

rt No. UMTA-MA-06-0025-77-16

DEVELOPMENT OF ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

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DECEMBER 1977 FINAL REPORT

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Prepared for

U.S. DEPARTMENT OF TRANSPORTATION URBAN MASS TRANSPORTATION ADMINISTRATION Office of Technology Development and Deployment Office of Rail Technology Washington DC 20590

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Technical Report Documentation Page

UMTA-MA-06-0025-77-16	2. Government Acces	sion No.	3. R	ecipient's Cotolog t	No.
4. Title and Subtitle				eport Date	
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L. R. Damskey and G. T. Gin	a			T-TSC-UMTA-7	
9. Performing Orgonization Nome and Addres	s		10. 1	York Unit No. (TRAI	5)
Bechtel Incorporated *				704/R8723	
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PREFACE

A study of the cost of construction of underground, rapid transit tunnels in soft ground was instituted under U.S. Department of Transportation contract DOT-TSC-1104. The scope of construction work to be considered was that:

- Between existing shafts or stations and
- Completion up to and including the pouring of all finished concrete

The study was completed through an estimation of tunneling hours and downtime hours to give an expected value, and distribution about that value, of the total shift hours involved from start to breakthrough of the tunnel. Additionally, some subjective factors influencing contingency and profit are presented.

The study was sponsored by the Office of Rail Technology of the Urban Mass Transportation Administration, the Transportation Systems Center under the direction of Mr. Andrew Sluz, the Technical Monitor. Mr. Joseph Keating, of Keating Associates, was the outside consultant and provided data for the effect of institutional factors.

Data from the Chicago tunnels were provided with the assistance of Messrs. R.I. Leland and S.J. Sulinski of the Metropolitan Sanitary District of Greater Chicago. Ing. Manuel Salvocho, of Ingenieros Civiles Asociados, S.A., kindly provided information on Mexico City tunnels. Other data were gathered and analyzed by Bechtel personnel; P.L. Shank (WMATA), N.N. Munnerlyn and F.E. Velez (BART) inspected hundreds of log sheets. Analysis of the data was performed principally by L.R. Damskey with the able assistance of V.J. Miller.

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METRIC CONVERSION FACTORS

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1. SUMMARY

Twenty-two tunnels from the San Francisco Bay Area Rapid Transit District (BART), the Chicago Metropolitan Sanitary District, and the Washington DC, Metropolitan Area Transit Authority (WMATA) have been analyzed to determine what factors influence the Rate of Advance (RoA) through the ground. The major effect is the increase in productivity achieved through the effect of the Learning Curve. Other effects, due to soil and equipment types, are multipliers to the basic equation.

Downtime for the various pieces of tunneling and muck-removal equipment are random events that are difficult to forecast, although trends were found and estimates determined.

An important aspect of the study was to quantify the variability of the rate of advance and down time calculations. The estimator does the same in a more subjective manner - each referring to his personal source of information to decide the effects of expected soils and equipment on the rate of progress through the ground. The results of our study in quantification of these variables are a step in the direction of understanding some of the tunneling cause and effect relations and giving the causes a numerical value. Quantification of these variables should reduce the size of the contingency applied by the bidding contractors to more meaningful terms of risk.

Data on the mining progress through the ground were of a poor quality. In order to provide better data for analysis from future tunnels, recommendations have been suggested for the tunnel (Ring & Face) log. At best, the recommended data acquisition will quantify the future tunneling rates. At worst, the analyst will be given a better subjective view of what occurred during tunneling.

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2. SELECTION OF COST ESTIMATING TECHNIQUES

2.1 REVIEW OF SYSTEMS ANALYSIS METHODS BASED ON COST ESTIMATES

Rapid transit tunneling is not an often repeated construction effort in which costs can be scaled to the next tunnel. Nor can a few inflation indexes be used to go from one time frame to a future period. And lastly, no two tunnels will have the same ground conditions and equipment uses. No two tunnels are the same!

Because of these differences, it seemed appropriate for the analysis to examine the tunneling systems and not their costs. Barring new technologies, some combination of personnel, equipment, and soils, taken from many experiences of the past, will be brought together for tunnels to be built in the future. Our effort, therefore, was to determine the individual contributions of each of the components. And with that knowledge, we can estimate the resources to be used for a specific future tunnel and price out the resources at their going market price at the time the tunnel is to be built. Escalation factors can be more accurately estimated on a component by component basis at that time.

2.2 SELECTION OF OPTIMUM COST ESTIMATING AND ANALYZING TECHNIQUES

The main components of a tunnel's construction are manhours, equipment depreciation and maintenance, and bulk materials.

• Bulk materials — concrete, rebar, grout materials — are largely a linear function of the tunnel's length.

2-1

- Equipment depreciation and maintenance should be available from historical records as well as from published data.
- Manhours represents the crew size multiplied by the shift hours from beginning to end. (The question is how many hours will be involved? Shift hours are composed of tunneling hours plus equipment shutdown hours.)

Estimates of tunneling hours based on linear feet per hour have not resulted in an adequate estimate. The main effort should be a systems analysis of the rate of advance (RoA) through the ground.

2.2.1 The Soils Estimate

A probability analysis relating core analyses to what was found during the tunneling should be conducted. Conditional probabilities, P (Soil B | Soil A), are based on the presence of one type to predict another. And Baysian probabilities can be used to increase the likelihood of predicting probable soil characteristics with the inclusion of additional data (new core samples).

All this can be displayed by a probability tree (1,2) to determine the soils most likely to be encountered at various distances through the ground.

2.2.2 Tunneling Equipment

Several different methods of face excavation are available: the onedirection rotating cutting wheel, the cutting wheel capable of reversal, the oscillating wheel (reputed to be no longer available), the digger arm (similar to a backhoe), and manual digging. Depending on how many types of excavating processes were to be found, Discriminate Analysis could be used to find which excavation process was likely to be used with which types of soil, tunnel length, and other tunnel parameters.

2.2.3 Mucking Equipment

Discriminate analysis could also be used to determine which muck transport system fits the other tunnel characteristics best.

2.2.4 Crew Size

Crew size and the various categories of skilled and unskilled crafts are expected to be a function of the equipment used. This can be found with a simple matrix having rows and columns of excavation and types of mucking equipment.

2.2.5 Rate of Advance (RoA)

Using the weekly advance rates as the dependent variable, regression analysis can be used to relate it with the many soil characteristics, equipment used, and primary liner types.

2.2.6 Downtime

Reliability theory, together with regression analysis, can be used to estimate the amount of time the equipment would be down and unavailable for tunneling operations. Maintenance costs are, of course, related to down time.

3. QUANTIFICATION OF FACTORS WHICH INFLUENCE CONSTRUCTION COSTS

3.1 PHYSICAL CHARACTERISTICS

The set of physical variables decided on, after reviewing several sets of tunneling data, were:

Tunnel Rate - ft/wk	Water Running in Tunnel – $1 \rightarrow 2$
Cumulative Feet of Tunnel to Date	Hp to Cutter/Digger
Tunneling Hours in Week	Total Jacking Potential of
Shield Down Time - hr/wk	Shield - tons
Excav Equip Down Time - hr/wk	OD of Shield - ft
Conveyor Down Time - hr/wk	Shield + Rotating Wheel - $1/2$
Muck Transport Down Time - hr/wk	Shield + Oscillating Arms - $1/2$
Misc Down Time - hr/wk	Shield + Digger Arm - 1/2
Admin Down Time - hr/wk	Shield + Manual Digging 1/2
Total Shift Time - hr/wk	Mucking Equip: Conv Belt + Train - 1/2
Silt & Clay - $1 \rightarrow 2$	Mucking Equip: Conv Belt + Truck - 1/2
Clay & Sand - $1 \rightarrow 2$	Mucking Equip: Rubber Tired Truck 1/2
Sand & Gravel - $1 \rightarrow 2$	Grnd: Non-Cohesive - $1 \rightarrow 2$
Cobbles & Boulders - $1 \rightarrow 2$	Grnd: Running $-1 \rightarrow 2$
Cemented - $1 \rightarrow 2$	Lining: Ribs & Lagging - 1/2
Peat & Trash - $1 \rightarrow 2$	Lining: Conc Pipe Jacked into
Cohesive - $1 \rightarrow 2$	Place - $1/2$
Tunnel Pressure - psig	Last Week of Tunneling = $1/2$

 $1 \rightarrow 2$: Varies between values of 1 and 2 1/2: A no/yes variable with a value of 1 or 2, usually

Based on the tunnels investigated, we believe these data items are adequate to describe the tunneling system and its RoA.

During the last six tunnels investigated, the soil was predominately sand with clay and with poor standup time. Some breasting was required, and consideration was given to adding this as another parameter. It was dropped because breasting was not the major cause of slowdown (even though

3-1

breasting did slow the RoA). The major cause was adequately described by the basic soil variables of Sand and Clay and Running Ground.

The quantification of the physical factors is discussed in Section 5 and 6, Analysis of Data and Predicting Equations.

3.2 INSTITUTIONAL EFFECTS

Institutional effects are generally subjective variables that enter into the contingency. To a large degree they are subjective because they are not directly measureable. The factors decided upon for this study are:

(1) Schedule/Time

Traditionally, bar charts have been used for scheduling; but these charts only show the time for beginning and end of activities. A network (CPM/PERT) chart shows the interrelation of activities which must be completed before another activity can start. Without this type of analysis, proper planning cannot occur; time overruns on subsequent activities are not likely to be understood.

(2) Direct Costs - Owner Acquisition

- Land and Rights-of-Way. Generally the owner can more expeditiously accomplish these activities (including the right of eminent domain). Entry to buildings and their preexcavation underpinning are also included.
- <u>Materials</u>. For items of equipment that will span more than one subcontract, procurement costs may be reduced, including the cost of financing monies.
- <u>Insurance</u>. The same rules would pertain to each subcontractor. The consistency of the policy and its jobwide scope should reduce the premium costs.
- <u>Building Permits</u>. This would not seem to be as cost sensitive to owner participation. Although

the reduction of personnel involved (owner and city agents) might expedite permit acquisitions, each must be processed individually. Negligible effect.

(3) Labor Productivity

Total job agreements are preferential so that each craft is responsible and is treated the same on each subcontract. It would appear to be more expeditious if the Owner negotiated the agreement and had it in hand by the time the bids were awarded.

It is expected that there are differences in productivity. Factors were investigated. Our findings indicate a wide range of subjectivity with little or no quantification of the indices.

The demand on a given labor market is believed to have an effect: e.g., if the building economy is booming in a specific area, additional demands on the local labor market are likely to be met with personnel of marginal productivity.

Compressed air work is subject to local labor negotiations. During the BART construction contracts 1M0031/1S0022, the generalized maximum hours of work were restricted by the air pressure to:

Max hr =
$$8.0-0.134$$
(psig) (3.1)

Labor negotiations resulted in an annual pay rate increase. For the three-year period, 1968 to 1971, and including the annual inflation index, the hourly wage rate is described by:

$$\$/Hr = \left[1.1036 \text{ (Max psig)}^{-0.0133}\right]^n \left\{\frac{1}{0.1715 - 0.0032 \text{ (Max psig)}}\right],$$
where: n = years since contract
was first in effect
(3.2)

The above applied to all union rates while under pressure. Foremen received \$4/shift in addition.

3-3/3-4

4. DATA DESCRIPTION

- 4.1 SOURCES. The data were found in the following forms:
 - 1. BART: 1M0031-MR, ML; 1R0053-RR, RL.

The excavation and downtime data had been summarized into weekly increments. Soil characteristics were taken from a soil profile and written verbal descriptions. Other data were in the tunnel report summaries.

2. BART: 1S0011-TR, TL, SR, SL; 1S0051A-SR, SL.

All data were obtained from rough logs: the ring erection log with two rings/page, the foreman's log, and a weekly advance summary.

3. Chicago Metropolitan Sanitary District: Upper Salt Creek tunnels 1, 2, and 3.

All data were taken from weekly data summaries, soil profiles, and written records of equipment used. In one case, it was necessary to contact the shield fabricator for data.

4. WMATA: 1F0012-FIB North Outbound, North Inbound, South Outbound, South Inbound; 1F0021-F2A Outbound, Inbound Branch Route Outbound, Branch Route Inbound; 1D0091-D9.

All data were taken from the ring report logs (one page/ ring), soil profiles, written rough logs, and oral communication with personnel involved in the tunnel excavations.

5. Mexico City Deep Sewer.

The data were received too late for study and analysis. The text is in Spanish and is appended (Appendix B) as a potential source of information. The tunnel characteristics were different enough to have been useful in the analysis.

Copies of the original data are found in Appendix A-1,2.

4.2 SOILS

Soils engineering suggested classifications other than those ultimately used. The difference lay in that the descriptions used by the face crew foreman were not those of a soils engineer, and the face crew foreman, for all his lack of exact scientific expertise, was in the hole and making a continuous log of the face conditions as he saw them. The categories finally used were:

- Silt and Clay
- Clay and Sand
- Sand and Gravel
- Cobbles and Boulders
- Peat and Trash
- Cemented
- Cohesive
- Running.

For each soil category, a value between 1 and 2 (0 to 100%) was to be assigned so as to describe the average face composition. The logged data did not permit the inclusive description, and in many cases the composition does not add to 100 percent. Fortunately, the transitory changes did not appear to have major effects on the RoA.

Running water affected the RoA whether the water was perched or from an unlowered water table. The quantity of flowing water was not metered. Our quantification became:

- 1.0 Dry
- 1.25 Moist
- 1.50 Wet
- 1.75 Running and impeding operations
- 2.0 Flooding and stopping operations.

4.3 PRIMARY LINING

All but one tunnel used either steel segmented rings or ribs and legging. The one exception was in Chicago's Upper Salt Creek No. 2 sewer intercept, where a 9.28-foot-diameter shield was used. The concrete lining, being both primary and finished, was lowered in segments through the nearest following shaft and jacked into place over a slip bed of wet bentonite. Later the bentonite was replaced with a cement grout.

4.4 MINING OPERATIONS

For each tunnel analyzed from the basic logged data, the time for the shove, the ring erection, and what is here called "dead time," was obtained. From these data, a pseudo RoA equation was developed for each tunnel involving the intercept and learning-curve exponent in the form of equation (5-1). Time and resources did not allow further analysis. It is suggested that further study of the data may disclose information that would permit the tunneling contractor to increase his efficiency for these operations.

4.5 DATA PROCESSING

In both the RoA and downtime estimating equations, the logic suggested that cumulative feet would be the dominant independent variable (in the latter equation, Σ ft represents time, most frequently found in reliability analyses), and all other independents would act as multipliers representing the perturbations around the relation between the dependent and independent variables. To accomplish this, the multiplier must have a value of 1 when the parameter in question has no effect; a "1" or a "2" was used in no/yes statements and a range of 1 to 2 was used to denote a characteristic that varied fractionally between 0 and 1.

4.6 GROUT

Only the BART 1S0011 TL/SL tunnel's grouting data were analyzed. Both pea gravel and cement grouts were used in the ratio of 1.54:1. The total grout consumption was 4.1 percent greater than the theoretical void left by the shield.

Although of minor cost, it may be possible to relate the consumption of grout to the soil types.

5. ANALYSIS OF DATA

5.1 BACKGROUND

Tunneling, taken in its entirety, comprises so many diverse activities that it soon became obvious that it would be necessary to divide it into subtasks that were basically homogeneous in order to model each as a unit operation. The resulting concept is shown in Figure 5-1.

The activities within the dotted line framework are concerned only with nonmonetary resources.

- The tunnel length defines the quantities of bulk materials to be used. It also influences the choice of tunneling equipment and influences the RoA.
- Soil characteristics and primary liner types both influence the tunnel equipment choice and affect the rate of advance.
- Tunnel equipment sets the crew size, influences the contractor's capital costs, and affects the RoA.
- The above then set the RoA and have a large effect on equipment reliability.
- From the RoA, the tunneling hours are estimated.
- Equipment reliability estimates the downtime hours.
- The combination of crew size, tunneling, and down hours provides the estimate of nonexempt crew manhours.
- Current costs are then applied to estimate the tunneling cost without contingencies and profit.
- Institutional factors (identified contingencies), unidentified contingencies, and profit are applied to reach a total cost.

• Throughout the calculations, an error of estimate is carried. The various costs (the result of the average values for all the above) and their variations are combined in a risk model (Monte Carlo) simulation to obtain a range of total costs and the probability of the occurrence of each.

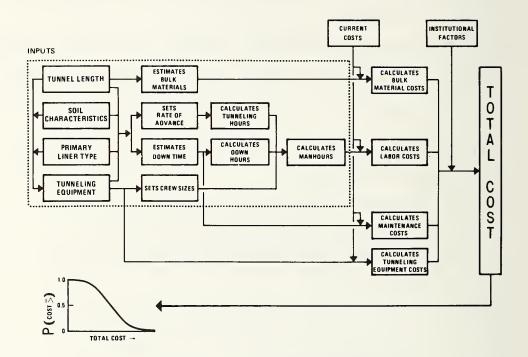


Figure 5-1. Economic Factors in Tunnel Construction

5.2 LEARNING CURVE

Literature research on Rate of Advance analysis yielded little in the way of mathematical analysis. Several authors mentioned that the RoA increased as the crews learned to work together and equipment deficiencies were eliminated.⁽³⁾ One author⁽⁴⁾ used the term "Learning Curve." An analytical approach is given by Pietrzak and McJunkin⁽⁵⁾ based on hard-rock tunneling. Although these authors do not provide details of their model's logic, it does appear that there may be similarities between their model and the work being reported on here. The concept of a learning curve where subsequent repetitive work is achieved at a higher rate of productivity is certainly not new.⁽⁶⁾ The airplane frame industry found that with their mixture of manual and machine work, an 80-percent curve, on the average, defined their increase in productivity. That is, each time the number of airframes produced was doubled, the last unit required only 80 percent as much time as the reference unit. In the case of tunneling, using the average learning curve exponent found for all the tunnels studied, 82.3 percent, and an initial rate of 4.0 hours/foot, the following rates might be expected.

Cumulative Feet of Tunnel	Hours/foot	Feet/hour(RoA)
1	4	0.25
2	3.29(4x0.823)	0.30
4	2.71(3.29x0.823)	0.37
:	•	•
128	1.02(1.243x0.823)	0.98
•		•
1024	0.57(0.693x0.823)	75
2048	$0.47(0.57 \times 0.823)$	2.13
4096	0.39(0.47x0.823)	2.59

In general, industry has found that the degree of learning depends on the mixture of men and machines used. Figure 5-2 describes the change in learning curve, as reported by Hirschmann,⁽⁷⁾ with the percentage of manual effort used in the specific task.

It seemed obvious that the learning curve should apply to the repetitive tasks of the shove and primary ring erection. Theoretically, the learning curve should be a continuous negative-sloping curve. In actual practice, interruptions to the work (equipment failures, planned shutdowns, etc) as well as modifications to the tasks (different soils, substitution of new equipment) occur to change the position of the curve. A new soil might displace the curve. New equipment might merely involve an upward perturbation and then a rapid increase in productivity to again reach the former curve position.

In general, what might have been expected from a theoretical "learning curve" approach to the analysis is what was found for the RoA in softground tunneling.

An example of the persistence of the Learning Curve was found in the BART RR/RL tunnels. Upon completion of the RR tunnel, the shield was immediately moved to the RL tunnel and tunneling continued. Except for an initial perturbation to the RoA, the advance rate quickly fell into line with the rate being achieved at the completion of the RR tunnel.

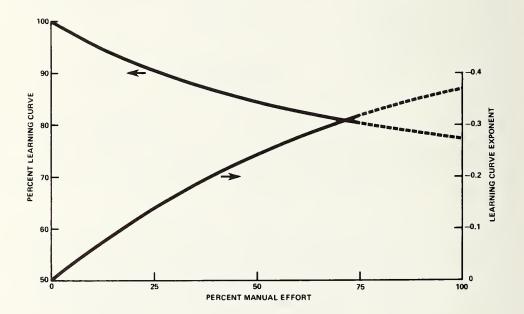


Figure 5-2. Relation Between the Percentage Mix of Manual and Machine Effort, Percent Learning Curve, and Learning Curve Exponent

5.3 PRELIMINARY ANALYSIS

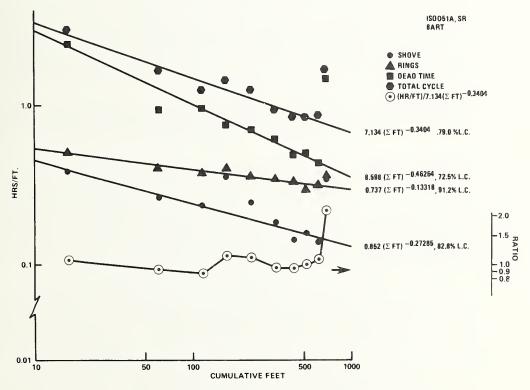
In order to explore the learning-curve concept, raw data for several tunnels were plotted; Log (hr/ft) vs Log (cumulative ft), Figure 5-3. The learning-curve function is of the form

$$hr/ft = I(\Sigma ft)^{E}$$
(5.1)

wh

here:
$$\Sigma$$
 ft = cumulative feet
I = hr/ft for the first foot of excavation
E = the learning-curve exponent
Hr/ft = (RoA)⁻¹
and: Percent learning curve = 100 exp (E * Ln 2) (5.2)

Data sets for the first three tunnels had been summarized into weekly units of data; therefore, all subsequent data accumulations were kept in a weekly format. The dependent variable (hr/ft) is the weekly tunneling hours, exclusive of any down time, divided by the feet of advance accomplished during the week.



