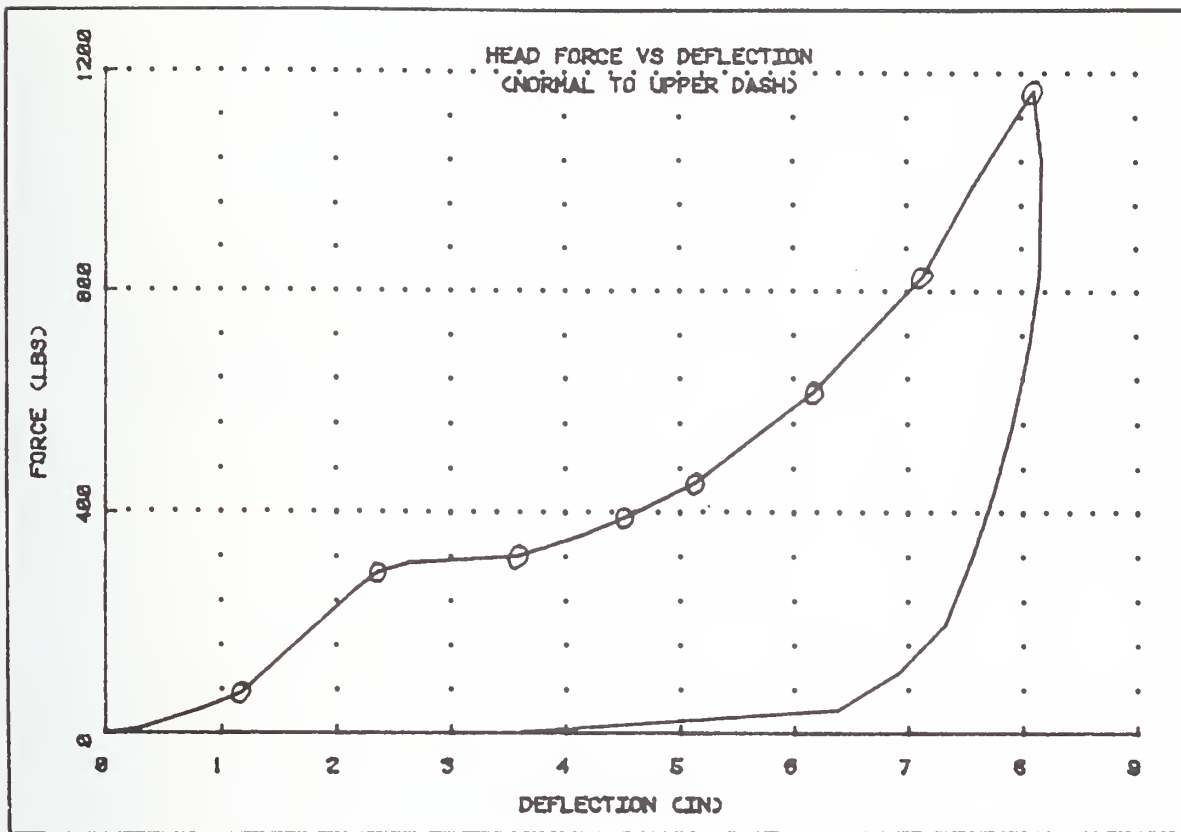
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 30.12  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>5.05</u>	<u>883.11</u>
<u>0.50</u>	<u>56.73</u>	<u>5.55</u>	<u>1024.84</u>
<u>1.25</u>	<u>184.70</u>	<u>5.67</u>	<u>1036.27</u>
<u>1.75</u>	<u>240.42</u>	<u>5.95</u>	<u>1201.17</u>
<u>3.07</u>	<u>493.86</u>	<u>6.36</u>	<u>1344.29</u>
<u>3.67</u>	<u>495.42</u>	<u>6.64</u>	<u>1400.42</u>
<u>4.51</u>	<u>623.60</u>		
<u>4.80</u>	<u>726.18</u>		

Test: Head (static) Date: September 11, 1984

Vehicle: Ford Pinto

Options: Metal dash with foam crash pad on top,  
heat control and radio missing



G= 0.440 R= 0.159 K= 787

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

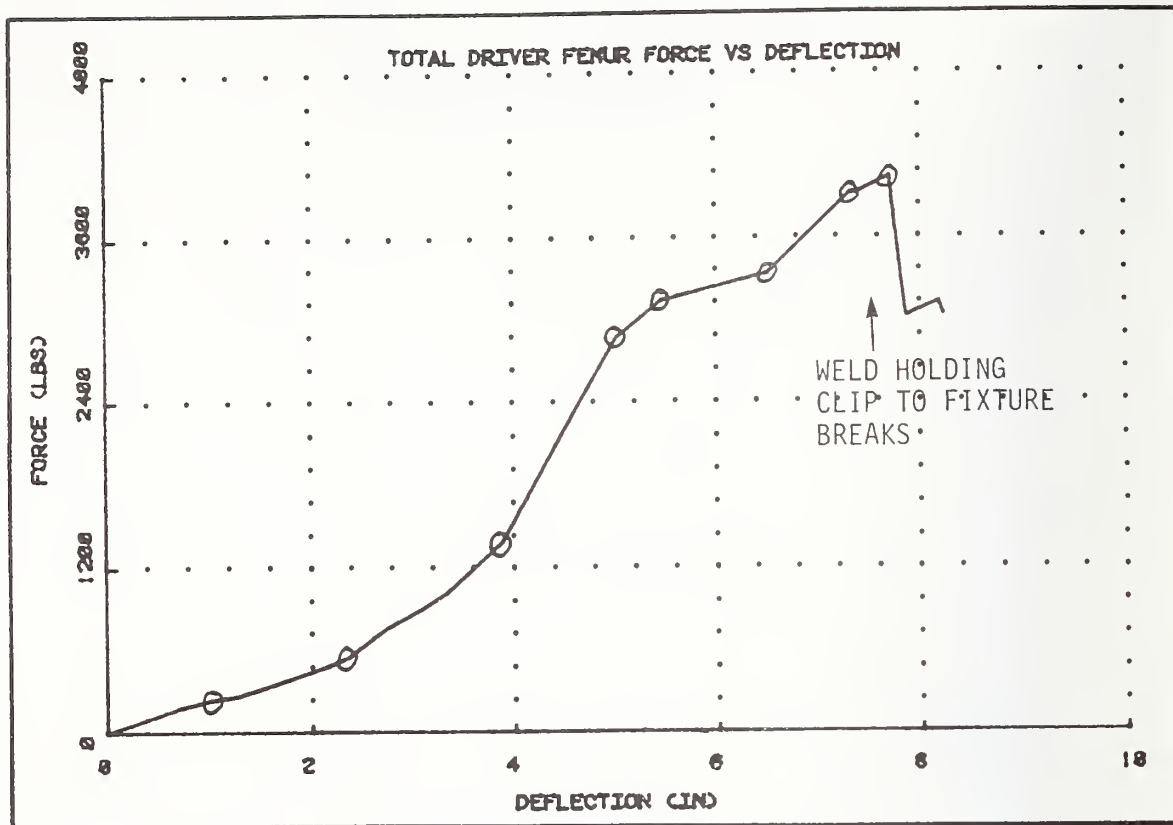
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
0.00	0.00		
1.16	73.72		
2.33	294.91		
3.59	324.09		
4.49	390.14		
5.16	462.33		
6.20	623.61		
7.15	827.90		
8.09	1188.89		

Test: Driver Side Femur (static) Date: September 11, 1984

Vehicle: Ford Pinto

Options: Metal dash with foam crash pad on top,  
heat control and radio missing



G= 0.687 R= 0.193 K= 1409

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = \_\_\_\_\_  $\delta_B$ = \_\_\_\_\_  $\delta_C$ = \_\_\_\_\_  $\delta_D$ = \_\_\_\_\_  $\delta_F$ = \_\_\_\_\_

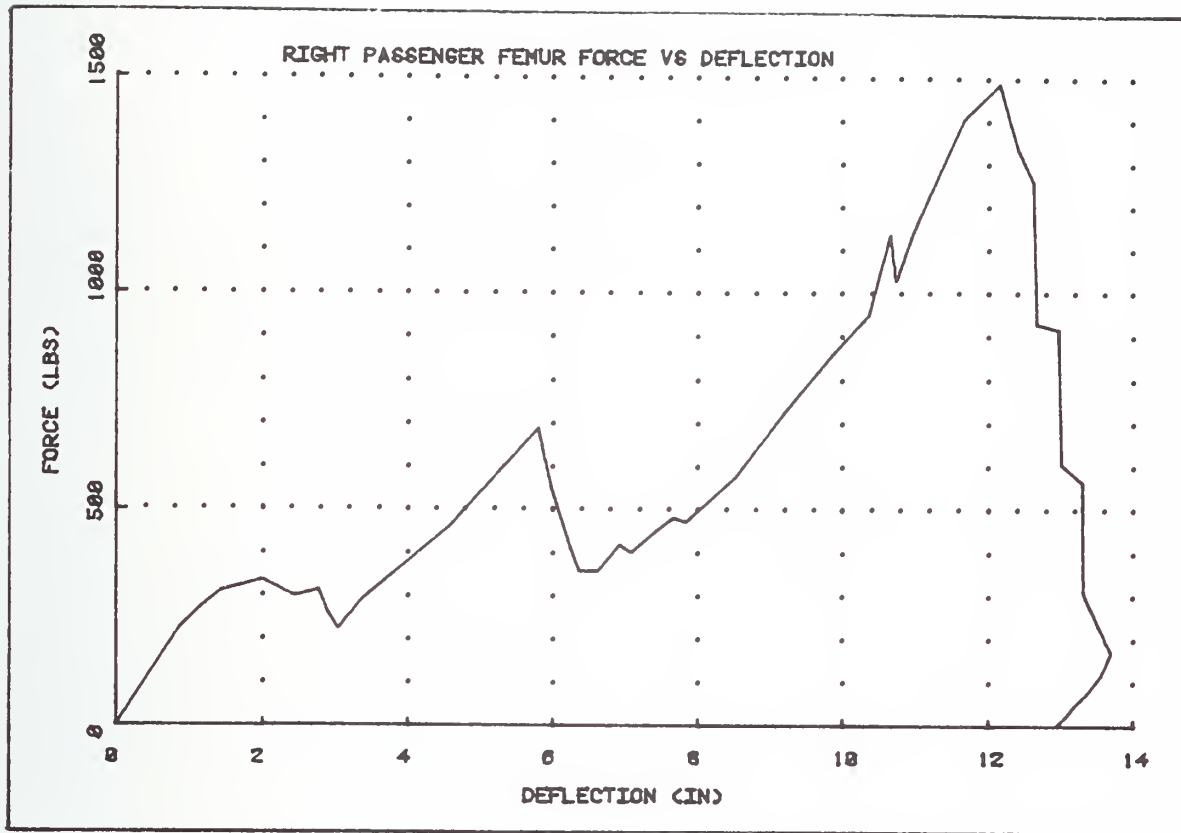
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
0.00	0.00	_____	_____
1.04	245.76	_____	_____
2.39	559.10	_____	_____
3.88	1394.68	_____	_____
5.04	2856.96	_____	_____
5.43	3121.15	_____	_____
6.52	3336.19	_____	_____
7.32	3913.72	_____	_____
7.71	4030.46	_____	_____
_____	_____	_____	_____

Test Right Passenger Femur

Date: September 11, 1984

Vehicle: Ford Pinto

Options: Metal dash with foam crash pad on top, Heat control and radio missing



G= \_\_\_\_\_

R= \_\_\_\_\_

K= \_\_\_\_\_

Deflection

Force

Deflection

Force

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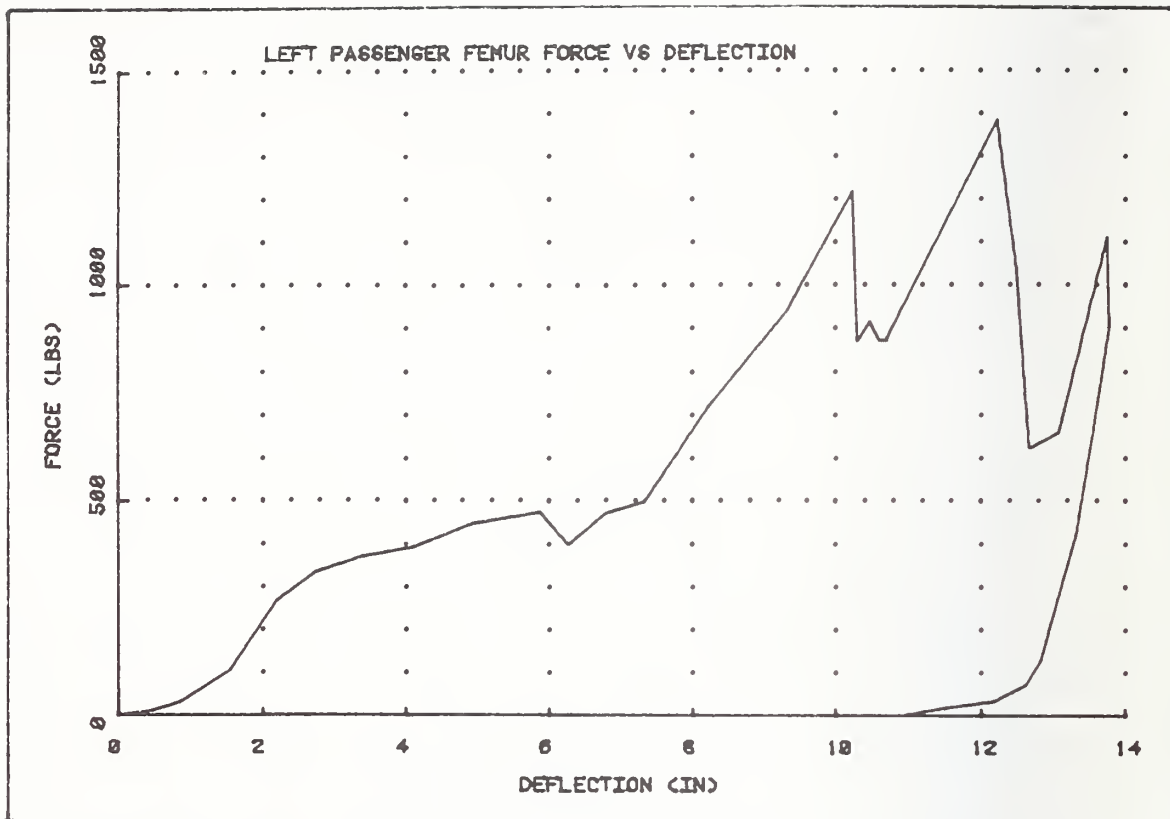
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Test Left Passenger Femur

Date: September 11, 1984

Vehicle: Ford Pinto

Options: Metal dash with foam crash pad on top, Heat control and radio  
missing



G= \_\_\_\_\_

R= \_\_\_\_\_

K= \_\_\_\_\_

Deflection

Force

Deflection

Force

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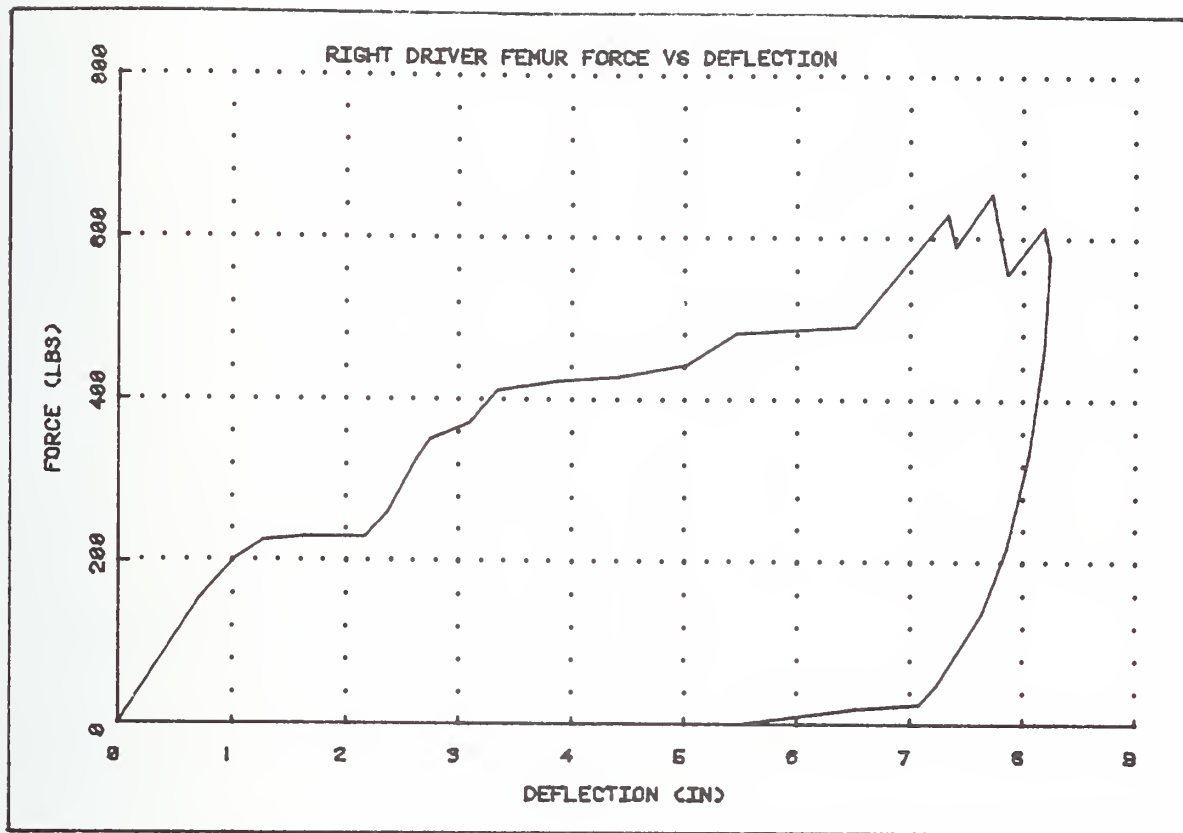


Test Right Driver Femur

Date: September 11, 1984

Vehicle: Ford Pinto

Options: Metal dash with foam crash pad on top, Heat control and radio missing



G= \_\_\_\_\_

R= \_\_\_\_\_

K= \_\_\_\_\_

Deflection

Force

Deflection

Force

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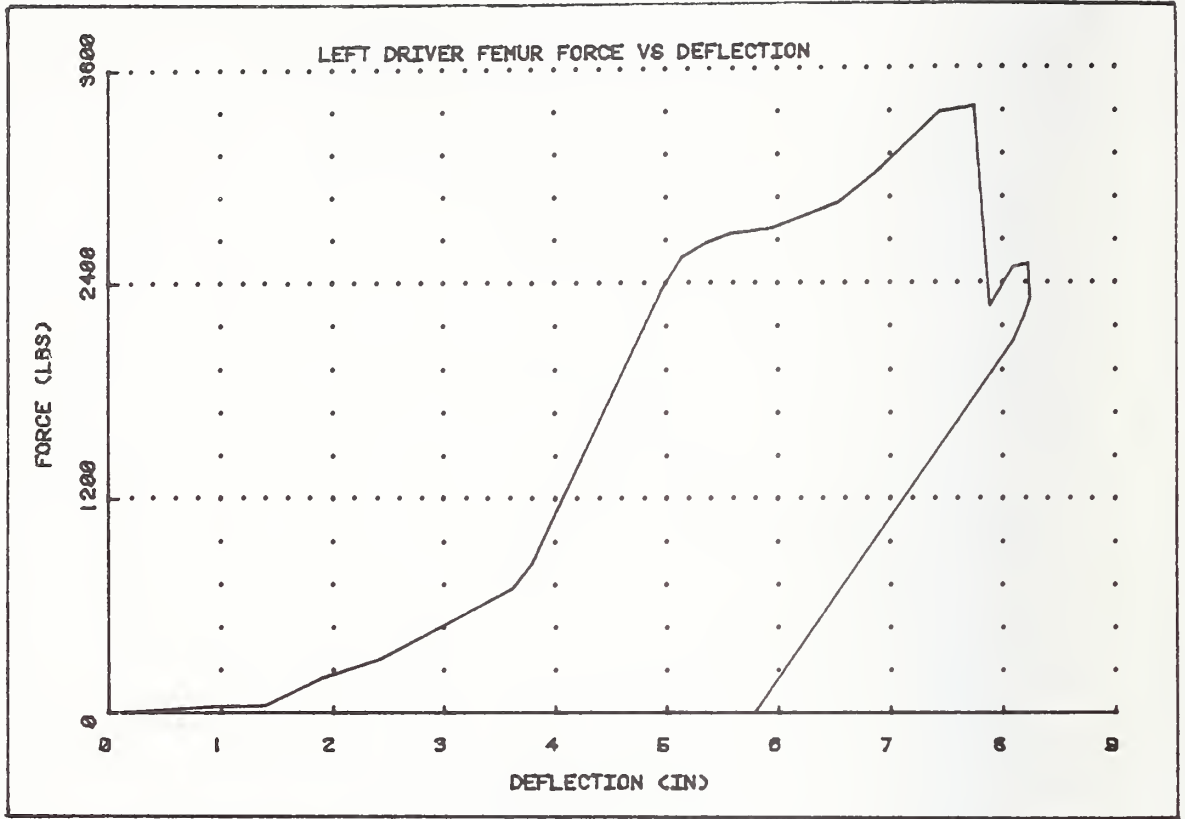
\_\_\_\_\_  
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\_\_\_\_\_

Test Left Driver Femur

Date: September 11, 1984

Vehicle: Ford Pinto

Options: Metal dash with foam crash pad on top, Heat control and radio  
missing



G= \_\_\_\_\_

R= \_\_\_\_\_

K= \_\_\_\_\_

Deflection

Force

Deflection

Force

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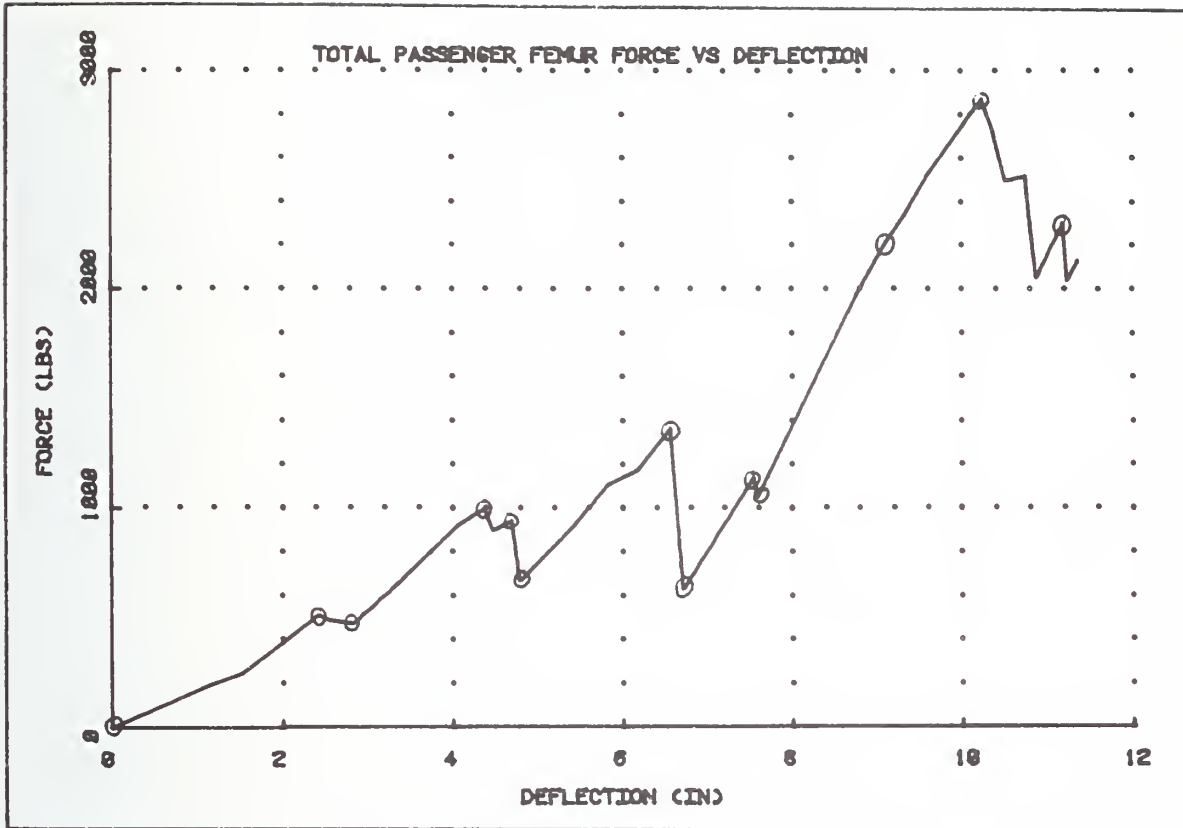
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Test: Total Passenger Femur (Static) Date: November 29, 1984

Vehicle: Ford Fairmont

Options: \_\_\_\_\_



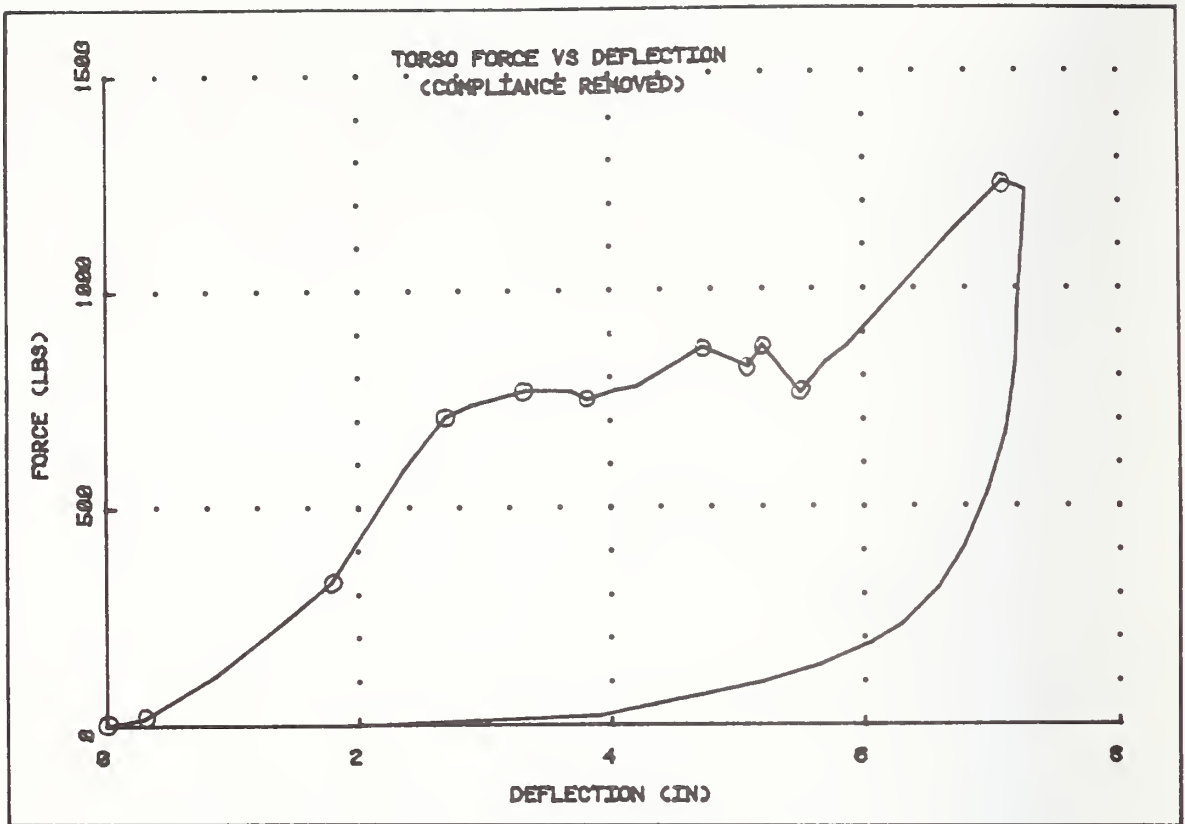
G= 0.862 R= 0.049 K= 2664

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>7.54</u>	<u>1140.3</u>
<u>2.41</u>	<u>505.7</u>	<u>7.59</u>	<u>1049.11</u>
<u>2.81</u>	<u>466.1</u>	<u>9.10</u>	<u>2200.8</u>
<u>4.37</u>	<u>1000.4</u>	<u>10.24</u>	<u>2870.7</u>
<u>4.70</u>	<u>940.9</u>	<u>11.19</u>	<u>2302.9</u>
<u>4.79</u>	<u>663.6</u>		
<u>6.56</u>	<u>1362.7</u>		
<u>6.71</u>	<u>628.1</u>		

Test: Torso (Static) Date: November 24, 1984  
 Vehicle: Ford Fairmont  
 Options: Compliance Removed



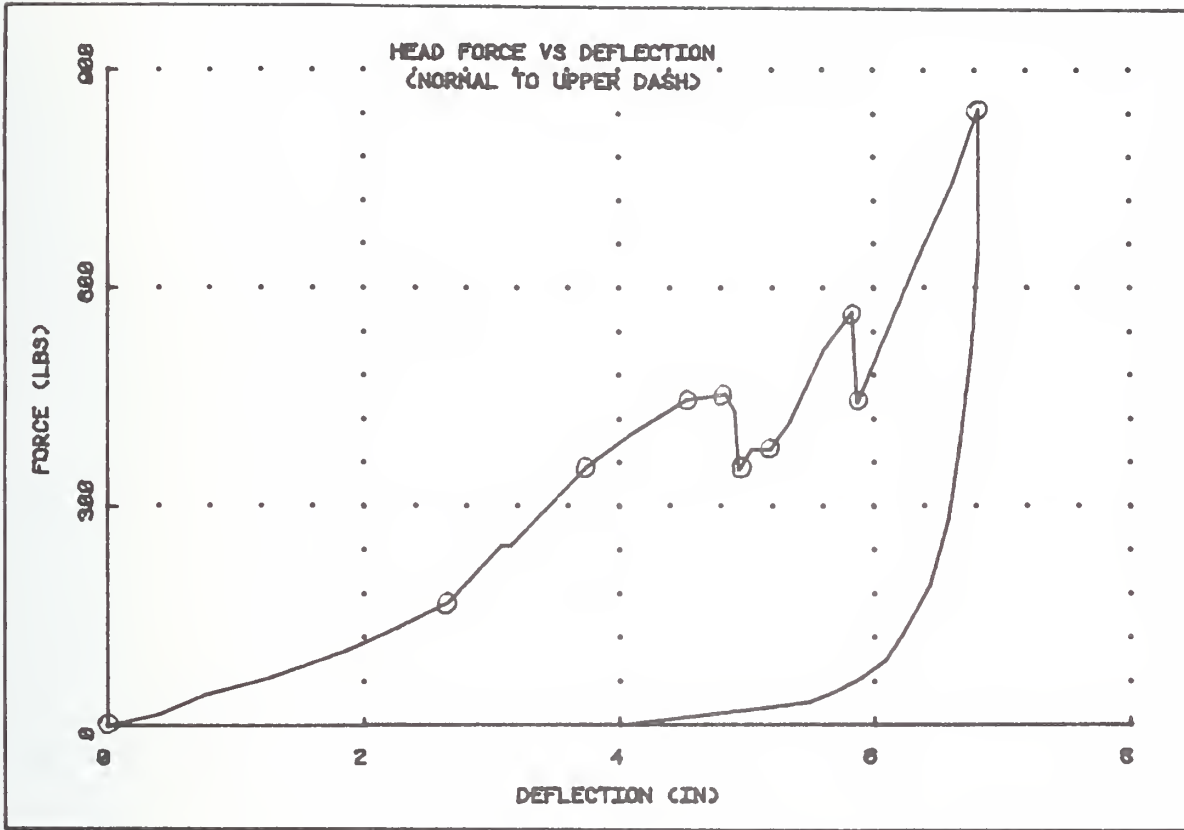
G= 0.307 R= 0.153 K= 1033  
 c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_  
 $\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>5.51</u>	<u>761.71</u>
<u>0.30</u>	<u>16.23</u>	<u>7.09</u>	<u>1246.86</u>
<u>1.79</u>	<u>330.14</u>		
<u>2.70</u>	<u>710.37</u>		
<u>3.33</u>	<u>770.04</u>		
<u>3.81</u>	<u>747.02</u>		
<u>4.72</u>	<u>865.24</u>		
<u>5.09</u>	<u>820.02</u>		
<u>5.21</u>	<u>871.45</u>		

Test: Static Head Test Date: November 29, 1984

Vehicle: Ford Fairmont

Options: Normal



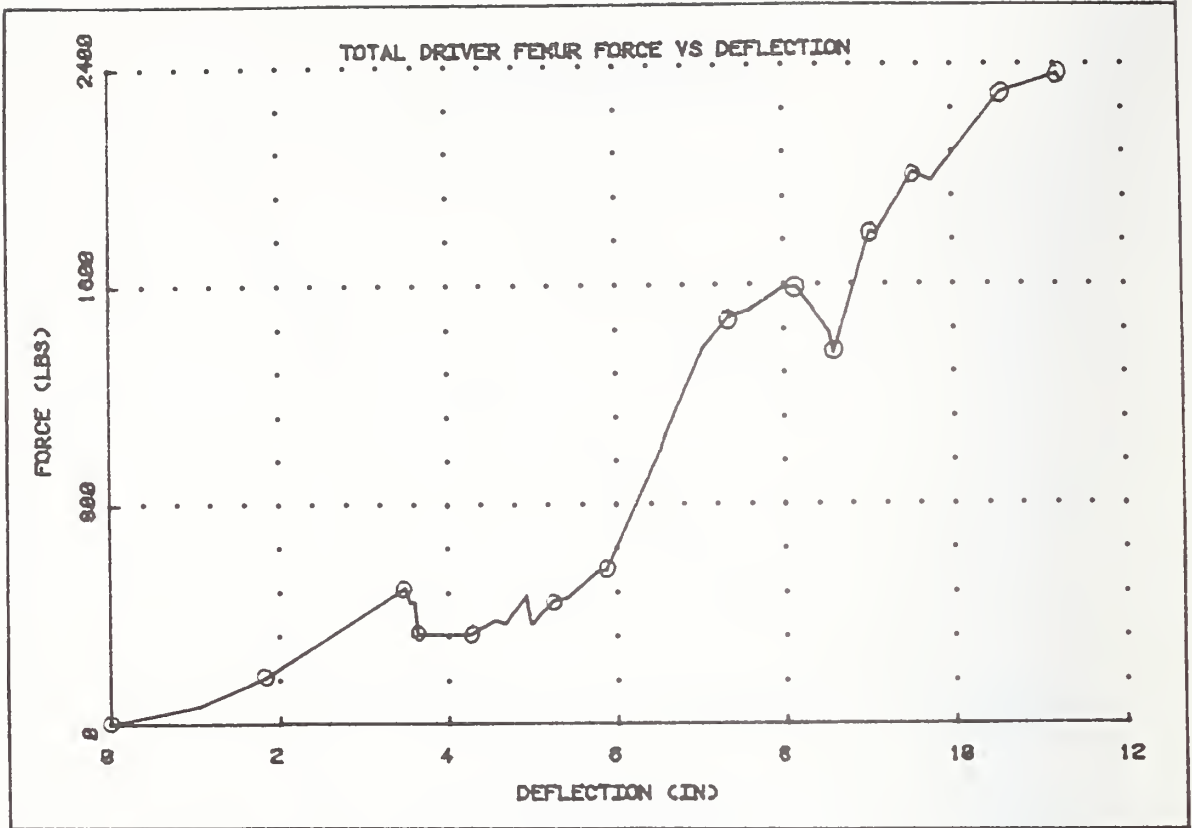
G= 0.596 R= 0.124 K= 1445

C= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>5.87</u>	<u>440.6</u>
<u>2.67</u>	<u>169.4</u>	<u>6.83</u>	<u>846.9</u>
<u>3.74</u>	<u>354.0</u>		
<u>4.52</u>	<u>445.6</u>		
<u>4.83</u>	<u>453.72</u>		
<u>4.94</u>	<u>348.74</u>		
<u>5.19</u>	<u>376.8</u>		
<u>5.83</u>	<u>566.6</u>		

Test: Total Driver Femur (Static) Date: November 29, 1984  
 Vehicle: Ford Fairmont  
 Options: \_\_\_\_\_



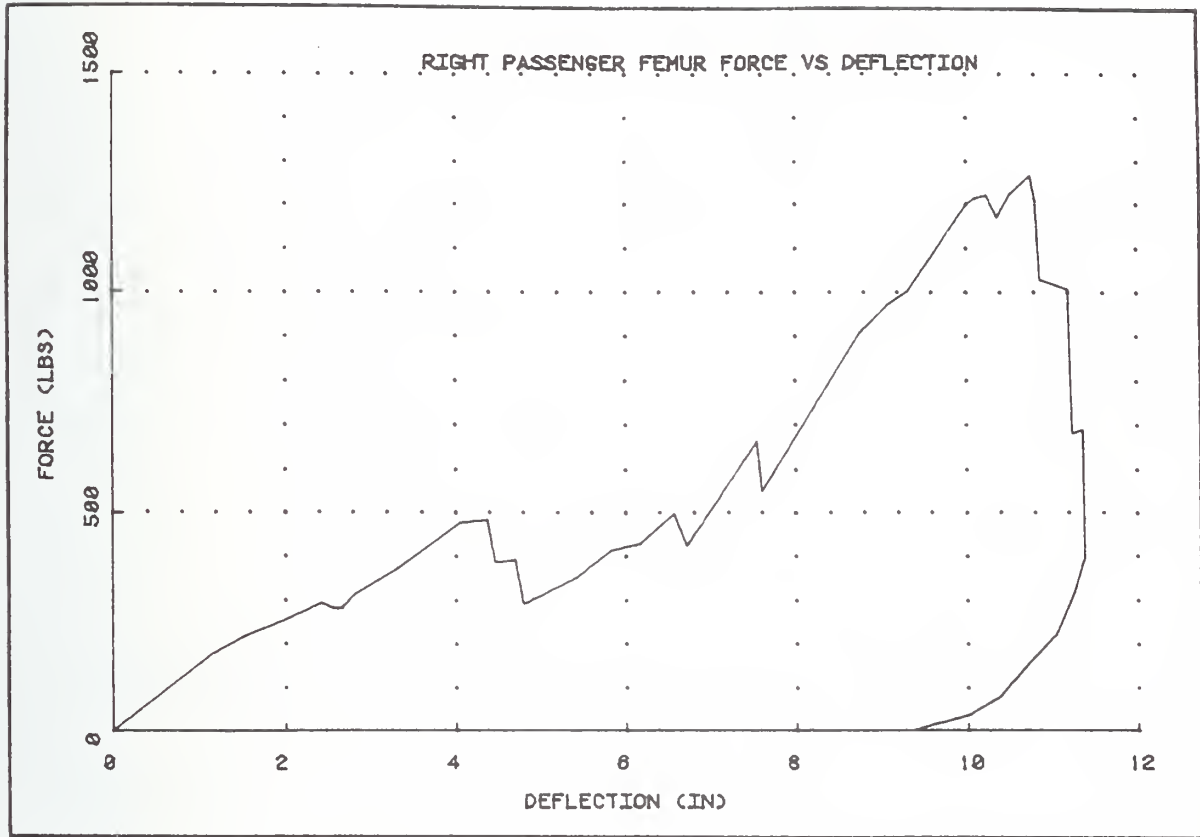
G= 0.864 R= 0.116 K= 1979  
 c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_  
 $\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

Deflection	Force	Deflection	Force
<u>0.0</u>	<u>0.0</u>	<u>8.14</u>	<u>1593.78</u>
<u>1.83</u>	<u>170.7</u>	<u>8.59</u>	<u>1345.64</u>
<u>3.50</u>	<u>498.2</u>	<u>9.03</u>	<u>1790.76</u>
<u>3.64</u>	<u>325.02</u>	<u>9.75</u>	<u>2002.55</u>
<u>4.24</u>	<u>323.9</u>	<u>10.58</u>	<u>2299.02</u>
<u>5.24</u>	<u>451.4</u>	<u>11.24</u>	<u>2366.22</u>
<u>5.87</u>	<u>559.5</u>		
<u>7.34</u>	<u>1483.93</u>		

Test: Right Passenger Femur Date: November 29, 1984

Vehicle: Ford Fairmont

Options: No Radio



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

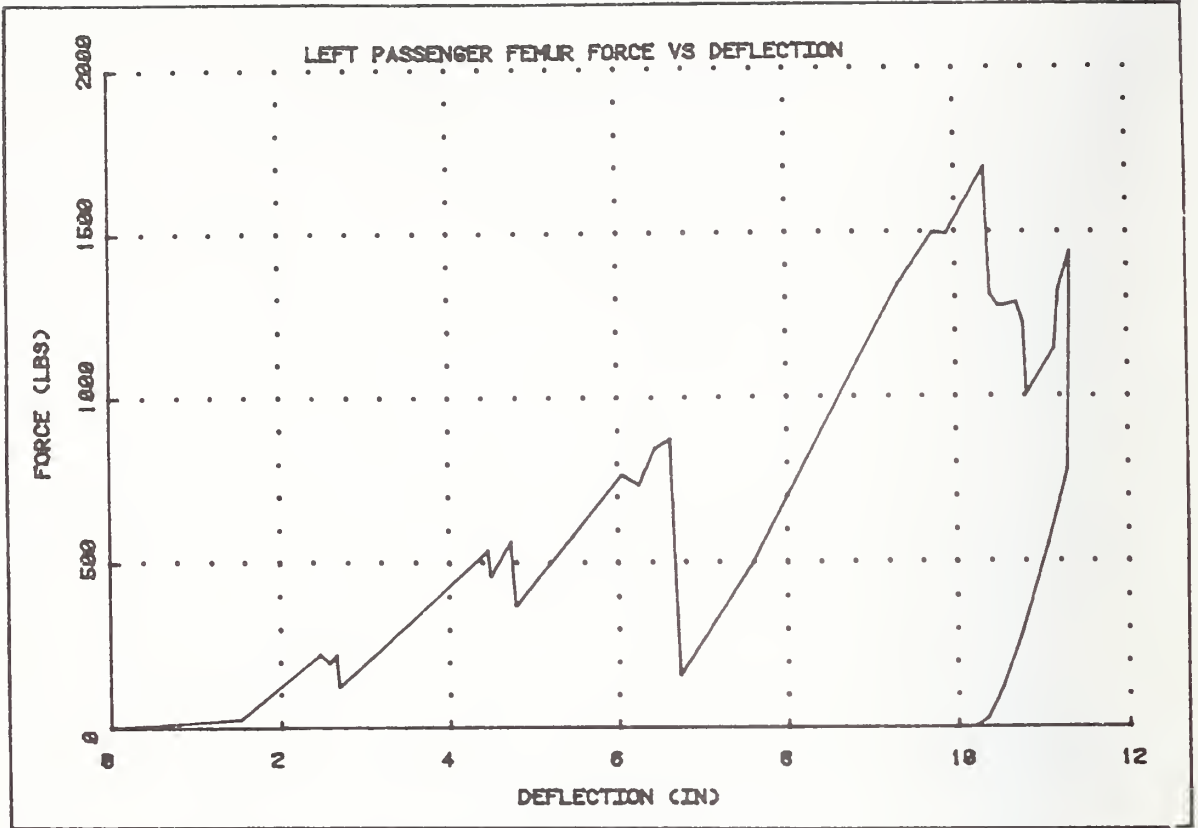
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Left Passenger Femur

Date: November 29, 1984

Vehicle: Ford Fairmont

Options: \_\_\_\_\_



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

C= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

Deflection

Force

Deflection

Force

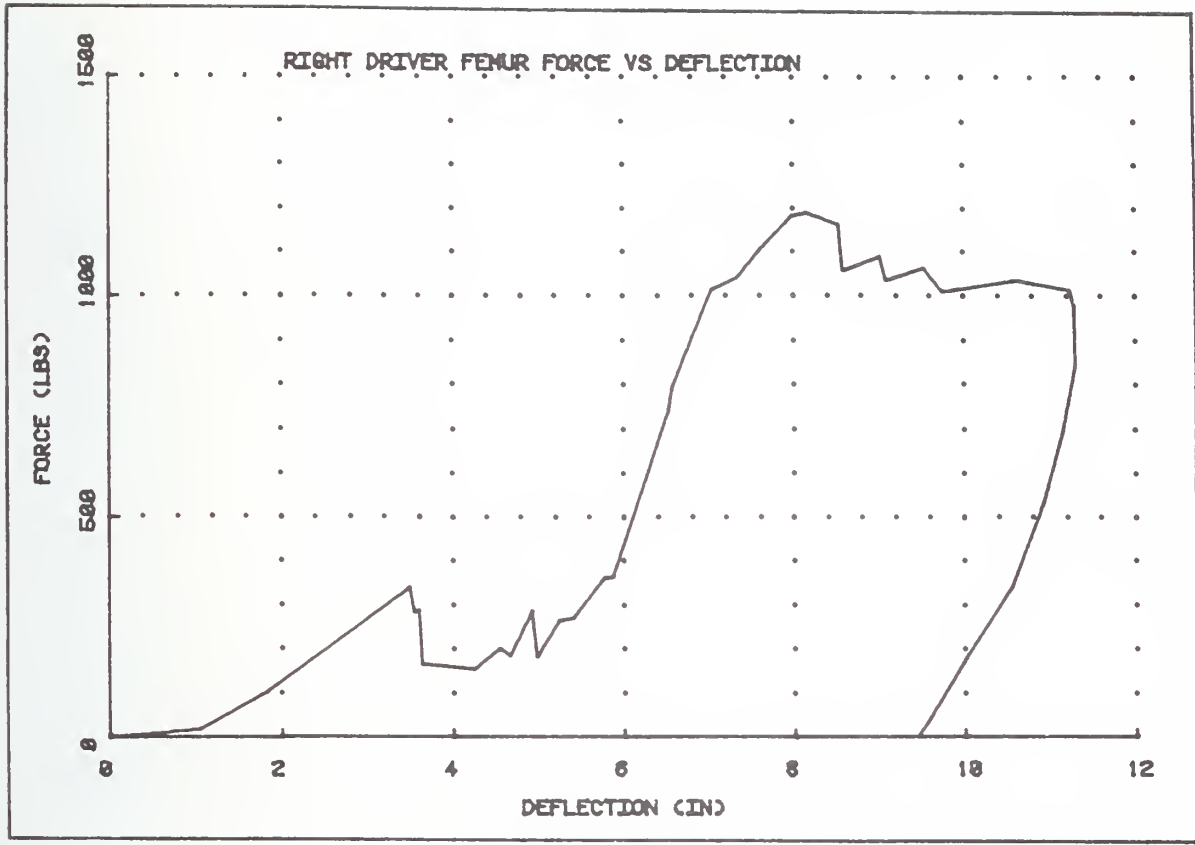
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____



Test: Right Driver Femur Date: November 29, 1984

Vehicle: Ford Fairmont

Options: \_\_\_\_\_



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

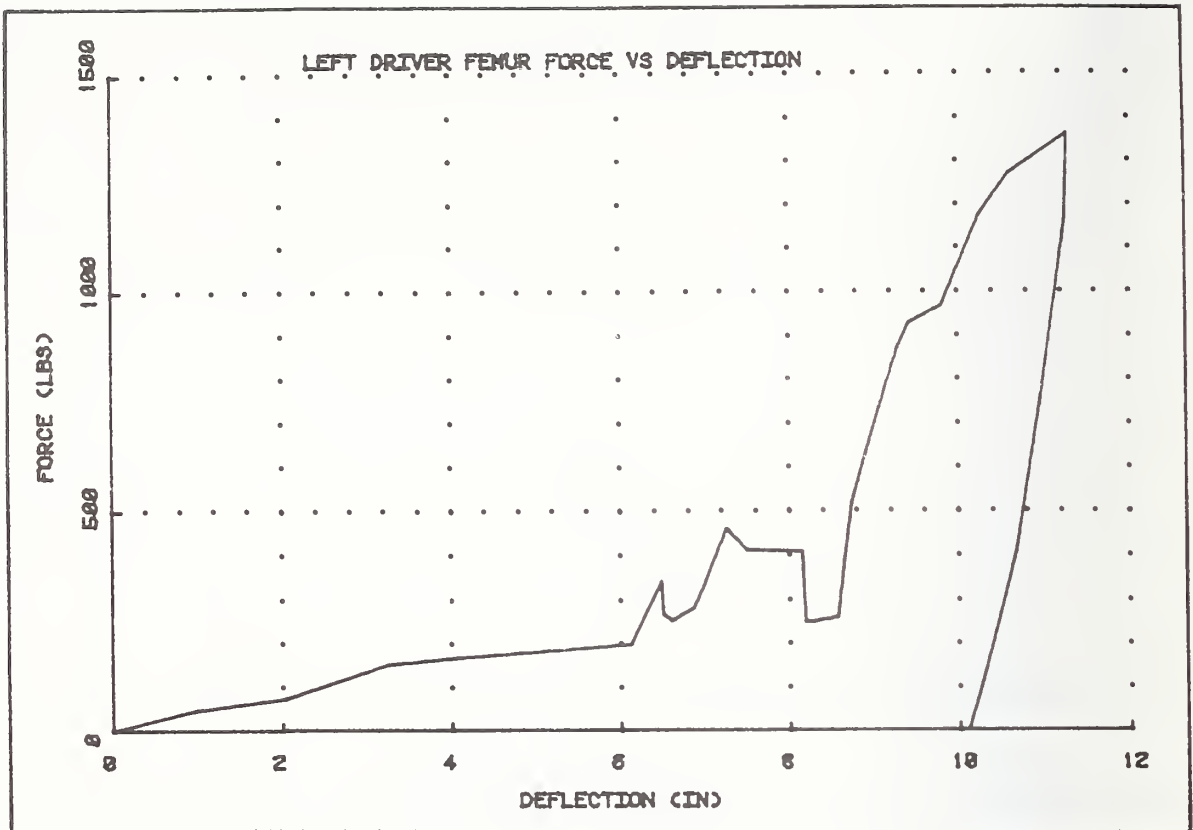
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Left Driver Femur Date: November 29, 1984

Vehicle: Ford Fairmont

Options: \_\_\_\_\_



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

C= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

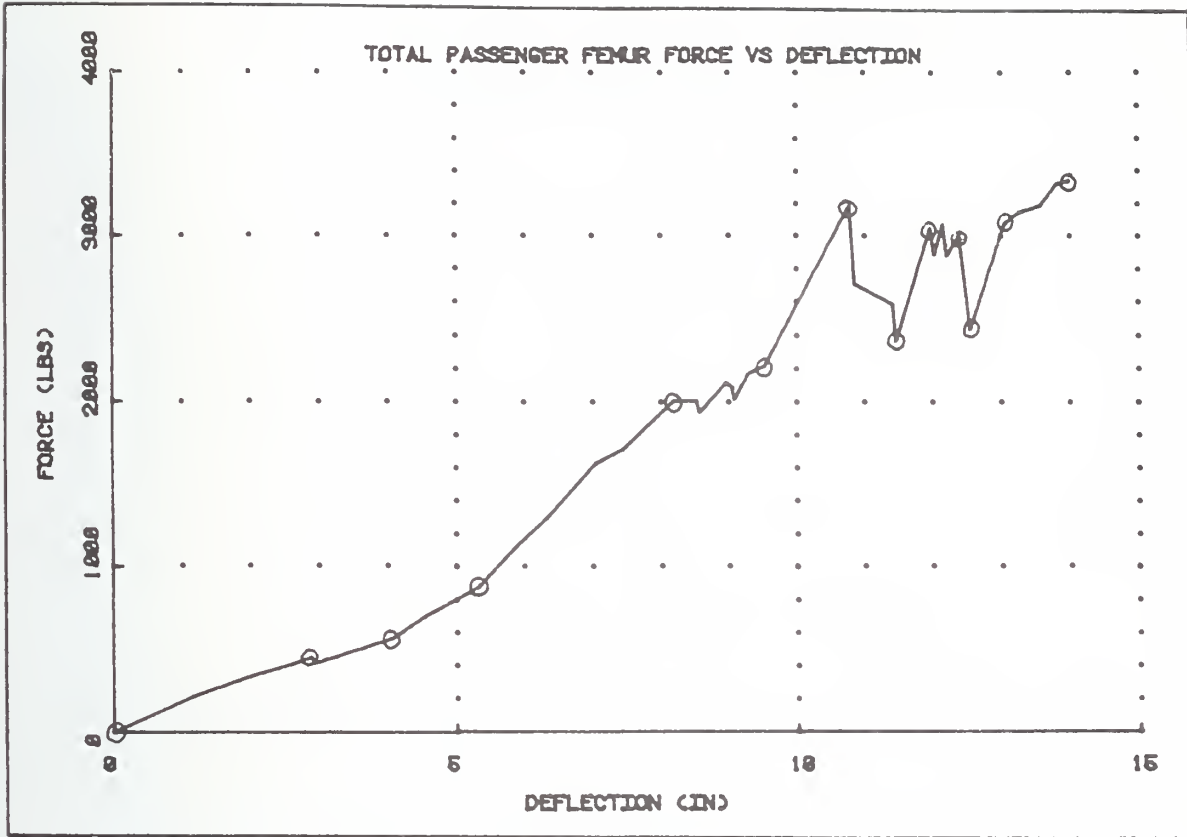
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Total Passenger Femur (Static) Date: January 5, 1985

Vehicle: Pontiac Firebird

Options: \_\_\_\_\_



G= 0.858 R= 0.074 K= 3288

C= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

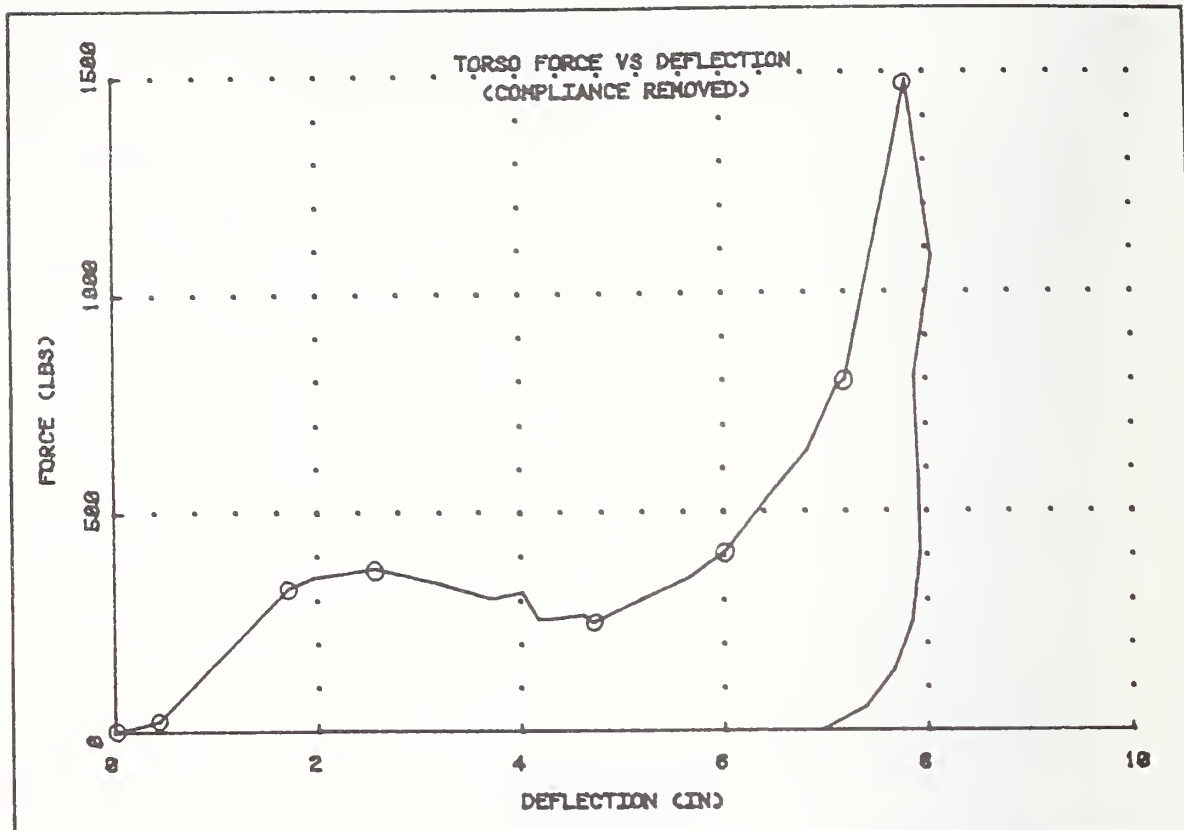
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>11.97</u>	<u>3045.8</u>
<u>2.87</u>	<u>447.4</u>	<u>12.39</u>	<u>3007.5</u>
<u>4.07</u>	<u>565.9</u>	<u>12.54</u>	<u>2426.0</u>
<u>5.33</u>	<u>875.5</u>	<u>13.06</u>	<u>3076.7</u>
<u>8.19</u>	<u>2002.7</u>	<u>14.01</u>	<u>3339.0</u>
<u>9.53</u>	<u>2214.6</u>		
<u>10.79</u>	<u>3190.2</u>		
<u>11.47</u>	<u>2354.9</u>		

Test: Torso Date: January 5, 1985

Vehicle: Pontiac Firebird

Options: \_\_\_\_\_



G= 0.864 R= 0.072 K= 2435

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

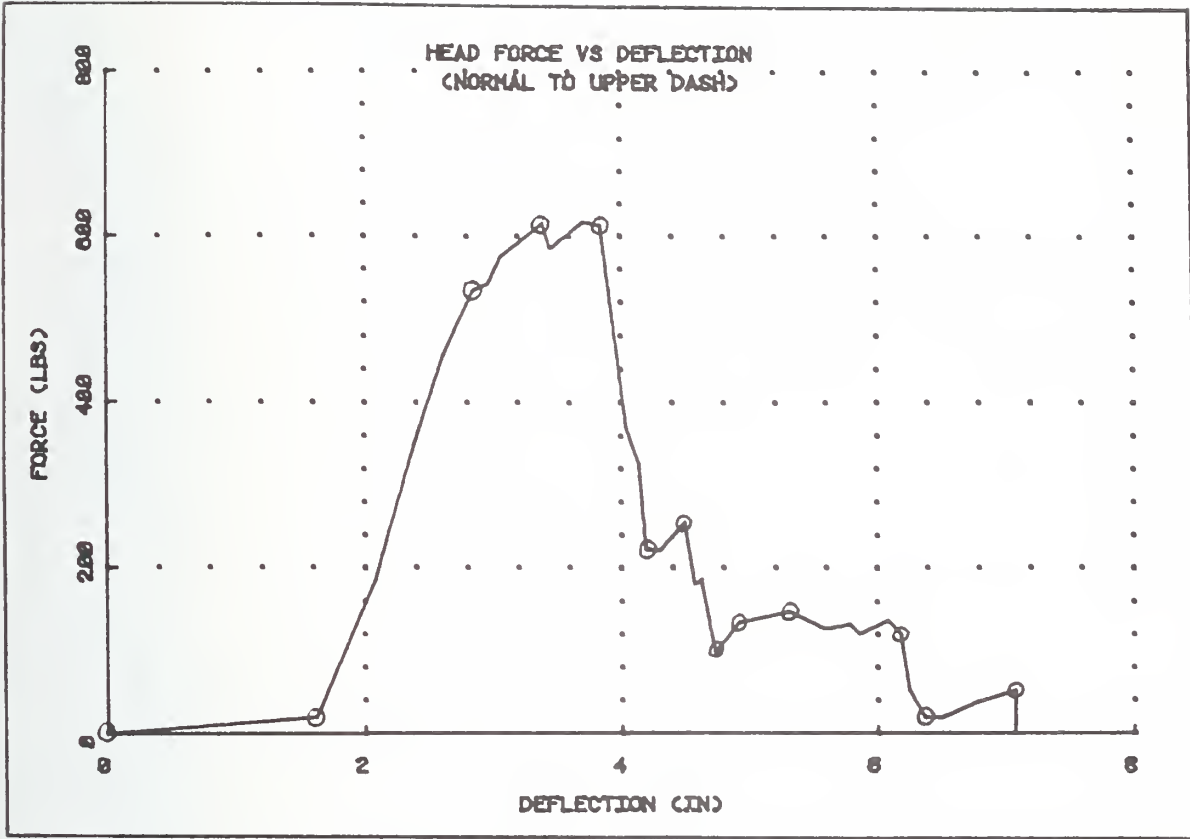
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	_____	_____
<u>0.44</u>	<u>23.7</u>	_____	_____
<u>1.71</u>	<u>327.3</u>	_____	_____
<u>2.54</u>	<u>371.8</u>	_____	_____
<u>4.70</u>	<u>249.4</u>	_____	_____
<u>6.04</u>	<u>413.8</u>	_____	_____
<u>7.11</u>	<u>780.4</u>	_____	_____
<u>7.83</u>	<u>1483.3</u>	_____	_____

Test: Head (Static) Date: January 5, 1985

Vehicle: Pontiac Firebird

Options: Normal



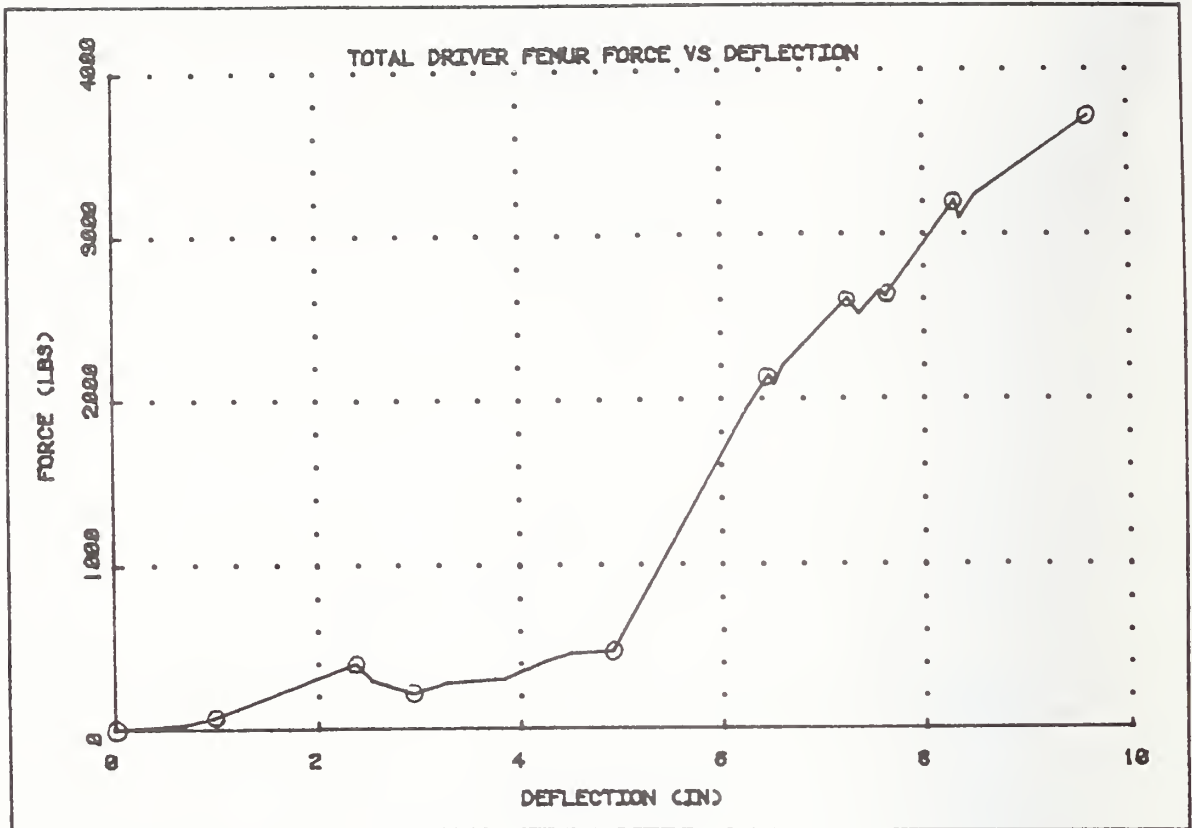
G= 0.999 R= 0.0001 K= 7638

c= μ<sub>1</sub>= μ<sub>2</sub>= μ<sub>3</sub>=

δ<sub>A</sub>= 0.0 δ<sub>B</sub>= 0.0 δ<sub>C</sub>= 0.0 δ<sub>D</sub>= 1000.0 δ<sub>F</sub>= 1000.1

Deflection	Force	Deflection	Force
0.0	0.0	4.92	133.8
1.62	19.73	5.30	147.6
2.85	534.1	6.19	119.3
3.40	615.6	6.37	18.8
3.85	612.3	7.08	51.8
4.19	220.9		
4.49	254.7		
4.73	97.4		

Test: Total Driver Femur (Static) Date: January 5, 1985  
 Vehicle: Pontiac Firebird  
 Options: \_\_\_\_\_



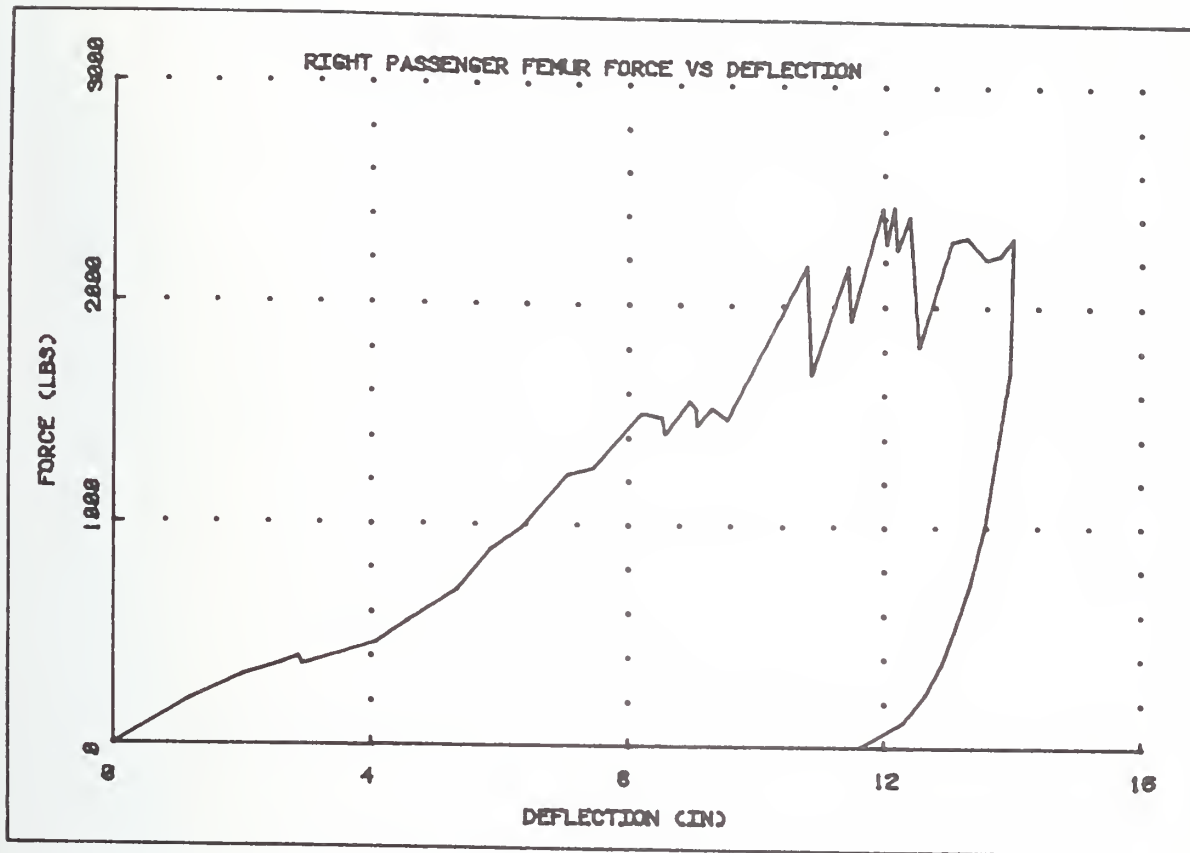
G= 0.743 R= 0.231 K= 2439  
 C= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_  
 $\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>8.31</u>	<u>3207.3</u>
<u>0.97</u>	<u>67.09</u>	<u>9.61</u>	<u>3718.5</u>
<u>2.37</u>	<u>403.4</u>		
<u>2.92</u>	<u>215.0</u>		
<u>4.91</u>	<u>477.3</u>		
<u>6.47</u>	<u>2138.5</u>		
<u>7.25</u>	<u>2606.7</u>		
<u>7.62</u>	<u>2621.9</u>		

Test: Right Passenger Femur Date: January 5, 1985

Vehicle: Pontiac Firebird

Options: \_\_\_\_\_  
\_\_\_\_\_



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

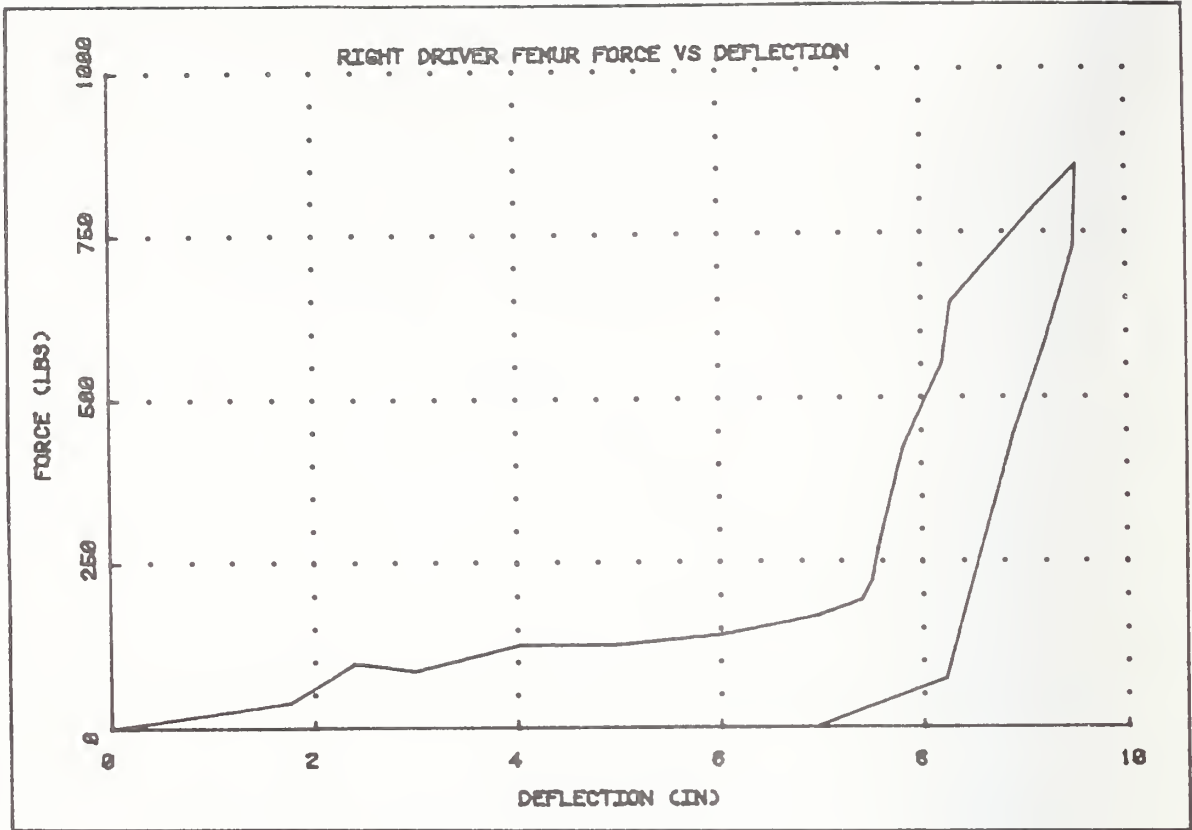
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Right Driver Femur Date: January 5, 1985

Vehicle: Pontiac Firebird

Options: \_\_\_\_\_



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

C= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

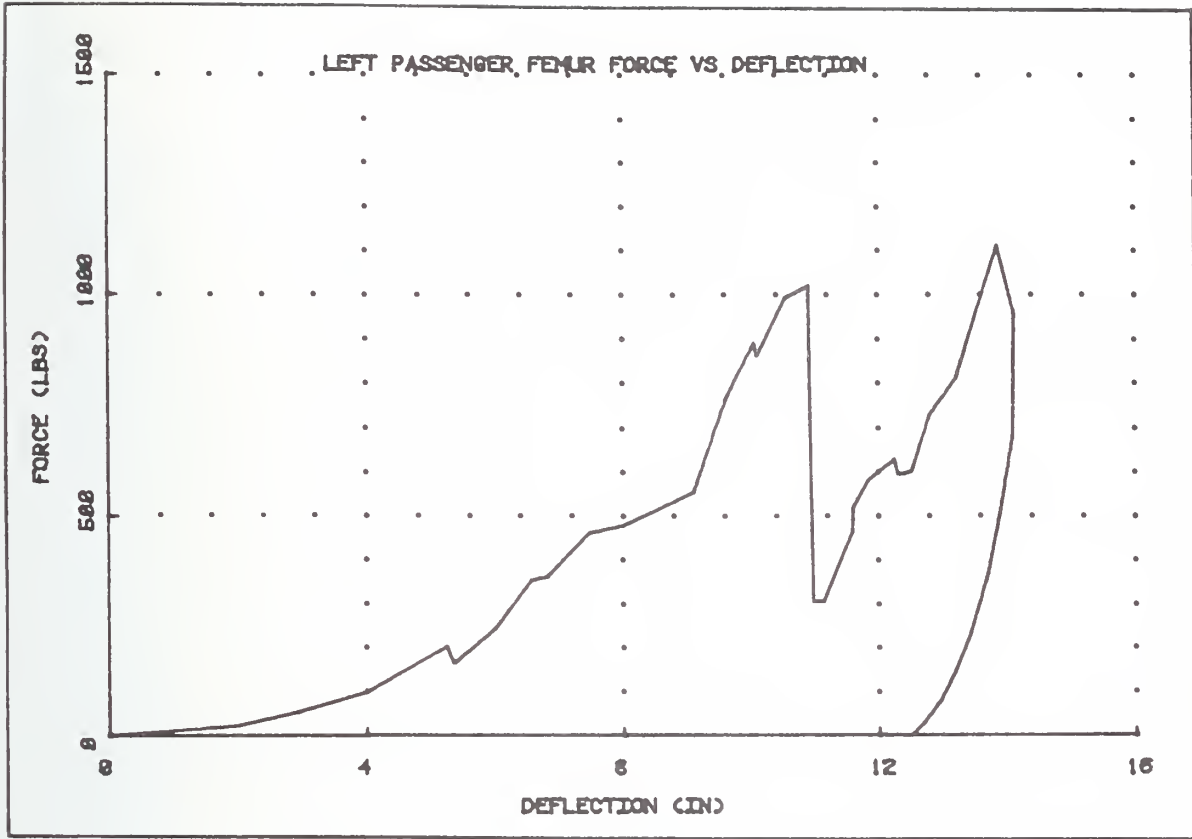
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____



Test: Left Passenger Femur Date: January 5, 1985

Vehicle: Pontiac Firebird

Options: \_\_\_\_\_



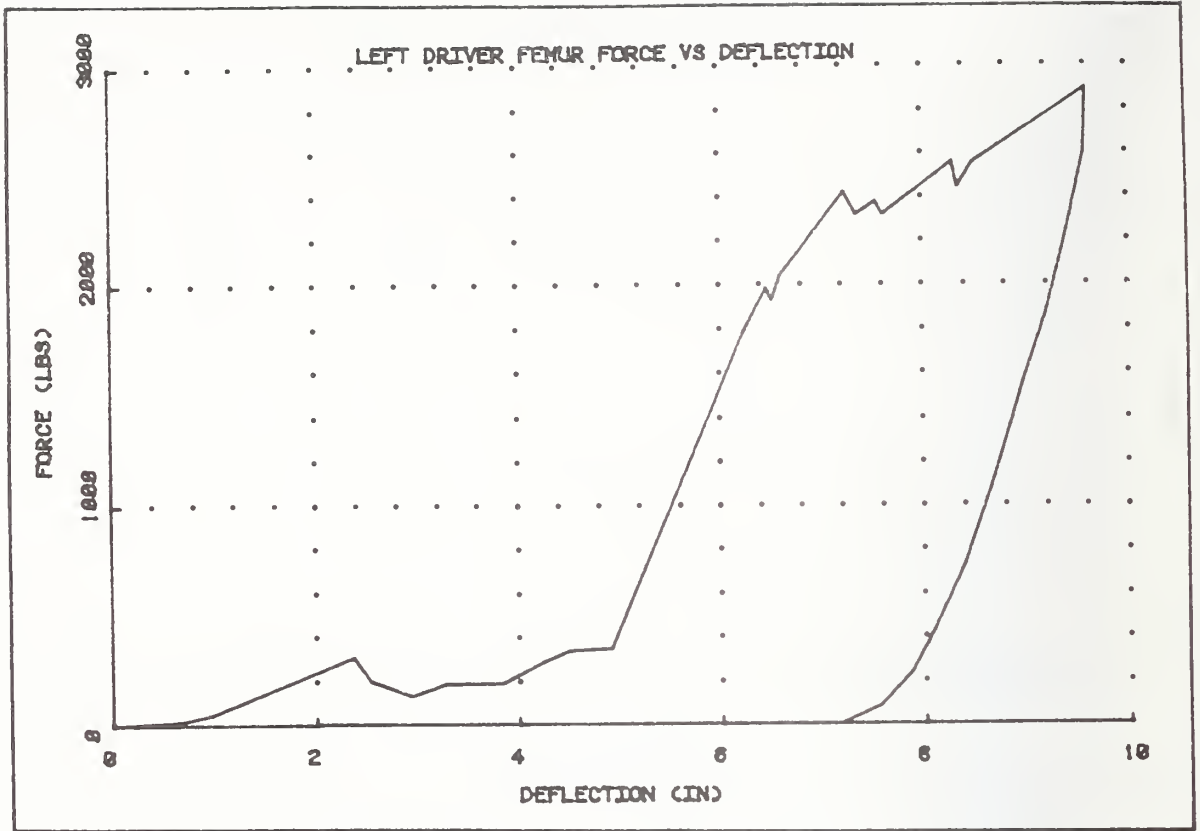
G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Left Driver Femur Date: January 5, 1985  
 Vehicle: Pontiac Firebird  
 Options: \_\_\_\_\_  
 \_\_\_\_\_



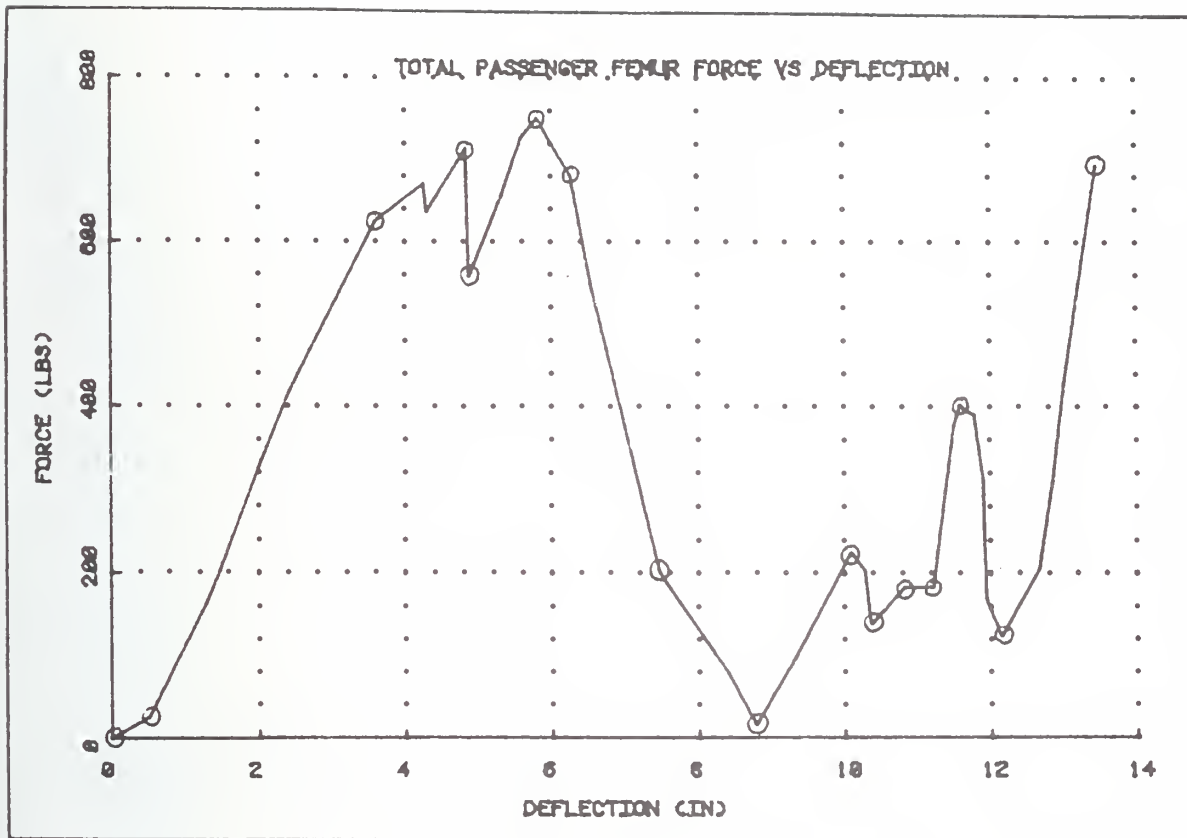
G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_  
 C= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_  
 $\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Total Passenger Femur (Static) Date: January 11, 1985