Tunneling Rate of Advance vs Cumulative Tunnel Length Figure 5-3.

The independent variable (Σ ft), in order to be compatible with the weekly average characteristics of the dependent variable, is calculated as the cumulative sum through the previous week's excavations plus half of the current week's distance.

The data can then be regressed to determine the values of I and E. The resultant equation can then be considered to be a rate equation

$$\frac{d(hr)}{d(ft)} = I(\Sigma ft) E$$
(5.3)

and can be integrated between distances n and n + m.

d (hr) =
$$I \int_{n}^{n+m} (\Sigma ft)^{E} d(ft)$$
 (5.4)

For reasons that will be discussed later, valid results will not be obtained by integration between zero and the total number of feet in the tunnel; integration should be in parts to conform to the types of soils and other perturbations expected to be encountered during the excavation.

By calculating the number of hours required to excavate the tunnel and given the crew size, the number of tunneling manhours is estimated.

However, equipment does fail. And when the equipment is down for repair (or, for that matter, whenever there is a shutdown), the crew is usually on standby and must be paid. Therefore, it is necessary to estimate the downtime that may be encountered. Reliability theory has found that equipment generally responds as shown in Figure 5-4.

In developing a failure-rate function, the dependent variable was defined as hrs down/ft and the major independent variable as cumulative feet; both specified in weekly terms as before. A predicting equation to develop the number of downtime hours during the tunnel excavation will permit the estimation of crew manhours idled. The sum of the tunneling and downtime hours is an estimate of the non-exempt payroll and the time duration of the tunneling.

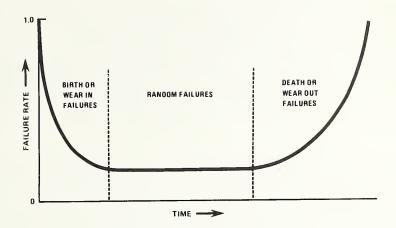


Figure 5-4. Typical Equipment Failure Rate Curve with Time

It is of primary importance to note that the Rate of Advance is not assumed (as is normally done). It is calculated, based on the conditions expected to be encountered. Among those conditions are the soil characteristics (either from a decision-tree estimate or a coreboring profile) and the equipment to be utilized.

Figure 5-1 shows the cost calculation logic. It is expected that, once the soils and tunnel length are specified, the tunneling and mucking machinery ranges are considerably reduced. And when the machinery is decided upon, barring labor union restraints, the crew size is determined. On the basis of the foregoing evolved concepts, some details of the analytical work will now be discussed.

5.4 METHOD OF ANALYSIS

Regression analysis was used to determine the effects of the so-called "independent" variables on the dependent variable, hr/ft. Independent variables should be independent from each other but, in commercial practice, a high degree of interdependence is usually found among these factors; i.e., a high degree of statistical randomness among the variables might well indicate a poorly managed project.

In fact, the lack of independence, when analyzing the individual tunnel data, resulted in the derivation of some learning-curve exponents that were considered to be impossible. The method of getting around this problem was to plot each tunnel's hr/ft vs Σ ft on log-log paper. The obvious outliers could then be eliminated. Outliers, in this sense, means those data points which are displaced from the negatively sloping line due to some other variable effects, such as a change in soils, a series of mechanical breakdowns, etc. The remaining data sets were then related, using only a desk calculator, to solve for the I and E of each tunnel.

The next step in the analysis was to find the effects of the remaining variables. The logic suggested that the effects of the other variables would be as multipliers; therefore, the regression used the logarithms of the variables.

$$\operatorname{Ln}\left(\frac{(\operatorname{hr/ft})}{I(\Sigma \operatorname{ft})^{E}}\right) = f(\operatorname{Ln} X_{1}, \operatorname{Ln} X_{2}, \dots, \operatorname{Ln} X_{n})$$
(5.5)

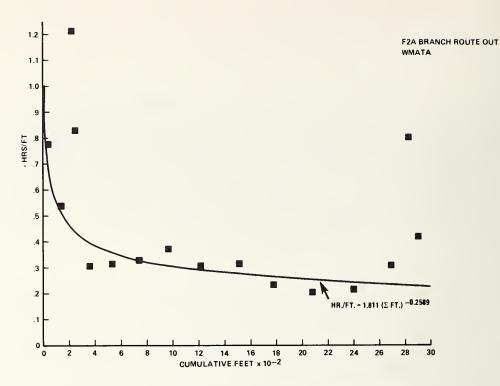
The above reasoning was tried on several tunnels. The following set of figures demonstrates an example from one of the WMATA tunnels. Figure 5-5 is the plot of hr/ft vs Σ ft. Figure 5-6 is a logarithmic plot of the same data with the assumed outliers circled. Figure 5-7 is a transformation of the dependent variable to the form used in equation (5.5) vs Σ ft; the learning-curve effect on productivity has been removed. The data have now been normalized and all data sets are scattered about a horizontal axis having a value of 1.0. Figure 5-8 is a plot of the unexplained residual (reported-predicted)* vs Σ ft after regressing in the form of equation (5.5).

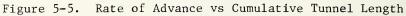
The scale of the ordinate is the same as that of Figure 5-7. It can be seen, in comparing Figures 5-7 and 5-8, that the variance from the horizontal line is greatly reduced in the latter. It appears that regression analysis can develop a mathematical model that will satisfactorily estimate a tunneling Rate of Advance.

To determine how closely the tunneling hours can be duplicated, a different set of tunnel data were regressed to estimate the weekly Rate of Advance. The corrections due to soils, equipment failures, etc., are fractional multipliers whose effects are different depending upon the numerical value of hr/ft.

Two methods were used in the calculation. One was to integrate the derived equation between the weekly stations. The other was to multiply hr/ft by the weekly advance. The results are shown in Figure 5-9.

^{*}Note that the word "reported" is used rather than the usual word "actual" in calculating the unexplained residual. In general, the reported data were extremely doubtful in character. In one case, the soil changed from sand and clay to sandy clay and back again as the shifts changed. And sometimes, damp, wet, or moist sand was used interchangeably. Throughout our investigation into the raw logged data, it was obvious that little or no attention had been given to consistent observation and logging of data. And certainly no thought had ever been given to the possible future use of the data in a quantified analysis.





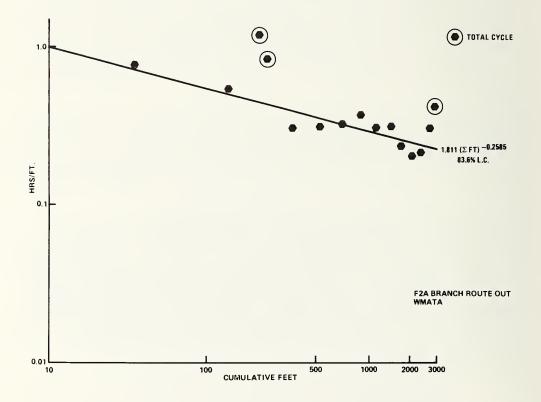


Figure 5-6. Tunneling Rate of Advance

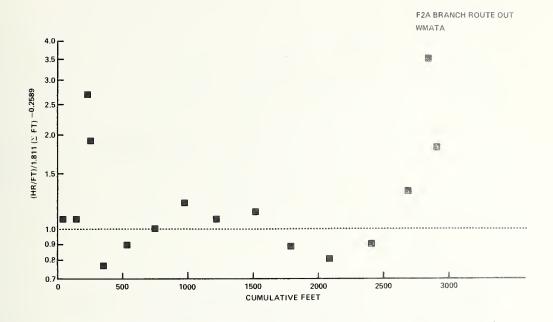


Figure 5-7. Tunnel Length; Unexplained Variations in Rate of Advance

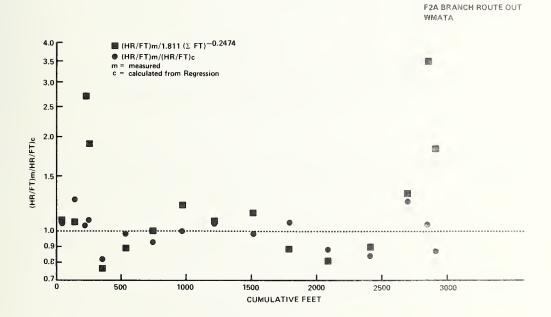
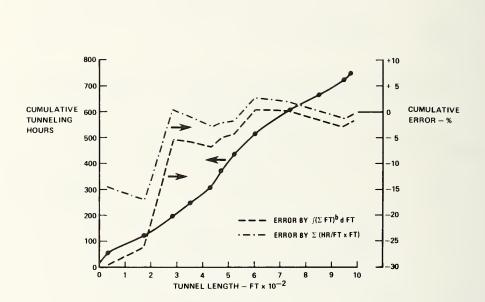


Figure 5-8. Reduction in Variance due to Equipment, Soil, and Length of Work-week Variables



F1B NORTH IN WMATA

Figure 5-9. Comparison of Calculated and Reported Cumulative Tunneling Hours vs Tunnel Length

In the integration case, the error was 2.2 percent - 749.4 hours reported vs 766.0 hours calculated. In the summation case, the error was 0.7 percent - 749.4 hours reported vs 754.6 hours calculated. Again, the logic of the model development appeared to satisfactorily duplicate the reported tunneling hours.

5.4.1 Cross Tunnel Derivations

RoA equations were derived for several individual tunnels in order to investigate potential problems which might occur when all the data were combined. For instance, there were statistical outlier data points in the individual tunnel data for which there were no explanatory variables.

- An error could have occurred in the dependent variable, hr/ft. The lineal tunneling distance was probably correct, because both the starting and finishing stations were always compared with the number of rings erected. The error was most likely in the tunneling hours; i.e., shutdowns had occurred and were not reported or were incorrectly reported. This would result in too great a value for hr/ft in this data set.
- Errors in the independent variable could (and did) occur because of incomplete tunneling data logs; e.g., the soil characteristics changed and were not reported.

These outlier data were generally removed from the regression data before combining all data sets.

The combination of all the tunnel excavation data, with all the soil and equipment variations, permitted the derivation of an RoA equation that could not be derived with the limited variations in soil characteristics and single equipment sets found in individual tunnels. Additionally, the RoA equation used the intercepts and learning-curve exponents derived from the individual tunnel data.

Both the intercepts and learning-curve exponents appeared to be functions of soils, equipment, and the managerial expertise of the contractors.

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No data to classify the expertise existed; therefore calculations were restricted to soils and equipment. Both derived equations gave statistically satisfactory results.

Substitution of I and E into the RoA equation permits the hr/ft to be calculated. Two methods were used to calculate the tunneling (operating) hours: integration and summing of finite units of tunneling feet.

The RoA equation (6.3) is derived in Section 6.3. For the purpose of this discussion, consider the equation to be of the form

F = A consolidation of all correction factors.

Calculation of the tunneling hours requires that the tunnel be broken into sectors of roughly equivalent soil expectations. Correction factors are then calculated for each sector. The weekly averages were used here.

5.4.2 Integration Method

Equation (5.6) is integrated between stations d and d+i along the tunnel. Each sector is considered. The tunneling hours are calculated by

$$hrs_{ii} = I F_{i} \int_{d}^{d+i} (\Sigma ft) \bar{e} d (ft)$$
(5.7)

to obtain

$$hrs_{ii} = \frac{IF_i}{E+1} (\Sigma ft) \begin{bmatrix} E+1 \\ d \end{bmatrix}^{d+i}_d$$
(5.8)

Total tunneling hours are the sum of the sector hours

Total Hours =
$$\sum_{i=1}^{j} (hr)_i$$
 (5.9)

5.4.3 Summation Method

The only difference in summation is the calculation of the sector hours; they are now estimated by using equation (5.6) directly and multiplying by the number of feet, m, in the sector, i.

hrs
$$_{ie} = ft_i | F_i (\Sigma ft_d + 0.5 ft_i) |^E$$
 (5.10)

The modification to the variable Σ ft is due to the RoA derivation useing the average rate during a sector having average correction characteristics. To conform to this logic, the cumulative feet of progress were taken to be half *c*he distance m in sector i plus the total distance excavated up to the beginning of sector i. Total tunneling hours are as in equation (5.9).

The two methods of estimating the total tunneling hours are shown, for each tunnel analyzed, in Appendix A-3.

5.4.4 Total Down Time

To estimate the total hours required to excavate the entire length of the tunnel, the amount of non-tunneling hours due to equipment failures and administrative shutdowns must be added to the tunneling hours. Total down time was fitted to an equation of the form shown in Figure 5-4. Because of the random nature of the failures, the equation fit is less satisfactory, statistically, than other derived equations. The results, on a tunnel-by-tunnel basis, are shown in Appendix A-4.

It was intended to derive equations to describe the failure rates of the various excavation systems; i.e., the shield, the rotating wheel/ digger arm, the mucking system, etc. Although the information is available in the data bank, insufficient time and resources precluded their derivations. Certain of these downtimes are needed in the RoA equation; e.g., shield, excavating equipment, misc. and administrative down hours/ft of advance. In addition, they are also needed to estimate maintenance costs. The latter could not be found as a separate category. Until the equations become available, the program user will continue to rely on his own data and that published by the AGC in their <u>Contractors'</u> Equipment Manual (7th Ed. 1974).

5.4.5 Total Hours

Total hours is the sum of tunneling and downtime hours. On a tunnelby-tunnel basis, Appendix A-5 shows total hours, by both the integration and summing methods compared with actual hours.

5.4.6 Variability of Predictions

The only certainty about estimating is that a single monetary projection is bound to be too high or too low when compared to the final actual costs. A more useful estimate will cover the range into which the final results will probably fall. The range may be estimated subjectively by the estimator using the knowledge and background of those familiar with the task to be performed. Or, as will be discussed here, it may be quantitatively estimated from the errors of estimate produced from the statistical procedures used in deriving the equations.

A method of imputing the range is known as Monte Carlo simulation.⁽⁸⁾ In this procedure, an equation is solved many times, and each time the equation is solved, each independent variable's coefficient is randomly

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changed within the confines of each coefficient's statistical variation. In this manner, the equation, or process series, is solved enough times to permit the estimation of the distribution of the answers. The curve in the lower left corner of Figure 5-1 illustrates the result of such a simulation.

The weekly progress rate, in hr/ft., is an example of tunneling variability. The median progress value is that rate most likely to occur. However, there is approximately a 50-percent chance that this value will be exceeded. Note that Figure 5-10 is not a normal distribution; it is approximately log normal. The cumulative distribution of these data is shown in Figure 5-11 where the median RoA was 0.60 hr/ft (1.67 ft/hr). At the 80-percent probability level, the RoA was 1.125 hr/ft (0.89 ft/hr) or less. And at the 20-percent probability level, the RoA was 0.325 hr/ft (3.08 ft/hr) or less.

The variability of the tunneling hours, using equation (5.8), would now be estimated, for the integration method, by

$$hrs_{ii} = \frac{(\mathbf{I} \pm \mathbf{r}, \sigma_{1}) e^{(\mathbf{Ln} \mathbf{F}_{i} \pm \mathbf{r}_{2} \sigma_{F})}}{(\mathbf{E} \pm \mathbf{r}_{3} \sigma_{E}) + 1} \left[\Sigma \text{ ft} \right]^{(\mathbf{E} \pm \mathbf{r}_{3} \sigma_{E}) + 1} d^{d+i}$$
(5.11)

and for the summation method, by

$$hrs_{is} = ft_i (I \pm r_1 \sigma_i) e^{(LnF_i \pm r_2 \sigma_F)} (\Sigma ft_d + 0.5 ft_i)^{(E \pm r_3 \sigma_F)}$$
(5.12)

where:

 σ = standard error of estimate of the individual

predicting equations

Total downtime hours are calculated by

D hrs_i = ft_i e
$$(\text{Ln DH}_1 \pm r \sigma_{\text{DH}})$$
 (5.13)

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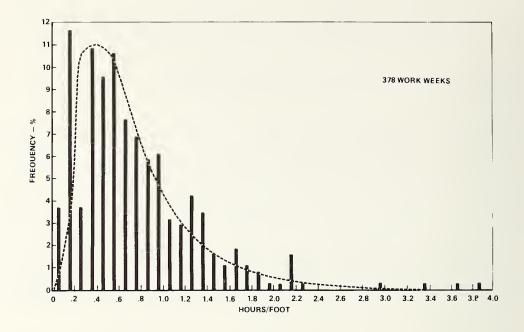


Figure 5-10. Distribution of Weekly Average Rates of Advance

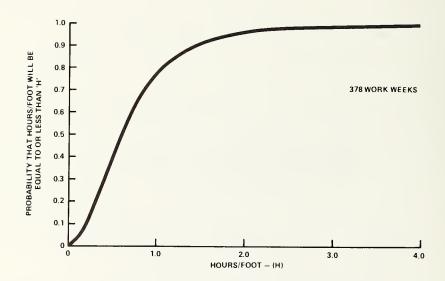


Figure 5-11. Cumulative Distribution of Weekly Average Rates of Advance

Equations (5.11) through (5.13) calculate the distribution of hours for sector i. To obtain the total hours over the tunnel's length, equation (5.9) is increased to include the individual sectors' variability. To do this it will be necessary to calculate the variance of the estimate for each sector, i, sum the variances over the sectors, and then take the square root of the sum. This is the standard error of estimate of the total hours.

$$\sigma_{i}^{2} = \frac{\Sigma (hr_{i}^{2}) - (\Sigma hr_{i})^{2}/N}{N-1}$$
(5.14)

hr_{i} = Hours calculated for sector i

N = Number of iterations used to calculate the

where;

N = Number of iterations used to calculate the distribution of hours

The total hours variation, or standard error, is

$$\sigma_{\Sigma hr} = \begin{bmatrix} i \\ \Sigma \\ i = 1 \end{bmatrix}^{0.5}$$
(5.15)

Equation (5.9) is now modified by adding the results of equation (5.15) to obtain

Total hours
$$= \sum_{i=1}^{j} (hr)_{i} \pm \begin{bmatrix} j \\ \Sigma \\ i=1 \end{bmatrix}^{0.5}$$
(5.16)

The distribution of total in-the-hole hours is calculated from equation (5.16).

The above means of estimating the tunneling and downhours are based on random occurrences during normal operations; extraordinary events were excluded from the analysis. For instance, on one pair of parallel tunnels, the shield passed through shafts at 12.5 and 44.5 percent of the total tunnel distance. The contractor opted to spend about two weeks at each shaft on each tunnel for shield and excavator wheel maintenance and modifications. In addition, when the shields were within 200 feet of the tunnels' ends, forward progress was halted as the station was not ready for the breakthrough.

5.4.7 Other Costs

After the total shift hours are estimated, crew staffing and current labor costs are combined to estimate the labor cost distribution. Data on staffing were obtained for most of the tunnels. Properly, the possible variance in both the staffing and labor costs are estimated and combined with total hours variance, using the technique of the propagation of error (variance), to calculate the labor cost distribution.

The parameters of tunnel length, anticipated soil characteristics, and primary liner types are expected to influence the selection of equipment for excavation and mucking.

In the time available, maintenance costs, either total or on individual items of equipment, could not be found. It is not known whether these costs are individually itemized or are buried in other operating costs.

The effect of not quantifying crew, equipment, and maintenance costs, either because all or part of the data were not available or could not be found, results in a void in the calculation procedure. These data are normally available to contractor's estimators from the contractor's properietary information data bank. The disadvantage to the proposed calculation procedure is that the information can not be weighed to benefit from the experience of many tunneling operations. We believe that future studies should find and analyze these histories.

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6. PREDICTING EQUATIONS

Derivation of the predicting equations was accomplished by stepwise multiple regression. The first equation computer run, after eliminating variables that logic suggested should not be included, was to determine the correlation coefficients between the individual remaining independent variables and those data sets that appeared to be outliers (due to a lack of explanatory variables or just poor data). Outlier data were eliminated on the preliminary tunnel-by-tunnel runs.

A technique used to reduce intercorrelation between variables is to create new variables by adding and subtracting; e.g., if X_1 and X_2 are highly correlated, it may be possible to find coefficients for each that are less correlated or completely independent by adding the new variables X_3 and X_4 to the regression matrix, where

$$x_3 = x_1 + x_2$$

 $x_4 = x_1 - x_2$

If the regression results included all four variables, such that

 $Y = a + b X_1 + cX_2 + d X_3 + e X_4$

the resulting coefficients for X_1 and X_2 would be for

$$X_1: b + d + e$$

and for

 X_2 : c + d

The above technique was used for all correlation coefficients > \pm 0.3. Unfortunately, this procedure does not directly give coefficient standard errors of estimate. In the example above, an error of estimate is calculated for all four variables.

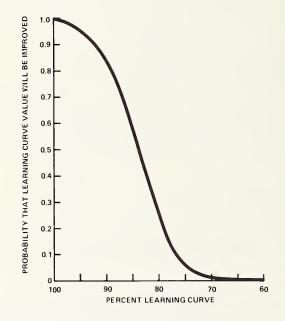


Figure 6-1. Distribution of Learning Curve Values

6.1 THE RATE OF ADVANCE EQUATION LEARNING CURVE EXPONENT

The Learning Curve Exponent varied from tunnel to tunnel; the average for the 21 tunnels was -0.281 (an 82.3 percent curve) with a standard deviation of 0.071. The cumulative distribution of the exponents found is shown in Figure 6-1. Because of the large variation in the exponent, a means of predicting is required. Managerial control undoubtedly has a large influence on the exponent (a measure of productivity) but was unknown for analytical purposes. We were quite aware of the potential value of such a subjective measure of supervisory control; however, in past attempts to quantify this variable after-the-fact, it was found that the inclusion was usually statistically nonsignificant. Nor did personnel want their gradings recorded. The subject is noted here to signify that the variable was recognized as meaningful.

In section 3.1 it was stated that the symbols $1 \rightarrow 2$ and 1/2 mean that a parameter either has an assigned value which varies between 1 and 2 or has a yes/no value of 1 or 2. The 1,2 variation was chosen for computational reasons rather than a 0,1 range, and is used in this and subsequent derived equations.

Equation (6.1) gives some quantitative insight into the effects of the independent variables on the rate of productivity increase. For instance,

- Increasing the work week from 40 to 80 hours is about a 19% increase in the exponent. A further increase to a 120-hour work week has a marginal increase of only about 9 percent. The rationale might be that the discontinuance of starting and stopping daily operations is reflected in the tunneling productivity exponent.
- Tunneling in running water (a value of 1.75 assigned) vs tunneling in moist ground (1.25) reduces the productivity rate exponent by approximately 250 percent.
- The productivity exponent is bettered by increasing the jacking potential, and it is reduced with the cross section area of the shield.

• Except for the coefficients for soil cobbles and boulders, and for peat and trash (for which there were insufficient data), the effects of soils on the productivity rate can be estimated.

Table 6-1 shows the exponent observed for the individual tunnels, the predicted value, and their differences.

LEARNING CURVE EXPONENT = -0.5538 - 0.00938 *

Ln (Total Shift Hr/Wk) + 0.03025 * Ln (Silt and Clay: 1 \rightarrow 2) - 0.03271 *

Ln (Cobbles and Boulders: $1 \rightarrow 2$) + 0.06094 * Ln (Cemented Ground: $1 \rightarrow 2$) - 0.23648 *

Ln (Peat and Trash: $1 \rightarrow 2$) + 0.03254 * Ln (Cohesive Ground: $1 \rightarrow 2$) - 0.03254 *

Ln (Running Ground: $1 \rightarrow 2$) + (1.02192 * Ln (Water Running at Face: $1 \rightarrow 2$) – 0.05555 *

Ln (Tunnel Working Pressure – Psia) – 0.03964 * Ln (Jacking Potential – Tons/ft²)

+ 0.17693 * Ln (OD of Shield - ft) + 0.04705 *

Ln (Shield and Wheel: 1/2) + 0.05597 * Ln (Shield and Digger Arm: 1/2) - 0.04746 *

Ln (Conveyor Belt and Trusk: 1/2) + 0.04705 * Ln (Rubber Tired Muck Vehicle: 1/2);

$$S_{\rm u} = 0.051$$
 $R^2 = 0.9699$

(6.1)

Table 6-1

System	Contract	Tunnel	Observed Value	Predicted Value	Difference
BART BART BART BART BART BART BART Chicago Chicago	1M0031 1M0031 1R0053 1S0011 1S0011 1S0011 1S0051A 1S0051A 68-404-2S 68-405-2S	MR ML RR/RL TR TL SR SL SR SL USC #1 USC #2	-0.2920 -0.2501 -0.2343 -0.2706 -0.3977 -0.2363 -0.3621 -0.3404 -0.3940 -0.4016 -0.3385	-0.2875 -0.2741 -0.2461 -0.3215 -0.2904 -0.2805 -0.3295 -0.3472 -0.3317 -0.3345 -0.3391	$\begin{array}{c} -0.0045\\ 0.0240\\ 0.0018\\ 0.0509\\ -0.1073\\ 0.0442\\ -0.0326\\ 0.0068\\ -0.0623\\ -0.0671\\ 0.0006\\ 0.0006\\ 0.0006\end{array}$
Chicago WMATA WMATA WMATA WMATA WMATA WMATA WMATA	68-406-2S 1F0021 1F0021 1F0021 1F0012 1F0012 1F0012 1F0012 1F0012 1F0012 1D0091	USC #3 F2A Out F2A In F2ABR Out F2ABR In F1B No. Out F1 No. In F1 So. Out F1B So. In D9 So. In	-0.2415 -0.2764 -0.2192 -0.2589 -0.3158 -0.2229 -0.2673 -0.1287 -0.2055 -0.2476	-0.3215 -0.2578 -0.2607 -0.2811 -0.2777 -0.1914 -0.2324 -0.1825 -0.1839 -0.2268	$\begin{array}{c} 0.0800 \\ -0.0186 \\ 0.0415 \\ 0.0222 \\ -0.0381 \\ -0.0315 \\ -0.0349 \\ 0.0538 \\ -0.0216 \\ -0.0208 \end{array}$

COMPARISON OF ESTIMATED AND PREDICTED LEARNING CURVE EXPONENT

Based on Individual Tunnels, the: Standard Error of Prediction: 0.0462 Amount of variability Removed by Predicting Equation: 55.4%

6.2 THE RATE OF ADVANCE EQUATION INTERCEPT

Each tunnel not only had a different learning curve exponent, but also had a different intercept value (the theoretical time to mine the first foot). The mean value of all the data was 3.815 with a standard deviation of 2.557 hr/ft. The cross tunnel computer run was made prior to the inclusion of all the data (322 data sets vs 388 finally available). Time and resources prevented a final run.

The derived equation (6.2) is given below. Table 6-2 shows the individual tunnel's observed intercept as well as that predicted.

$$\begin{aligned} \text{Intercept} &= 0.4121 * \begin{pmatrix} \text{Silt} \text{ and } \text{Clay} \\ 1 \rightarrow 2 \end{pmatrix}^{0.2215} * \begin{pmatrix} \text{Clay} \text{ and } \text{Sand} \\ 1 \rightarrow 2 \end{pmatrix}^{0.1216} * \\ \begin{pmatrix} \text{Sand} \text{ and } \text{Gravel} \\ 1 \rightarrow 2 \end{pmatrix}^{0.1928} * \begin{pmatrix} \text{Peat and } \text{Trash} \\ 1 \rightarrow 2 \end{pmatrix}^{-1.2698} * \begin{pmatrix} \text{Cemented Ground} \\ 1 \rightarrow 2 \end{pmatrix}^{0.146} * \\ \begin{pmatrix} \text{Cohesive Ground} \\ 1 \rightarrow 2 \end{pmatrix}^{0.208} * \begin{pmatrix} \text{H}_2\text{O at } \text{Face} \\ 1 \rightarrow 2 \end{pmatrix}^{0.2069} * \begin{pmatrix} \text{Tunnel Pressure} \\ 1 \rightarrow 2 \end{pmatrix}^{-0.1276} * \\ \begin{pmatrix} \text{Running Ground} \\ 1 \rightarrow 2 \end{pmatrix}^{0.3538} * \begin{pmatrix} \text{Shield and Wheel} \\ 1 \rightarrow 2 \end{pmatrix}^{0.0716} * \begin{pmatrix} \text{Shield and Digger arm} \\ 1 \rightarrow 2 \end{pmatrix}^{0.2068} * \\ \begin{pmatrix} \text{Shield and Manual Digging} \\ 1 \rightarrow 2 \end{pmatrix}^{0.5694} * \begin{pmatrix} \text{Conveyor Belt and Train} \\ 1/2 \end{pmatrix}^{-0.2784} * \\ \begin{pmatrix} \text{Conveyor Belt and Truck} \\ 1/2 \end{pmatrix}^{-0.4136} * \\ \begin{pmatrix} \text{Rubber Tired Vehicle} \\ 1/2 \end{pmatrix}^{1.5395} * \\ 1/2 \end{pmatrix}^{-1.1369} * \\ \begin{pmatrix} \text{Ribs and Lagging} \\ 1/2 \end{pmatrix}^{-1.1369} * \begin{pmatrix} \text{Concrete Pipe Jacked In} \\ 1/2 \end{pmatrix}^{-2.6217} * e^{-7.3957 * \text{E}} \\ \text{R}^2 = 0.925, \text{ Ln S}_{\text{Y}} = 0.1956 \end{aligned}$$

Table 6-2

System	Contract	Tunnel	Observed Value	Predicted Value	Difference
BART BART BART BART BART BART BART BART	1M0031 1M0031 1R0053 1S0011 1S0011 1S0011 1S0051 1S0051 68-404-2S 68-405-2S 68-406-2S	MR ML RR/RL TR TL SR SL SR SL USC #1 USC #2 USC #3	2.497 2.391 9.314 3.035 6.754 2.811 7.856 7.134 8.553 3.476 0.722 0.783	2.692 2.689 10.661 5.045 5.368 3.823 5.136 6.338 10.639 1.961 0.716 1.675	-0.195 -0.298 -1.347 -2.010 1.386 -1.012 2.720 0.796 -2.086 1.515 0.006 -0.892
WMATA WMATA WMATA WMATA WMATA WMATA WMATA WMATA WMATA	1F0021 1F0021 1F0021 1F0021 1F0012 1F0012 1F0012 1F0012 1F0012 1F0012	F2A Out F2A In F2ABR Out F2ABR In F1B No. Out F1B No. In F1B So. Out F1B So. In D9 So. In	2.390 2.353 1.811 2.928 3.083 3.456 1.776 2.108 4.879	3.194 3.624 2.488 3.007 2.431 2.872 2.398 2.453 4.217	-0.804 -1.271 -0.677 -0.074 0.652 0.584 -0.622 -0.345 0.662

COMPARISON OF ESTIMATED AND PREDICTED RATE OF ADVANCE INTERCEPT

Based on Individual Tunnels, the:

Standard Error or Prediction: 1.201

Amount of Variability Removed by Predicting Equation: 76.8%

Some conclusions that can be inferred about the initial Rate of Advance from the equation are:

- Relative to the clay and sand category,
 - silt and clay is about 7 percent slower,
 - sand and gravel is about 5 percent slower,
 - cemented ground is about 2 percent slower,
 - cohesive ground is about 6 percent slower,
 - running ground is about 17 percent slower.
- Compared with the rotating cutting wheel, and where soil conditions will permit alternate excavation methods,
 - the digger arm is about 10 percent slower,
 - manual digging is about 41 percent slower
- Compared with a conveyor belt and tram for muck removal,
 - a conveyor belt and truck are about 9 percent faster,
 - a rubber-tired vehicle is about 35 percent slower.
- The initial rate is inversely proportional to the learning curve exponent (E).

6.3 RATE OF ADVANCE EQUATION

The large matrix size, 115 real and created variables, required the location of a computer program with larger capacity. The time delay reduced the time available for analysis. Although equation (6.3) predicts with a high degree of accuracy, improvements can be made by manipulation of data and the inclusion of new types of soils (no glacial till soils were included).

The predicting equation (6.3) is given below. Table 6-3 shows the standard error of estimate, based on equation (6.3), for each tunnel.

$$\begin{aligned} & \operatorname{Hr/Ft} = I\left(\Sigma F t\right)^{E} * \left[\left(\frac{\operatorname{Total Dwn Hr}}{Ft} + 1 \right)^{0.4095} * \left(\frac{\operatorname{Shield Dwn Hr}}{Ft} + 1 \right)^{0.1088} * \left(\frac{\operatorname{Admin Dwn Hr}}{Ft} + 1 \right)^{0.1088} * \left(\frac{\operatorname{Admin Dwn Hr}}{Ft} + 1 \right)^{0.0095} * \left(\frac{\operatorname{Admin Dwn Hr}}{Ft} + 1 \right)^{-0.3783} * \left(\frac{\operatorname{Admin Dwn Hr}}{Ft} + 1 \right)^{0.643} * \left(\frac{\operatorname{Silt \& Clay}}{1 \to 2} \right)^{-0.192} * \left(\frac{\operatorname{Clay \& Sand}}{1 \to 2} \right)^{-0.192} * \left(\frac{\operatorname{Sand \& Gravel}}{1 \to 2} \right)^{0.2468} * \left(\frac{\operatorname{Cobbles \& Boulders}}{1 \to 2} \right)^{-0.1753} * \left(\frac{\operatorname{Cemented G 'nd}}{1 \to 2} \right)^{0.25} * \left(\frac{\operatorname{Cobesive Grnd}}{1 \to 2} \right)^{-0.22} * \left(\frac{\operatorname{Jacking Potential}}{\operatorname{Tons}/Ft^{2}} \right)^{-0.1766} * \left(\frac{\operatorname{O D Shield}}{Ft} \right)^{0.942} * \left(\frac{\operatorname{Shield \& Digger Arm}}{1/2} \right)^{-0.138} * \left(\frac{\operatorname{Shield \& Ma \ nual Digging}}{1/2} \right)^{0.1284} * \left(\frac{\operatorname{Rubber Tired Vehicle}}{1/2} \right)^{-0.41} * \left(\frac{\operatorname{Ribs \& Lagging}}{1/2} \right)^{0.438} * \left(\frac{\operatorname{Concrete Pipe}}{1/2} \right)^{1.105} * \left(\frac{\operatorname{Last Week}}{1/2} \right)^{0.8074} * 0.10377 \right] \\ S_{Y} = 0.294 \quad R^{2} = 0.72 \end{aligned}$$

 $S_{\gamma} = 0.294$ R² = 0.72 Ln S_F = 0.4094 (the variables between the square brackets)

Table 6-3

Tunnel System	Contract	Tunnel Number	Standard Error Relative to Equation 6.3
BART	1M0031	MR	.277
	1M0031	ML	.204
	1R0053	RR/RL	.358
	1S0011	TR	.429
	1S0011	TL	.587
	1S0011	SR	.279
	1S0011	SL	.493
	1S051A	SR	.305
	1S051A	SL	.391
Chicago	68-404-2S	USC #1	.218
	68-405-2S	USC #2	.159
	68-406-2S	USC #3	.041
WMATA	1F0012	F1B No. Out	.242
	1F0012	F1B No. In	.452
	1F0012	F1B So. Out	.232
	1F0021	F1B So. In	.177
	1F0021	F2A Out	.279
	1F0021	F2A In	.293
	1F0021	F2A B.R. Out	.253
	1F0021	F2A B.R. In	.257
	1D0091	D9 So. In	.403

RATE OF ADVANCE PREDICTION ERROR OF ESTIMATE

Average

0.270

Amount of variability removed by predicting equation 71.8%

The errors are logarithmically distributed. USC #3 is not in the log normal distribution; without USC #3, the Mean = 0.297.

Some interesting observations may be made relative to the effect of certain correction factors.

Equation (6.3) suggests that soils effects on the RoA, from greatest impediment to greatest ease of progress, would be: cemented ground, sand and gravel, running ground, cobbles and boulders, silt, clay and sand mixes, cohesive ground. Logic doesn't support the above order. The cobbles and boulders should be a higher order and probably resulted in its position (and exponent) due to interactions with more favorable conditions in the few data sets in which they appeared. Statistically, considering the numerical values of the derived exponents and their individual errors of estimate, the first three soils are different from the last three, but in the two groups of three there is not much difference.

The RoA is increased with increasing jacking potential and decreased with increasing diameter of the shield.

The last week of tunneling is inefficient relative to the RoA.

There are correlation interactions between the various down times as well as the equipment in use. Table 6-3 shows the standard error of estimate by individual tunnels.

6.4 TOTAL DOWNTIME EQUATION

Total downtime per foot of mining was not a good prediction — the event appears to be too random. Reliability theory suggests that a U-shaped curve, Figure 5-4, should describe the events with time, and the regression, equation (6.4), was done in that form. However, because of the poor fit of the equation, it is suggested that the average downtimes, hr/ft, may be used. For all equipment failures, the averages are shown in Table 6-4.

 $(TOTAL DOWN HOURS + 0.001)/Ft = 4.5054 \times 10^{-3} Exp[-5.0536 \times 10^{-5} * (\Sigma Ft) - 1.3573 \times 10^{-7} \times$

 $(\Sigma Ft)^2 + 2.1773 \times 10^{-11} * (\Sigma Ft)^3 + 0.85647 * (Silt and Clay: 1 \rightarrow 2) + 0.67523 *$

(Clay and Sand: $1 \rightarrow 2$) + 0.82934 * (Sand and Gravel: $1 \rightarrow 2$) + 0.30376 *

(Cobbles and Boulders: $1 \rightarrow 2$) – 1.27427 * (Cohesive Ground: $1 \rightarrow 2$) + 1.28616 x 10⁻³ *

(Total Jacking Potential of Shield - Tons) - 0.18252 * (OD Shield - Ft) + 2.66974 *

(Shield and Cutting Wheel: 1/2) + 0.80838 * (Shield and Digger Arm: 1/2) - 1.46578 *

(Conveyor Belt and Train: 1/2) - 0.39557 * (Rubber Tired Truck: 1/2)];

 $R^2 = 0.174$, $Ln S_v = 1.9563$ (6.4)

Table 6-4

Category	Average Hr/Ft Down	Standard Deviation	σ/μ [*]
Total Hours	0.1720	0.3718	2.16
Shield	0.0249	0.0878	3.53
Excavating Equipment	0.0440	0.2410	5.48
Conveyor	0.0113	0.0404	3.04
Muck and Other Transportation	0.0166	0.0789	4.75
Miscellaneous	0.0697	0.1459	3.53
Administrative	0.0089	0.0400	4.49

AVERAGE DOWNTIME - HR/FT

*The coefficient is a relative measure of the variability of the data about the mean. A satisfactory value, for nominal use, would be less than 0.5.

A further investigation into the total down hours is shown in Figure 6-2. The plot between cumulative total down hours and cumulative feet of tunnel suggests a relationship that could be developed and would involve the cumulative history of soils penetrated, and the equipment types in use, as well as the shield diameter and jacking potential in tons/ft².

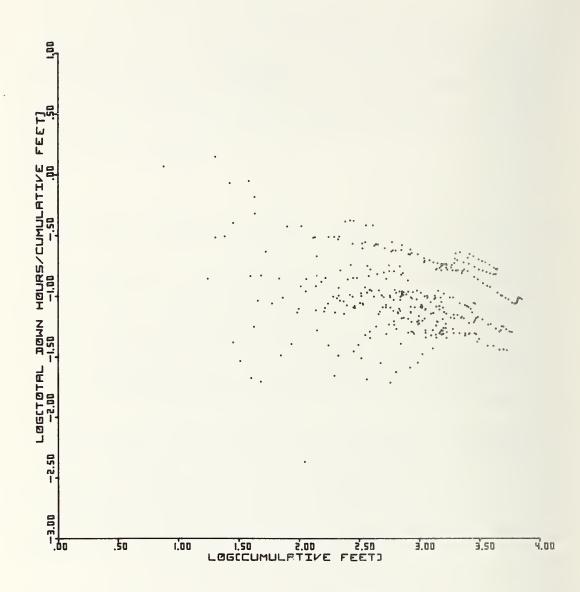


Figure 6-2. Total Downtime as Related to Cumulative Feet of Tunneling

6.5 OTHER DOWN HOURS

The "other equipment down hours" were investigated plotwise and are shown merely to display their potential as a means for prediction.

Figure 6-3 shows the downtime for the excavating cutting wheel used on the Chicago USC No. 1 tunnel.

Figures 6-4, 5(a), 5(b), 6 and 7 indicate the cumulative downtime hours vs cumulative tunneling feet for the shield, excavating equipment, miscellaneous, and administrative down hours.

Statistical analysis of these data would likely develop usable predicting equations except for predicting the shield and administrative down hours. These events appear to be completely random.