Vehicle: Chevy Celebrity

Options: \_\_\_\_\_



G= 0.966 R= 0.034 K= 1587

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

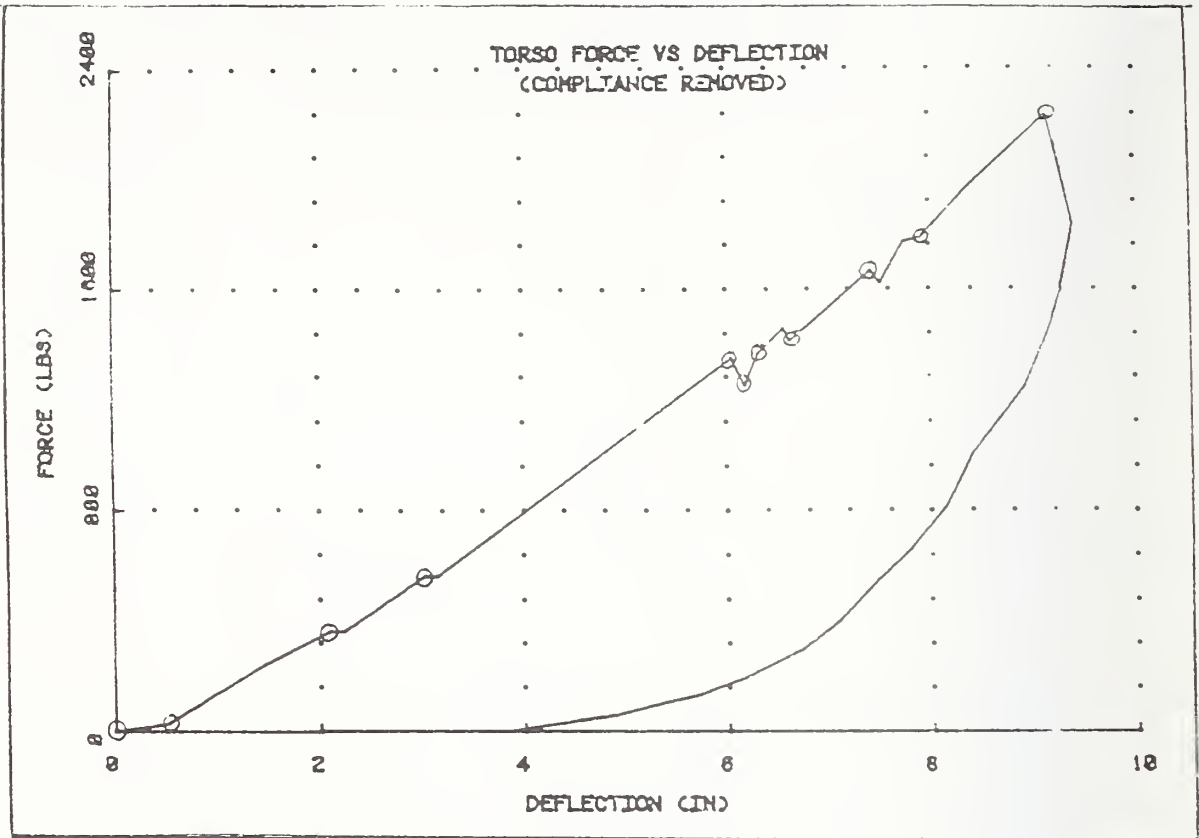
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>8.70</u>	<u>14.46</u>
<u>0.51</u>	<u>25.4</u>	<u>10.10</u>	<u>224.6</u>
<u>3.60</u>	<u>624.2</u>	<u>10.37</u>	<u>137.5</u>
<u>4.84</u>	<u>714.1</u>	<u>10.84</u>	<u>183.1</u>
<u>4.88</u>	<u>556.3</u>	<u>11.22</u>	<u>182.5</u>
<u>5.81</u>	<u>751.5</u>	<u>11.59</u>	<u>399.6</u>
<u>6.27</u>	<u>678.6</u>	<u>12.14</u>	<u>122.4</u>
<u>7.48</u>	<u>200.2</u>	<u>13.48</u>	<u>694.1</u>

Test: Torso (Static) Date: January 11, 1985,

Vehicle: Chevy Celebrity

Options: \_\_\_\_\_



G= 0.414 R= 0.275 K= 650

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

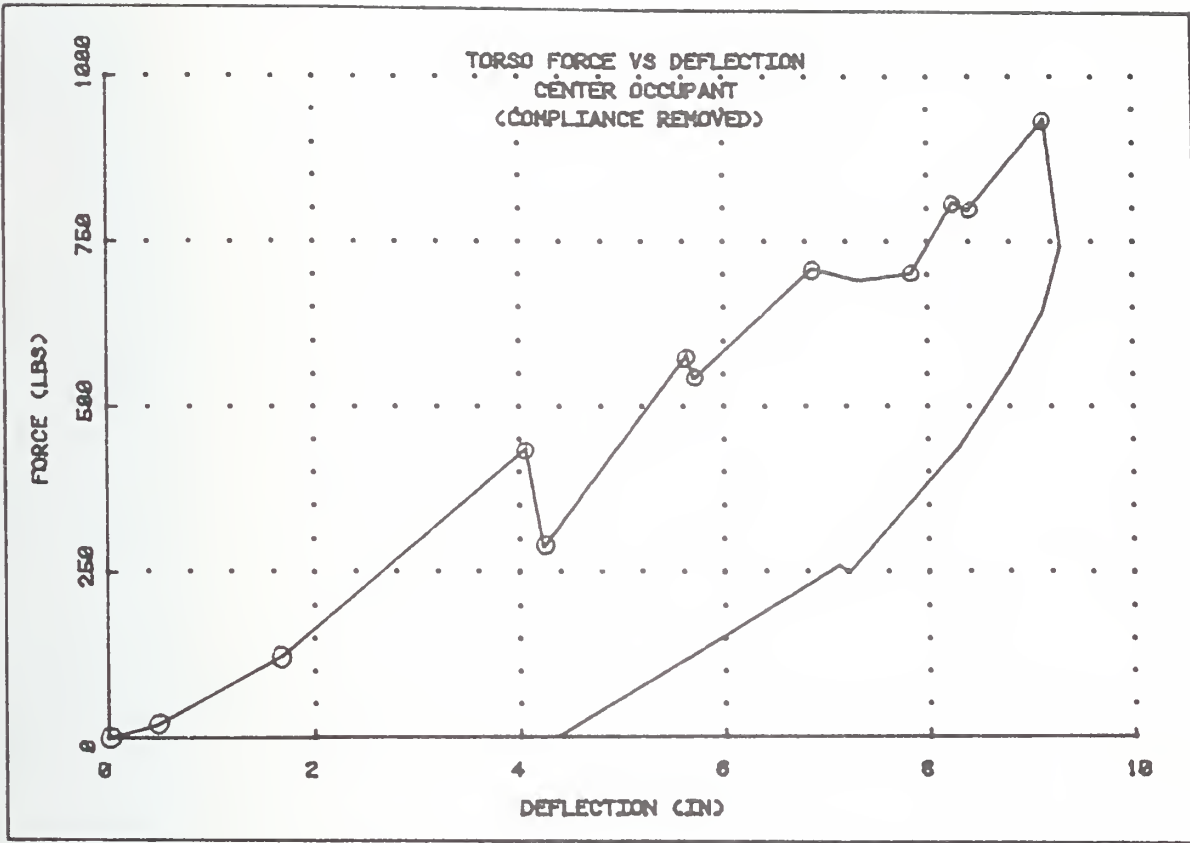
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

Deflection	Force	Deflection	Force
<u>0.0</u>	<u>0.0</u>	<u>7.43</u>	<u>1667.8</u>
<u>0.51</u>	<u>25.9</u>	<u>7.93</u>	<u>1785.9</u>
<u>2.09</u>	<u>363.4</u>	<u>9.16</u>	<u>2238.5</u>
<u>3.02</u>	<u>563.9</u>		
<u>6.05</u>	<u>1347.1</u>		
<u>6.18</u>	<u>1245.9</u>		
<u>6.32</u>	<u>1364.1</u>		
<u>6.63</u>	<u>1410.7</u>		

Test: Torso (center occupant) Date: January 11, 1985

Vehicle: Chevy Celebrity

Options: Compliance Removed



G= 0.470 R= .0.322 K= 210

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

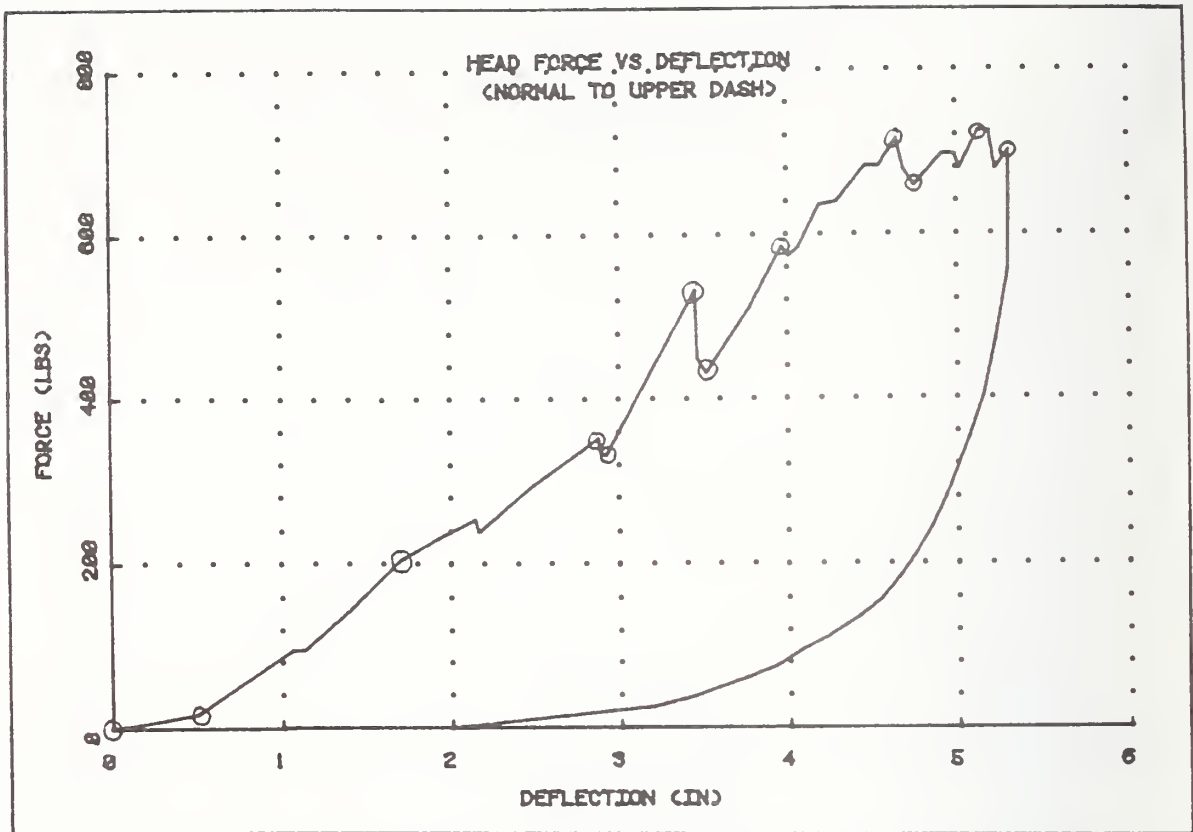
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>7.85</u>	<u>701.8</u>
<u>0.47</u>	<u>18.5</u>	<u>8.25</u>	<u>809.0</u>
<u>1.69</u>	<u>123.4</u>	<u>8.39</u>	<u>795.5</u>
<u>4.07</u>	<u>434.8</u>	<u>9.14</u>	<u>935.8</u>
<u>4.24</u>	<u>286.5</u>		
<u>5.64</u>	<u>577.8</u>		
<u>5.71</u>	<u>541.0</u>		
<u>6.86</u>	<u>707.6</u>		

Test: Head (Static) Date: January 11, 1985

Vehicle: Chevy Celebrity

Options: Normal



G= 0.385 R= 0.190 K= 701

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

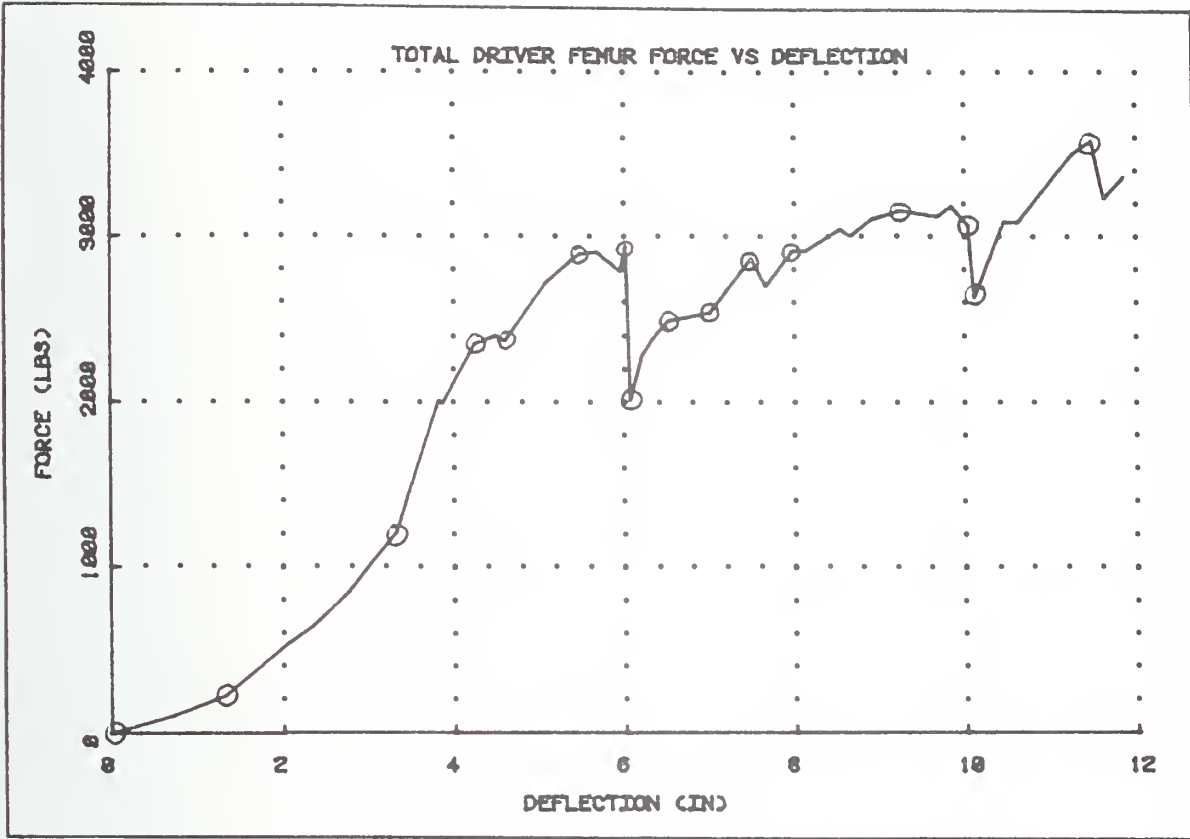
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>4.65</u>	<u>714.5</u>
<u>0.50</u>	<u>16.6</u>	<u>4.75</u>	<u>657.7</u>
<u>1.70</u>	<u>204.6</u>	<u>5.13</u>	<u>724.4</u>
<u>2.88</u>	<u>352.4</u>	<u>5.31</u>	<u>699.7</u>
<u>2.89</u>	<u>330.9</u>		
<u>3.46</u>	<u>532.5</u>		
<u>3.52</u>	<u>430.2</u>		
<u>3.97</u>	<u>584.5</u>		

Test: Total Driver Femur (Static) Date: January 11, 1985

Vehicle: Chevy Celebrity

Options: \_\_\_\_\_



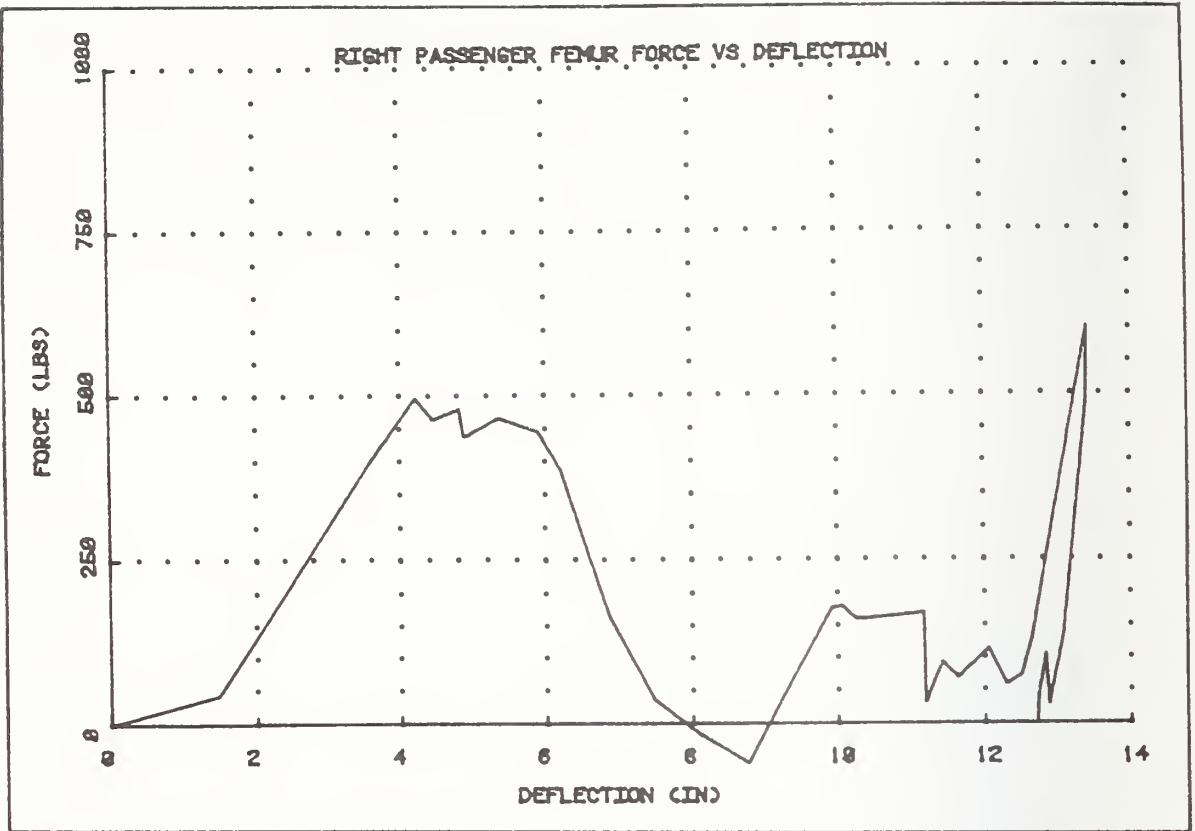
G= 0.748 R= 0.106 K= 2409

C= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>6.51</u>	<u>2490.1</u>
<u>1.33</u>	<u>217.3</u>	<u>7.01</u>	<u>2535.4</u>
<u>3.33</u>	<u>2106.6</u>	<u>7.49</u>	<u>2867.7</u>
<u>4.24</u>	<u>2349.1</u>	<u>7.97</u>	<u>2912.1</u>
<u>4.60</u>	<u>2364.4</u>	<u>9.27</u>	<u>3155.4</u>
<u>5.48</u>	<u>2892.3</u>	<u>10.04</u>	<u>3067.3</u>
<u>6.02</u>	<u>2940.2</u>	<u>10.11</u>	<u>2624.6</u>
<u>6.07</u>	<u>2002.4</u>	<u>11.48</u>	<u>3579.4</u>

Test: Right Passenger Femur Date: January 11, 1985  
 Vehicle: Chevy Celebrity  
 Options: \_\_\_\_\_  
 \_\_\_\_\_



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_  
 c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_  
 $\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

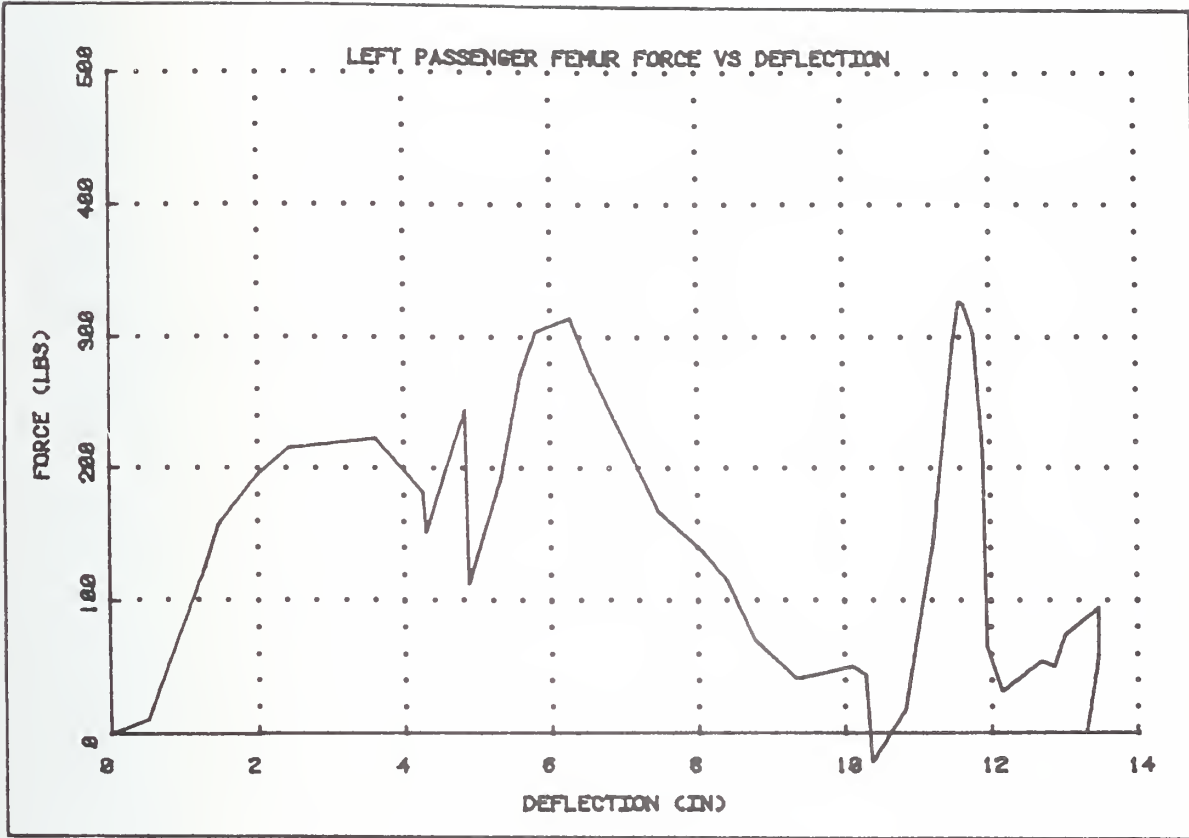
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____



Test: Left Passenger Femur Date: January 11, 1985

Vehicle: Chevy Celebrity

Options: \_\_\_\_\_  
\_\_\_\_\_



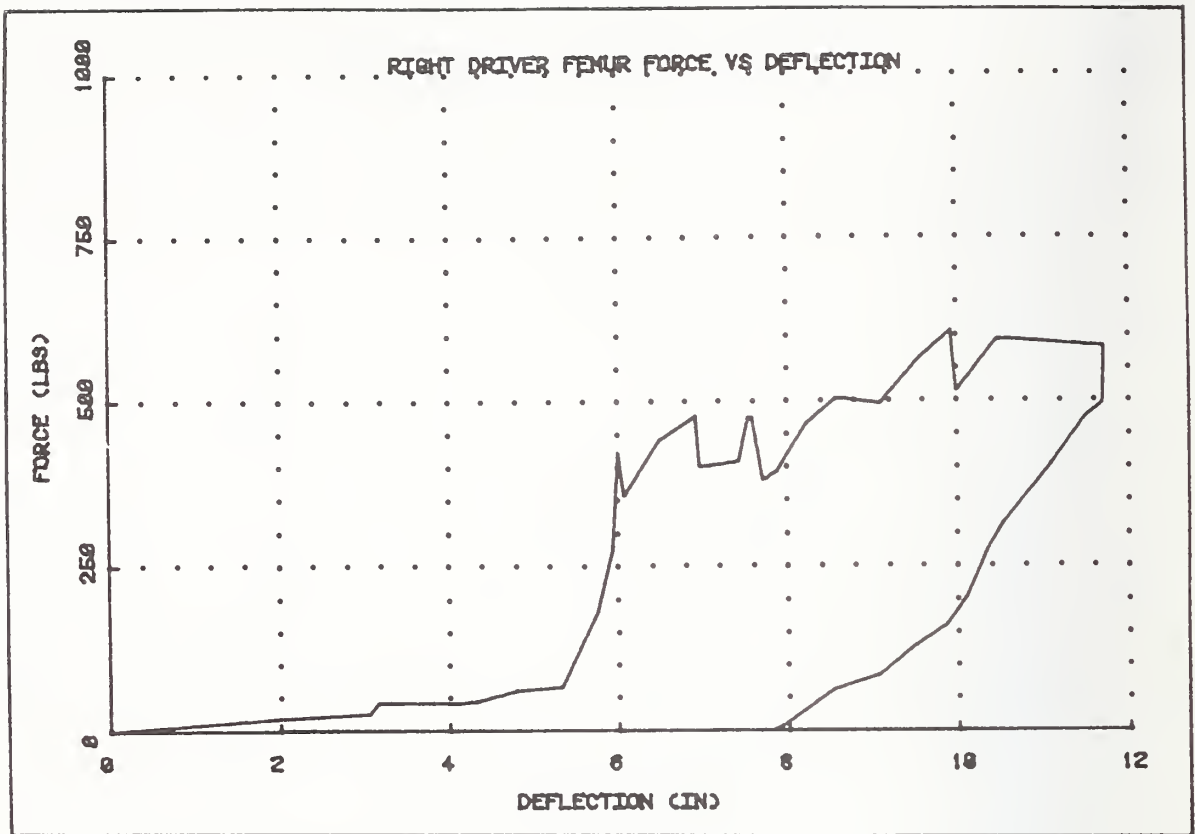
G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Right Driver Femur Date: January 11, 1985  
 Vehicle: Chevy Celebrity  
 Options: \_\_\_\_\_



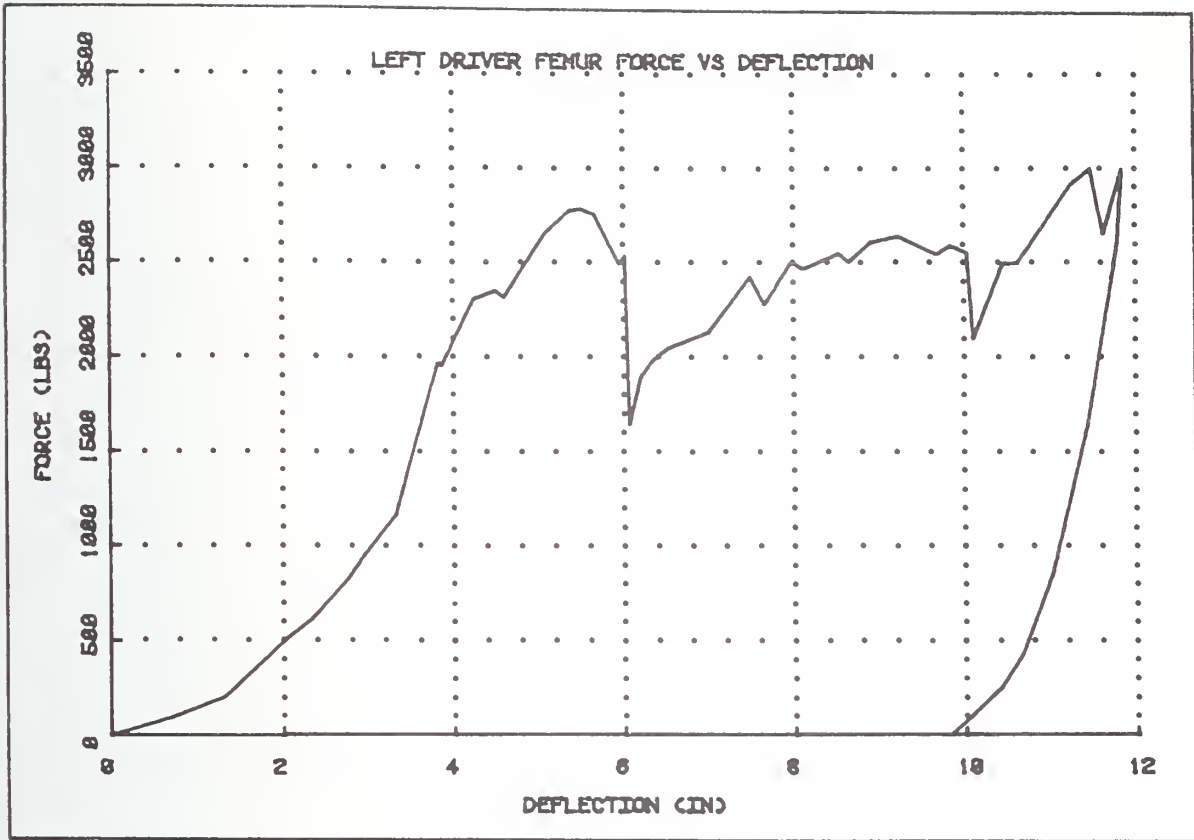
G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_  
 c= \_\_\_\_\_  $\nu_1$ = \_\_\_\_\_  $\nu_2$ = \_\_\_\_\_  $\nu_3$ = \_\_\_\_\_  
 $\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Left Driver Femur Date: January 11, 1985

Vehicle: Chevy Celebrity

Options: \_\_\_\_\_



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

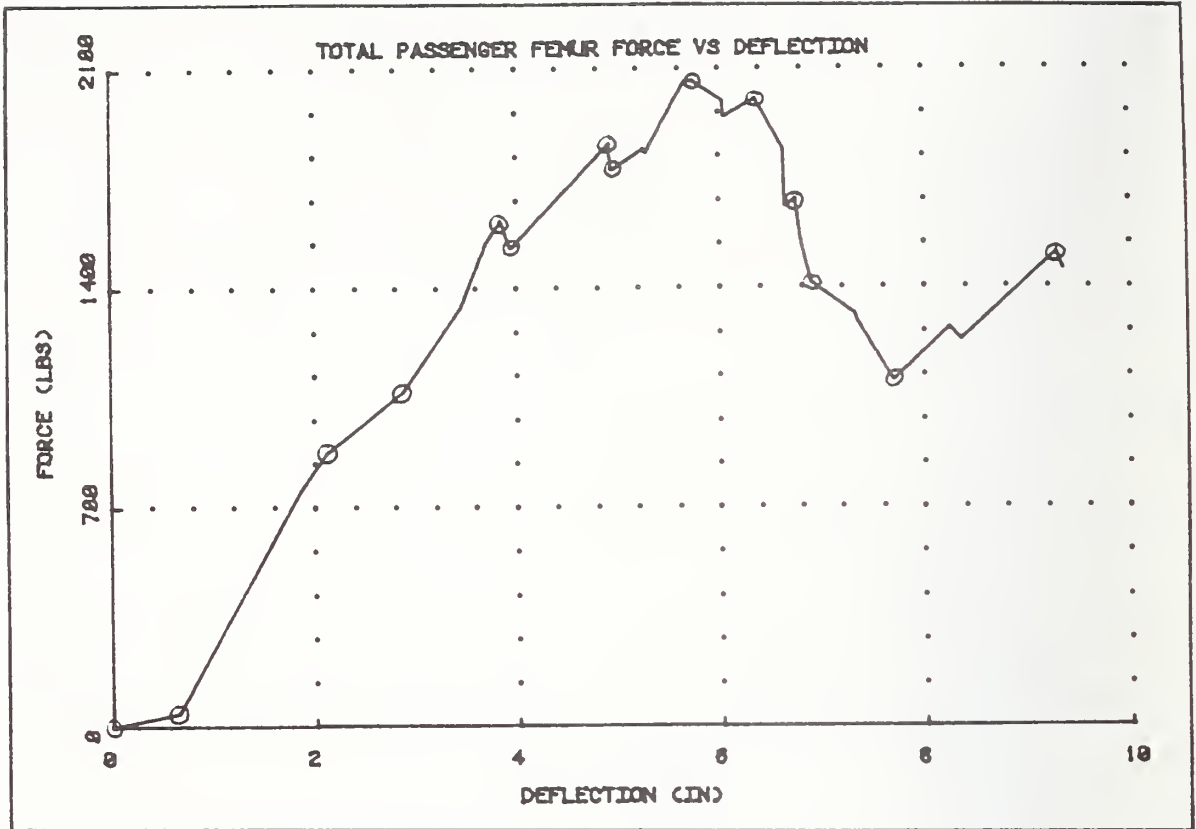
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Total Passenger Femur (Static) Date: January 15, 1985

Vehicle: Datsun 210

Options: \_\_\_\_\_



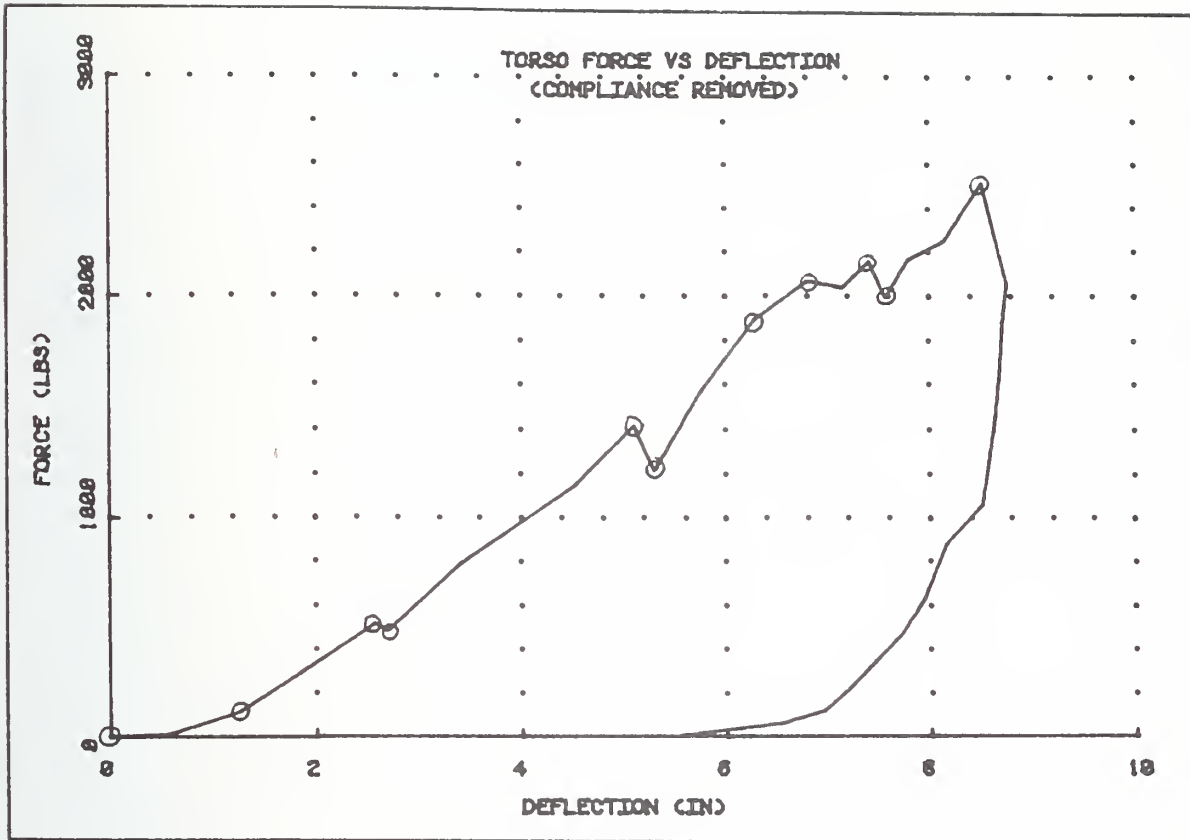
G= 0.821 R= 0.097 K= 1778

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>5.73</u>	<u>2060.9</u>
<u>0.65</u>	<u>42.27</u>	<u>6.36</u>	<u>2003.7</u>
<u>2.12</u>	<u>875.0</u>	<u>6.75</u>	<u>1678.1</u>
<u>2.88</u>	<u>1072.6</u>	<u>6.90</u>	<u>1409.1</u>
<u>3.85</u>	<u>1616.6</u>	<u>7.69</u>	<u>1100.2</u>
<u>3.94</u>	<u>1525.7</u>	<u>9.29</u>	<u>1507.6</u>
<u>4.93</u>	<u>1860.3</u>		
<u>4.95</u>	<u>1773.9</u>		

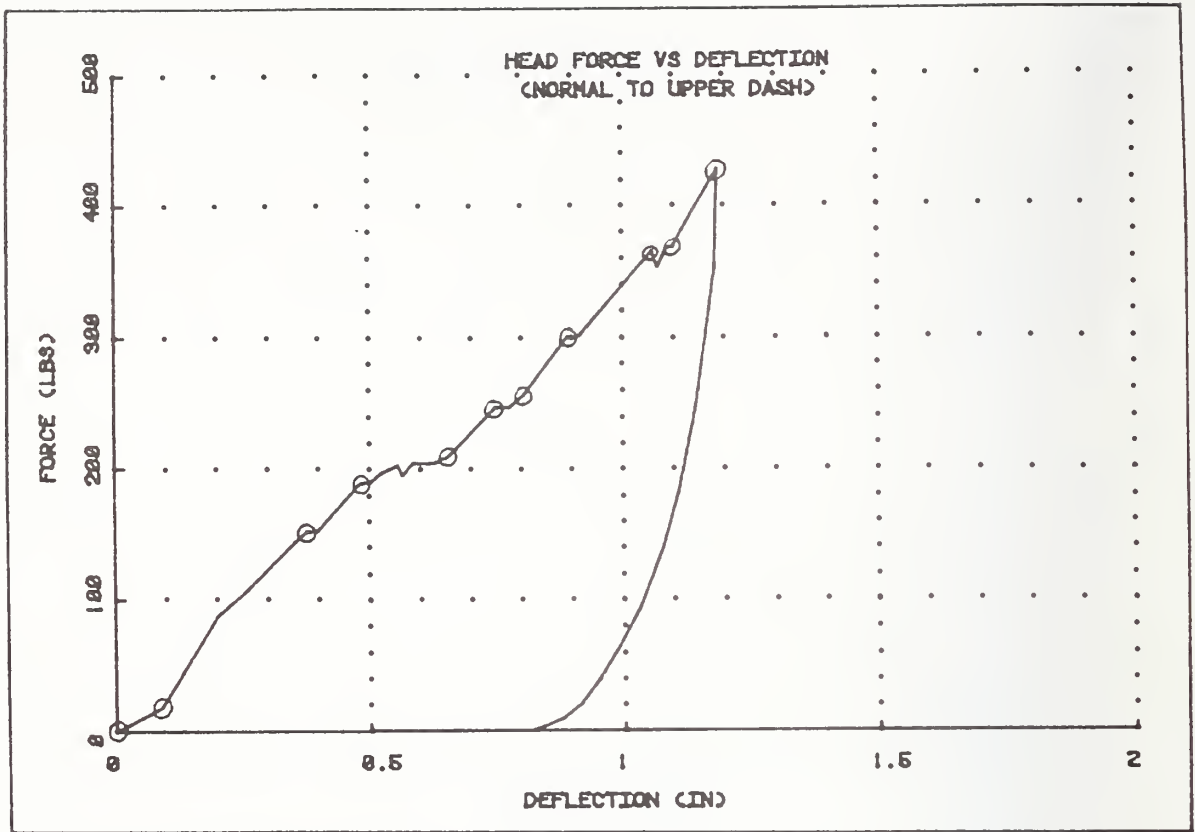
Test: Torso (Static) Date: January 15, 1985  
 Vehicle: Datsun 210  
 Options: Compliance Removed



G= 0.631 R= 0.130 K= 1639  
 c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_  
 $\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>7.41</u>	<u>2158.3</u>
<u>1.25</u>	<u>113.1</u>	<u>7.58</u>	<u>1990.5</u>
<u>2.56</u>	<u>516.8</u>	<u>8.53</u>	<u>2516.3</u>
<u>2.68</u>	<u>480.0</u>		
<u>5.10</u>	<u>1415.23</u>		
<u>5.30</u>	<u>1212.5</u>		
<u>6.30</u>	<u>1892.5</u>		
<u>6.80</u>	<u>2065.8</u>		

Test: Head (Static) Date: January 15, 1985  
 Vehicle: Datsun 210  
 Options: Normal



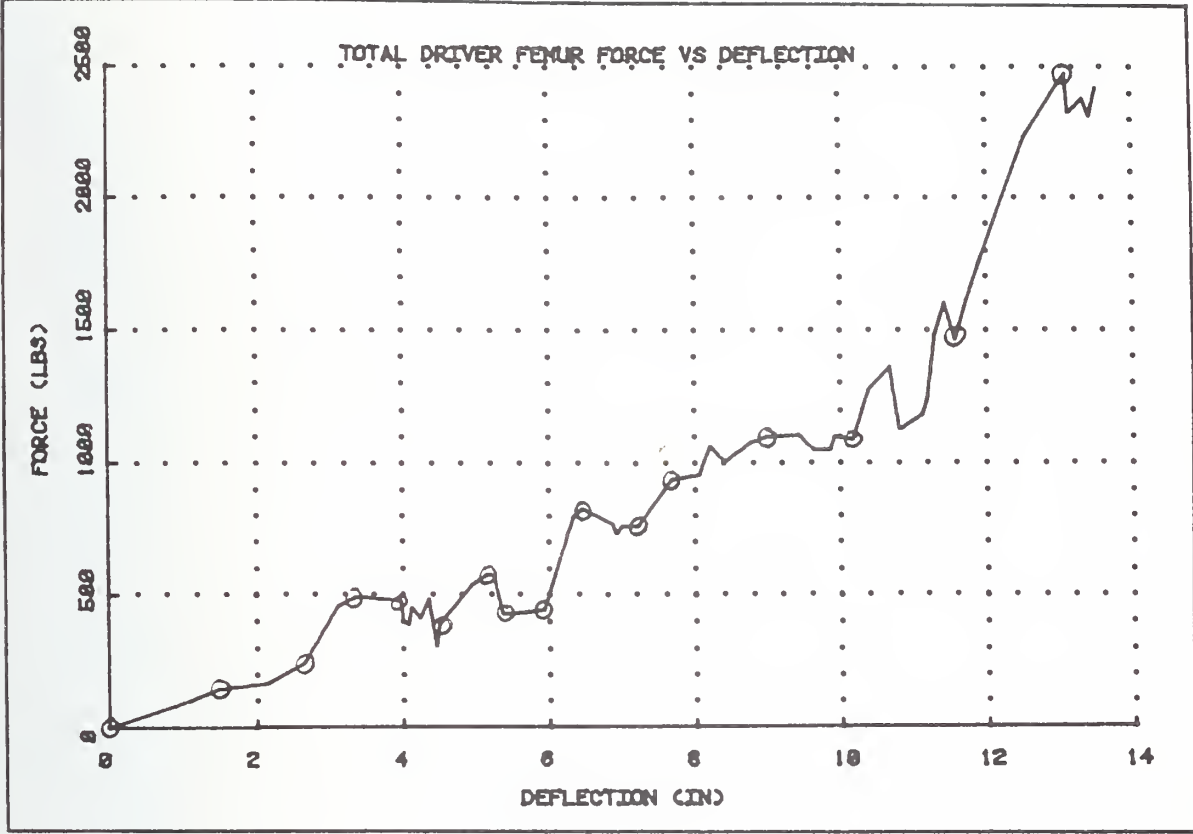
G= 0.690 R= 0.159 K= 2354  
 c= u<sub>1</sub>= u<sub>2</sub>= u<sub>3</sub>=  
 f<sub>A</sub>= 0.0 f<sub>B</sub>= 0.0 f<sub>C</sub>= 0.0 f<sub>D</sub>= 1000.0 f<sub>F</sub>= 1000.1

Deflection	Force	Deflection	Force
0.0	0.0	1.06	365.1
0.09	17.66	1.10	368.7
0.37	152.2	1.19	427.6
0.48	188.9		
0.65	209.9		
0.75	246.9		
0.81	257.3		
0.89	300.7		

Test: Total Driver Femur (Static) Date: January 15, 1985

Vehicle: Datsun 210

Options: \_\_\_\_\_



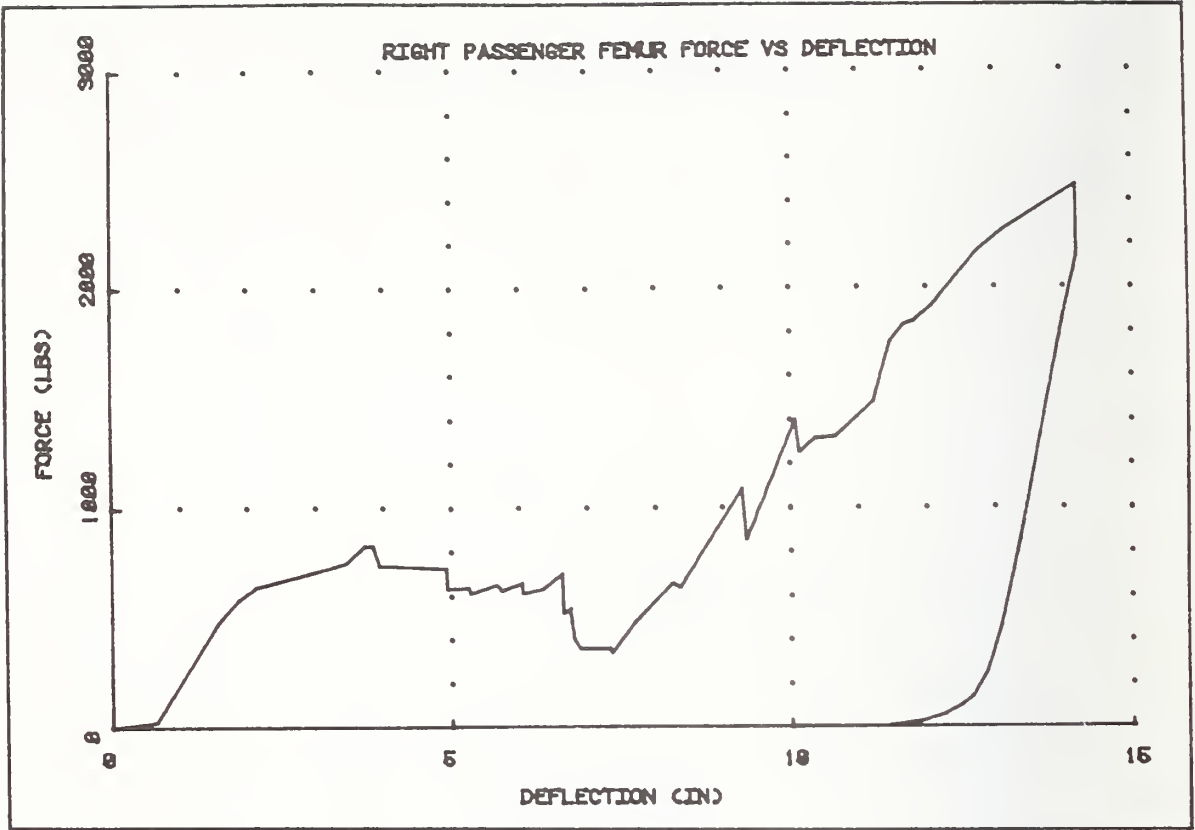
G= 0.929 R= 0.101 K= 2623

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>5.94</u>	<u>443.32</u>
<u>1.48</u>	<u>144.4</u>	<u>6.45</u>	<u>824.44</u>
<u>2.65</u>	<u>243.4</u>	<u>7.22</u>	<u>758.47</u>
<u>3.33</u>	<u>492.3</u>	<u>7.68</u>	<u>939.8</u>
<u>3.97</u>	<u>474.3</u>	<u>8.99</u>	<u>1098.4</u>
<u>4.50</u>	<u>389.1</u>	<u>10.17</u>	<u>1086.4</u>
<u>5.14</u>	<u>575.4</u>	<u>11.58</u>	<u>1457.1</u>
<u>5.37</u>	<u>427.1</u>	<u>13.11</u>	<u>2476.8</u>

Test: Right Passenger Femur Date: January 15, 1985  
 Vehicle: Datsun 210  
 Options: \_\_\_\_\_



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_  
 C= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_  
 $\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

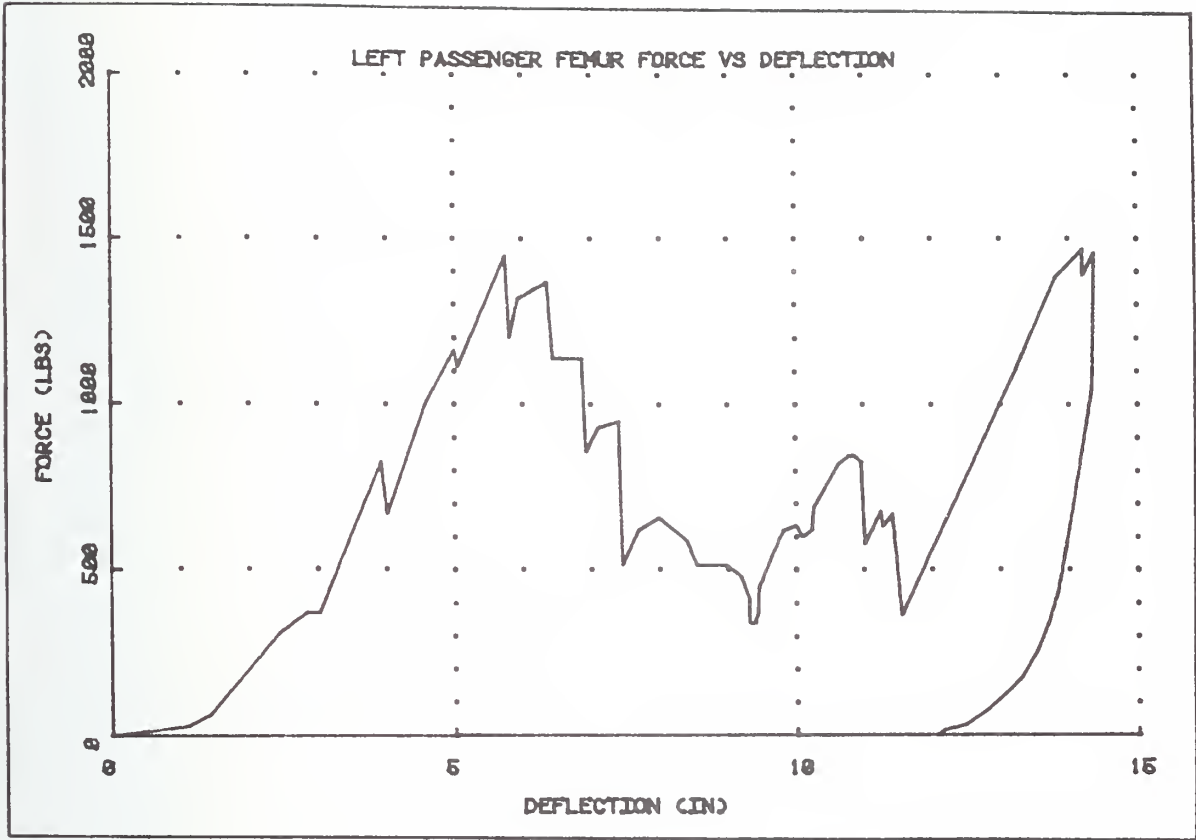
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____



Test: Left Passenger Femur Date: January 15, 1985

Vehicle: Datsun 210

Options: \_\_\_\_\_



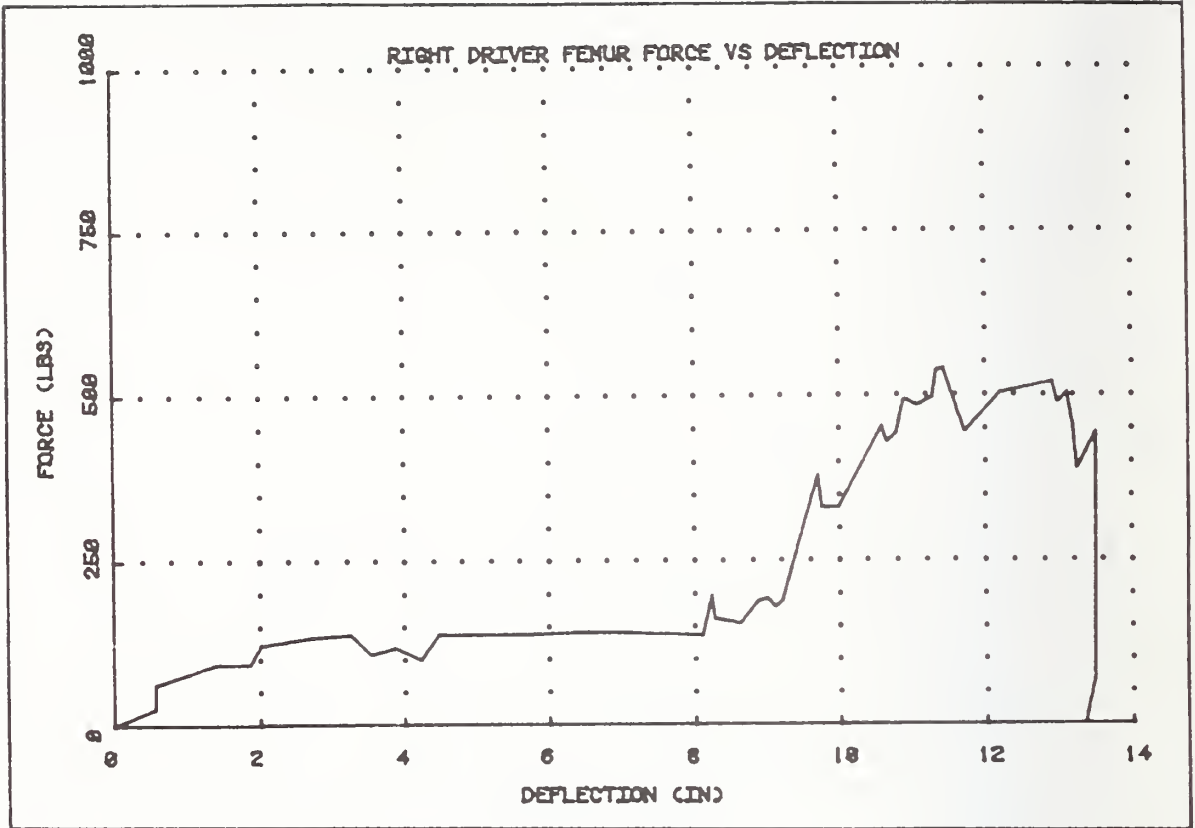
G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Right Driver Femur Date: January 15, 1985  
 Vehicle: Datsun 210  
 Options: \_\_\_\_\_



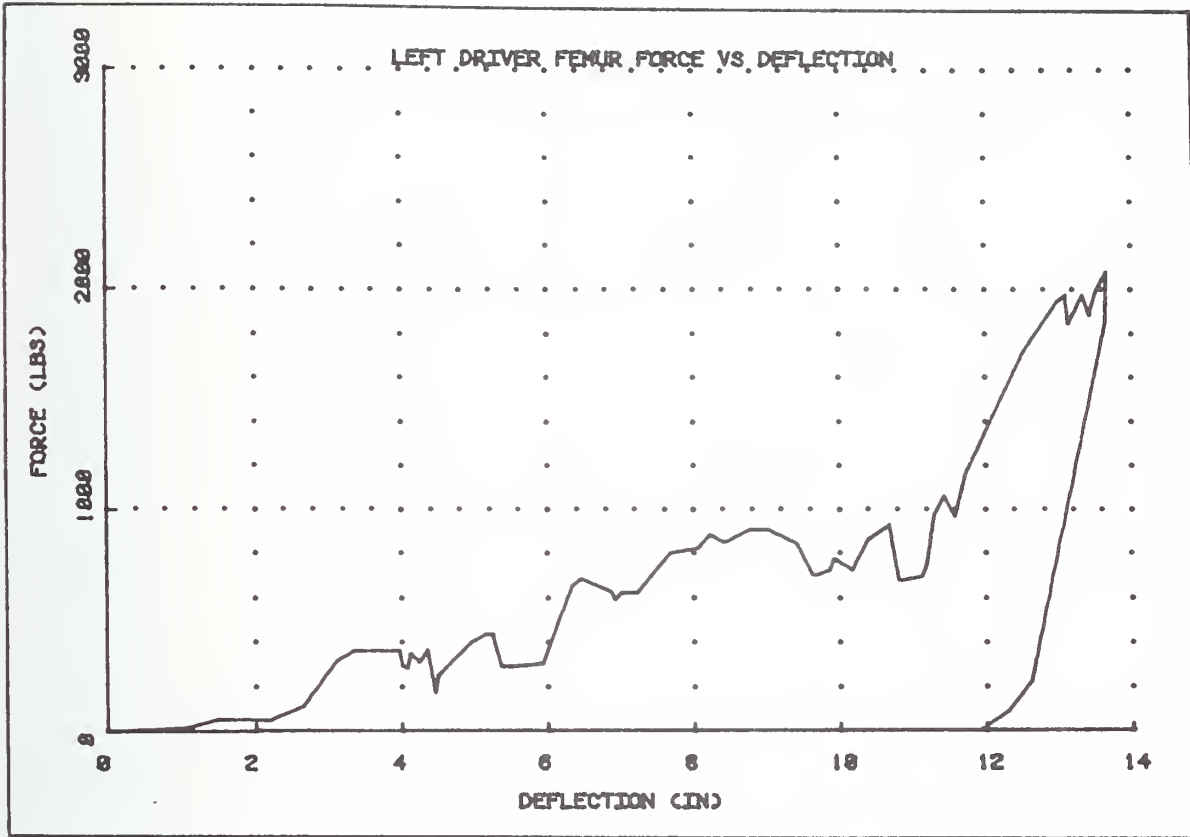
G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_  
 c= \_\_\_\_\_  $u_1$ = \_\_\_\_\_  $u_2$ = \_\_\_\_\_  $u_3$ = \_\_\_\_\_  
 $\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Left Driver Femur Date: January 15, 1985

Vehicle: Datsun 210

Options: \_\_\_\_\_



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

C= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

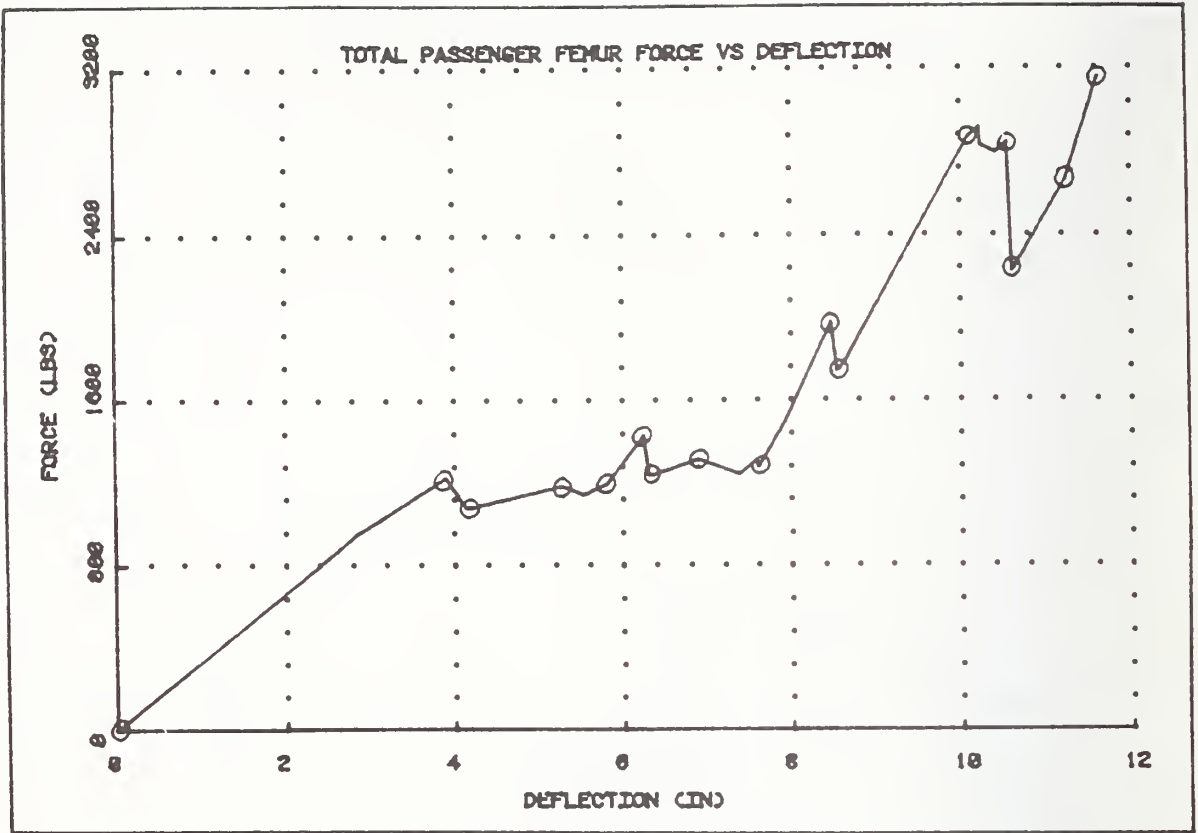
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Total Passenger Femur (Static) Date: January 16, 1985

Vehicle: Pontiac LeMans

Options: \_\_\_\_\_



G= 0.815 R= 0.116 K= 2988

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

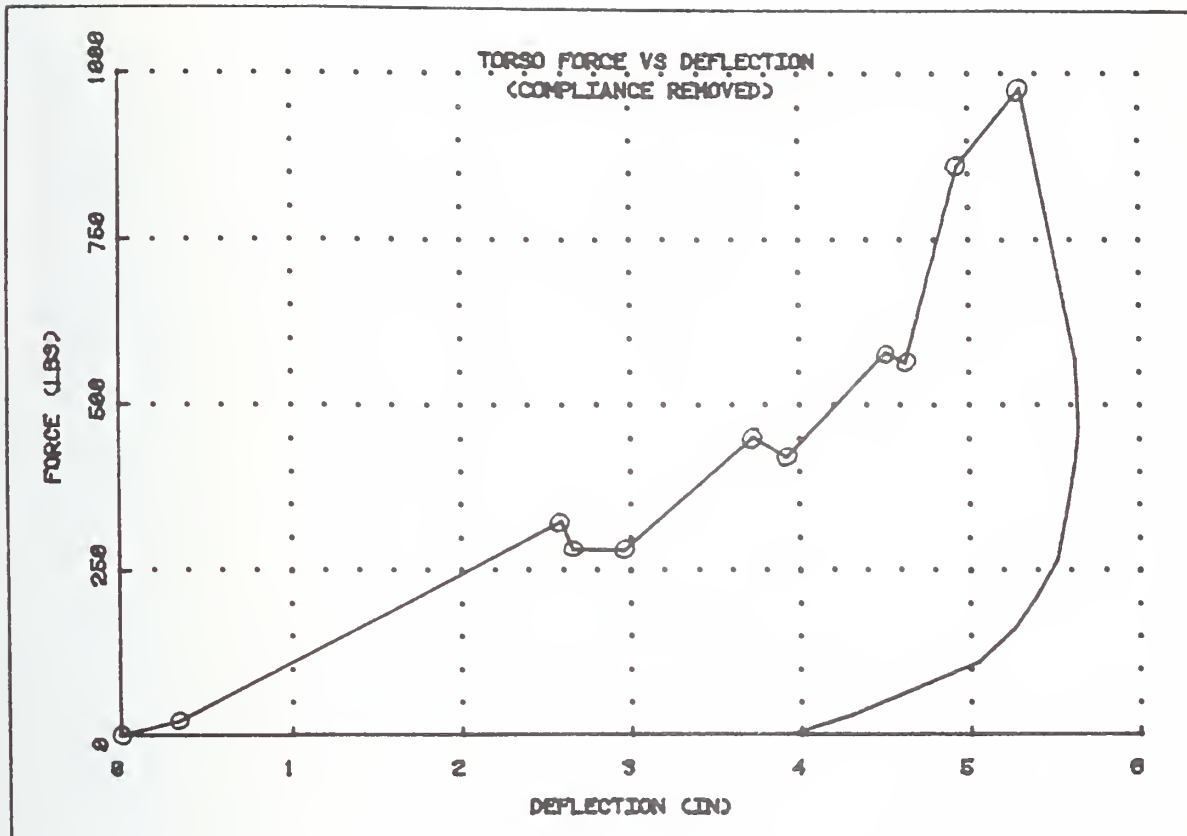
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>7.59</u>	<u>1310.9</u>
<u>3.90</u>	<u>1223.0</u>	<u>8.49</u>	<u>1975.9</u>
<u>4.14</u>	<u>1075.24</u>	<u>8.55</u>	<u>1736.37</u>
<u>5.26</u>	<u>1182.52</u>	<u>10.12</u>	<u>2872.0</u>
<u>5.81</u>	<u>1194.4</u>	<u>10.58</u>	<u>2842.9</u>
<u>6.25</u>	<u>1428.3</u>	<u>10.61</u>	<u>2216.8</u>
<u>6.31</u>	<u>1231.37</u>	<u>11.25</u>	<u>2663.5</u>
<u>6.87</u>	<u>1310.78</u>	<u>11.64</u>	<u>3155.8</u>

Test: Torso (Static) Date: January 16, 1985

Vehicle: Pontiac LeMans

Options: Compliance Removed



G= 0.699 R= 0.091 K= 581

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

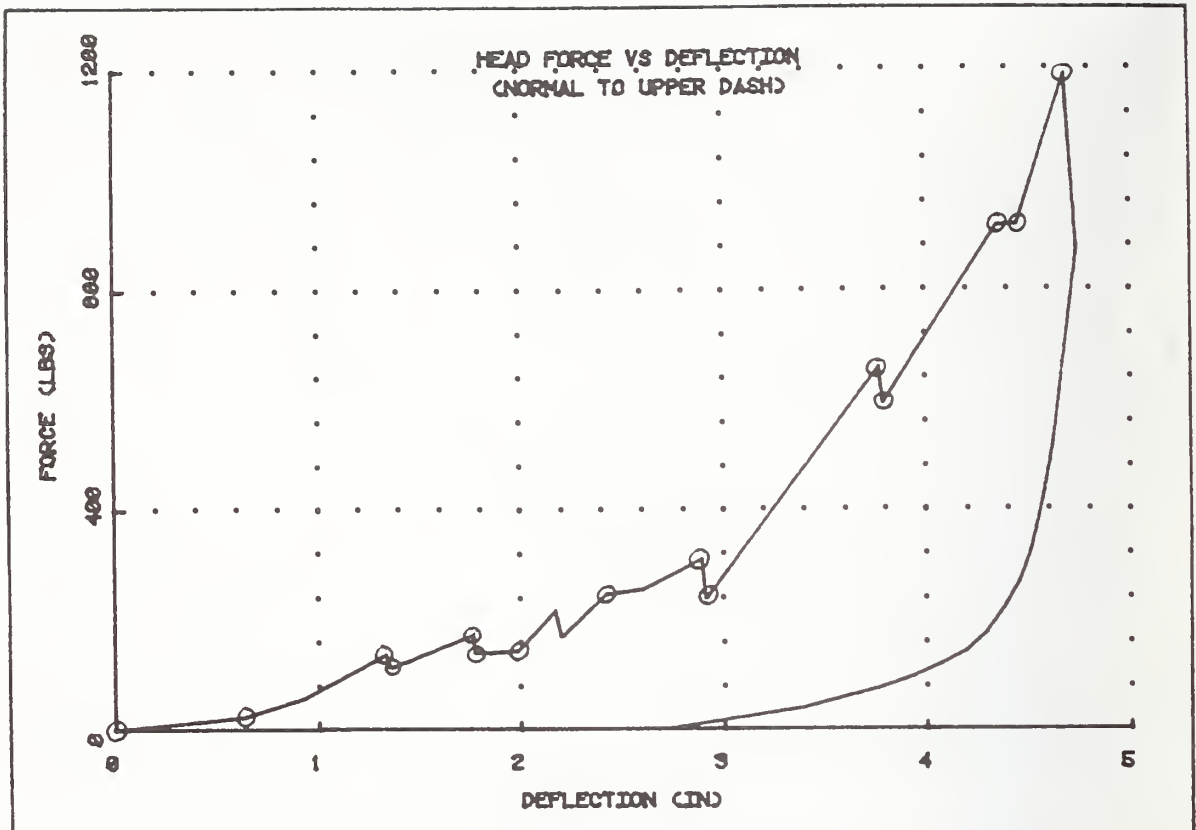
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>4.63</u>	<u>561.2</u>
<u>0.34</u>	<u>22.7</u>	<u>4.94</u>	<u>861.7</u>
<u>2.59</u>	<u>323.74</u>	<u>5.31</u>	<u>978.7</u>
<u>2.66</u>	<u>280.75</u>		
<u>2.96</u>	<u>278.3</u>		
<u>3.72</u>	<u>451.22</u>		
<u>3.92</u>	<u>420.5</u>		
<u>4.51</u>	<u>578.0</u>		

Test: Head (Static) Date: January 16, 1985

Vehicle: Pontiac LeMans

Options: Normal



G= 0.578 R= 0.173 K= 1392

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

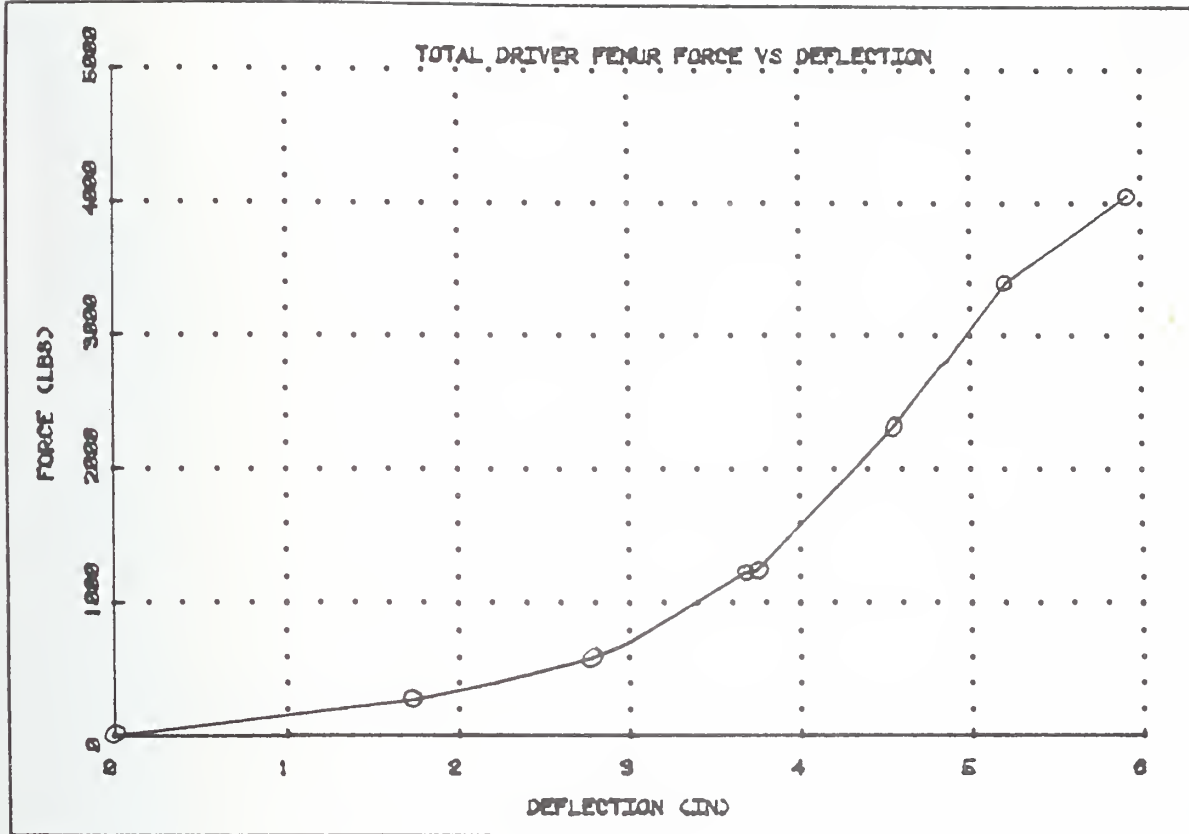
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>2.90</u>	<u>309.79</u>
<u>0.63</u>	<u>23.4</u>	<u>2.92</u>	<u>236.07</u>
<u>1.33</u>	<u>137.5</u>	<u>3.78</u>	<u>658.89</u>
<u>1.35</u>	<u>112.95</u>	<u>3.80</u>	<u>591.18</u>
<u>1.76</u>	<u>172.87</u>	<u>4.36</u>	<u>915.4</u>
<u>1.77</u>	<u>138.11</u>	<u>4.46</u>	<u>917.5</u>
<u>1.99</u>	<u>143.5</u>	<u>4.69</u>	<u>1190.4</u>
<u>2.42</u>	<u>247.29</u>		

Test: Total Driver Femur

Date: January 17, 1985

Vehicle: Pontiac LeMans

Options: \_\_\_\_\_



G= 0.711 R= 0.292 K= 3729

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_5$ = \_\_\_\_\_

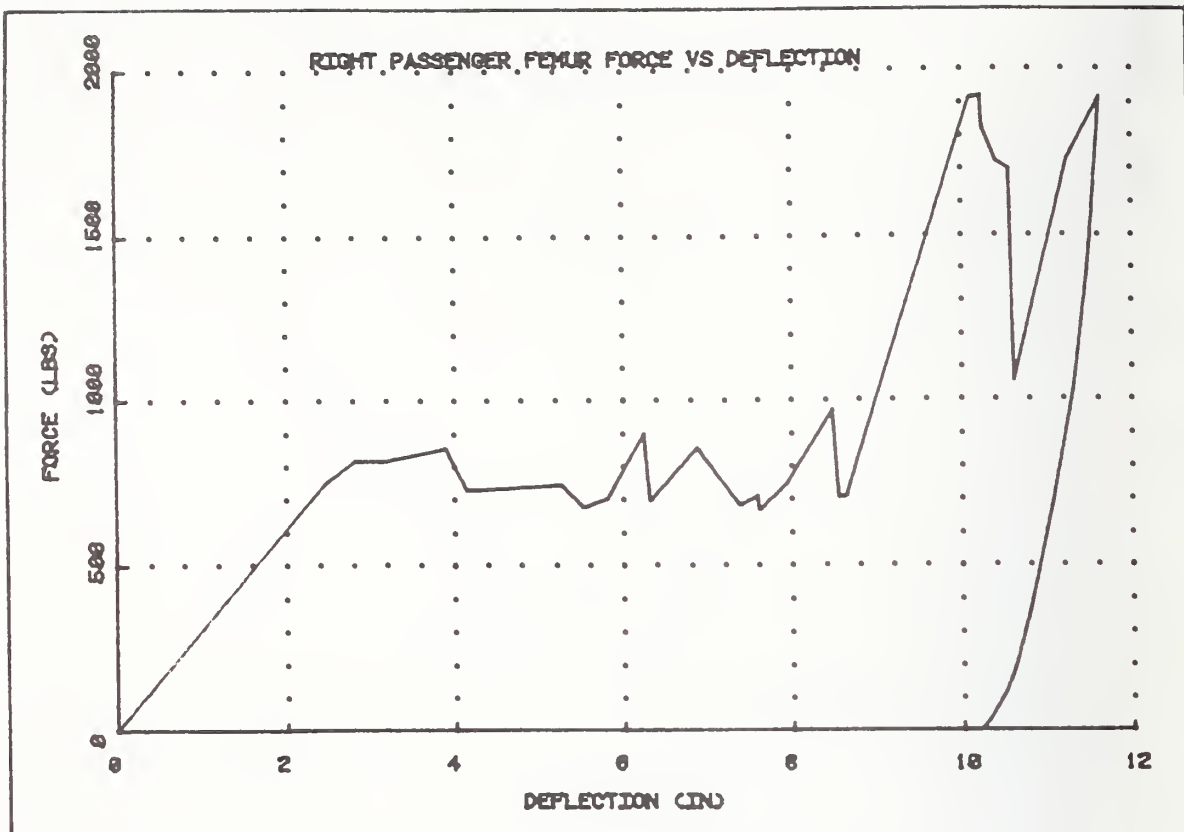
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	_____	_____
<u>1.75</u>	<u>269.8</u>	_____	_____
<u>2.78</u>	<u>591.4</u>	_____	_____
<u>3.68</u>	<u>1227.0</u>	_____	_____
<u>3.74</u>	<u>1242.0</u>	_____	_____
<u>4.56</u>	<u>2334.1</u>	_____	_____
<u>5.21</u>	<u>3397.7</u>	_____	_____
<u>5.93</u>	<u>4065.4</u>	_____	_____

Test: Right Passenger Femur Date: January 16, 1985

Vehicle: Pontiac LeMans

Options: \_\_\_\_\_



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

Deflection

Force

Deflection

Force

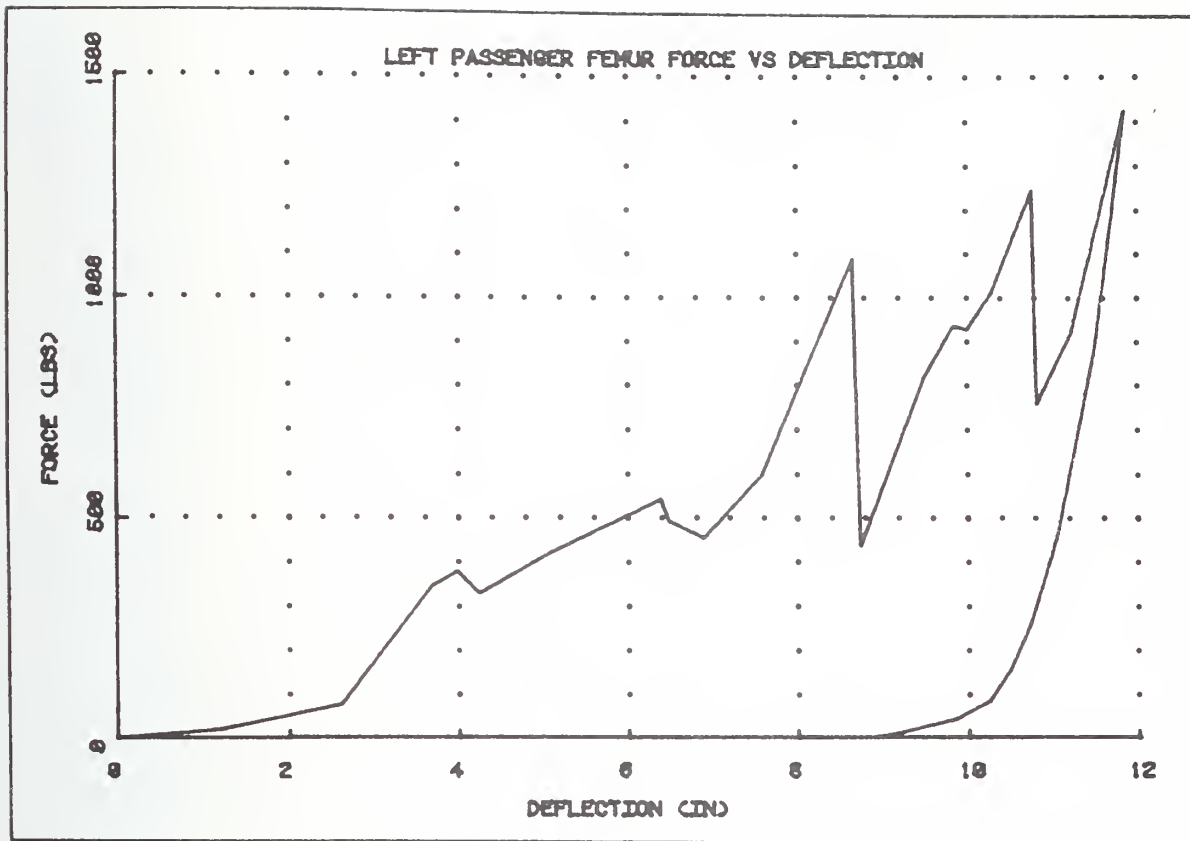
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____