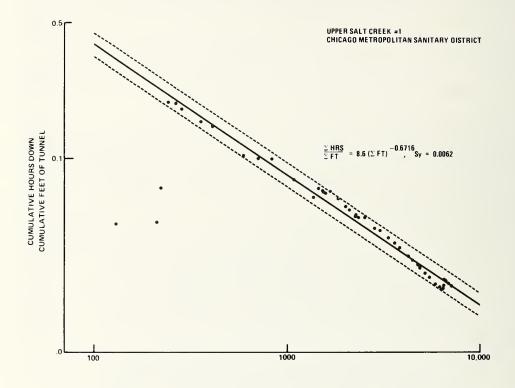
The conclusion that may be drawn from Figures 6-2 to 6-7 is that

- There appears to be a linear relation between down hours and cumulative distance of tunneling (time) for total down hours, excavating equipment, and miscellaneous hours. Statistical analysis of the data would be expected to result in a useful predicting equation,
- The shield and administrative down hours appear to be random events not correlated with tunneling distance (time). Under these circumstances, the mean and standard deviation of downtime (Table 6-4) is a satisfactory means of estimation.

The disadvantage of using a mean downtime for equipment that shows wearout characteristics is that:

- Short tunnels will be overstated for downtime
- Long tunnels will show too much downtime at the beginning and insufficient downtime at the end.

The argument for further analysis is pervasive.



Cumulative Feet of Tunnel

Figure 6-3. Excavating Cutting Wheel Downtime for USC No. 1

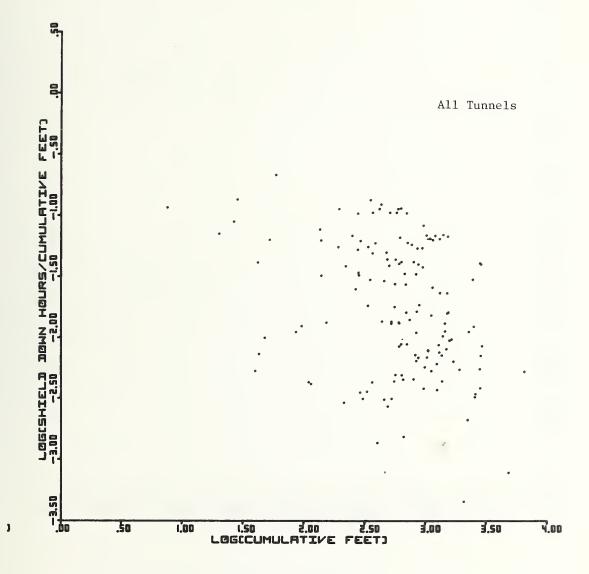


Figure 6-4. Shield Downtime

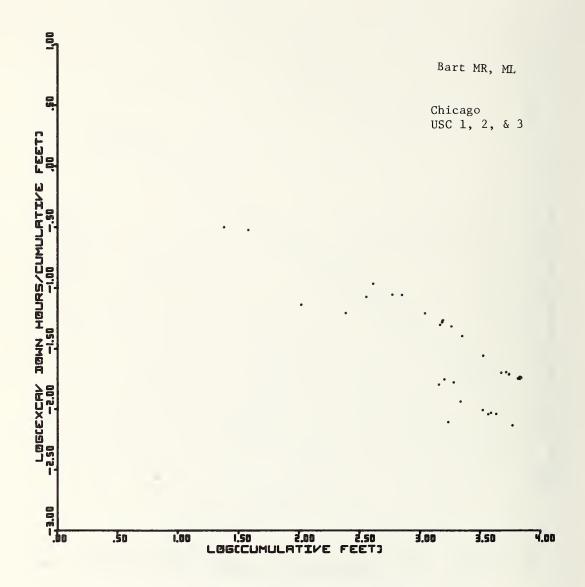


Figure 6-5A. Rotating Cutting Wheel Downtime

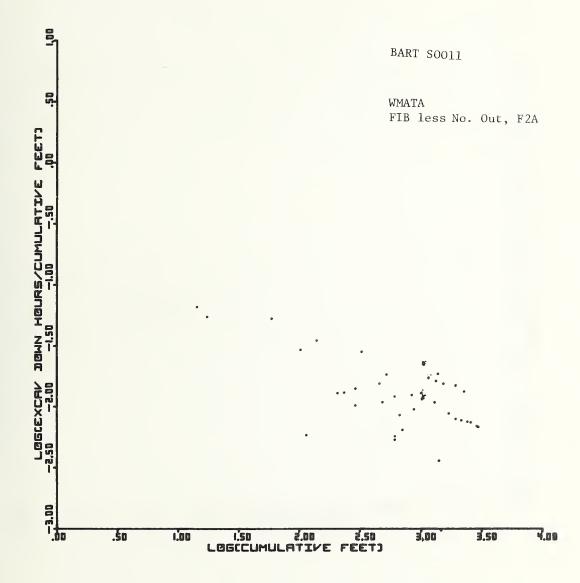


Figure 6-5B. Digger Arm Downtime

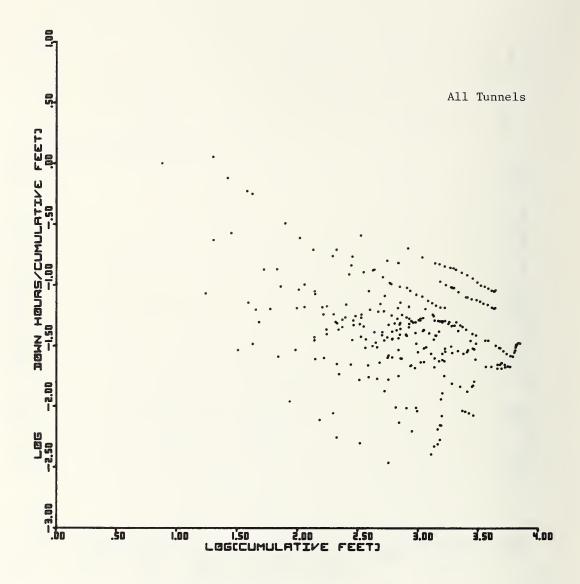


Figure 6-6. Miscellaneous Downtime

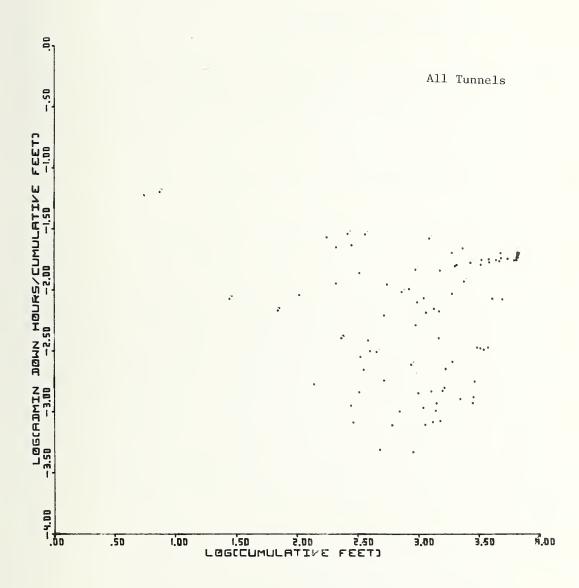


Figure 6-7. Administrative Downtime

7. INSTITUTIONAL EFFECTS

Institutional effects are those factors, usually subjective, that are applied as multipliers to the direct labor costs to allow for identified parameters with unknown or partially known ranges of variability. In the categories of

- Risk an action with a known set of outcomes and each outcome occurring with a known probability distribution; and
- Uncertainty an action with a known set of outcomes, but each outcome occurs without a known probability distribution

institutional effects fall into the classification of uncertainty. In order to reduce some of the uncertainty, a number of questions were asked of tunneling contractors relative to the effects of various institutional factors. The results of the analysis of the questionnaire answers have been incorporated into a guideline for planners' use for determining the factors' impact on costs. The factors examined were those deemed most significant in their effect on project costs. Discussions with transit system owners and tunneling contractors by Bechtel's consultant, J.M. Keating, as well as Bechtel's own estimating staff, led to the following selection of eleven major institutional factors.

1. Availability and Analysis of Subsurface Geological Conditions

This factor covers the extent to which the Ownerengineer has collected, evaluated, and disseminated subsurface information to the contractor prior to the contractor's bid preparation. Included in this information would be any geological interpretations obtained by the Owner-engineer.

- 2. The Extent of Owner Disclaimers with Regard to Subsurface Information Provided to the Contractors
- 3. Flexibility of Engineering Specifications

Flexibility refers to the degree to which the engineering specifications allow for design changes suggested by the contractors to accommodate the selected construction method.

4. Quality of Engineering Specifications

Quality refers to the accuracy of the Owner-engineer design including assumptions on which the design and specifications are based.

5.A Owner-obtained Rights-of-way

Rights-of-way include arrangements with all Owners of property, including utilities that must be relocated. Rights-of-way are also construed to include areas needed by the contractor as work and storage areas, including any rights-of-way needed for muck disposal.

5.B Owner-obtained Construction and Entry Permits

These include permanent and temporary construction permits and entry permits where required.

6. Potential Contractor Liability

Liability here is used to include only the contractor liability related to changed conditions.

7. Labor Agreements

The existence of systemwide labor agreements.

8. Labor Union History in the Area

Included in the history are work practices, craft availability, work stoppages, jurisdictional disputes, and union management relations.

- 9. Owner Payment and Retention Periods
- 10. Owner History of Claims Settlements on Past Projects

7.1 DATA COLLECTION AND ANALYSIS

The impact of institutional factors on tunneling costs, for the most part, has a twofold effect. First, there are what we have chosen to call the <u>identifiable costs</u>. These represent, for example, estimated expenditures incurred by the contractor to:

- Collect and evaluate subsurface data where none is provided by the Owner,
- Obtain rights-of-way and construction permits not obtained by the Owner, and
- Cover added financing costs where owner payment periods are excessive or retention amounts excessive.

The second effect of the institutional factors is on contingency costs included by the contractor at the time of bid to cover expenditures that are "likely" to occur during the tunnel drive, but which cannot be quantified at the time of the estimate. Contingency costs are directly related to the risks incurred by the contractor. The greater the risk burden, the greater the contingency costs. This second impact, the impact on contingency costs, is by far the greater of the two and also less visible to the owner.

7.2 DATA

Since current industry practices do not require sufficient detailing of contractor bids to identify contingency costs, an alternate approach was taken to obtain data from which to evaluate institutional cost factors. The questionnaire discussed in paragraph 7.7 was sent to 25 softground tunneling contractors through Bechtel's consultant, to determine the impact of each of the institutional factors on contingency. Since contingency costs are a measure of the contractor's risk and risk is theoretically related to profit, the questionnaire also included several questions relating to profit. Profit, in this case, can be

7-3

construed to mean gross margin. Of the 25 questionnaires sent out, 12 were returned; 2 of the responses were rejected because of incompleteness. The questionnaire established a base project; twin 3,000lineal-feet tunnels from a common work shaft through standing soil, primary liners of segmented steel, and the drive assumed through free air with wrap-up insurance provided by the Owner. The contractor's labor costs were assumed to be 50 percent of his total costs before contingency and profit.

7.3 ANALYSIS AND FINDINGS

The questionnaire asked each contractor to evaluate the relative contribution of each of the eleven factors to the contingency he would apply to his estimate under the best and worst circumstances associated with each factor. He was also asked to express, as a percentage of his base labor package, the total contingency and total profit that would be included in his bid price under the best and worst circumstances. It should be noted that the best and worst cases are unlikely to occur but were included here as upper and lower boundaries.

Each respondent was asked to add to the list of factors if he chose to do so; two did.

As expected, the responses showed a wide range of variation. Part of the variation is obviously attributable to differing interpretations of the questions.

Table 7-1 illustrates the spread in responses to the questions regarding contingency and profit amounts. The median value is that for which half the responses are lower or higher. From the contractor's point of view, in the worst case, where the majority of risks must be shouldered, contingency could be an amount equal to his total labor bill. As classically interpreted, potential profits should increase as the contractor's risk increases. This is illustrated in Figure 7-1 where contingency is plotted on the horizontal scale and contingency and profit on the vertical. The contingency figures from the questionnaires represent the contractor's evaluation of relative uncertainty.

The "best" and "worst" case responses were analyzed by arranging them into frequency distributions. For the best case, the 10% to 90% frequency spread covered the range of 0% to 24% contingency; for the worst case, the 10% to 90% spread covered 19% to 96% contingency. As shown in Figure 7-1, there is a small overlap in what is considered best and worst. In fact, the graph could be interpreted as a continuum of responses representing profit and contingency as a function of the contractor's uncertainty (contingency).

The center curve (in the two fan-shaped projections) is bounded by an upper and lower limit, and this range of uncertainty contains the area into which approximately 70 percent of responses would be expected to fall.

When the contingency is removed from the Profit and Contingency, it can be seen that, in both the expected values of the best and worst cases, profit reaches a maximum and then decreases; in the best case, it is at approximately 10 percent contingency, and, in the worst case, it is at approximately 70 percent contingency. It could be surmised that the profit percentage represents the contractor's <u>minimum expected profits</u> and the contingency plus profit percentages his maximum expected profit.

No inferences should be drawn concerning the justification of these maximum profit levels. It only indicates that owners can significantly reduce tunneling costs by minimizing the monetary risks to be assumed by the contractor and thereby reducing the applied contingencies.

Table 7-1

HIGH-LOW RANGE OF RESPONSES CONTINGENCY AND PROFIT ASSIGNED AS A PERCENT OF LABOR

	Best Case			Wo		
	Lowest	Median	Highest	Lowest	Median	Highest
Contingency Profit Profit + Contingency	$0\\\frac{10}{10}$	6 <u>29</u> 35	25 <u>40</u> 65	15 20 35	40 <u>51</u> 91	$ \begin{array}{r} 100\\ \underline{100}\\ 200 \end{array} $

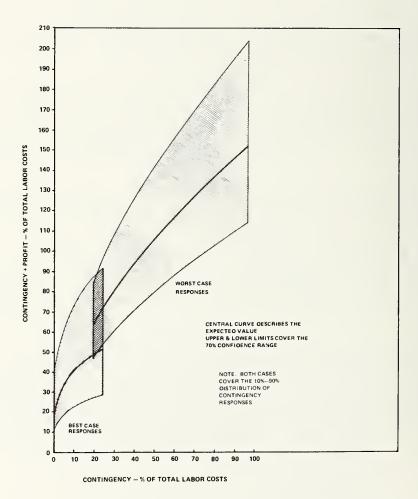


Figure 7-1. The Change in Profit Plus Contingency With Changes in Contingency

7.4 INSTITUTIONAL FACTORS IMPACT ON CONTINGENCY

The impact of the various institutional factors on contingency varied significantly among contractors; the ranges and averages are shown in Figure 7-2. Table 7-2 lists the factors by <u>best</u> and <u>worst</u>, and the median response of all contractors sampled. Availability of subsurface information in both cases is the highest contingency factor. The Owner's history of claims settlement and the labor union history account for the next largest amounts.

Figure 7-3 is a plot of the average contractor responses to the best and worst cases for each factor, in descending order, and indicates the cost differentials between the best and worst conditions.

Under usual contracting conditions, institutional factors do not generally fall completely into "best" and "worst" classes; statistically, this is a highly unlikely condition. There will more likely be a mixture of the two. In order to examine this aspect, the data for the two cases were combined and analyzed. Table 7-3 shows the result of the combination. The mean is the arithmetic average and the median divides the data into halves. The 10 percent and 90 percent points cover the statistical range into which 80 percent of the data are most likely to fall.

The spread between the mean and the median is a rough measure of the degree to which the distribution is skewed. The sign of the difference between the (Median-Mean) indicates the direction of the skewness; a negative sign means the distribution is skewed to the higher side. For instance, it is believed that it is more likely to require a greater contingency for subsurface geology information than less (Question No. 1).

Table 7-1 can now be added to recognize the variability of the data and to consider the responses as a total distribution.

Note that only the median values are added arithmetically. The 10 percent and 90 percent points are by the root-mean-square $-(\sqrt{10\chi^2 + 90\chi^2})$.

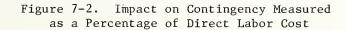
Table 7-2

AVERAGE UNCERTAINTY EFFECTS ON CONTINGENCY

Unce	rtainty Items	Percent	Contributio Best Case	ns to Contingency Worst Case
1.	The availability and analysis on subsurface geological conditions		2.5	15.7
2.	Extent of Owner disclaimer with n to subsurface conditions	regard	0.7	5.4
3.	Flexibility of engineering specif	l fications I	0.6	3.1
4.	Quality of engineering specificat	l tions	0.6	3.3
5.	Owner obtained rights-of-way		0.2	2.0
6.	Owner obtained permits for constr and entry	 ruction 	0.1	1.5
7.	Liability		0.6	3.8
8.	Labor agreements		0.7	2.8
9.	Labor union history in area		1.1	4.9
10.	Owner retention period		0.3	0.4
11.	Owner history of claims settlement	nt	0.6	4.0
12.	Mobilization payments			
13.	Scheduling problems		0 /	1.7
14.	Weather		0.4	1.7
15.	Proximity to water			
	Average Total Contingency as a Percentage of Total Labor Costs		8.4	48.6
	Median Total Contingency as a Percentage of Total Labor Costs		6.0	40.0

INSTITUTIONAL FACTOR		PERCENT OF DIRECT LABOR COSTS 5 10 15 20 25 30 1
AVAILABILITY AND ANALYSIS OF SUBSURFACE CONDITIONING	BEST G WORST	
OWNER HISTORY OF CLAIMS SETTLEMENT	BEST WORST	
LABOR UNION HISTORY IN THE AREA	BEST WORST	
EXTENT OF OWNER DISCLAIME WITH REGARD TO SUBSURFACE CONDITIONS AND ANALYSIS		
LABOR AGREEMENTS	BEST WORST	
LIABILITY	BEST WORST	••••
QUALITY OF ENGR. SPECS.	BEST WORST	44 1111110 • 11111
FLEXIBILITY OF ENGR. SPECS.	BEST WORST	<u>که</u> ۱۰۰۰۰ ۹۰۰۰۰
OWNER OBTAINEO RIGHTS-OF-WAY	BEST WORST	
OWNER OBTAINED PERMITS FOR CONSTRUCTION AND ENTR	BEST V WORST	110-11-01
OWNER RETENTION PERIOOS	BEST WORST	± • ● • • • • • • • • •
OTHER FACTORS	BEST WORST	11.01111111111

AVERAGE OF



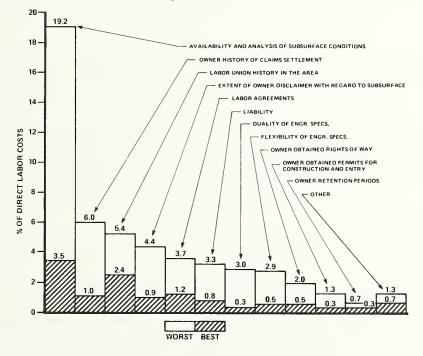


Figure 7-3. Risk Components of Contingency Under Best and Worst Cases

This again indicates to the user that extreme values are not very likely to occur.

In use, Table 7-2 would be modified by using the data from Table 7-3 (or a modification to suit the user) and Table 7-4. Medians of Table 7-3 and the contingency of Table 7-4 would be multiplied and the 10-percent and 90-percent points combined, by propagation of error, to obtain the individual contingencies as a percentage of total labor costs.

7.5 CONTINGENCY SIMULATION

To integrate the contingency information collected by the sample, three stochastic simulations were carried out, using a Monte Carlo technique; one for the average case and another for both the best and worst cases. Figure 7-4 depicts the results of this simulation. The curves representing the best and worst cases are highly unlikely and are included here for reference.

The interpretation of the lines is as follows: under the best conditions, 50 percent of the contractors will include contingency values greater than 35 percent of direct labor. Similarly, under best conditions:

 85% will have contingency value 	ues greater than 11%	of direct labor
---	----------------------	-----------------

- 70% will have contingency values greater than 18% of direct labor
- 50% will have contingency values greater than 33% of direct labor
 30% will have contingency values greater than 51% of direct labor
- 15% will have contingency values greater than 68% of direct labor.

Similar figures can be extracted for the average and worse cases from Figure 7-4.

As a starting point, planners may find the following work sheet, Figure 7-5, useful in evaluating the impact order-of-magnitude of these institutional factors on contingency. Numerical values are based on the average values calculated from the questionnaire sample.

Table 7-3

Question Number	10%	Mean	Median (50%)	90%
1. Soils	8.5	30.9	29.0	56
2. Soils Disclaimer	-6	8.4	7.0	27.5
3. Engineering Specs.	0	6.6	5.5	15
4. Spec. Quality	0.5	7.0	4.0	20
5. Right-of-Way	0	3.1	3.0	8
6. Permits	0	2.3	1.5	6
7. Liability	0	7.8	8.0	16
8. Labor Agreements	0.5	7.2	7.5	14
9. Labor History	1	11.4	9.5	23
10. Retention	0	2.1	1.0	7
11. Claim Settlement	1	7.6	7.5	15
Mobilization	0	1.6	0	7.5

DISTRIBUTION OF CONTINGENCY RESPONSES-BEST AND WORST CASES COMBINED

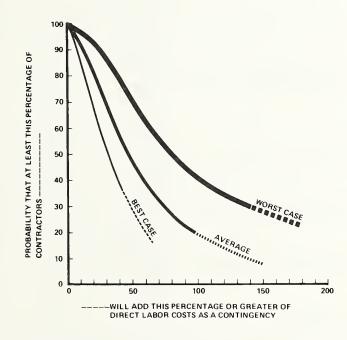


Figure 7-4. Contingency Level Probabilities

Table 7-4

CONTINGENCY AND PROFIT ASSIGNED AS A PERCENTAGE OF DIRECT LABOR-BEST AND WORST CASES COMBINED

	10%	Mean	Median (50%)	90%
Contingency Profit	1 17.5	28.5 40.5	21 37.5	61 71
TOTAL	17.5		58.5	93.6

Soft Ground Tunneling

IMPACT OF INSTITUTIONAL FACTORS ON COST CONTINGENCY

	FACTORS	ĬF	ADD	CONTINGENCY- PERCENT (%) OF DIRECT LABDR	
1.	AVAILABILITY AND ANALYSIS OF SUBSURFACE GEOLOGICAL CONDITIONS	NONE MARGINAL ADEQUATE GOOD EXCELLENT	-	31.0 16.5 8.5 5.0 1.0	
2.	EXTENT OF OWNER DISCLAIMERS WITH REGARD TD SUBSURFACE CONDITIONS	EXTENSIVE NOMINAL FEW	-	8.0 2.5 0	
3.	FLEXIBILITY OF ENGINEERING SPECIFICATIONS	RIGID ADEQUATE FLEXIBLE		3.0 * 1.5 0.5	
4.	QUALITY DF ENGINEERING SPECIFICATIONS	MARGINAL SATISFACTORY EXCELLENT		3.0 1.5 0	
5.	DWNER O8TAINEO RIGHTS DF WAY, ENTRY PERMITS ANO CONSTRUCTION PERMITS	NONE MAJOR ONES ALL		5.5 1.5 0	
6.	LIABILITY	EXTENSIVE NOMINAL MINIMAL		5.5 2.5 0	
7.	SYSTEM WIDE LABOR AGREEMENTS	NO YES		7.0 , 0.5	
8.	LABOR UNION HISTORY IN THE AREA	POOR MARGINAL AVERAGE GOOO EXCELLENT		7.0 5.5 4.5 1.5 1.0	
9.	DWNER RETENTION PERIOD	LONGER THAN AVERAGE AVERAGE SHORTER THAN AVERAGE		2.5 0.5 0	
0.	DWNER HISTORY OF CLAIMS SETTLEMENT	POOR MARGINAL AVERAGE GOOO EXCELLENT		12.0 5.5 1.5 1.0 0.5	

Figure 7-5. Impact of Institutional Factors on Cost Contingency

7.6 AREA PRODUCTIVITY

The concept that productivity of skilled and unskilled craft workers varies in different geographical areas of the U.S. is generally accepted as a subjective variable. The quantification of this subjectivity is another matter and, at the present stage of knowledge, is not well established.

From proprietary sources, it is estimated, based on a value of 1.0 for the West Coast, that manhour requirements for other areas of the U.S. would have multipliers of

1.1 for the Midwest
1.15 for the East Coast (excluding New York City)
and Southeast
1.2 for the Gulf Coast

based on 1972 data.

In general, the multiplier is skewed to the high side (less productive) rather than the low side. When a range of values is to be considered, the expected value +0.5, -0.3 can be considered a range into which, by chance, 20 percent of the productivity values will fall; e.g.

For the East Coast: 1.15 + 0.5 = 1.651.15 - 0.3 = 0.85

7.7 TUNNELING QUESTIONNAIRE

As explained earlier in this section, data had to be gathered by direct contact with major contractors, since usual breakdowns of bid figures did not provide adequate insight into the built-up estimates for our purposes. The following letter was dispatched to some 25 tunneling specialists late in December 1976.

7-13

"We are working on a D.O.T. study evaluating the cost of soft ground tunneling.

"This report is being prepared by Bechtel Corporation and basically has involved gathering statistical data from job reports in North America. The information gathered to date shows a good correlation at the direct cost level when adjusted for regional variations.

"In the areas of contingency and profit, we would like your assistance and have included a questionnaire that we hope you will take the time to fill out.

"The questionnaire is being sent to twenty-five men in the tunneling business and your response will be anonymous and tabulated to develop ranges for contingency and profit.

"The format is laid out in such a way as to reflect the extra cost of construction if the contractor is saddled with the unknown and ownerengineer has put the burden of solving problems on the contractor.

"Please respond to both cases "best" and "worst." The "best" condition would be ideal from the contractor's standpoint; for example, no disclaimer by owner-engineer regarding data and evaluation of subsurface conditions, job labor agreement, etc. The "worst" case would be your opinion of the opposite of "ideal."

"In your evaluation you will have to make assumptions based on your experience with soft ground tunneling projects but consider the basic project as:

- A. 2 3000 LF tunnel from a common work shaft. Ground tends to stand up as steel liners are extruded from the tail of the shield.
- B. Compressed air is not required and the contractor is covered by owners wrap-up insurance.
- C. The contractor's labor package is equal to 50% of the total cost without contingency and profit.

"Thank you for your time on this questionnaire and we will send you a summary of the results."

Contingency Areas

Working with the job conditions described, how would the "Risk Components" tabulated below change when considering the "best" and "worst" cases.

Contribution of Risk Items to Contingency		ntribution "Best"	% Contribution Worst"
. The availability and ana subsurface geological co			
. Extent of owner disclaim to subsurface conditions			
. Flexibility of engineeri	ng specifications		
. Quality of engineering s	pecifications		
. Owner obtained right-of-	way		
. Owner obtained permits f and entry	or construction		
. Liability			
. Labor agreements			
. Labor union history in a	rea		
. Owner retention period			
. Owner history of claim s	ettlement		
. Etc.			
. Etc.			
. Etc.	-		
Total Cont	ingency	100%	100%
Co	ntingency Values		
Working under the above tw contingency vary.	o case conditions	how would	the percent of
As % of total labor		"Best"	"Worst"
AS /0 UI LULAI IADUI			

As % of total cost

Profit

A. Working under the above two case conditions and assuming good confidence in estimate cost and contingency value, how would the percent of profit vary.

	"Best"	"Worst"
As % of total labor		
As % of total cost		
Same as A. with additional conditions	noted.	
	"Best"	"Worst"
5 or more bidders As % of total labor		
As % of total cost		
3 bidders As % of total labor		
As % of total cost		<u> </u>

B

C. Modify contracting method to target estimate with 10% fixed fee plus 25% sharing in profit or losses based on target estimate.

	"Best"	"Worst"
As % of total labor		
As % of total cost		

7.8 CONCLUSION

The above data processing has been discussed with a degree of precision probably not supported by the accuracy of the data. The purpose was to indicate the statistical procedures involved. It is a first step in the reduction of uncertainty concerning institutional factors and can be used as a reflection of the concern of ten tunneling contractors.

More contractors should be concerned and contribute to reducing such uncertainty to the level of risk by contributing their subjective (and quantitative, if available) values to increase the discipline's total knowledge. It does seem unfortunate that a much higher degree of accuracy can be achieved in estimating tunneling labor and total costs, only to have this accuracy destroyed by the present high degree of uncertainty of institutional effects.

8. RECOMMENDATIONS

8.1 FUTURE DATA COLLECTION

Rapid Transit tunneling data generally have not been summarized into formats whereby the data could be used for future estimating. Reports, as such, have been in terms of funds expended. Because of the rapid rates of inflation during the last ten years, between and during tunnel construction, the extrapolation of past to future costs is deemed infeasible; there is no one inflation index that can be applied to all the resources used during construction.

In order to use past data, the actual resources consumed — manhours, equipment, and bulk materials — must be known so that current costs and expected escalation factors can be applied at the time new construction is contemplated to estimate the total cost of a finished tunnel.

Based on the above concept and in conformation with the study contract, the following are recommended as minimum information requirements to be reported on completion of future tunneling contracts subsidized by U.S. Department of Transportation funds.

8.1.1 Economic Factors in Tunnel Construction/Case History Data

The format is shown (filled out) in Appendix A-1. Sheets 1 through 5 summarize all but the weekly progress. The unnumbered pages are for weekly progress summaries and average soil characteristics.

The latter breakdown is not displayed. The characteristics used in this study resulted from the descriptions found in the tunneling logs. Better

8-1

descriptions can and should be developed by soils engineers — but <u>must be compatible</u> with the capability of the face crew foreman to quickly recognize and log. It must not be time-consuming, as his primary responsibility is the safe advancement of the tunnel face.

8.1.2 Ring and Face Log (Figure 8-1)

The weekly summary of tunnel progress is composed of Ring and Face Log data. The latter should contain sufficient information so that only clerical assistance is needed for compilation.

A suggested set of face description criteria are included that are mutually exclusive and in combination will give an adequate picture of the advancing face. The BART log sheet contained data for two rings per sheet, and the WMATA log had one ring per sheet.

8.2 ADDITIONAL STUDIES

The results reported upon here are based on tunnels whose data appeared to be quickly available. There may be data errors because there was not sufficient time to verify certain reported information that, upon study, raised questions of correctness. These data should be verified or corrected.

Not enough different soil types were included. Glacial till soils, to evaluate the effect of cobbles and boulders, need inclusion. The Toronto subway and Edmonton sewer systems have those soil characteristics and one or more tunnels should be added to the data deck.

All the collected data were not studied and should be analyzed to determine:

• Equipment types most applicable to expected tunneling conditions and lengths.

8-2

RING & FACE LOG

Tunnel # (OB/IB), Contract #,	Contractor, Walker:, Shifter:
Date:/ 19, Shift:, To	unnel Pressure: psig, Weather:
Ring #, Station @ Start of Shove:	
	n:, Time @ Start of Ring Erection:
Expansion Time:, Expander Press:	psig, Time @ End of Ring Erection: Minutes:
ESTIMATED SOIL FACE COMPOSITION	FACE PROFILE BEFORE SHOVE
Silt:%, Clay:%, Sand:%, Gravel:%, Rocks & Boulders:%, Peat & Trash:%.	(Sketch Soil Characteristics & Location)
ESTIMATED FACE CONDITION (SCALE 0-1.0) Running:	
Dry:(0), Damp:(.2), Slight Flow:(.5) Operating w/Pumps:(.75), Flooded Out:(1.) Shove Jacks, Show jacking pressures on profile.	
TARGET POSITIONS AFTER SHOVE:	
Left Right Hi Lo	
Rear	(Note: Outside circle = 100 units. Each square = 1% of total area)
Grout Used:(gravel/cement)	Roll of Shield:
SHUTDOWNS	
	_, Time @ End:, Reason:
	_, Time @ End:, Reason:
Time @ Beginning:, Continuing (ck)	_, Time @ End:, Reason:
Slowdowns, Reasons For:	
Other Comments:	
(Note crew size on first ring log of shift)	

Figure 8-1. Ring and Face Log

• Crew staffing as a function of equipment to be used and expected tunneling conditions.

Bulk material requirements must be added to the system.

Although a beginning was made in estimating the effects of institutional factors, it was only a beginning. Mailed-out questionnaires are notorious for their poor responses. Because of the gross effects these factors have on costs — which far overshadow the quantitized tunneling effort — a more detailed study needs to be made. Contractors should be interviewed because the response percentage will be increased. And more factors will be included.

Our questionnaire only went to transit tunneling contractors. All tunneling contractors, including those for large-diameter sewers, for both soft ground and hard rock should be included. The questionnaire should be expanded.

Equipment maintenance and depreciation were not readily found, but need to be included.

The derived predicting equations should be analyzed for stability of the derived coefficients. Ridge analysis⁽⁹⁾ is one method of modifying the coefficients to achieved satisfactory stability. It was precluded in this study by the restraints of time and resources.

8.3 RISK MODEL

All the above data, including the results of the study to date together with their variances, will be useless unless they are combined in a simulation model. Not only useless, but incomprehensible. A risk analysis model must be written to facilitate the complete use of the data (10) and allow the decision maker to make a rational judgment about the economics of the project.

9. GUIDELINES

Two forms are suggested for future data acquisition. Section 3.1.1 lists the data used in this study. The data are keypunched in a 7F10.5 format on the card deck forwarded separately as part of this report.

The key document on the advance rate is the Ring and Face Log. Daily perusal of the shift's logs should be made by supervisory personnel to ensure accuracy and completion. Weekly averaging of the data is highly recommended so that questions on omissions and errors can be corrected before memories of events are forgotten. To save time, the weekly averages should be posted directly to keypunch sheets. The forms used are shown in Appendix A-6.

In the following, consider each variable on the keypunch form of Appendix A-6 as XI, X2, ----, X42.

The intercept and learning curve exponents are estimated first:

- Plot X4/X2 (hr/ft) vs X3-0.5*X2(Σft) on log-log paper.
- Remove obvious outliers from the immediate analysis (they will be used later).
- Regress $Ln(hr/ft) = f[Ln(\Sigma ft)]$

The estimated values are punched into the data cards as X38 and X42.

Analysis of the tunnel RoA or a larger matrix composed of many tunnels is made by -

- Obtaining correlation coefficients between all input variables,
- Eliminating variables that have no logical (engineering) basis for being included in the analysis,
- Eliminating variables having correlation coefficients greater than ± 0.9 (the analyst may have his own level for elimination). In such cases, one variable is probably adequately explaining the variation in the other,
- Eliminating variables that appear only a few times. These variables may induce an exaggerated effect. If the variable is considered to be logically important, it may be useful to examine its effect in a smaller matrix of data with other variable characteristics of a similar nature.

Based on the inter-correlation coefficients of independent variables left for consideration, new dummy variables may be constructed (see section 6.0) that will increase the explanatory value of the predicting equation.

The effect of the learning curve and intercept have been previously determined. Only the multiplier effects of soils, equipment types, and their breakdowns are to be found. The dependent variable (see Figure 5-7) is calculated by

$$Y = \frac{X4/X2}{X38* (X3-0.5*X2)**X42} = \frac{hr/ft}{I* (\Sigma ft)^{E}}$$

The Ln Y is regressed against the logs of the independent variables and their dummys.

A best equation can now be selected.

The same basic procedure is followed for estimating the other prediction equations.

The best form for the downtime predictions is not yet finalized. Figure 6-2 may provide a satisfactory basis for analysis.

Figure 5-1 shows the system calculations for estimating the tunnel construction cost. As a final step, the equations are combined, together with costs and derived (as well as subjective) variabilities into a Monte Carlo simulation to estimate the expected cost and its distribution. This is known as risk analysis ⁽¹⁰⁾. The contractor can then bid, based on his "feel" for the degree of confidence he believes is justified. The advantage of risk analysis is that it quantifies a large portion of the unknown.

Appendix A

PHYSICAL DATA

Data included in this appendix are:

- A-1 Characteristics of tunnels and equipment
- A-2 Average weekly progress
- A-3 Rate of advance calculations
- A-4 Calculation of downtime hours
- A-5 Total estimated shift hours and percentage of error
- A-6 Keypunch forms

.

Appendix A-1

A partial record of the physical characteristics of the individual tunnel and equipment used in several tunnels.

Although it is expected that the complete history is available in the historical record files, complete information could not be located in the time available for the searches.

It is recommended that this or a similar form be used to record the pertinent history of future tunneling operations.

CASE HISTORY DATA

A DESCRIPTION	B. OESIGN INFORMATION
1. PROJECT NAME 24th to Randall St. NUMBER IM0031	1. PLAN AND PROFILE ATTACHED
LOCATION San Francisco, California	2. TYPICAL SECTION DRAWING ATT
3 OWNER BAY Area Rapid Transit District ENGINEER PIST B	3. TEMPORARY LININGS OFTAILS AT
4 CONTRACTOR Morrison-Knudsen Calloc, Brown + Root Loc, Perini Corp(JV)	4. PERMANENT LININGS DETAILS AT
5. DATES: START May 27, 1967 [COMPLETE November 17, 1969]	5. GEOLOGICAL PROFILE ATTACHED
6 PROJECT SCOPE (INCLUDE ANY APPURTENANT STRUCTURES)	6. VERBAL DESCRIPTION OF SOIL CO
Includes construction of subway line	Soil consists or
tunnels of approximately 4525 LF of MR line and	to very dense; gray
4500 LE of ML line, placing tunnel invert and	and gray clay, a
wolkway concrete; construction of a vent shaft	dense, plus two
and switching station and a pumping station;	of fractured rock
mechanical and electrical work; and installation	fractured churt
of segmented steel tunnel rings, fons and	
pumps.	
7. OWNER FURNISHED MATERIAL AND EQUIPMENT LIST	7. DEWATERING PLAN ATTACHED
Segmented steel rings, pumping station	8. GROUNO WATER CONDITIONS DES
equipment and ventilation equipment	Underground w
squipinent and venination equipment,	throughout the righ:
	entire tunnel length

8. OTHER OWNER SUPPLIED COST ITEMS (e.g. INSURANCE)

Right of -ways

TYPICAL SECTION DRAWING ATTACHED YES NO TEMPORARY LININGS OFTAILS ATTACHED YES NO PERMANENT LININGS DETAILS ATTACHED YES NO GEOLOGICAL PROFILE ATTACHEO: YES NO VERBAL DESCRIPTION OF SOIL CONDITIONS Soil consists of sandy clay ranging from medium overy dense; gray elay with some sond; red, brown and gray clay, all with density of medium to very dense, plus two oreas that had a large amount f fractured rock. The contractor ran into some ractured churt **OEWATERING PLAN ATTACHED** YES ND GROUND WATER CONDITIONS DESCRIPTION Underground water table showed to be consistent throughout the right-of-way so contractor dewatered the entire tunnel length making it passible to drive only 1/3 of tunnel length in compressed air. 9 SITE PREPARATION & RESTORATION DESCRIPTION

SHEET _____ OF _

YES NO

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY OATA

OESIGN INFORMATION (CONTINUED)
10. UNDERPINNING DESCRIPTION
Underpinning of the Sears store at Mission and
Army streets was accomplished by drilling
caisson holes to extend obcut 10 ft below the
invert of the future tunnel. Bentonite slurry was used
to keep the holes open. Then reinforcing was
lowered into the caisson holes and tremie concrete
was placed in the slurry filled holes. New concrete
pile caps were constructed to support the
existing pile caps and the building.
11. UTILITIES. DESCRIPTION
Relocation is minimal. Electric, gas and water
lines on the east side of Mission St. were
relocated around the end of the access shaft.
All other utilities supported in place.

C. CONSTRUCTION METHODS		SHEET 2	OF
1. FREE AIR 2/3 of tur	inel	LENGTH (FT)	6018
	tunnel	LENGTH (FT)	3007
PSIG MIN O	PSIG MAX 14	PSIG WTO AVG.	3.233
3. DESCRIPTIONS			
TUNNEL EXCAVATION			
Excavation 1	uas with 0 17.92	' shield s	with
	Sheel-Type Mining		
and a conveyo	r system consi	sting of	
skiphcist and cor	r system consi weyer extending i	45 LF.	
PRIMARY LINING			
Composed of	30-inch wide, 17.	3-ft autic	le
diameter circular	welded steel rings	each coa	asisting
diameter circular of 6 larger segi	ments and one s	mall key	ion our ng
segment	TICHIO UNICI ONE O	man acy	
signitur			
FINAL LINING.			