Test: Left Passenger Femur Date: January 16, 1985

Vehicle: Pontiac LeMans

Options: \_\_\_\_\_



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

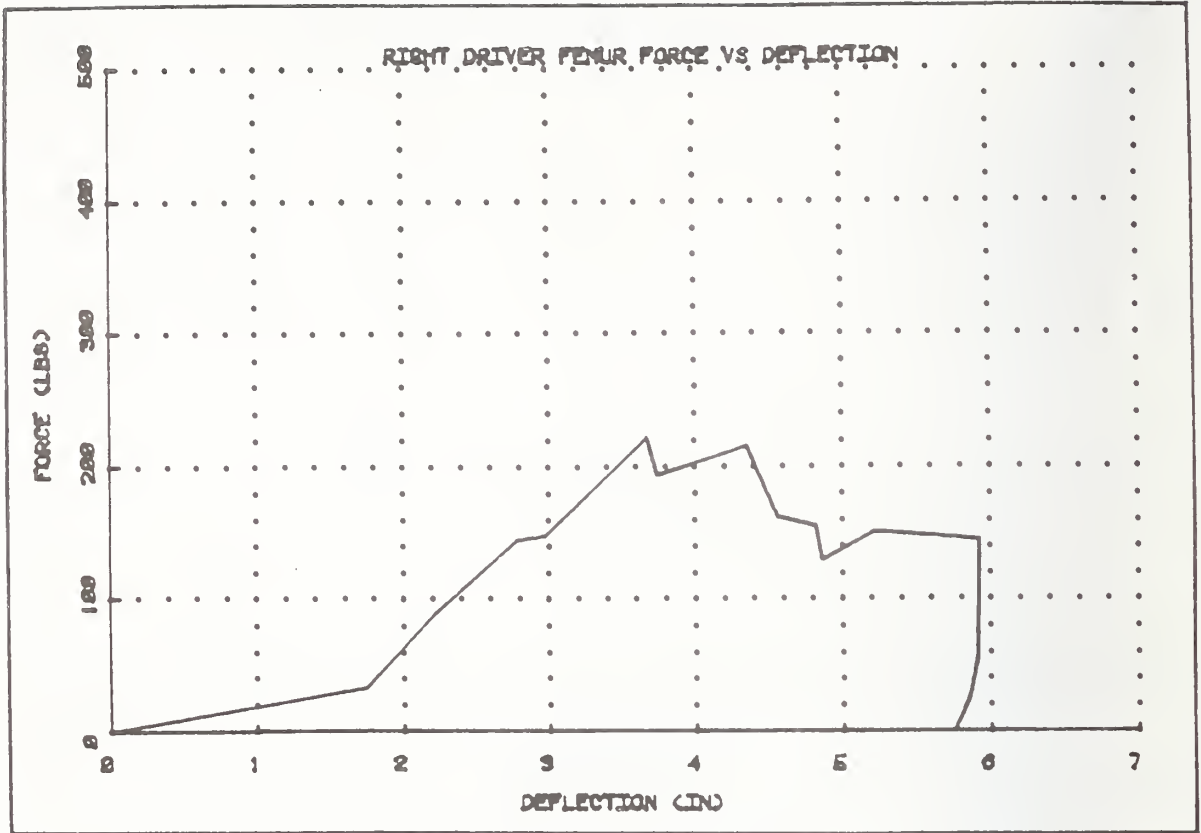
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Right Driver Femur

Date: January 17, 1985

Vehicle: Pontiac Lemans

Options: \_\_\_\_\_



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_ u<sub>1</sub>= \_\_\_\_\_ u<sub>2</sub>= \_\_\_\_\_ u<sub>3</sub>= \_\_\_\_\_

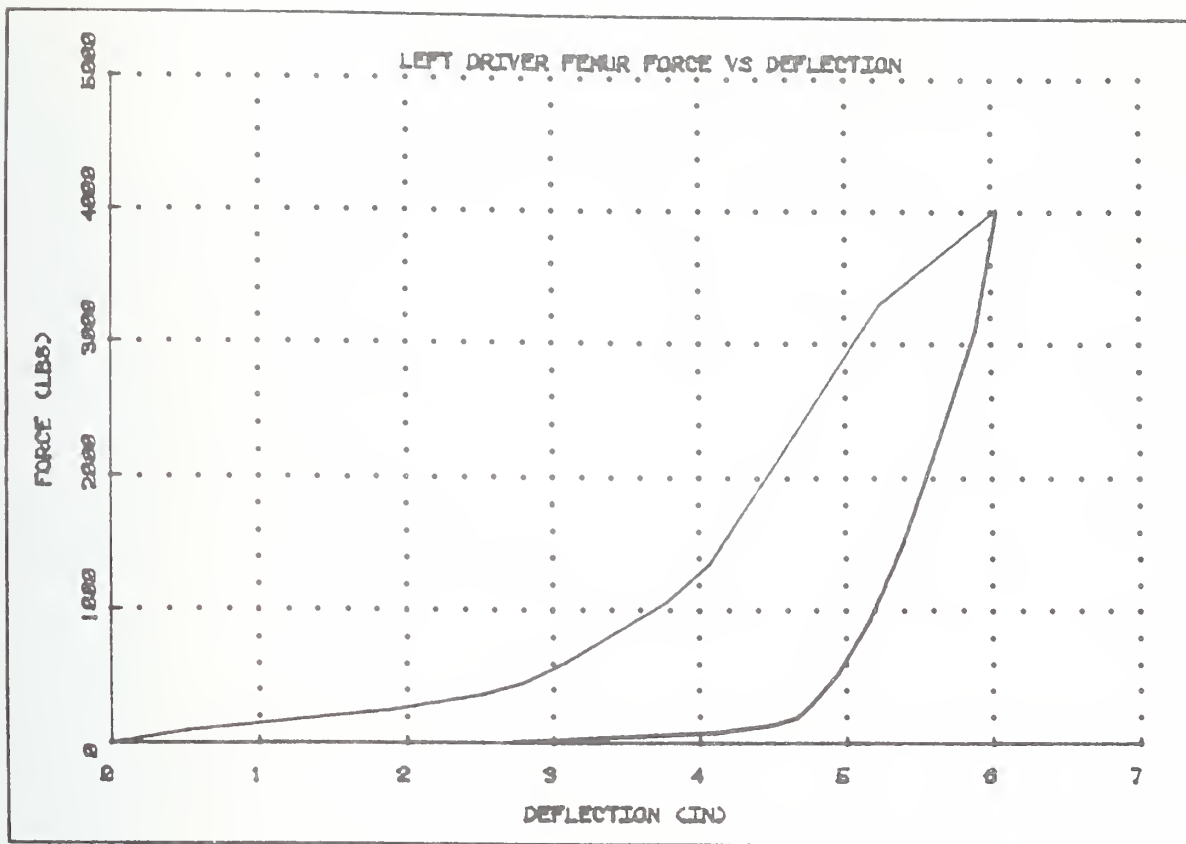
δ<sub>A</sub>= 0.0 δ<sub>B</sub>= 0.0 δ<sub>C</sub>= 0.0 δ<sub>D</sub>= 1000.0 δ<sub>F</sub>= 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Left Driver Femur Date: January 17, 1985

Vehicle: Pontiac LeMans

Options: \_\_\_\_\_



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

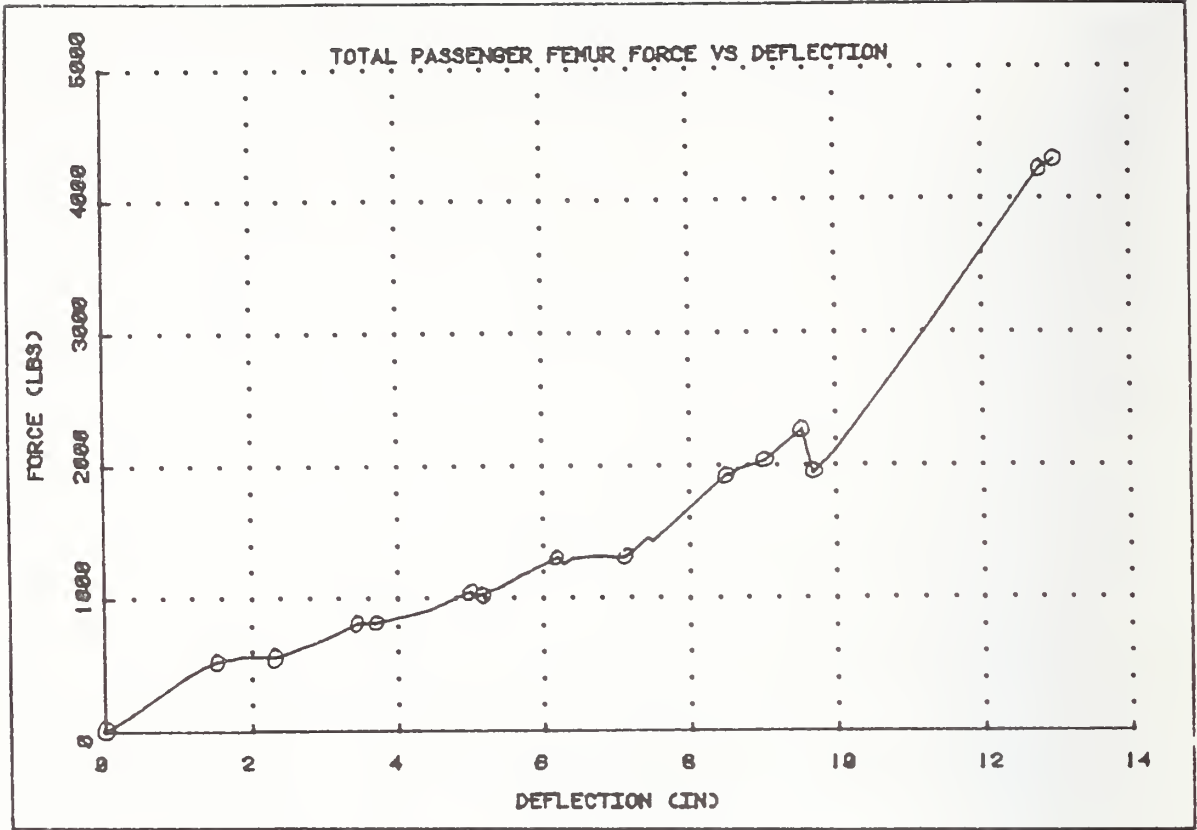
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Passenger Side Femur

Date: January 18, 1985

Vehicle: Chevy Nova

Options: \_\_\_\_\_



G= 0.815

R= 0.142

K= 3163

c= \_\_\_\_\_

$\nu_1$ = \_\_\_\_\_

$\nu_2$ = \_\_\_\_\_

$\nu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0

$\delta_B$ = 0.0

$\delta_C$ = 0.0

$\delta_D$ = 1000.0

$\delta_F$ = 1000.1

Deflection

Force

Deflection

Force

0.0

0.0

7.07

1302.5

1.52

527.4

8.51

1934.5

2.28

560.8

9.05

2046.5

3.46

820.4

9.54

2278.2

3.68

815.4

9.69

1938.5

5.01

1057.5

12.80

4232.5

5.12

1032.7

12.98

4293.7

6.20

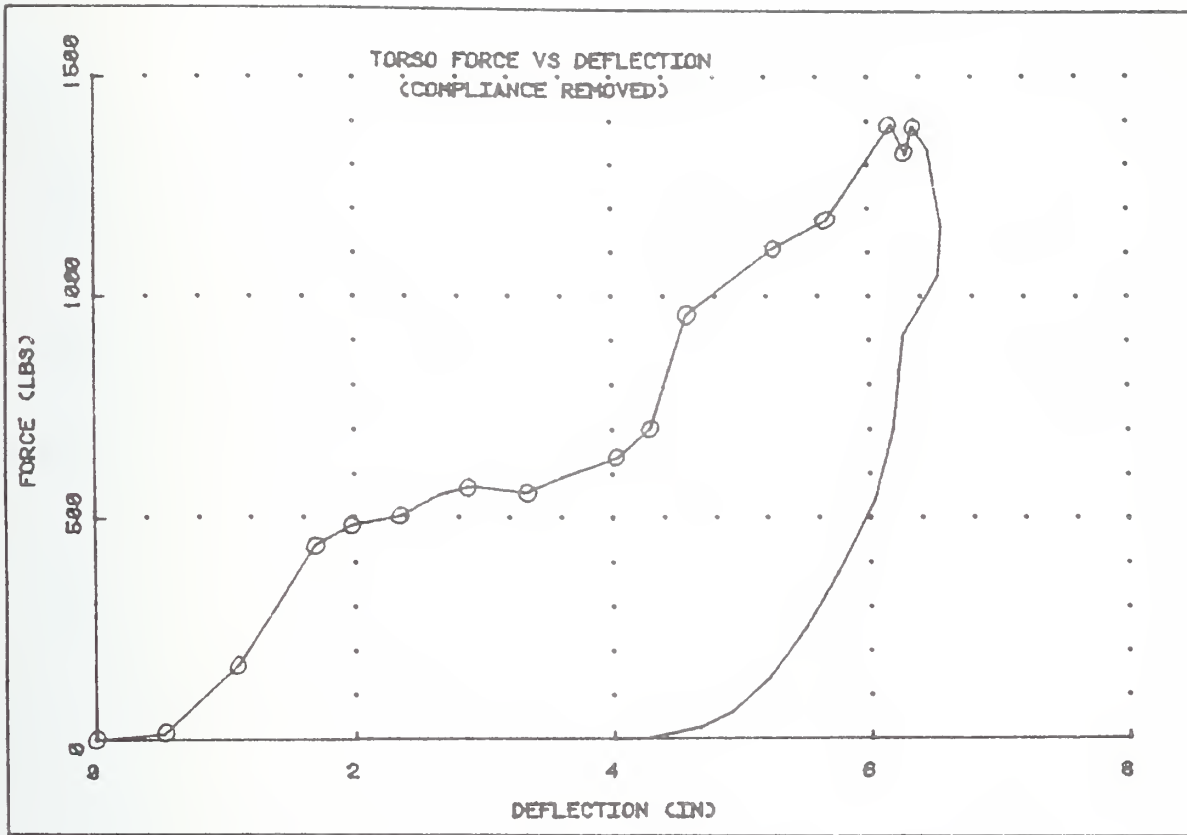
1312.9

Test: Torso

Date: January 18, 1985

Vehicle: Chevy Nova

Options:



G= 0.650

R= 0.179

K= 880

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

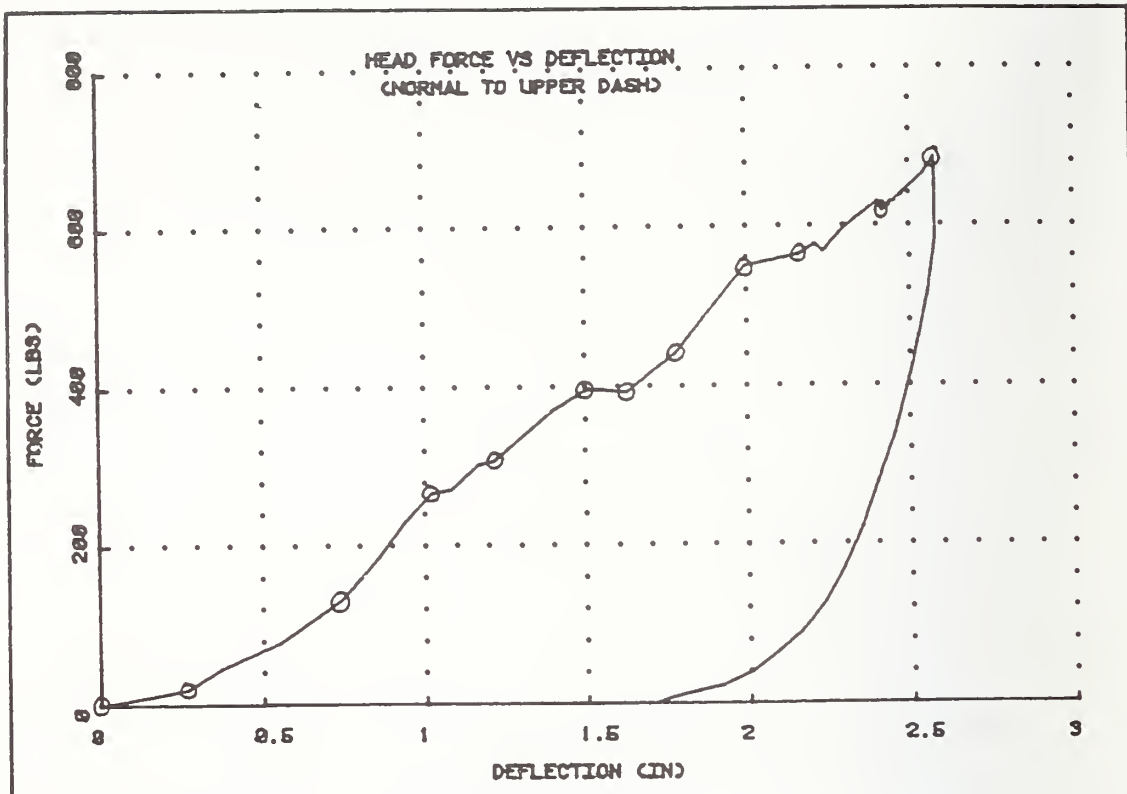
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

Deflection	Force	Deflection	Force
0.0	0.0	4.04	639.7
0.53	13.6	4.30	704.7
1.10	170.1	4.58	958.6
1.69	440.1	5.26	1112.7
1.98	485.2	5.68	1175.7
2.36	507.8	6.19	1391.6
2.88	572.6	6.30	1321.2
3.31	557.5	6.35	1387.7

Test: Head Date: January 18, 1985

Vehicle: Chevy Nova

Options: \_\_\_\_\_



G= 0.664 R= 0.157 K= 1831

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

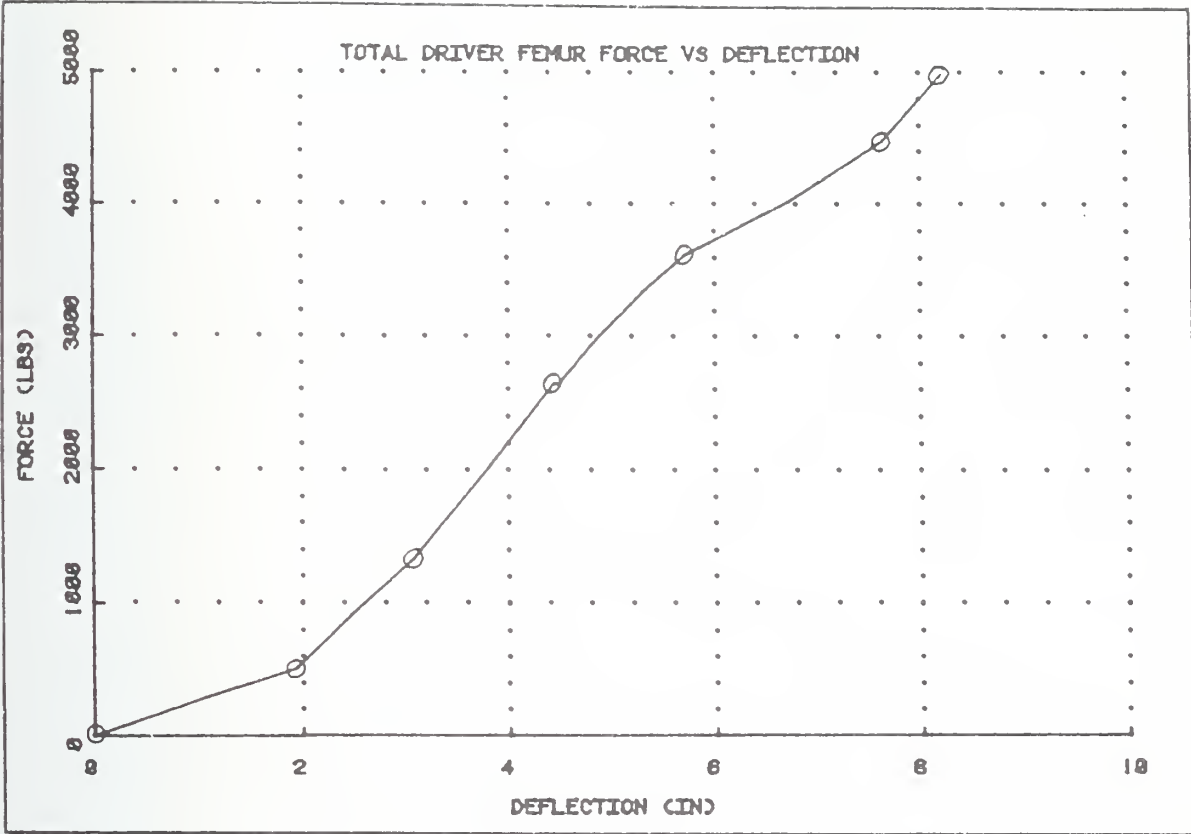
Deflection	Force	Deflection	Force
<u>0.0</u>	<u>0.0</u>	<u>2.00</u>	<u>549.9</u>
<u>0.27</u>	<u>20.1</u>	<u>2.16</u>	<u>564.3</u>
<u>0.75</u>	<u>132.8</u>	<u>2.42</u>	<u>616.8</u>
<u>1.02</u>	<u>267.0</u>	<u>2.58</u>	<u>685.3</u>
<u>1.22</u>	<u>307.1</u>		
<u>1.50</u>	<u>396.4</u>		
<u>1.62</u>	<u>392.6</u>		
<u>1.78</u>	<u>442.1</u>		

Intermediate Unloads	Maximum Deflection (in.)	G	R	K
First	1.41	0.641	0.297	1072
Second	2.02	0.641	0.232	1075

Test: Driver Side Femur Date: January 18, 1985

Vehicle: Chevy Nova

Options: \_\_\_\_\_



G= 0.715 R= 0.163 K= 4071

c= \_\_\_\_\_ u<sub>1</sub>= \_\_\_\_\_ u<sub>2</sub>= \_\_\_\_\_ u<sub>3</sub>= \_\_\_\_\_

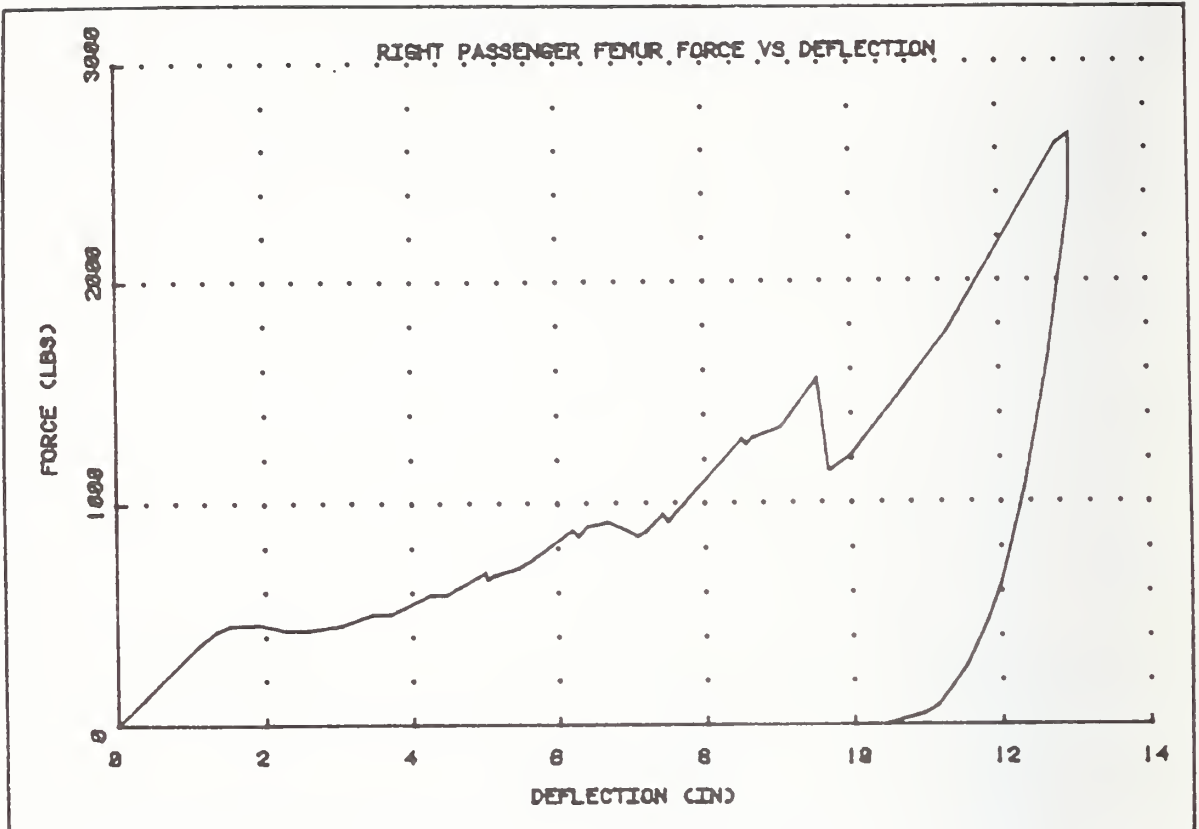
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	_____	_____
<u>1.94</u>	<u>508.6</u>	_____	_____
<u>3.07</u>	<u>1336.3</u>	_____	_____
<u>4.45</u>	<u>2650.0</u>	_____	_____
<u>5.72</u>	<u>3620.5</u>	_____	_____
<u>7.64</u>	<u>4482.1</u>	_____	_____
<u>8.22</u>	<u>4978.9</u>	_____	_____
_____	_____	_____	_____

Test: Right Passenger Femur Date: January 18, 1985

Vehicle: Chevy Nova

Options: \_\_\_\_\_



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

C= \_\_\_\_\_  $u_1$ = \_\_\_\_\_  $u_2$ = \_\_\_\_\_  $u_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

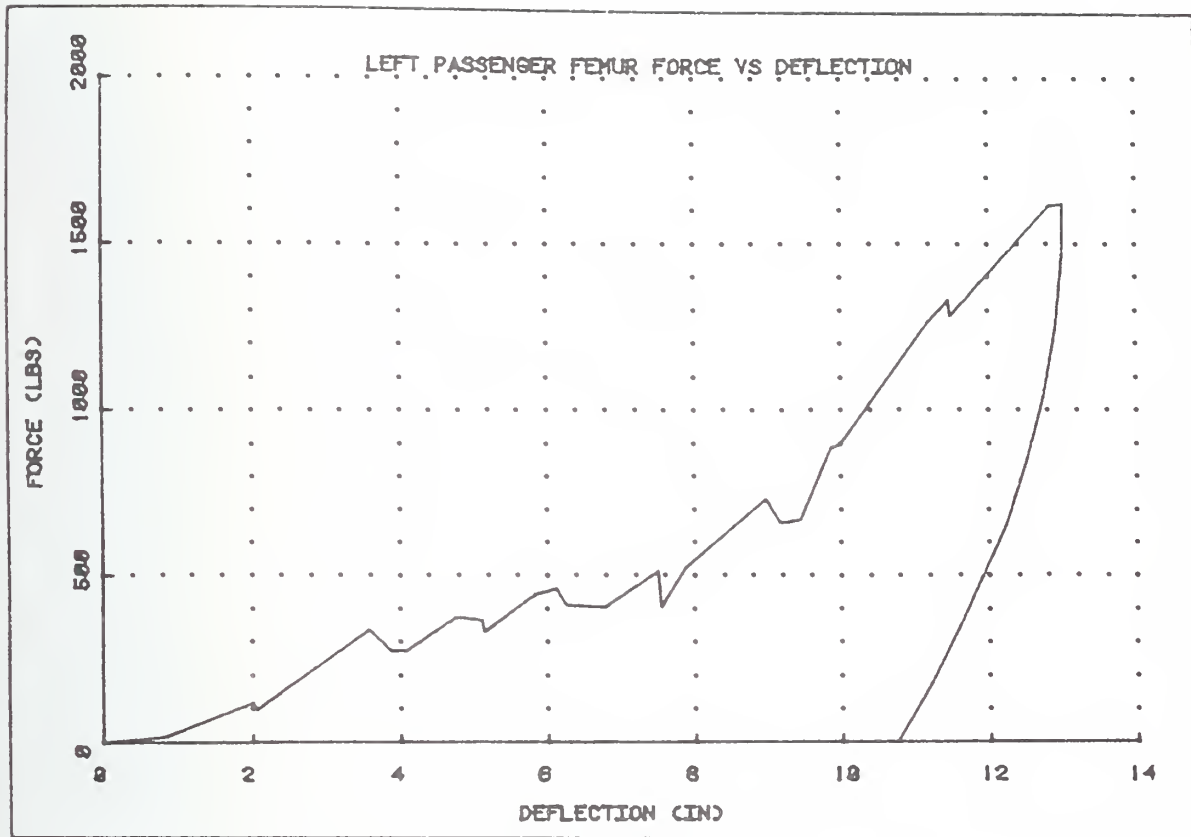
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____



Test: Left Passenger Femur Date: January 18, 1985

Vehicle: Chevy Nova

Options: \_\_\_\_\_



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_ u<sub>1</sub>= \_\_\_\_\_ u<sub>2</sub>= \_\_\_\_\_ u<sub>3</sub>= \_\_\_\_\_

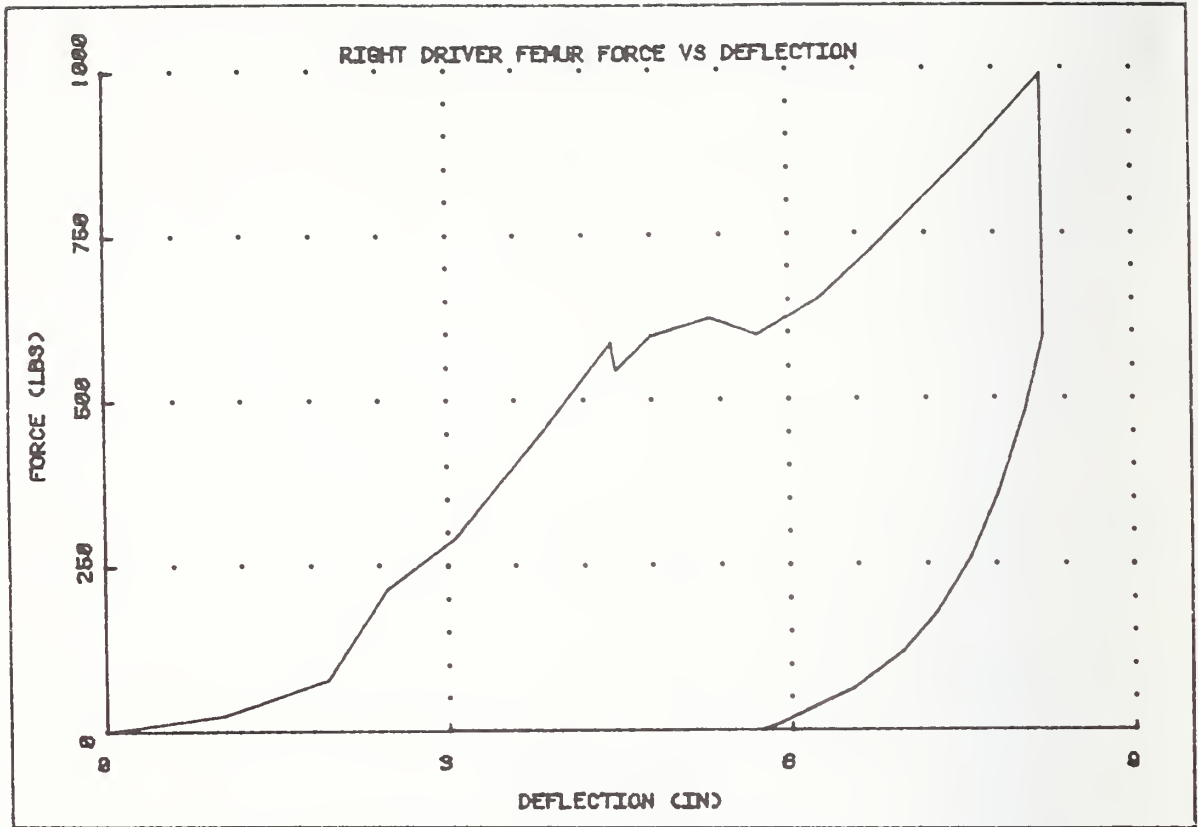
δ<sub>A</sub>= 0.0 δ<sub>B</sub>= 0.0 δ<sub>C</sub>= 0.0 δ<sub>D</sub>= 1000.0 δ<sub>F</sub>= 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Right Driver Femur Date: January 18, 1985

Vehicle: Chevy Nova

Options: \_\_\_\_\_



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $u_1$ = \_\_\_\_\_  $u_2$ = \_\_\_\_\_  $u_3$ = \_\_\_\_\_

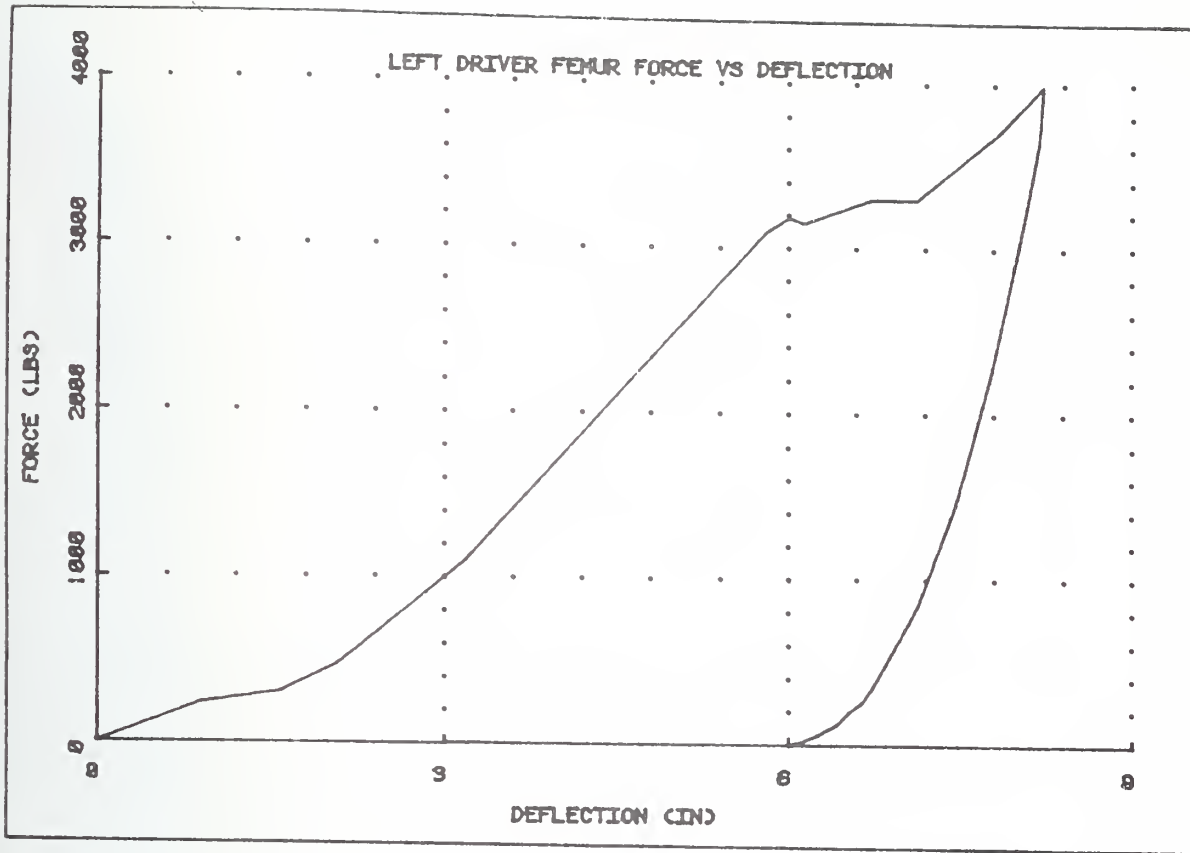
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Left Driver Femur Date: January 18, 1985

Vehicle: Chevy Nova

Options: \_\_\_\_\_  
\_\_\_\_\_



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

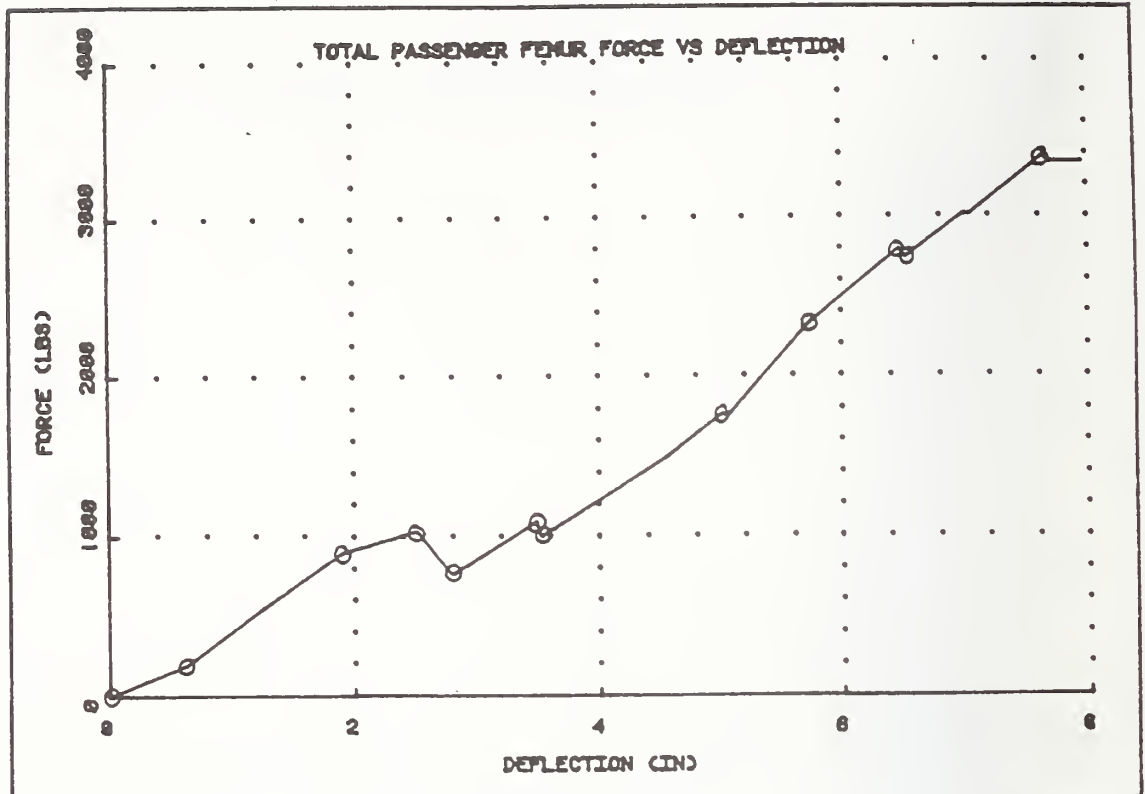
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Passenger Side Femur Date: January 24, 1985

Vehicle: Ford Granada

Options: \_\_\_\_\_



G= 0.677 R= 0.135 K= 2492

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

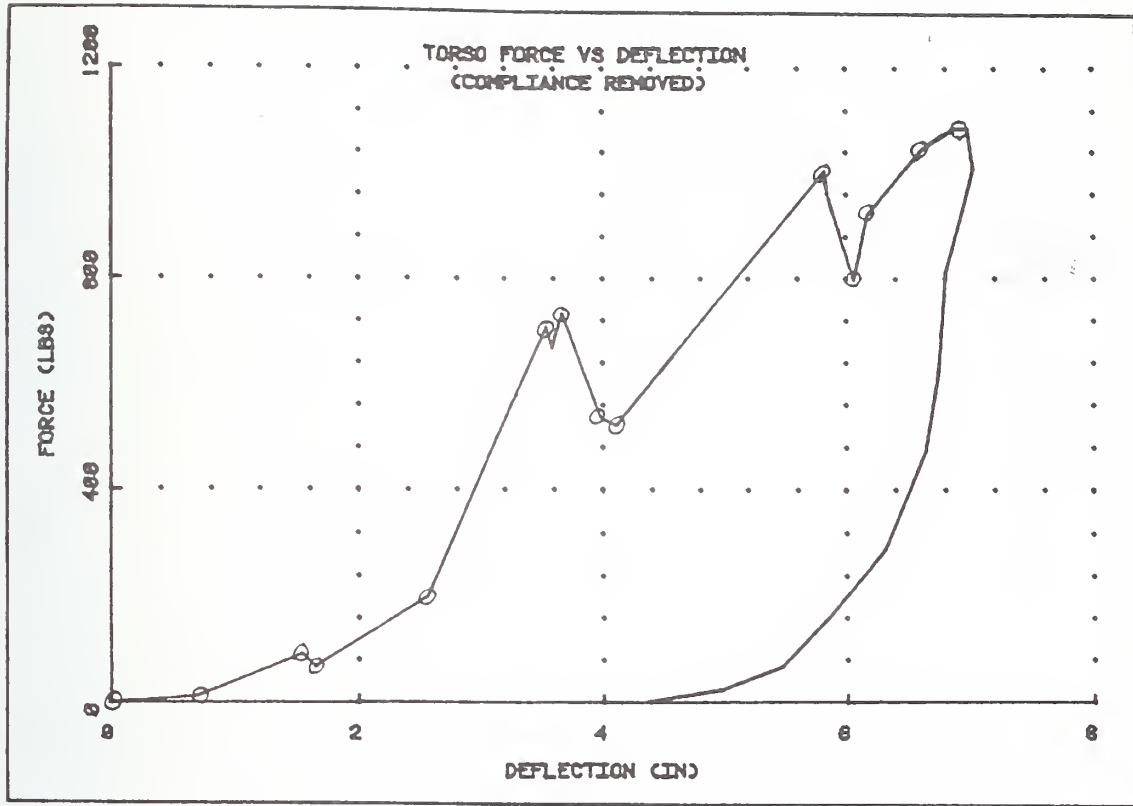
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>5.73</u>	<u>2327.6</u>
<u>0.63</u>	<u>189.0</u>	<u>6.47</u>	<u>2791.2</u>
<u>1.91</u>	<u>900.3</u>	<u>6.52</u>	<u>2740.7</u>
<u>2.50</u>	<u>1031.3</u>	<u>7.65</u>	<u>3381.6</u>
<u>2.79</u>	<u>758.2</u>		
<u>3.49</u>	<u>1092.3</u>		
<u>3.53</u>	<u>995.1</u>		
<u>5.02</u>	<u>1761.6</u>		

<u>Intermediate Unload</u>	<u>Maximum Deflection (in.)</u>	<u>G</u>	<u>R</u>	<u>K</u>
<u>First</u>	<u>5.03</u>	<u>0.502</u>	<u>0.313</u>	<u>1080</u>
<u>Second</u>	<u>4.92</u>	<u>0.641</u>	<u>0.252</u>	<u>1903</u>

Test: Torso Date: January 24, 1985

Vehicle: Ford Granada

Options: \_\_\_\_\_



G= 0.621 R= 0.175 K= 836

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

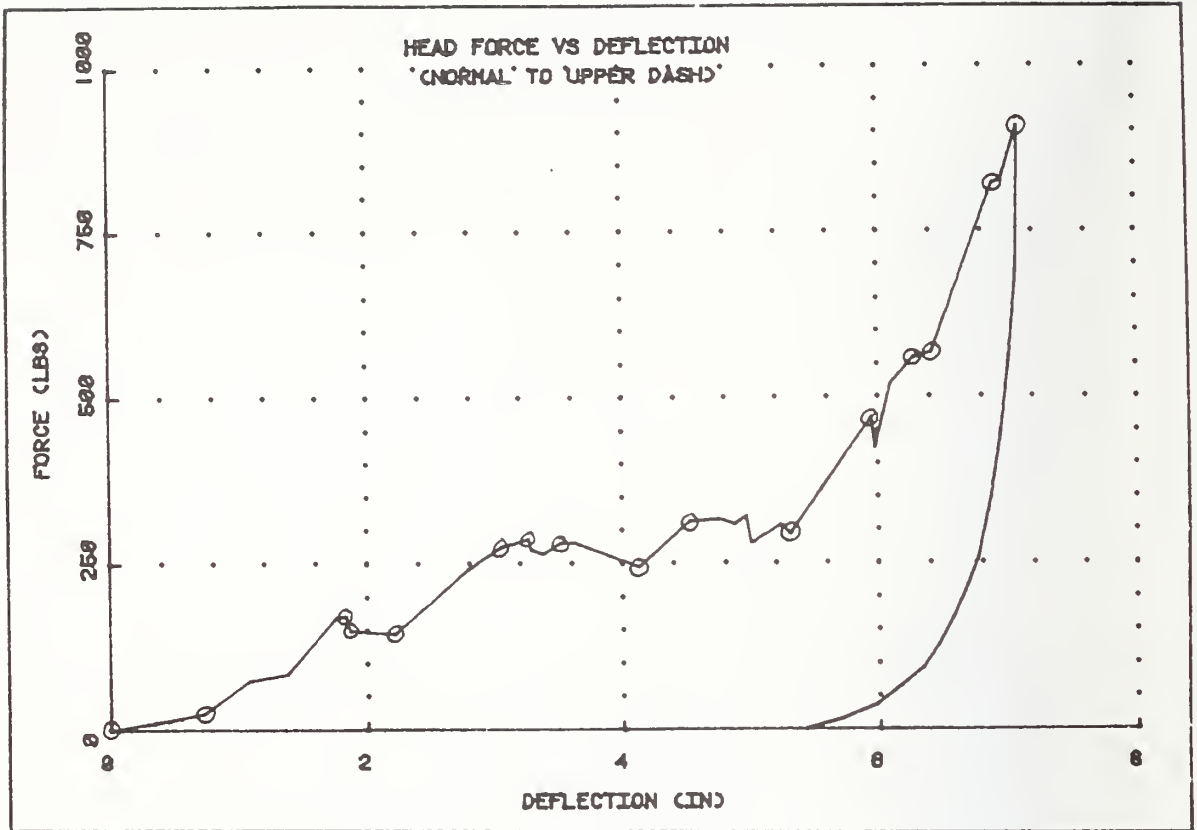
Deflection	Force	Deflection	Force
0.0	0.0	4.11	521.0
0.69	12.1	5.83	1003.9
1.53	89.8	6.06	797.5
1.64	65.4	6.17	922.8
2.56	201.4	6.61	1044.4
3.54	706.1	6.93	1086.7
3.67	732.7		
3.99	533.4		

Intermediate Unload	Maximum Deflection (in.)	G	R	K
First	4.14	0.671	0.220	611
Second	6.61	0.701	0.119	1431

Test: Head Date: January 24, 1985

Vehicle: Ford Granada

Options: \_\_\_\_\_



G= 0.764 R= .0129 K= 1613

C= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

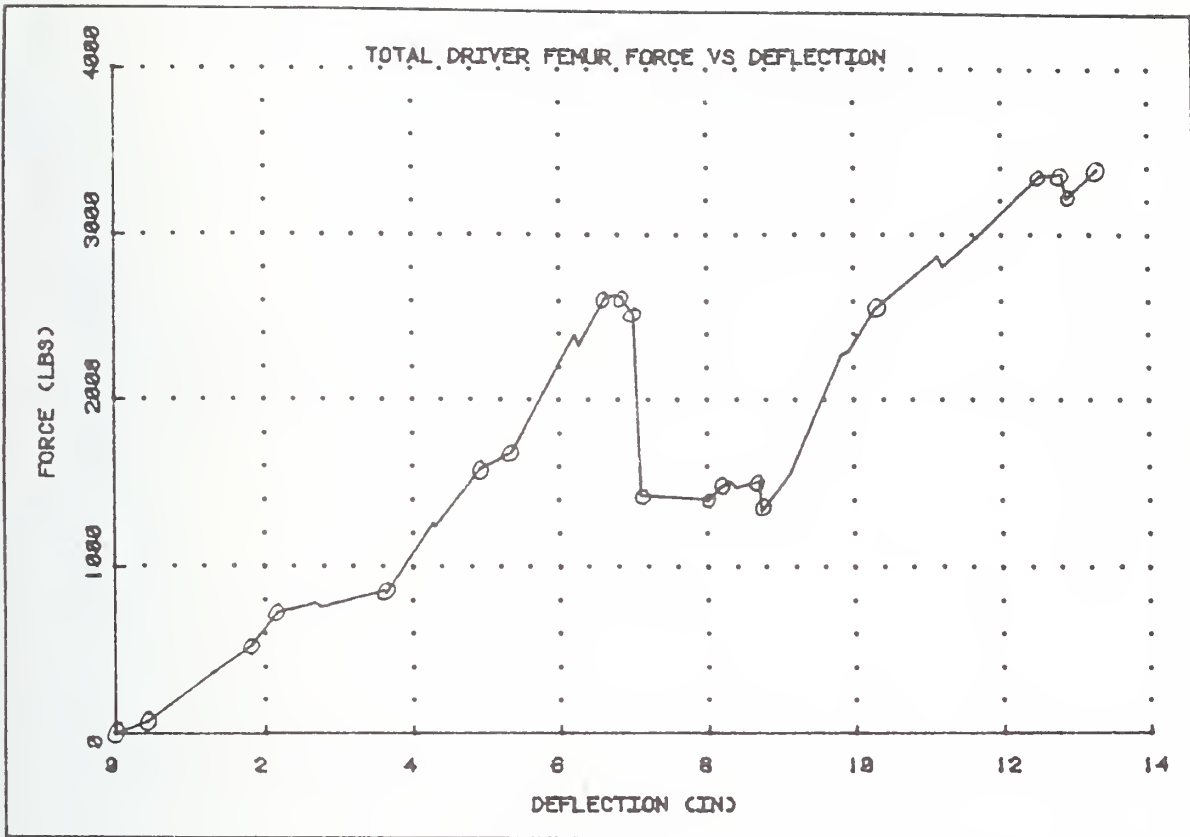
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>4.12</u>	<u>243.7</u>
<u>0.73</u>	<u>24.7</u>	<u>4.53</u>	<u>313.0</u>
<u>1.83</u>	<u>171.7</u>	<u>5.31</u>	<u>292.6</u>
<u>1.87</u>	<u>147.9</u>	<u>5.95</u>	<u>469.5</u>
<u>2.21</u>	<u>143.0</u>	<u>6.28</u>	<u>559.9</u>
<u>3.06</u>	<u>275.4</u>	<u>6.42</u>	<u>566.7</u>
<u>3.26</u>	<u>287.7</u>	<u>6.90</u>	<u>820.5</u>
<u>3.52</u>	<u>280.9</u>	<u>7.10</u>	<u>908.3</u>

Test: Driver Side Femur

Date: January 24, 1985

Vehicle: Ford Granada

Options: \_\_\_\_\_



G= 0.822 R= 0.116 K= 2228

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

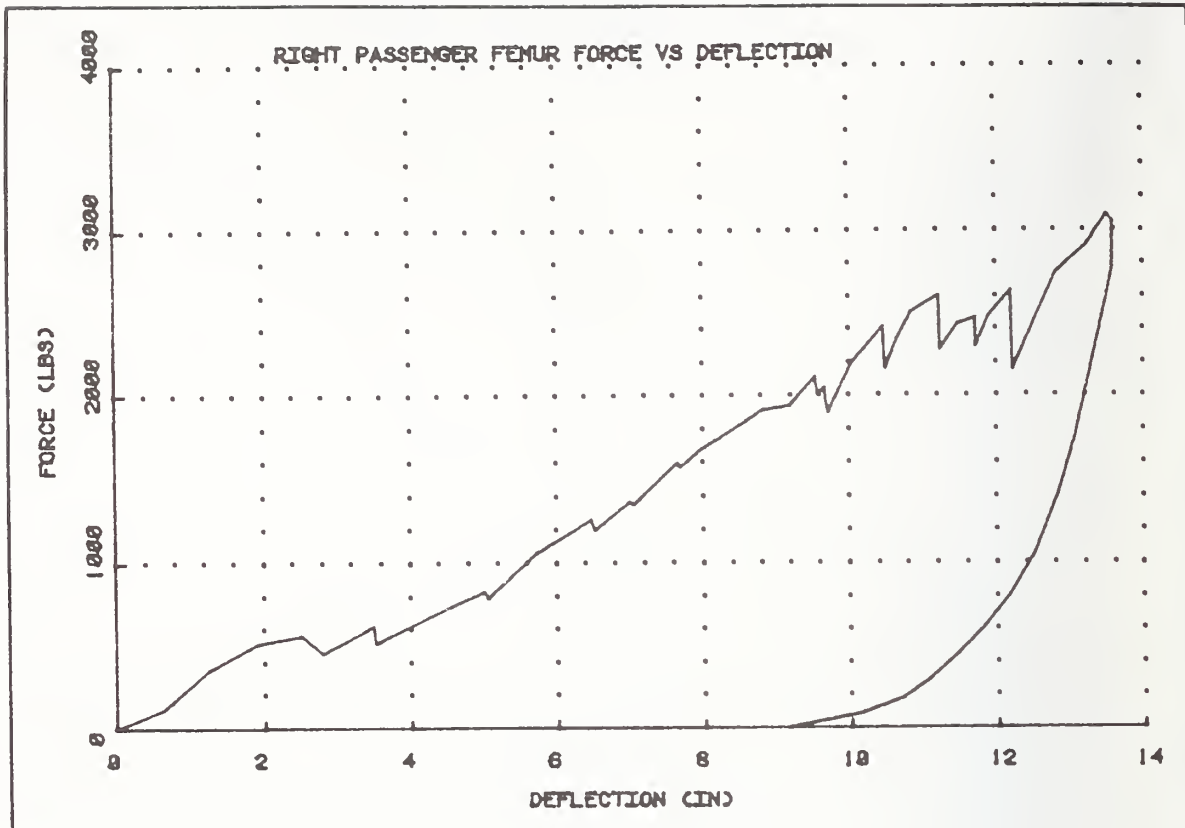
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>7.10</u>	<u>1420.4</u>
<u>0.44</u>	<u>73.8</u>	<u>7.99</u>	<u>1399.1</u>
<u>1.82</u>	<u>527.2</u>	<u>8.18</u>	<u>1481.1</u>
<u>2.18</u>	<u>730.0</u>	<u>8.70</u>	<u>1515.2</u>
<u>3.64</u>	<u>839.2</u>	<u>8.74</u>	<u>1330.9</u>
<u>4.93</u>	<u>1588.3</u>	<u>10.28</u>	<u>2550.6</u>
<u>5.36</u>	<u>1686.9</u>	<u>12.52</u>	<u>3353.4</u>
<u>6.63</u>	<u>2624.2</u>	<u>12.83</u>	<u>3366.9</u>
<u>6.84</u>	<u>2620.3</u>	<u>12.88</u>	<u>3213.3</u>
<u>7.01</u>	<u>2512.3</u>	<u>13.31</u>	<u>3394.9</u>

Test: Right Passenger Femur Date: January 24, 1985

Vehicle: Ford Granada

Options: \_\_\_\_\_



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

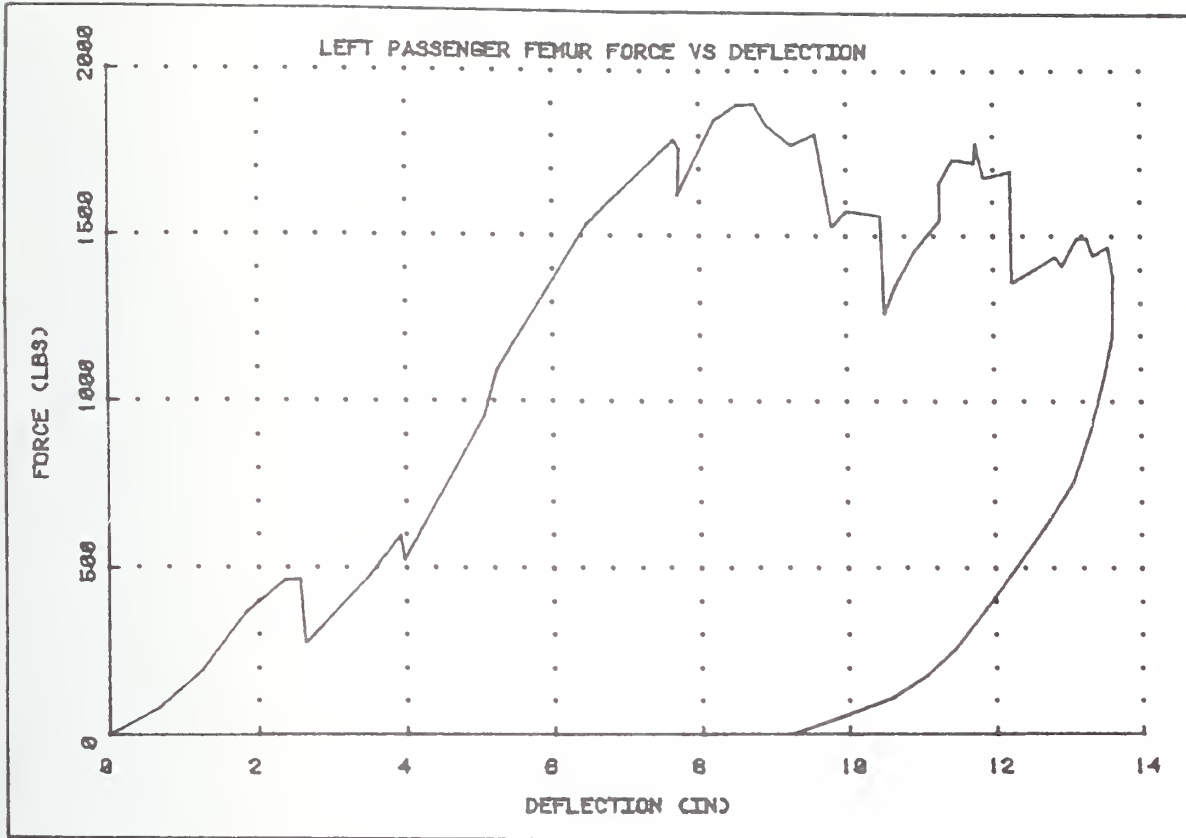
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____



Test: Left Passenger Femur Date: January 24, 1985

Vehicle: Ford Granada

Options: \_\_\_\_\_  
\_\_\_\_\_



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

Deflection

Force

Deflection

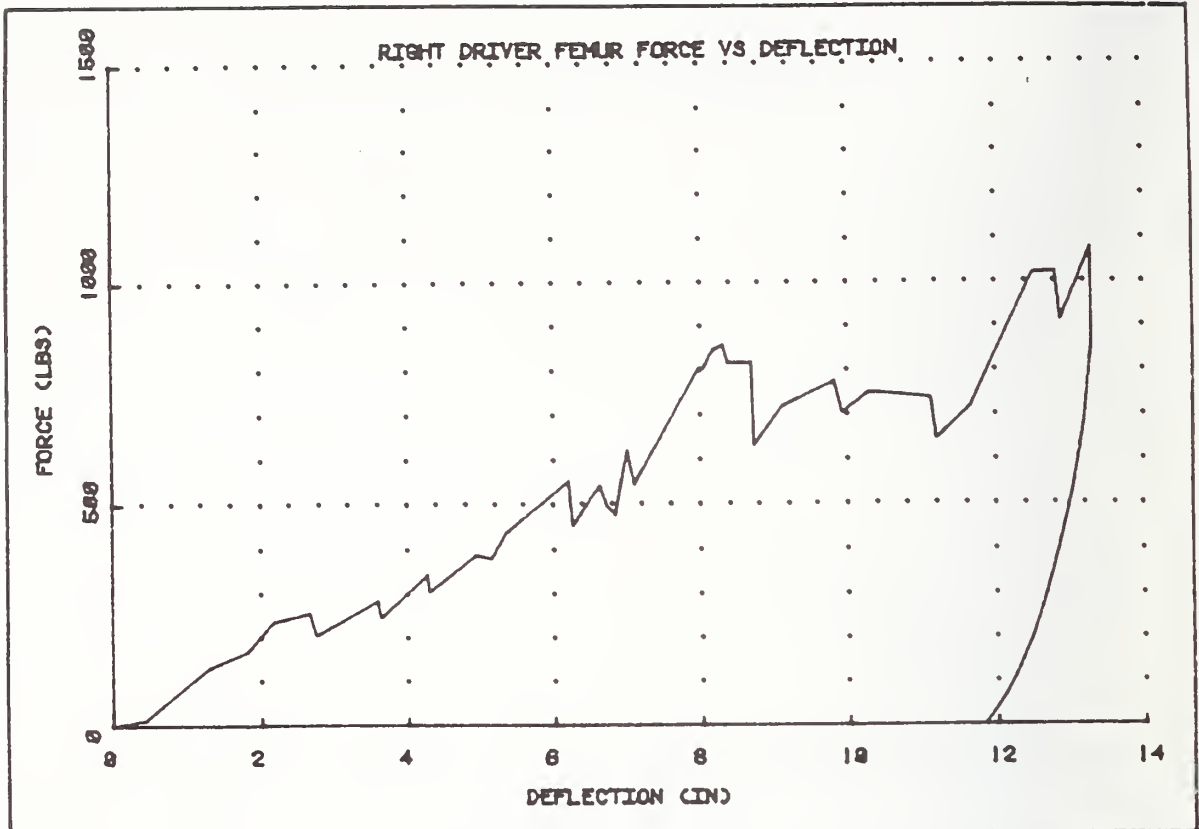
Force

_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Right Driver Femur Date: January 24, 1985

Vehicle: Ford Granada

Options: \_\_\_\_\_



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

C= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

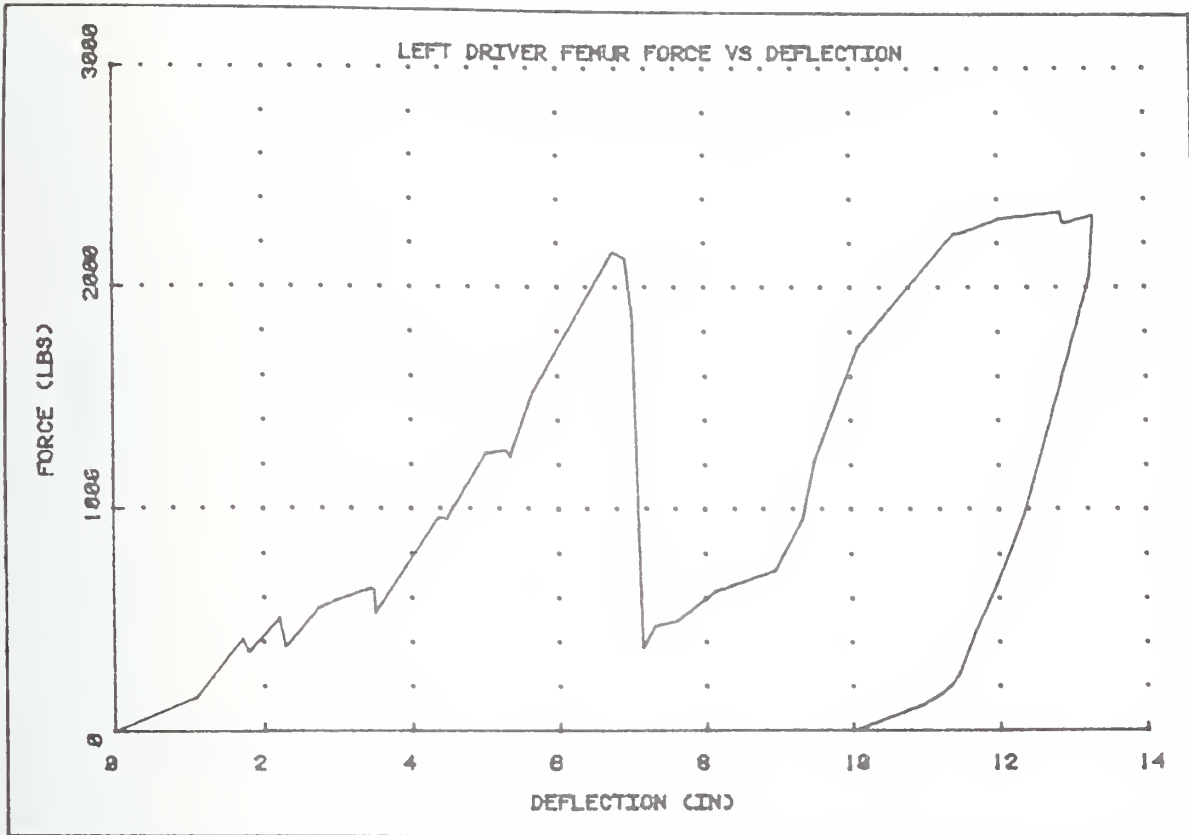
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Left Driver Femur Date: January 24, 1985

Vehicle: \_\_\_\_\_

Options: \_\_\_\_\_



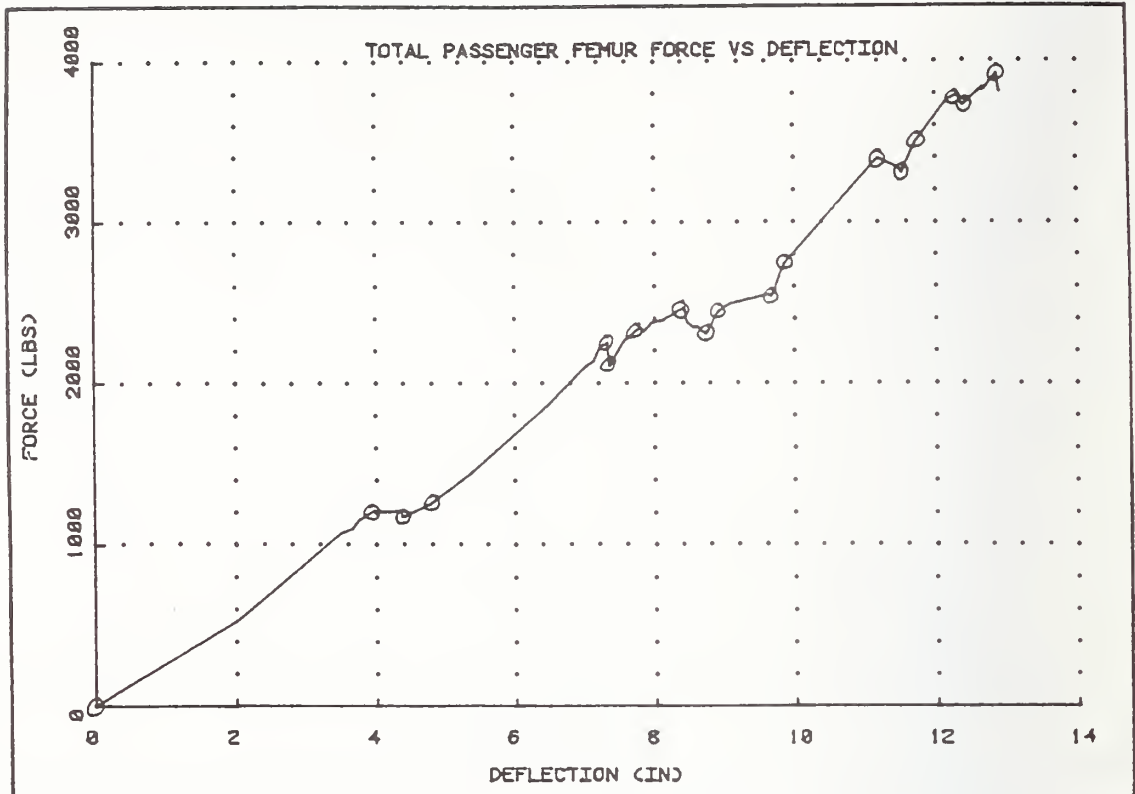
G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Passenger Femur Date: January 28, 1985  
 Vehicle: 1979 Chrysler Cordoba  
 Options: \_\_\_\_\_

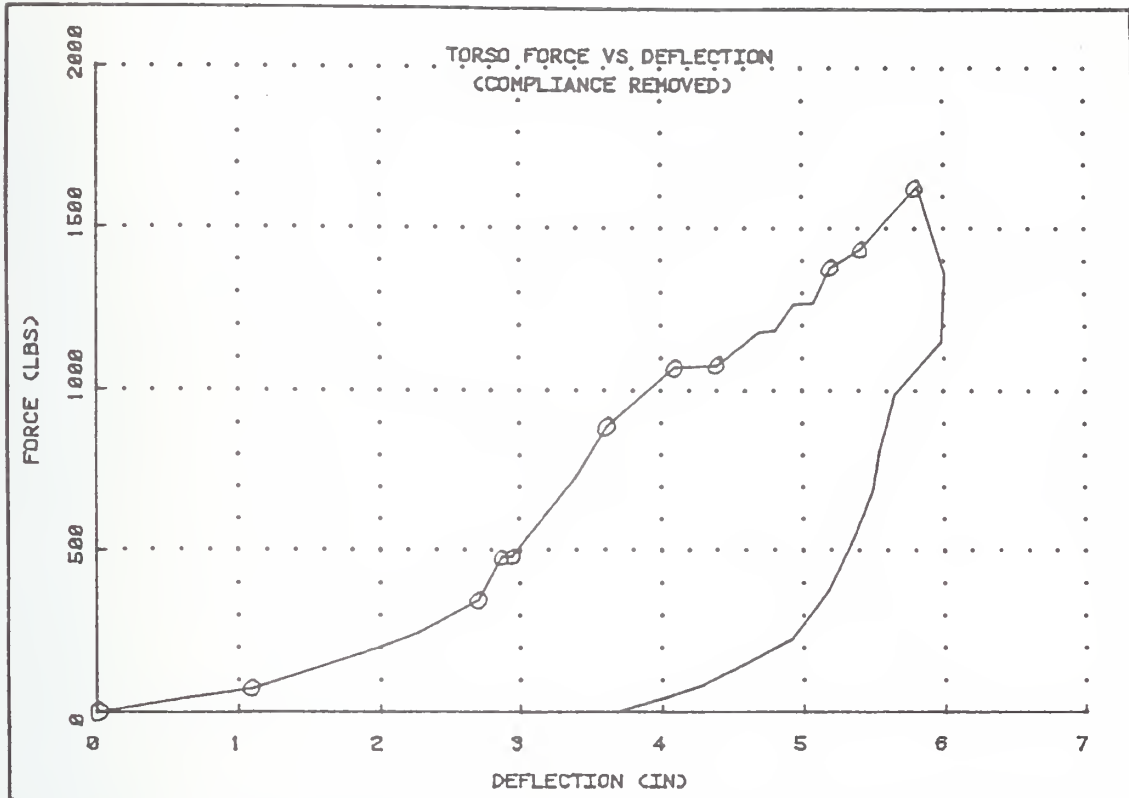


G= 0.784 R= 0.104 K= 2806  
 c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_  
 $\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

Deflection	Force	Deflection	Force
<u>0.0</u>	<u>0.0</u>	<u>8.91</u>	<u>2438.3</u>
<u>3.96</u>	<u>1209.7</u>	<u>9.67</u>	<u>2532.2</u>
<u>4.38</u>	<u>1170.9</u>	<u>9.85</u>	<u>2739.5</u>
<u>4.80</u>	<u>1256.2</u>	<u>11.21</u>	<u>3393.6</u>
<u>7.33</u>	<u>2244.0</u>	<u>11.54</u>	<u>3303.1</u>
<u>7.35</u>	<u>2097.5</u>	<u>11.73</u>	<u>3489.6</u>
<u>7.80</u>	<u>2341.1</u>	<u>12.32</u>	<u>3789.9</u>
<u>8.43</u>	<u>2470.0</u>	<u>12.40</u>	<u>3719.8</u>
<u>8.75</u>	<u>2297.1</u>	<u>12.87</u>	<u>3922.1</u>

Intermediate Unloads	Maximum Deflection	G	R	K
First	4.07	0.708	0.223	1316
Second	8.09	0.669	0.185	1649

Test: Torso Date: January 28, 1985  
 Vehicle: 1979 Chrysler Cordoba  
 Options: \_\_\_\_\_



G= 0.614 R= .0226 K= 1056  
 C= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_  
 $\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

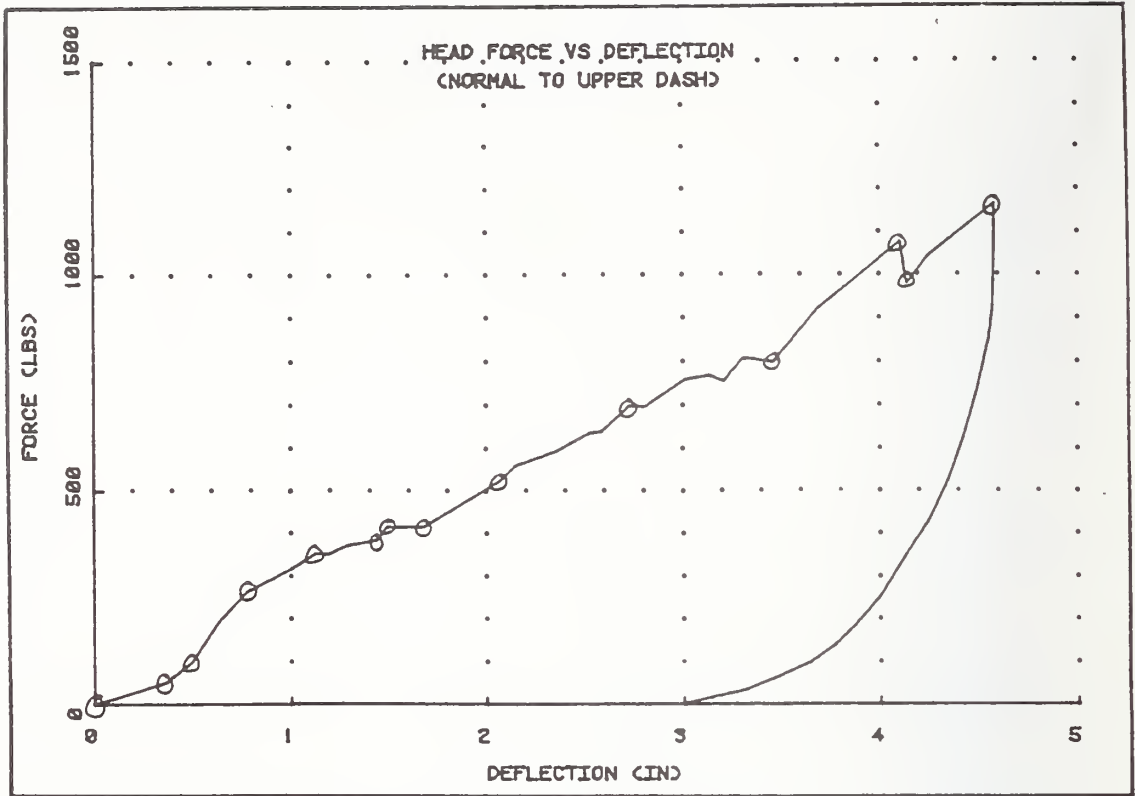
Deflection	Force	Deflection	Force
0.0	0.0	5.2	1378.1
1.10	73.2	5.42	1438.6
2.71	349.3	5.82	1630.4
2.88	481.8		
2.95	481.2		
3.62	891.8		
4.10	1071.7		
4.40	1076.6		

Intermediate Unloads	Maximum Deflection	G R K		
		G	R	K
First	2.27	0.629	0.325	424.
Second	3.43	0.662	0.230	1194.

Test: Head Date: January 28, 1985

Vehicle: 1979 Chrysler Cordoba

Options: \_\_\_\_\_



G= 0.656 R= 0.144 K= 1775

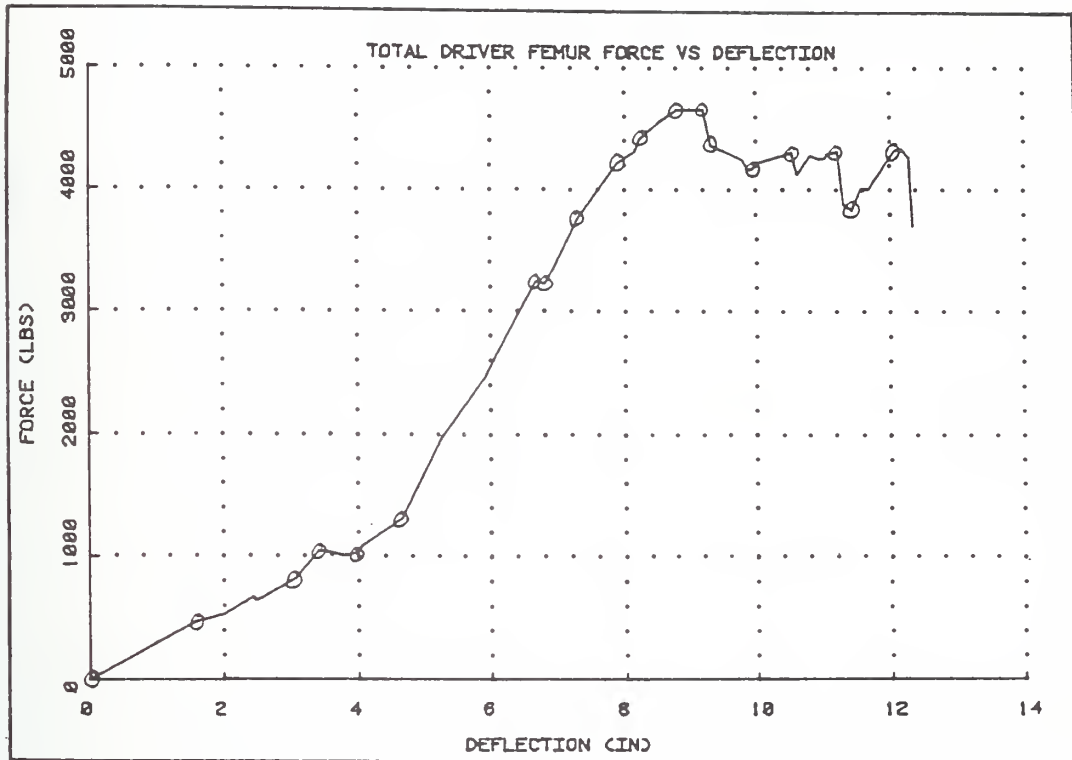
c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

Deflection	Force	Deflection	Force
<u>0.0</u>	<u>0.0</u>	<u>2.07</u>	<u>524.8</u>
<u>0.37</u>	<u>150.2</u>	<u>2.73</u>	<u>698.5</u>
<u>0.50</u>	<u>99.7</u>	<u>3.46</u>	<u>794.8</u>
<u>0.78</u>	<u>262.3</u>	<u>4.11</u>	<u>1076.4</u>
<u>1.12</u>	<u>354.1</u>	<u>4.15</u>	<u>976.3</u>
<u>1.44</u>	<u>385.7</u>	<u>4.58</u>	<u>1164.2</u>
<u>1.49</u>	<u>415.0</u>		
<u>1.67</u>	<u>412.9</u>		

Intermediate Unloads	Maximum Deflection	G	R	K
First	1.29	0.526	0.298	995
Second	2.59	0.510	0.226	1011

Test: Driver Femur Date: January 28, 1985  
 Vehicle: 1979 Chrysler Cordoba  
 Options: \_\_\_\_\_



G= 0.825 R= 0.083 K= 2493.

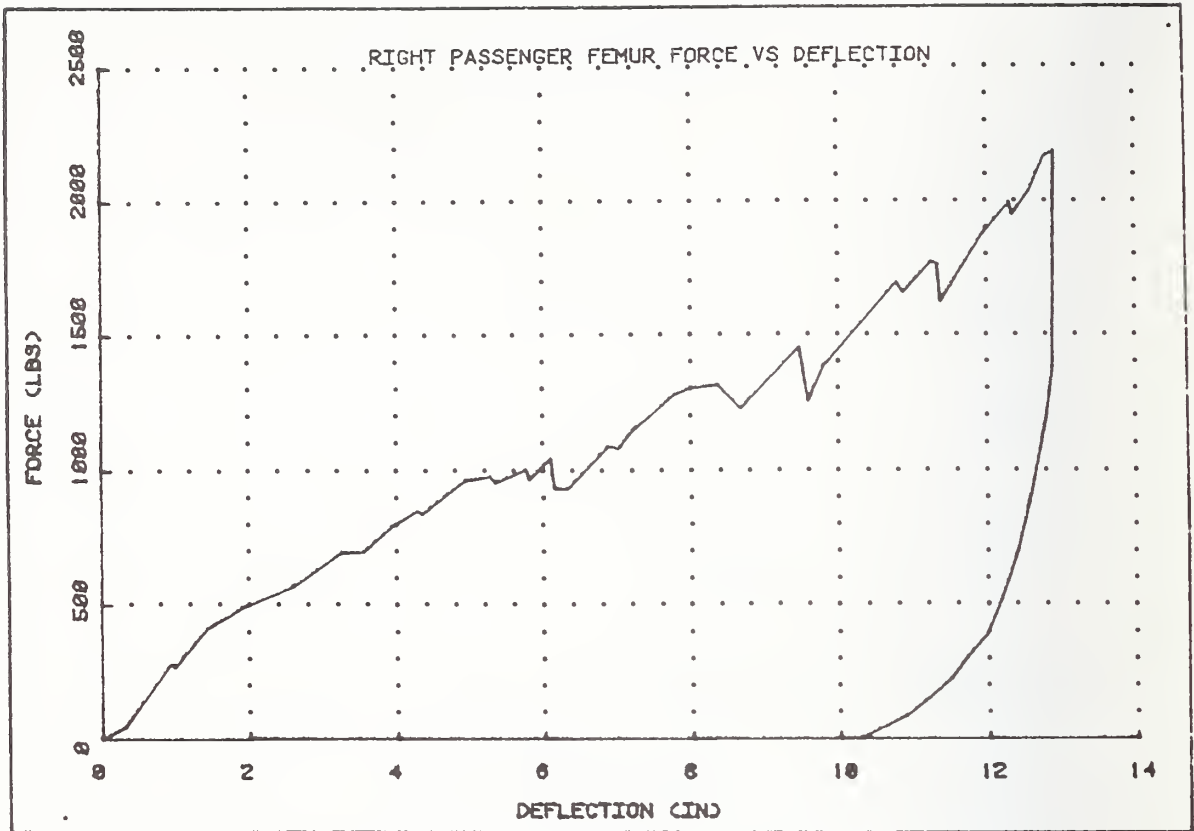
c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

Deflection	Force	Deflection	Force
0.0	0.0	9.21	4659.7
1.58	470.9	9.32	4359.7
3.07	819.0	9.93	4166.5
3.42	1050.3	10.55	4305.0
4.00	1031.4	11.23	4311.7
4.66	1313.0	11.43	3827.0
6.67	3245.4	12.08	4329.6
6.79	3220.9		
7.29	3759.9		
7.89	4216.9		
8.24	4416.7		
8.81	4658.9		

Intermediate Unloads	Maximum Deflection	G	R	K
First	3.45	0.443	0.308	1103.
Second	7.31	0.521	0.269	2576.