Appendix A-1. Characteristics of Tunnels and Equipment

CASE HISTORY DATA

D. MAJOR EQUIPMENT UTILIZED

1. CUTTING AND EXCAVATING				
MAKE Mining , MODEL	Equipment	Hanufa	turing	Corp.
TYPE	ROTATING WHEEL	OSCILL	ATING ARMS	DIGGING ARM
	OTHER (SPECIFY)			
CONNECTEO HORSE PO	WER 225			
NO. USED 2				
2. SHIELO				
OUTSIDE DIA.	17.92	Ft	LENGTH	12 ft. 5 in.
NO. OF JACKS 3 HOU	L 19 THRUST	FORCE (TONS	115 NO. OF	JACKING MOTORS 4
HORSE POWER EA. JAC	KING MOTOR 50	2		
NO. SHIELOS USEO	1			
3. MUCKING EQUIPMENT (UNDE	RGROUNO)			
TYPE CONUCY	or and :	skipho	ist	•
CONVEYOR LENGTH	165 (FT.)		CAPACI	1 5,400,000 165
RAIL CARS NO.	_ 5		CAPACI	<u>τν 7 cy</u> (π)
RUBBER TIRE VEHICLE N)		CAPACI	TY (T)
COMBINATION (SPECIFY)				
4. MUCKING EQUIPMENT UNDER	GROUND TO SURFAC	E (OESCRIBE)		
A skip hoist	extending f	com a s	ump 15A	below the
base slab to an er				
surface was crea				
at the top of the	e structure	603 U	sed to k	noist a ten-
cubic yord ski,	o from th	e sum	pto a	conveyor_
attached to th	c hoist :	structu	UC 25-1	7. chouc
the street su	rface. The.	skipwas	lifted up	othe hoist and
tipped and emptice				

LINERS (PRE CAST)		
DESCRIPTION	CAPACITY	NO.
GROUTING		
DESCRIPTION	CAPACITY	NO.
Mayna Grout Rimp - Rator - Stater pum Kwik-Mix Cyclo Grout Mixer	ing type	a
Kwik-Mix Cuclo Grout Mixer	1/2 ud	
Grout cars	1/2 cud.	i
	3.	
CONCRETE INVERT (ANO WALKWAYS)		
DESCRIPTION	CAPACITY	NO,
P80 Whiteman Concrete pump - 90 hp	14-1/2 cuft	r
6. VENTING, PUMPING, COMPRESSION, EQUIPMENT		
DESCRIPTION	CAPACITY	NO
Low Air compressors - 300 Hp cc.	11,000 tota/	5
••••••••••••••••••••••••••••••••••••••		
7. OTHER (Specify)		

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY DATA

1 TUNNEL (IF MULTIPLE, SHO			
LENGTH Both tur	6" 90	300 L	F
INSIDE DIA. 16 -	6	00 /*	7 - 6
	rcular		
NO. CROSS OVERS, IF MULT	PLE		EA
TOTAL EXCAVATION	80,80	0	- CY
TUNNEL PRESSURE RANGE	12	PSI _ /	4 PS
2 GROUTING (CY)			
	E\$T	ACT	UAL
BEHINO TEMP. LINING		40	500
CONSOLIDATION (FACE)			
PREGROUTING			
3 PRIMARY LINI	NG		
DESCRIPTION	1	OUAR	ITITY
Liner Segmen	ts steel	36	12
4. SECONDARY L	INING		
TYPE Type II C	ement		
NO LINERS IF PREFAB OR P	RECAST		E
OUANTITIES IF CAST IN PLA	CE		
OESCRIPTION		ÛUAN	TITY
CONCRETE			(C
			(TOP
REINFORCING			

6. INVERT (AND WALKWAYS), ARCH	
OESCRIPTION	QUANTITY
CONCRETE - Invert, Type I	6539 (CY)
REBAR	(TONS)
FORMS - 8ft long Steel	(S.F.)
STRUC STEEL	(TONS)
concrete - Walkways	Ta cy
7. MAJOR UNDERPINNINGS	
DESCRIPTION	AREA (S.F.)
TOTAL	
B. AIBLOCK SYSTEM (IF USED)	
MAN LOCKS	
NUMBER	2 (EA)
LENGTH 40	D (FT)
DIAMETER 6	(FT)
MUOLOCK	
NUMBER a) (EA)
LENGTH 14	(FT)
DIAMETER 9	(FT)
BULK HEAO OESIGN	50 PSIG

	SHEI	ET OF
9 APPURTENANT STRU	CTURES	
VENT AND FAN SHAF	TS	
CONSTRUCTION METHO	Soldier E	Beam and
Laggin	G	
	J	
WIOTH 94 (FT)	BREADTH 27 FT	DEPTH JO FT
WALL THICKNESS	3 yt	
EXCAVATION OUANTIT		(CY)
CONCRETE OUANTITIES	2200	(CY)
PUMPING STATIONS		
CONSTRUCTION METHO	Sheet Pilo	es and
	Support	
	<u>ouppor</u>	
CONFIGURATION C	culor Manhol	- Type Struct
		8-16 (FT)
EXCAVATION QUANTIT		· (CY)
CONCRETE OUANTITIES	130	
OTHER APPURTENAN		
DESC RIPTION	EXCAV (CV)	CONCRETE (CY)
241th street	11,706	
Construction Shaft		
10. SITE PREPARATION	BRESTORATION	
DESCRIPTION	TYPE	AREA (S.F.)
CLEAR & GRUB		
REMOVAL		
RESTORATION		

CASE HISTORY OATA

F TYPICAL CREW SIZE A	AND UT	LIZATI	ON (1)
1. CREW - Heading	- Fre	.c Ai	r
SHIFTS / DAY 3	HDURS /		-
WORKING DESIGNATION	1ST Shift	2 ncl SHIFT	3rd Shift
, Shifter	1	1	
Heading Engr	1	1	
Mole Operator	1	1	
Mole Mechanic	2	a	a
Iron Movers	2	2	a
Fron Workers	4	4	4
Hog Rod and Brocket Men	a	a	2
Grait Rimp Oper.	1	1	1
Grout Hen	2	2	2
Locomotive Oper.	1	1	1
Brakeman	1	1	1
Electrician	1/2	1/2	1/2
	(one i	nan o he	dina
			J
TDTAL	18.1/2	18/2	181/2

2 CREW - Heading - G	ompra	:sord	Air		3 CREW - TOP Sic	lc		
SHIFTS / DAY	HDURS /	SHIFT	6		SHIFTS / DAY 3	HDURS /	SHIFT	8
WDRK DESIGNATION	1ST SHIFT	2 ND Shift	3RD Shift	ATH	WDRK DESIGNATION	1ST Shift	2ND SHIFT	3RD Shift
Heading Engr.	1		1	1	General Supt.	1	-	-
Shifter	1		1	1	Walker	1	1	
Mole Lead Mechanic	1		1	1	Surveyor	3	-	-
Mechanic	1		1_		Mechanic Foreman	1	1	1
Mole Operator	1			1	Mechanic	4	1	1
Iron Worker	4	4	4	4	Electrical Fareman	1	-	-
Iron Moyer	2	2	2	2	Electricion	3	1	1
Iran Mayer Hog Rod and Bracket Man	2	a	a	2	Top Laborer	2	a	a
Grout Rump Operator	1.		1	1	Bridge (ranc	1	1	1
Grout Man	2	2	2	a	Lube Engineer	1	-	-
Locomotive Oper.		1	1	1	Gen'l Operator	I	l	1
Brakeman	1	. 1.	1	1	Compressor Opr.	1	1	1
Electrician	1/2	1/2	1/2	1/2	Compressor Opr. Change House Attendant	1	1	1
Monlock Operator	1	_1	1		Warehouseman	2	~	~
Gutside Muck- lock Operator Inside Muck-		1	1	1				
lock Operator	1	1_	1	1				
TOTAL	21-12	21-1/2	alla	21-1/2	TOTAL	23	10	10

SH	EET <u>5</u>	OF	
4_CREW - Invert	Con	crete	
SHIFTS / DAY	HOURS /	SHIFT	8
WORK DESIGNATION	1ST Shift	2ND Shift	3R D Shift
Foreman	1		
Winch Operator	1		
Vibrator Men	2		
Kement Finishers	3		
Rebar Man			
Laborers	2		
Laborers	4		
Rump-Laborer			
Operator at Rump			
TOTAL	16		
5. Crew-Prep. and			ting
SHIFTS DAY	HRSS	ніят	8
Foreman			
Laborers	18		
Laborers	9		
TOTAL	28		

11) NOTE CATEGORY OF CREWS INEADING, SUPPORT SURFACE SHAFT ETC.) REPORT AS LOGGED

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY DATA

A DESCRIPTION	
	NUMBER IROOJ3
2 LOCATION Berkeley, California	
3 OWNERBOY Area Rapid Transit District	NGINEER PBTB
4 CONTRACTOR Sheq - MOLCO	
5 DATES START //28/66	COMPLETE 3/5/68
6 PROJECT SCOPE (INCLUDE ANY APPURTENANT STRUCTURE	S)
Approximately 1,475 feet of a	urved twin subway
line tunnels, Approximately 2.70	o feet of eut-and-cover
twin box subway structure, in	reluding installation of
mechanical and electrical equ relocation and constructi	ipment and the
relocation and constructi	on of utilitics.
7 DWNER FURNISHEC MATERIAL AND EDUIPMENT LIST	
Our contractory as pool tupool lipipo	of 30 inches wide 18 ft
Queer furnished tunnel lining outside diameter circular welde	d steel rings, pumping
	- mig-, paniping
and Annual State	1 V LW JW L Amage
8 OTHER DWNER SUPPLIED CDST ITEMS (# q INSURANCE)	
at the	
	· · · · · · · · · · · · · · · · · · ·

B DESIGN INFORMATION	SHEET	OF
1 PLAN AND PROFILE ATTACHED	YES	NO
2 TYPICAL SECTION DRAWING ATTACHED.	YES	NO
3 TEMPDRARY LININGS DETAILS ATTACHED	YES	NO
4 PERMANENT LININGS DETAILS ATTACHED	YES	NO
5 GEOLDGICAL PROFILE ATTACHED	YES	NO

6 VERBAL DESCRIPTION OF SOIL CONDITIONS Interfingering leases of clayey gravel, sandy and silty clays, and clayey or silty sands Layers are of irregular thickness and grade into each other within shart distances, bath harizantally and vertically. Olive gray sandstane was encountered in the invert of the tunnel, weathered to a light brown at the upper soil contact and underlain by a dark alive green shale.

7 DEWATERING PLAN ATTACHED B GROUND WATER CONDITIONS DESCRIPTION

Beiere dewatering, the water level was 10 ft above the topof the future structure. No dewatering systeministalled outside excavation. Submersible Sweek pump was placed in tunnel invert at heading and was in all cases sufficient. 9 Site preparation & Restantion bescription

YES NO

Approximately 150-ft wide area above future cut-and. sourr area was quailable as a work area. Owner provided a lat about 55 ft wide and 280ft long to contractor for use during construction. Temporary

CASE HISTORY DATA

в	DESIGN	INFORMATION	(CONTINUED)

work area on the adjacent contract (ROOST) was used a saw yord until contract ROOST was bid, mid-194

10. UNDERPINNING DESCRIPTION
· · · · · · · · · · · · · · · · · · ·
17. UTILITIES. DESCRIPTION

C. CONSTRUCTION METHODS SHEET ____OF ____ 1. FREE AIR: LENGTH (FT) 4, /75 C. CDMPRESSED AIR. OCT US CC LENGTH (FT) --PSIG MIN _____PSIG MAX ____PSIG WTD AVG. PSIG MIN _____PSIG MAX ____PSIG WTD AVG. TUNNEL EXCAVATION

Excavation was with an 18ft 8/2 in shield. A rubber-tired truck transported the muck from the heading to the Temporary Access shaft. After the last mucking run, the mucker brought in a set of ring segments for the next ring. The tunnel was hand-mined.

PRIMARY LINING

30" wide, 18.0 ft outside diameter circular welded steel rings each consisting of 6 larger segments and one small key segment.

FINAL LINING

aggregate size. Walkway concrete used a t-in. maximum aggregate size.

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY DATA

D. MAJOR EQUIPMENT UTILIZED

1. CUTTING AND EXCAVATING								
MAKE								
MODEL								
TYPE.	BOTATING	WHEEL	OSCILLAT	TING ARMS		DIGGING AI	RM	Γ
,	OTHER (SP	ECIFY) Ma	inual	Diggi	<u>n</u> a			-
CONNECTED HORSE PO	WER				3			
NO USED								
2. SHIELO								
OUTSIDE DIA.	18ft 5	81/2 in.		ENGTH	1	13'6" - "	ottom	37
NO. OF JACKS	2001	THRUST FORC	CE (TONS)	109/50 NO		ACKING MOTO	DRS 4	¥
HORSE POWER EA. JACK				1			_	
NO. SHIELOS USED	1							_
3. MUCKING EQUIPMENT (UNDER	AGROUNO)							
TYPE: Diesel Pa	owerer	d Mucl	KCT					
CONVEYOR LENGTH		FT.)		CAP	ACITY			(T)
RAIL CARS NO.				CAP	ACITY			(T)
AUBBER TIRE VEHICLE NO	1. L 8L 7	114 Mor	del	CAP	ACITY	22,000	Lbs	
COMBINATION (SPECIFY)								
4. MUCKING EDUIPMENT UNDERG	GROUND TD S	SURFACE (DE	SCRIBE)					_
								_
							-	
							_	
							-	_
·····					_			

LINERS (PRE CAST)		
DESCRIPTION	CAPACITY	NO.
Gardner Denver Air Hoist - Model 86-24-	DOL	
Impact Wrenches		
GROUTING		
DESCRIPTION	CAPACITY	NO.
Moyna grout pumps	az Hp	2
Grout Plant for Cement		
Graut Mixer (First twank loaly), 1000 West		
CONCRETE INVERT (ANO WALKWAYS)	·	
DESCRIPTION	CAPACITY	NO.
Belterete Swinger conveyor system		
VENTING, PUMPING, COMPRESSION, EQUIPMENT		
DESCRIPTION	CAPACITY	NO.
Joy Air Ean for Ventilation	50,H0	
Joy Air Fan for Ventilation Gardner Denver compressor	50 Hp 185 Hp 500 Cfm	2
7 DTHER (Specify)		

CASE HISTORY DATA

E QUANTITIES (NOT INCL. ACCESS SHAFT)

UANTITIES (NOT INCL 1. TUNNEL (IF MULTIPLE, SH			-
LENGTH	2,903		F
INSIDE O RR : 17	"0" RL: 1	1'- 0"	
	reular		
NO. CROSS OVERS, IF MUL			E,
TOTAL EXCAVATION			c
TUNNEL PRESSURE RANG	E O	PSI C) P
2. GROUTING (CY)	· · · · · · · · · · · · · · · · · · ·		
	EST	ACT	UAL
BEHINO TEMP. LINING			
CONSOLIDATION (FACE)			
PREGROUTING			
3. PRIMARY LININ	G		
OESCRIPTIC	N	OUAI	ITITY
Welded Steel Ric	as-Circular	58	ò
	J		
4. FINAL LINING			
TYPE CONCECTC			
NO. LINERS IF PREFAB OR	PRECAST		E
OUANTITIES IF CAST IN PL	ACE		
DESCRIPTIO	N	OUAN	ITITY
CONCRETE			(C
			(T 0)
REINFORCING			
REINFORCING FORMING			(5
			(5

6. INVERT (AND WALKWAYS), ARCH	
DESCRIPTION	OUANTITY
CONCRETE - Invert	RR: 1196 (CY)
REBAR	(TONS)
FORMS	(S.F.)
STRUC. STEEL	(TONS)
Walkways RR: 299 cy Cross-Passage	RL: 285 CY
7. MAJOR UNDERPINNINGS	1 I
DESCRIPTION	AREA (S.F.)
	11
TOTAL	
8. AIRLOCK SYSTEM (IF USEO)	1
MANLOCKS	
N UM BE R	(EA)
LENGTH	(FT)
DIAMETER	(FT)
MUOLOCK	
NUMBER	(EA)
LENGTH	(FT)
DIAMETER	(FT)
BULK HEAD DESIGN	PSIG

_		SHE	т_4	_ OF
9 APPURTENANT STR	UCTURES			
TEMPORAR	ACCESS	SHAFT		
CONSTRUCTION METH	00. Jole	licr pil	c an	ď
Lagging wi	th tic	bast	or lo	teral
support for				
WIDTH 45 IFT			DEPTH	FT
WALL THICKNESS				
EXCAVATION OVANTI	TES			(C Y)
CONCRETE OUANTITIE	\$			(C Y)
PUMPING STATIONS		• • •		
CONSTRUCTION METH	00			
<u> </u>				
CONFIGURATION				
DEPTH	(FT)	DIAMETER		(FT)
EXCAVATION QUANTI	TIES			(C Y)
CONCRETE OVANTITIE	s			
OTHER APPURTENA	NCES (SPECIF	Y}		
DESCRIPTION	EXCA	/ (CY)	CON	CRETE (CY)
	1		-	
10. SITE PREPARATION	& RESTORAT	rion .		
DESCRIPTION	TY	PE	A	REA (S.F.)
CLEAR & GRUB				
REMOVAL				
RESTORATION				

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY DATA

8 3RO SHIFT

> ist 2

1. CREW - Heading	a Cr	cw		2. CREW - Grout	Crew	
HIFTS / DAY 3		SHIFT =	8	SHIFTS / DAY	HOURS /	SHIF
WORKING DESIGNATION	1ST Shift	2ND SHIFT	3 R D SHIFT	WORK DESIGNATION	1ST Shift	Z SH
Shift Boss	1	1	1	Grout Forema	01	
Surveyor	1	1)	Grout Man	3	
ihield Operator	1	1.	1		_	
luck Operator	1	1				
Miner	4	4	н			
				TOTAL	4	\vdash
				Coulking Crew		ic y
				Laborer		
					_	
						-
					-	
TOTAL	8	8	8	TOTAL		

3. CREW - Top and 3	haft	Crei	ى
SHIFTS / DAY	HOURS /		
WORK DESIGNATION	1\$T Shift	ZN D Shift	3RO SHIFT
Compressor Operate	1	1	1
Compressor Operate Forklift	1		
Laborer	1		
TOTAL	3	1	1
Corpenter Crew		hrs	11111
Corpenter Supt.			
Carpenter Foreman	11		
Carpenter Supt. Carpenter Foremon Carpenter	4		
,			
TOTAL	6		

SH	EET5	0F	
4 CREW - Cleanup	Crei	<u>ى</u>	
SHIFTS/DAY	HOURS /		8
WORK DESIGNATION	1ST SHIFT	2NO SHIFT	3RO Shift
Shifter		1	
		1.	
Compressor		1	
Laborer Compressor Berrator Forklift		1	
TOTAL		9	
Concrete Crew	1-8	hr St	nift
Shifter			
Belt Operator	1		
Swing Operator			
Vibrator Man	3		
Laborer	3		
Finisher	a		
TOTAL	11		

1) NOTE CATEGORY OF CREWS (HEADING, SUPPORT SURFACE, SHAFT ETC.) REPORT AS LOGGED

Appendix A-1. (Continued)

2

CASE HISTORY DATA

PROJECT NAMENEN CARPOLITO	Rome DONUMBER	100001
		100091
OWNER WHATA	Tax, D.C.	JOSEPH K. KNOERLE
CONTRACTOR FRUIN - CO		JOSEPH L. LNOERLL
		AC
OATES: START /- 30 -		5.4.15
PROJECT SCOPE (INCLUDE ANY APPUI	RTENANT STRUCTURES)	
735 L.F.	DUAL TUNNEL U	U POCTAL
VESKINED AS OPE	a Cuy- CHANG	EO TO FOUNEC \$ \$ 520,000 =
	- SAVINGS O	F # 520,000 =
DWNER FURNISHED MATERIAL AND E	OUIPMENT LIST Nor	E
)THER OWNER SUPPLIED COST ITEMS	(e.g INSURANCE)	
DTHER OWNER SUPPLIED COST ITEMS	(e.g INSURANCE)	
OTHER OWNER SUPPLIED COST ITEMS	(e.g INSURANCE)	

. DESIGN INFORMATION.		SHEET_	1	JF
1. PLAN AND PROFILE ATTACHED			YES	NO
2. TYPICAL SECTION DRAWING ATTACHED:			YES	NO
3. TEMPORARY LININGS DETAILS ATTACHED			YES	NO
4. PERMANENT LININGS DETAILS ATTACHED:			YES	NO
5. GEOLOGICAL PROFILE ATTACHEO:			YES	NO
6. VERBAL DESCRIPTION OF SOIL CONDITIONS:				
MOSTLY CLAY WITH SOME SAND	Е Семе	N16	0	_
			YES	NO
8. GROUND WATER CONDITIONS DESCRIPTION			YES	NO
8. GROUND WATER CONDITIONS DESCRIPTION			YES	NO
7. DEWATERING PLAN ATTACHED 8. GROUND WATER CONDITIONS DESCRIPTION 9. SITE PREPARATION & RESTORATION DESCRIPTION			YES	NO

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY DATA

. DESIGN INFORMATION (CONTINUED)	C. CONSTRUCTION METHOD	s	SHEET	2 OF
	1. FREE AIR. YE	5	LENGTH (FT)	735-755
	2. COMPRESSED AIR:		LENGTH (FT)	
	PSIG MIN	PSIG MAX	PSIG WTO AVG.	
	3. DESCRIPTIONS			
10. UNDERPINNING DESCRIPTION	TUNNEL EXCAVATIO	N		
UNDERPORT 22' x 23:6" SEWER STRUCTURE				
UNDERPAN 22' x 23'6" SEWER STRUCTURE 4-6" \$ INTERCEPTOR SEWER				
			· · · · · · · · · · · · · · · · · · ·	
	-			
11. UTILITIES. DESCRIPTION	TEMPORARY LINING			
STANDARD UNDERSTREET UTRATIES		e lacence 1	Cand	
SUPPOPTED AND/A RELACTED - A LADER	N/DS ¢	ELAGGING +	GROOI	
UTILITY SAVINES IN CONTRACT PARE PERMISED				
SUPPORTED AND/OR RELOCATED - A LARGE UTILITY SAVINES IN CONTRACT PRICE RESULTED IN CHANGING FROM- OPEN CUT TO TONNEL				
	FINAL LINING			
	15"	CONCRETS_		

CASE HISTORY DATA

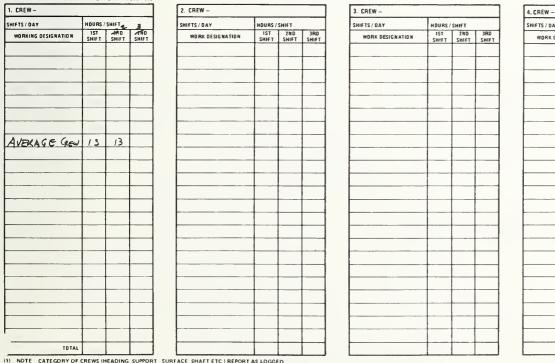
n		EOUIPMENT	UTILIZED
υ.	MAJON	COOLEMENT	UNCILED

1. CUTTING AND EXCAVATING	HAND	EXCAVATION	
MAKE			
MODEL			
TYPE:	ROTATING WHEEL	DSCILLATING ARMS	DIGGING ARM
	OTHER (SPECIFY)		
CONNECTED HORSE PO	WER		
NO. USEO			
2. SHIELD	GOOD MA	YD	
OUTSIDE DIA.	18'	LENGTH -	16:6.
NO. OF JACKS	24 THRUST	ORCE (TONS) 75 NO. O	F JACKING MOTORS
HORSE POWER EA. JAC	KING MOTOR	20	
NO. SHIELOS USEO	1		
3. MUCKING EQUIPMENT (UNDE	RGRDUND)		
TYPE FRO	WT END	LOADER	
CONVEYOR LENGTH	(FT.)	CAPAC	ПТУ (Т
RAIL CARS: NO		CAPAC	T) YTI
RUBBER TIRE VEHICLE N	EIMCO 91	ISE-LHD CAPAC	TY SCY "
COMBINATION (SPECIFY)			
4. MUCKING EDUIPMENT UNDER	GRDUND TO SURFACE	(DESCRIBF)	
LOADER T	5 TUNNE	L POLTAL	
PELADED	ON TO T	WCK FOR DIS	PaSAL
			<u> </u>

LINERS (PRE CAST)		
DESCRIPTION	CAPACITY	ND.
GROUTING	l	
DESCRIPTION	CAPACITY	ND.
CONCRETE INVERT (AND WALKWAYS)		
DESCRIPTION	CAPACITY	ND.
VENTING, PUMPING COMPRESSION EDUIPMENT		
DESCRIPTION	CAPACITY	ND
· · · · · · · · · · · · · · · · · · ·		
. DTHER (Specify)	I	

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY DATA



F. TYPICAL CREW SIZE ANO UTILIZATION (1)

SHIFTS / DAY HOURS / SHIFT WORK DESIGNATION IST ZND 3RD SHIFT SHIFT SHIFT

SHEET _____ OF __

1) NOTE CATEGORY OF CREWS INEADING, SUPPORT SURFACE SHAFT ETC) REPORT AS LOGGED

CASE HISTORY DATA

А	DESCRIPTION
---	-------------

PROJECT NAMESECTION FZA- BRANCE ROUTE	NUMBER (FOOZI		
LOCATION WASHINGTON D.C.			
3. OWNER WMATA	ENGINEER PBQD		
4. CONTRACTOR TRAYLOR BOOS. &	S,M.		
5. DATES: START	COMPLETE		
6 PROJECT SCOPE (INCLUDE ANY APPURTENANT STRUCTU	RES)		
8.855 LE TUNNEL (TWIN E	BORES- INBOUND - OUTBOUND)		
PLUS : VENTILATION ST			
UNDERGROUN ELECTRICA	K SUBSTATION,		
DRAINAGE PUMPING	STATIONS		
UNDERPINNING OF SE	REARE STRUCTURES		
7. OWNER FURNISHED MATERIAL AND EQUIPMENT LIST			
NONE			
8. OTHER OWNER SUPPLIED COST ITEMS (e.g. INSURANCE) .			

B. DESIGN INFORMATION	SHEET_	1	OF	
1. PLAN AND PRDFILE ATTACHED		YES	NB	The
2. TYPICAL SECTION DRAWING ATTACHED.		YES	NO	2
3. TEMPORARY LININGS DETAILS ATTACHED:		YES	NO	-
4. PERMANENT LININGS DETAILS ATTACHED:		YES	NO	~
5. GEOLOGICAL PROFILE ATTACHEO		YES	NO	
6. VERBAL DESCRIPTION OF SOIL CONDITIONS				
SAND WITH CLAY LENSER, SOME MEDI	UM STIFF	. 0	LAY	
SAND WITH CLAY LENSES, SOME MEDI SAND & GRAVEL LAYER WITH SM	5 BOUL	DE-	1	
7. DEWATERING PLAN ATTACHED		YES	NO	V
B. GROUND WATER CONDITIONS DESCRIPTION				
9. SITE PREPARATION & RESTORATION DESCRIPTION				
REPLACE 482 SY OF STREET PAV	EMENT			_
1075 LF - CURB & GUTTER & 555	SY Sin	cu	MAC	
TUTA LE - CURD & YUTTER & 350		000		

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY DATA

B DESIGN INFORMATION (CONTINUED)	C. CONSTRUCTION METHODS	SHEET OF
	1. FREE AIR.)ES	LENGTH (FT)
	2. COMPRESSED AIR	LENGTH (FT)
	PSIG MIN PSIG MAX	PSIG WTO AVG.
	3. DESCRIPTIONS	
10. UNDERPINNING DESCRIPTION	TUNNEL EXCAVATION	
TEMPORARY SUPPORT OF 7th STREET BRIDGE	BRENITOE EXCAVATION	THRU SHIGED - MUCK
WITH GROUT UNDER PINNING	REMOVED BY CONVE	YOR BELT TO RAIL
	NOUNTED MUCK CA	ves .
GROUT UNDER PINNING- JEFFERSON MEMORIAL	TUNNEL GROUTED TH	RU STEEL LINER
JUNIOR HIGH SCHOOL	PLATES	
11. UTILITIES. DESCRIPTION	TEMPORARY LINING NONE.	
STANDARD UTILITY INSTALLATIONS BURIED IN		
STREETS ABOVE-SUPPORTED AND/OR RELACTED		
AS REQUIRED		-
	SINAL LINING STEEL LINA	ER CATES

CASE HISTORY DATA

D. MAJOR EQUIPMENT UTILIZED

1. CUTTING	AND EXC	AVATING							
м	AKE								
M	OOEL								
T	PE		ROTATING	G WHEEL	OSCI	LATING AR	MS	DIGGING ARM	
			OTHER (S	SPECIFY)					
C	DNNECTEO	HOR SE POW	ER						
N	O. USEO							,	
2. SHIELO			A	ROBL	SINS				
0	UTSIOE OI	A.		8'-0"		LENGTH	1	16:60	
N	0. OF JACH	<s< td=""><td>24</td><td>THRUST I</td><td>FORCE (TON</td><td>51 73</td><td>NO. OF</td><td>JACKING MOTORS</td><td>4</td></s<>	24	THRUST I	FORCE (TON	51 73	NO. OF	JACKING MOTORS	4
Þ	ORSE POW	ER EA. JACK	ING MOTO	R	2	50			
N	O. SHIELO	S USEO		/					
. MUCKIN	G EOUIPM	ENT (UNDER	GROUNO)						
т	YPE		FROM	IT EN	o ha	DER	2		
0	DNVEYOR	LENGTH		(FT.)			CAPACI	ТУ	(T)
R	AIL CARS	NO					CAPACI	ТУ	{ T
R	UBBER TIRE	E VEHICLE NO		9150	41L	EIMO	CAPACIT	IN SEY	(т
° с.	DMSINATIO	N (SPECIFY)							
MUCKIN		NT UNDERG	ROUNO TO	SURFACE	(DESCRIBE)			
							-		_
		_							

LINERS (PRE CAST)		
DESCRIPTION	CAPACITY	NO.
GROUTING		
DESCRIPTION	CAPACITY	ND.
-		
CONCRETE INVERT (ANO WALKWAYS)		
CONCRETE INVERTIANO WALKWAYS)		
DESCRIPTION	CAPACITY	NO.
VENTING, PUMPING, COMPRESSION, EQUIPMENT		
DESCRIPTION	CAPACITY	NO.
0.00111107		
OTHER (Specify)		

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY DATA

E. QUANTITIES (NOT INCL. ACCESS SHAFT)

1. TUNNEL (IF MULTIPLE, SHO	W FOR EACH)		
LENGTH 2942	1B - 298	O'OB	FT
INSIDE D.D.	OUTSIDE O	° 18'+	.,
CONFIGURATION			
NO. CROSS OVERS, IF MULT	IPLE		EA.
TOTAL EXCAVATION			CY
TUNNEL PRESSURE RANGE		PSI	PSI
2. GROUTING (CY)			
	ESY	ACTUAL	
BEHINO TEMP. LINING			_
CONSOLIDATION (FACE)			
PREGROUTING			_
3. TEMPORARY LINING (IF USE	0)		
OESCRIPTION		OUANTITY	
. FINAL LINING			
TYPE STA	LINER 1	PATE	
NO. LINERS IF PREFAB OR PR			EA
OUANTITIES IF CAST-IN-PLAC	CE		
OESCRIPTION		OUANTITY	
CONCRETE			(C Y)
REINFORCING) (T	0 % 5)
FORMING			(SF)

6. INVERT (AND WALKWAYS), ARCH	
DESCRIPTION	OUANTITY
CONCRETE	(C)
REBAR	(TON:
FORMS	(S.F
STRUC STEEL	(TO N
7. MAJOR UNDERPINNINGS	
DESCRIPTION	AREA (S.F.)
CHEMICAL GROUT -	
JEFFERSON LUSION #15.	
CHEMICAL GROUT- JEFFERSON JUSION H.S. 715 STREET BRADGE	1
TOTAL	
AIRLOCK SYSTEM (IF USED)	
MAN LOCKS	
NUMBER	(EA)
LENGTH	(FT)
DIAMETER	(FT)
MUO LOCK	÷
NUMBER	. (EA
LENGTH	(FT)
DIAMETER	(FT)
BULK HEAO OESIGN	PSIG

		SHE	ET	OF
9. APPURTENANT ST	RUCTURES			
VENT AND FAN SH	IAFTS			
CONSTRUCTION MET	HOO: 501.0	ina Ri	est L	SEGING
CONSTRUCTION MET	Course	To klas	11.	Same
		/ / 9/75	~q ·	
WIOTH (F	T) BREADTH	FT	ОЕРТН	FT
WALL THICKNESS			l	
EXCAVATION OUANT	ITES			(CY)
CONCRETE OUANTIT	IES			(CY)
PUMPING STATION	s			
CONSYRUCTION MET	H0 0:		_	
CONFIGURATION				
OEPTH	(FT)	DIAMETER		(F T)
EXCAVATION OUANT	ITIES			(C Y)
CONCRETE DUANTITI	ES			
OTHER APPURTEN	ANCES (SPECIF	Y)		
DESCRIPTION	EXCA	V. (CY)	CONC	RETE (CY)
	-			
10. SITE PREPARATIO	N & RESTORA	TION		
OESCRIPTION	TY	PE	ARE	A (S.F.)
CLEAR & GRUB				
REMOVAL	PAVIA	16		
RESTORATION	REPA	VE		

CASE HISTORY DATA

F. TYPICAL CREW SIZE AND UTILIZATION (1)

1. CREW -				2. CREW -	
SHIFTS / DAY	HOURS	SHIFT	3	SHIFTS / DAY	
WORKING DESIGNATIO	N 1ST SHIFT	SHIFT	SHIFT	WORK DESI	SNATION
SUPERWIENDE	J7 1	1			
WALKER	li	1			
SHIFTER	1	1			
DPERATOR	2	1			
MECHANIC		1			
MINER	8	8			
ENGINEER		1			
SURVEYOR	2	2			
ELECTRICIA	<u> </u>	'			
	_				
TOTAL	23	23			
10140		5			
-	_				
	-				
TO	TAL				

]	3. CREW ~
	HOURS /				SHIFTS / DAY
	1ST SHIFT	2ND SHIFT	3RO Shift		WORK DESIGNATION
				1	
_					
-					
-					
				1	
-					
_			L		

CREW ~			
HIFTS / DAY	HOURS/		
WORK DESIGNATION	1ST Shift	2NO SHIFT	3RO Shift
		1	
	1		

SH	EET5	OF	
4. CREW –			
SHIFTS / DAY	HOURS /		
WORK DESIGNATION	1ST SHIFT	2ND SHIFT	3R O Shift
		_	
	_		

(1) NOTE CATEGORY OF CREWS (HEADING, SUPPORT SURFACE, SHAFT ETC) REPORT AS LOGGED

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY DATA

1. CREW- Mining Crew				م ب 2. CREW – ع	2. CREW - Support Crew				Cre	ω		4. CREW - Bull Gaing			
HIFTS/DAY 3	HOURS /	SHIFT S		SHIFTS / DAY 3	HOUR	S / SHIFT	8	SHIFTS / DAY 3	HOURS /		8	SHIFTS / DAY 3	HOURS / SHIFT 8		8
WORKING DESIGNATION	1ST Shift	SHIFT	3 R D SHIFT	WORK DESIGNATION	1ST SHIF	2ND SHIFT	3RO Shift	WORK DESIGNATION	1ST SHIFT	2ND SHIFT	3R0 SHIFT	WORK DESIGNATION	1ST SHIFT	2ND SHIFT	3F SH
Foreman	T	1	1	Foreman	1	1	1	Foreman	1	1	1	Foreman	1	1	1
shield Operator				Crane Operat	ar I	1	1	Nozzlemen	2	a	a	Miners	H	4	4
Miners	7	7	7	Crane Oiler	- 1	1	1	Pumpman	1 1	1	1				1
luck Operator	1	1		Botton Mer	n a	a	a	Helpers	2	a	2				L
onveyor Operator	I.	i		Compressor	Qar I	1	1								
conveyor Operator occurative Oper	à	a	a	Top Man	. 1	1									L
									+						╞
					_		 							-	⊢
							 								-
			\vdash				<u> </u>								-
							+						+		
													-		-
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									+ · · ·						\vdash
						-									-
													+		-
					_								1		
TOTAL	13	13	13	TOTE	17	7	7	TOTAL	1	(7	TOTAL	5	5	

CASE HISTORY DATA

A. OESCRIPTION		
1. PROJECT NAME	1F0012	NUMBER FIB
2. LOCATION	NASHINGTON D	, C.
3. OWNER	MATA	ENGINEER
4. CONTRACTOR		
5. OATES: START		COMPLETE
6. PROJECT SCOPE (INCLU	DE ANY APPURTENANT STRUCTU	RES)
		_
7. OWNER FURNISHED MAT	FERIAL AND EQUIPMENT LIST	
	*	
8. OTHER OWNER SUPPLIER	D COST ITEMS (e.g. INSURANCE)	

8. DESIGN INFORMATION S	SHEET	1	OF .		
1. PLAN AND PROFILE ATTACHED		YES	1	NO	L
2. TYPICAL SECTION DRAWING ATTACHED		YES	1	NO	-
3. TEMPORARY LININGS DETAILS ATTACHED:		YES	1	NO	~
4. PERMANENT LININGS OETAILS ATTACHEO:		YES	1	NO	2
5. GEOLOGICAL PROFILE ATTACHEO:		YES		NO	v
			4		
6. VERBAL DESCRIPTION OF SOIL CONDITIONS.					_
SAND - SOME CLAY, BOULDERS	ĘĢ		410	-	
7. OEWATERING PLAN ATTACHED 8. GROUNO WATER CONDITIONS DESCRIPTION		YES	1	NO	-
9. SITE PREPARATION & RESTORATION DESCRIPTION					

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY DATA

B. DESIGN INFORMATION (CONTINUEO)	C. CONSTRUCTION METHODS	SHEET OF .	
	1. FREE AIR YES	LENGTH (FT) ラろろ	, K
	2. COMPRESSED AIR	LENGTH (FT)	
	PSIG MIN PSIG MAX	PSIG WTO AVG.	
	3. DESCRIPTIONS		
10. UNDERPINNING DESCRIPTION NONC	TUNNEL EXCAVATION		
· · · · · · · · · · · · · · · · · · ·			
11. UTILITIES. DESCRIPTION	PRIMARY LINING		
No SPECIAL GROUTING, ETC	STEEL RIBS \$	WOOD LAGGING	
No SIBELAL GROWTING, ETC.			
	FINAL LINING		
	15" CONCRETE		
L			

CASE HISTORY DATA

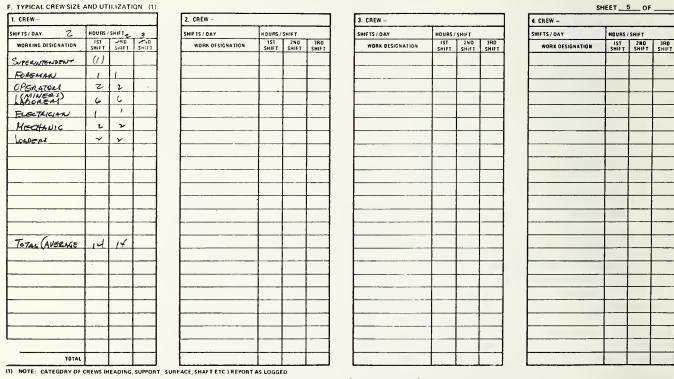
D. MAJOR EQUIPMENT UTILIZED

1. CUTTING AND EXCAVATING HAND MINING					
MAKE					
MODEL					
TYPE:	ROTATING WHEEL	OSCILLATIN	G ARMS	DIGGING ARM	
	OTHER ISPECIFY)				
CONNECTED HORSE P	OWER				
NO. USEO					
2. SHIELD M	ILWAUKEE	BOILER	S MEG		
OUTSIDE DIA.	2017	LEI	NGTH	21,9'	
NO. OF JACKS	THRUST	FORCE (TONS)	Z, SOO NO. OF	JACKING MOTORS	
HORSE POWER EA. JA					
NO, SHIELOS USEO					
3. MUCKING EQUIPMENT (UND	ERGROUNO)				
TYPE:					
CONVEYOR: LENGTH	(FT.)		CAPACIT	r¥	(11)
RAIL CARS: NO.			CAPACIT	ГY	៣
RUGGER TIRE VEHICLE	NO.		CAPACIT	rv	(11)
COMBINATION OPECIFY)				
4. MUCKING EQUIPMENT UNDE	AGROUND TO SURFAC	E (DESCRIBE)			

OTHER MATERIAL HANDLING EQUIPMENT (SPECIFY) SURF	ALE TO HEADING	
LINERS (PRE CAST)		
DESCRIPTION	CAPACITY	NO.
GROUTING		
DESCRIPTION	CAPACITY	NO.
CONCRETE · INVERT (AND WALKWAYS)		
DESCRIPTION	CAPACITY	NO.
VENTING, PUMPING, COMPRESSION, EQUIPMENT		
DESCRIPTION	CAPACITY	NO.
7. OTHER (Specify)		

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY DATA



CASE HISTORY DATA

A. DESCRIPTION	
1. PRDJECT NAME Embarcoders to Montgomery.	NUMBER 150051-14
2. LOCATION San Francisco, Calife	
3. OWNER BARTD	ENGINEER PBTB
4. CONTRACTOR	
5. DATES: START /0/8/70	COMPLETE 2/5/7/
6. PRDJECT SCOPE (INCLUDE ANY APPURTENANT STRUCTU	
Approximately 1440 ft	of twin subway
Approximately 1440 ft line tunnels	J
7. OWNER FURNISHED MATERIAL AND EQUIPMENT LIST	
8. DTHER OWNER SUPPLIED CDST ITEMS (e.g. INSURANCE)	-

B. DESIGN INFORMATION.	SHEET	1 (OF
1. PLAN AND PRDFILE ATTACHED:		YES	ND
2. TYPICAL SECTION DRAWING ATTACHED		YES	ND
3. TEMPDRARY LININGS DETAILS ATTACHED:		YES	ND
4. PERMANENT LININGS DETAILS ATTACHED:		YES	ND
5. GEOLDGICAL PRDFILE ATTACHED:		YES	ND
6. VERBAL DESCRIPTION OF SOIL CONDITIONS. Mostly, clay, and sand with sar	ne ha	ard	
Mostly clay and sand with sar ground encountered. Ground stoo well	d up	fai	rly
7. DEWATERING PLAN ATTACHED		YES	ND
8. GROUND WATER CONDITIONS DESCRIPTION			
Dewatering wells were used the	rougl	hoc	<u>.t.</u>
9. SITE PREPARATION & RESTORATION DESCRIPTION			