Test: Right Passenger Femur Date: January 28, 1985  
 Vehicle: 1979 Chrysler Cordoba  
 Options: \_\_\_\_\_



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_  
 C= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_  
 $\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

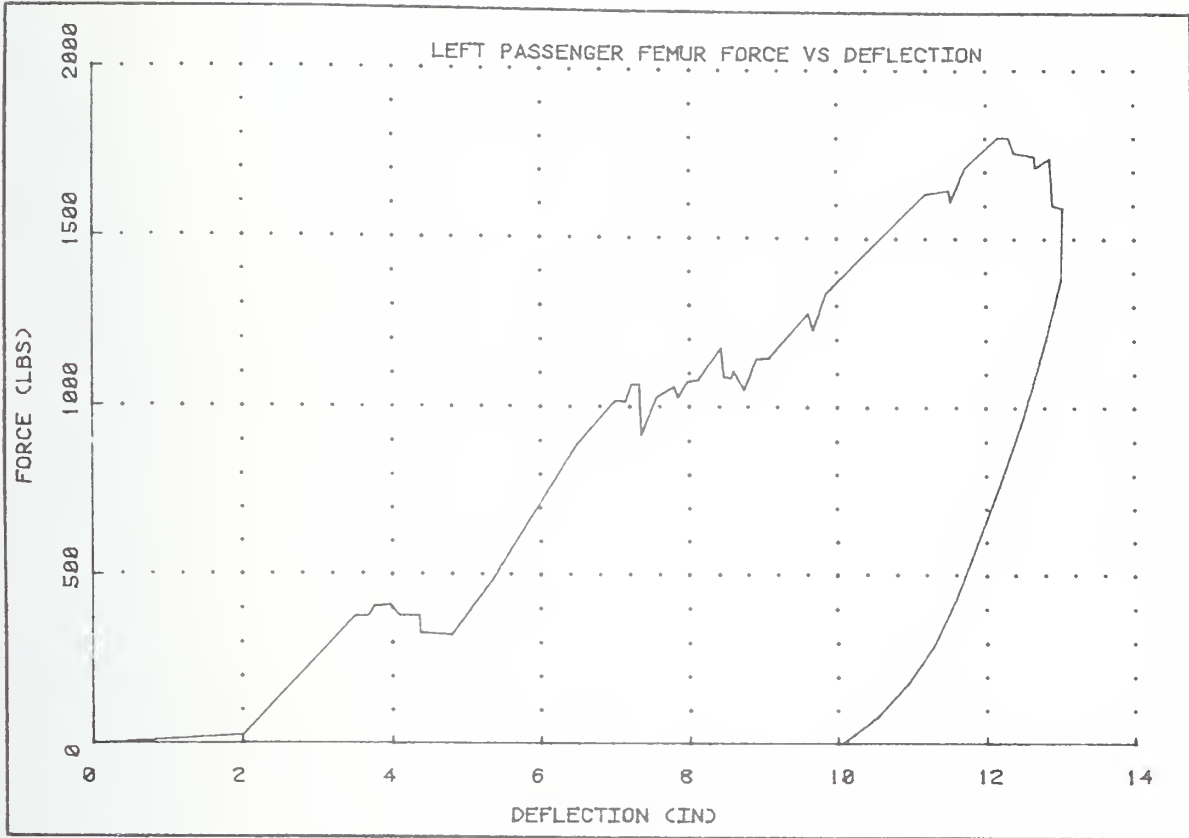
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____



Test: Left Passenger Femur Date: January 28, 1985

Vehicle: 1979 Chrysler Cordoba

Options: \_\_\_\_\_  
\_\_\_\_\_



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

C= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

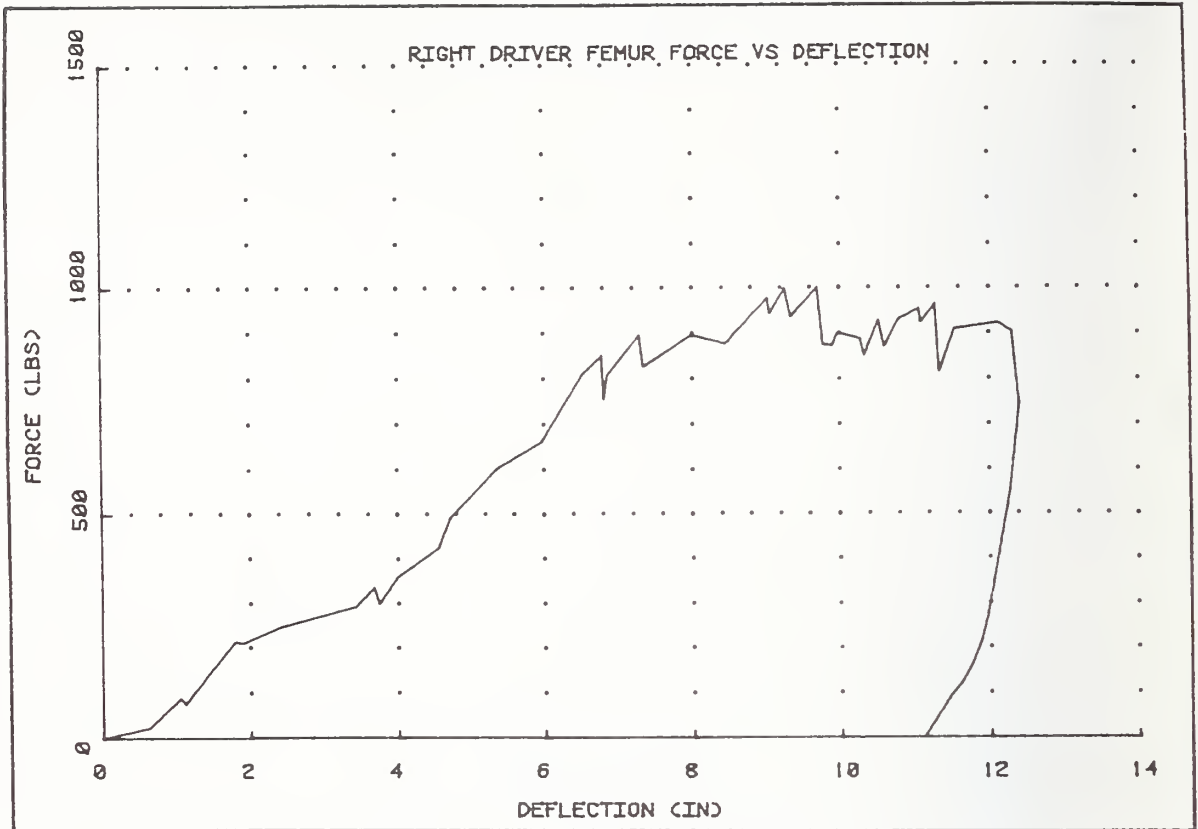
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Right Driver Femur Date: January 28, 1985

Vehicle: 1979 Chrysler Cordoba

Options: \_\_\_\_\_  
\_\_\_\_\_



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

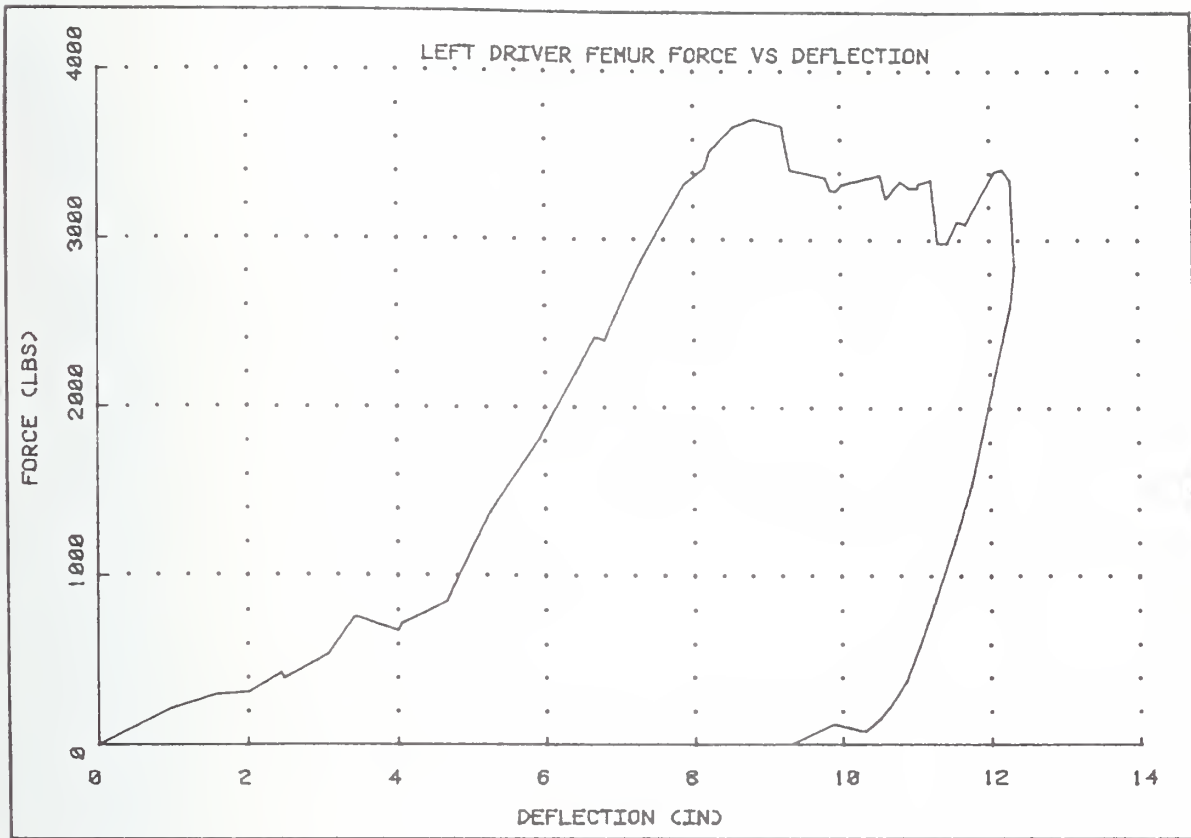
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Left Driver Femur Date: January 28, 1985

Vehicle: 1979 Chrysler Cordoba

Options: \_\_\_\_\_



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

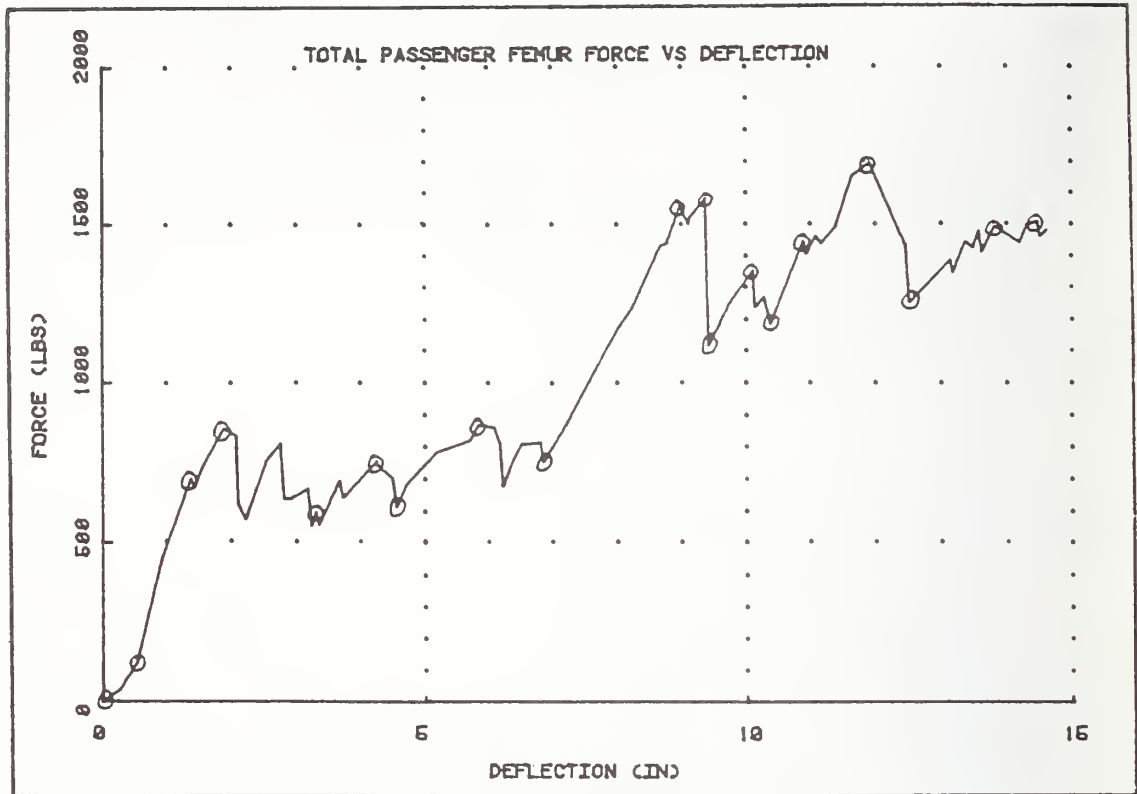
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Passenger Side Femur

Date: January 30, 1985

Vehicle: Buick LeSabre

Options: \_\_\_\_\_



G= 0.776 R= 0.043 K= 1728

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_E$ = 1000.1

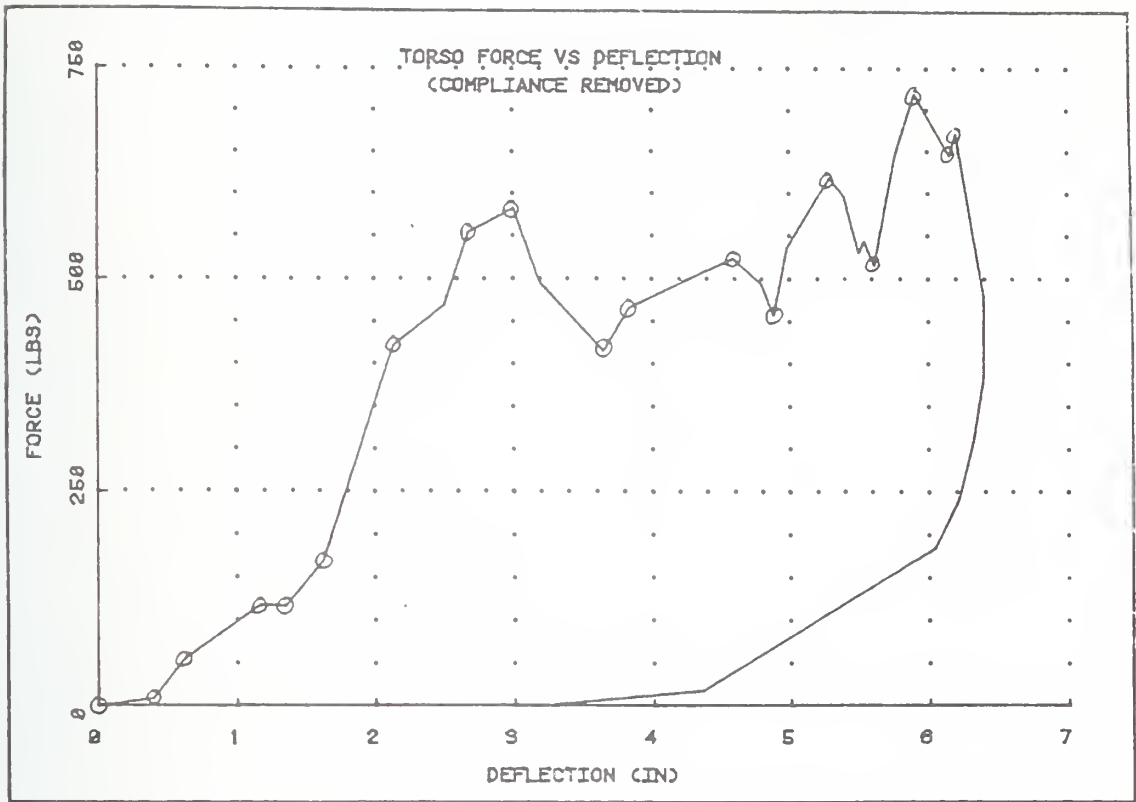
Deflection	Force	Deflection	Force
<u>0.0</u>	<u>0.0</u>	<u>9.38</u>	<u>1580.0</u>
<u>0.54</u>	<u>123.9</u>	<u>9.42</u>	<u>1112.2</u>
<u>1.37</u>	<u>700.5</u>	<u>10.11</u>	<u>1352.5</u>
<u>1.88</u>	<u>855.7</u>	<u>10.39</u>	<u>1183.2</u>
<u>3.31</u>	<u>595.7</u>	<u>10.89</u>	<u>1445.7</u>
<u>4.25</u>	<u>755.7</u>	<u>11.92</u>	<u>1692.3</u>
<u>4.56</u>	<u>610.5</u>	<u>12.52</u>	<u>1247.8</u>
<u>5.84</u>	<u>867.2</u>	<u>13.82</u>	<u>1489.9</u>
<u>6.85</u>	<u>752.8</u>	<u>14.48</u>	<u>1508.7</u>
<u>8.99</u>	<u>1558.3</u>		

Intermediate Unloads	Maximum Deflection	G	R	K
First	3.95	0.515	0.194	543
Second	8.03	0.670	0.140	910

Test: Torso Date: January 30, 1985

Vehicle: Buick LeSabre

Options: \_\_\_\_\_



G= 0.514 R= .0107 K= 427

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

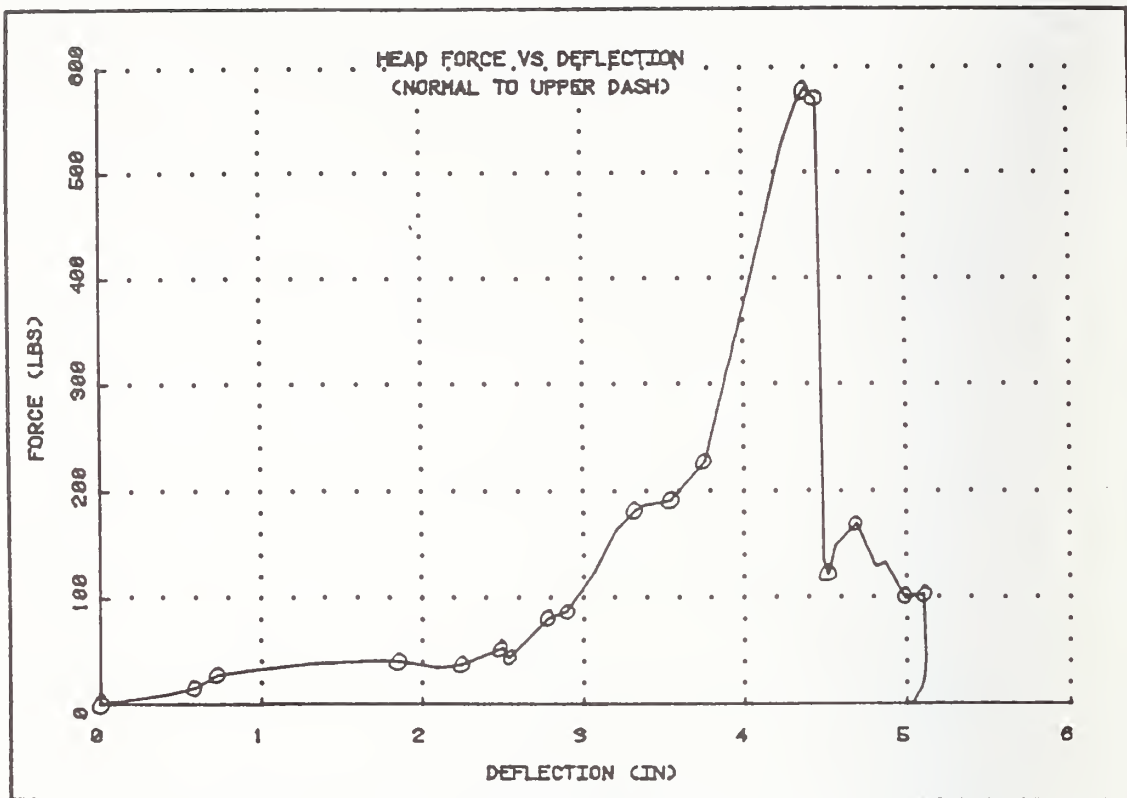
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

Deflection	Force	Deflection	Force	
<u>0.0</u>	<u>0.0</u>	<u>3.64</u>	<u>413.7</u>	
<u>0.41</u>	<u>8.9</u>	<u>3.84</u>	<u>466.2</u>	
<u>0.63</u>	<u>55.5</u>	<u>4.59</u>	<u>523.0</u>	
<u>1.16</u>	<u>117.8</u>	<u>4.88</u>	<u>456.6</u>	
<u>1.34</u>	<u>115.2</u>	<u>5.30</u>	<u>618.7</u>	
<u>1.63</u>	<u>169.9</u>	<u>5.62</u>	<u>514.3</u>	
<u>2.14</u>	<u>421.3</u>	<u>5.92</u>	<u>719.2</u>	
<u>2.68</u>	<u>554.7</u>	<u>6.16</u>	<u>644.7</u>	
<u>3.01</u>	<u>582.5</u>	<u>6.20</u>	<u>671.8</u>	
Intermediate Unload	Maximum Deflection	G	R	K
First	2.38	0.535	0.351	759
Second	4.37	0.437	0.228	426

Test: Head Date: January 30, 1985

Vehicle: Buick LeSabre

Options: \_\_\_\_\_



G= 0.984 R= 0.002 K= 906

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

Deflection	Force	Deflection	Force
0.0	0.0	3.33	182.5
0.59	15.9	3.55	191.1
0.74	28.3	3.76	227.1
1.87	39.5	4.40	580.6
2.24	38.1	4.47	569.7
2.50	53.1	4.52	120.7
2.54	44.1	4.70	169.0
2.79	81.6	4.99	100.6
2.90	87.7	5.11	103.3

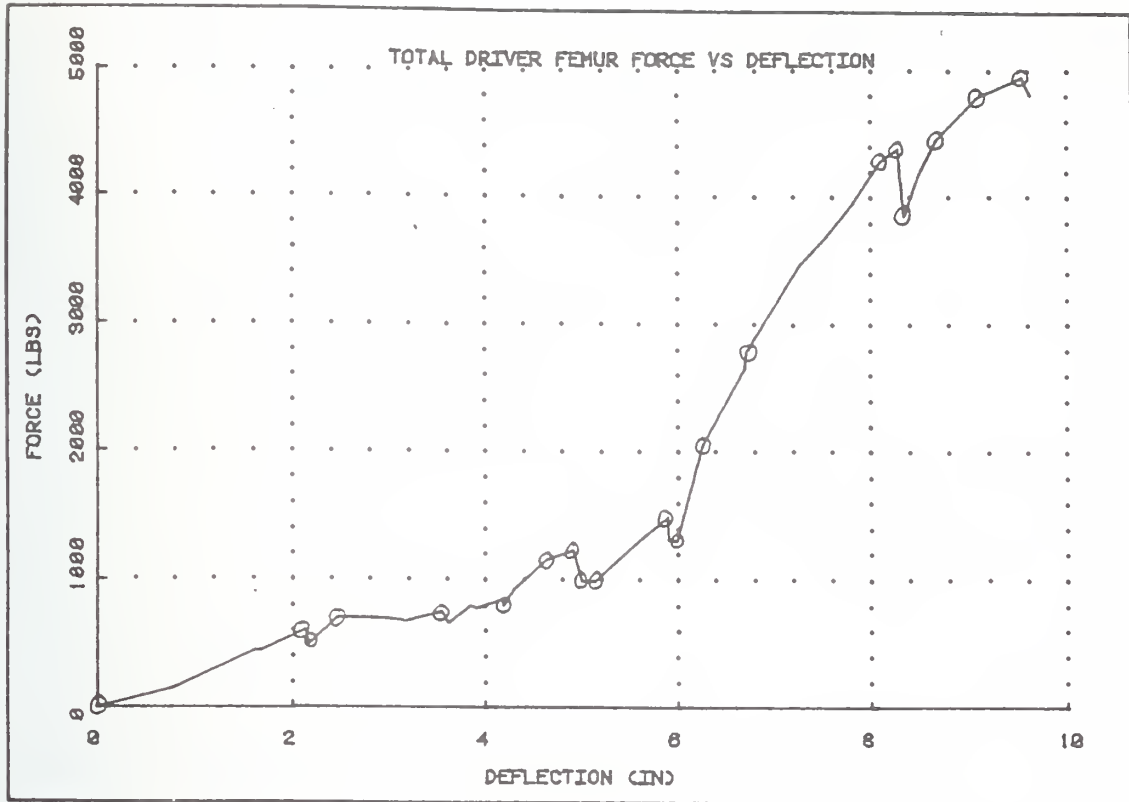
Intermediate Unloads	Maximum Deflection	G	R	K
First	2.89	0.883	0.081	318
Second	4.03	0.857	0.178	1302

Test: Driver Side Femur

Date: January 30, 1985

Vehicle: Buick LeSaber

Options: \_\_\_\_\_



G= 0.728                      R= 0.215                      K= 3042

c= \_\_\_\_\_                       $\mu_1$ = \_\_\_\_\_                       $\mu_2$ = \_\_\_\_\_                       $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0                       $\delta_B$ = 0.0                       $\delta_C$ = 0.0                       $\delta_D$ = 1000.0                       $\delta_F$ = 1000.1

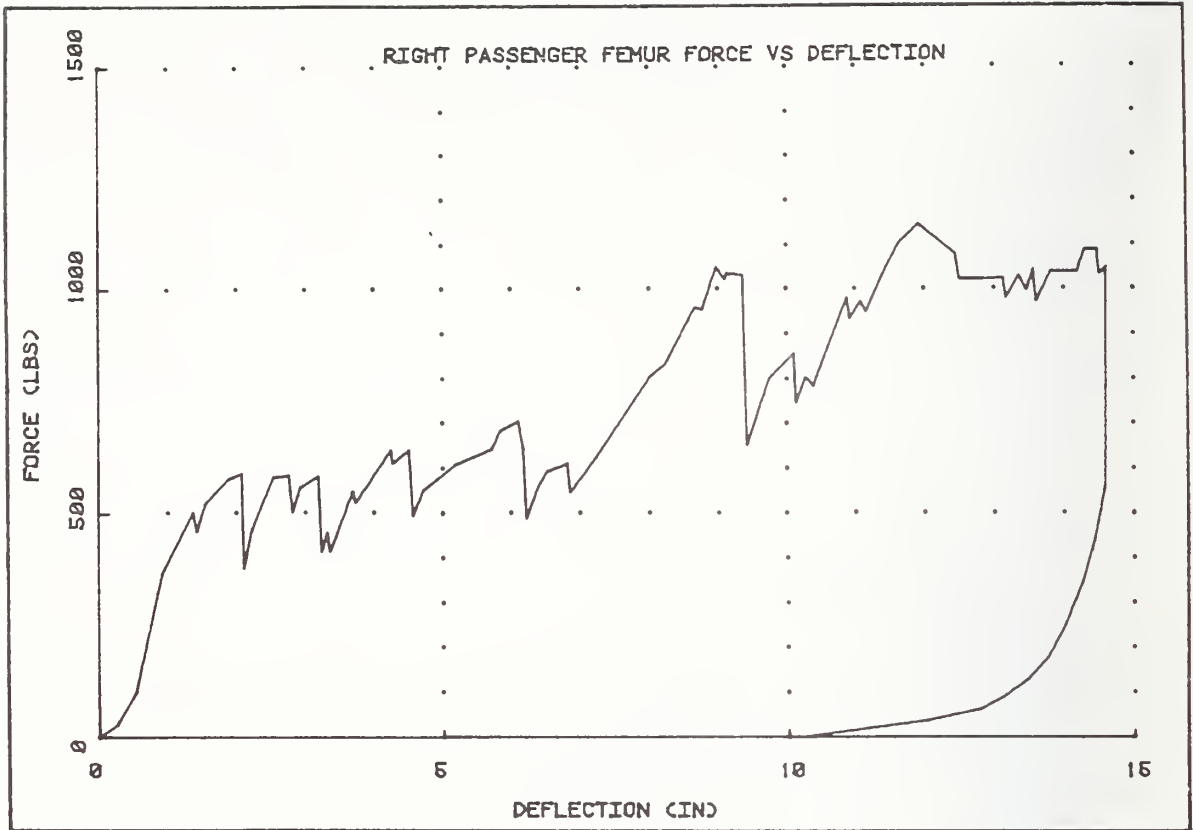
Deflection	Force	Deflection	Force
<u>0.0</u>	<u>0.0</u>	<u>5.89</u>	<u>1487.4</u>
<u>2.13</u>	<u>608.3</u>	<u>5.99</u>	<u>1298.7</u>
<u>2.17</u>	<u>493.6</u>	<u>6.27</u>	<u>2049.8</u>
<u>2.46</u>	<u>705.5</u>	<u>6.71</u>	<u>2783.7</u>
<u>3.54</u>	<u>751.0</u>	<u>8.10</u>	<u>4283.3</u>
<u>4.19</u>	<u>796.0</u>	<u>8.28</u>	<u>4386.6</u>
<u>4.64</u>	<u>1155.4</u>	<u>8.35</u>	<u>3853.4</u>
<u>4.91</u>	<u>1230.5</u>	<u>8.67</u>	<u>4454.4</u>
<u>5.00</u>	<u>981.7</u>	<u>9.09</u>	<u>4795.0</u>
<u>5.13</u>	<u>991.3</u>	<u>9.54</u>	<u>4951.4</u>

Intermediate Unloads	Maximum Deflection	G	R	K
First	4.96	0.548	0.179	985
Second	7.51	0.713	0.275	2998

Test: Right Passenger Femur Date: January 30, 1985

Vehicle: Buick LeSabre

Options: \_\_\_\_\_



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

C= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

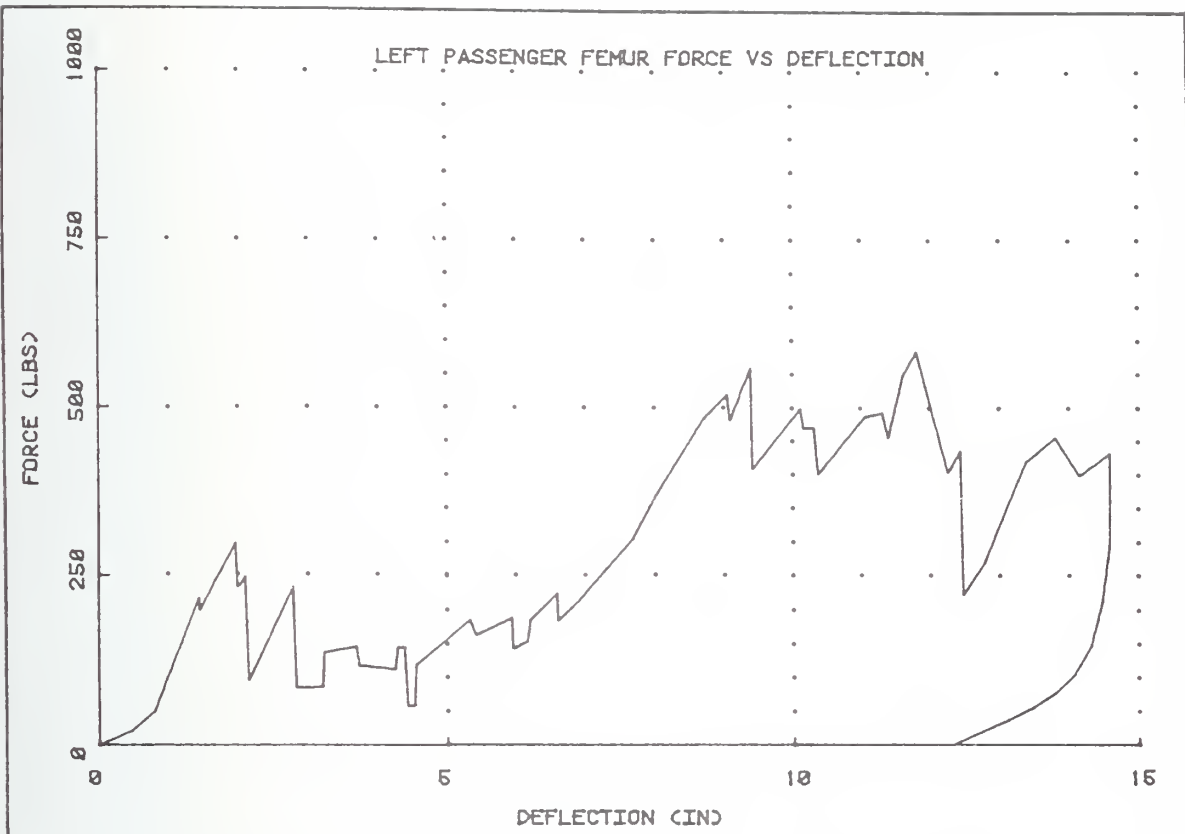
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____



Test: Left Passenger Femur Date: January 30, 1985

Vehicle: Buick LeSabre

Options: \_\_\_\_\_  
\_\_\_\_\_



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

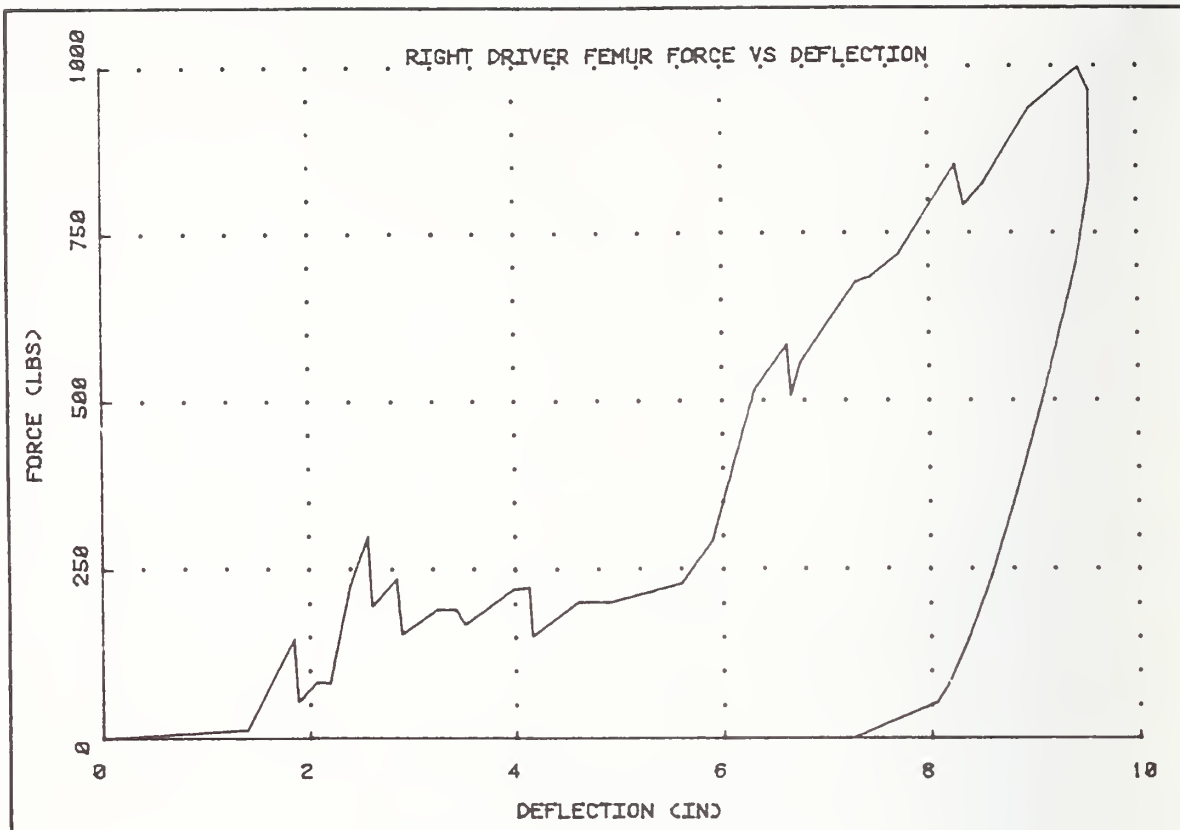
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Right Driver Femur Date: January 30, 1985

Vehicle: Buick LeSabre

Options: \_\_\_\_\_



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

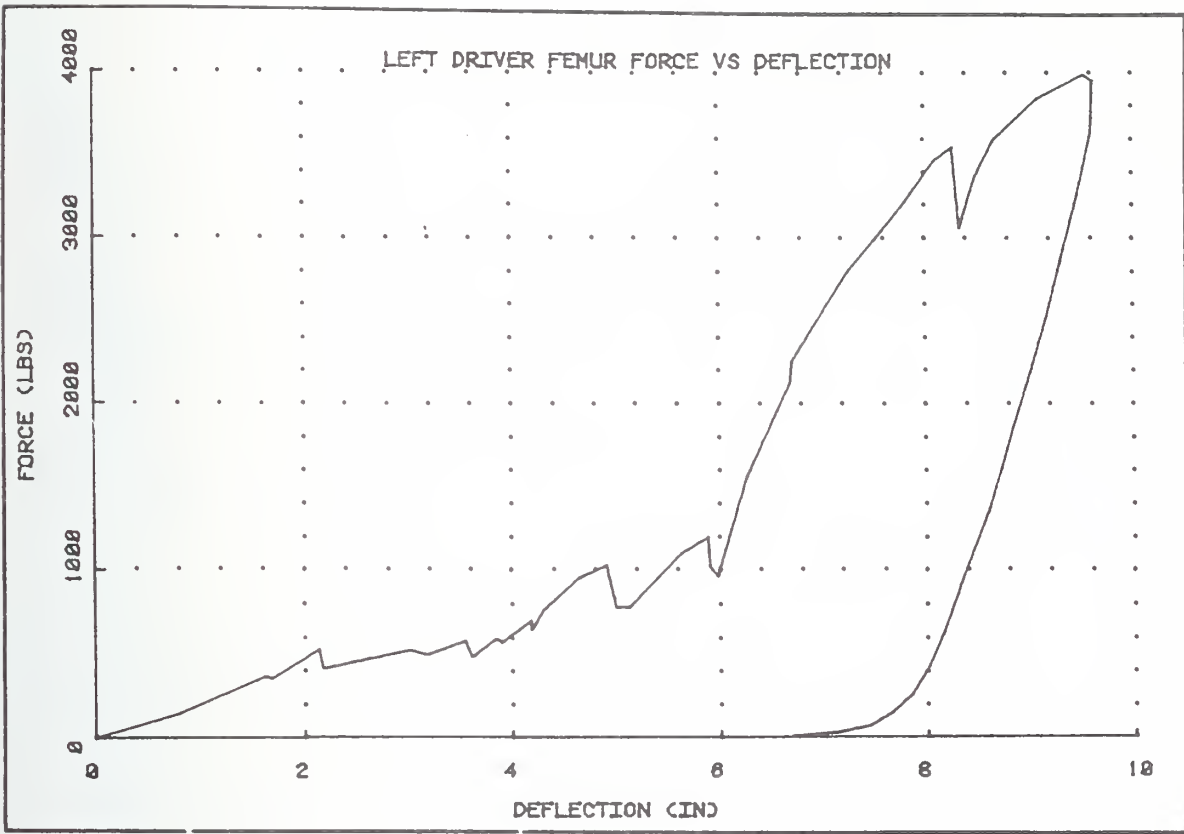
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Left Driver Femur Date: January 30, 1985

Vehicle: Buick LeSabre

Options: \_\_\_\_\_  
\_\_\_\_\_



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

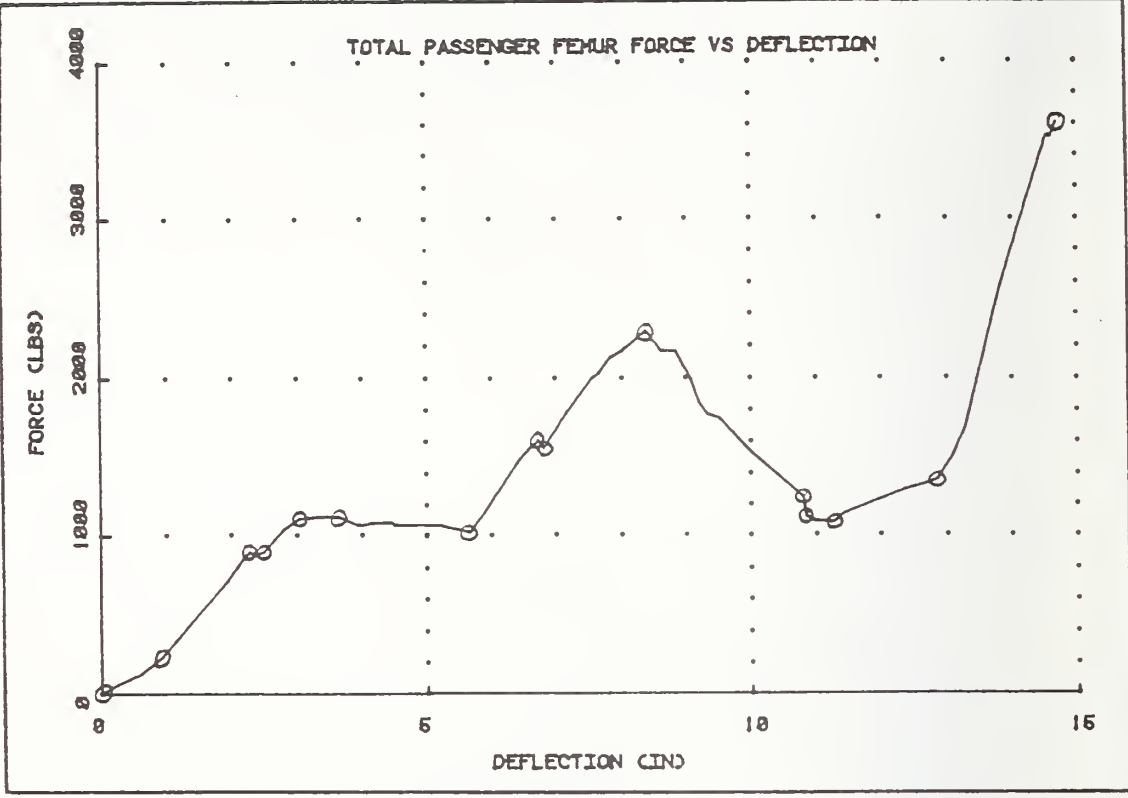
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.0

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Passenger Side Femur Date: February 12, 1985

Vehicle: V W Rabbit

Options: \_\_\_\_\_



G= 0.884 R= 0.074 K= 4414.

C= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

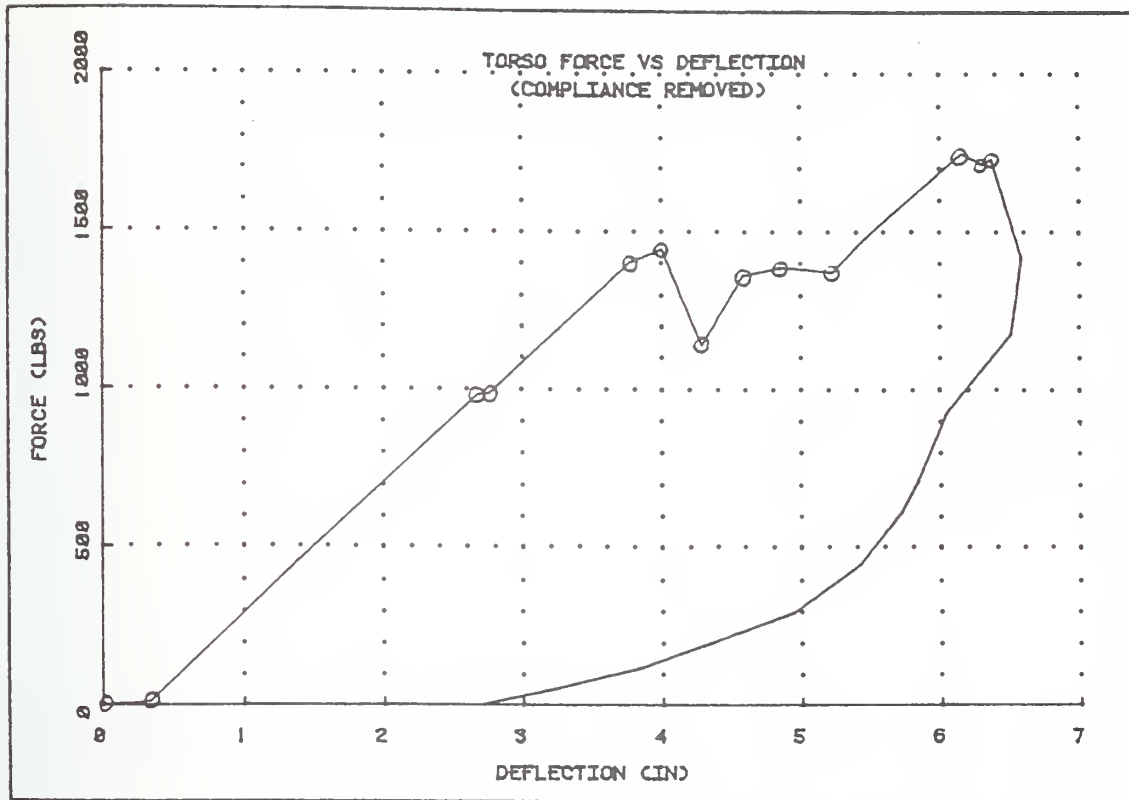
Deflection	Force	Deflection	Force
<u>0.0</u>	<u>0.0</u>	<u>6.82</u>	<u>1555.4</u>
<u>0.94</u>	<u>232.6</u>	<u>8.38</u>	<u>2287.4</u>
<u>2.29</u>	<u>895.8</u>	<u>10.81</u>	<u>1234.4</u>
<u>2.50</u>	<u>906.2</u>	<u>10.84</u>	<u>1114.3</u>
<u>3.03</u>	<u>1113.9</u>	<u>11.25</u>	<u>1080.9</u>
<u>3.64</u>	<u>1120.6</u>	<u>12.87</u>	<u>1357.3</u>
<u>5.66</u>	<u>1017.9</u>	<u>14.71</u>	<u>3608.4</u>
<u>6.74</u>	<u>1607.6</u>		

Intermediate Unloadings	Maximum Deflection	G	R	K
First	3.09	0.483	0.311	1174.
Second	6.12	0.699	0.119	1259.

Test: Torso Date: February 12, 1985

Vehicle: V W Rabbit

Options: \_\_\_\_\_



G= 0.411 R= 0.221 K= 694.

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

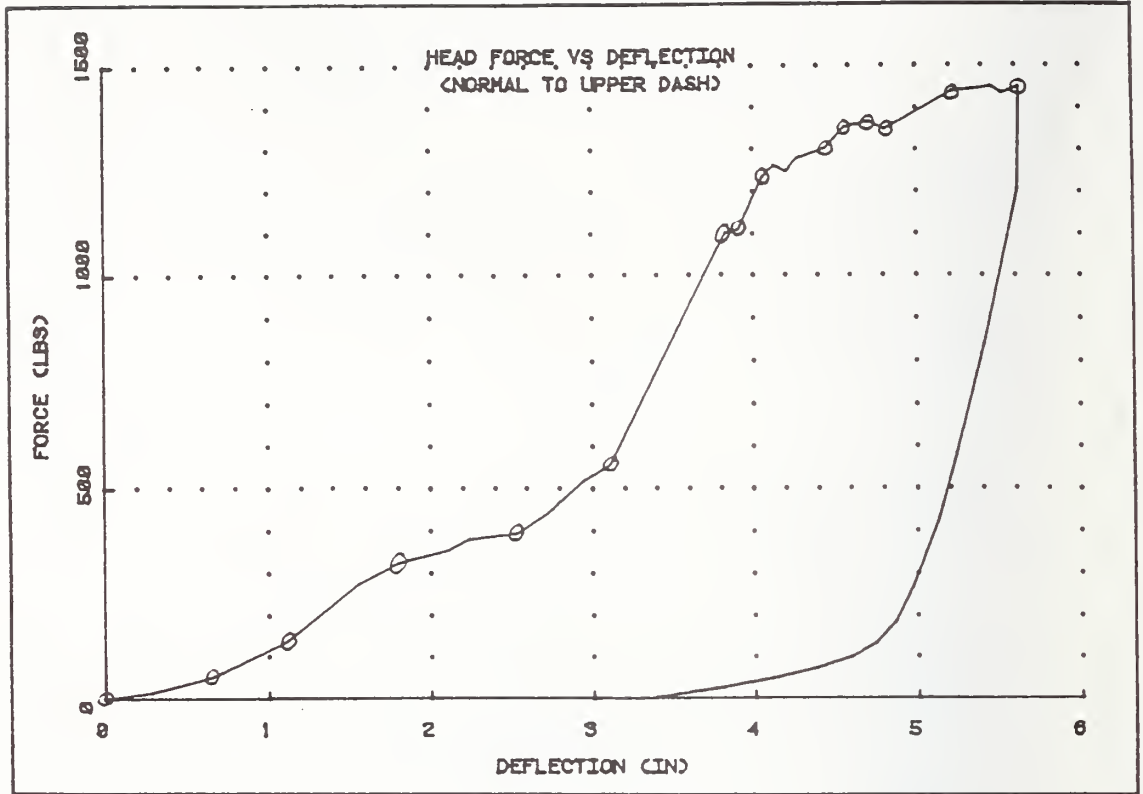
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

Deflection	Force	Deflection	Force
<u>0.0</u>	<u>0.0</u>	<u>4.84</u>	<u>1385.3</u>
<u>0.34</u>	<u>12.6</u>	<u>5.22</u>	<u>1370.1</u>
<u>2.68</u>	<u>982.2</u>	<u>6.15</u>	<u>1746.6</u>
<u>2.77</u>	<u>987.6</u>	<u>6.30</u>	<u>1714.3</u>
<u>3.77</u>	<u>1405.3</u>	<u>6.37</u>	<u>1729.6</u>
<u>4.00</u>	<u>1445.4</u>		
<u>4.29</u>	<u>1137.6</u>		
<u>4.58</u>	<u>1362.1</u>		

Intermediate Unload

Maximum Deflection	G	R	K
<u>3.16</u>	<u>0.300</u>	<u>0.536</u>	<u>635.</u>

Test: Head Date: February 12, 1985  
 Vehicle: V W Rabbit  
 Options: \_\_\_\_\_



G= 0.599 R= 0.152 K= 1832

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

Deflection	Force	Deflection	Force
<u>0.0</u>	<u>0.0</u>	<u>4.06</u>	<u>1232.4</u>
<u>0.66</u>	<u>52.8</u>	<u>4.46</u>	<u>1304.8</u>
<u>1.11</u>	<u>137.4</u>	<u>4.57</u>	<u>1354.5</u>
<u>1.80</u>	<u>323.3</u>	<u>4.71</u>	<u>1366.8</u>
<u>2.54</u>	<u>395.1</u>	<u>4.81</u>	<u>1347.8</u>
<u>3.11</u>	<u>560.1</u>	<u>5.23</u>	<u>1440.4</u>
<u>3.83</u>	<u>1101.1</u>	<u>5.63</u>	<u>1450.8</u>
<u>3.91</u>	<u>1109.7</u>		

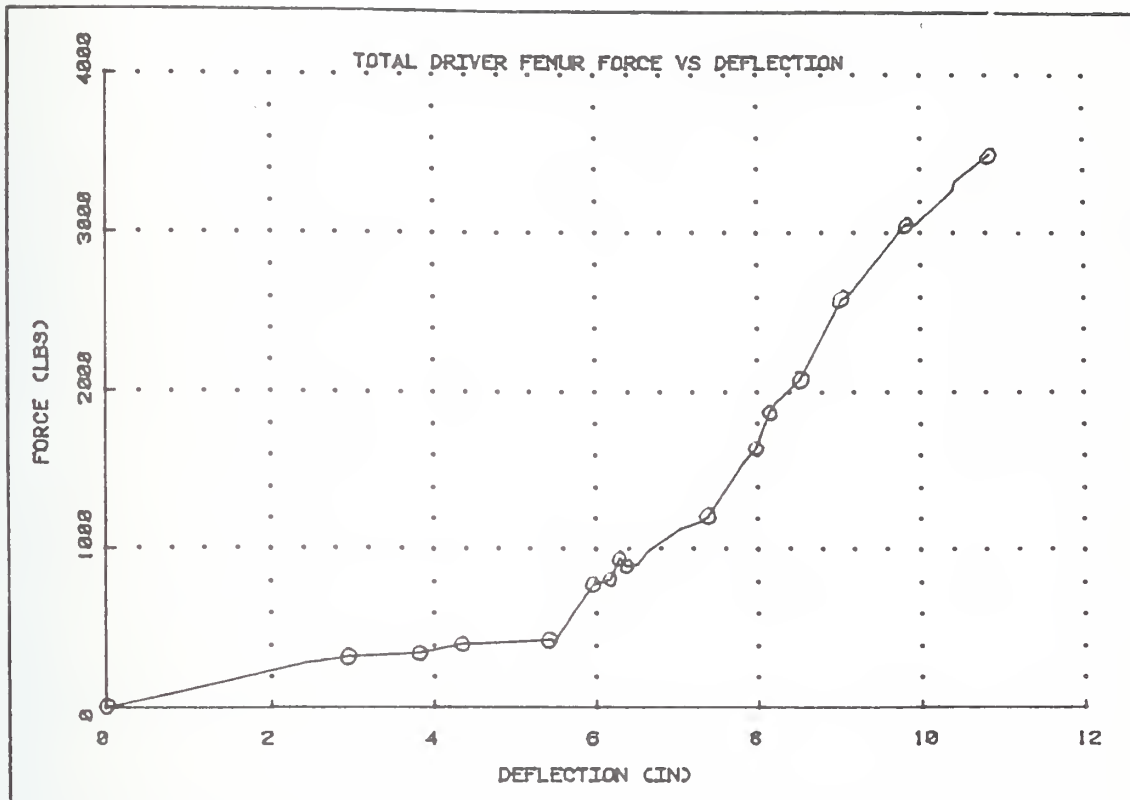
Intermediate Unload

Maximum Deflection	G	R	K
<u>1.88</u>	<u>0.359</u>	<u>0.440</u>	<u>497.</u>

Test: Driver Side Femur Date: February 12, 1985

Vehicle: V W Rabbit

Options: \_\_\_\_\_



G= 0.872 R= 0.106 K= 5075.

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

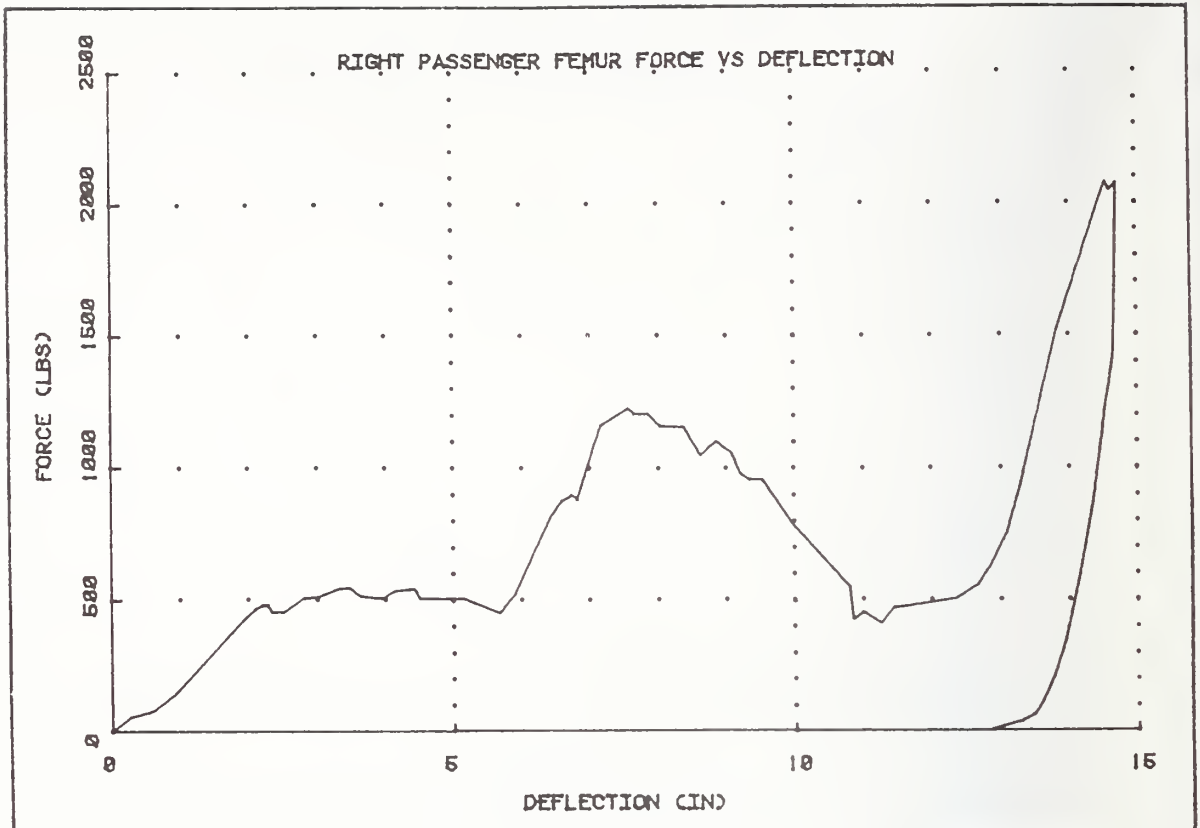
Deflection	Force	Deflection	Force
0.0	0.0	6.37	891.8
2.95	325.0	7.38	1208.7
3.82	350.1	7.98	1646.5
4.34	410.3	8.16	1876.2
5.45	440.6	8.53	2078.0
5.96	780.7	9.05	2588.2
6.18	818.9	9.82	3055.4
6.29	944.6	10.84	3497.0

Intermediate Unloadings	Maximum Deflection	G	R	K
First	4.12	0.794	0.091	805.
Second	8.01	0.846	0.158	2310.

Test: Right Passenger Femur Date: February 12, 1985

Vehicle: V W Rabbit

Options: \_\_\_\_\_



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

C= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

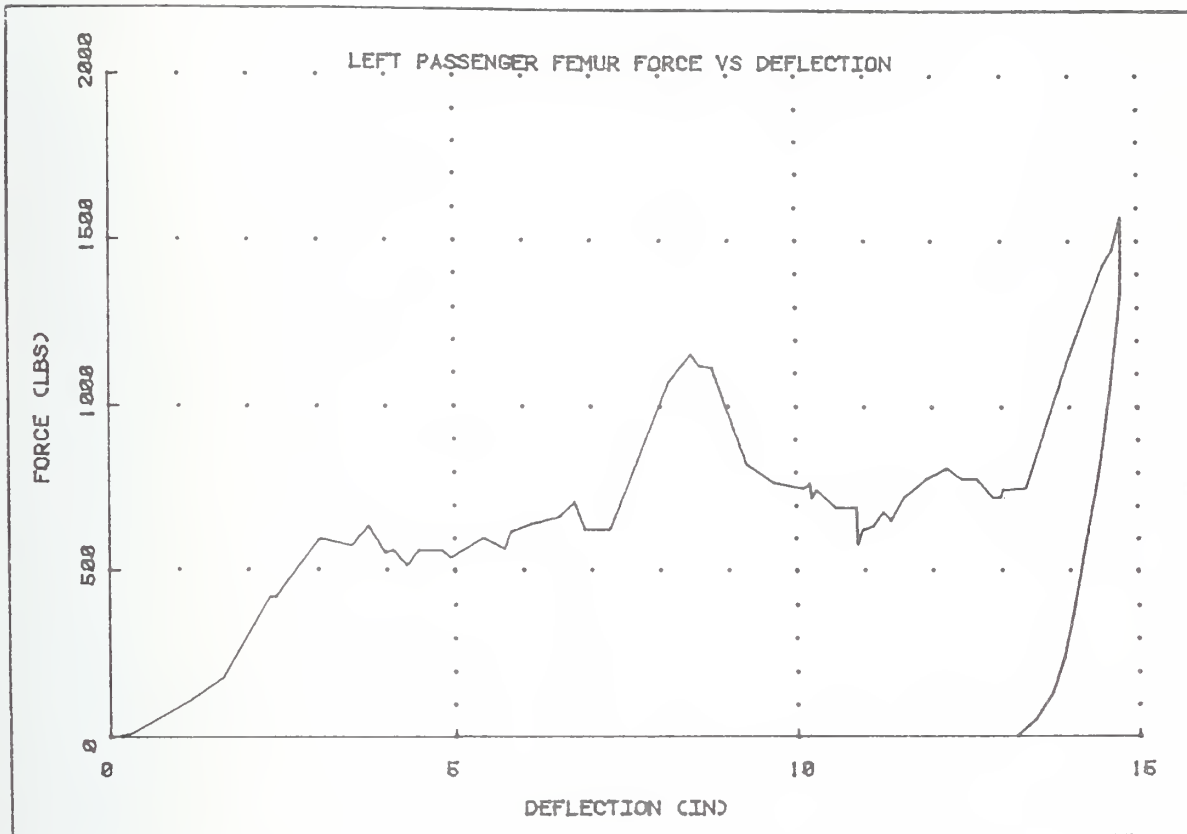


Test: Left Passenger Femur Date: February 12, 1985

Vehicle: V W Rabbit

Operator: \_\_\_\_\_

\_\_\_\_\_



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

C= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

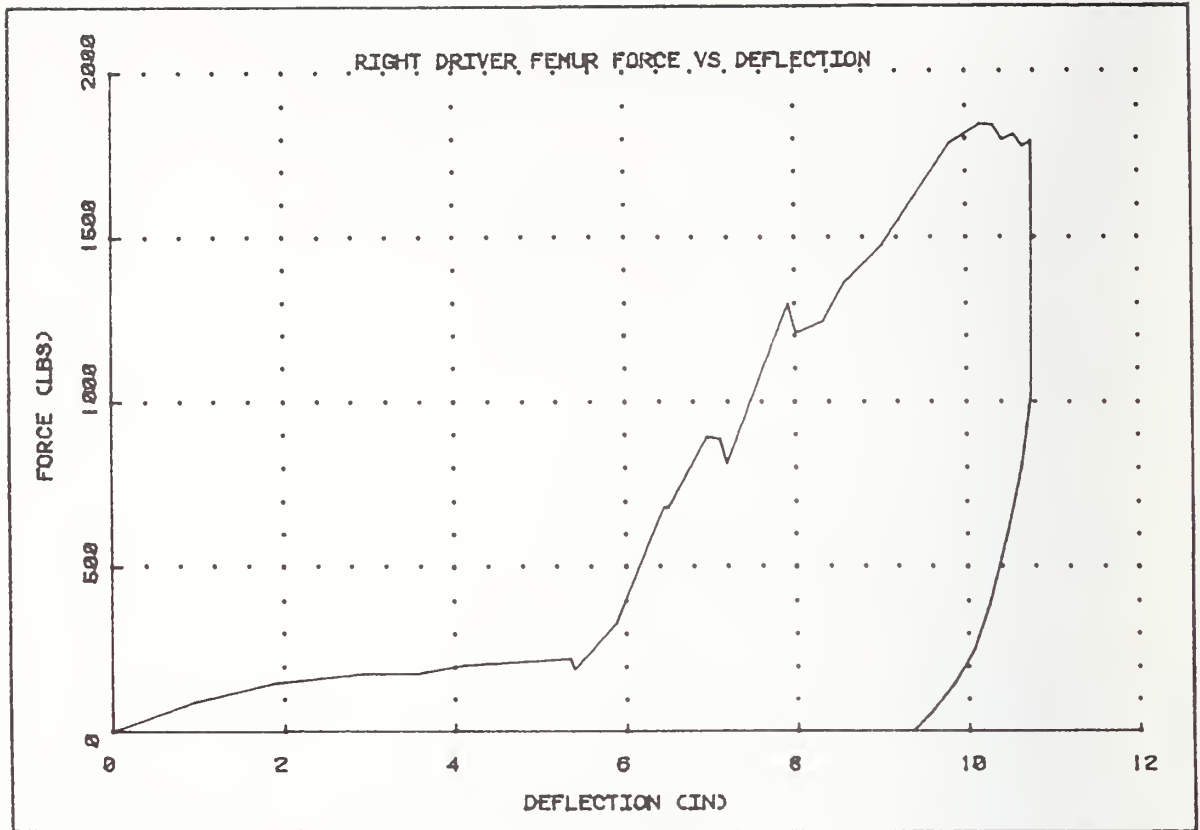
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Right Driver Femur

Date: February 12, 1985

Vehicle: V W Rabbit

Options: \_\_\_\_\_



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

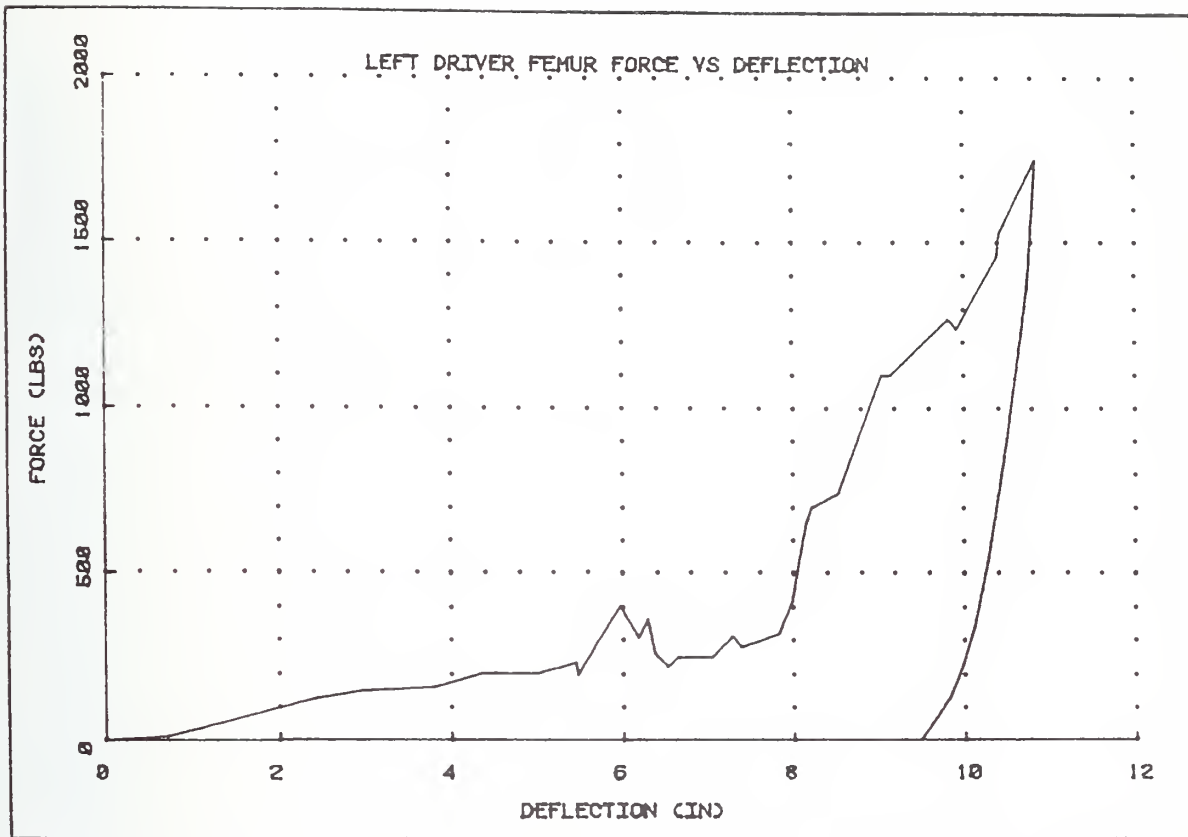
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Left Driver Femur Date: February 12, 1985

Vehicle: V W Rabbit

Options: \_\_\_\_\_



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

C= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

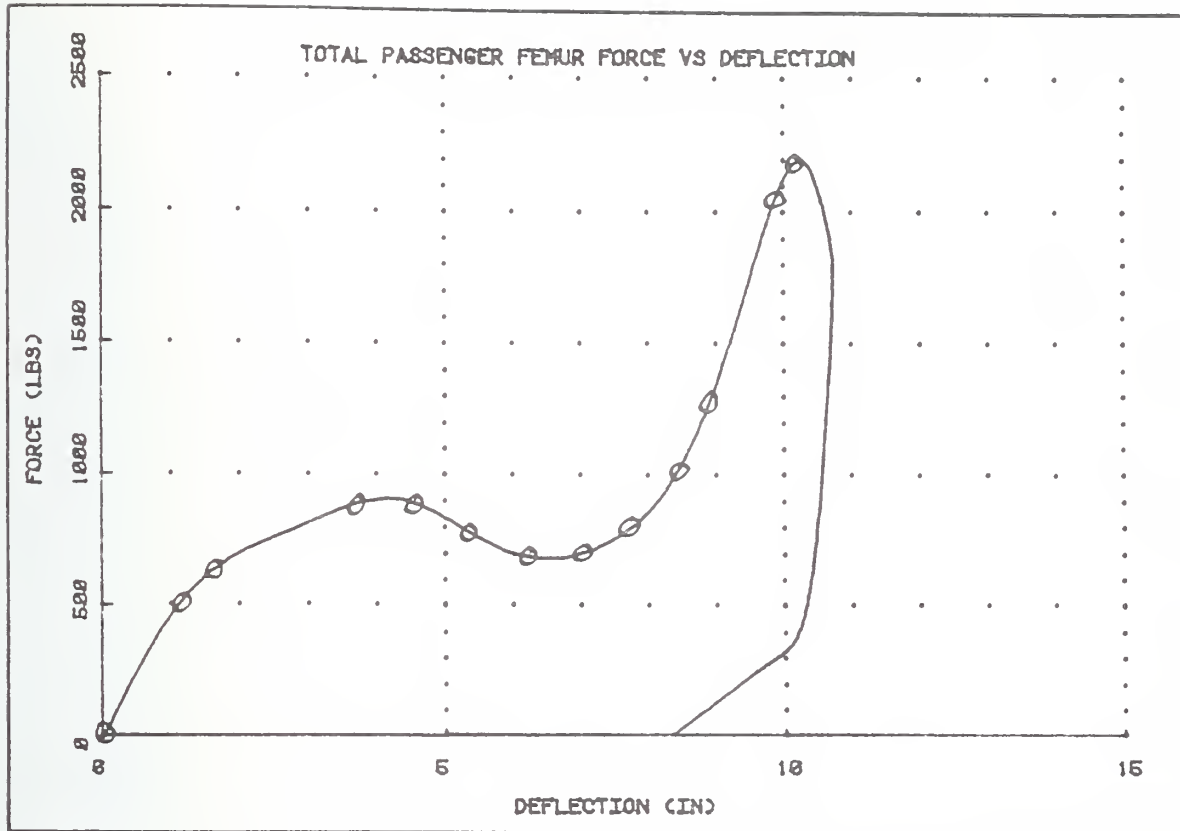


APPENDIX B

DYNAMIC INSTRUMENT PANEL TEST RESULTS



Test: Passenger Side Femur (dynamic) Date: October 4, 1984  
 Vehicle: Chevy Monza  
 Options: No radio, no heater



G= 0.777 R= 0.080 K= 1983.45  
 c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_  
 $\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

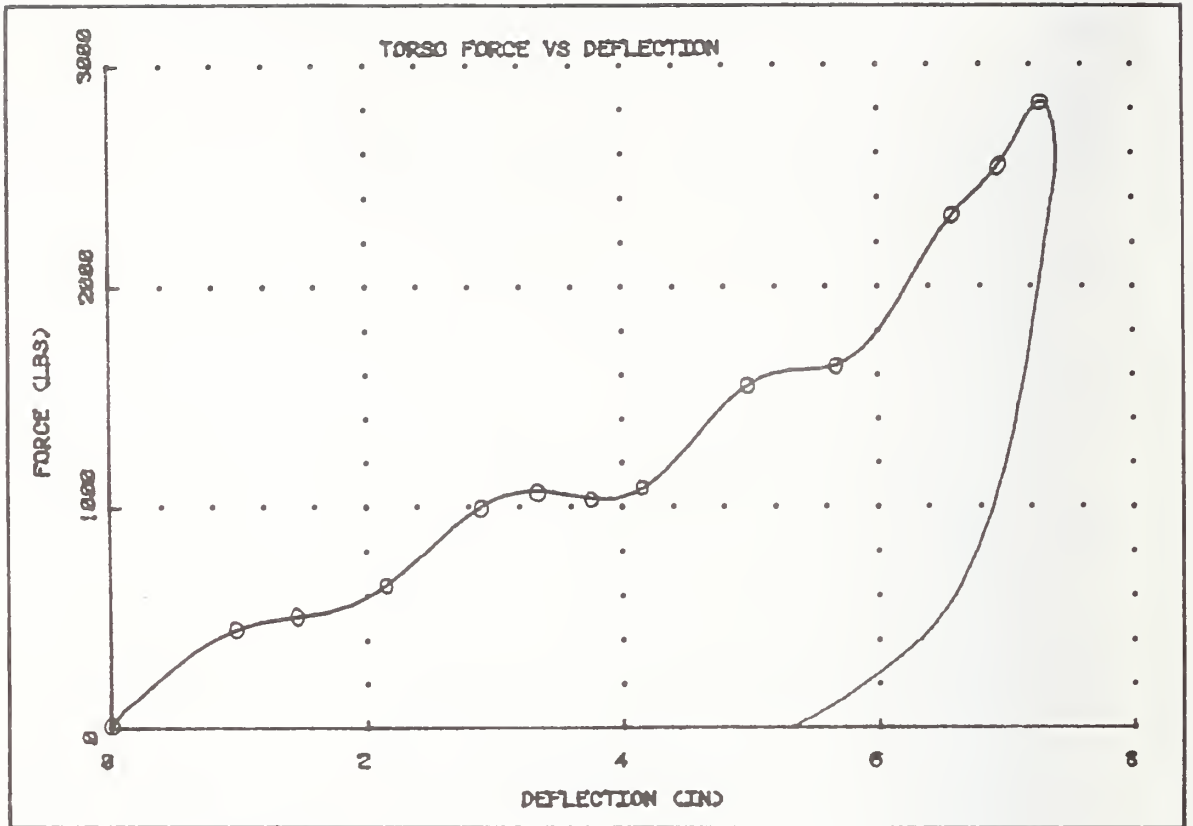
Deflection	Force	Deflection	Force
0.0	0.0	7.84	819.20
1.12	506.88	8.43	1018.88
1.71	645.12	8.88	1259.52
3.88	906.24	9.92	2078.72
4.63	885.76	10.15	2196.48
5.38	783.36		
6.20	680.96		
7.03	701.44		

Filter cutoff frequency: 25 Hz.

Test: Torso (dynamic) Date: October 5, 1984

Vehicle: Chevy Monza

Options: No radio, no heater



G= 0.717 R= 0.158 K= 2357.99

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

Deflection	Force	Deflection	Force
<u>0.0</u>	<u>0.0</u>	<u>4.93</u>	<u>1528.89</u>
<u>0.95</u>	<u>443.26</u>	<u>5.61</u>	<u>1633.51</u>
<u>1.47</u>	<u>506.50</u>	<u>6.65</u>	<u>2363.40</u>
<u>2.19</u>	<u>663.36</u>	<u>6.97</u>	<u>2554.22</u>
<u>2.88</u>	<u>997.94</u>	<u>7.29</u>	<u>2832.41</u>
<u>3.36</u>	<u>1074.51</u>		
<u>3.82</u>	<u>1036.11</u>		
<u>4.17</u>	<u>1092.72</u>		

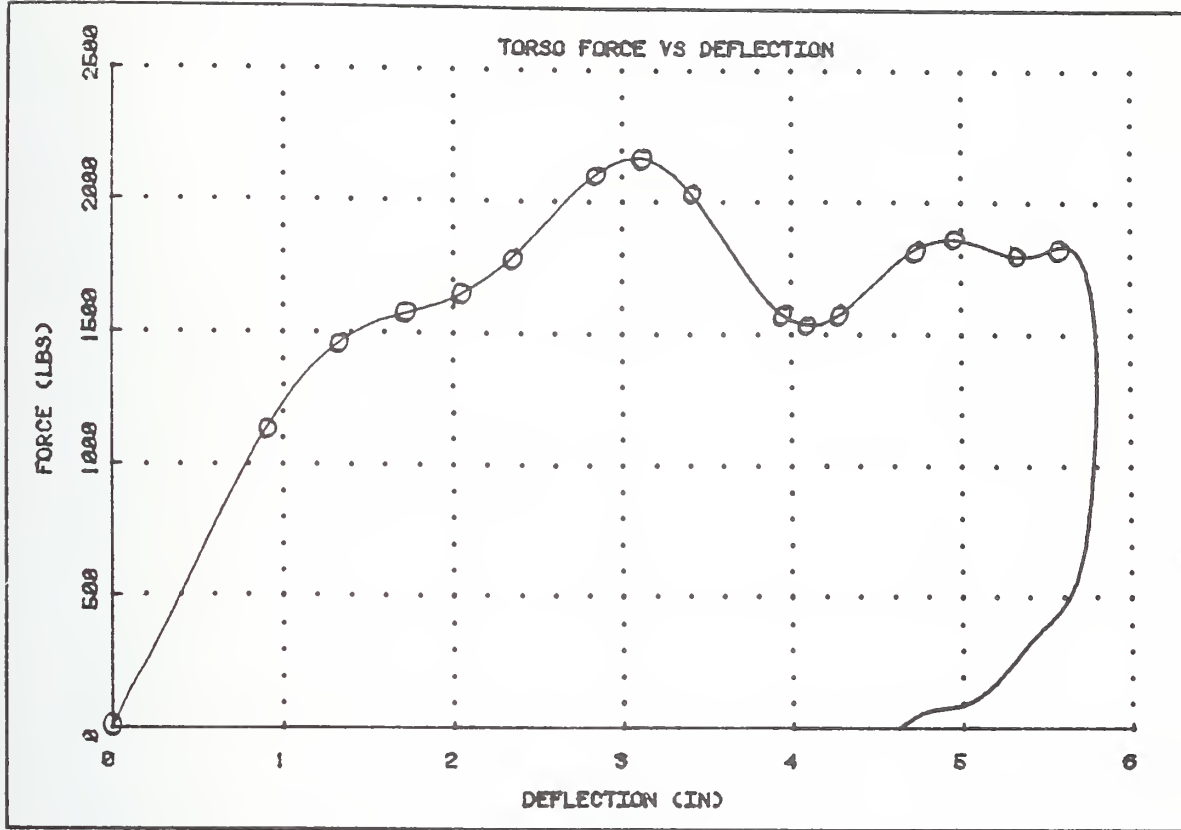
Filter cutoff frequency: 100 Hz.



Test: Torso (dynamic) Date: October 9, 1984

Vehicle: Honda Civic CVCC

Options: No radio



G= 0.797 R= 0.035 K= 2908.47

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

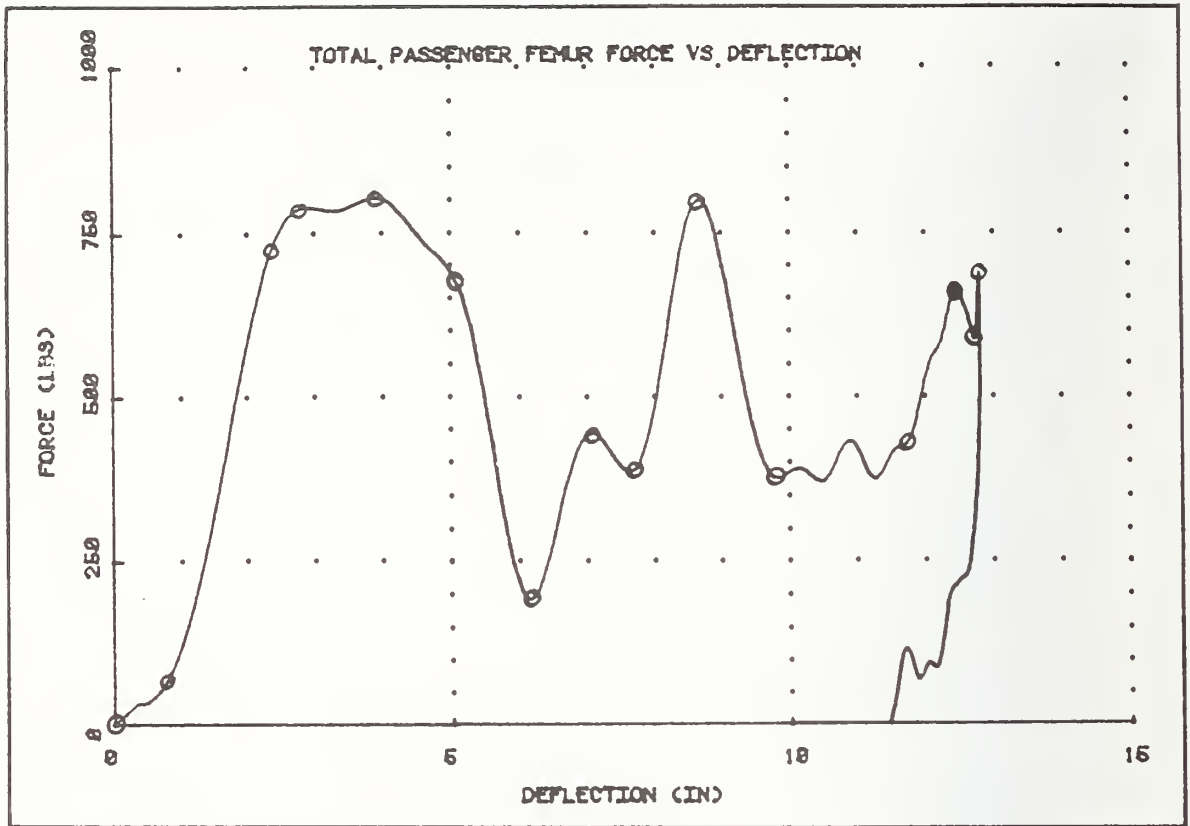
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>3.40</u>	<u>2048.00</u>
<u>0.96</u>	<u>1203.20</u>	<u>3.91</u>	<u>1587.20</u>
<u>1.33</u>	<u>1459.20</u>	<u>4.06</u>	<u>1546.24</u>
<u>1.70</u>	<u>1576.96</u>	<u>4.28</u>	<u>1566.72</u>
<u>2.07</u>	<u>1653.76</u>	<u>4.73</u>	<u>1827.84</u>
<u>2.36</u>	<u>1792.00</u>	<u>4.87</u>	<u>1848.32</u>
<u>2.88</u>	<u>2129.92</u>	<u>5.32</u>	<u>1807.36</u>
<u>3.10</u>	<u>2170.88</u>	<u>5.54</u>	<u>1827.84</u>

Filter cutoff frequency: 100 Hz.

Test: Passenger Side Femur (dynamic) Date: October 10, 1984

Vehicle: Dodge Omni

Options: No radio



G= 0.892 R= -0.033 K= 946.95

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

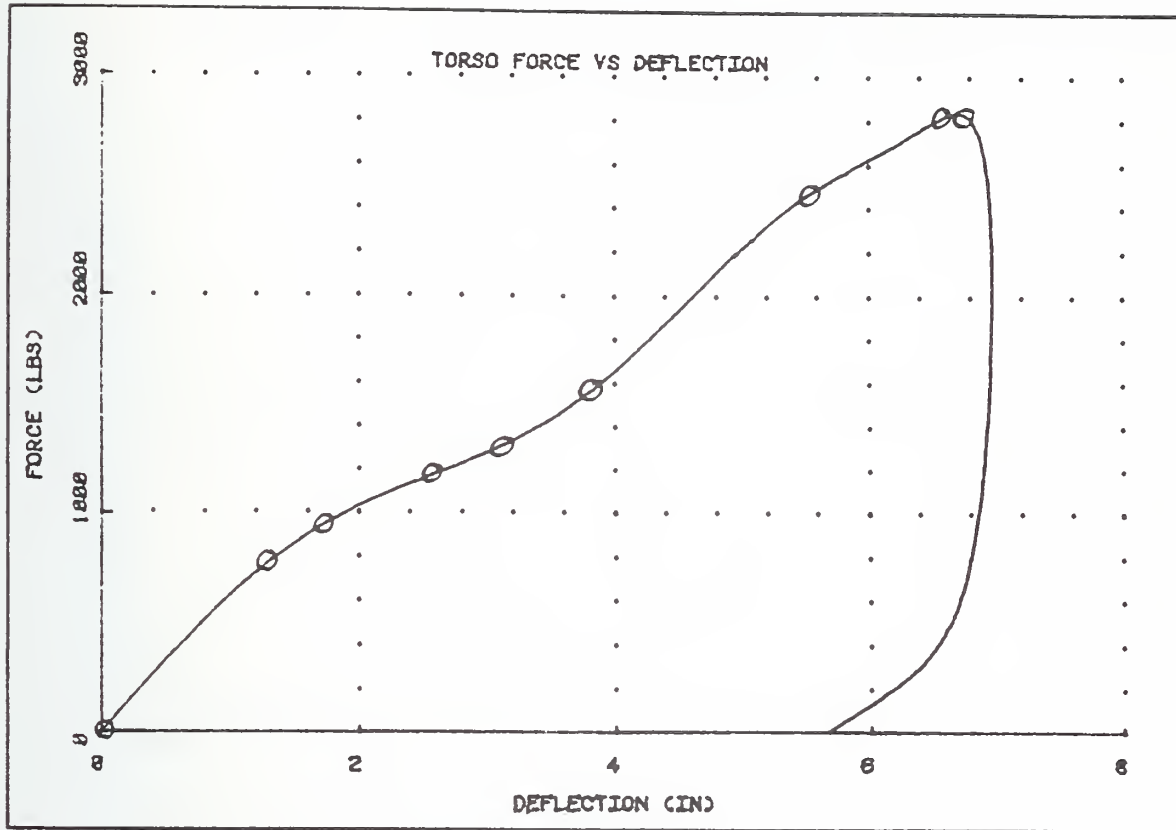
Deflection	Force	Deflection	Force
<u>0.0</u>	<u>0.0</u>	<u>7.61</u>	<u>386.56</u>
<u>0.74</u>	<u>55.04</u>	<u>8.65</u>	<u>796.16</u>
<u>2.38</u>	<u>733.44</u>	<u>9.78</u>	<u>380.16</u>
<u>2.74</u>	<u>783.36</u>	<u>11.73</u>	<u>424.96</u>
<u>3.85</u>	<u>802.56</u>	<u>12.47</u>	<u>664.32</u>
<u>5.05</u>	<u>682.24</u>	<u>12.69</u>	<u>583.68</u>
<u>6.10</u>	<u>192.00</u>	<u>12.76</u>	<u>688.64</u>
<u>7.00</u>	<u>441.60</u>		

Filter cutoff frequency: 100 Hz.

Test: Torso (dynamic) Date: October 10, 1984

Vehicle: Dodge Omni

Options: No radio



G= 0.813 R= 0.047 K= 4296.33

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

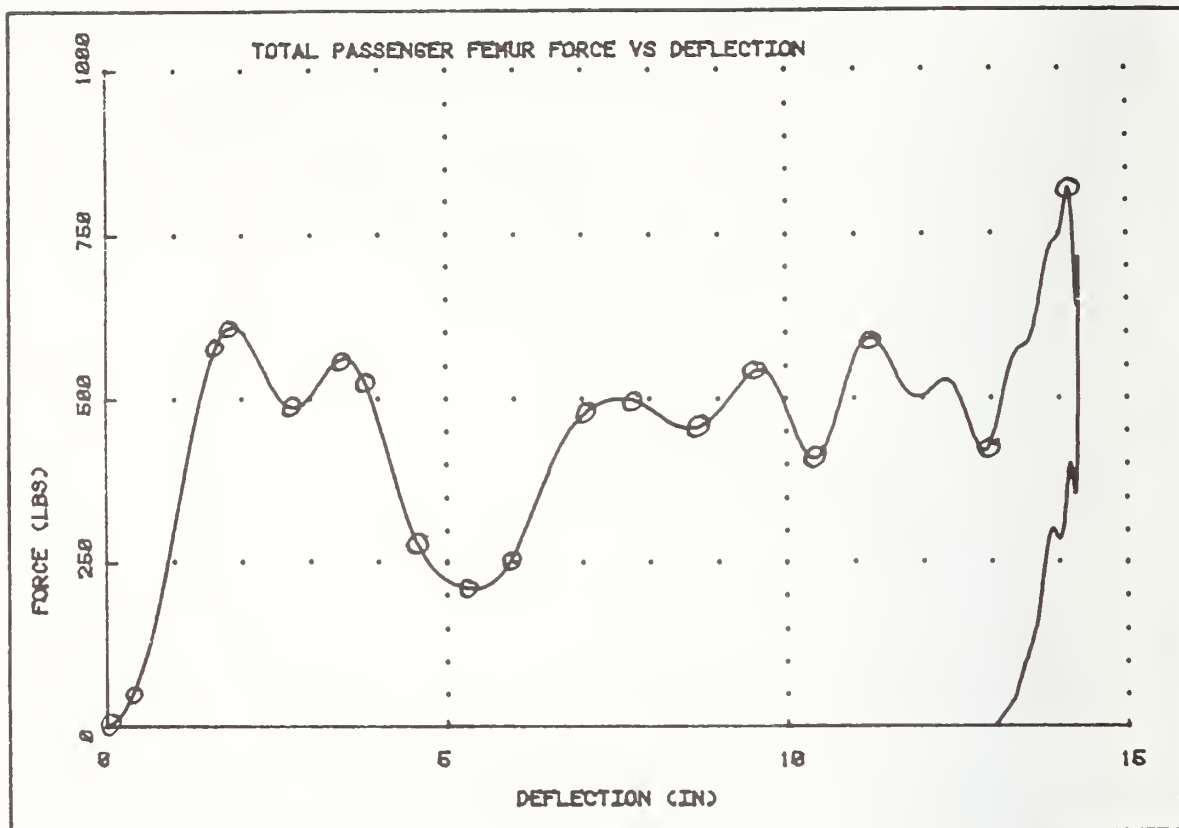
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>6.71</u>	<u>2841.60</u>
<u>1.27</u>	<u>768.00</u>	_____	_____
<u>1.71</u>	<u>947.20</u>	_____	_____
<u>2.30</u>	<u>1105.92</u>	_____	_____
<u>3.20</u>	<u>1346.56</u>	_____	_____
<u>3.72</u>	<u>1525.76</u>	_____	_____
<u>5.58</u>	<u>2483.20</u>	_____	_____
<u>6.48</u>	<u>2800.00</u>	_____	_____

Filter cutoff frequency: 25 Hz.

Test: Passenger Side Femur (dynamic) . Date: October 11, 1984

Vehicle: Ford Mustang

Options: No radio



G= 0.912 R= 0.037 K= 972.62

c=  $\mu_1$ =  $\mu_2$ =  $\mu_3$ =

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

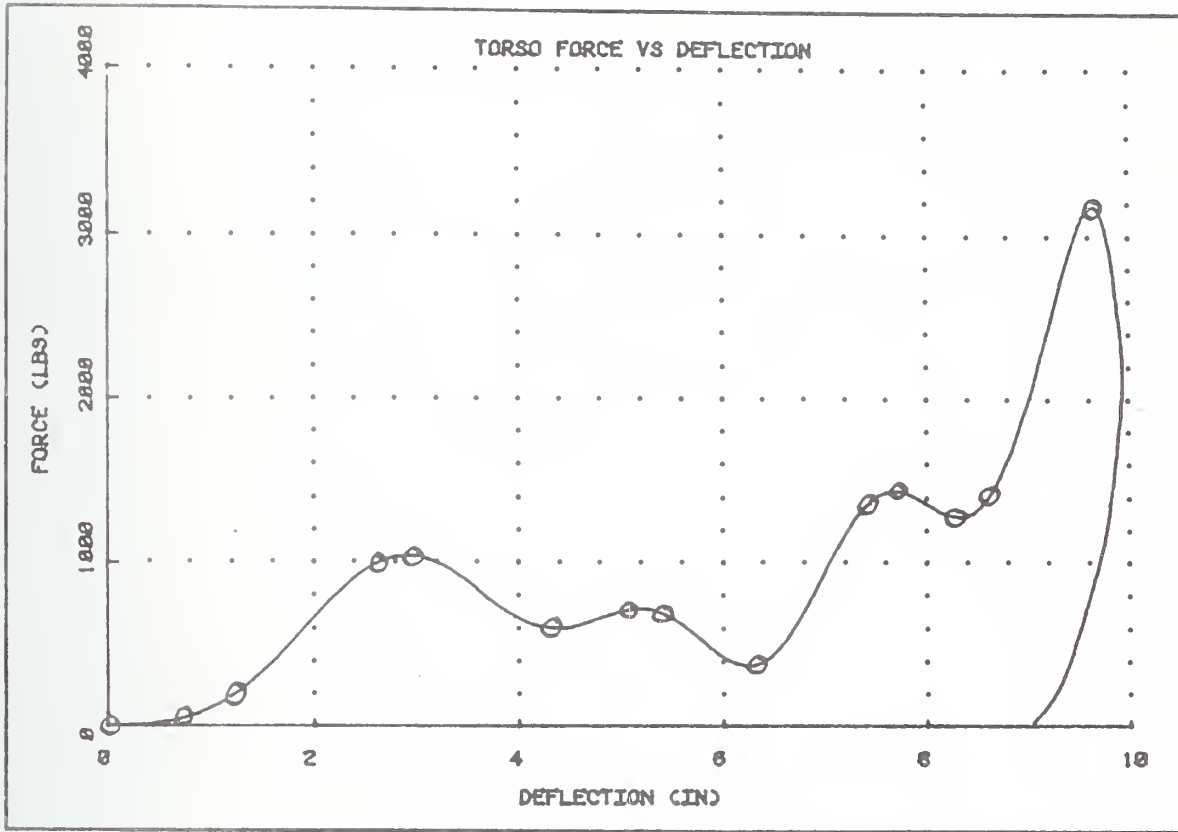
Deflection	Force	Deflection	Force
0.0	0.0	5.95	256.00
0.37	46.09	7.00	476.16
1.57	563.20	7.61	496.64
1.79	604.16	8.65	455.68
2.61	501.76	9.63	552.96
3.43	558.08	10.38	409.60
3.80	517.12	11.12	588.80
4.61	276.48	12.91	430.08
5.20	215.40	14.10	808.96

Filter cutoff frequency: 100 Hz.

Test: Torso (dynamic) Date: October 11, 1984

Vehicle: Ford Mustang

Options: No Radio



G= 0.907 R= 0.066 K= 4150.69

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

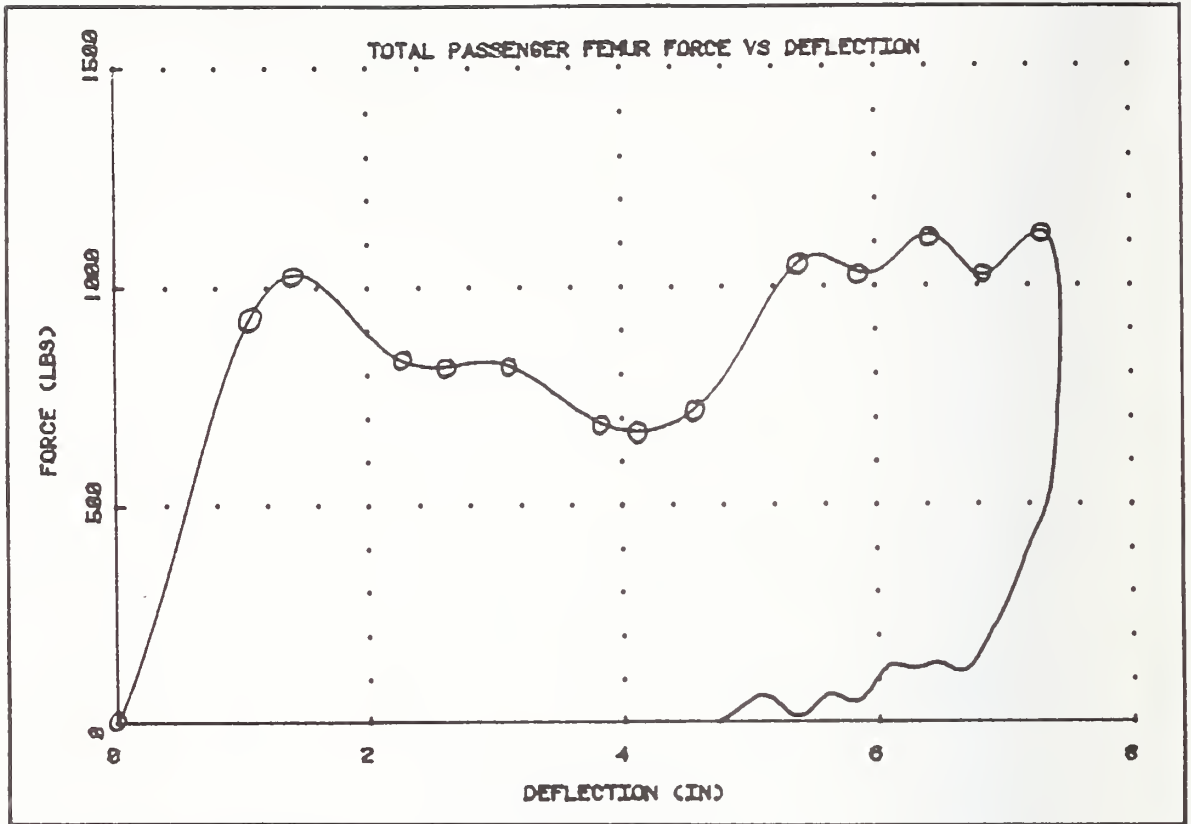
Deflection	Force	Deflection	Force
0.0	0.0	6.26	373.76
0.75	46.08	7.31	1274.88
1.20	184.32	7.68	1433.60
2.61	998.40	8.29	1274.88
2.91	1039.36	8.65	1433.60
4.25	599.04	9.63	3174.40
5.07	716.80		
5.44	675.84		

Filter cutoff frequency: 100 Hz.

Test: Passenger side femur (dynamic) Date: October 12, 1984

Vehicle: Ford Pinto

Options: Metal dash



G= 0.636 R= 0.065 K= 1102.31

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>4.52</u>	<u>732.16</u>
<u>0.96</u>	<u>921.60</u>	<u>5.27</u>	<u>1049.60</u>
<u>1.33</u>	<u>1039.36</u>	<u>5.79</u>	<u>1029.12</u>
<u>2.16</u>	<u>839.68</u>	<u>6.31</u>	<u>1126.40</u>
<u>2.53</u>	<u>819.20</u>	<u>6.68</u>	<u>1024.00</u>
<u>2.97</u>	<u>839.68</u>	<u>7.19</u>	<u>1121.28</u>
<u>3.71</u>	<u>696.32</u>		
<u>4.00</u>	<u>675.84</u>		

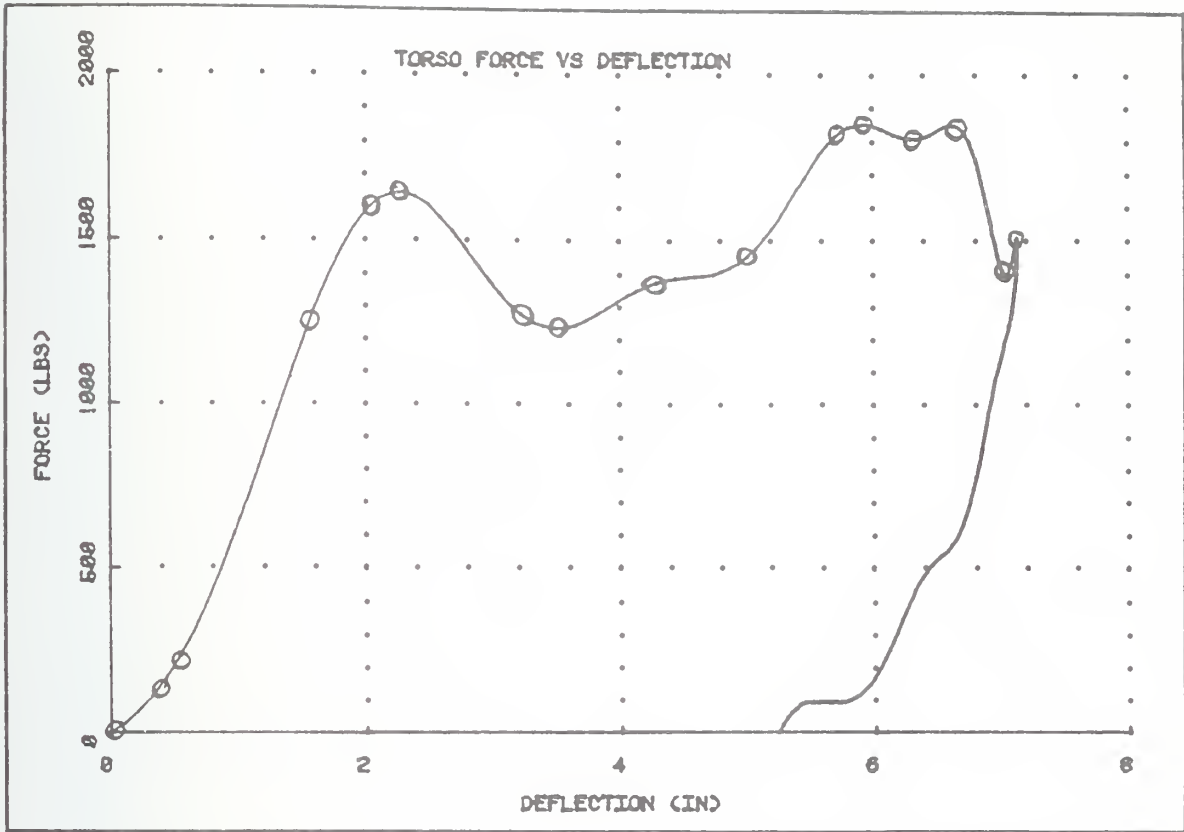
Filter cutoff frequency: 100 Hz.

Test: Torso (dynamic)

Date: October 12, 1984

Vehicle: Ford Pinto

Options: Metal dash



G= 0.734

R=0.086

K= 1394.66

c=

$\mu_1$ =

$\mu_2$ =

$\mu_3$ =

$\delta_A$ = 0.0

$\delta_B$ = 0.0

$\delta_C$ = 0.0

$\delta_D$ = 1000.0

$\delta_F$ = 1000.1

Deflection

Force

Deflection

Force

0.0

0.0

4.25

1377.28

0.30

107.52

5.01

1454.08

0.52

225.28

5.67

1812.48

1.57

1264.64

5.89

1853.44

2.01

1602.56

6.26

1812.48

2.30

1643.52

6.63

1853.44

3.20

1280.00

6.93

1413.12

3.43

1239.04

7.07

1510.40

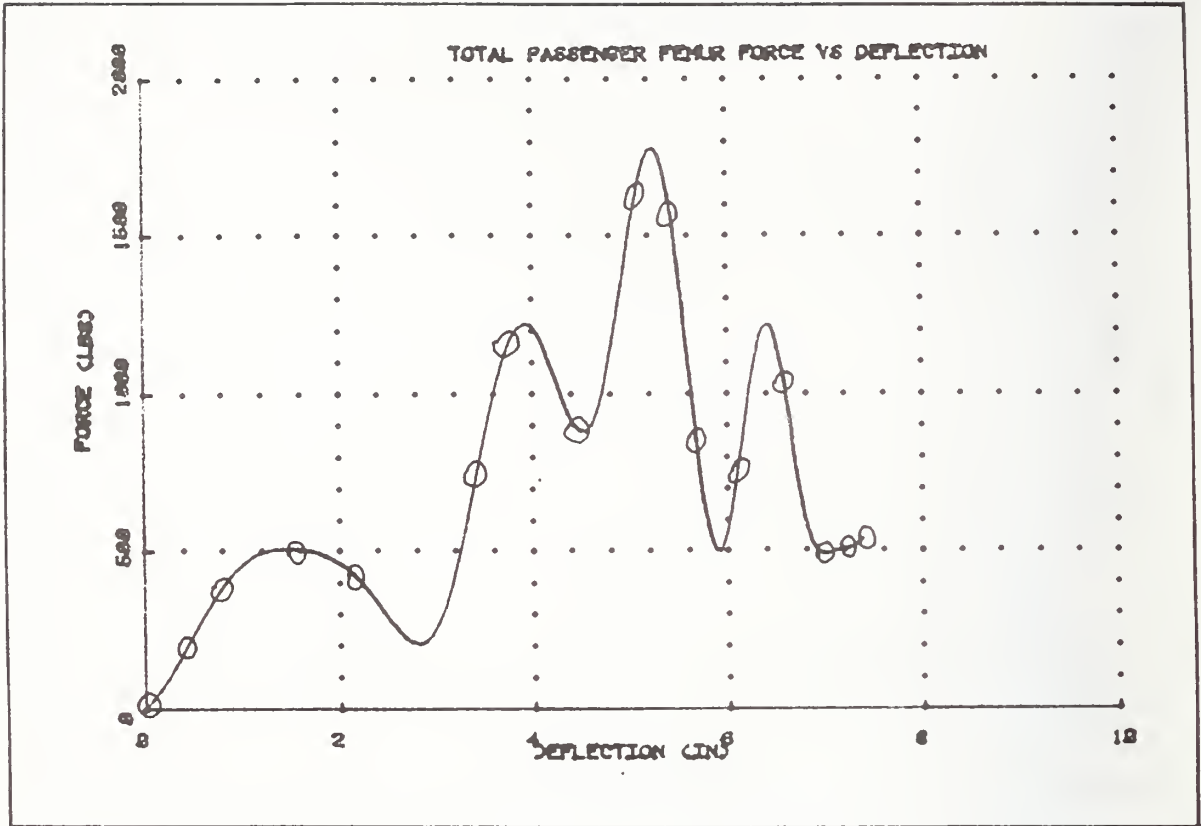
Filter cutoff frequency: 100 Hz.

Test: Passenger Side Femur (dynamic)

Date: October 14, 1984

Vehicle: Chevy Chevette

Options: No radio



G= 1.0

R= 0.0

K= N/A

c=

$\mu_1$ =

$\mu_2$ =

$\mu_3$ =

$\delta_A$ = 0

$\delta_B$ = 0

$\delta_C$ = 0

$\delta_D$ = 1000.0

$\delta_F$ = 1000.1

Deflection

Force

Deflection

Force

0.0

0.0

5.21

1775.80

0.47

221.27

5.49

1409.36

0.86

416.27

5.95

518.34

1.48

508.26

6.11

768.63

2.08

442.32

6.56

1063.63

3.44

773.17

7.04

493.50

3.78

1178.16

7.13

501.84

4.54

878.87

7.38

536.07

Filter cutoff frequency: 100 Hz.

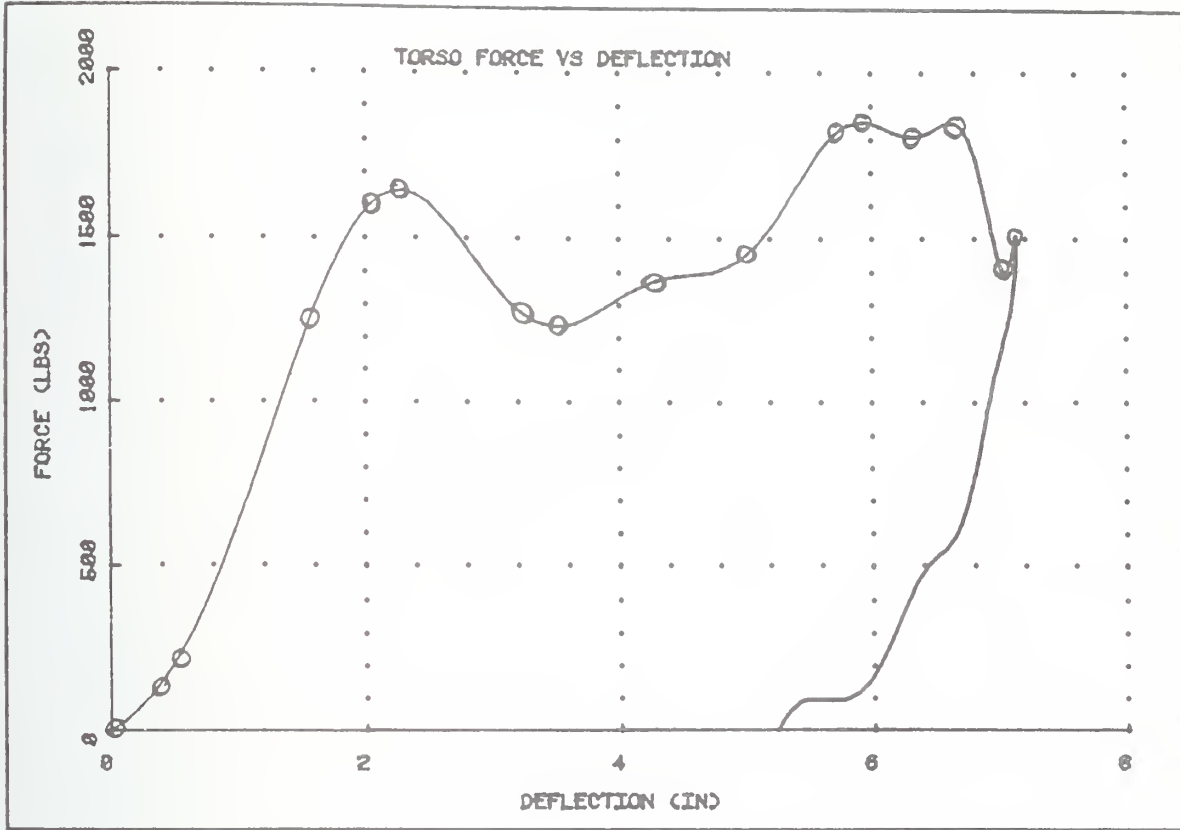


Test: Torso (dynamic)

Date: October 12, 1984

Vehicle: Ford Pinto

Options: Metal dash



G= 0.734

R=0.086

K= 1394.66

c=

$\mu_1$ =

$\mu_2$ =

$\mu_3$ =

$\delta_A$ = 0.0

$\delta_B$ = 0.0

$\delta_C$ = 0.0

$\delta_D$ = 1000.0

$\delta_F$ = 1000.1

Deflection

Force

Deflection

Force

0.0

0.0

4.25

1377.28

0.30

107.52

5.01

1454.08

0.52

225.28

5.67

1812.48

1.57

1264.64

5.89

1853.44

2.01

1602.56

6.26

1812.48

2.30

1643.52

6.63

1853.44

3.20

1280.00

6.93

1413.12

3.43

1239.04

7.07

1510.40

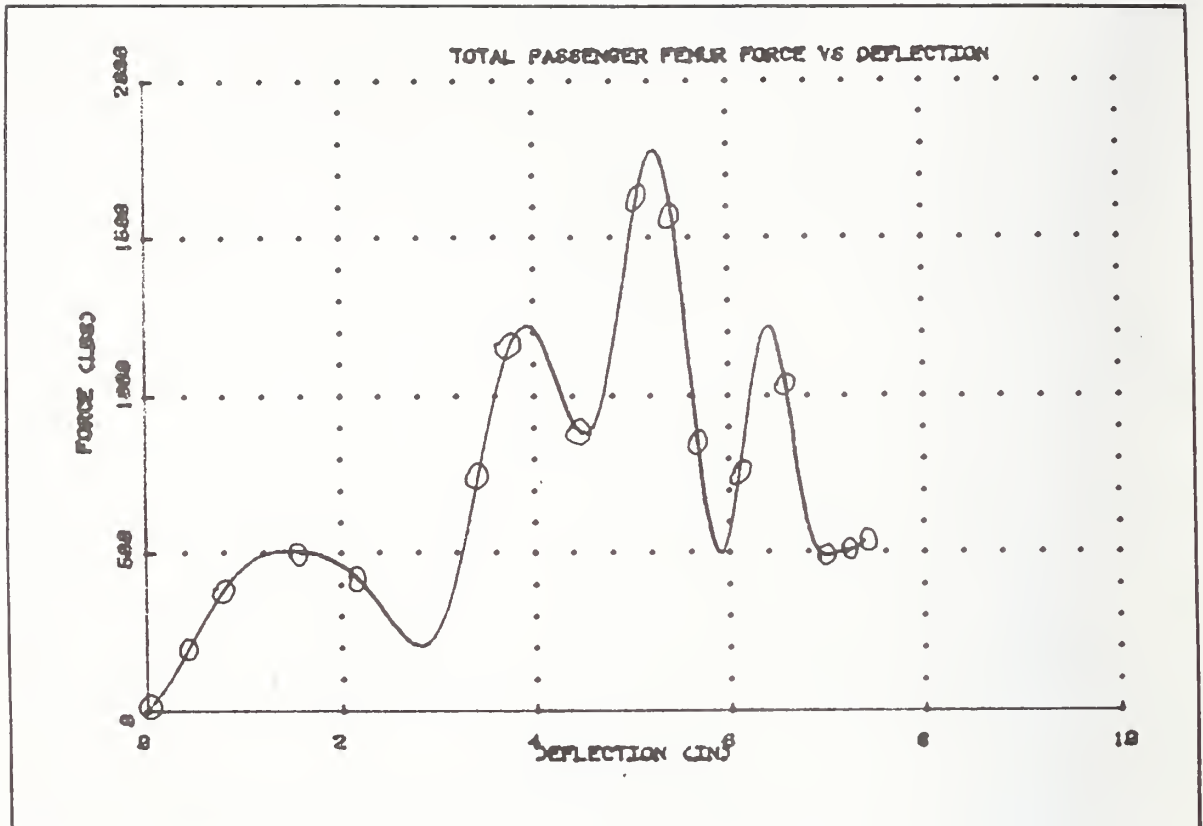
Filter cutoff frequency: 100 Hz.

Test: Passenger Side Femur (dynamic)

Date: October 14, 1984

Vehicle: Chevy Chevette

Options: No radio



G= 1.0 R= 0.0 K= N/A  
 c= u<sub>1</sub>= u<sub>2</sub>= u<sub>3</sub>=  
 δ<sub>A</sub>= 0 δ<sub>B</sub>= 0 δ<sub>C</sub>= 0 δ<sub>D</sub>= 1000.0 δ<sub>F</sub>= 1000.1

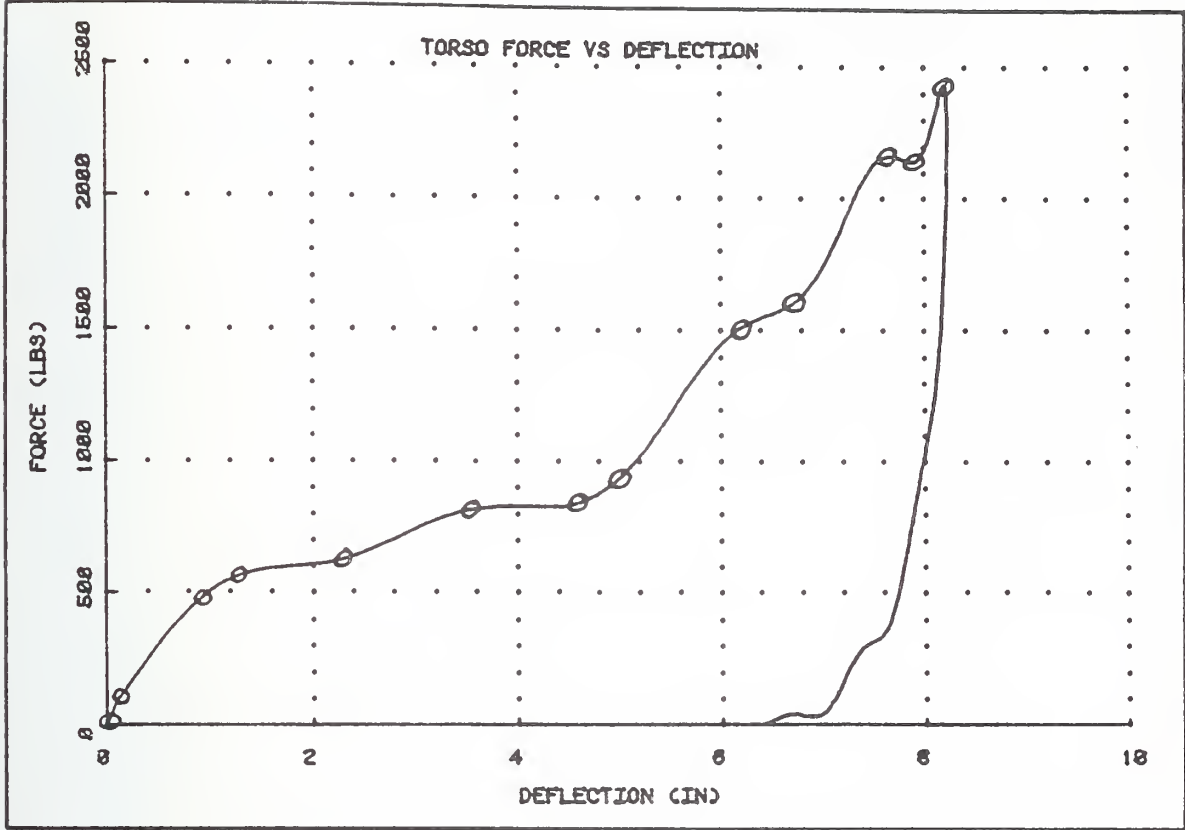
Deflection	Force	Deflection	Force
0.0	0.0	5.21	1775.80
0.47	221.27	5.49	1409.36
0.86	416.27	5.95	518.34
1.48	508.26	6.11	768.63
2.08	442.32	6.56	1063.63
3.44	773.17	7.04	493.50
3.78	1178.16	7.13	501.84
4.54	878.87	7.38	536.07

Filter cutoff frequency: 100 Hz.

Test: Torso (dynamic) Date: October 14, 1984

Vehicle: Chevy Chevette

Options: No radio



G= 0.780 R= 0.086 K= 3505.84

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

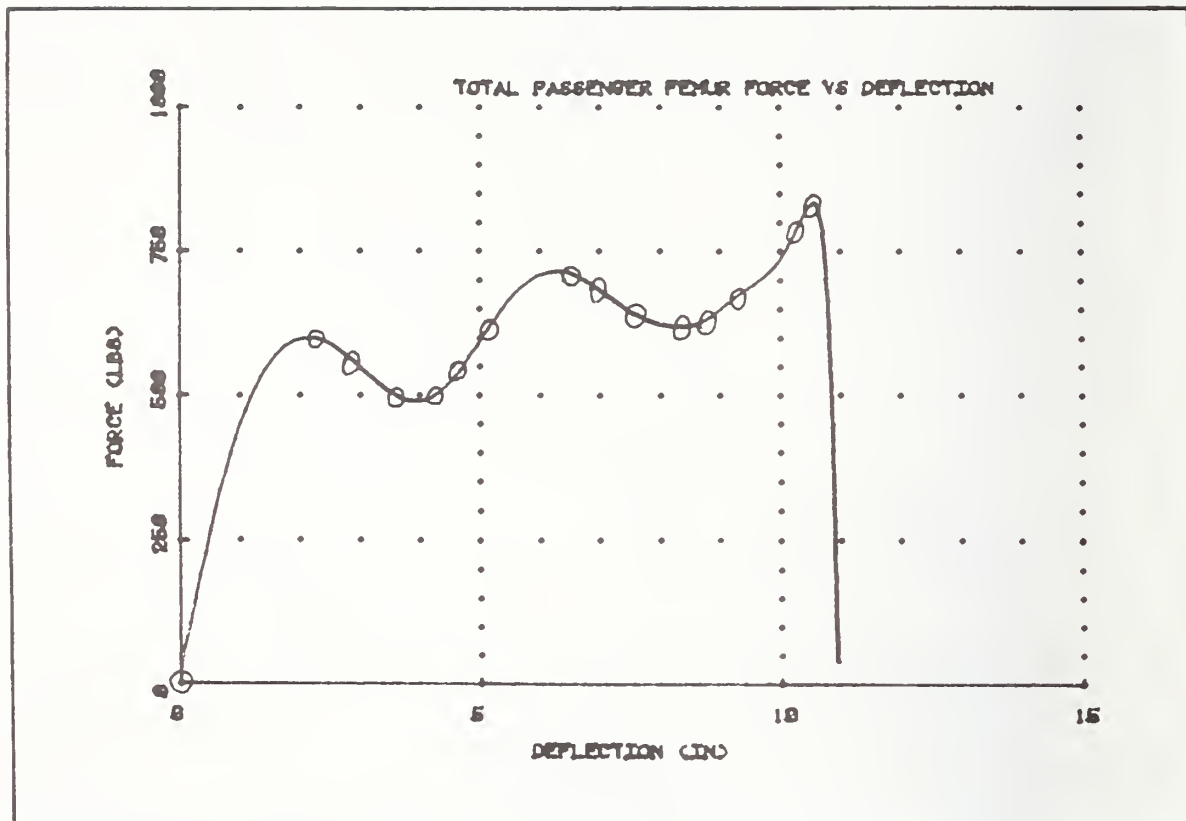
Deflection	Force	Deflection	Force
<u>0.0</u>	<u>0.0</u>	<u>6.19</u>	<u>1515.52</u>
<u>0.15</u>	<u>128.00</u>	<u>6.78</u>	<u>1633.28</u>
<u>0.90</u>	<u>465.92</u>	<u>7.67</u>	<u>2165.76</u>
<u>1.27</u>	<u>563.20</u>	<u>7.89</u>	<u>2145.28</u>
<u>2.38</u>	<u>640.00</u>	<u>8.18</u>	<u>2426.88</u>
<u>3.57</u>	<u>819.20</u>	_____	_____
<u>4.55</u>	<u>839.68</u>	_____	_____
<u>4.92</u>	<u>916.48</u>	_____	_____

Filter cutoff frequency: 100 Hz.

Test: Passenger Side Femur (dynamic) Date: October 15, 1984

Vehicle: Plymouth Volare

Options: \_\_\_\_\_



G= 1.0 R= 0.0 K= N/A

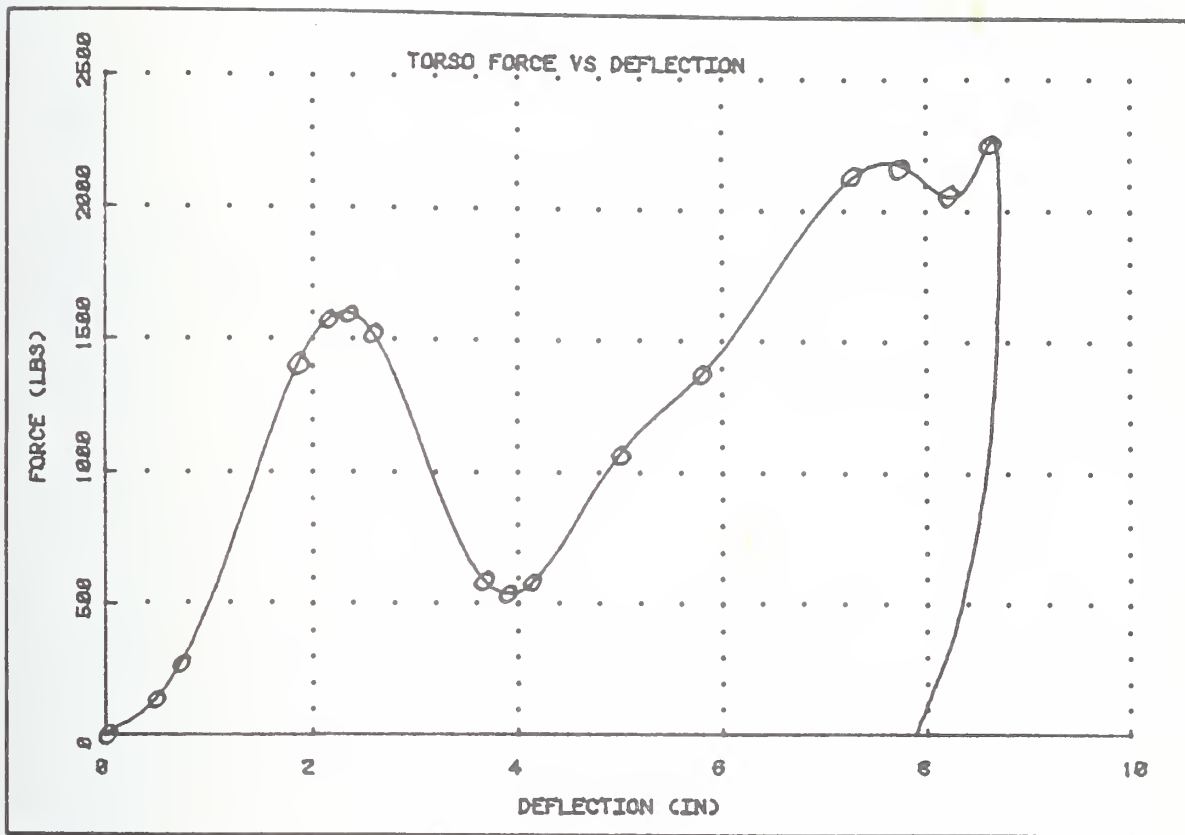
c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0  $\delta_B$ = 0  $\delta_C$ = 0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
0.0	0.0	6.92	686.37
2.15	599.92	7.51	643.38
2.93	553.35	8.38	618.02
3.53	500.97	8.72	629.04
4.11	491.51	9.27	671.34
4.67	543.96	10.36	804.36
5.08	606.41	10.72	772.41
6.46	712.07		

Filter cutoff frequency: 25 Hz.

Test: Torso (dynamic) Date: October 16, 1984  
 Vehicle: Plymouth Volare  
 Options: \_\_\_\_\_



G= 0.904 R= 0.042 K= 4338.77

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>3.87</u>	<u>537.60</u>
<u>0.44</u>	<u>102.40</u>	<u>4.09</u>	<u>578.56</u>
<u>0.74</u>	<u>302.08</u>	<u>4.99</u>	<u>1075.20</u>
<u>1.87</u>	<u>1402.88</u>	<u>5.82</u>	<u>1392.64</u>
<u>2.08</u>	<u>1561.60</u>	<u>7.31</u>	<u>2150.40</u>
<u>2.38</u>	<u>1582.08</u>	<u>7.68</u>	<u>2191.36</u>
<u>2.60</u>	<u>1520.64</u>	<u>8.29</u>	<u>2053.12</u>
<u>3.65</u>	<u>599.04</u>	<u>8.65</u>	<u>2273.28</u>

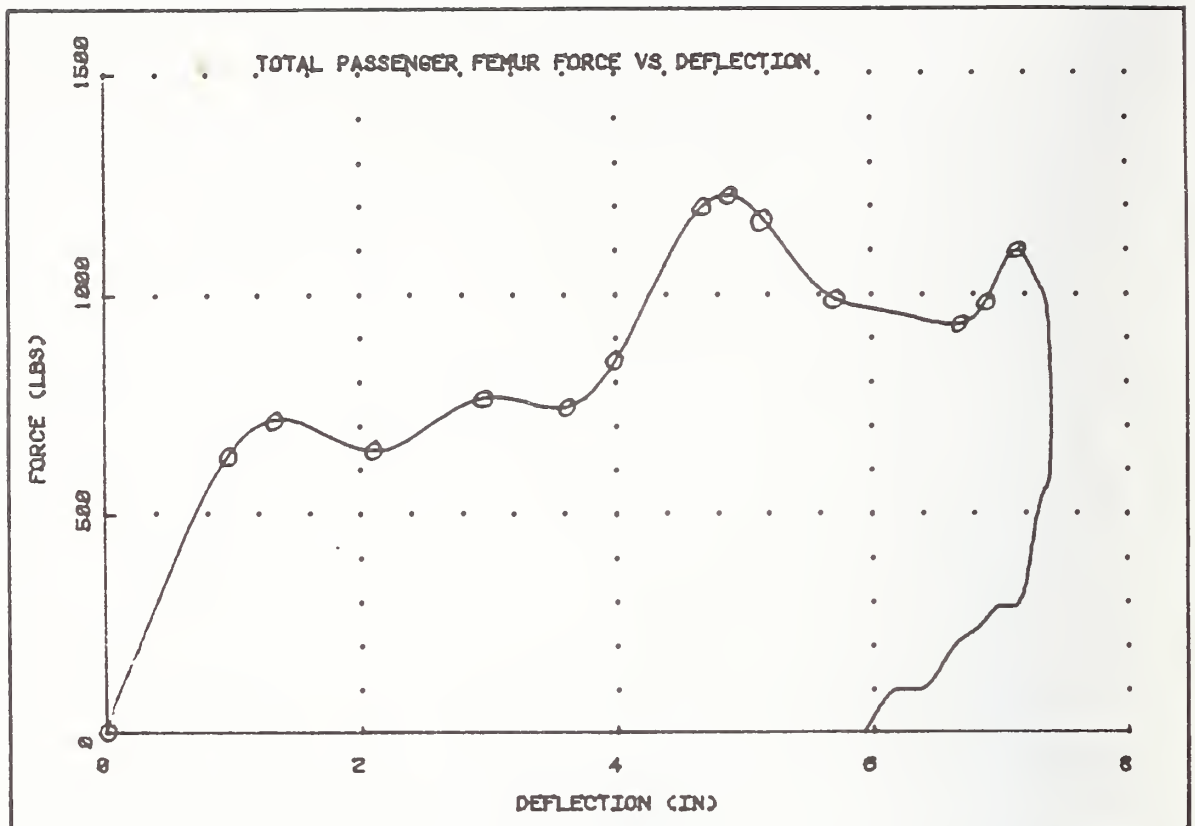
Filter cutoff frequency: 100 Hz.

Test: passenger Side Femur (dynamic)

Date: October 18, 1984

Vehicle: Ford LTD

Options: \_\_\_\_\_



G= 0.801 R= 0.053 K= 856.43

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

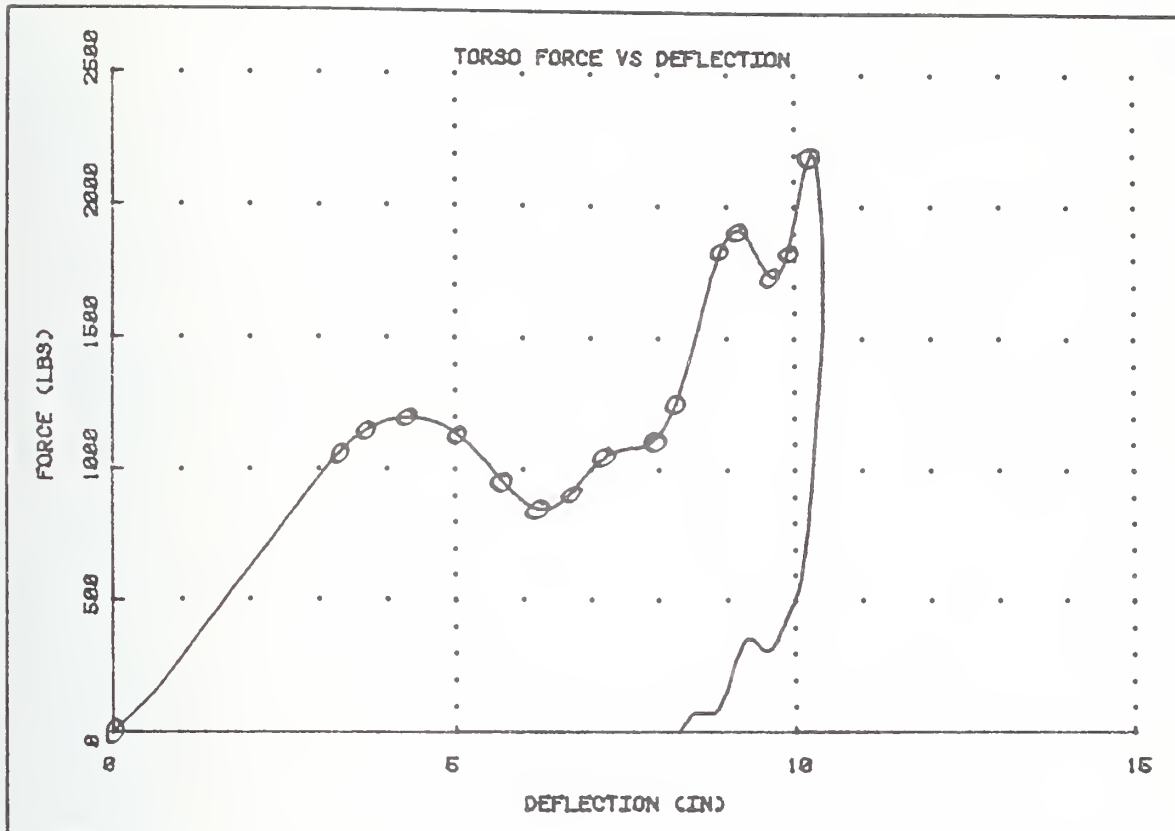
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>4.86</u>	<u>1228.80</u>
<u>0.90</u>	<u>619.52</u>	<u>5.15</u>	<u>1167.36</u>
<u>1.27</u>	<u>716.80</u>	<u>5.67</u>	<u>988.16</u>
<u>2.10</u>	<u>634.88</u>	<u>6.72</u>	<u>926.72</u>
<u>3.00</u>	<u>773.12</u>	<u>6.87</u>	<u>983.04</u>
<u>3.60</u>	<u>752.64</u>	<u>7.16</u>	<u>1100.80</u>
<u>3.97</u>	<u>849.92</u>		
<u>4.64</u>	<u>1187.84</u>		

Filter cutoff frequency: 100 Hz.

Test: Torso (dynamic) Date: October 18, 1984

Vehicle: Ford LTD

Options: \_\_\_\_\_



G= 0.795 R= 0.073 K= 1858.08

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

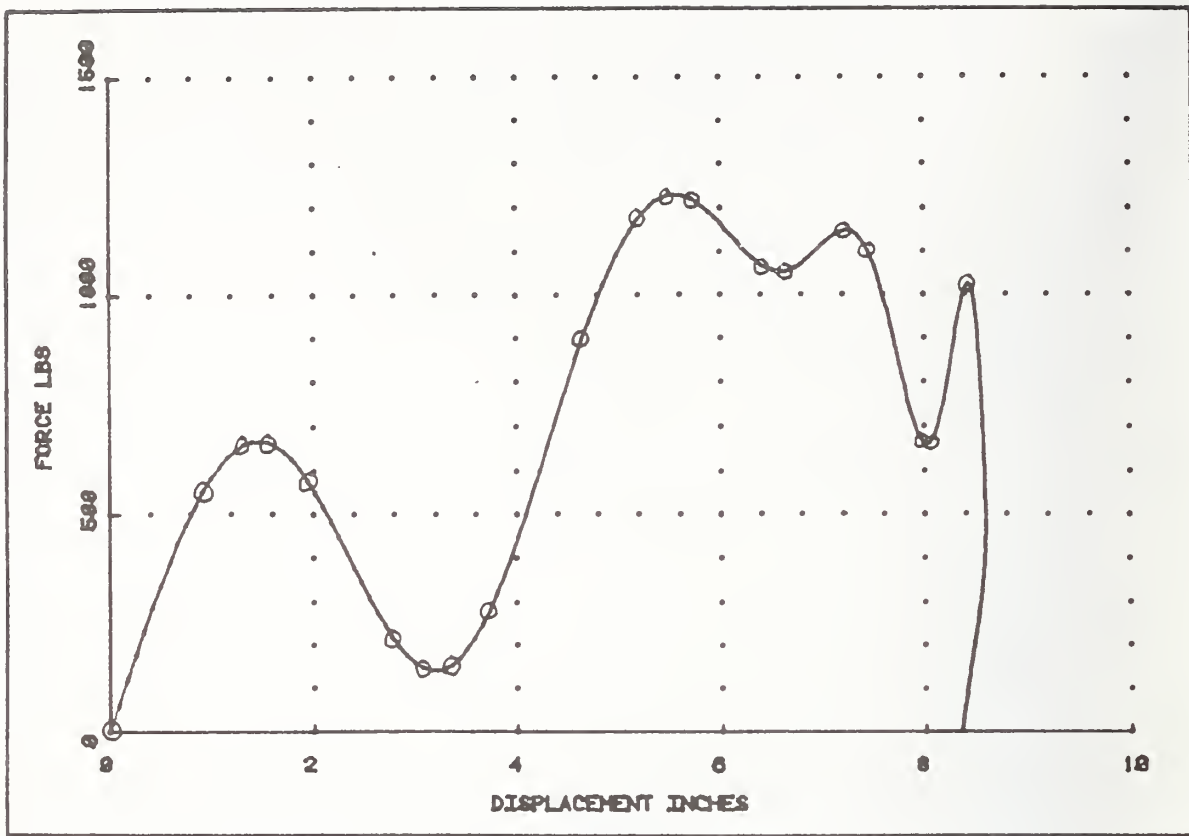
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>7.22</u>	<u>1049.60</u>
<u>3.29</u>	<u>1059.84</u>	<u>7.89</u>	<u>1111.04</u>
<u>3.96</u>	<u>1177.60</u>	<u>8.26</u>	<u>1249.28</u>
<u>4.40</u>	<u>1198.08</u>	<u>8.92</u>	<u>1848.32</u>
<u>5.01</u>	<u>1136.64</u>	<u>9.14</u>	<u>1909.76</u>
<u>5.60</u>	<u>972.80</u>	<u>9.67</u>	<u>1730.56</u>
<u>6.19</u>	<u>849.92</u>	<u>9.90</u>	<u>1807.36</u>
<u>6.63</u>	<u>890.88</u>	<u>10.26</u>	<u>2206.72</u>

Filter cutoff frequency: 100 Hz.

Test: Passenger side femur (dynamic) Date: February 4, 1985

Vehicle: Chevy Celebrity

Options: No radio or ashtray



G= .971 R= .008 N= 2343

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_1$ = 1000.0  $\delta_F$ = 1000.0

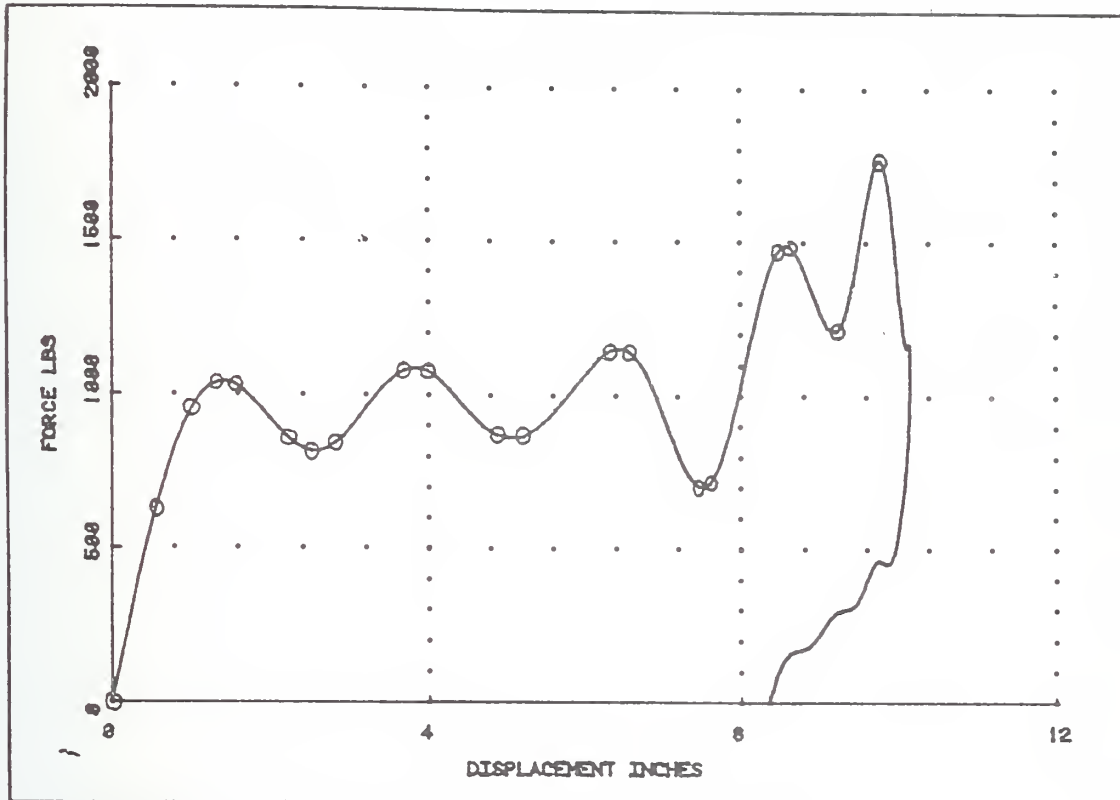
Deflection	Force	Deflection	Force
<u>0.0</u>	<u>0.0</u>	<u>5.23</u>	<u>1186.5</u>
<u>.91</u>	<u>549.9</u>	<u>5.54</u>	<u>1228.7</u>
<u>1.31</u>	<u>658.5</u>	<u>5.71</u>	<u>1217.9</u>
<u>1.55</u>	<u>663.8</u>	<u>6.36</u>	<u>1073.5</u>
<u>1.90</u>	<u>578.4</u>	<u>6.60</u>	<u>1051.4</u>
<u>2.76</u>	<u>217.4</u>	<u>7.19</u>	<u>1146.5</u>
<u>3.21</u>	<u>139.5</u>	<u>7.49</u>	<u>1102.5</u>
<u>3.43</u>	<u>169.1</u>	<u>7.98</u>	<u>662.2</u>
<u>3.72</u>	<u>279.2</u>	<u>8.02</u>	<u>658.2</u>
<u>4.64</u>	<u>897.6</u>	<u>8.43</u>	<u>1024.5</u>



Test: Torso (dynamic) Date: February 4, 1985

Vehicle: Chevy Celebrity

Options: No radio or ashtray



G= .819 R= .057 K= 1095

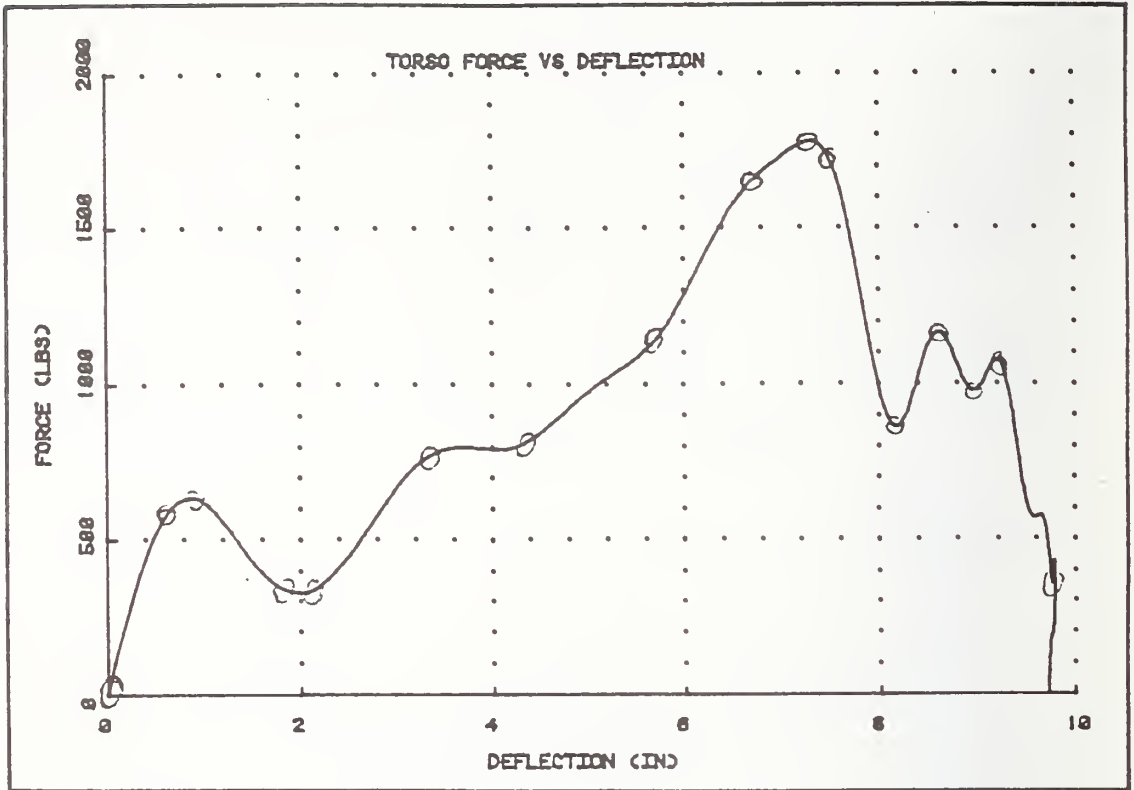
c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_E$ = 1000.0

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
0.0	0.0	4.87	870.5
.56	634.9	5.29	879.8
1.01	955.2	6.18	1121.4
1.34	1039.7	6.56	1143.0
1.55	1029.5	7.53	702.7
2.19	860.8	7.59	715.3
2.50	815.1	8.45	1465.6
2.81	842.6	8.61	1484.3
3.78	1086.9	9.18	1209.0
4.06	1061.4	9.78	1769.5

Note: Corresponding VAX data file is [MGAPROG] CELEBRITY. F20;1

Test: Torso (dynamic) Date: March 12, 1985  
 Vehicle: Chevy Celebrity  
 Options: \_\_\_\_\_  
 \_\_\_\_\_



G= 0.993 R= 0.001 K= 7279.0  
 c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_  
 $\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.0

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>6.74</u>	<u>1661.8</u>
<u>0.57</u>	<u>556.0</u>	<u>7.27</u>	<u>1778.9</u>
<u>0.88</u>	<u>634.5</u>	<u>7.49</u>	<u>1732.1</u>
<u>1.82</u>	<u>335.4</u>	<u>8.18</u>	<u>861.7</u>
<u>2.13</u>	<u>337.5</u>	<u>8.62</u>	<u>1164.7</u>
<u>3.33</u>	<u>769.7</u>	<u>8.96</u>	<u>975.8</u>
<u>4.33</u>	<u>810.8</u>	<u>9.20</u>	<u>1075.8</u>
<u>5.71</u>	<u>1146.8</u>	<u>9.76</u>	<u>353.2</u>

\*Note:  
 Corresponding VAX data file is [MGAPROG] CELEBRITY. F20;2 (second test done to check out MGA's data acquisition system).

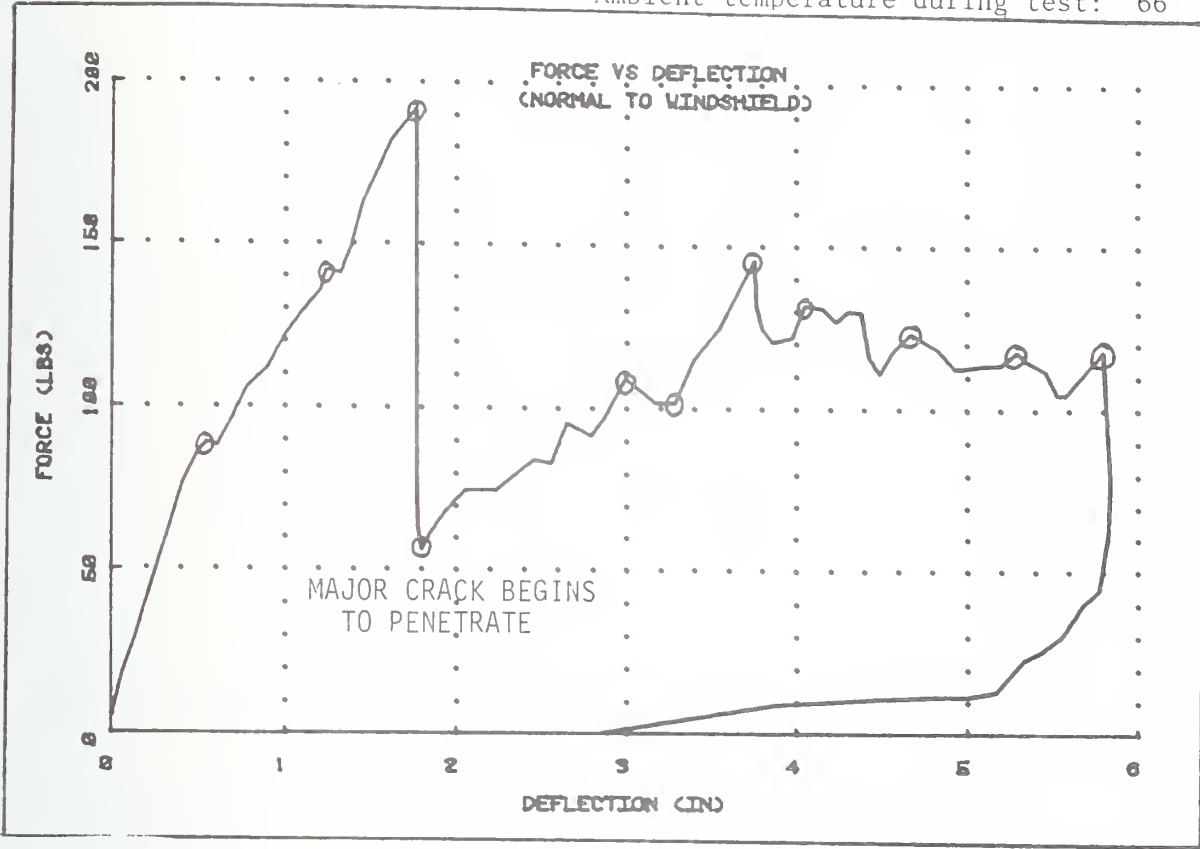
APPENDIX C

STATIC WINDSHIELD TEST RESULTS



Test: Windshield (static) Date: August 21, 1984  
 Vehicle: Honda Civic CVCC  
 Options: No radio

Windshield DOT #: 20 M 355 Ambient temperature during test: 66°



G= 0.489 R= 0.062 K= 218  
 c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_  
 $\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.00</u>	<u>0.00</u>	<u>5.29</u>	<u>118.01</u>
<u>0.53</u>	<u>88.32</u>	<u>5.80</u>	<u>119.04</u>
<u>1.22</u>	<u>142.33</u>		
<u>1.76</u>	<u>191.23</u>		
<u>1.79</u>	<u>56.06</u>		
<u>2.99</u>	<u>109.05</u>		
<u>3.29</u>	<u>101.12</u>		
<u>3.74</u>	<u>146.17</u>		
<u>4.04</u>	<u>132.09</u>		
<u>4.67</u>	<u>123.13</u>		

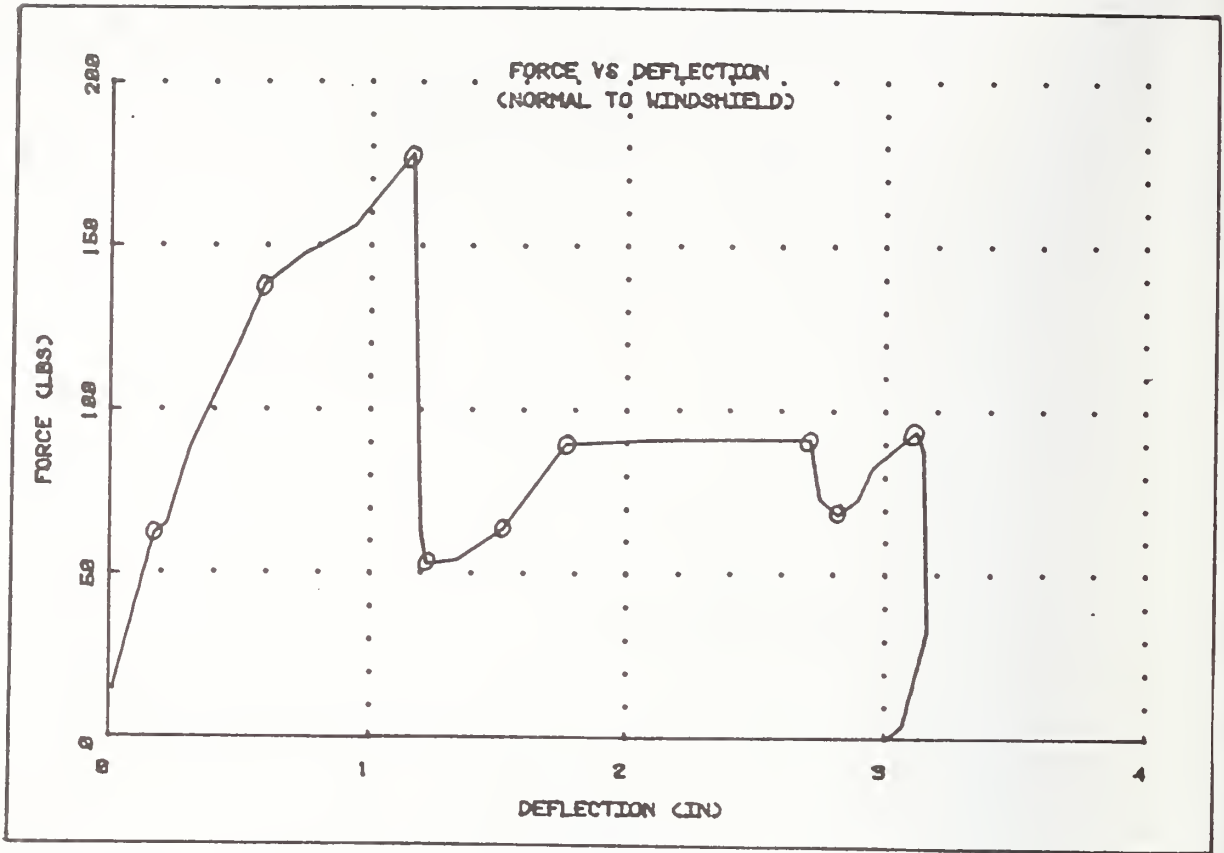
COMMENT: Static test data is not representative of dynamic data

Test: Windshield (static) Date: August 28, 1984

Vehicle: Ford LTD

Options: Air conditioning, radio missing

Windshield DOT #: 75FM-M91 Ambient temperature during test: 75°



G= 0.953 R= 0.006 K= 300

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
0.00	0.00		
0.17	62.47		
0.59	138.05		
1.17	178.20		
1.22	53.04		
1.53	63.91		
1.76	89.54		
2.71	91.21		
2.81	68.18		
3.12	97.97		

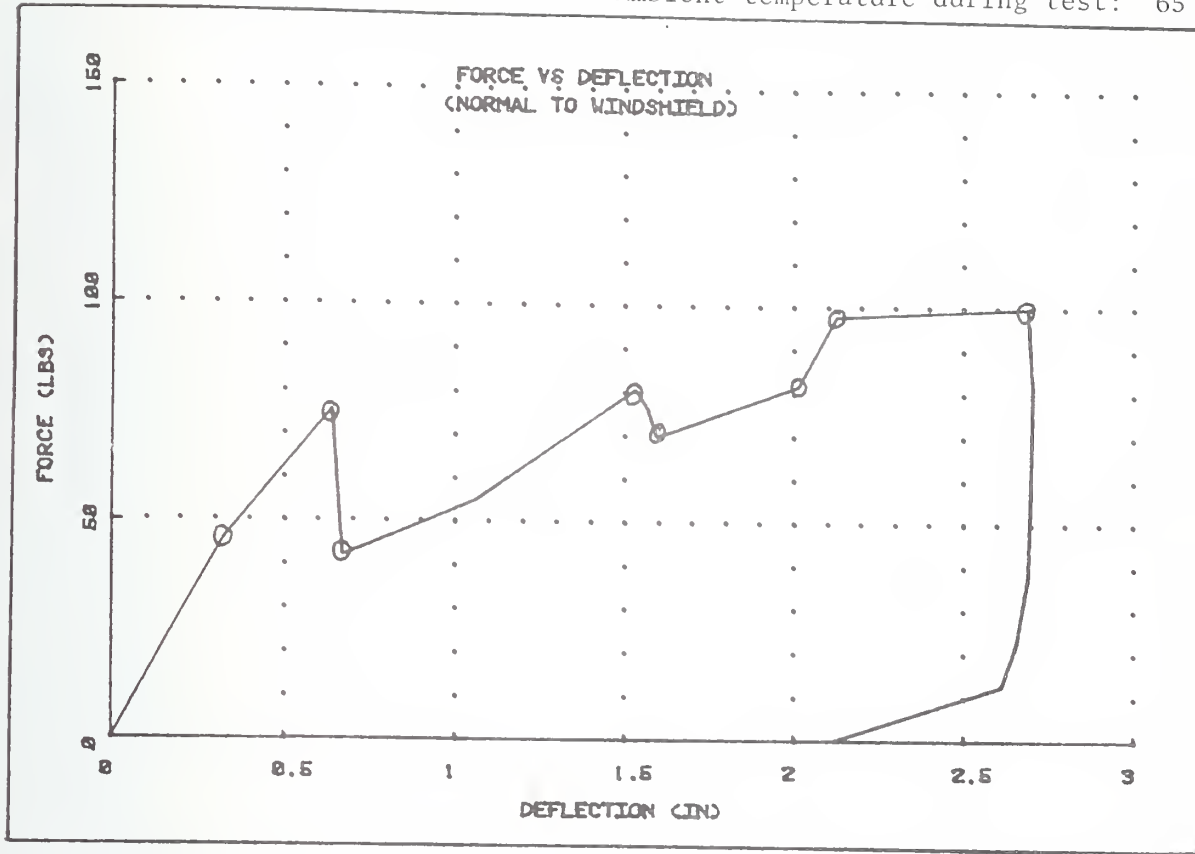
COMMENT: Static test data is not representative of dynamic data

Test: Windshield (static) Date: September 5, 1984

Vehicle: Ford Mustang

Options: \_\_\_\_\_

Windshield DOT #: 75 FM-M90 Ambient temperature during test: 65°



G= 0.784 R= 0.031 K= 345

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.00</u>	<u>0.00</u>	_____	_____
<u>0.32</u>	<u>46.07</u>	_____	_____
<u>0.63</u>	<u>75.40</u>	_____	_____
<u>0.67</u>	<u>41.89</u>	_____	_____
<u>1.53</u>	<u>80.63</u>	_____	_____
<u>1.59</u>	<u>69.64</u>	_____	_____
<u>2.01</u>	<u>81.68</u>	_____	_____
<u>2.12</u>	<u>97.91</u>	_____	_____
<u>2.68</u>	<u>100.01</u>	_____	_____

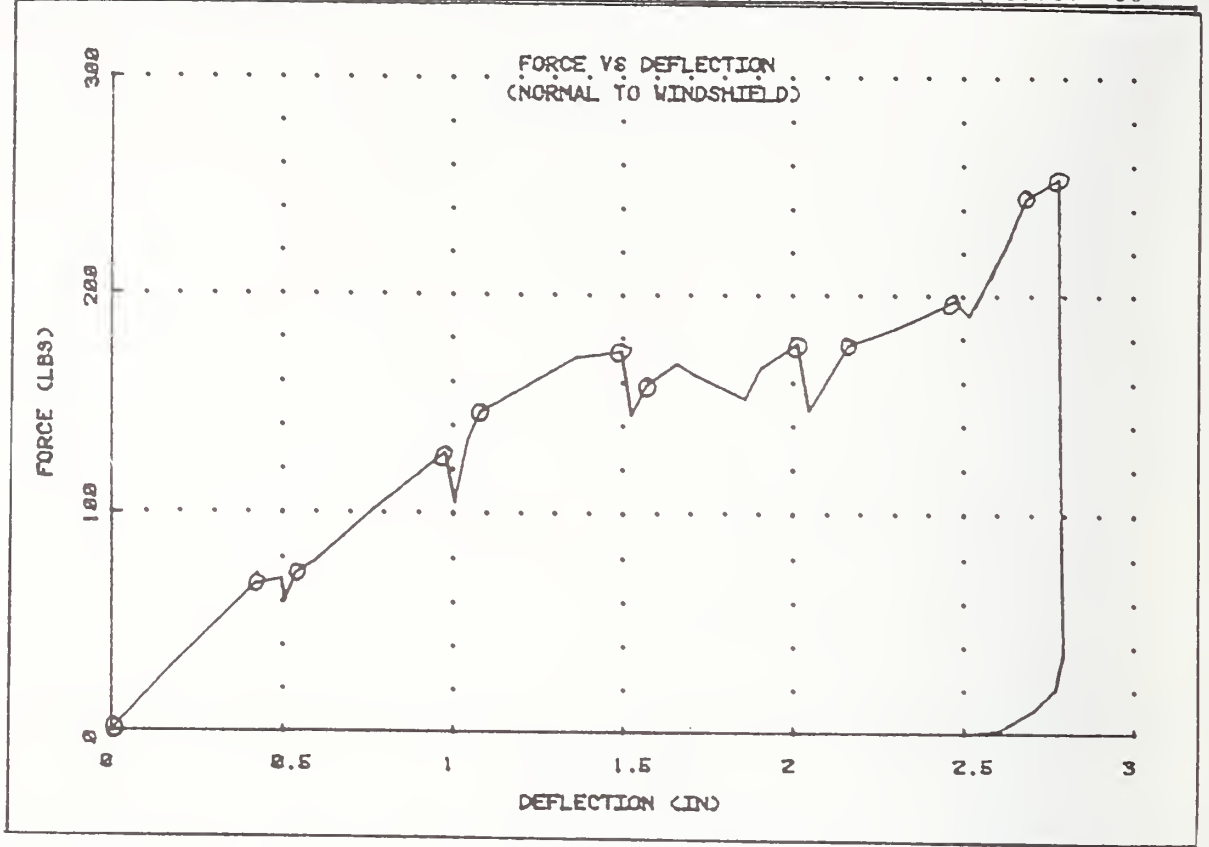
COMMENT: Static test data is not representative of dynamic data

Test: Windshield (static) Date: August 17, 1984

Vehicle: 1976 Chevy Monza

Options: Metal dash with foam crash pad on front

Windshield DOT #: 19 M-46 1 Ambient temperature during test: 80°



G= 0.911 R= 0.006 K= 612

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.1

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.00</u>	<u>0.00</u>	<u>2.16</u>	<u>176.64</u>
<u>0.41</u>	<u>67.96</u>	<u>2.46</u>	<u>197.76</u>
<u>0.54</u>	<u>73.72</u>	<u>2.69</u>	<u>245.76</u>
<u>0.97</u>	<u>127.48</u>	<u>2.77</u>	<u>254.54</u>
<u>1.07</u>	<u>146.68</u>		
<u>1.49</u>	<u>173.56</u>		
<u>1.57</u>	<u>158.59</u>		
<u>2.02</u>	<u>178.17</u>		

COMMENT: Static test data is not representative of dynamic data

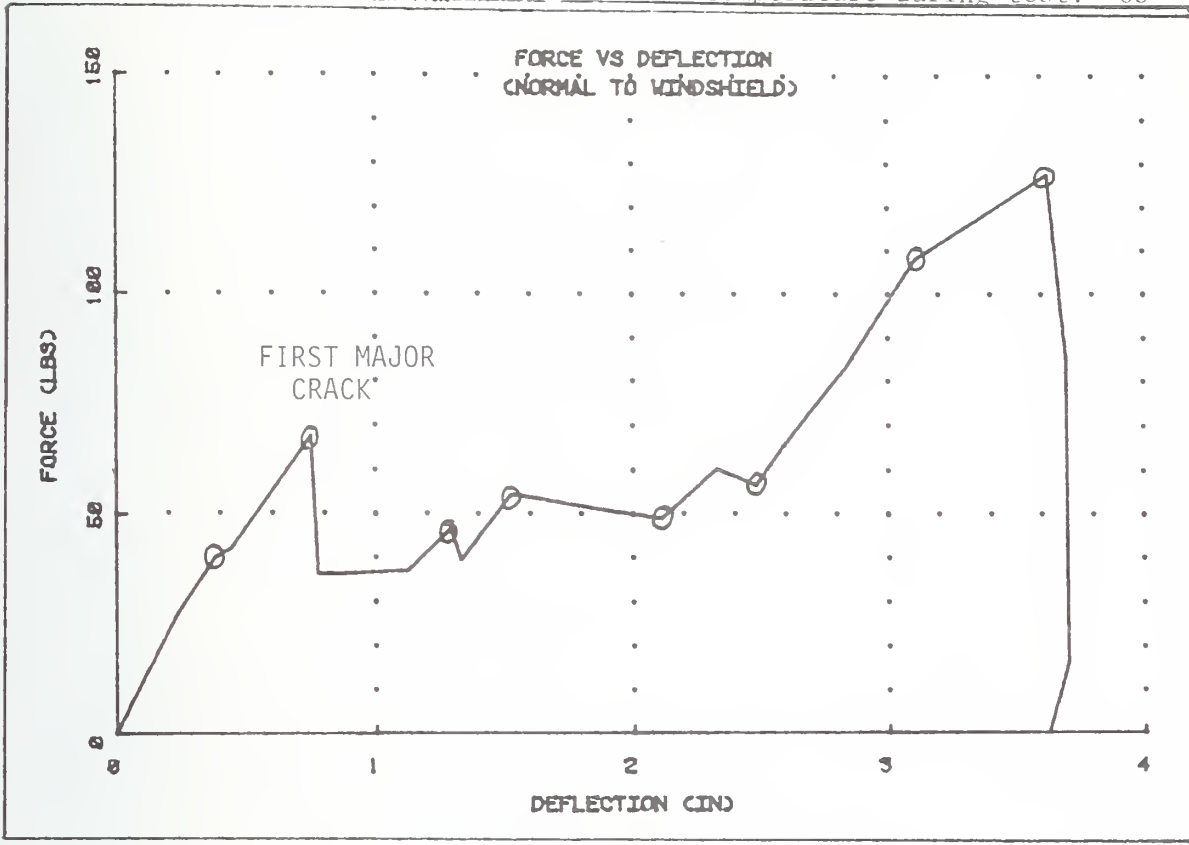


Test: Windshield (static) Date: September 11, 1984

Vehicle: Ford Pinto

Options: Metal dash with foam crash pad on top,  
heat control and radio missing

Windshield DOT #: 75FM-M90 Ambient temperature during test: 65°



G= 0.978 R= 0.003 K= 1077

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = \_\_\_\_\_  $\delta_B$ = \_\_\_\_\_  $\delta_C$ = \_\_\_\_\_  $\delta_D$ = \_\_\_\_\_  $\delta_F$ = \_\_\_\_\_

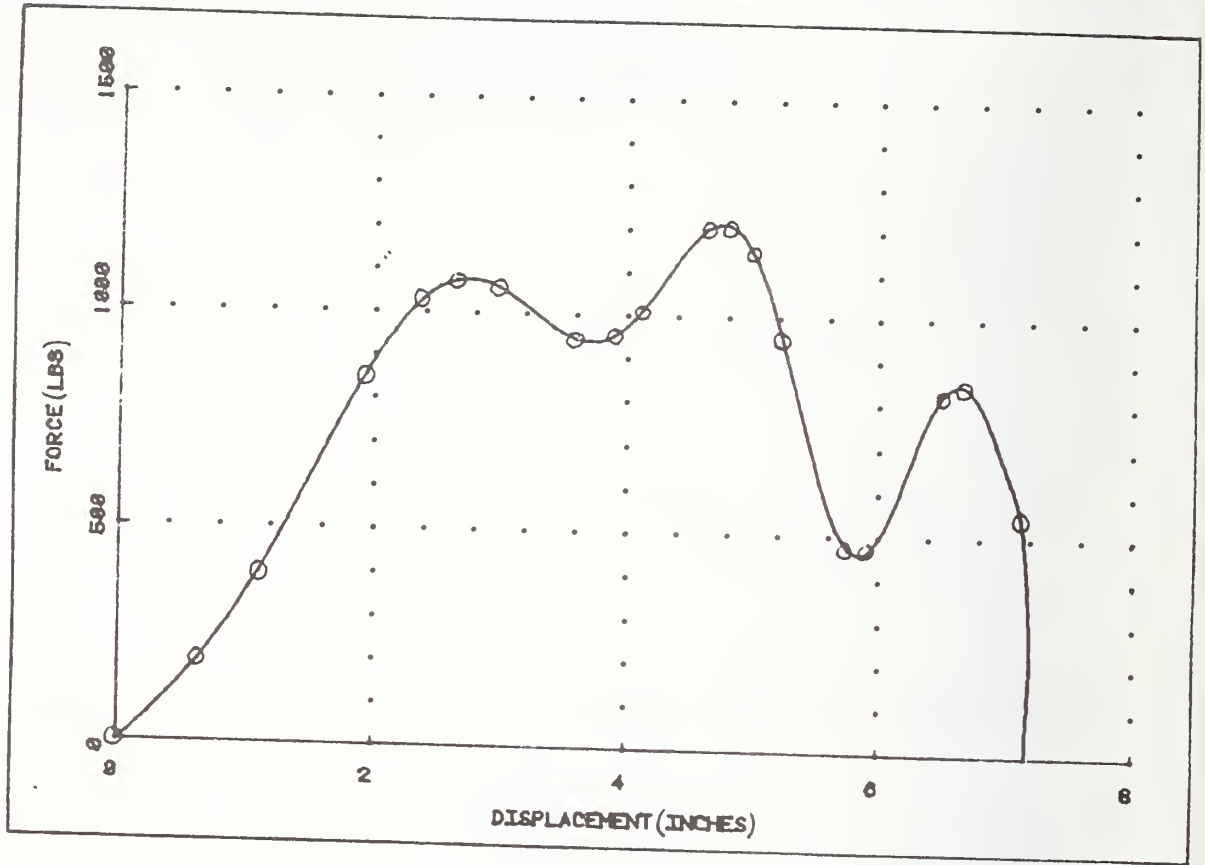
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
0.00	0.00	_____	_____
0.39	40.70	_____	_____
0.73	67.58	_____	_____
1.29	47.23	_____	_____
1.53	54.72	_____	_____
2.11	48.57	_____	_____
2.47	56.83	_____	_____
3.11	108.48	_____	_____
3.63	127.87	_____	_____

COMMENT: Static test data is not representative of dynamic data

Test: Driver side femur (dynamic) Date: February 1, 1985

Vehicle: Chevy Celebrity

Options: No radio or ashtray



G= 0.994 R= 0.0008 R= 5803  
 c= \_\_\_\_\_  $w_1$ = \_\_\_\_\_  $w_2$ = \_\_\_\_\_  
 $\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta$ = 1000.0  $\delta$ = 1000.0

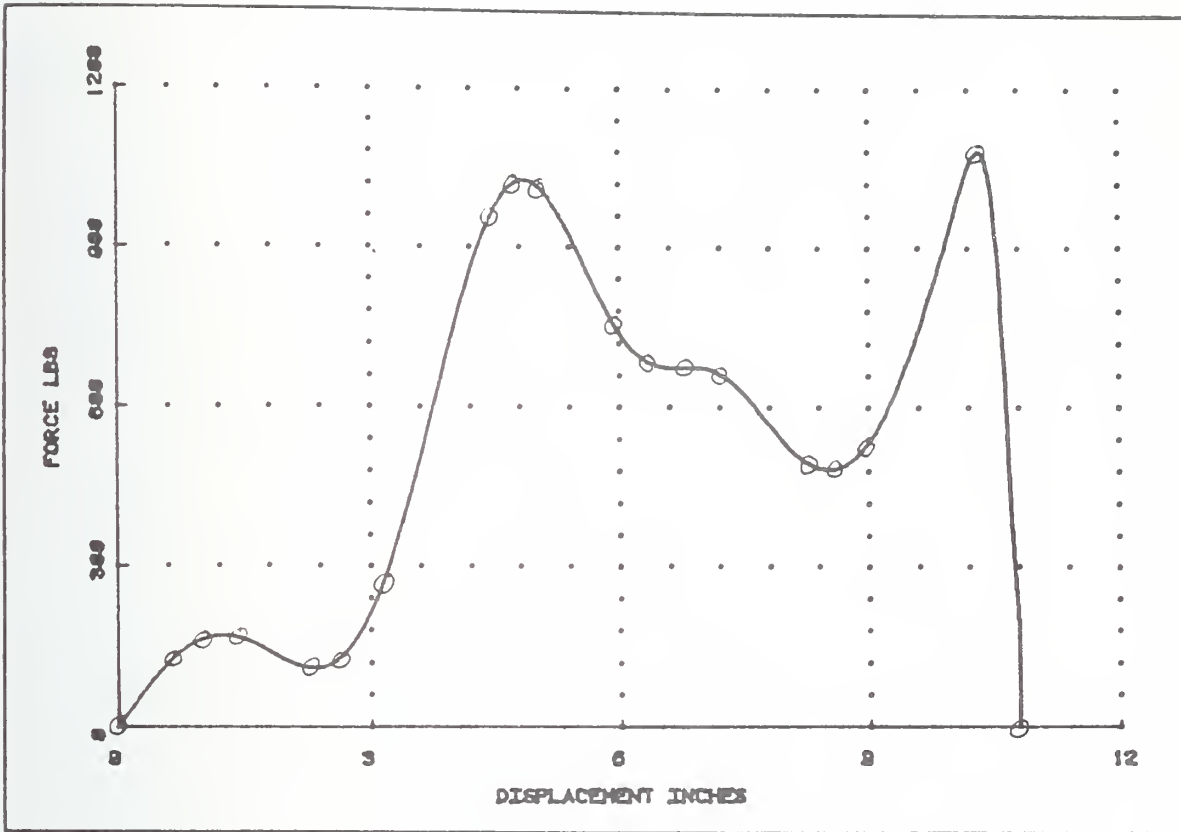
Deflection	Force	Deflection	Force
<u>0.0</u>	<u>0.0</u>	<u>4.61</u>	<u>1202.5</u>
<u>0.63</u>	<u>191.7</u>	<u>4.80</u>	<u>1210.5</u>
<u>1.09</u>	<u>396.9</u>	<u>4.98</u>	<u>1150.7</u>
<u>1.93</u>	<u>856.8</u>	<u>5.21</u>	<u>952.7</u>
<u>2.36</u>	<u>1028.7</u>	<u>5.72</u>	<u>483.7</u>
<u>2.64</u>	<u>1074.0</u>	<u>5.88</u>	<u>463.5</u>
<u>2.90</u>	<u>1067.5</u>	<u>6.48</u>	<u>822.4</u>
<u>3.59</u>	<u>942.7</u>	<u>6.64</u>	<u>850.8</u>
<u>3.88</u>	<u>951.6</u>	<u>7.12</u>	<u>549.3</u>
<u>4.10</u>	<u>1010.1</u>		

Test: Passenger side femur (dynamic)

Date: February 5, 1985

Vehicle: Buick LeSabre

Options: \_\_\_\_\_



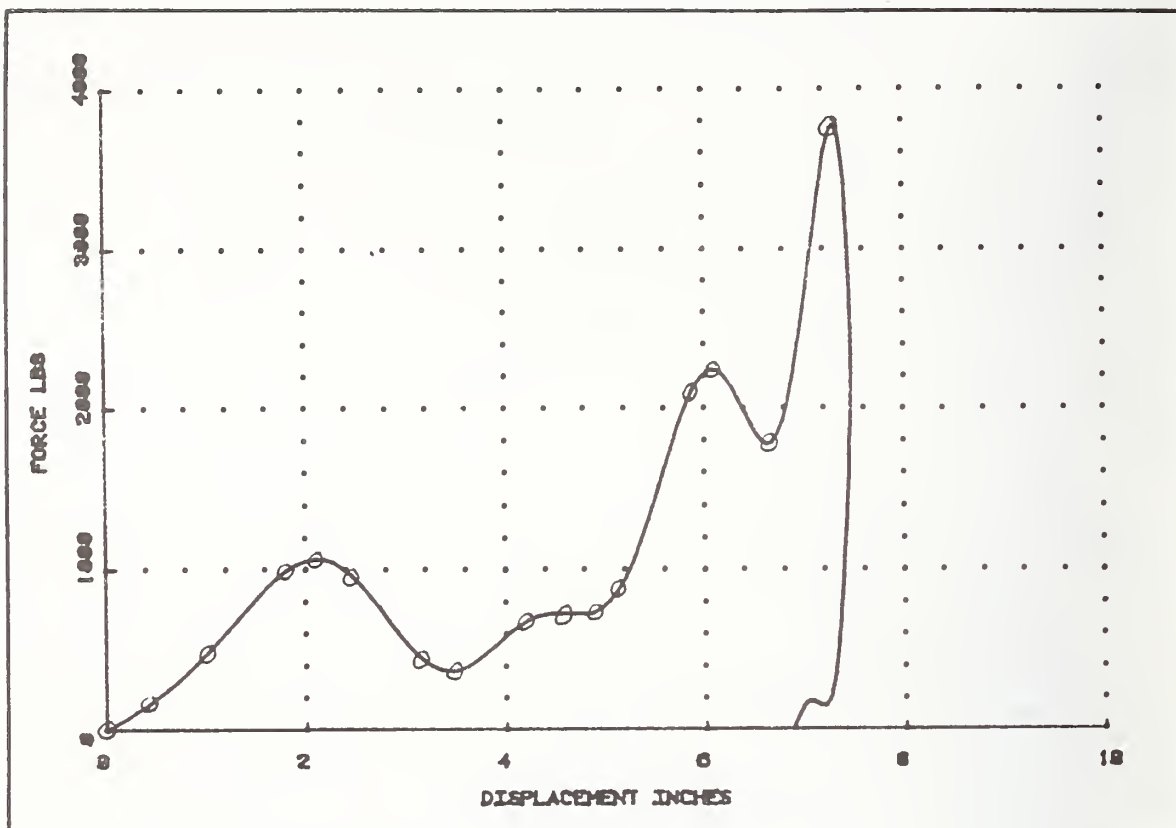
G= 1.0 R= 0.0 K= N/A

c= \_\_\_\_\_ L1= \_\_\_\_\_ L2= \_\_\_\_\_ L3= \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 10.31  $\delta_F$ = 10.78

Deflection	Force	Deflection	Force
0.0	0.0	5.91	759.5
.57	115.1	6.33	688.8
.97	162.7	6.78	673.3
1.38	166.8	7.21	660.5
2.18	109.9	8.22	496.9
2.59	123.2	8.62	486.4
3.14	270.4	8.91	517.9
4.44	956.1	10.31	1080.1
4.72	1019.1		
5.01	1014.8	10.78	0

Test: Torso (dynamic) Date: February 5, 1985  
 Vehicle: Buick LeSabre  
 Options: \_\_\_\_\_



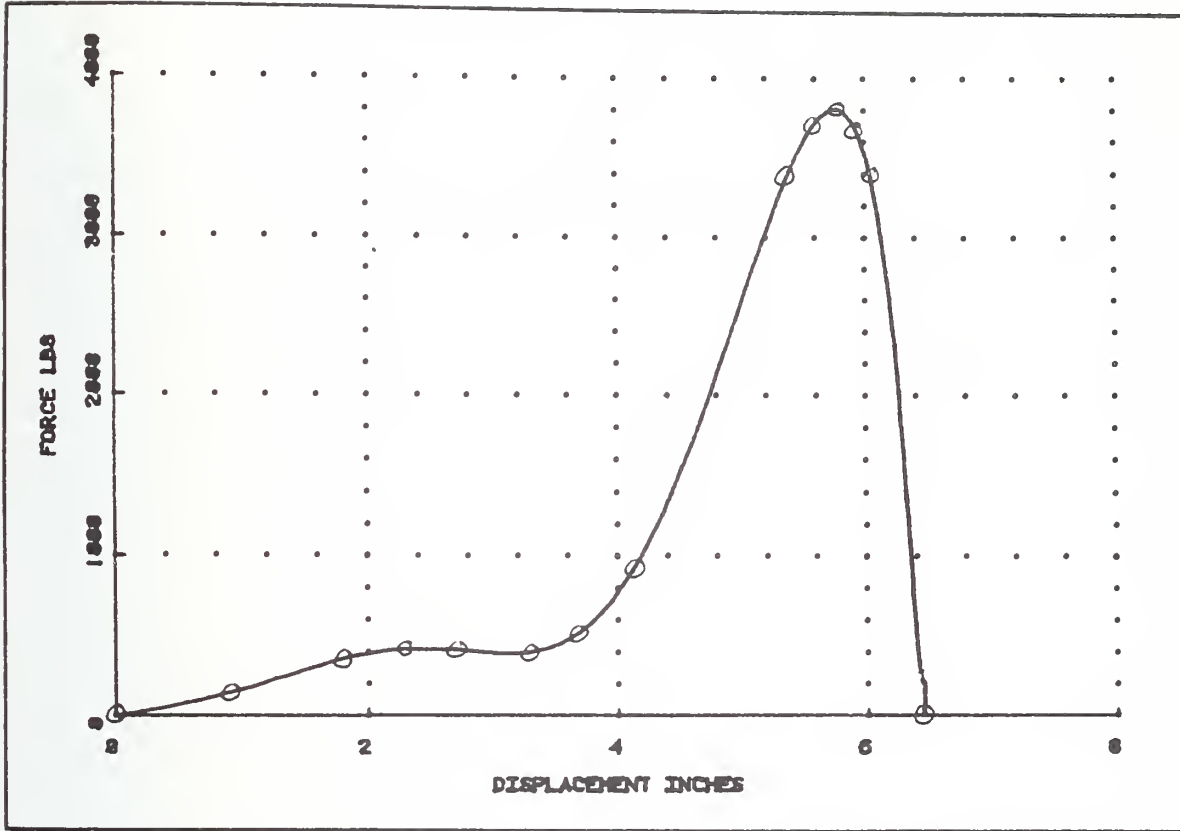
G= .919 R= .030 K= 11234.  
 c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_  
 $\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.0

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>4.22</u>	<u>685.2</u>
<u>.51</u>	<u>196.1</u>	<u>4.64</u>	<u>724.8</u>
<u>1.01</u>	<u>479.0</u>	<u>4.88</u>	<u>737.5</u>
<u>1.80</u>	<u>993.8</u>	<u>5.13</u>	<u>869.8</u>
<u>2.08</u>	<u>1064.3</u>	<u>5.88</u>	<u>2107.3</u>
<u>2.45</u>	<u>957.8</u>	<u>6.08</u>	<u>2235.4</u>
<u>3.17</u>	<u>425.4</u>	<u>6.62</u>	<u>1773.4</u>
<u>3.44</u>	<u>363.8</u>	<u>7.31</u>	<u>3770.9</u>

Test: Driver side femur (dynamic) Date: February 5, 1985

Vehicle: Buick LeSabre

Options: \_\_\_\_\_  
 \_\_\_\_\_



G= 1.0 R= 0.0 K= N/A

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 5.79  $\delta_F$ = 6.44

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>5.39</u>	<u>3414.6</u>
<u>.90</u>	<u>142.4</u>	<u>5.59</u>	<u>3708.6</u>
<u>1.80</u>	<u>354.4</u>	<u>5.79</u>	<u>3804.5</u>
<u>2.33</u>	<u>417.1</u>	<u>5.94</u>	<u>3641.9</u>
<u>2.68</u>	<u>408.3</u>	<u>6.03</u>	<u>3415.0</u>
<u>3.27</u>	<u>395.4</u>	<u>6.44</u>	<u>0.0</u>
<u>3.69</u>	<u>532.1</u>	_____	_____
<u>4.11</u>	<u>907.9</u>	_____	_____



APPENDIX D

DYNAMIC WINDSHIELD TEST RESULTS

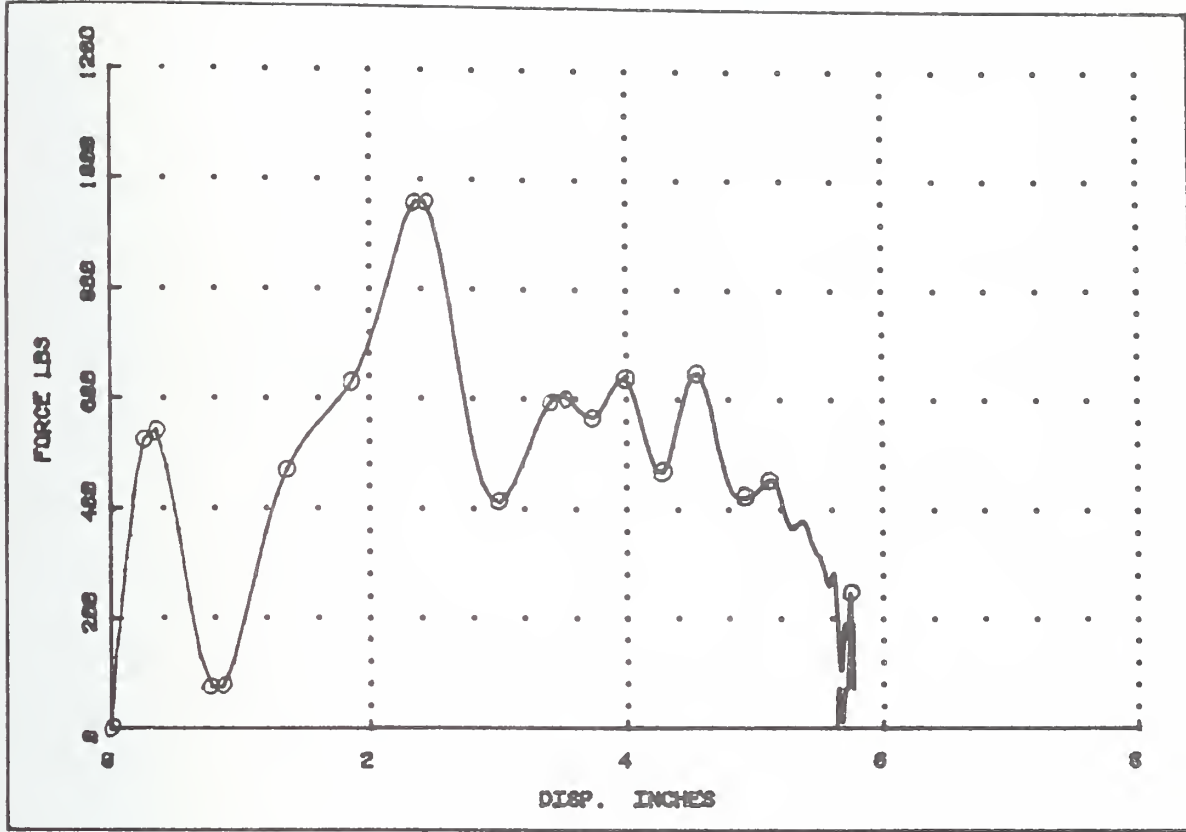




Test: Windshield (dynamic) Date: January 10, 1985

Vehicle: Chevy Celebrity

Options: \_\_\_\_\_



G= 0.977 R= 0.004 K= 601

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

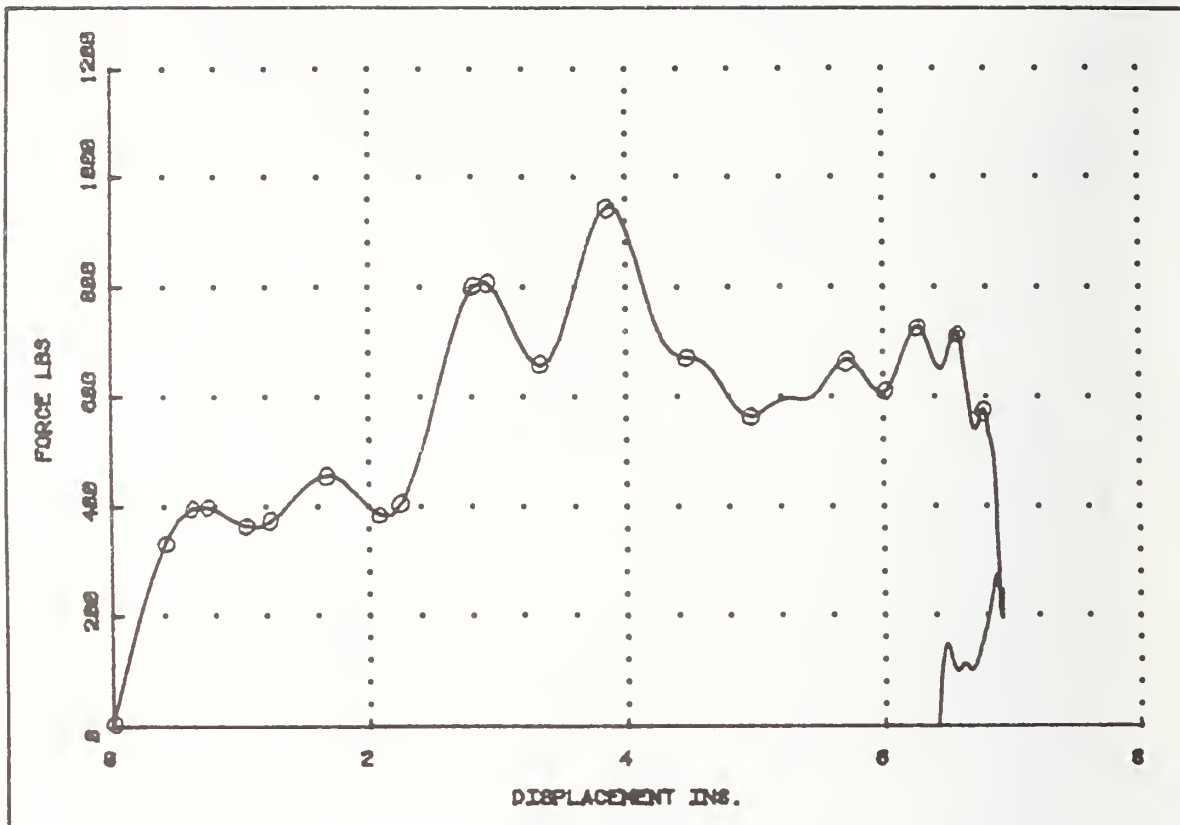
$\delta_A$ = \_\_\_\_\_  $\delta_B$ = \_\_\_\_\_  $\delta_C$ = \_\_\_\_\_  $\delta_D$ = \_\_\_\_\_  $\delta_F$ = \_\_\_\_\_

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>3.39</u>	<u>592.9</u>
<u>0.28</u>	<u>529.9</u>	<u>3.51</u>	<u>605.2</u>
<u>0.35</u>	<u>542.2</u>	<u>3.74</u>	<u>568.3</u>
<u>0.75</u>	<u>73.7</u>	<u>3.98</u>	<u>634.4</u>
<u>0.87</u>	<u>73.7</u>	<u>4.25</u>	<u>471.6</u>
<u>1.35</u>	<u>470.0</u>	<u>4.53</u>	<u>645.1</u>
<u>1.87</u>	<u>637.4</u>	<u>4.89</u>	<u>416.3</u>
<u>2.35</u>	<u>960.0</u>	<u>5.13</u>	<u>451.6</u>
<u>2.43</u>	<u>960.0</u>	<u>5.73</u>	<u>247.3</u>
<u>2.99</u>	<u>413.2</u>		

Test: Windshield (dynamic) Date: January 14, 1985

Vehicle: Datsun - Nissan 210

Options: \_\_\_\_\_



G= 0.926 R= 0.019 K= 313

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

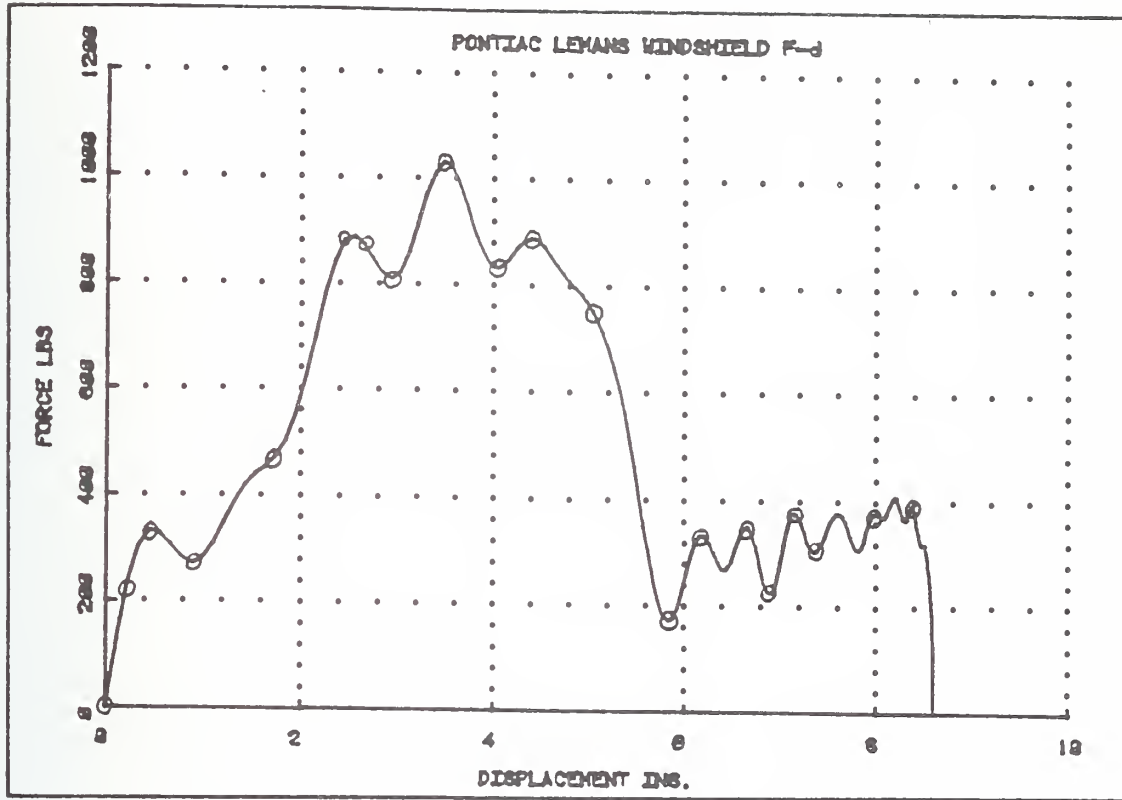
$\delta_A$ = \_\_\_\_\_  $\delta_B$ = \_\_\_\_\_  $\delta_C$ = \_\_\_\_\_  $\delta_D$ = \_\_\_\_\_  $\delta_F$ = \_\_\_\_\_

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>2.91</u>	<u>809.5</u>
<u>0.40</u>	<u>328.7</u>	<u>3.31</u>	<u>652.8</u>
<u>0.60</u>	<u>394.8</u>	<u>3.87</u>	<u>946.2</u>
<u>0.72</u>	<u>400.9</u>	<u>4.43</u>	<u>669.7</u>
<u>1.03</u>	<u>364.0</u>	<u>4.94</u>	<u>560.6</u>
<u>1.23</u>	<u>370.2</u>	<u>5.70</u>	<u>668.2</u>
<u>1.67</u>	<u>454.7</u>	<u>6.01</u>	<u>608.3</u>
<u>2.07</u>	<u>382.5</u>	<u>6.28</u>	<u>728.1</u>
<u>2.23</u>	<u>400.9</u>	<u>6.56</u>	<u>715.8</u>
<u>2.83</u>	<u>803.3</u>	<u>6.76</u>	<u>577.5</u>

Test: Windshield (dynamic) Date: January 16, 1985

Vehicle: Pontiac LeMans

Options: \_\_\_\_\_



G= 1.0 R= 0 K= N/A

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 8.39\*  $\delta_F$ = 8.6\*

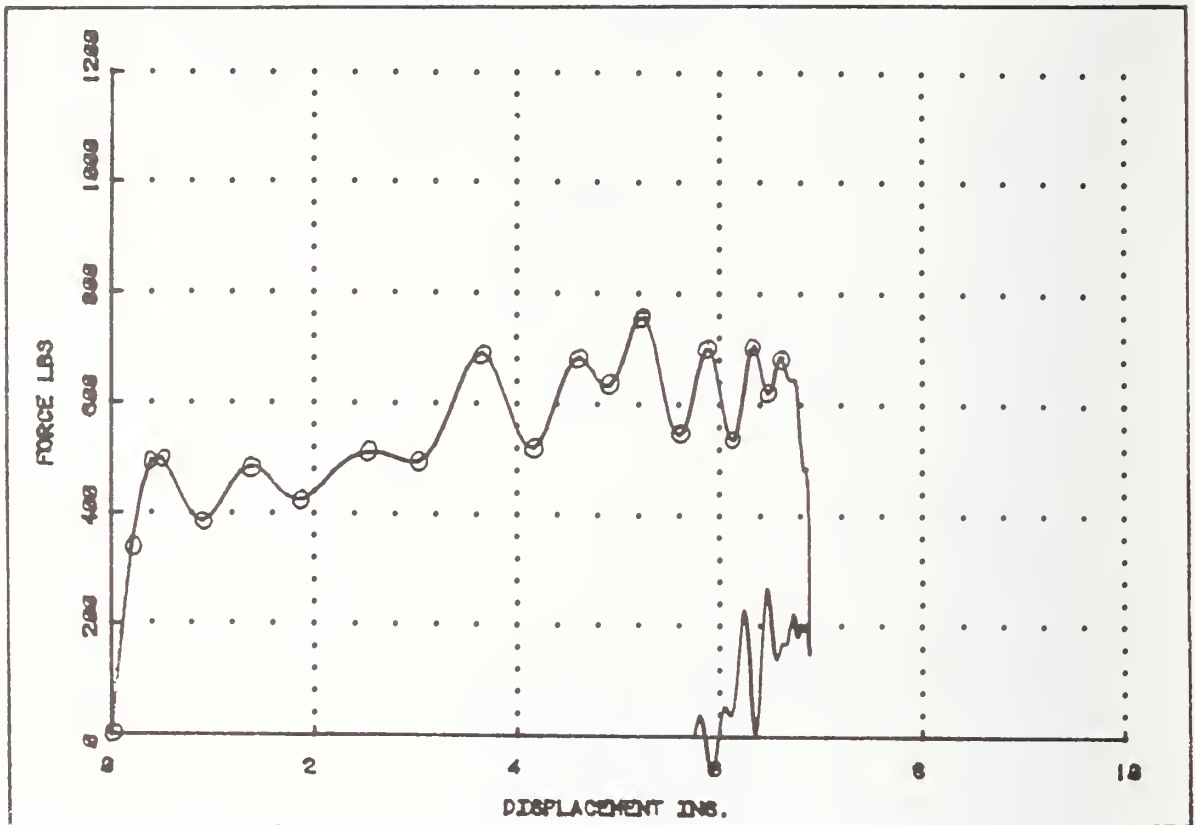
Deflection	Force	Deflection	Force
0	0	4.39	888.1
0.22	231.7	5.05	753.8
0.44	331.0	5.83	172.2
0.88	270.8	6.17	333.7
1.74	471.8	6.66	350.1
2.45	880.7	6.90	224.5
2.65	872.7	7.13	377.4
2.93	808.9	7.35	303.8
3.46	1029.0	8.00	378.6
4.03	831.4	8.39	393.2

\*Values for  $\delta_D$  and  $\delta_F$  are estimates there is no unloading due to complete penetration.

Test: Windshield (dynamic) Date: January 17, 1985

Vehicle: Chevy Nova

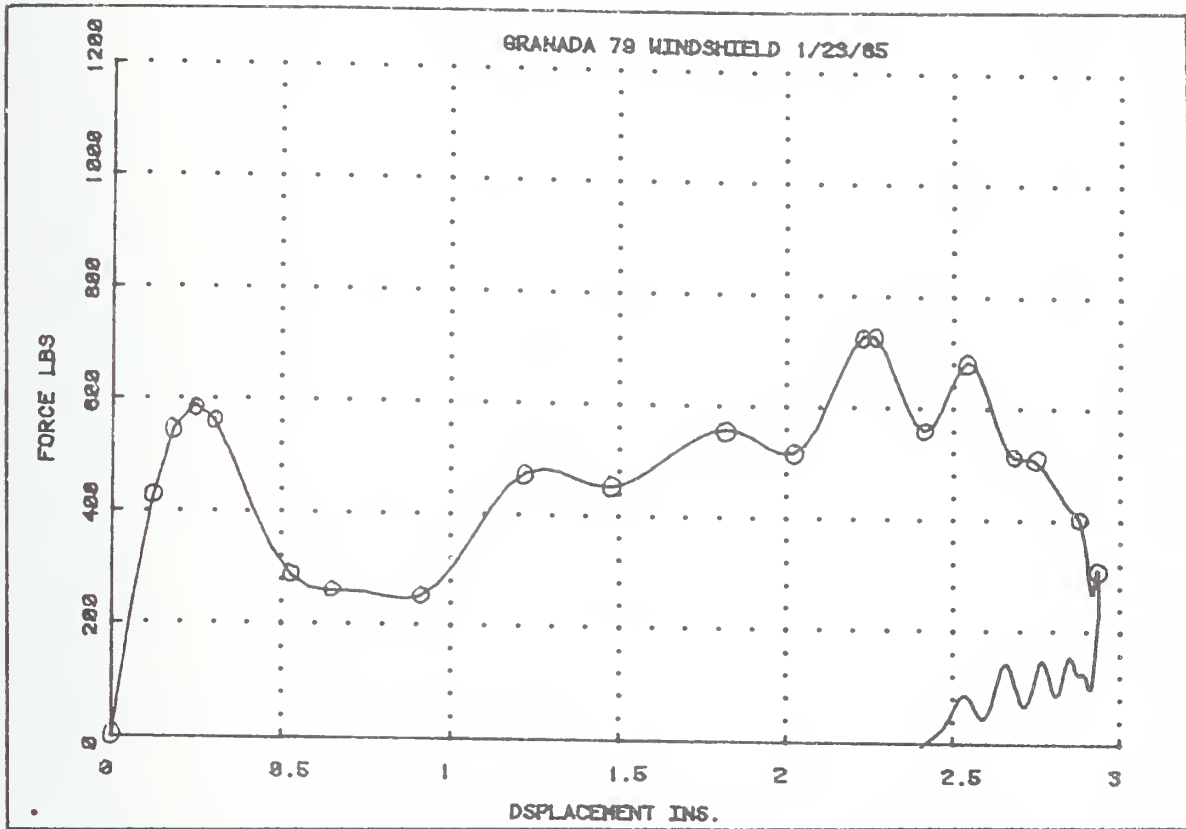
Options: \_\_\_\_\_



G= 0.834 R= 0.033 K= 257  
 c= \_\_\_\_\_ u<sub>1</sub>= \_\_\_\_\_ u<sub>2</sub>= \_\_\_\_\_ u<sub>3</sub>= \_\_\_\_\_  
 δ<sub>A</sub>= 0.0 δ<sub>B</sub>= 0.0 δ<sub>C</sub>= 0.0 δ<sub>D</sub>= 1000.0 δ<sub>F</sub>= 1000.0

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0</u>	<u>0</u>	<u>4.16</u>	<u>519.3</u>
<u>0.20</u>	<u>335.5</u>	<u>4.62</u>	<u>682.1</u>
<u>0.40</u>	<u>494.6</u>	<u>4.86</u>	<u>631.9</u>
<u>0.50</u>	<u>498.0</u>	<u>5.26</u>	<u>755.7</u>
<u>0.89</u>	<u>383.8</u>	<u>5.61</u>	<u>543.3</u>
<u>1.37</u>	<u>484.7</u>	<u>5.87</u>	<u>699.4</u>
<u>1.83</u>	<u>423.8</u>	<u>6.14</u>	<u>535.1</u>
<u>2.53</u>	<u>510.3</u>	<u>6.34</u>	<u>705.0</u>
<u>2.95</u>	<u>493.5</u>	<u>6.48</u>	<u>618.2</u>
<u>3.65</u>	<u>689.1</u>	<u>6.60</u>	<u>685.4</u>

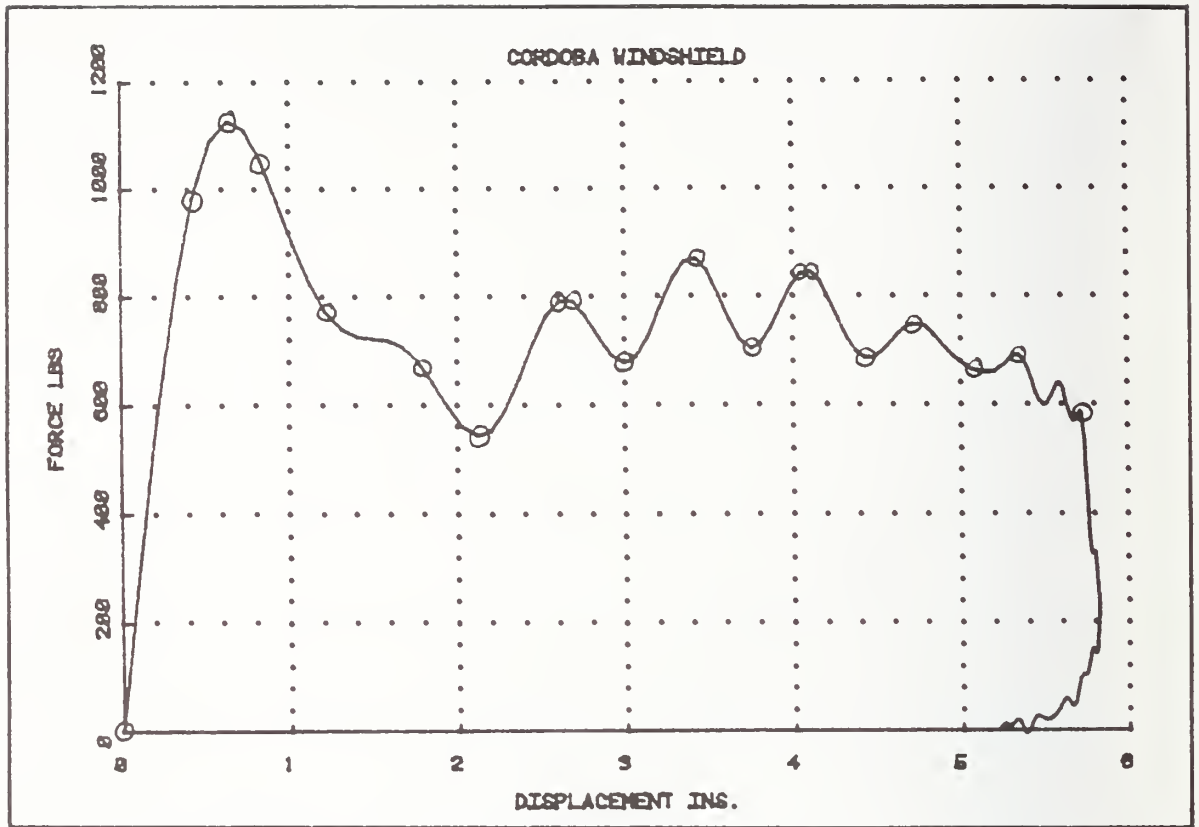
Test: Windshield (dynamic) Date: January 23, 1985  
 Vehicle: Ford Granada  
 Options: \_\_\_\_\_



G= 0.761 R= 0.032 K= 783  
 C= \_\_\_\_\_ B1= \_\_\_\_\_ B2= \_\_\_\_\_ B3= \_\_\_\_\_  
 δ<sub>A</sub>= 0.0 δ<sub>B</sub>= 0.0 δ<sub>C</sub>= 0.0 δ<sub>D</sub>= 1000.0 δ<sub>E</sub>= 1000.0

Deflection	Force	Deflection	Force
0.0	0.0	1.82	557.0
0.12	424.6	2.02	516.9
0.18	546.7	2.23	728.2
0.24	589.1	2.26	725.5
0.30	562.4	2.41	559.8
0.53	286.7	2.54	683.0
0.64	258.8	2.68	512.5
0.91	252.9	2.74	505.7
1.22	475.5	2.88	403.5
1.46	451.4	2.93	311.1

Test: Windshield (dynamic) Date: January 25, 1985  
 Vehicle: 1979 Chrysler Cordoba  
 Options: \_\_\_\_\_



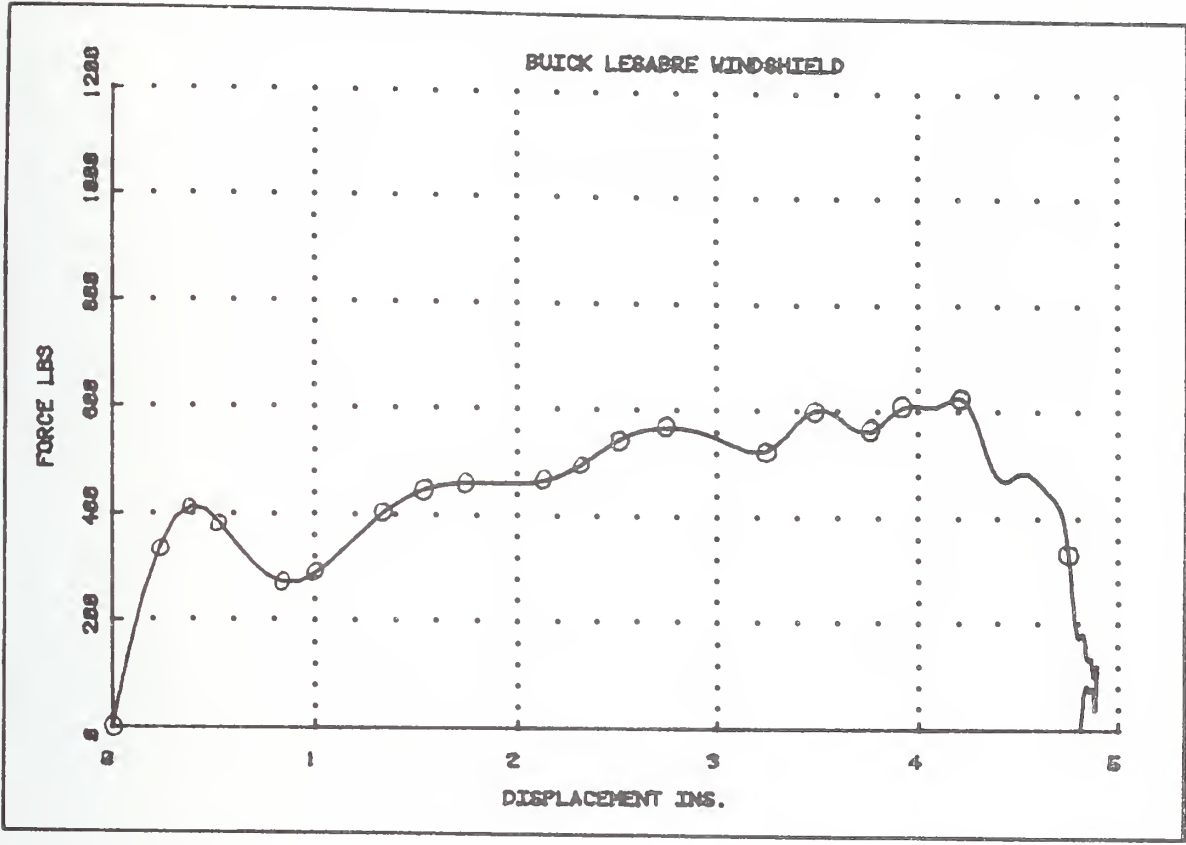
G= 0.896 R= 0.007 K= 966  
 c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_  
 $\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.0

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0</u>	<u>0</u>	<u>3.42</u>	<u>869.9</u>
<u>0.43</u>	<u>987.6</u>	<u>3.75</u>	<u>702.9</u>
<u>0.64</u>	<u>1126.1</u>	<u>4.05</u>	<u>841.3</u>
<u>0.84</u>	<u>1052.3</u>	<u>4.11</u>	<u>844.2</u>
<u>1.22</u>	<u>769.7</u>	<u>4.42</u>	<u>684.4</u>
<u>1.77</u>	<u>677.1</u>	<u>4.75</u>	<u>746.7</u>
<u>2.11</u>	<u>541.7</u>	<u>5.13</u>	<u>657.5</u>
<u>2.61</u>	<u>791.8</u>	<u>5.35</u>	<u>689.3</u>
<u>2.69</u>	<u>790.3</u>	<u>5.72</u>	<u>585.0</u>
<u>2.99</u>	<u>675.4</u>		

Test: Windshield (dynamic) Date: January 28, 1985

Vehicle: Buick LeSabre

Options: \_\_\_\_\_  
 \_\_\_\_\_



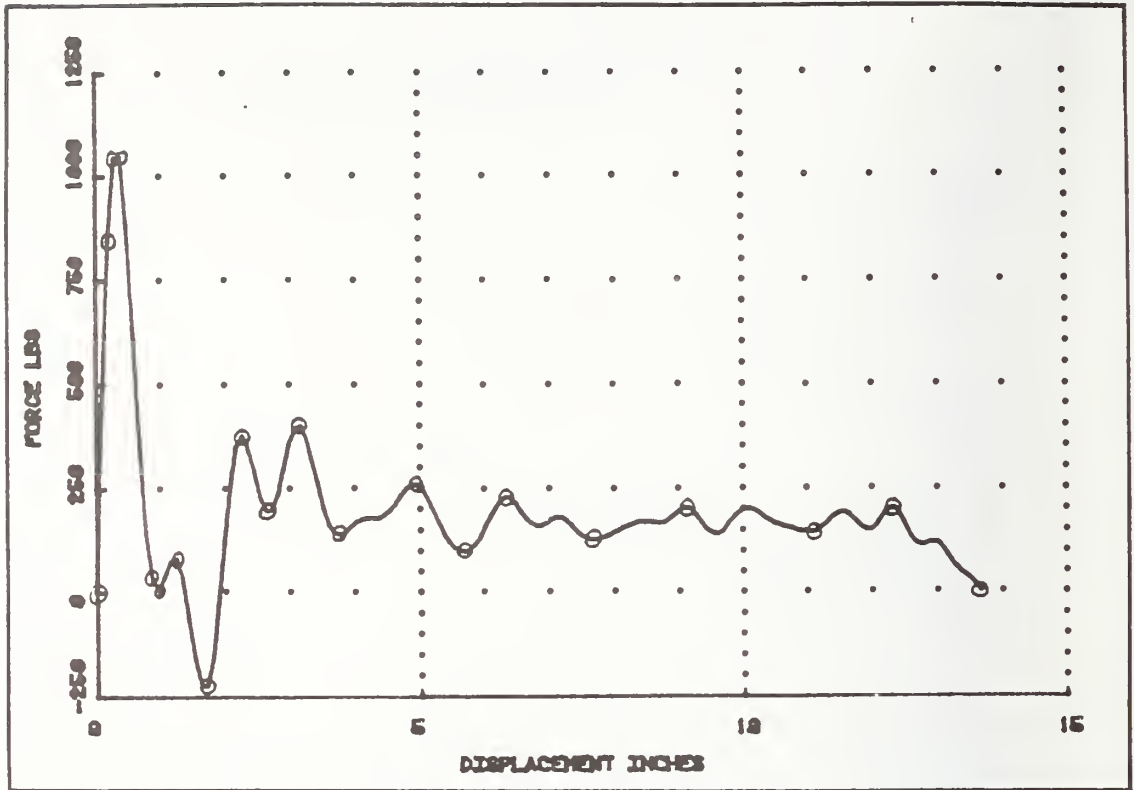
G= 0.983 R= 0.002 K= 1247  
 c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_  
 $\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.0

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>2.33</u>	<u>498.2</u>
<u>0.23</u>	<u>337.2</u>	<u>2.51</u>	<u>542.1</u>
<u>0.46</u>	<u>405.7</u>	<u>2.74</u>	<u>566.3</u>
<u>0.54</u>	<u>378.5</u>	<u>3.21</u>	<u>522.2</u>
<u>0.84</u>	<u>270.6</u>	<u>3.49</u>	<u>600.9</u>
<u>0.98</u>	<u>283.3</u>	<u>3.74</u>	<u>560.8</u>
<u>1.34</u>	<u>403.5</u>	<u>3.93</u>	<u>608.2</u>
<u>1.55</u>	<u>448.2</u>	<u>4.22</u>	<u>625.1</u>
<u>1.75</u>	<u>461.3</u>	<u>4.75</u>	<u>358.4</u>
<u>2.08</u>	<u>463.3</u>		

Test: Windshield (dynamic) Date: February 15, 1985

Vehicle: V. W. Rabbit

Options: Windshield was mounted using a gasket with no adhesive.



G= 1.0 R= 0.0 K= N/A

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 12.67  $\delta_F$ = 12.93

Deflection	Force	Deflection	Force
<u>0.0</u>	<u>0.0</u>	<u>3.16</u>	<u>398.6</u>
<u>0.20</u>	<u>846.0</u>	<u>3.77</u>	<u>136.5</u>
<u>0.30</u>	<u>1044.6</u>	<u>4.96</u>	<u>258.0</u>
<u>0.39</u>	<u>1047.3</u>	<u>5.69</u>	<u>97.9</u>
<u>0.87</u>	<u>27.8</u>	<u>6.33</u>	<u>228.9</u>
<u>0.96</u>	<u>3.5</u>	<u>7.63</u>	<u>126.2</u>
<u>1.24</u>	<u>78.6</u>	<u>9.08</u>	<u>202.8</u>
<u>1.70</u>	<u>-228.2</u>	<u>11.02</u>	<u>144.1</u>
<u>2.26</u>	<u>374.9</u>	<u>12.30</u>	<u>201.0</u>
<u>2.62</u>	<u>194.7</u>	<u>13.67</u>	<u>0.0</u>

Entire windshield was separated from mounting  $\delta_D$  and  $\delta_F$  are estimated from above data.



APPENDIX E

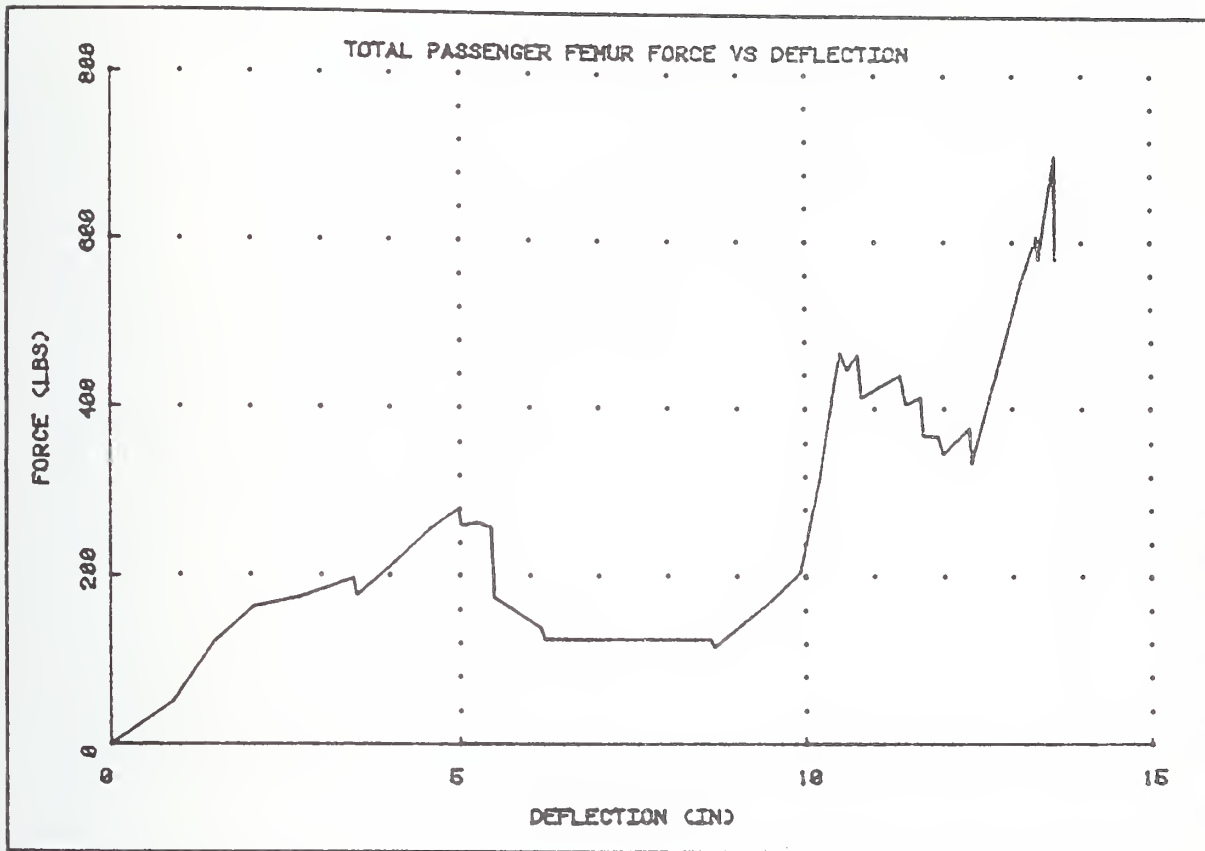
PARAMETRIC INSTRUMENT PANEL TEST RESULTS



Test: Passenger Femur Date: \_\_\_\_\_

Vehicle: Plymouth Volare

Options: Loading Point Variation Test



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

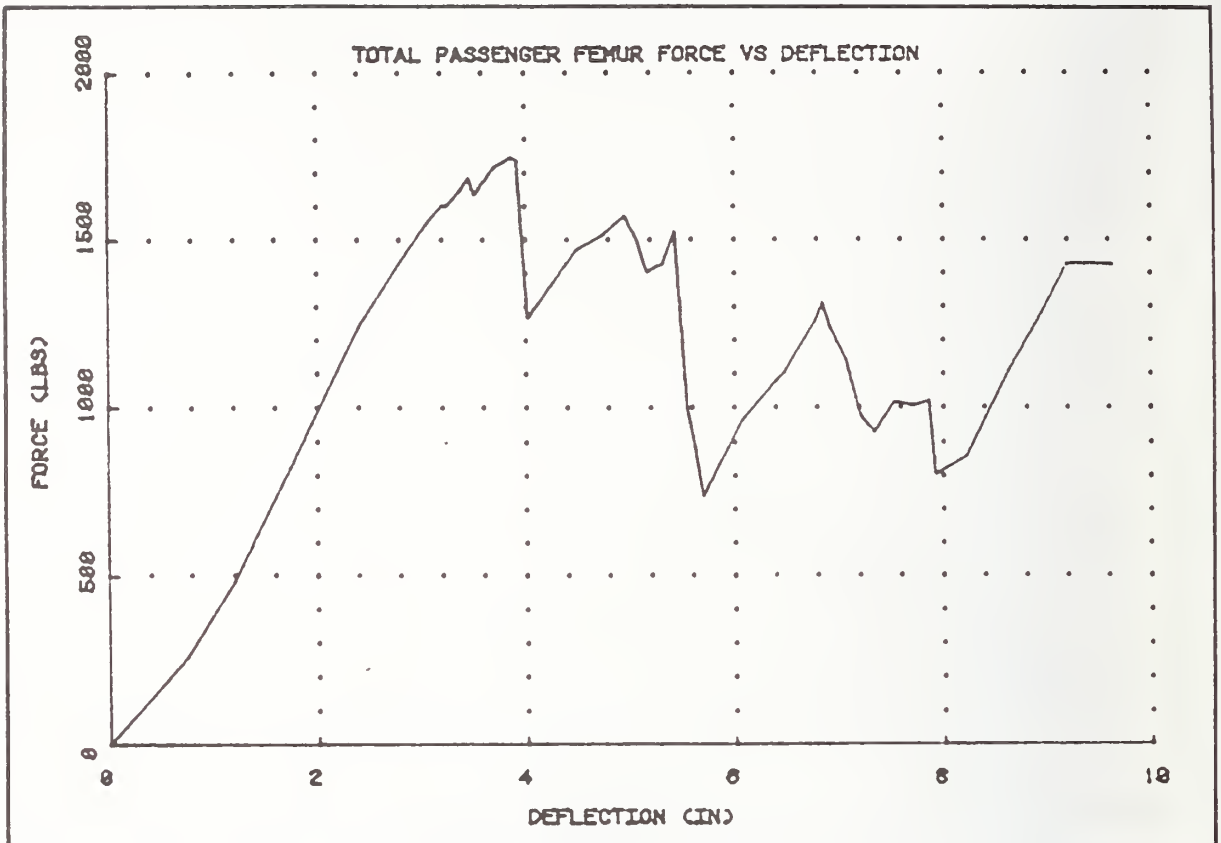
$\delta_A$ = \_\_\_\_\_  $\delta_B$ = \_\_\_\_\_  $\delta_C$ = \_\_\_\_\_  $\delta_D$ = \_\_\_\_\_  $\delta_F$ = \_\_\_\_\_

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Passenger Femur Date: \_\_\_\_\_

Vehicle: Honda Civic

Options: Loading Point Variation Test



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = \_\_\_\_\_  $\delta_B$ = \_\_\_\_\_  $\delta_C$ = \_\_\_\_\_  $\delta_D$ = \_\_\_\_\_  $\delta_F$ = \_\_\_\_\_

Deflection

Force

Deflection

Force

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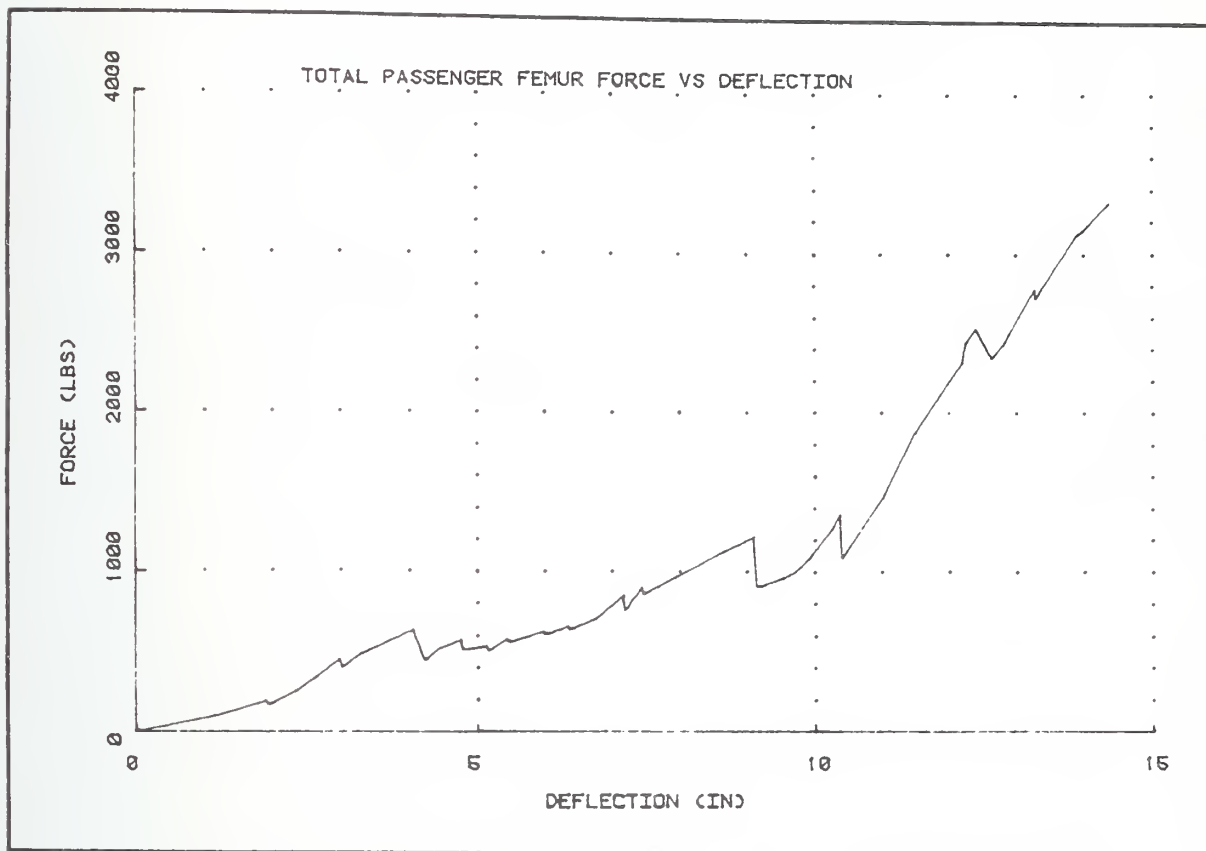
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Test: Passenger Femur Date: \_\_\_\_\_

Vehicle: Ford LTD

Options: Loading Point Variation Test



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

C= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

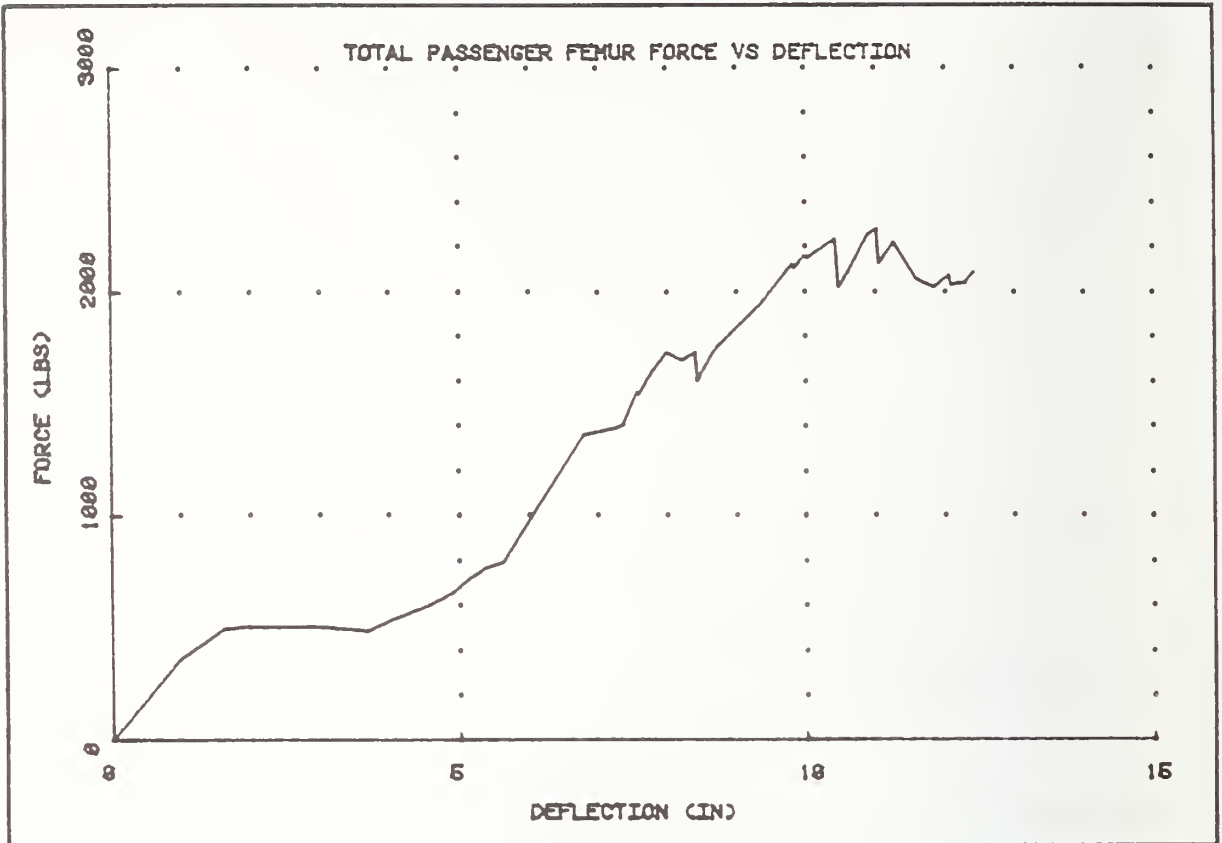
$\delta_A$ = \_\_\_\_\_  $\delta_B$ = \_\_\_\_\_  $\delta_C$ = \_\_\_\_\_  $\delta_D$ = \_\_\_\_\_  $\delta_F$ = \_\_\_\_\_

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
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_____	_____	_____	_____
_____	_____	_____	_____

Test: Total Passenger Femurs Date: \_\_\_\_\_

Vehicle: Chevy Monza

Options: Loading Point Variation Test



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

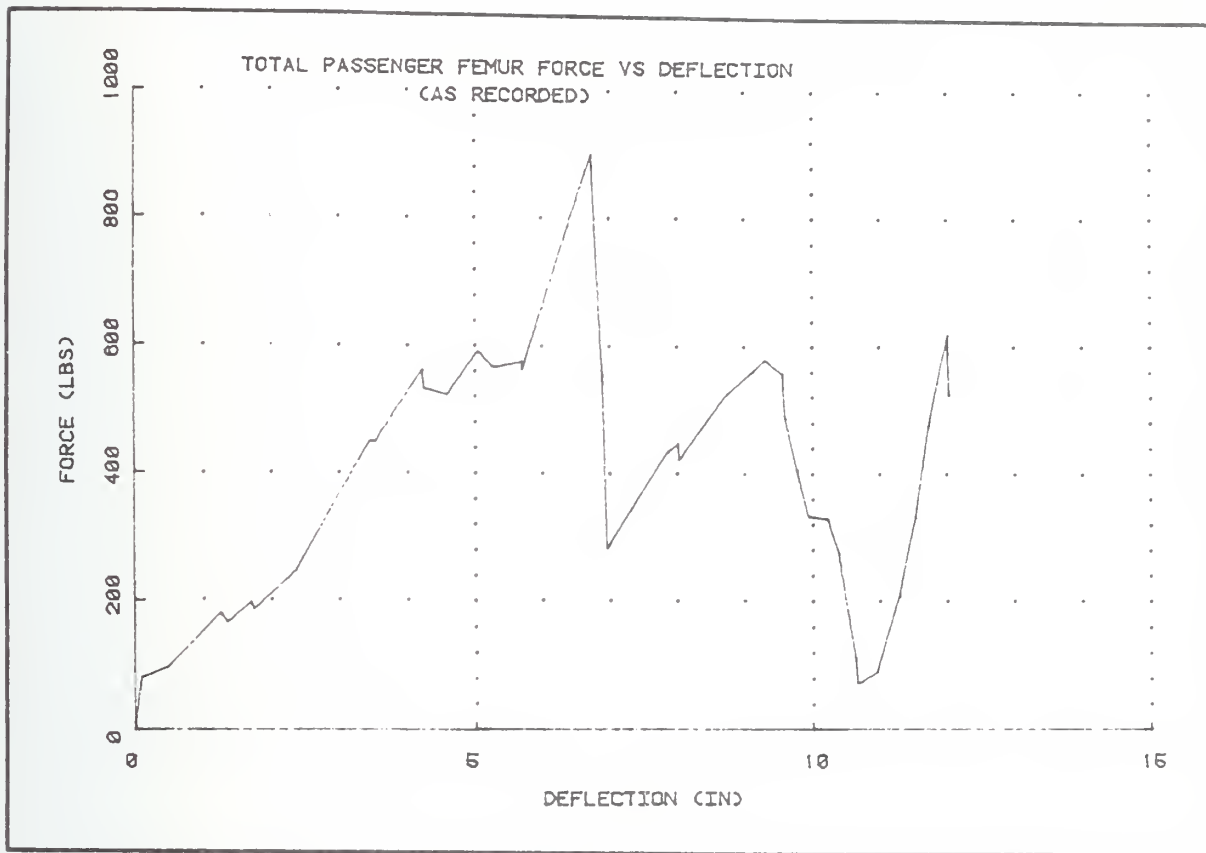
$\delta_A$ = \_\_\_\_\_  $\delta_B$ = \_\_\_\_\_  $\delta_C$ = \_\_\_\_\_  $\delta_D$ = \_\_\_\_\_  $\delta_F$ = \_\_\_\_\_

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
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Test: Passenger Femur Date: \_\_\_\_\_

Vehicle: Plymouth Volare

Options: Loading Angle Variation Test



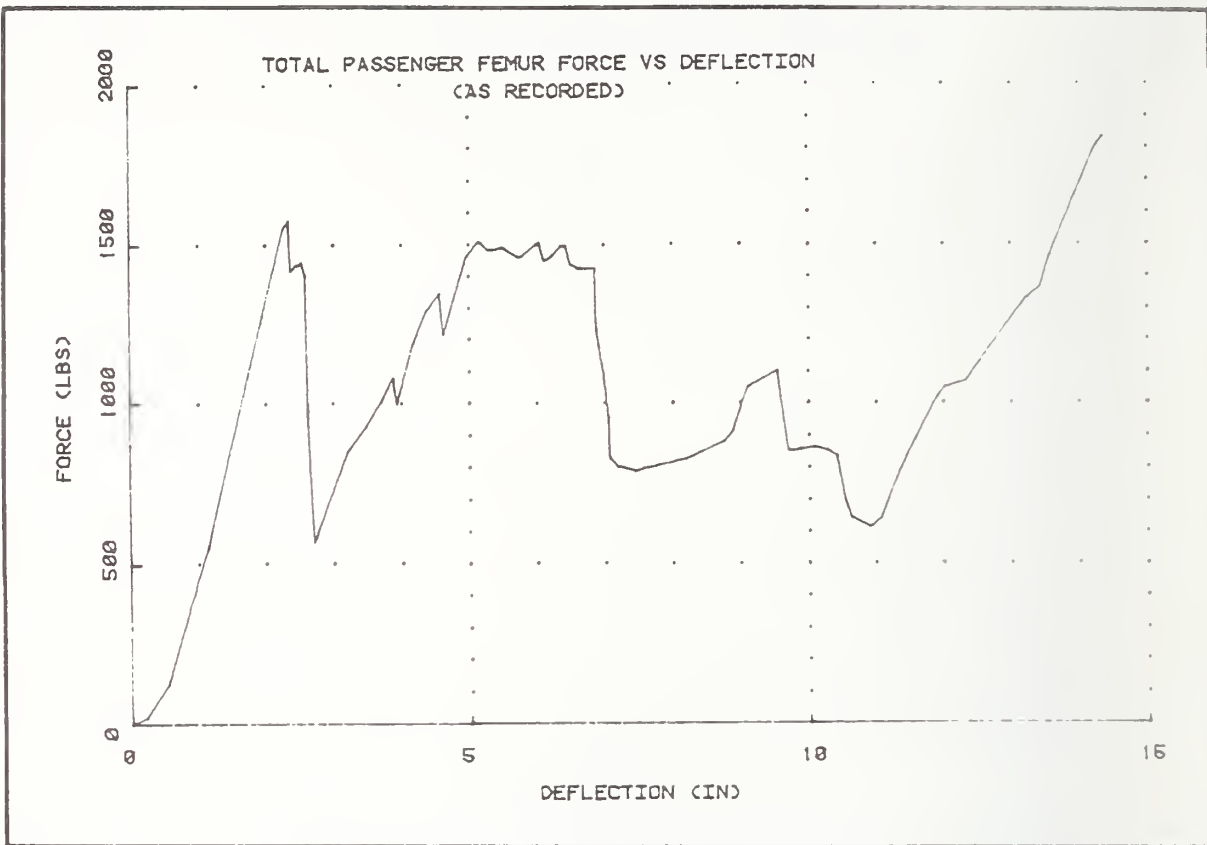
G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = \_\_\_\_\_  $\delta_B$ = \_\_\_\_\_  $\delta_C$ = \_\_\_\_\_  $\delta_D$ = \_\_\_\_\_  $\delta_F$ = \_\_\_\_\_

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
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_____	_____	_____	_____
_____	_____	_____	_____

Test: Passenger Femur Date: \_\_\_\_\_  
 Vehicle: Honda Civic  
 Options: Loading Angle Variation Test



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_  
 c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_  
 $\delta_A$ = \_\_\_\_\_  $\delta_B$ = \_\_\_\_\_  $\delta_C$ = \_\_\_\_\_  $\delta_D$ = \_\_\_\_\_  $\delta_F$ = \_\_\_\_\_

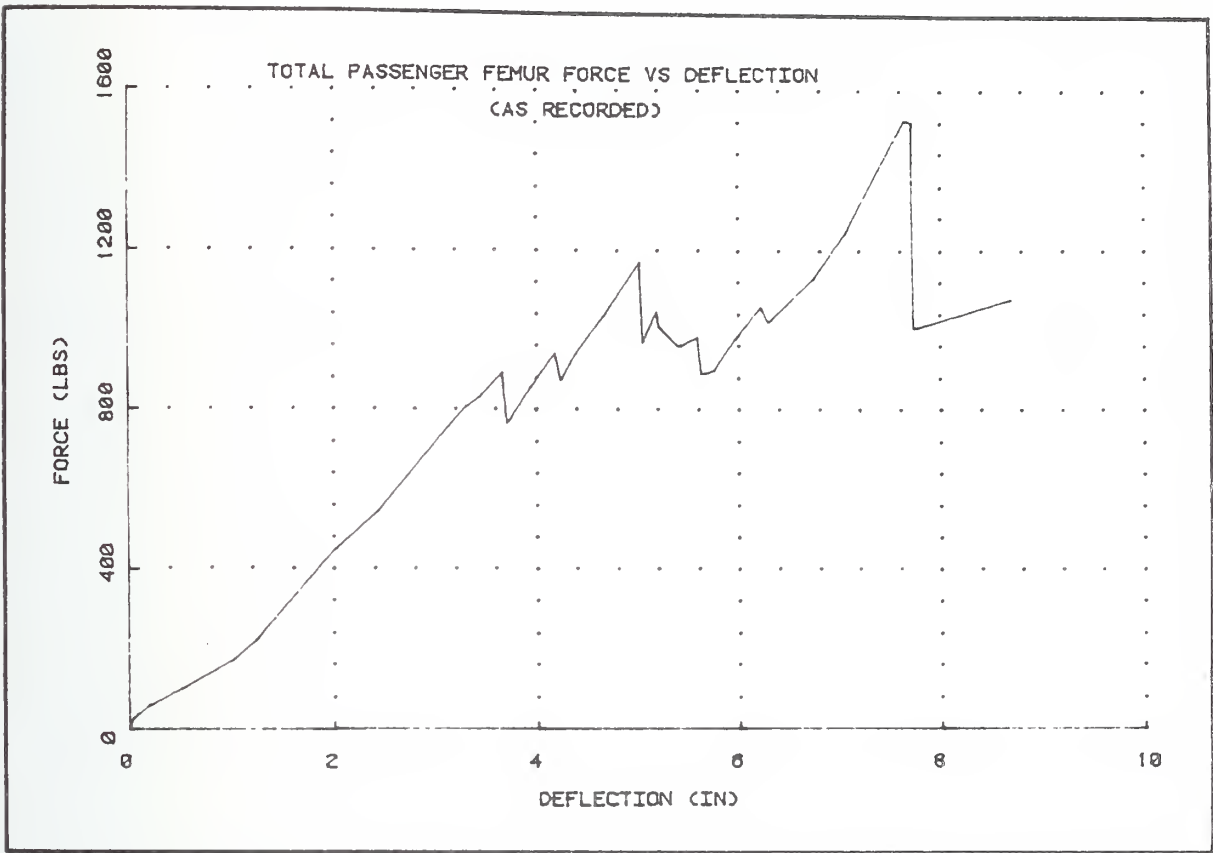
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
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Test: Passenger Femur Date: \_\_\_\_\_

Vehicle: Ford LTD

Options: Loading Angle Variation Test



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

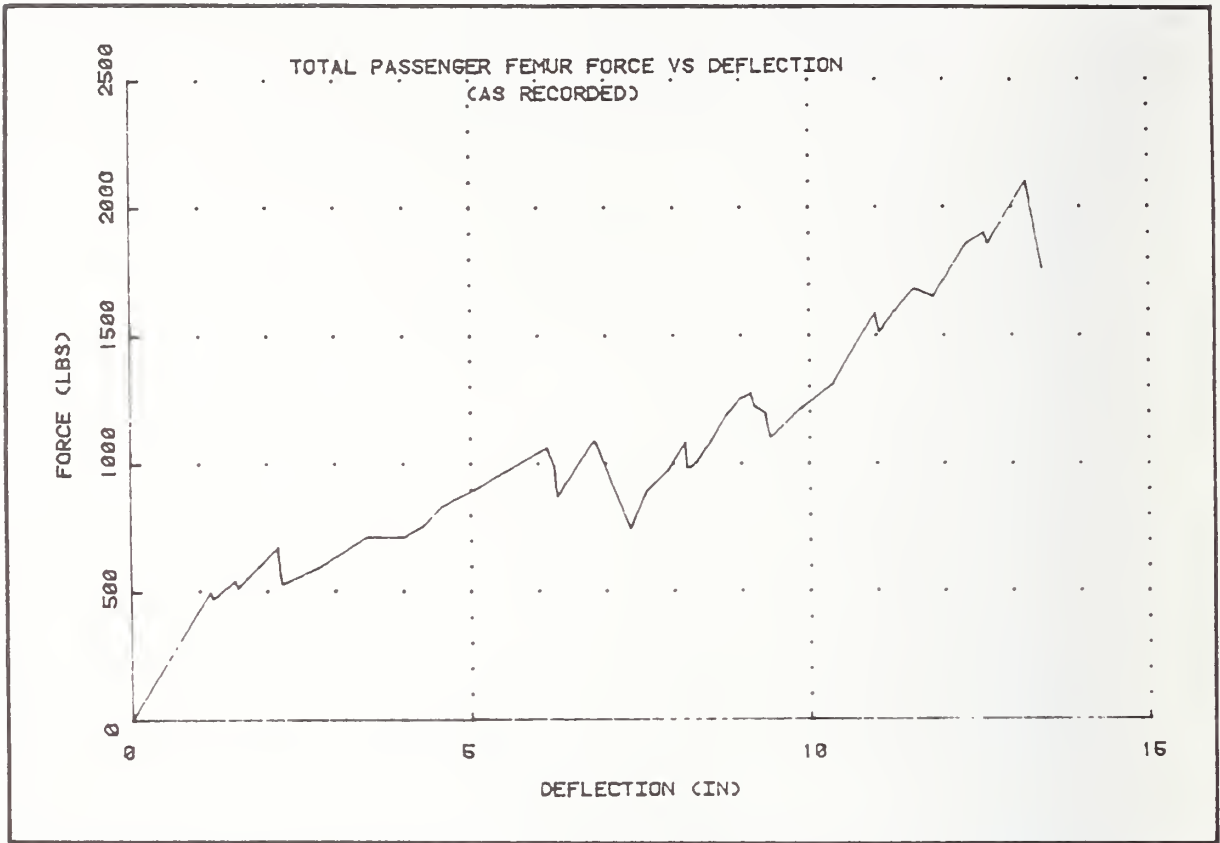
$\delta_A$ = \_\_\_\_\_  $\delta_B$ = \_\_\_\_\_  $\delta_C$ = \_\_\_\_\_  $\delta_D$ = \_\_\_\_\_  $\delta_F$ = \_\_\_\_\_

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
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_____	_____	_____	_____
_____	_____	_____	_____

Test: Passenger Femur Date: \_\_\_\_\_

Vehicle: Chevy Monza

Options: Loading Angle Variation Test



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = \_\_\_\_\_  $\delta_B$ = \_\_\_\_\_  $\delta_C$ = \_\_\_\_\_  $\delta_D$ = \_\_\_\_\_  $\delta_F$ = \_\_\_\_\_

Deflection

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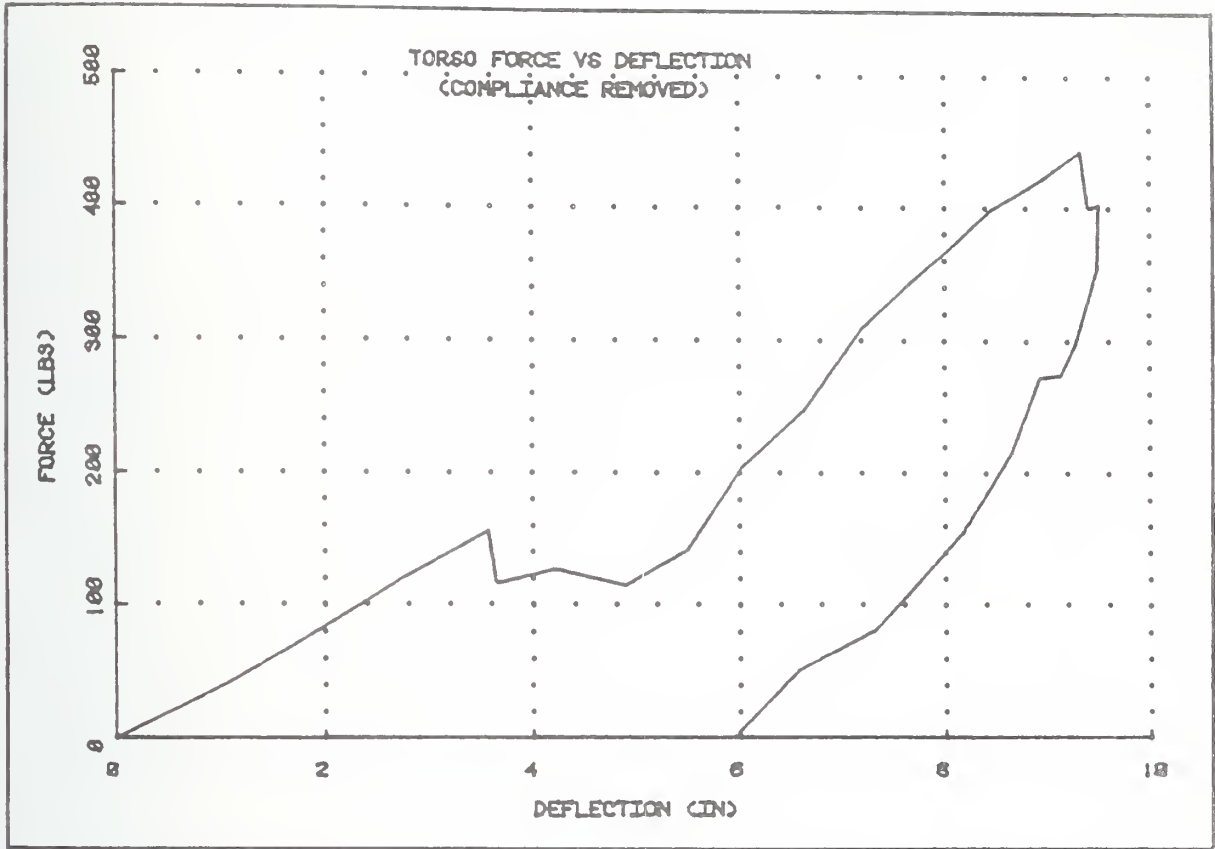
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Test: Torso Date: \_\_\_\_\_

Vehicle: Plymouth Volare

Options: Loading Point Variation Test



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

C= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

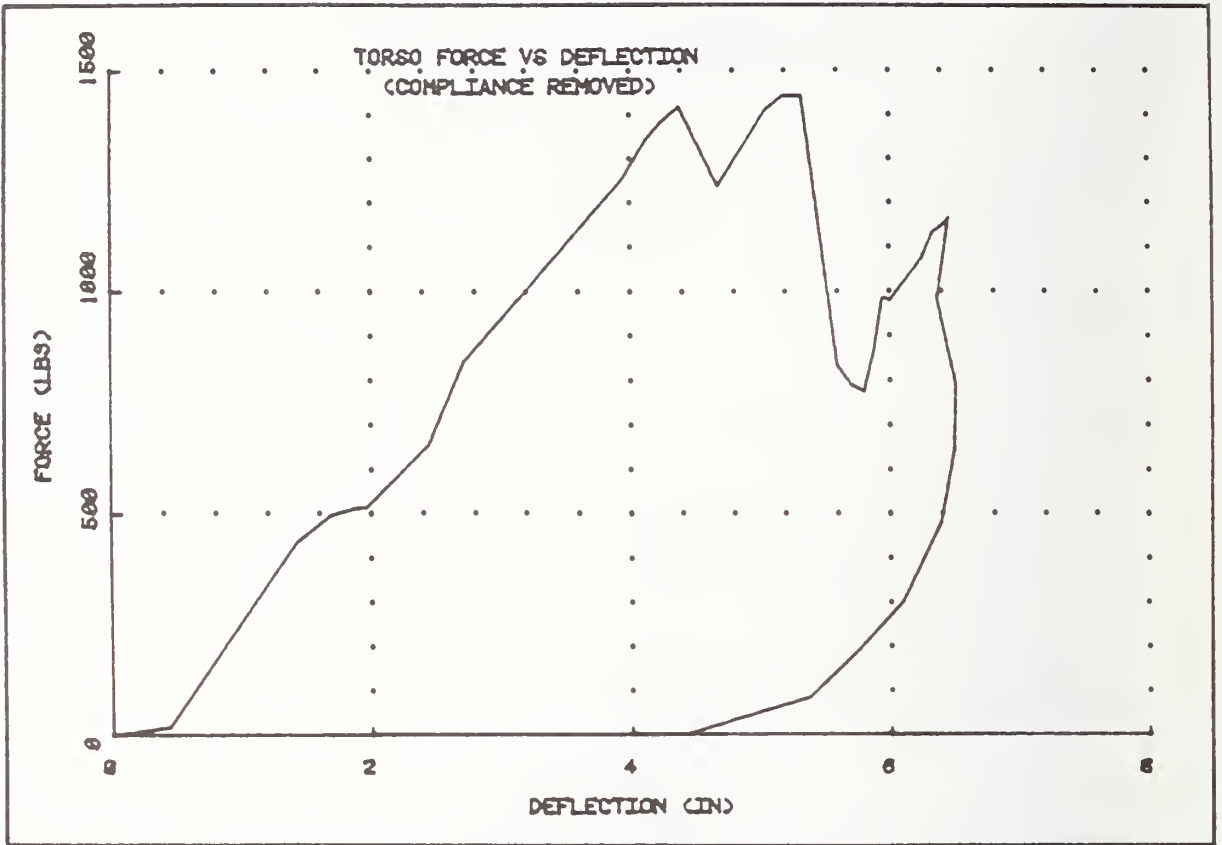
$\delta_A$ = \_\_\_\_\_  $\delta_B$ = \_\_\_\_\_  $\delta_C$ = \_\_\_\_\_  $\delta_D$ = \_\_\_\_\_  $\delta_F$ = \_\_\_\_\_

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
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Test: Torso Date: \_\_\_\_\_

Vehicle: Honda Civic

Options: Loading Point Variation Test



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

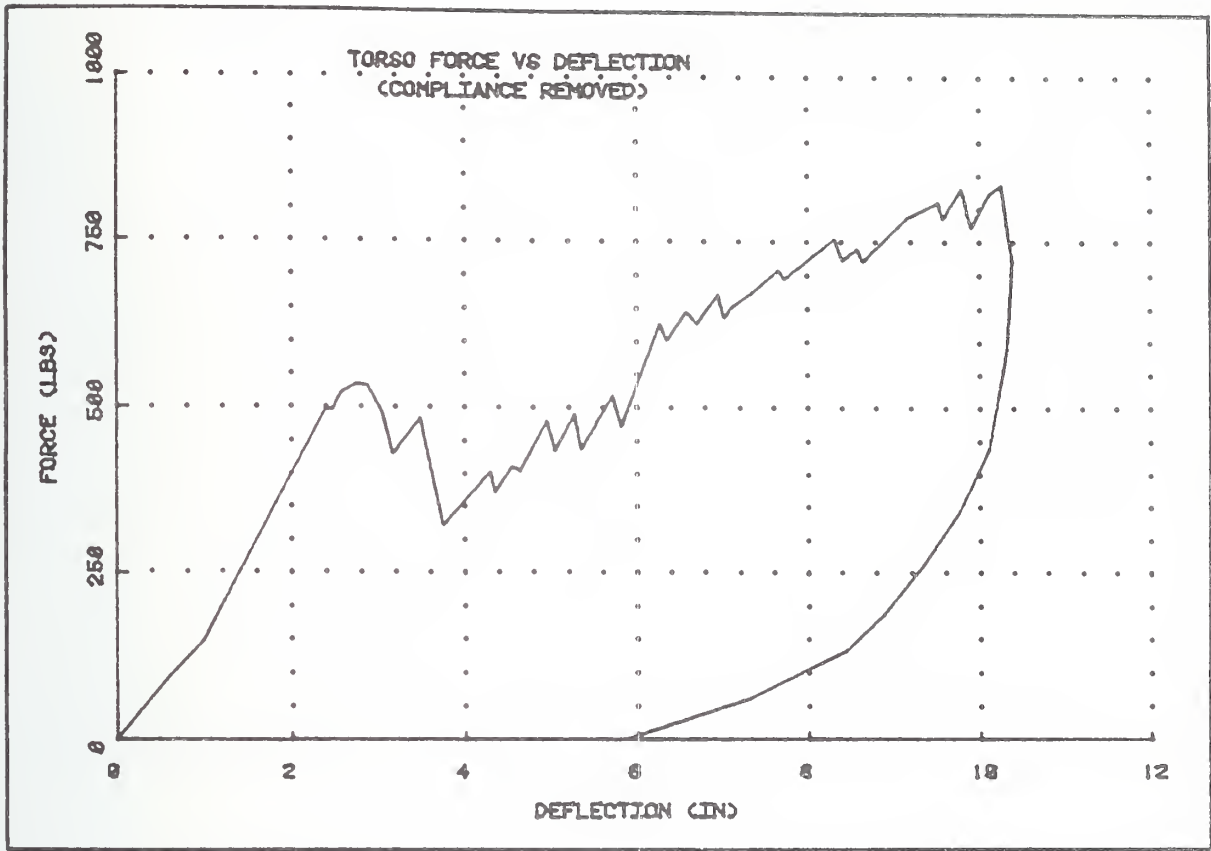
$\delta_A$ = \_\_\_\_\_  $\delta_B$ = \_\_\_\_\_  $\delta_C$ = \_\_\_\_\_  $\delta_D$ = \_\_\_\_\_  $\delta_F$ = \_\_\_\_\_

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
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Test: Torso Date: \_\_\_\_\_

Vehicle: Ford LTD

Options: Loading Point Variation Test



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

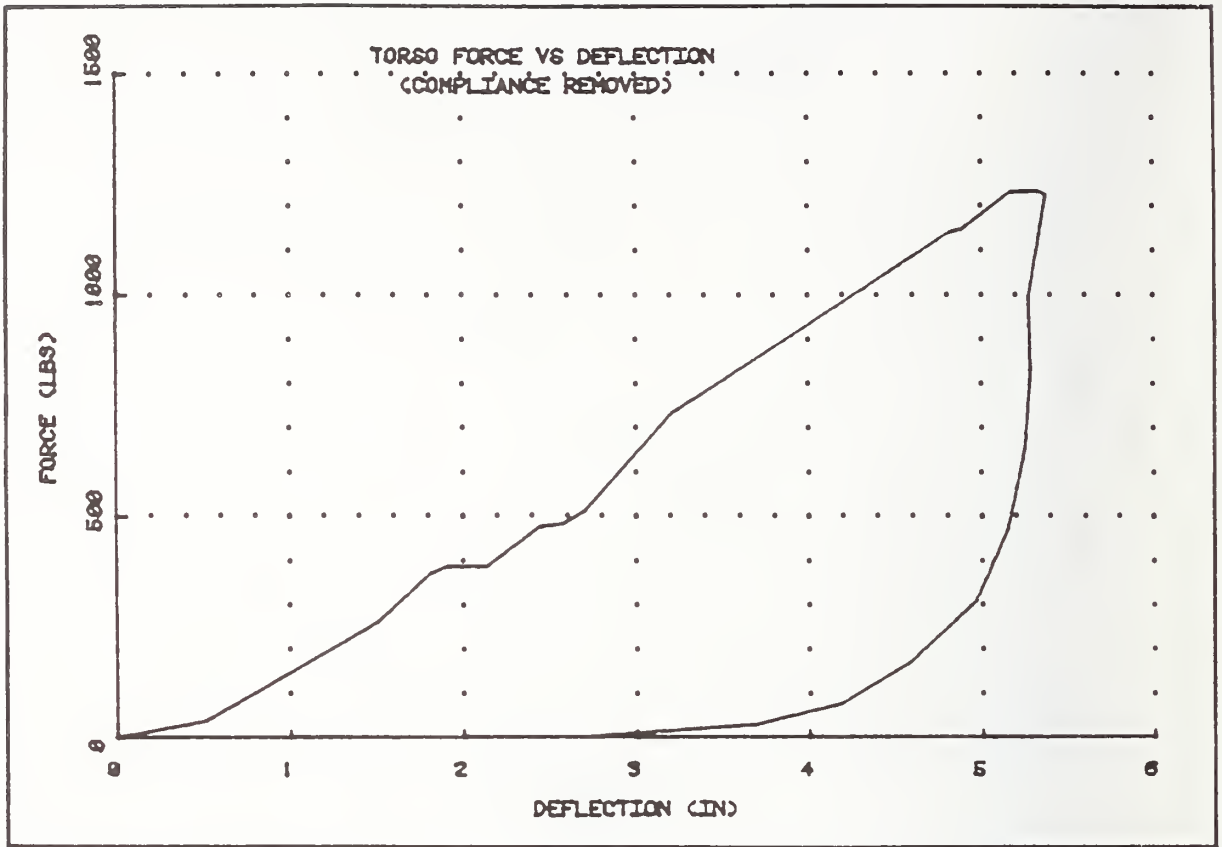
$\delta_A$ = \_\_\_\_\_  $\delta_B$ = \_\_\_\_\_  $\delta_C$ = \_\_\_\_\_  $\delta_D$ = \_\_\_\_\_  $\delta_F$ = \_\_\_\_\_

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
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_____	_____	_____	_____

Test: Torso Date: \_\_\_\_\_

Vehicle: Chevy Monza

Options: Loading Point Variation Test



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = \_\_\_\_\_  $\delta_B$ = \_\_\_\_\_  $\delta_C$ = \_\_\_\_\_  $\delta_D$ = \_\_\_\_\_  $\delta_F$ = \_\_\_\_\_

Deflection

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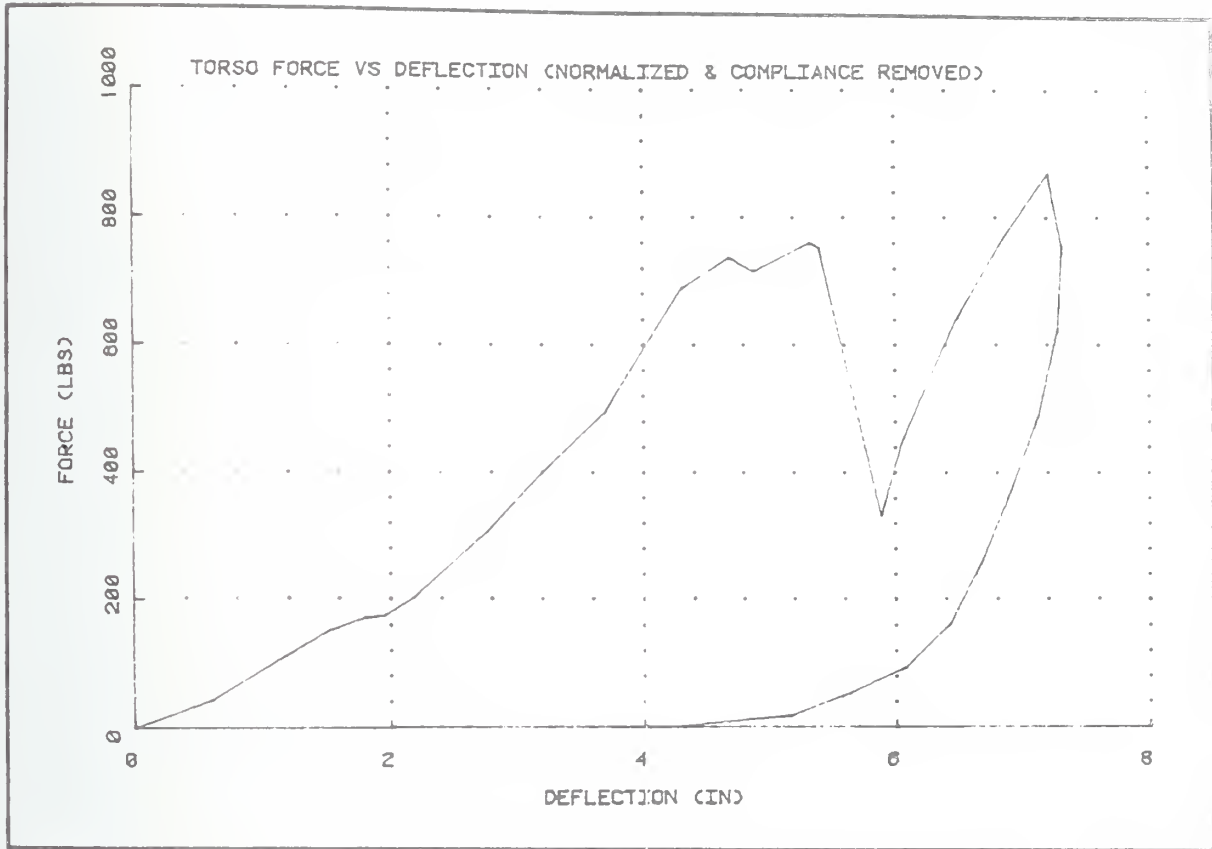
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Test: Torso Date: \_\_\_\_\_

Vehicle: Plymouth Volare

Options: Loading Angle Variation Test



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

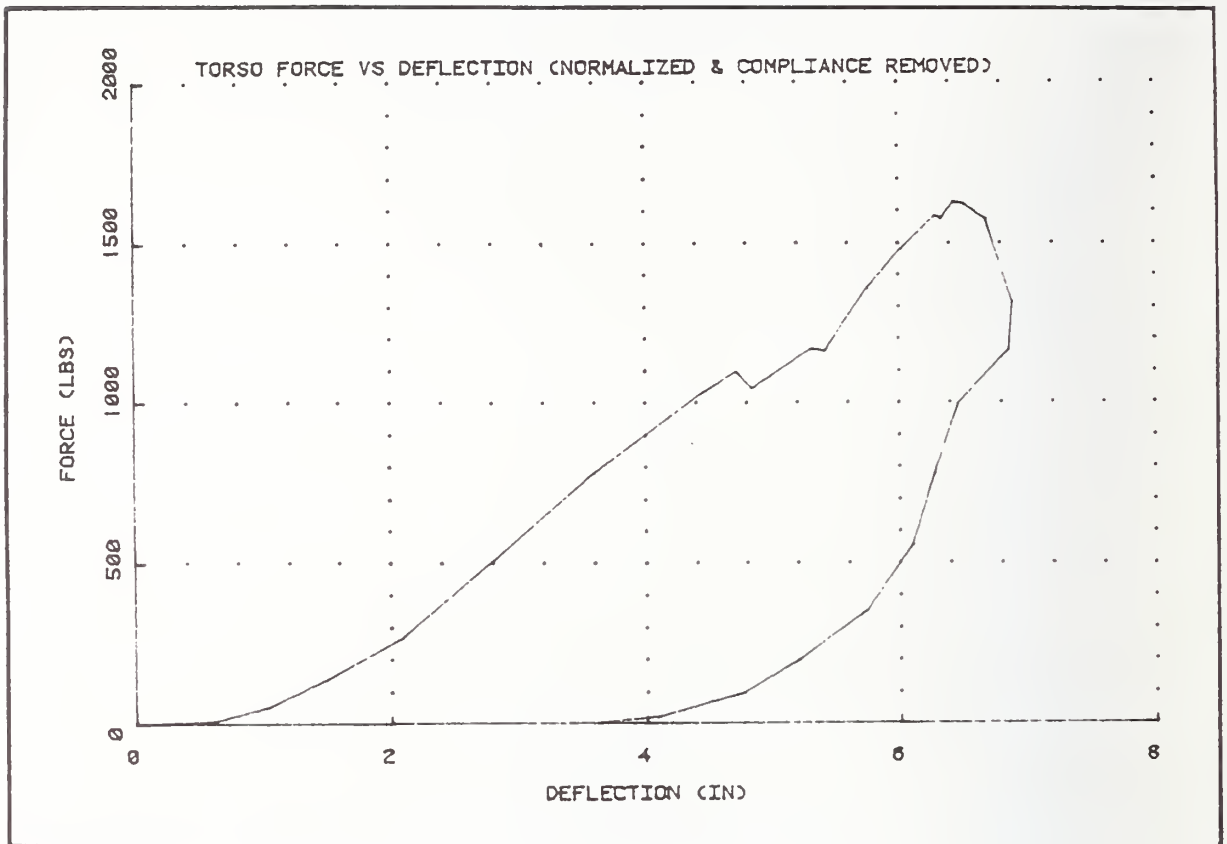
$\delta_A$ = \_\_\_\_\_  $\delta_B$ = \_\_\_\_\_  $\delta_C$ = \_\_\_\_\_  $\delta_D$ = \_\_\_\_\_  $\delta_F$ = \_\_\_\_\_

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Torso Date: \_\_\_\_\_

Vehicle: Honda Civic

Options: Loading Angle Variation Test



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = \_\_\_\_\_  $\delta_B$ = \_\_\_\_\_  $\delta_C$ = \_\_\_\_\_  $\delta_D$ = \_\_\_\_\_  $\delta_F$ = \_\_\_\_\_

Deflection

Force

Deflection

Force

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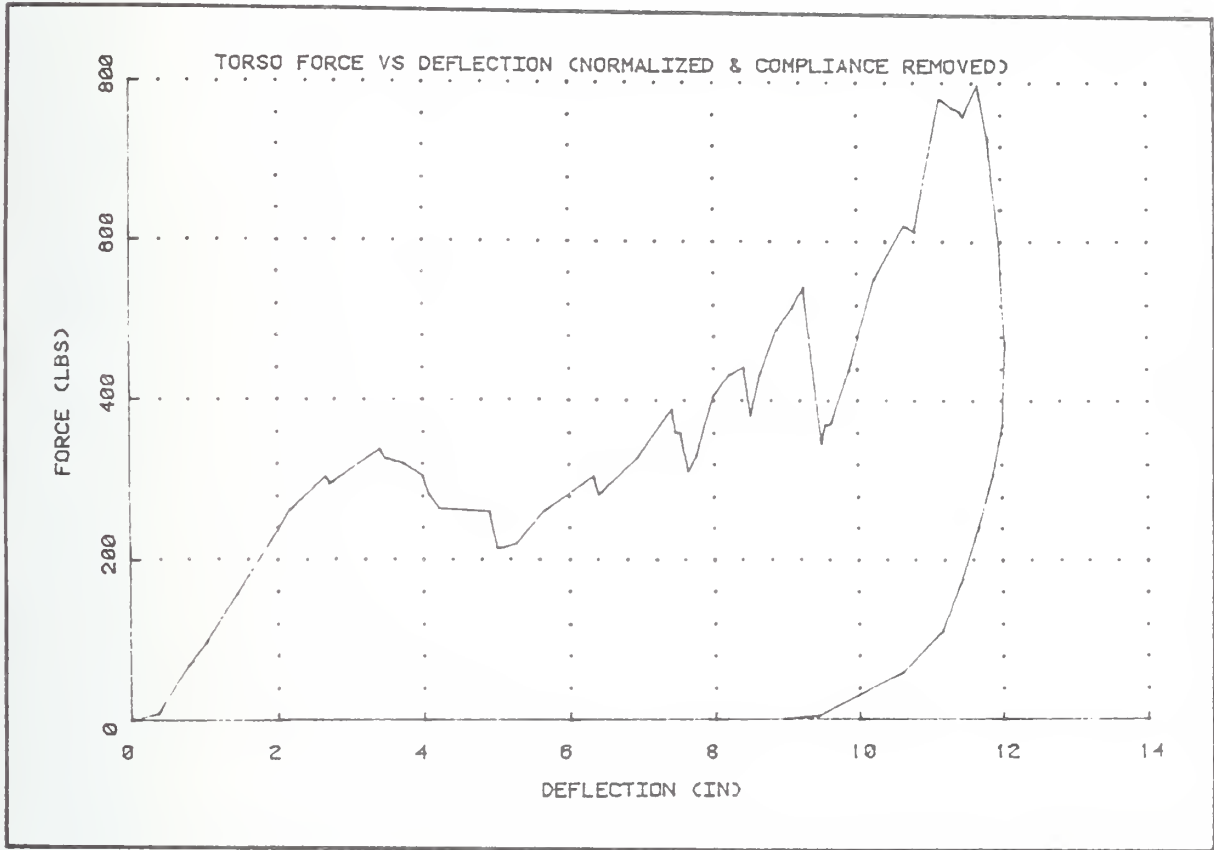
\_\_\_\_\_



Test: Torso Date: \_\_\_\_\_

Vehicle: Ford LTD

Options: Loading Angle Variation Test



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

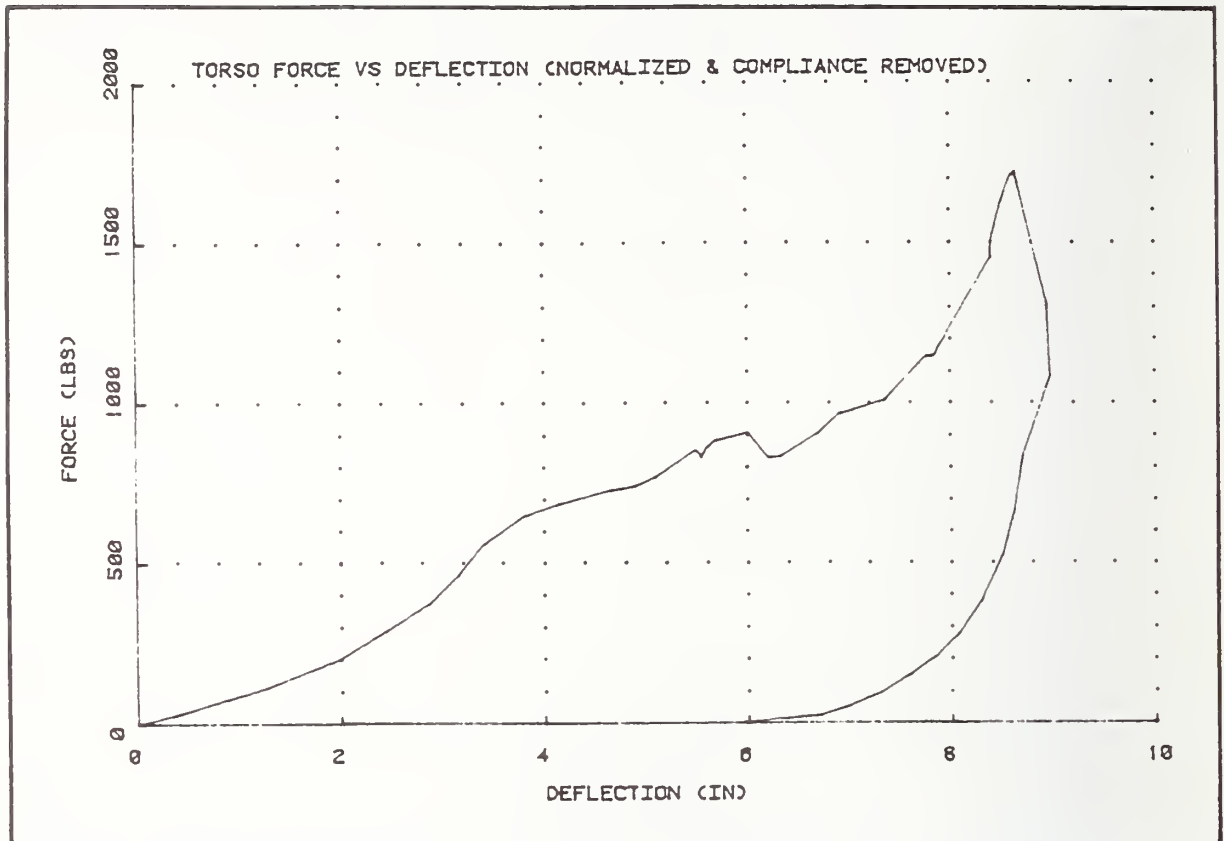
$\delta_A$ = \_\_\_\_\_  $\delta_B$ = \_\_\_\_\_  $\delta_C$ = \_\_\_\_\_  $\delta_D$ = \_\_\_\_\_  $\delta_F$ = \_\_\_\_\_

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Test: Torso Date: \_\_\_\_\_

Vehicle: Chevy Monza

Options: Loading Angle Variation Test



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

C= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

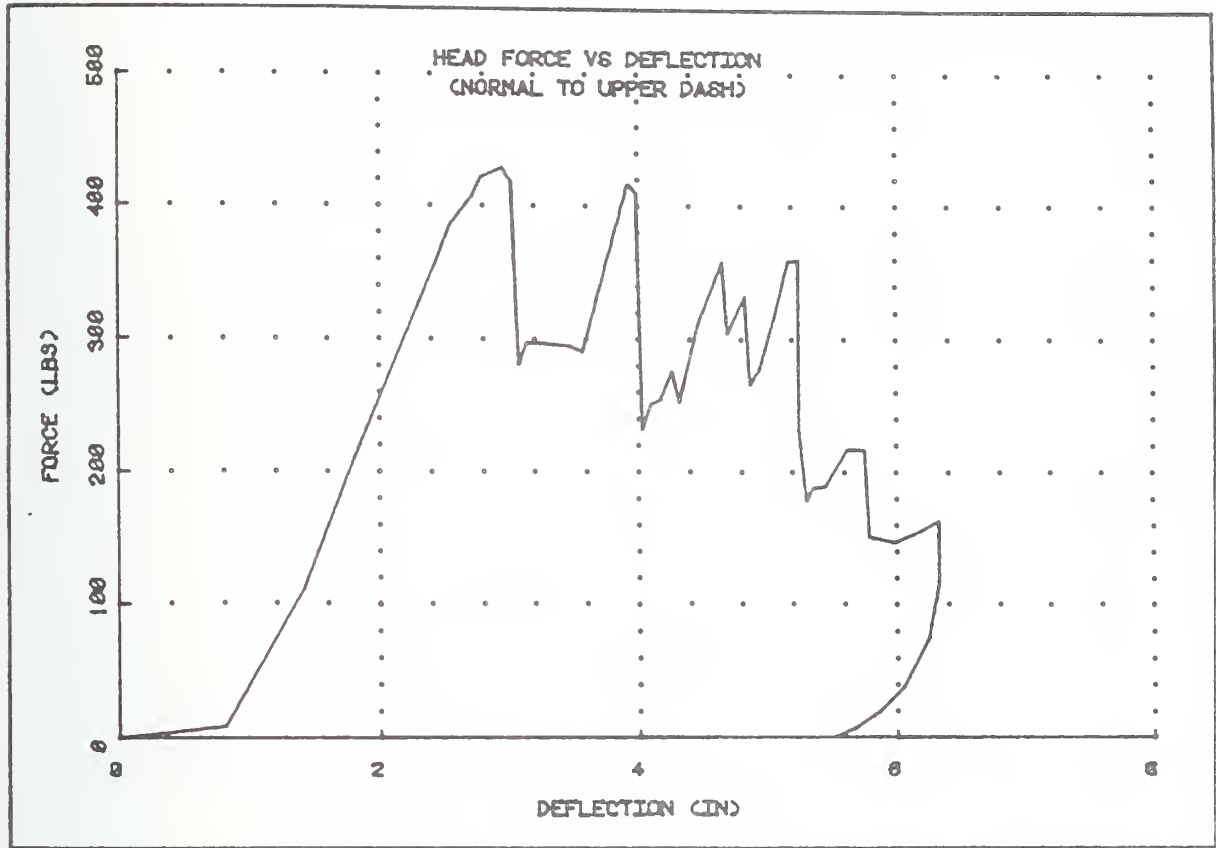
$\delta_A$ = \_\_\_\_\_  $\delta_B$ = \_\_\_\_\_  $\delta_C$ = \_\_\_\_\_  $\delta_D$ = \_\_\_\_\_  $\delta_F$ = \_\_\_\_\_

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
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Test: Head Date: \_\_\_\_\_

Vehicle: Plymouth Volare

Options: Loading Point Variation Test



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

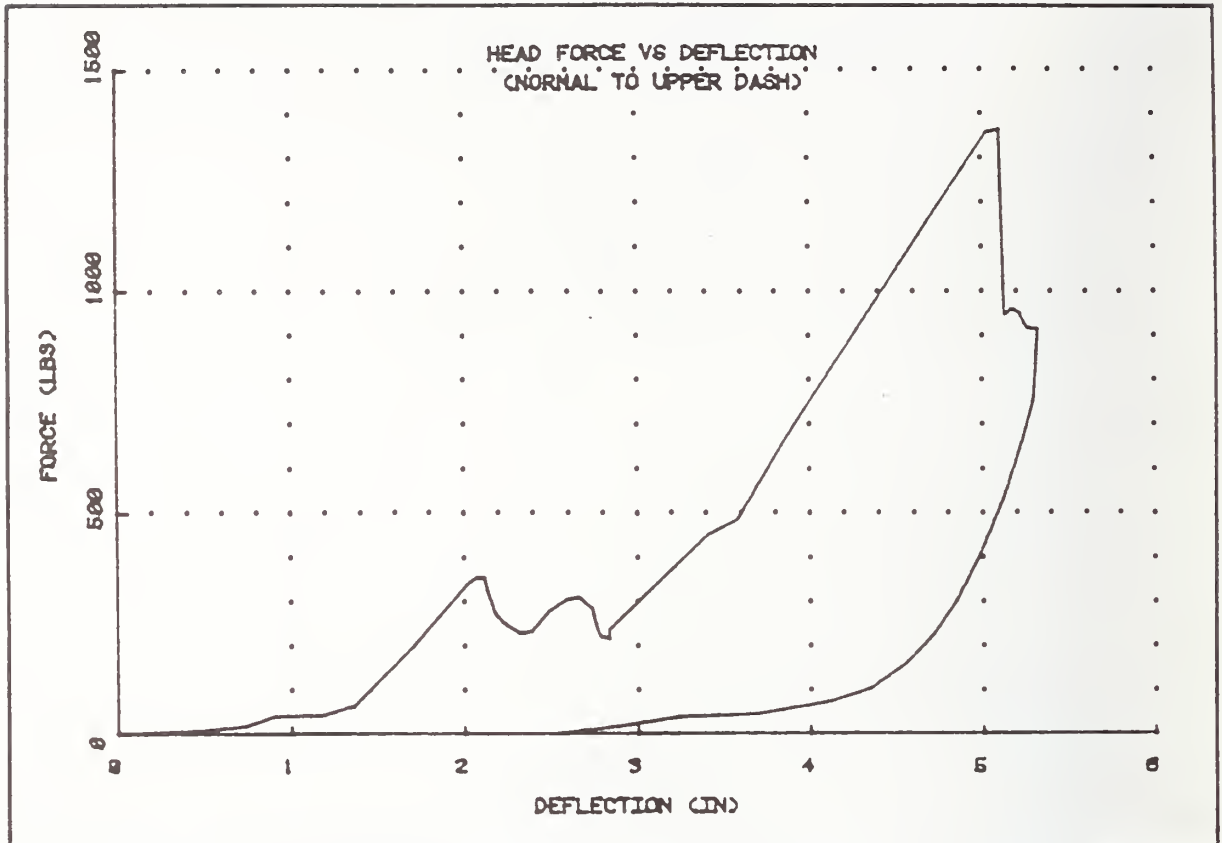
$\delta_A$ = \_\_\_\_\_  $\delta_B$ = \_\_\_\_\_  $\delta_C$ = \_\_\_\_\_  $\delta_D$ = \_\_\_\_\_  $\delta_F$ = \_\_\_\_\_

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
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_____	_____	_____	_____

Test: Head Date: \_\_\_\_\_

Vehicle: Honda Civic

Options: Loading Point Variation Test



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

C= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = \_\_\_\_\_  $\delta_B$ = \_\_\_\_\_  $\delta_C$ = \_\_\_\_\_  $\delta_D$ = \_\_\_\_\_  $\delta_F$ = \_\_\_\_\_

Deflection

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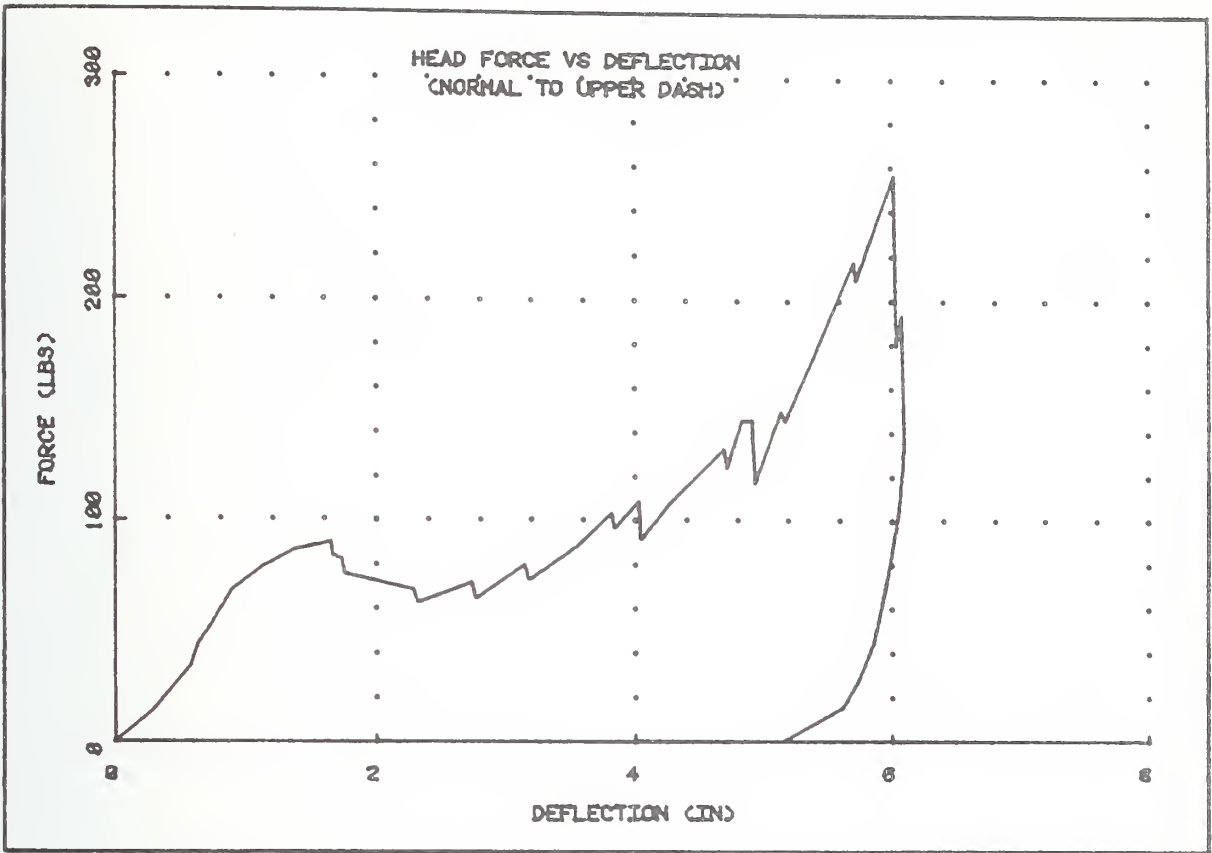
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Test: Head Date: \_\_\_\_\_

Vehicle: Ford LTD

Options: Loading Point Variation Test



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

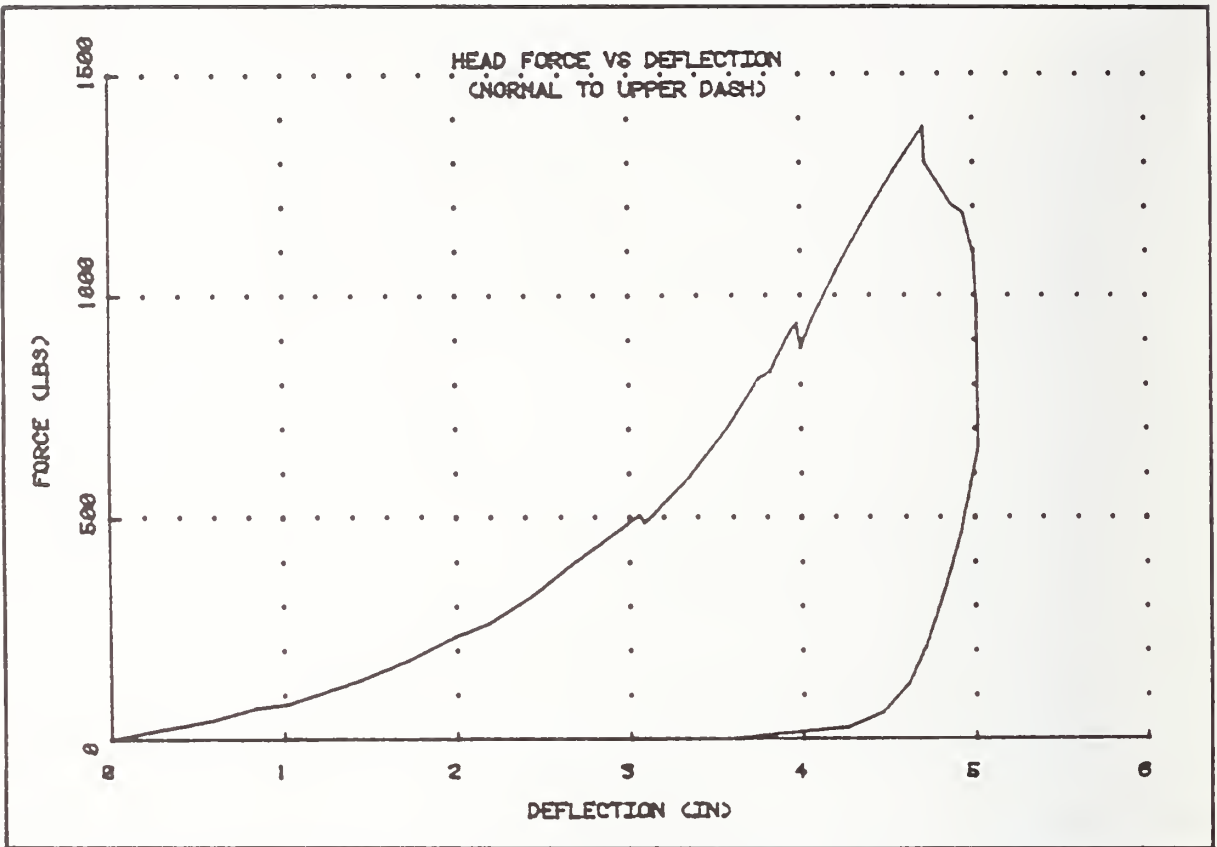
$\delta_A$ = \_\_\_\_\_  $\delta_B$ = \_\_\_\_\_  $\delta_C$ = \_\_\_\_\_  $\delta_D$ = \_\_\_\_\_  $\delta_F$ = \_\_\_\_\_

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
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_____	_____	_____	_____
_____	_____	_____	_____
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_____	_____	_____	_____

Test: Head Date: \_\_\_\_\_

Vehicle: Chevy Monza

Options: Loading Point Variation Test



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = \_\_\_\_\_  $\delta_B$ = \_\_\_\_\_  $\delta_C$ = \_\_\_\_\_  $\delta_D$ = \_\_\_\_\_  $\delta_F$ = \_\_\_\_\_

Deflection

Force

Deflection

Force

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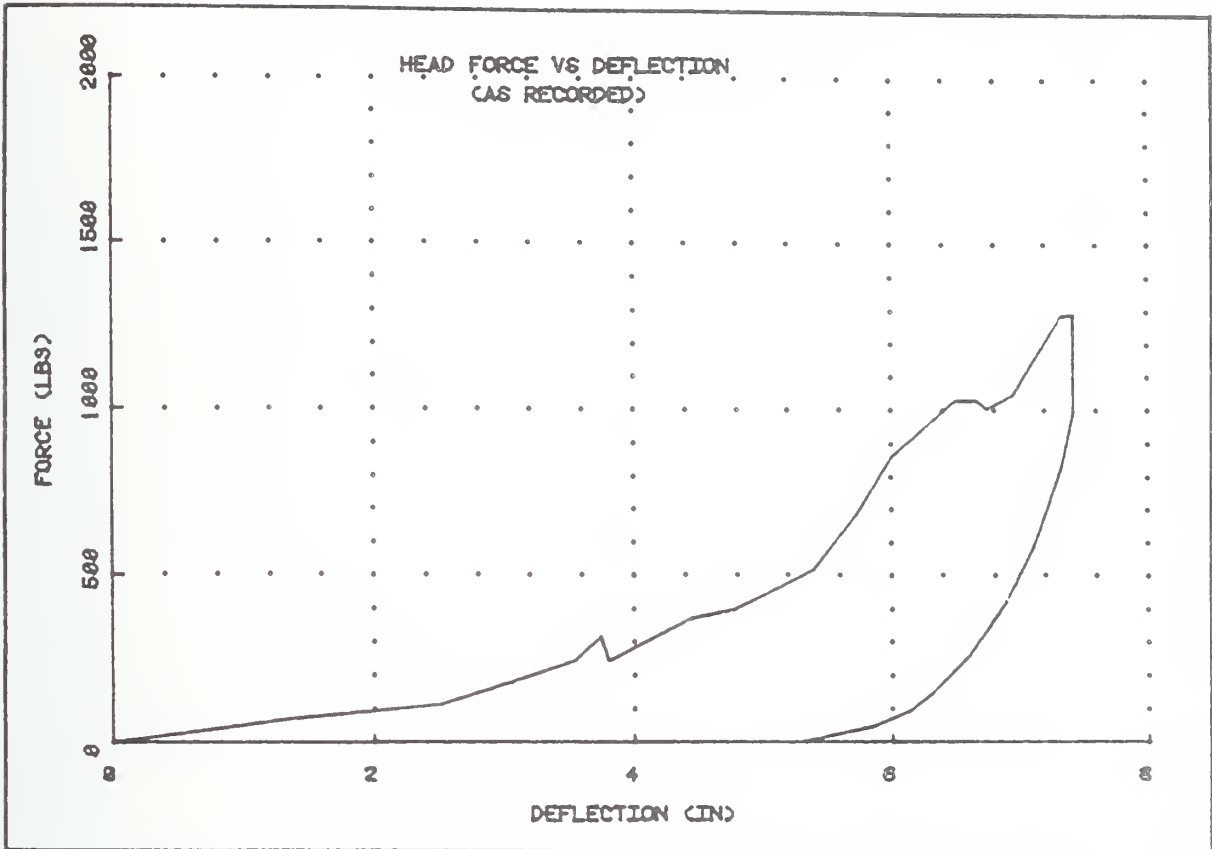
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Test: Head Date: \_\_\_\_\_

Vehicle: Plymouth Volare

Options: Loading Angle Variation Test



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

C= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

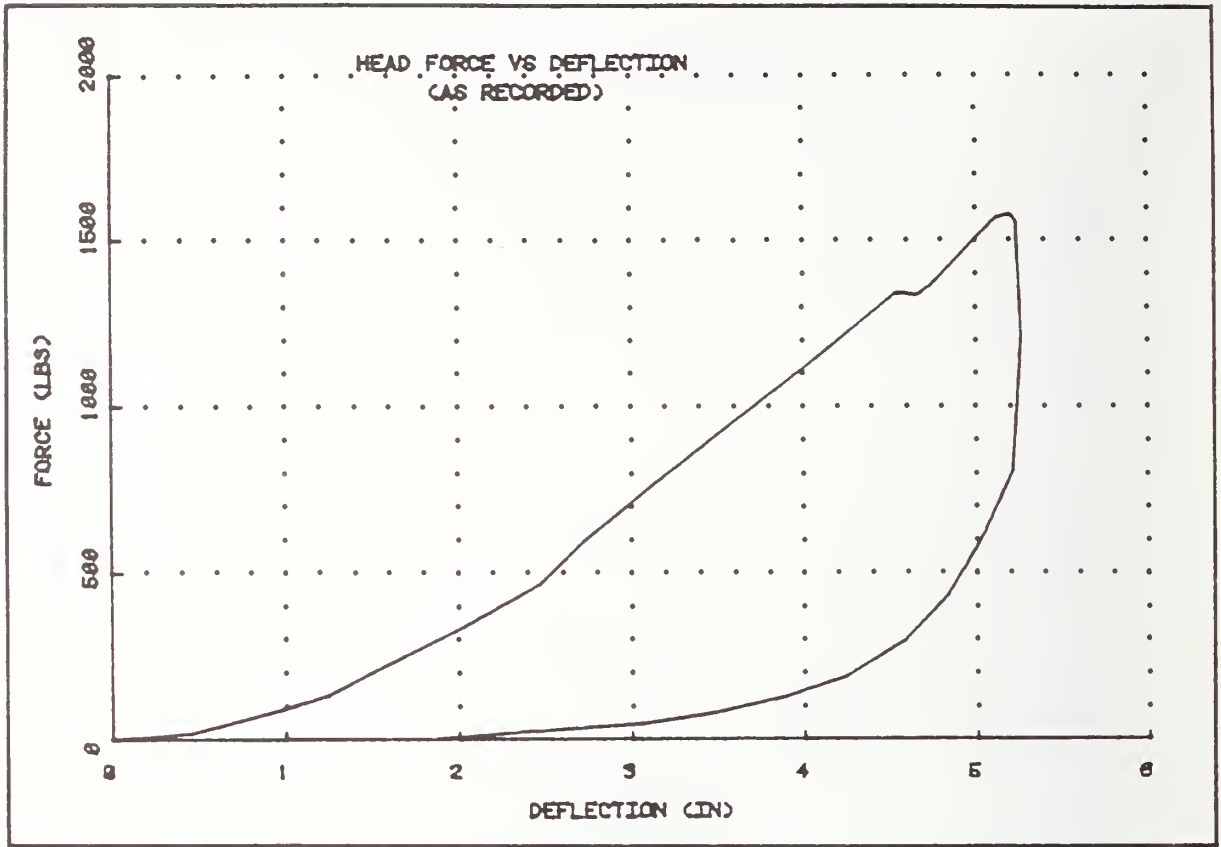
$\delta_A$ = \_\_\_\_\_  $\delta_B$ = \_\_\_\_\_  $\delta_C$ = \_\_\_\_\_  $\delta_D$ = \_\_\_\_\_  $\delta_F$ = \_\_\_\_\_

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
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Test: Head Date: 11/15/84

Vehicle: Honda Civic

Options: Loading Angle Variation Test



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = \_\_\_\_\_  $\delta_B$ = \_\_\_\_\_  $\delta_C$ = \_\_\_\_\_  $\delta_D$ = \_\_\_\_\_  $\delta_F$ = \_\_\_\_\_

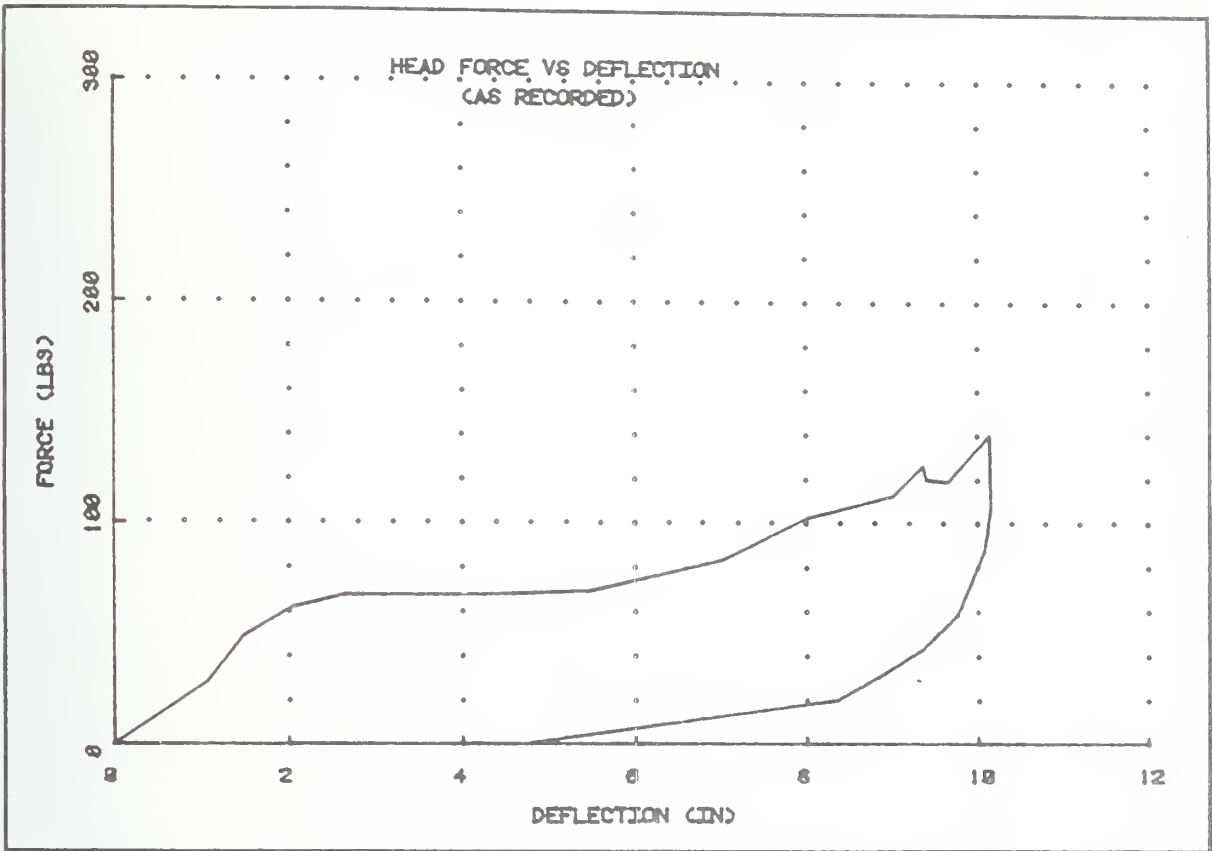
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
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Test: Head Date: 11/14

Vehicle: Ford LTD

Options: Loading Angle Variation Test



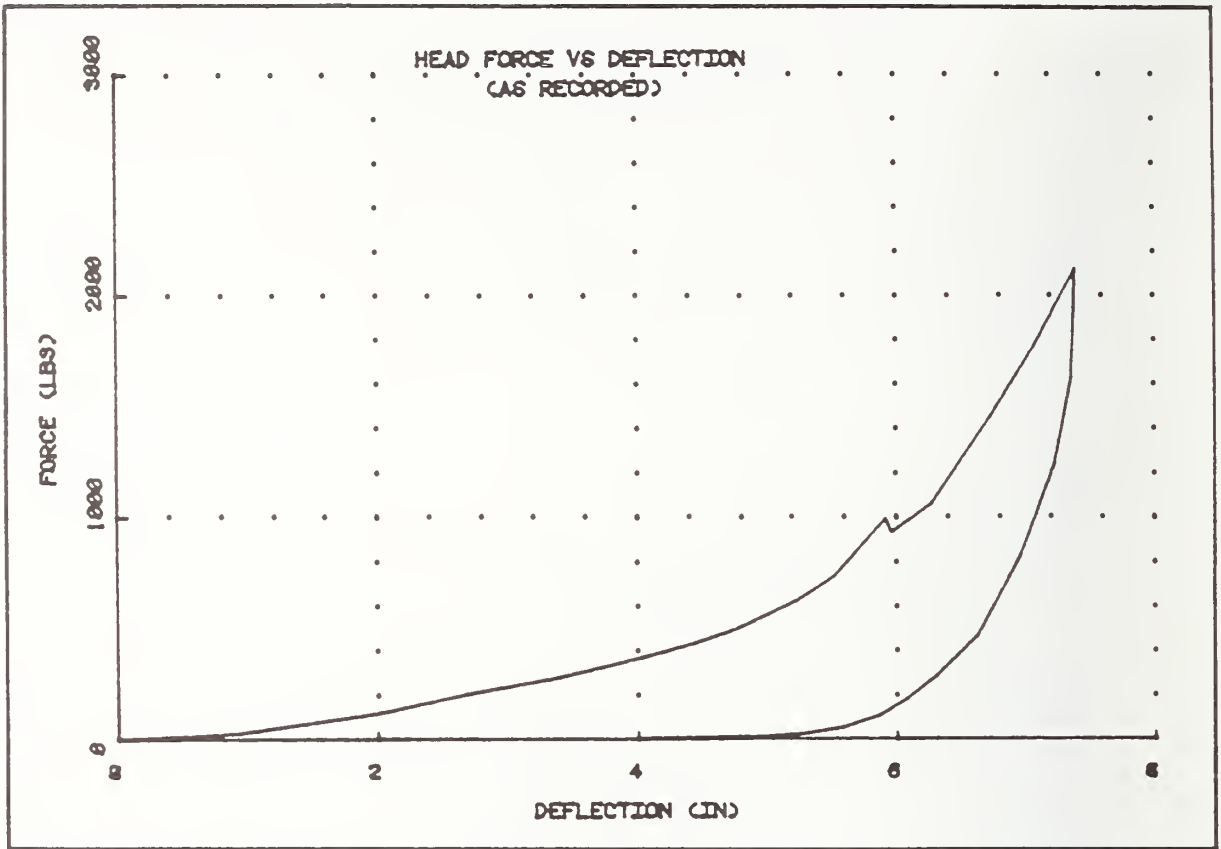
G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_

C= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = \_\_\_\_\_  $\delta_B$ = \_\_\_\_\_  $\delta_C$ = \_\_\_\_\_  $\delta_D$ = \_\_\_\_\_  $\delta_F$ = \_\_\_\_\_

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
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_____	_____	_____	_____
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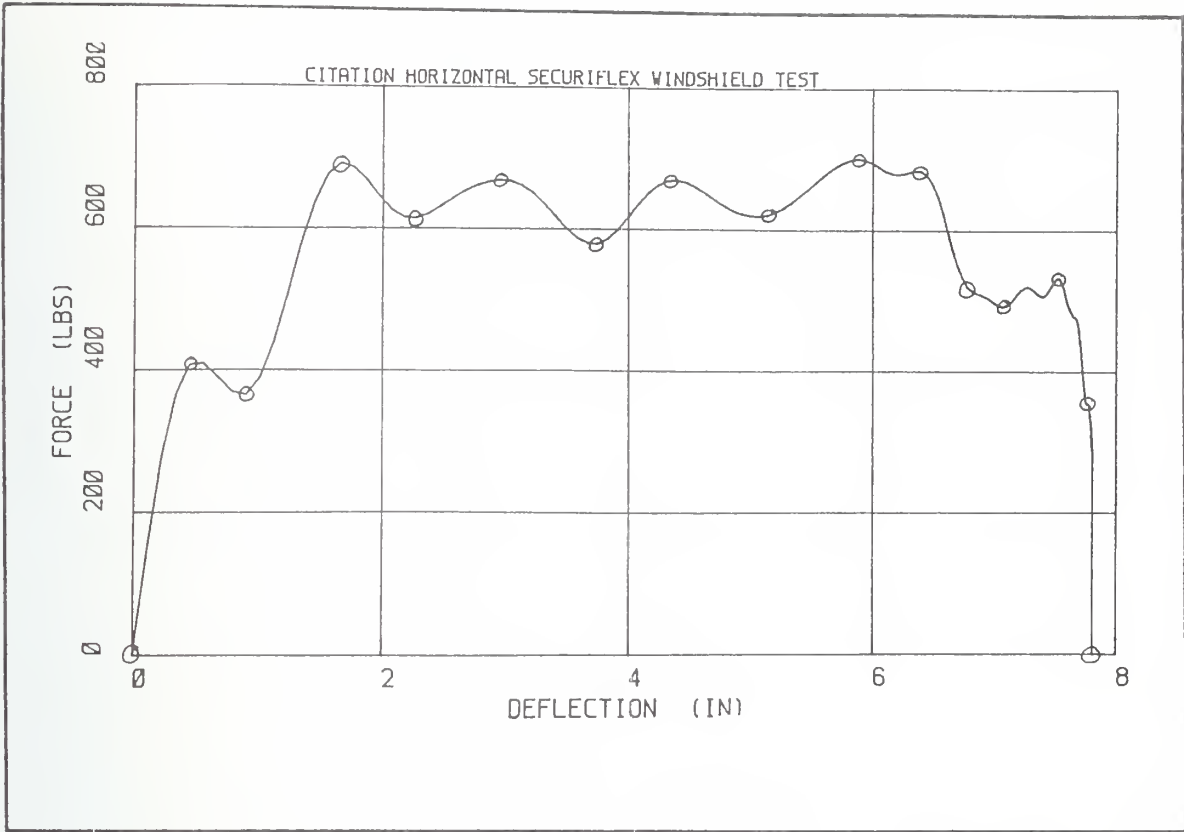
Test: Head Date: \_\_\_\_\_  
 Vehicle: Chevy Monza  
 Options: Loading Angle Variation Test



G= \_\_\_\_\_ R= \_\_\_\_\_ K= \_\_\_\_\_  
 c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_  
 $\delta_A$ = \_\_\_\_\_  $\delta_B$ = \_\_\_\_\_  $\delta_C$ = \_\_\_\_\_  $\delta_D$ = \_\_\_\_\_  $\delta_F$ = \_\_\_\_\_

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
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_____	_____	_____	_____
_____	_____	_____	_____

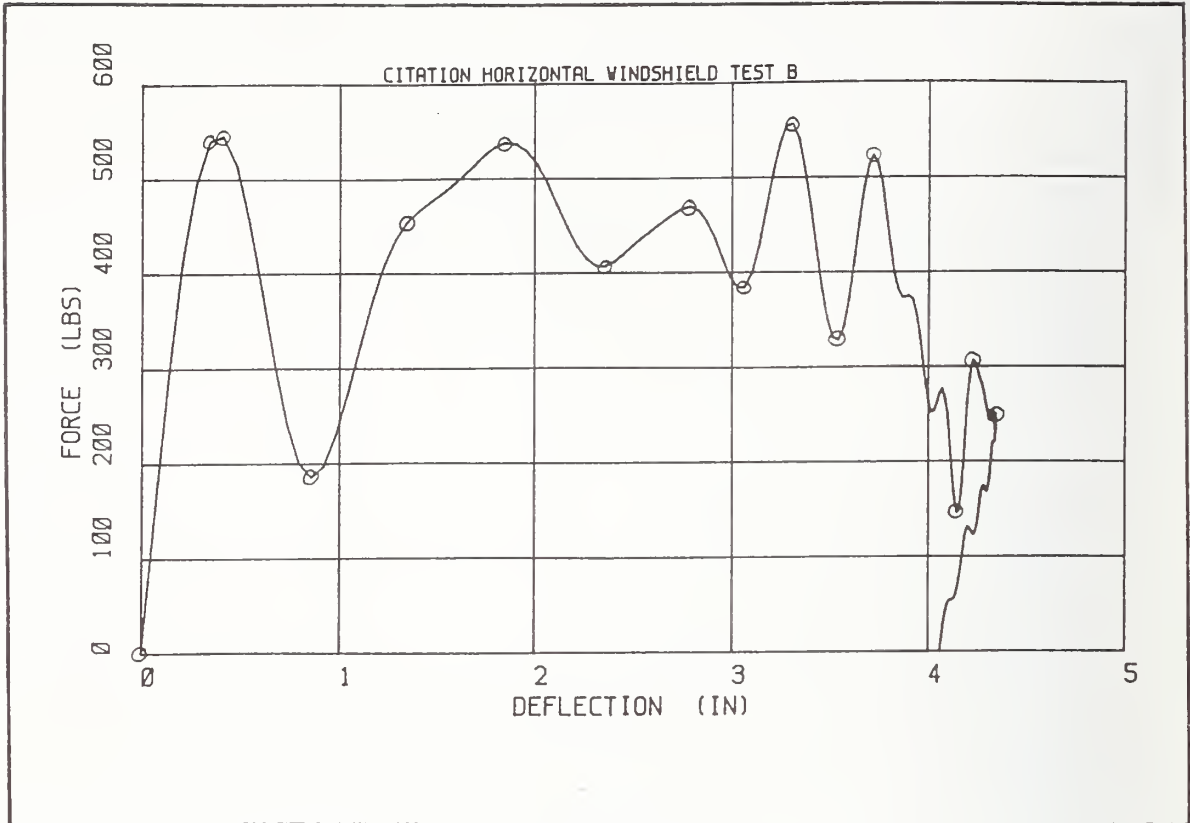
Test: Windshield Date: March 20, 1985  
 Vehicle: Chevy Citation  
 Options: Test A - Horizontal - Securiflex  
(Data not normalized)



G= 1.0 R= 0.0 K= N/A  
 c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_  
 $\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 7.77  $\delta_F$ = 7.81

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>5.06</u>	<u>618.6</u>
<u>.46</u>	<u>407.0</u>	<u>5.88</u>	<u>700.3</u>
<u>.90</u>	<u>365.2</u>	<u>6.34</u>	<u>684.4</u>
<u>1.66</u>	<u>691.8</u>	<u>6.78</u>	<u>520.0</u>
<u>2.28</u>	<u>613.8</u>	<u>7.06</u>	<u>491.5</u>
<u>2.95</u>	<u>667.8</u>	<u>7.58</u>	<u>531.7</u>
<u>3.75</u>	<u>578.9</u>	<u>7.77</u>	<u>354.3</u>
<u>4.40</u>	<u>669.3</u>	<u>7.81</u>	<u>0.0</u>

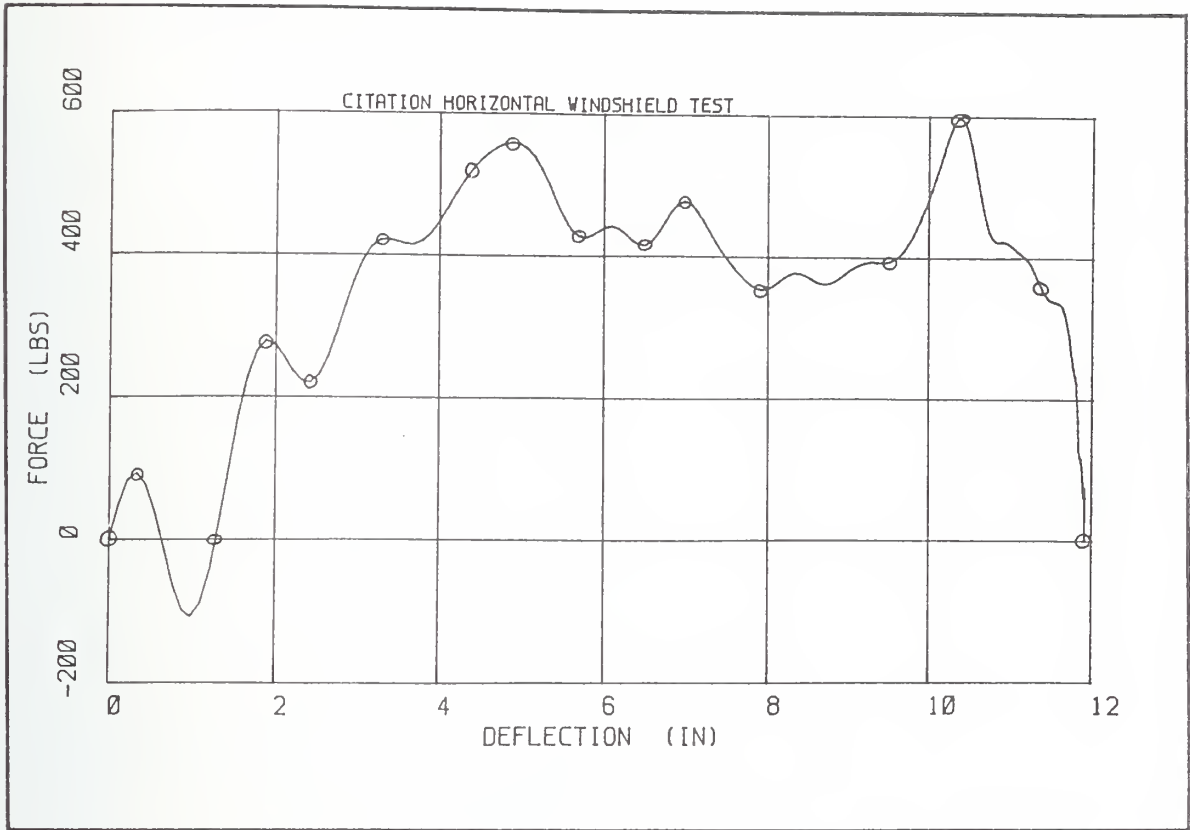
Test: Windshield (dynamic) Date: February 8, 1985  
 Vehicle: Chevy Citation  
 Options: Test B - Horizontal  
(Data not normalized)



G= 0.934 R= 0.019 K= 916  
 c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_  
 $\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.0

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>3.02</u>	<u>383.2</u>
<u>0.34</u>	<u>539.4</u>	<u>3.30</u>	<u>555.3</u>
<u>0.41</u>	<u>544.9</u>	<u>3.54</u>	<u>328.2</u>
<u>0.86</u>	<u>185.0</u>	<u>3.72</u>	<u>522.0</u>
<u>1.35</u>	<u>453.3</u>	<u>4.15</u>	<u>145.5</u>
<u>1.86</u>	<u>537.1</u>	<u>4.23</u>	<u>305.9</u>
<u>2.35</u>	<u>406.2</u>	<u>4.30</u>	<u>249.6</u>
<u>2.79</u>	<u>468.9</u>		

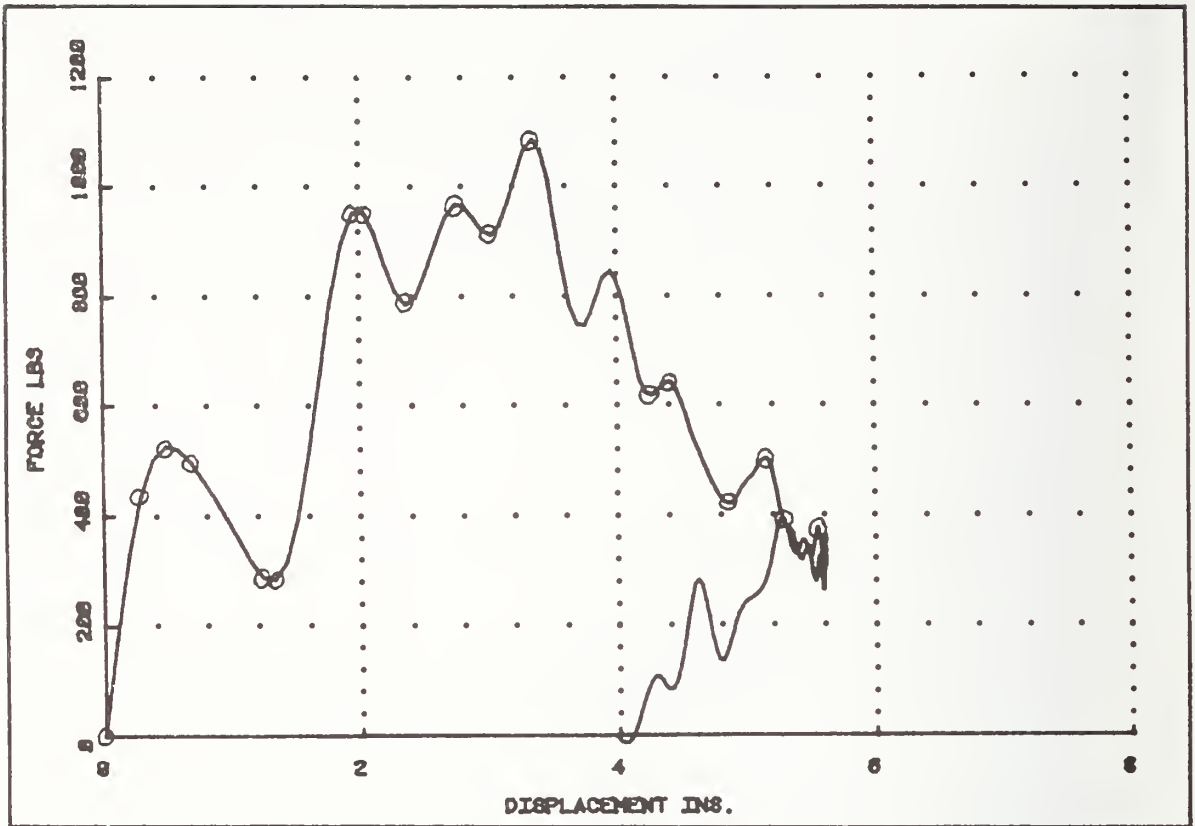
Test: Windshield (dynamic) Date: March 15, 1985  
 Vehicle: Chevy Citation  
 Options: Test B2 - Horizontal  
(Data not normalized)



G= 1.0 R= 0.0 K= N/A  
 c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_  
 $\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 11.34  $\delta_F$ = 11.90

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>5.76</u>	<u>425.3</u>
<u>0.33</u>	<u>93.6</u>	<u>6.67</u>	<u>432.7</u>
<u>1.29</u>	<u>0.0</u>	<u>6.98</u>	<u>477.4</u>
<u>1.88</u>	<u>277.1</u>	<u>7.91</u>	<u>352.4</u>
<u>2.43</u>	<u>219.4</u>	<u>9.57</u>	<u>397.2</u>
<u>3.49</u>	<u>418.1</u>	<u>10.39</u>	<u>596.7</u>
<u>4.39</u>	<u>519.8</u>	<u>11.34</u>	<u>361.3</u>
<u>5.05</u>	<u>550.3</u>	<u>11.90</u>	<u>0.0</u>

Test: Windshield (dynamic) Date: January 14, 1985  
 Vehicle: Chevy Citation  
 Options: Securiflex windshield (E2)



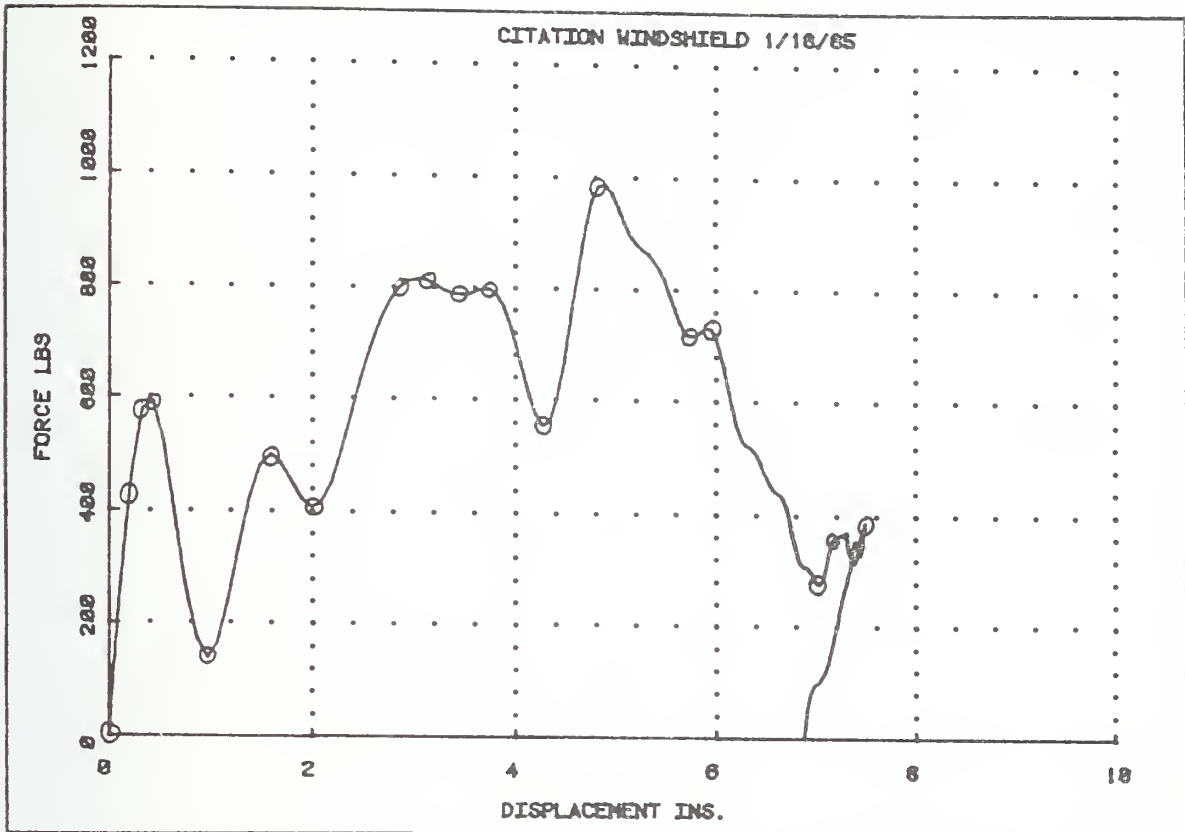
G= 0.707 R= 0.095 K= 154  
 c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_  
 $\delta_A$ = \_\_\_\_\_  $\delta_B$ = \_\_\_\_\_  $\delta_C$ = \_\_\_\_\_  $\delta_D$ = \_\_\_\_\_  $\delta_F$ = \_\_\_\_\_

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>2.73</u>	<u>965.0</u>
<u>0.28</u>	<u>434.1</u>	<u>3.01</u>	<u>913.4</u>
<u>0.47</u>	<u>524.0</u>	<u>3.36</u>	<u>1084.8</u>
<u>0.67</u>	<u>497.4</u>	<u>4.28</u>	<u>617.2</u>
<u>1.23</u>	<u>289.4</u>	<u>4.40</u>	<u>635.5</u>
<u>1.35</u>	<u>282.72</u>	<u>4.88</u>	<u>420.8</u>
<u>1.95</u>	<u>951.6</u>	<u>5.16</u>	<u>499.0</u>
<u>2.02</u>	<u>951.6</u>	<u>5.23</u>	<u>394.2</u>
<u>2.34</u>	<u>788.6</u>	<u>5.55</u>	<u>374.2</u>

Test: Windshield (dynamic) Date: January 18, 1985

Vehicle: Chevy Citation

Options: TSC Demo - Test F



G= 0.917 R= 0.028 K= 604

c=             $\mu_1$ =             $\mu_2$ =             $\mu_3$ =           

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.0

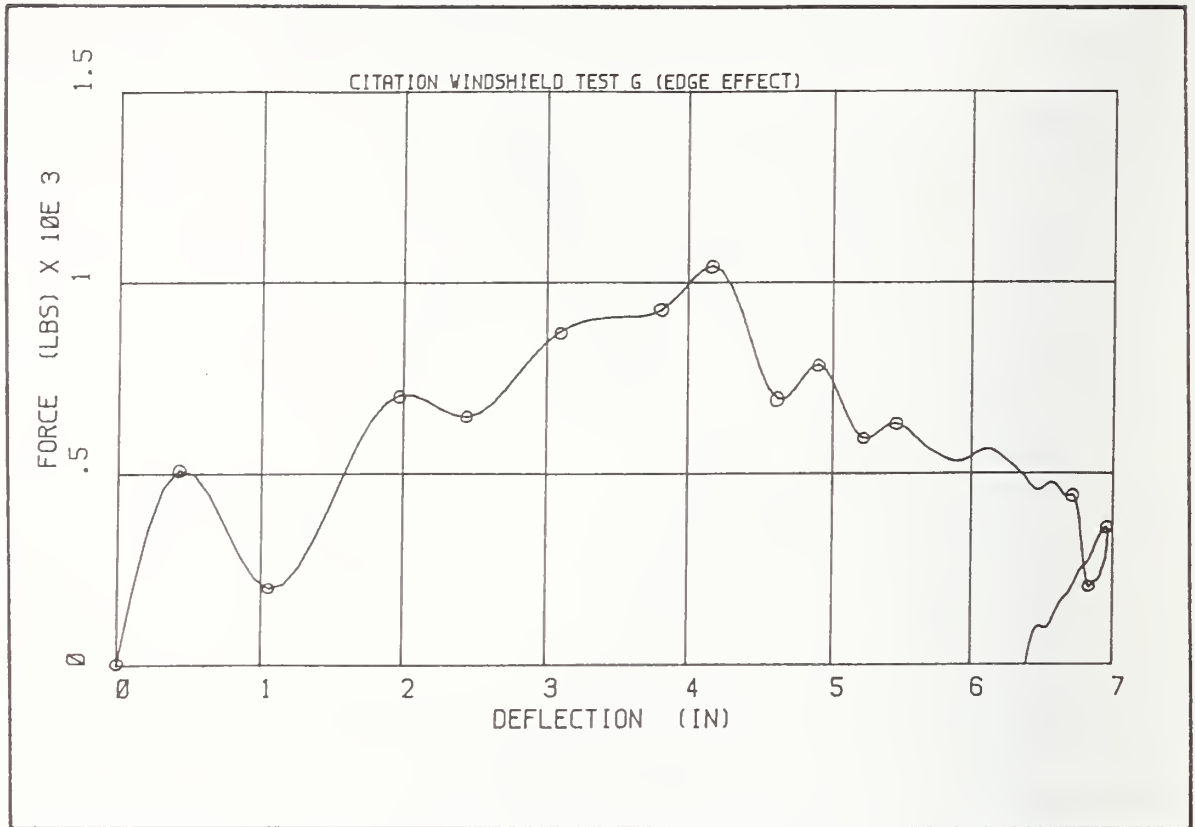
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>3.47</u>	<u>786.3</u>
<u>0.22</u>	<u>461.1</u>	<u>3.72</u>	<u>798.6</u>
<u>0.33</u>	<u>577.1</u>	<u>4.26</u>	<u>555.2</u>
<u>0.43</u>	<u>591.8</u>	<u>4.83</u>	<u>983.6</u>
<u>0.96</u>	<u>136.6</u>	<u>5.74</u>	<u>715.3</u>
<u>1.58</u>	<u>499.0</u>	<u>5.92</u>	<u>732.0</u>
<u>1.99</u>	<u>406.0</u>	<u>7.04</u>	<u>276.4</u>
<u>2.85</u>	<u>799.7</u>	<u>7.19</u>	<u>360.7</u>
<u>3.13</u>	<u>811.9</u>	<u>7.49</u>	<u>387.4</u>

Note: Vo - Adjusted up to satisfy displacement.

Test: Windshield (dynamic) Date: February 14, 1985

Vehicle: Chevy Citation

Options: Test G - Normal  
Edge Effect



G= 0.917 R= 0.026 K= 560  
 c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_  
 $\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.0

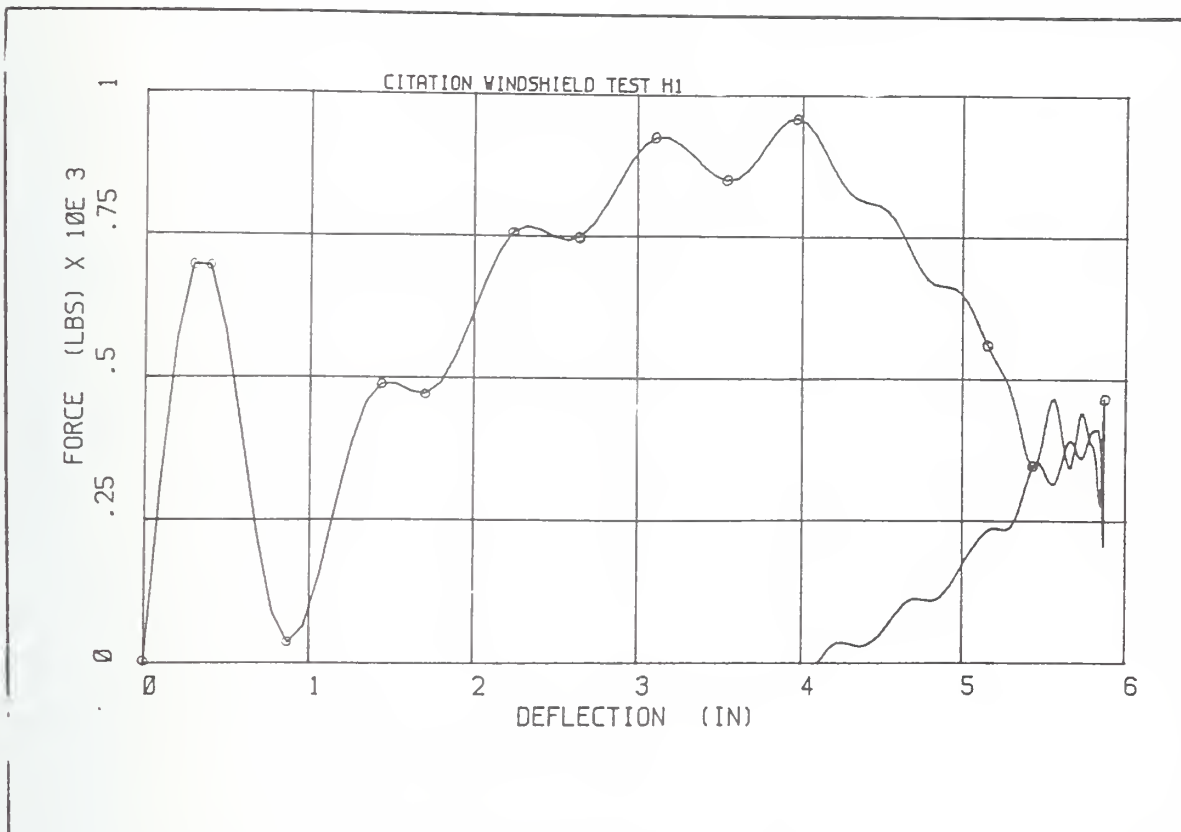
<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>4.62</u>	<u>695.0</u>
<u>0.43</u>	<u>509.4</u>	<u>4.91</u>	<u>784.2</u>
<u>1.06</u>	<u>201.5</u>	<u>5.22</u>	<u>593.2</u>
<u>1.98</u>	<u>705.2</u>	<u>5.46</u>	<u>631.6</u>
<u>2.45</u>	<u>647.8</u>	<u>6.72</u>	<u>442.5</u>
<u>3.17</u>	<u>885.3</u>	<u>6.85</u>	<u>203.5</u>
<u>3.81</u>	<u>926.6</u>	<u>6.96</u>	<u>354.7</u>
<u>4.17</u>	<u>1041.9</u>		



Test: Windshield (dynamic) Date: February 5, 1985

Vehicle: Chevy Citation

Options: Test H1 - Normal



G= 0.698 R= 0.091 K= 244

C= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

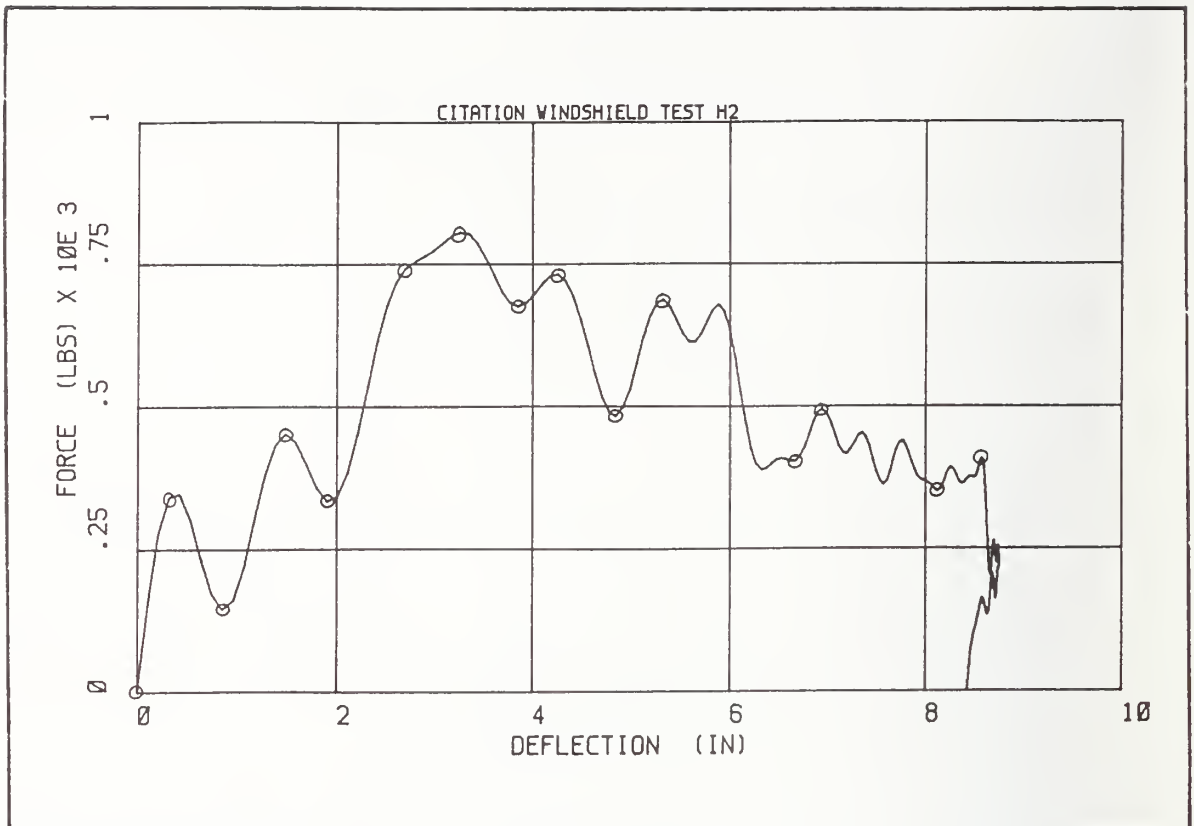
$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.0

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>3.11</u>	<u>924.8</u>
<u>0.30</u>	<u>695.7</u>	<u>3.53</u>	<u>848.8</u>
<u>0.39</u>	<u>695.2</u>	<u>3.97</u>	<u>958.8</u>
<u>0.87</u>	<u>34.8</u>	<u>5.17</u>	<u>543.9</u>
<u>1.43</u>	<u>488.3</u>	<u>5.44</u>	<u>345.7</u>
<u>1.71</u>	<u>471.5</u>	<u>5.86</u>	<u>465.2</u>
<u>2.24</u>	<u>755.4</u>		
<u>2.65</u>	<u>748.8</u>		

Test: Windshield (dynamics) Date: February 19, 1985

Vehicle: Chevy Citation

Options: Test H2 - Normal



G= 0.963 R= 0.010 K= 594

c= \_\_\_\_\_  $\mu_1$ = \_\_\_\_\_  $\mu_2$ = \_\_\_\_\_  $\mu_3$ = \_\_\_\_\_

$\delta_A$ = 0.0  $\delta_B$ = 0.0  $\delta_C$ = 0.0  $\delta_D$ = 1000.0  $\delta_F$ = 1000.0

<u>Deflection</u>	<u>Force</u>	<u>Deflection</u>	<u>Force</u>
<u>0.0</u>	<u>0.0</u>	<u>4.26</u>	<u>730.8</u>
<u>0.33</u>	<u>341.9</u>	<u>4.85</u>	<u>482.6</u>
<u>0.86</u>	<u>145.2</u>	<u>5.33</u>	<u>685.7</u>
<u>1.49</u>	<u>452.4</u>	<u>6.66</u>	<u>403.1</u>
<u>1.90</u>	<u>334.0</u>	<u>6.94</u>	<u>494.5</u>
<u>2.60</u>	<u>717.2</u>	<u>8.12</u>	<u>349.8</u>
<u>3.26</u>	<u>804.8</u>	<u>8.58</u>	<u>407.1</u>
<u>3.86</u>	<u>675.0</u>		





APPENDIX F

VEHICLE DIMENSIONAL DATA SUMMARIES



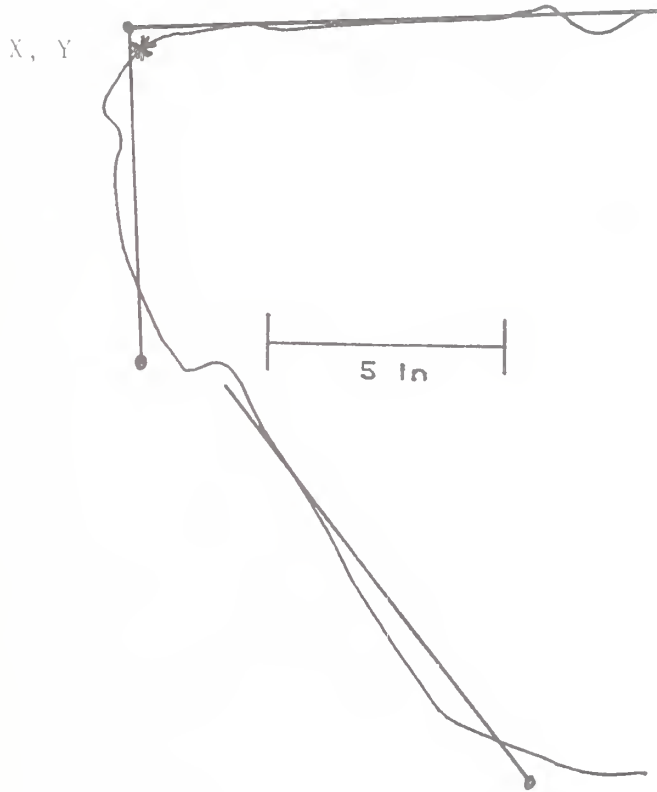
Test \_\_\_\_\_

Date: July 27, 1984

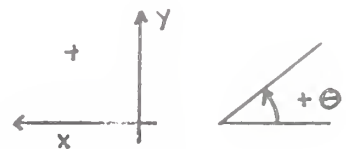
Vehicle: 1977 Plymouth Volare

INSTRUMENT PANEL PROFILE

Passenger Side



\* X, Y = 15.375", 26.75"



Origin (0,0) located at junction of toeboard and floorboard

Suggested Instrument Panel Profile Descriptors

Plane	X	Y	Angle (deg.)	Length
Lower Instrument Panel (3)	<u>8.05</u>	<u>10.58</u>	<u>124.77</u>	<u>10.63</u>
Center Instrument Panel (4)	<u>15.47</u>	<u>19.31</u>	<u>96.35</u>	<u>7.42</u>
Upper Instrument Panel (5)	<u>16.29</u>	<u>26.68</u>	<u>4.87</u>	<u>10.83</u>
Windshield (6)	<u>3.0</u>	<u>27.5</u>	<u>147.9°</u>	<u>25.0</u>
Header (7)	<u>23.0</u>	<u>40.0</u>	<u>160.3°</u>	<u>4.0</u>

Number in parenthesis represents the corresponding contact plane numbers for the PADS2 Program.





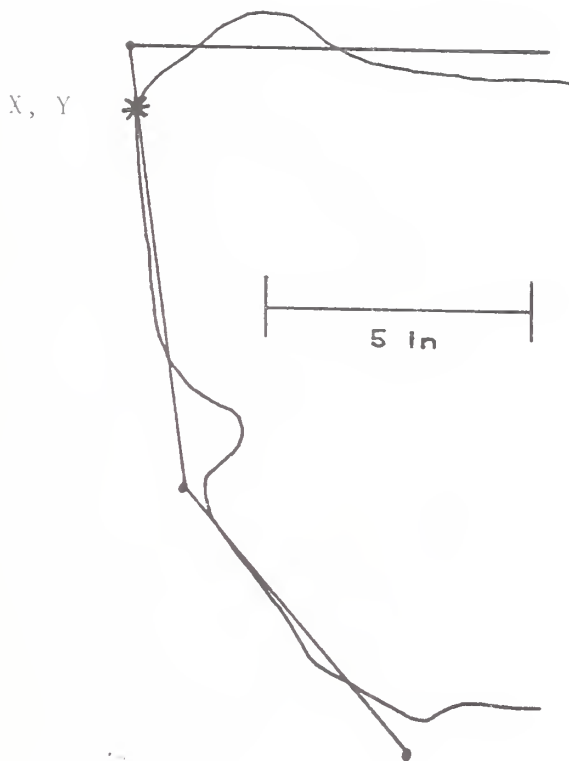
Test \_\_\_\_\_

Date: August 17, 1984

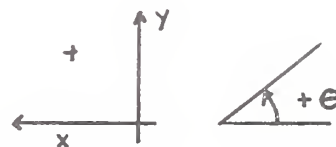
Vehicle: 1976 Chevy Monza

INSTRUMENT PANEL PROFILE

Passenger Side



\* X, Y = 15.4375", 26"



Origin (0,0) located at junction of toeboard and floorboard

Suggested Instrument Panel Profile Descriptors

Plane	X	Y	Angle (deg.)	Length
Lower Instrument Panel (3)	10.39	13.43	128.19	6.62
Center Instrument Panel (4)	14.48	18.63	98.05	8.65
Upper Instrument Panel (5)	15.69	27.19	358.91	8.39
Windshield (6)	7.0	26.75	152.5°	25.0
Header (7)	29.0	38.0	164°	3.0

Number in parenthesis represents the corresponding contact plane numbers for the PADS2 Program.

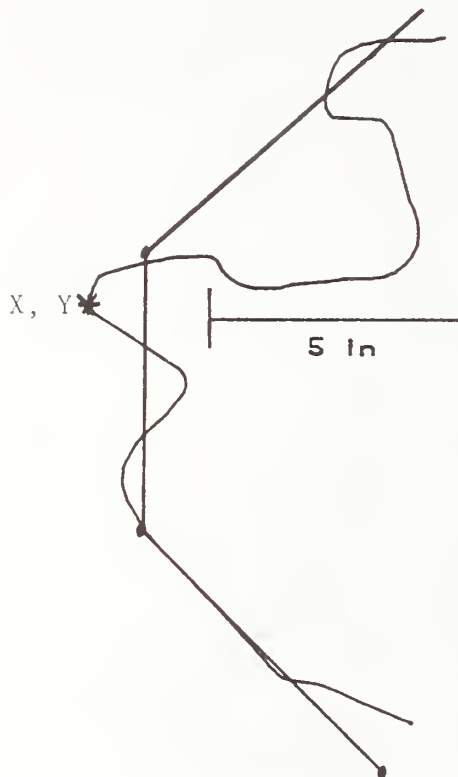
Test \_\_\_\_\_

Date: August 21, 1984

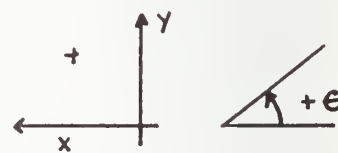
Vehicle: Honda Civic CVCC

INSTRUMENT PANEL PROFILE

Passenger Side



\* X, Y = 13.3215", 21"



Origin (0,0) located at junction of toeboard and floorboard

Suggested Instrument Panel Profile Descriptors

Plane	X	Y	Angle (deg.)	Length
Lower Instrument Panel (3)	<u>8.65</u>	<u>12.04</u>	<u>131.11</u>	<u>5.84</u>
Center Instrument Panel (4)	<u>12.49</u>	<u>16.44</u>	<u>90.0</u>	<u>5.44</u>
Upper Instrument Panel (5)	<u>12.49</u>	<u>21.88</u>	<u>41.03</u>	<u>7.75</u>
Windshield (6)	<u>5.0</u>	<u>27.5</u>	<u>143.67°</u>	<u>21.5</u>
Header (7)	<u>21.75</u>	<u>40.0</u>	<u>163.5°</u>	<u>3.25</u>

Number in parenthesis represents the corresponding contact plane numbers for the PADS2 Program.

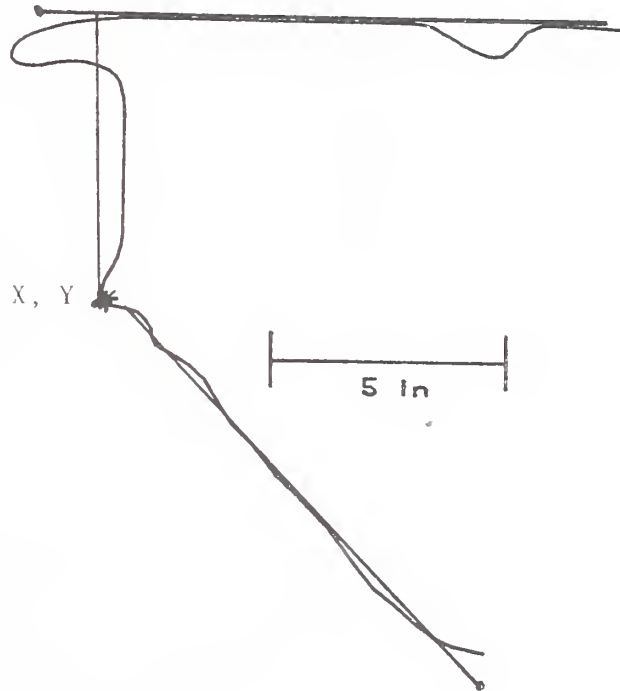
Test \_\_\_\_\_

Date: August 28, 1984

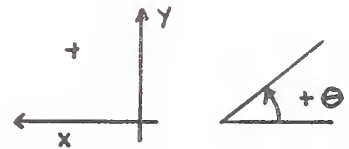
Vehicle: Ford LTD

### INSTRUMENT PANEL PROFILE

Passenger Side



\* X, Y = 10.9375", 21.25"



Origin (0,0) located at junction of toeboard and floorboard

#### Suggested Instrument Panel Profile Descriptors

Plane	X	Y	Angle (deg.)	Length
Lower Instrument Panel (3)	<u>3.35</u>	<u>13.37</u>	<u>133.36</u>	<u>10.61</u>
Center Instrument Panel (4)	<u>11.06</u>	<u>21.06</u>	<u>93.53</u>	<u>6.49</u>
Upper Instrument Panel (5)	<u>12.68</u>	<u>27.54</u>	<u>0.42</u>	<u>12.15</u>
Windshield (6)	<u>-2.0</u>	<u>24.0</u>	<u>143.5°</u>	<u>28.0</u>
Header (7)	<u>20.0</u>	<u>40.0</u>	<u>157°</u>	<u>5.5</u>

Number in parenthesis represents the corresponding contact plane numbers for the PADS2 Program.



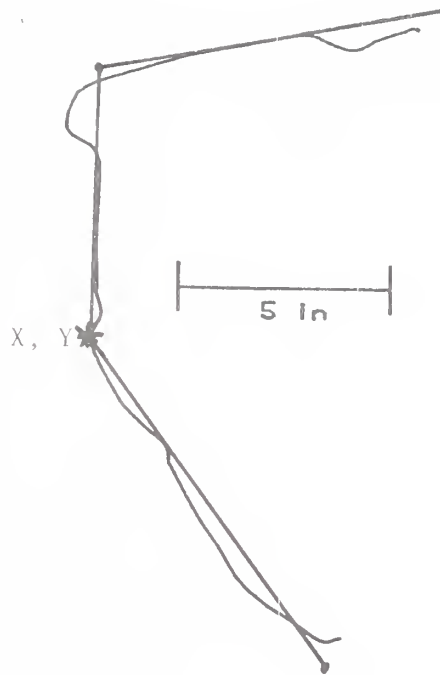
Test \_\_\_\_\_

Date: September 5, 1984

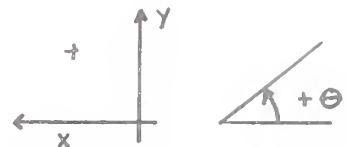
Vehicle: Ford Mustang

INSTRUMENT PANEL PROFILE

Passenger Side



\* X, Y = 13", 21.625"



Origin (0,0) located at junction of toeboard and floorboard

Suggested Instrument Panel Profile Descriptors

Plane	X	Y	Angle (deg.)	Length
Lower Instrument Panel (3)	7.81	13.61	122.47	9.74
Center Instrument Panel (4)	13.04	21.83	92.77	6.21
Upper Instrument Panel (5)	13.34	28.03	13.37	8.17
Windshield (6)	3.5	27.0	148.0°	24.0
Header (7)	23.5	38.0	165.5°	4.5

Number in parenthesis represents the corresponding contact plane numbers for the PADS2 Program.

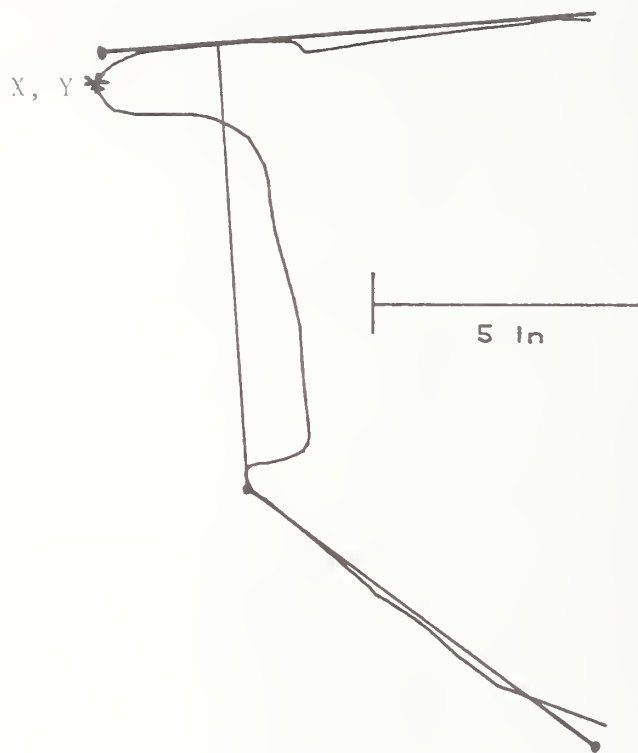
Test \_\_\_\_\_

Date: September 5, 1984

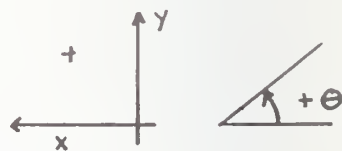
Vehicle: Ford Mustang

INSTRUMENT PANEL PROFILE

Driver Side



\* X, Y = 15.125", 27.25"



Origin (0,0) located at junction of toeboard and floorboard

Suggested Instrument Panel Profile Descriptors

Plane	X	Y	Angle (deg.)	Length
Lower Instrument Panel (3)	<u>5.7</u>	<u>14.51</u>	<u>144.56</u>	<u>8.55</u>
Center Instrument Panel (4)	<u>12.67</u>	<u>19.47</u>	<u>96.53</u>	<u>8.54</u>
Upper Instrument Panel (5)	<u>15.32</u>	<u>27.95</u>	<u>4.95</u>	<u>9.27</u>
Windshield (6)	<u>3.5</u>	<u>27.0</u>	<u>148.0°</u>	<u>24.0</u>
Header (7)	<u>23.5</u>	<u>38.0</u>	<u>165.0°</u>	<u>4.5</u>

Number in parenthesis represents the corresponding contact plane numbers for the PADS2 Program.

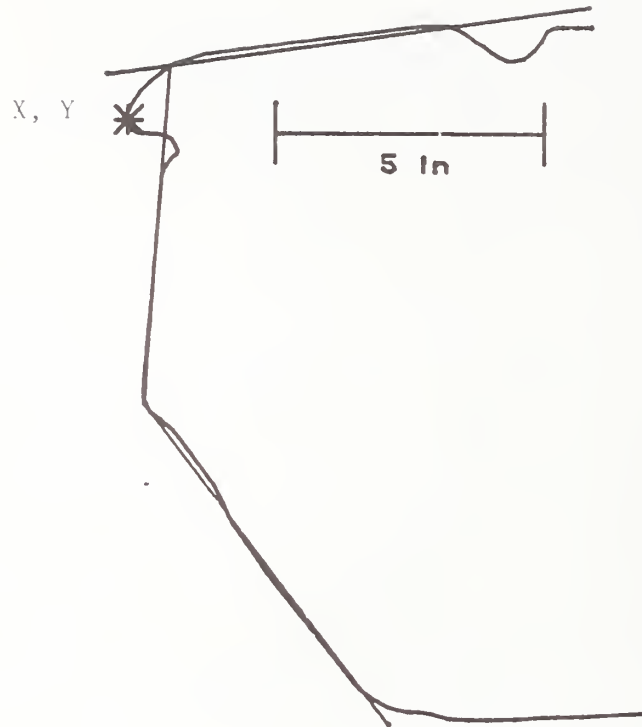


Test \_\_\_\_\_

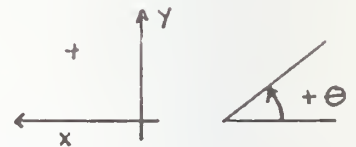
Date: November 29, 1984

Vehicle: Ford Fairmont

INSTRUMENT PANEL PROFILE  
PASSENGER SIDE



\* X, Y = 13.75, 25.25



Origin (0,0) located at junction of toeboard and floorboard

Suggested Instrument Panel Profile Descriptors

Plane	X	Y	Angle (deg.)	Length
Lower Instrument Panel (3)	8.9	13.3	125.8	7.80
Center Instrument Panel (4)	13.4	19.6	86.0	6.74
Upper Instrument Panel (5)	14.2	26.2	8.7	9.10
Windshield (6)	1.0	29.0	129.0	26.25
Header (7)	18.0	43.0	146.0	4.75

Number in parenthesis represents the corresponding contact plane numbers for the PADS2 Program.

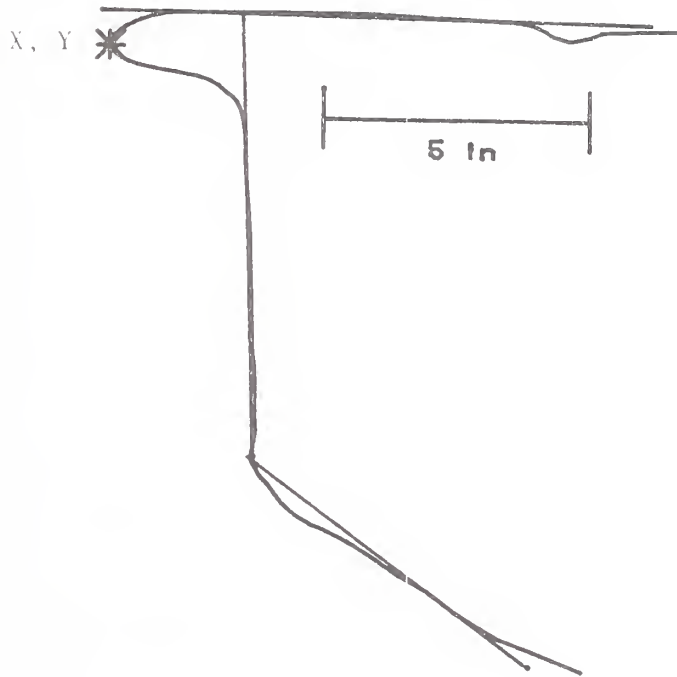


Test \_\_\_\_\_

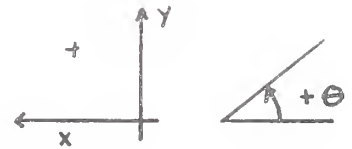
Date: November 29, 1984

Vehicle: Ford Fairmont

INSTRUMENT PANEL PROFILE  
DRIVER SIDE



\* X, Y = 15, 27.38



Origin (0,0) located at junction of toeboard and floorboard

Suggested Instrument Panel Profile Descriptors

Plane	X	Y	Angle (deg.)	Length
Lower Instrument Panel (3)	7.1	15.1	141.7	6.71
Center Instrument Panel (4)	12.3	19.3	91.5	8.79
Upper Instrument Panel (5)	15.2	28.1	0.9	10.30
Windshield (6)	1.0	29.0	129.0	26.25
Header (7)	18.0	43.0	146.0	4.75

Number in parenthesis represents the corresponding contact plane numbers for the PADS2 Program.

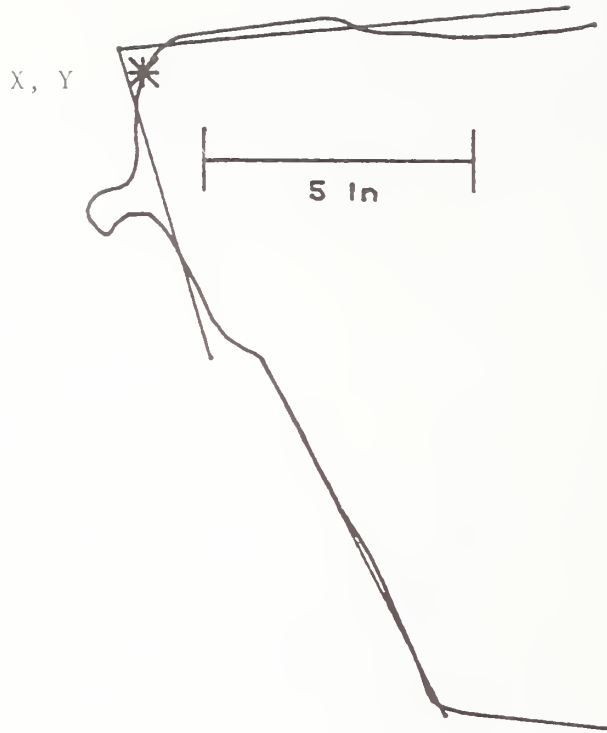
Test \_\_\_\_\_

Date: January 5, 1985

Vehicle: Pontiac Firebird

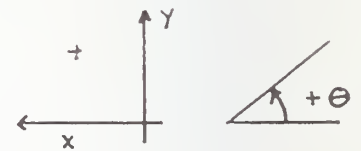
### INSTRUMENT PANEL PROFILE

Passenger Side



\* X, Y = 13.13, 24.75

Origin (0,0) located at junction of toeboard and floorboard



#### Suggested Instrument Panel Profile Descriptors

Plane	X	Y	Angle (deg.)	Length
Lower Instrument Panel (3)	<u>7.5</u>	<u>12.1</u>	<u>115.5</u>	<u>7.79</u>
Center Instrument Panel (4)	<u>11.9</u>	<u>19.1</u>	<u>105.6</u>	<u>6.32</u>
Upper Instrument Panel (5)	<u>13.6</u>	<u>25.2</u>	<u>6.0</u>	<u>8.44</u>
Windshield (6)	<u>0.0</u>	<u>22.5</u>	<u>145.0</u>	<u>24.75</u>
Header (7)	<u>20.75</u>	<u>38.0</u>	<u>160.0</u>	<u>7.5</u>

Number in parenthesis represents the corresponding contact plane numbers for the PADS2 Program.

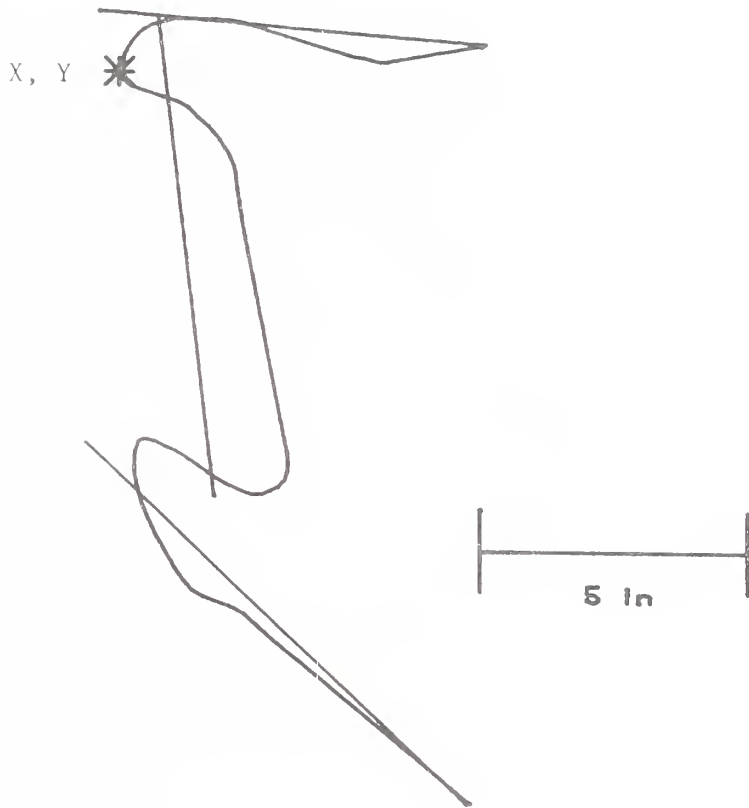
Test \_\_\_\_\_

Date: January 5, 1985

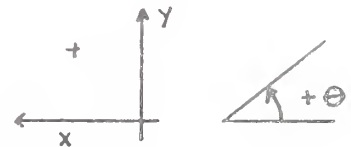
Vehicle: Pontiac Firebird

INSTRUMENT PANEL PROFILE

Driver Side



\* X, Y = 14.75, 24.75



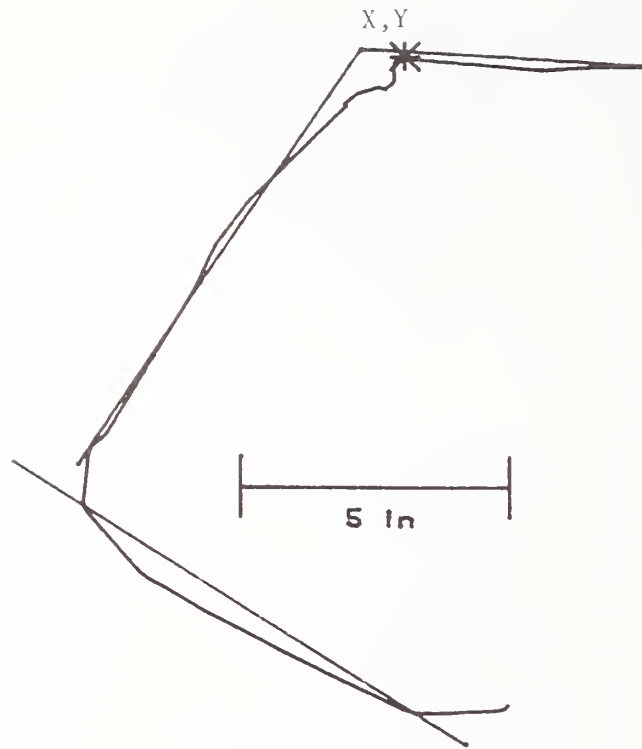
Origin (0,0) located at junction of toeboard and floorboard

Suggested Instrument Panel Profile Descriptors

Plane	X	Y	Angle (deg.)	Length
Lower Instrument Panel (3)	<u>8.3</u>	<u>14.0</u>	<u>143.3</u>	<u>8.84</u>
Center Instrument Panel (4)	<u>13.0</u>	<u>18.5</u>	<u>98.7</u>	<u>7.16</u>
Upper Instrument Panel (5)	<u>15.1</u>	<u>25.6</u>	<u>356.7</u>	<u>7.22</u>
Windshield (6)	<u>0.0</u>	<u>22.5</u>	<u>145</u>	<u>24.75</u>
Header (7)	<u>20.75</u>	<u>38.0</u>	<u>160</u>	<u>7.5</u>

Number in parenthesis represents the corresponding contact plane numbers for the PADS2 Program.

INSTRUMENT PANEL PROFILE  
Passenger Side



\* X, Y = 11.94, 29.0



Origin (0,0) located at junction of toeboard and floorboard

Suggested Instrument Panel Profile Descriptors

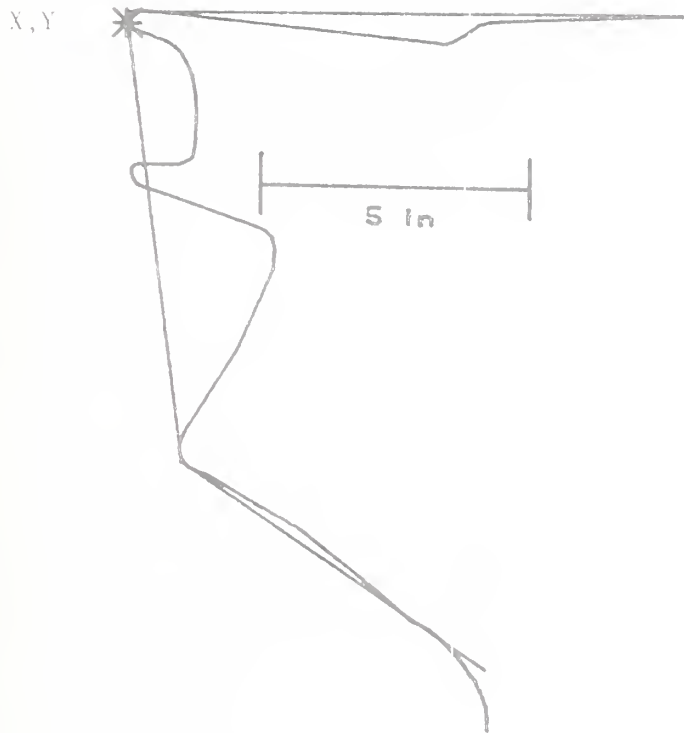
Plane	X	Y	Angle (deg.)	Length
Lower Instrument Panel (3)	<u>10.8</u>	<u>15.5</u>	<u>146.6</u>	<u>10.05</u>
Center Instrument Panel (4)	<u>18.0</u>	<u>20.9</u>	<u>57.4</u>	<u>9.78</u>
Upper Instrument Panel (5)	<u>12.8</u>	<u>29.1</u>	<u>356.5</u>	<u>5.40</u>
Windshield (6)	<u>0.0</u>	<u>29.75</u>	<u>147.0</u>	<u>27.5</u>
Header (7)	<u>27.0</u>	<u>48.0</u>	<u>157.0</u>	<u>6.5</u>

Number in parenthesis represents the corresponding contact plane numbers for the PADS2 Program.

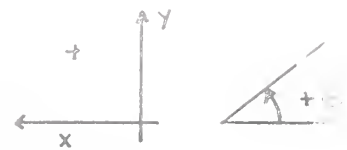
Test \_\_\_\_\_ Date: January 11, 1985

Vehicle: Chevy Celebrity

INSTRUMENT PANEL PROFILE  
Driver Side



\* X, Y = 17,28.13



Origin (0,0) located at junction of toeboard and floorboard

Suggested Instrument Panel Profile Descriptors

Plane	X	Y	Angle (deg.)	Length
Lower Instrument Panel (3)	10.3	15.5	144.6	6.90
Center Instrument Panel (4)	15.9	19.5	96.9	8.87
Upper Instrument Panel (5)	17.0	28.3	0.9	10.42
Windshield (6)	0.0	29.75	147.0	27.5
Header (7)	27.0	48.0	157.0	6.5

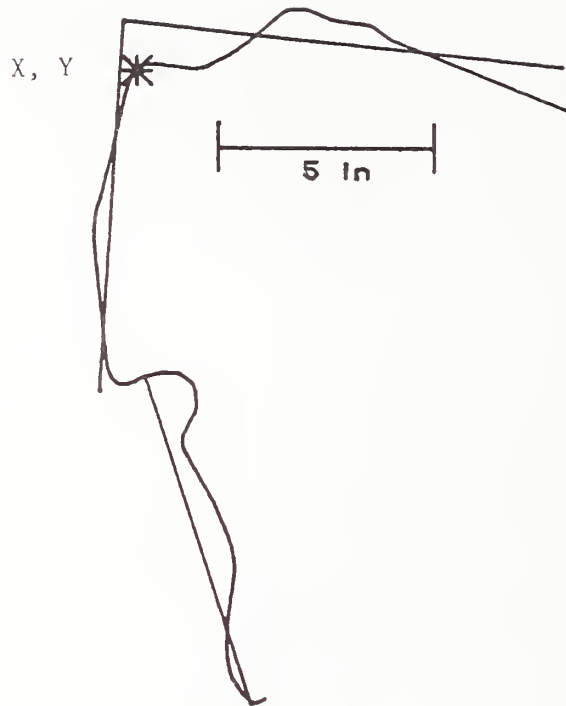
Number in parenthesis represents the corresponding contact plane number for the PADS2 Program.

Test \_\_\_\_\_

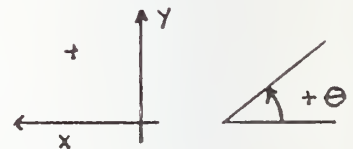
Date: January 15, 1985

Vehicle: Datsun 210

INSTRUMENT PANEL PROFILE  
Passenger Side



\* X, Y = 15.38, 26.88



Origin (0,0) located at junction of toeboard and floorboard

Suggested Instrument Panel Profile Descriptors

Plane	X	Y	Angle (deg.)	Length
Lower Instrument Panel (3)	<u>12.8</u>	<u>11.3</u>	<u>106.7</u>	<u>8.44</u>
Center Instrument Panel (4)	<u>16.3</u>	<u>19.0</u>	<u>86.3</u>	<u>9.11</u>
Upper Instrument Panel (5)	<u>15.7</u>	<u>28.1</u>	<u>353.8</u>	<u>10.25</u>
Windshield (6)	<u>3.0</u>	<u>29.0</u>	<u>144.0</u>	<u>23.5</u>
Header (7)	<u>27.0</u>	<u>48.0</u>	<u>155</u>	<u>4.5</u>

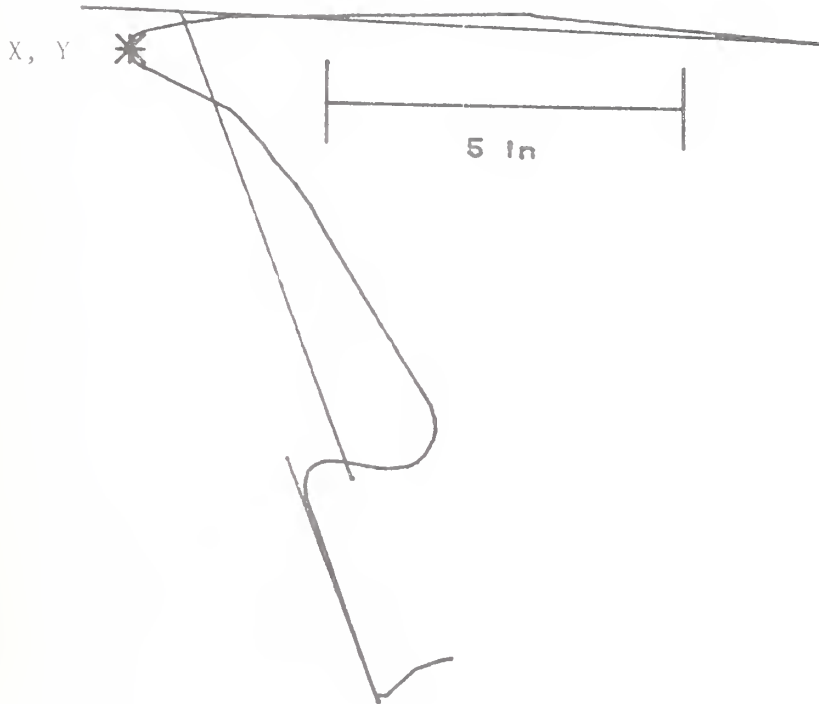
Number in parenthesis represents the corresponding contact plane numbers for the PADS2 Program.

Test \_\_\_\_\_

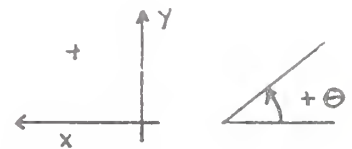
Date: January 15, 1985

Vehicle: Datsun 210

INSTRUMENT PANEL PROFILE  
Driver Side



\* X, Y = 13.75, 28.75



Origin (0,0) located at junction of toeboard and floorboard

Suggested Instrument Panel Profile Descriptors

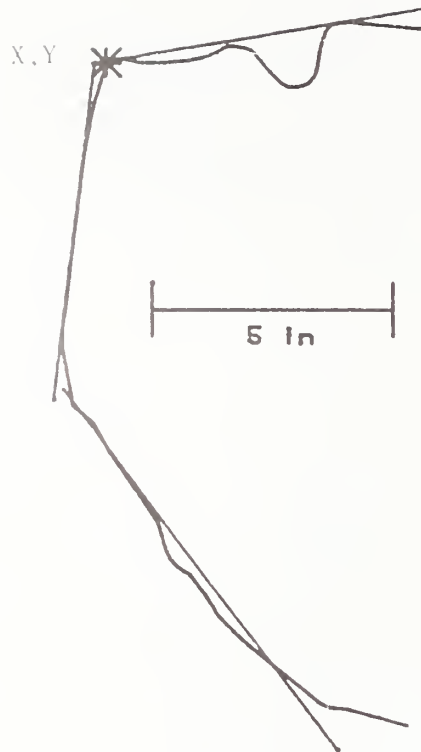
Plane	X	Y	Angle (deg.)	Length
Lower Instrument Panel (3)	<u>10.3</u>	<u>19.2</u>	<u>109.5</u>	<u>3.83</u>
Center Instrument Panel (4)	<u>10.6</u>	<u>22.5</u>	<u>109.6</u>	<u>7.25</u>
Upper Instrument Panel (5)	<u>14.4</u>	<u>29.4</u>	<u>358.0</u>	<u>10.36</u>
Windshield (6)	<u>3.0</u>	<u>29.0</u>	<u>144.0</u>	<u>23.5</u>
Header (7)	<u>27.0</u>	<u>48.0</u>	<u>155.0</u>	<u>4.5</u>

Number in parenthesis represents the corresponding contact plane numbers for the PADS2 Program.

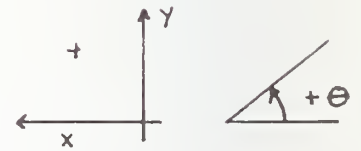
Test \_\_\_\_\_ Date: January 16, 1985

Vehicle: Pontiac LeMans

INSTRUMENT PANEL PROFILE  
Passenger Side



\*  $X, Y = 7.75, 26.5$



Origin (0,0) located at junction of toeboard and floorboard

Suggested Instrument Panel Profile Descriptors

Plane	X	Y	Angle (deg.)	Length
Lower Instrument Panel (3)	<u>3.2</u>	<u>11.25</u>	<u>125.4</u>	<u>9.82</u>
Center Instrument Panel (4)	<u>9.1</u>	<u>19.0</u>	<u>83.5</u>	<u>7.52</u>
Upper Instrument Panel (5)	<u>8.2</u>	<u>26.5</u>	<u>10.0</u>	<u>7.04</u>
Windshield (6)	<u>-1.0</u>	<u>28.0</u>	<u>148.0</u>	<u>27.5</u>
Header (7)	<u>21.0</u>	<u>42.0</u>	<u>159.0</u>	<u>5.25</u>

Number in parenthesis represents the corresponding contact plane numbers for the PADS2 Program.



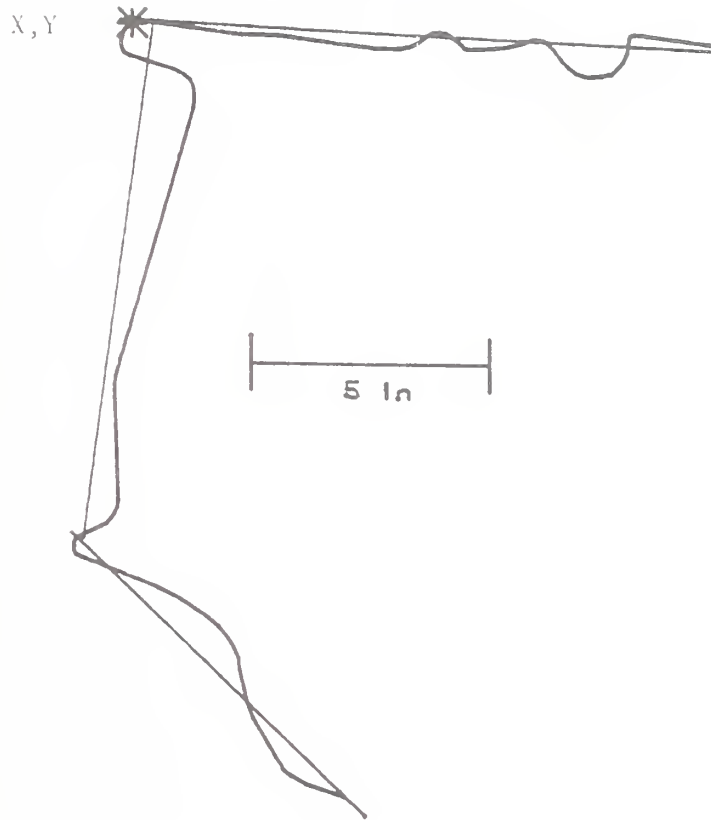
Test \_\_\_\_\_

Date: January 16, 1985

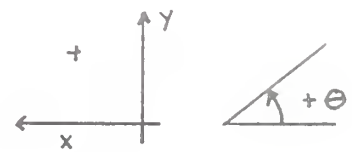
Vehicle: Pontiac LeMans

INSTRUMENT PANEL PROFILE

Driver Side



\* X, Y = 13.5, 27.49



Origin (0,0) located at junction of toeboard and floorboard

Suggested Instrument Panel Profile Descriptors

Plane	X	Y	Angle (deg.)	Length
Lower Instrument Panel (3)	8.63	10.0	134.4	8.75
Center Instrument Panel (4)	14.5	16.3	84.3	11.47
Upper Instrument Panel (5)	13.75	27.53	357.6	12.5
Windshield (6)	-1.0	28.0	148.0	27.5
Header (7)	21.0	42.0	159.0	5.25

Number in parenthesis represents the corresponding contact plane numbers for the PADS2 Program.

Test \_\_\_\_\_ Date: January 18, 1985

Vehicle: Chevy Nova

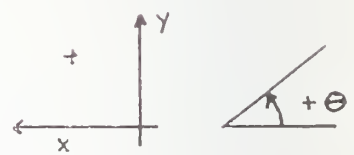
INSTRUMENT PANEL PROFILE

Passenger Side



$(x, y) = 13.125, 28.75$

$(0,0)$  located at junction of toeboard and floorboard



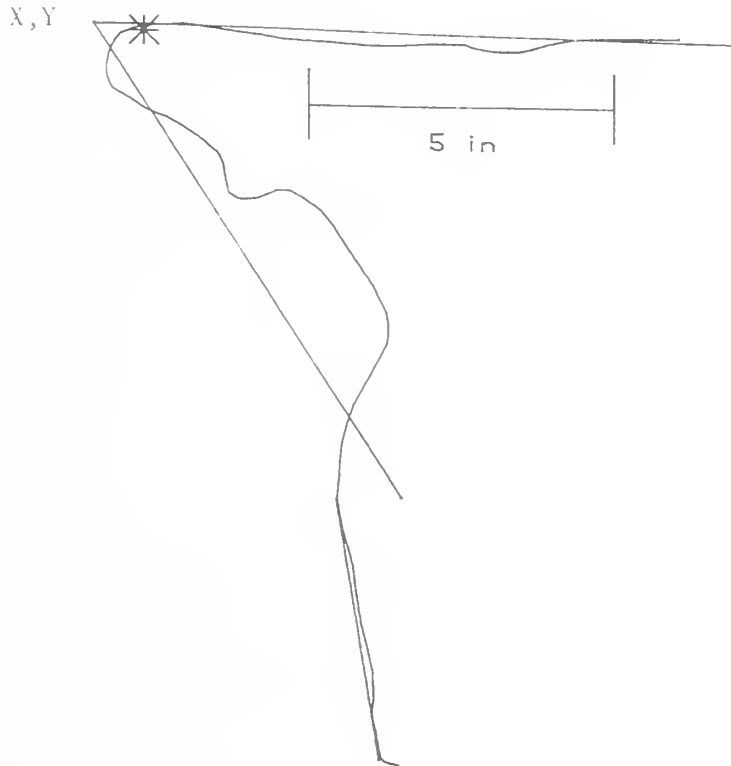
Suggested Instrument Panel Profile Descriptors

Plane	X	Y	Angle (deg.)	Length
Lower Instrument Panel (3)	7.0	14.5	126.2	10.38
Center Instrument Panel (4)	13.5	22.9	90.0	5.88
Upper Instrument Panel (5)	13.5	28.8	352.5	9.58
Windshield (6)	4.8	29.8	147.0	26.00
Rearview (7)	26.5	42.0	158.0	8.00

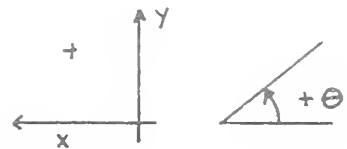
Number in parenthesis represents the corresponding contact plane numbers for the PADS2 Program.

Test \_\_\_\_\_ Date: January 18, 1985  
 Vehicle: Chevy Nova

INSTRUMENT PANEL PROFILE  
 Driver Side



\* X, Y =



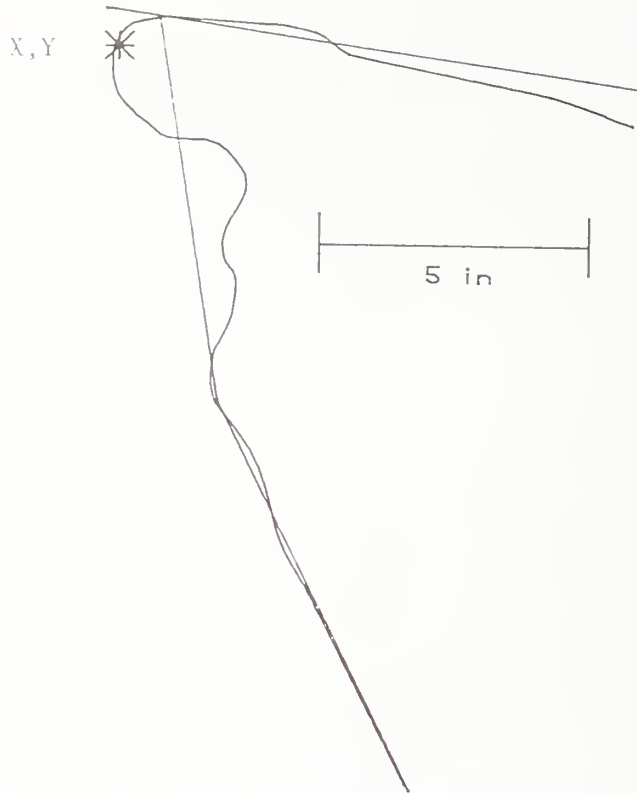
Origin (0,0) located at junction of toeboard and floorboard

Suggested Instrument Panel Profile Descriptors

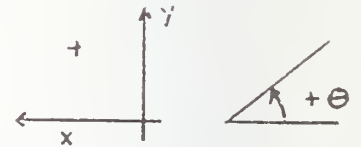
Plane	X	Y	Angle (deg.)	Length
Lower Instrument Panel (3)	<u>7.9</u>	<u>15.3</u>	<u>95.1</u>	<u>4.55</u>
Center Instrument Panel (4)	<u>7.5</u>	<u>19.8</u>	<u>121.6</u>	<u>9.54</u>
Upper Instrument Panel (5)	<u>12.5</u>	<u>27.9</u>	<u>358.6</u>	<u>10.50</u>
Windshield (6)	<u>4.8</u>	<u>29.8</u>	<u>147.0</u>	<u>26.0</u>
Header (7)	<u>26.5</u>	<u>42.0</u>	<u>158.0</u>	<u>8.0</u>

Number in parenthesis represents the corresponding contact plane numbers for the PADS2 Program.

INSTRUMENT PANEL PROFILE  
 Passenger Side



\* X, Y =



Origin (0,0) located at junction of toeboard and floorboard

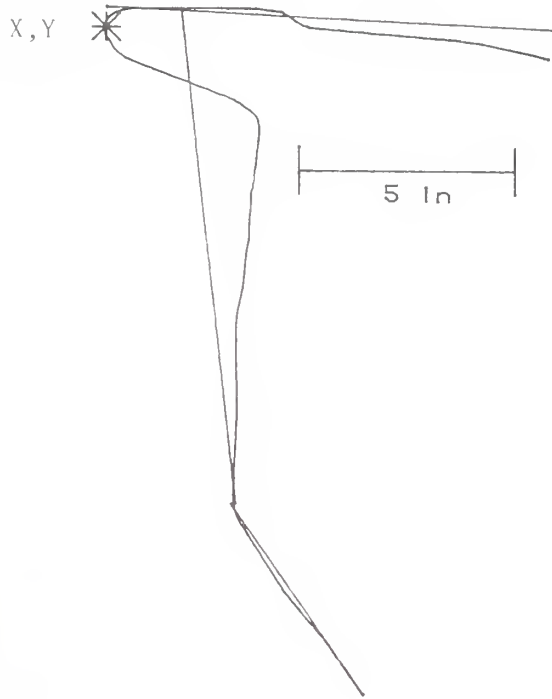
Suggested Instrument Panel Profile Descriptors

Plane	X	Y	Angle (deg.)	Length
Lower Instrument Panel (3)	10.8	14.8	115.4	8.47
Center Instrument Panel (4)	14.4	22.4	98.5	7.62
Upper Instrument Panel (5)	16.5	30.1	351.5	10.11
Windshield (6)	1.0	32.0	148.0	25.00
Header (7)	23.0	42.5	156.0	7.75

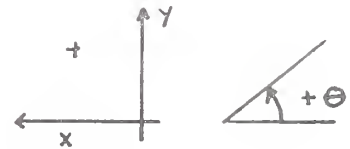
Number in parenthesis represents the corresponding contact plane numbers for the PADS2 Program.

Test \_\_\_\_\_ Date: January 24, 1985  
 Vehicle: Ford Granada

INSTRUMENT PANEL PROFILE  
 Driver Side



\* X, Y =



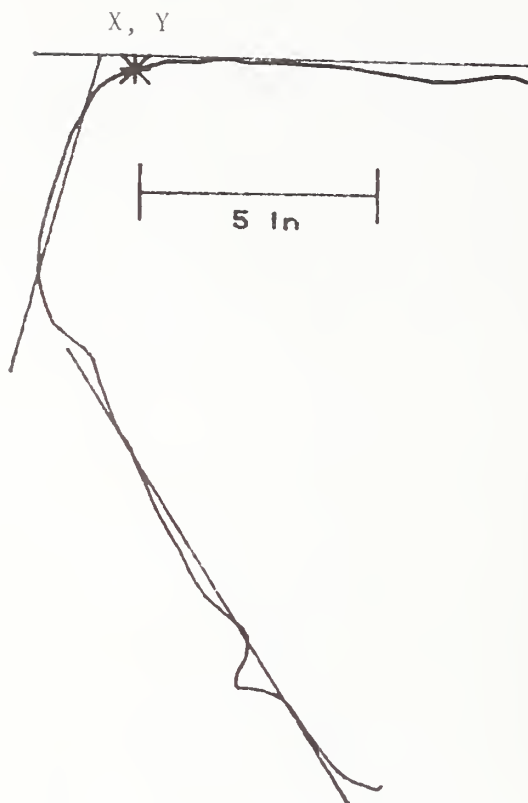
Origin (0,0) located at junction of toeboard and floorboard

Suggested Instrument Panel Profile Descriptors

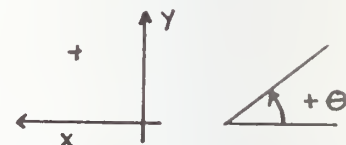
Plane	X	Y	Angle (deg.)	Length
Lower Instrument Panel (3)	<u>10.6</u>	<u>15.5</u>	<u>123.2</u>	<u>5.59</u>
Center Instrument Panel (4)	<u>13.5</u>	<u>19.8</u>	<u>95.9</u>	<u>12.26</u>
Upper Instrument Panel (5)	<u>16.5</u>	<u>32.0</u>	<u>357.3</u>	<u>10.51</u>
Windshield (6)	<u>1.0</u>	<u>32.0</u>	<u>148.0</u>	<u>25.00</u>
Header (7)	<u>23.0</u>	<u>42.5</u>	<u>156.0</u>	<u>7.75</u>

Number in parenthesis represents the corresponding contact plane numbers for the PADS2 Program.

INSTRUMENT PANEL PROFILE  
Passenger Side



\*  $X, Y = 14.125, 26.75$



Origin (0,0) located at junction of toeboard and floorboard

Suggested Instrument Panel Profile Descriptors

Plane	X	Y	Angle (deg.)	Length
Lower Instrument Panel (3)	9.5	10.5	121.0	11.66
Center Instrument Panel (4)	16.7	20.0	75.4	7.23
Upper Instrument Panel (5)	16.3	27.1	359.3	10.50
Windshield (6)	1.5	31.5	148.0	25.75
Header (7)	23.5	42.0	161.0	7.00

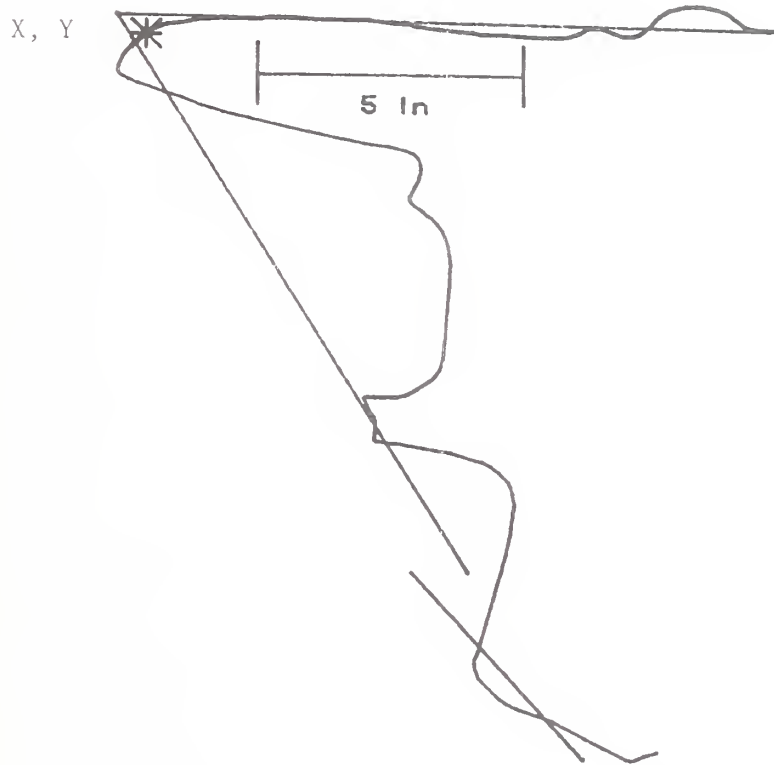
Number in parenthesis represents the corresponding contact plane numbers for the PADS2 Program.

Test \_\_\_\_\_

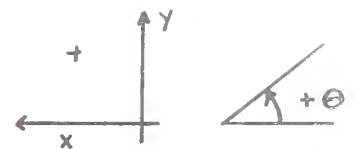
Date: January 28, 1985

Vehicle: 1979 Chrysler Cordoba

INSTRUMENT PANEL PROFILE  
Driver Side



\* X, Y = 14.0625, 27.75



Origin (0,0) located at junction of toeboard and floorboard

Suggested Instrument Panel Profile Descriptors

Plane	X	Y	Angle (deg.)	Length
Lower Instrument Panel (3)	5.9	13.5	138.9	4.91
Center Instrument Panel (4)	8.1	17.2	121.0	12.75
Upper Instrument Panel (5)	14.6	28.1	359.1	12.25
Windshield (6)	1.5	31.5	148.0	25.75
Header (7)	23.5	42.0	161.0	7.00

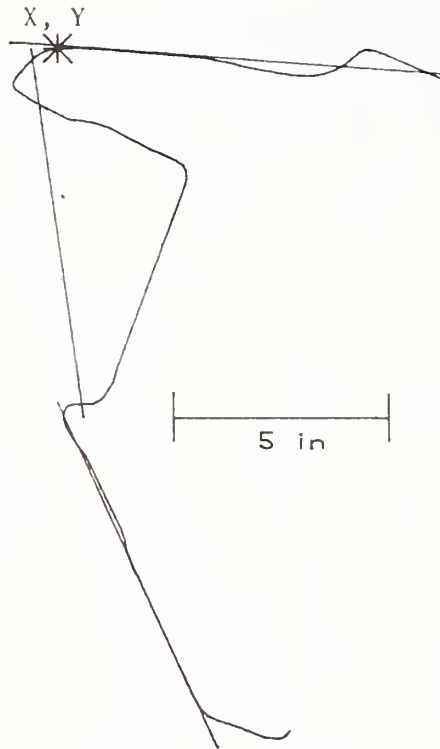
Number in parenthesis represents the corresponding contact plane numbers for the PADS2 Program.

Test \_\_\_\_\_

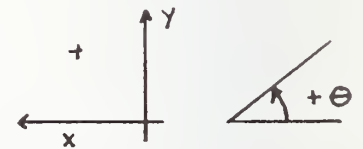
Date: January 30, 1985

Vehicle: Buick LeSabre

INSTRUMENT PANEL PROFILE  
Passenger Side



\* X, Y = 15.125, 27.125



Origin (0,0) located at junction of toeboard and floorboard

Suggested Instrument Panel Profile Descriptors

Plane	X	Y	Angle (deg.)	Length
Lower Instrument Panel (3)	<u>11.6</u>	<u>9.9</u>	<u>113.3</u>	<u>9.23</u>
Center Instrument Panel (4)	<u>14.6</u>	<u>18.0</u>	<u>97.2</u>	<u>9.20</u>
Upper Instrument Panel (5)	<u>16.3</u>	<u>27.3</u>	<u>355.8</u>	<u>10.15</u>
Windshield (6)	<u>0.0</u>	<u>29.8</u>	<u>144.0</u>	<u>27.00</u>
Header (7)	<u>22.0</u>	<u>43.0</u>	<u>164.0</u>	<u>7.50</u>

Number in parenthesis represents the corresponding contact plane numbers for the PADS2 Program.

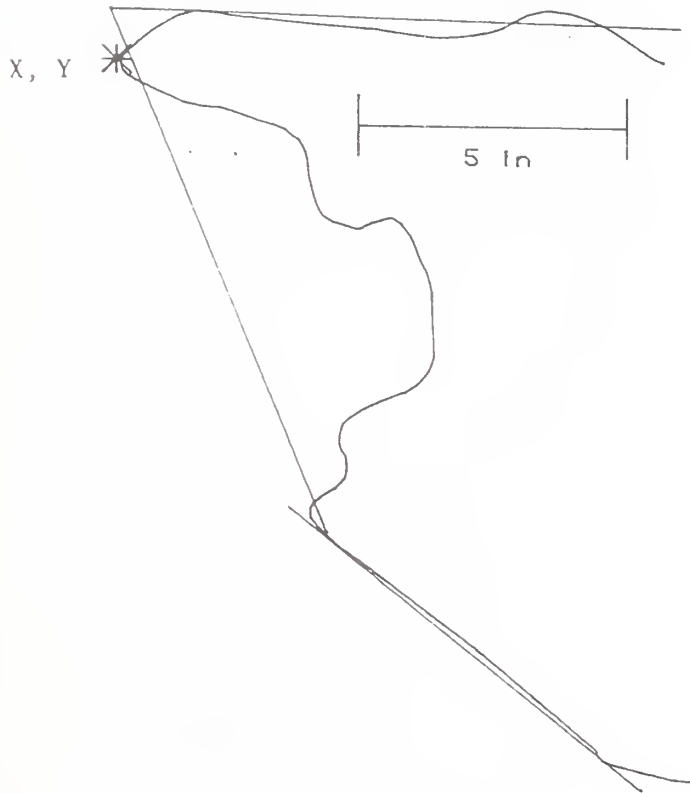


Test \_\_\_\_\_

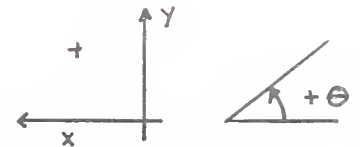
Date: January 30, 1985

Vehicle: Buick LeSabre

INSTRUMENT PANEL PROFILE  
Driver Side



\* X, Y = 15.5, 28.25



Origin (0,0) located at junction of toeboard and floorboard

Suggested Instrument Panel Profile Descriptors

Plane	X	Y	Angle (deg.)	Length
Lower Instrument Panel (3)	5.8	14.0	140.0	8.55
Center Instrument Panel (4)	11.6	19.0	111.4	11.01
Upper Instrument Panel (5)	15.6	29.3	358.7	10.63
Windshield (6)	0.0	29.8	144.0	27.00
Header (7)	22.0	43.0	164.0	7.50

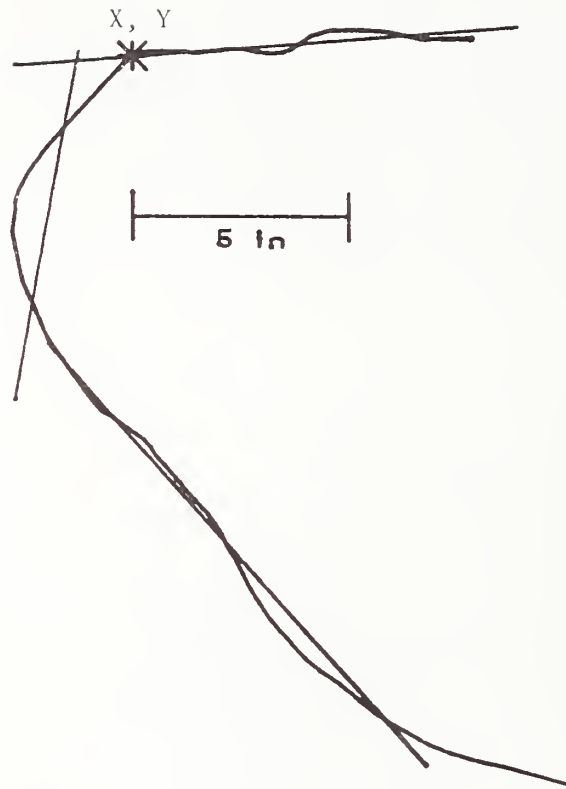
Number in parenthesis represents the corresponding contact plane numbers for the PADS2 Program.

Test \_\_\_\_\_

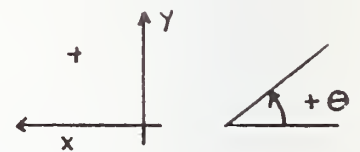
Date: February 12, 1985

Vehicle: V W Rabbit

INSTRUMENT PANEL PROFILE  
Passenger Side



\* X, Y = 5.5, 25.0



Origin (0,0) located at junction of toeboard and floorboard

Suggested Instrument Panel Profile Descriptors

Plane	X	Y	Angle (deg.)	Length
Lower Instrument Panel (3)	-1.3	7.5	130.0	13.59
Center Instrument Panel (4)	8.3	16.5	80.1	8.75
Upper Instrument Panel (5)	8.3	24.8	4.9	11.79
Windshield (6)	-5.0	26.0	128.0	25.00
Header (7)	15.0	42.0	157.0	3.75

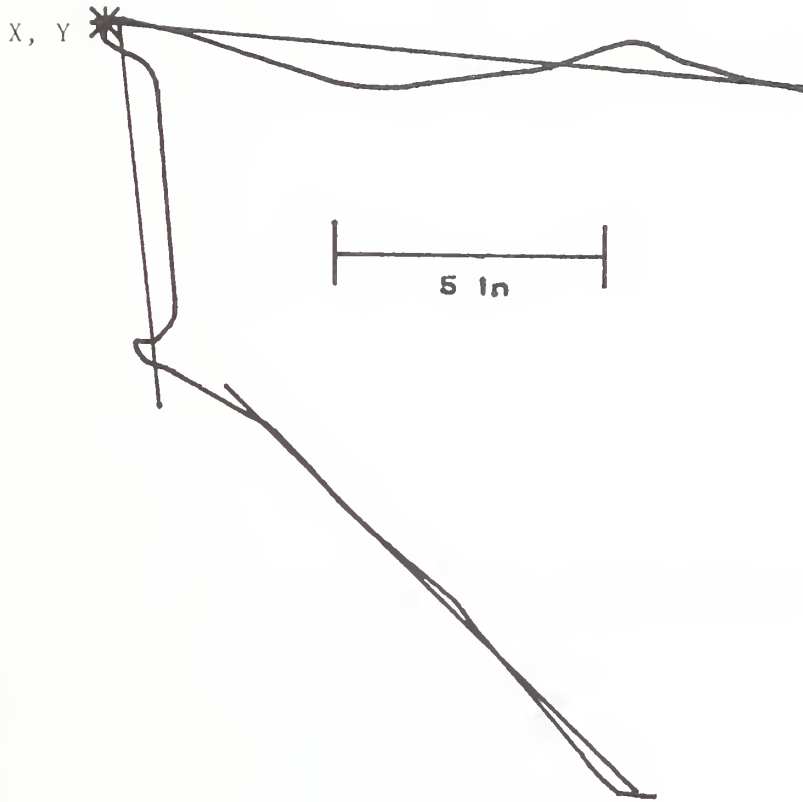
Number in parenthesis represents the corresponding contact plane numbers for the PADS2 Program.

test \_\_\_\_\_

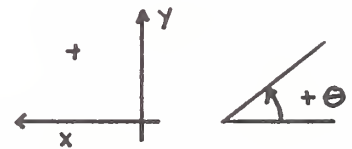
Date: February 12, 1985

Vehicle: V W Rabbit

INSTRUMENT PANEL PROFILE  
Driver Side



\* X, Y = 8.25, 23.5



Origin (0,0) located at junction of toeboard and floorboard

Suggested Instrument Panel Profile Descriptors

Plane	X	Y	Angle (deg.)	Length
Lower Instrument Panel (3)	-1.6	8.5	133.9	10.96
Center Instrument Panel (4)	7.2	16.0	96.0	7.64
Upper Instrument Panel (5)	8.3	23.5	355.2	13.09
Windshield (6)	-5.0	26.0	128.0	25.00
Header (7)	15.0	42.0	157.0	3.75

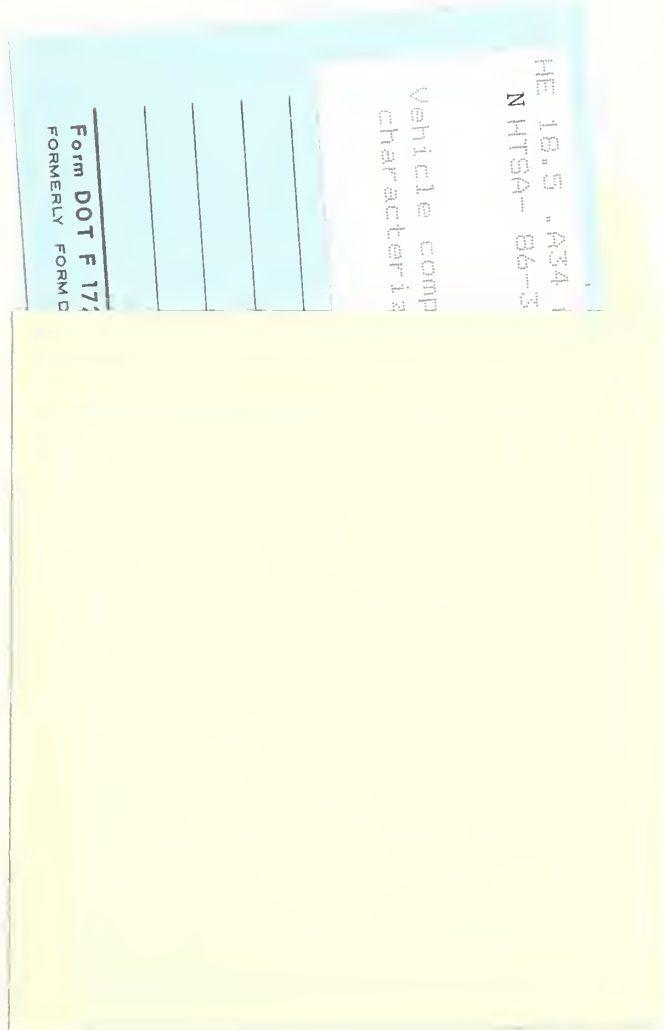
Number in parenthesis represents the corresponding contact plane numbers for the PADS2 Program.



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