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY OATA

DESIGN INFORMATION (CON	TINUED)
0. UNDERPINNING DESCRIPTION	
. UTILITIES. DESCRIPTION	

C. CONSTRUCTION METHODS	SHEET	2 OF
1. FREE AIR: VCS	LENGTH (FT)	729.7 Ft.
2. COMPRESSED AIR: V,CS	LENGTH (FT)	709.96+
PSIG MIN O PSIG MAX 13,82	PSIG WTD AVG.	
3. DESCRIPTIONS		
TUNNEL EXCAVATION		
Excaugtion was carried out	by a shi	eld
used with a muck conveyor	with trai	ins.
A rubber-tired uchicle was a	ulso used	
PRIMARY LINING		
Steel liner rings 21/2	ft wide	
EINAL LINING		
Concrete		

CASE HISTORY DATA

D.	MAJOR	EQUIPMENT	UTILIZED
----	-------	-----------	----------

LINERS (PRE CAST)		
DESCRIPTION	CAPACITY	ND.
•		
•		
GROUTING		
DESCRIPTION	CAPACITY	NO.
Grout Agitators		a
Chemical Grout Plant		1
Grout Pump Cars		a
,		
CONCRETE. INVERT (AND WALKWAYS)		
DESCRIPTION	CAPACITY	NO.
Concrete trucks		_10
Batch plant		1
,		
VENTING, PUMPING, COMPRESSION, EQUIPMENT		
DESCRIPTION	CAPACITY	NO.
Bottery Locomotives, Trains Cranes Muck Cors	15 Tan	1-2
Cranes	10-50 Tons	1-3
Muck Cars		6

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY DATA

E. QUANTITIES (NOT INCL. ACCESS SHAFT)				
1. TUNNEL (IF MULTIPLE, SH	OW FOR EACH)			
LENGTH SR - 709,9	6 SR-7	29.1	FT	
INSIDE DIA. 17				
CONFIGURATION CIT	cular			
NO. CROSS OVERS, IF MUL	TIPLE		EA	
TOTAL EXCAVATION			C٧	
TUNNEL PRESSURE RANG	· 2.75	PSI - 13.82	₽S	
2. GROUTING (CY)				
	EST	ACTUAL		
BEHINO TEMP. LINING		1163.5	сy	
CONSOLIDATION (FACE)			-	
PREGROUTING		1		
3. PRIMARY LINI	NG			
DESCRIPTION DUANTITY				
2. 1/a ft. Steel Rings				
4. FINAL LINING				
TYPE Concrete	-			
			EA	
OUANTITIES IF CAST-IN-PL	ACE			
DESCRIPTION DUANTITY				
CONCRETE		(C Y		
REINFORCING (ONS		
FDRMING		(\$ F		

6. INVERT (AND WALKWAYS), ARCH	
DESCRIPTION	DUANTITY
CONCRETE	(CY)
REBAR	(TONS)
FORMS	(S.F.)
STRUC. STEEL	(TONS)
7. MAJOR UNDERPINNINGS	
DESCRIPTION	AREA (S.F.)
TOTAL	
B. AIRLOCK SYSTEM (IF USEO)	
MAN LOCKS DODE	
NUMBER	(EA)
LENGTH	(FT)
DIAMETER (F	
MUDLOCK NONC	
NUMBER	(EA)
LENGTH	(FT)
DIAMETER	(FT)
BULK HEAD DESIGN	PSIG

	SHE	ET OF
9. APPURTENANT STRU	CTURES	
VENT AND FAN SHAP	TS	
CONSTRUCTION METHO	0:	
WIOTH (FT)	BREADTH FT	OEPTH FT
WALL THICKNESS		.
EXCAVATION QUANTITI	is .	(CY)
CONCRETE OUANTITIES		(CY)
PUMPING STATIONS		
CONSTRUCTION METHO):	
CONFIGURATION		
DEPTH	(FT) DIAMETER	(FT)
EXCAVATION DUANTITI	ES	(CY)
CONCRETE OU ANTITIES		
OTHER APPURTENAN	CES (SPECIFY)	
DESCRIPTION	EXCAV. (CY)	CONCRETE (CY)
10. SITE PREPARATION &	RESTORATION	
DESCRIPTION	TYPE	AREA (S.F.)
CLEAR & GRUB		
REMOVAL		
RESTORATION		

CASE HISTORY DATA

F. TYPICAL CREW SIZE AND UTILIZATION (1)						
1. CREW- Heading (rew						
SHIFTS/DAY 2	HOURS /	SHIFT	8			
WORKING DESIGNATION	1ST Shift	2 N D SHIFT	3RD SHIFT			
Superintendent	1					
Shift Bass	1					
Heading Engineer	1-2					
Miners	8-13					
Mechanics	1-4					
Walker	1_					
Brakeman	1	ļ				
Operators	1-2					
Motorman		ļ				
Laborers	5					
Iron Workers		<u> </u>				
Oiler						
		L				
TOTAL	28-29	21				

2. CREW - Sorface SHIFTS/DAY HOURS/SHIFT				
WORK DESIGNATION	1ST	2NO SHIFT	3R(
	SHIFT	SHIFT	SHI	
			<u> </u>	
		I	I	
	-			
			-	
			-	
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		[1	
		ļ	-	
		L		
			1	
		1	1-	
	1			
	-			

SHIF#S / DAY	HOURS /	SHIFT	
WORK DESIGNATION	1ST SHIFT	2NO SHIFT	3RO Shift
	_		
		[
			-
	-+	-	-
	-		
	1		
	-		

SH	EET <u>5</u>	OF			
4. CREW -					
SHIFTS / DAY	HOURS /	SHIFT			
WORK DESIGNATION	1ST SHIFT	2NO SHIFT	3RO Shift		

(1) NOTE. CATEGORY OF CREWS (HEADING, SUPPORT: SURFACE, SHAFT ETC.) REPORT AS LOGGED

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY OATA

A. DESCRIPTION

1. PROJECT NAME LOWER Market Street	NUMBER 15001
2. LOCATION Son Francisco, Calif.	
3. OWNER BARTD	ENGINEER PBTB
4. CONTRACTOR Shea- Ball- Granite - C	lsen
5. DATES: START 7/7/67	COMPLETE 4/10/70
6. PROJECT SCOPE (INCLUGE ANY APPURTENANT STRUCTUR	RES)
Four-bore (two bores on co	ich of a levels) stacked
steel ring lined. Total drive	
heading approximately 1570	DLF. Includes 2
cross over passages and 8	terminating tunnel
lends.	J
7. OWNER FURNISHED MATERIAL AND EQUIPMENT LIST	
Segmented steel liners	S
Electrical switchgear	
Lighting fixtures	
Vent fons with drive	rs, controls + dampers.
Power distribution (ponels
0. OTHER OWNER SUPPLIED COST ITEMS (e.g. INSURANCE)	
Right-of-ways	
System wide Workme	n's compensation Insur.
J	÷

B. DESIGN INFORMATION. SHEET 1 OF 1. PLAN AND PROFILE ATTACHED YES ND 2. TYPICAL SECTION DRAWING ATTACHED YES NO 3. TEMPORARY LININGS OFTAILS ATTACHED. YES NO 4. PERMANENT LININGS DETAILS ATTACHED YES NO 5. GEOLOGICAL PROFILE ATTACHEO: YES NO 6. VERBAL DESCRIPTION OF SOIL CONDITIONS. soil was mostly clay and sand with some solid blue clay. The ground was mostly schesive except for occassional Some areas of running arcas sand. were very ticm in consistency 7. DEWATERING PLAN ATTACHEO YES NO 8. GROUNO WATER CONDITIONS DESCRIPTION There were a few instances where water appeared at the face Wetness stayed mostly below a level of "wet" but there were instances of running water. 9. SITE PREPARATION & RESTORATION DESCRIPTION

CASE HISTORY DATA

B. OESIGN INFORMATION (CONTINUED)	C. CONSTRUCTION METHOOS	SHEET OF
	1. FREE AIR:	LENGTH (FT) 6, 283
	2. COMPRESSED AIR: not yacd	LENGTH (FT)
	PSIG MIN PSIG MAX	PSIG WTD AVG.
	3. DESCRIPTIONS	
10. UNDERPINNING DESCRIPTION	TUNNEL EXCAVATION	
	Excavation for tunnel s	L was with a 17.92 H
	shield with a digger orm	Tunnels SR. TR. and
	The used on 18.08 ft. 31	nicld with a digger
	arm. All tunnels used	a conveyor belt
	and train for muck rer	noval. About one-
	half of the mining wa	s done by hand.
	J	J
11. UTILITIES. DESCRIPTION	PRIMARY LINING	
Remove relocate, support or replace existing utility lines such as storm drains sonitary sewers, water, gas, lighting and power distribution, and Muni lines.	Segmented 2-1/2 ft. stee	el liners
existing utility lines such as storm drains		
sonitory sewers, water, gas, lighting and		
power distribution, and Muni lines.		
	FINAL LINING	
	Concrete	

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY DATA

MAJOR EOUIPMENT					*	_
MAKE						
MDDEL						
TYPE	B	DTATING WHEEL	OSCILLATING ARMS DIGGING A		OIGGING ARM	X
		THER (SPECIFY)	lond 1			1
CONNECTED HD		Not Au	- ilabla	-lining		
ND, USED		Not HU	u la Dic	-		
2. SHIELO						
OUTSIDE DIA.		18.08 f		LENGTH		
NO. OF JACKS		THRUST F	ORCE (TONS)	54-5800	TR - 4800	
HORSE POWER E	A. JACKING		<u> </u>	3/(+14	- 3600	
ND, SHIELOS US	seo /					
3. MUCKING EQUIPMENT	UNDERGRO	UND)				
TYPE: COC	UEUOC	But an	d tonin	15		
CONVEYOR: LE		(FT.)		CAPACIT	Y	(1
RAIL CARS.	NO.			CAPACIT	Y	(7
RUDDER TIRE VE	ICLE NO.			CAPACIT	Y	ſ
CONBINATION (SP	ECIFY)					
. MUCKING EQUIPMENT	UNDERGRO	UND TO SURFACE	(OESCRIBE)			
						-

LINERS (PRE CAST)		
DESCRIPTION	CAPACITY	NO.
GRDUTING		
OESCRIPTION	CAPACITY	NO.
Grout Machine		1
CONCRETE INVERT (AND WALKWAYS)		
DESCRIPTION	CAPACITY	NO.
Truck Mounted Thompson Concrete Pump		1
. VENTING, PUMPING, COMPRESSION, EQUIPMENT		
DESCRIPTION	CAPACITY ·	NO.
Battery Las amotives		1-2
Battery Locomotives Einco Air Mucker		
Crones	60 tons	1-2
7. OTHER (Specify)		

Appendix A-1. (Continued)

CASE HISTORY DATA

TUNNEL (IF MULTIPLE, SH	IOW FOR EACH)		
	567		FI
INSIDE DIA. 16	6 OUTSIO		
CONFIGURATION & SIG	à levels -	ores on	each
NO. CROSS OVERS, IF MUL		2	EA
TOTAL EXCAVATION			CI
TUNNEL PRESSURE RANG	E O	PSI	PS
2. GROUTING (CY)			
-	EST		ACTUAL
BEHINO TEMP_LINING			
CONSOLIDATION (FACE)			
PREGROUTING			
3. PRIMARY LINING	1		
PRIMARY LINING	G		
DESCRIPTIO	DN	0	UANTITY
	DN	0	IUANTITY
DESCRIPTIO	DN	0	IUANTITY
Description Segmented ste	DN	0	UANTITY
Description	cl rings	0	IUANTITY E/
DESCRIPTIC Segmented ste A. FINAL LINING TYPE CONCRET	C.	0	
DESCRIPTION Segmented ste 4. FINAL LINING TYPE CONCICCT NO. LINERS IF PREFABOR	CL Fings		
DESCRIPTION Segmented ste 4. FINAL LINING TYPE CONCICCT NO. LINERS IF PREFAB OR OUANTITIES IF CAST IN PL	CL Fings		E/
DESCRIPTIC Segmented ste 4. FINAL LINING TYPE CONCIECT NO. LINERS IF PREFAB OR OUANTITIES IF CAST-IN-PL DESCRIPTIC	CL Fings		E/ UANTITY
DESCRIPTION Segmented ste 4. FINAL LINING TYPE CONCICCT NO. LINERS IF PREFABOR	C.		

6. INVERT (AND WALKWAYS), ARCH	
DESCRIPTION	DUANTITY
CONCRETE	(CY)
REBAR	(TONS)
FD RMS	(S.F.)
STRUC. STEEL	(TONS)
7. MAJOR UNDERPINNINGS	
DESCRIPTION	AREA (S.F.)
TOTAL	
8 AIRLOCK SYSTEM (IF USED)	
MAN LOCKS DODC	
N UMBE R	(EA)
LENGTH	(FT)
DIAMETER	(FT)
MUOLOCK NONE	
NUMBER	(EA)
LENGTH	(FT)
DIAMETER	(F T)
BULK HEAO OESIGN	PSIG

		SHE	ET	OF		
9. APPURTENANT STRUCTURES						
VENT ANO FAN SHAFTS						
CONSTRUCTION METHOD						
WIDTH (FT)	BREADTH	FT	DEPTH	FT		
WALL THICKNESS						
EXCAVATION QUANTIT	ES			(CY)		
CONCRETE OVANTITIES	5			(C Y)		
PUMPING STATIONS						
CONSTRUCTION METHO	0:					
			_			
CONFIGURATION						
DEPTH	(FT)	DIAMETER		(FT)		
EXCAVATION OUANTIT	IES			(C Y)		
CONCRETE OUANTITIES	i					
OTHER APPURTENAN	ICES (SPECIF	Y)				
DESCRIPTION	EXCA	(CY)	CON	ICRETE (CY)		
10. SITE PREPARATION & RESTORATION						
DESCRIPTION	τy	PE	A	REA (S.F.)		
CLEAR & GRUB						
REMOVAL						
RESTORATION						

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY DATA

1. CREW -				2. CREW -				3. CREW			
SHIFTS / DAY 3	HOURS		γ	SHIFTS / DAY	HOURS /	SHIFT		SHIFTS / DAY	HOURS /	SHIFT	
WORKING DESIGNATION	1ST SHIFT	2 N D SHIFT	3 R O Shift	WORK DESIGNATION	1ST SHIFT	2NO Shift	3RD SHIFT	WORK DESIGNATION	IST '	2ND SHIFT	3R0 SHIFT
Compressor Husens	1										
Laborers					_					<u> </u>	-
Mechanics	1-5										ļ
Operator	1-2	1-2	1-2		-						
Motorman	1	1	1								
Brokeman	1	L.							1		
Oiler	1	1									
Shifter		1							-		
Miners	7-13	7-13	7-13								
Surveyors			3-5						ĩ		
Iron Workers											
Grout Crew									_		
Grout Crew Superintendent Walkers	,	1			1						
L blkers	1	1	1		1					-	
	†										
					+				-		
	†					-					
					+						
					-						
	-										
TOTAL											

	HEET <u>5</u>		
4. CREW -			
SHIFTS / OAY	HOURS /	SHIFT	
WORK DESIGNATION	IST SHIFT	2N D Shift	3AD Shift
	1		
	+		
	+		
	+		
······································	+ +		
	+ +		
	+		
	1		
	+ +		
	1		

(1) NOTE CATEGORY OF CREWS (HEADING, SUPPORT, SURFACE, SHAFT ETC.) REPORT AS LOGGED



Appendix A-2

A record of the weekly average, for each tunnel studied, of the

- progress rate,
- down hours and
- soils encountered.

All data, including those concluded to be outliers, are listed. These data are also available on the punched-card data sets submitted.

PROGRESS AND PRODUCTION

(AY AREA RAPIO TRANSIT DISTRICT CONTRACT NUMBER IPOD3I PR TUNNEL - 24TH TO FANJALL STPLEY SAN FRANCISCO, CALIFORNIA

					00%	NHOURS -	HOURS.	A MEE K			FEL	ATIVE	FFLO	LENCY THE W		IL T	YPE C	URING	
				-====							= = = :		=====			= = = = = =	====		
STATION AT START OF WEEK	RATE FT/wK	FEET TC LATE	HRS 1N ⊾EE⊁		EQUIP		TRANS	s		HOURS	-		11I =====		v =====				RUNNING #ATER#
														_					
300.83	15.00	15.00	8°CO	• JO	•00	•CU	. 60	• 0 0	• 90	• 00	.00	1.00	.00	• วย	- C C	• 00	1.00	.00	•20
360.68	32.50	47.50	32 •f G	00،	5.00	• C O	• CO	2.50	.U0	7.5C	• C 0	1.00	+00	•ûJ	•00	•00	1.00	.00	•20
300.35	187.50	235.00	110+00	0ب و	• O C	• 0 0	• 00	10.60	•00	10.60	.Ľ0	1.00	۰U0 ه	. 96	.00	00.	1.00	• • • 0	•20
298.48	97.50	332.50	41.60	ូមព	.00	• G D	+00	78.00	1.00	79.00	0،	1.00	•00	. 30	۰00	•CO	1.00	• O C	•20
257.50	220.00	552+5C	111.00	• 0	2.00	•00	4 • 00	3.00	. 30	9.00	•50	•50	• O C	.00	.00	•CC	1.00	•00	•20
295.30	127.50	680.00	56.00	.00	5.00	• 0 0	•00	I7.00	.00	22.00	.57	.50	.00	.00	•00	•00	I+CO	.00	•20
294.03	145.00	825.00	54.00	• 30	• C C	• ว 0		66.50	•00	66.50	• 50	•5C	• 2 O	•00	•00	•C0	1.00	•00	.20
252.56	260.00	1685.00	94.fi	• J0	7.00	• 0 0	+ U 0	19+00	.00	26.00	.50	.56	•2 C	.00	+ C/C	• C D	1.00	•00	•26
289.98	292.50	1377.50	94 .(.)	•C.0	.00	.CO	.LC	26.50	.00	26.50	•10	1.00	•1C	.05	• C O	۰۳۵	1.00	. nc	.20
287.05	125.00	1502.50	64.CD	• .0	19.00	.00	۵۵ •	17.00	.00	36.00	.10	1.00	+10	. 96	00،	•00	1.00		•20
215.80	155.00	1657.50	77.CJ	00	29.00	• D D	-60	14.UC	۰UO	43.06	.10	1.00	.10	.00	•00	.00	1.00	.00	.20
264.25	192.50	1650.00	90.00	.00	٤.00	.00	• C O	22,00	.00	30.00	+10	1.00	.IC	ن0.	.00	⇔(:0	1.04	J + 00	•20
262.33	I18.00	I96C.00	56.CO	•60	56.00	•00	.00	13.50	• J D	69.50	.10	1.00	.35	.00	.00	.00	1.00	.00	•20
261.23	96.00	2050.00	112+50	0 ن ه	3.00	.00	.00	5.40	.00	8.06	.10	1.00	.35	.00	•60	.00	1.00	.00	.20
280.33	250.00	2300.00	86.FU	• JN	15+00	• 0 0	• 00	18.50	۰00	33.50	.10	1.00	.35	•9J	•60	.00	1.00	.00	•20
277.63	257.50	2557.50	82.00	• 10	19.50	• C O	•OC	18.50	.00	38.00	· 10	1.00	.35	.00	.00	.00	1.00	.00	•20
275.25	306.00	2857.50	95.00	.J0	5.50	• C D	4.00	15.50	.00	25.00	.10	I+0C	• 3 5	•00	•00	• C O	1.00	.00	• 2 O
272.25	245.00	3102.50	100.00	.00	16.00	• 00	• 00	4.00	.00	20.00	.15	1.00	.15	.Où	.00	.00	1.00	.00	+ 2 O
269.80	237.50	3 34 0 + 0 0	88.0	16	22.00	.00		4.50	.00	31.50					+ OC	.00	1.00	.00	2Ó
		3597.50			7.00			19.50	. JO	26.50					• 80	.00	1.00	.00	.50
FEY FOR S				+ 00		,				EY TO V									
I - S1L					v - ca	MENTED	ROUND												
11 - CLA						AT AND				- ORY		.75		NNING	WATER				

		TO CENT			CLILITICO	010010							
1I -	CLAY A	ND SAND	V1	-	PEAT AND	TRASH	0	Ξ	ORY	.75	Ξ	RUNNING	WATE
111 -	SAND A	NU GRAVEL	¥I1	-	CORESIVE	GROUNC	.25	Ξ	MOIST	I	2	FLOODED	
IV -	COBBLE	S AND COULDERS	¥111	-	RUNNING	GROUNC	.50	Ξ	WET				

PROGRESS AND PRODUCTION

.50

FAY AREA RAPID TRANSIT DISTFICT CONTRACT NUMBER IMOUSI MA TUNNEL – 24TH TO RANDALL STREET CAN FRANCISCO, CALIFORMIA CONNHOURS - HOURS/WEEK EV CAUSE STATION TUNNLL CUMUL, PEOC AT START RATE FEET TG HRS IN SHILLD EACAV CONVEYOR MUCK MISC ADMIN CF WZEK FI/WK LATE WEEP CUUIP TPANS TOTAL CONVEYOR MUCK MISC ADMIN HOURS TOTAL CONVEYOR MUCK MISC ADMIN HOURS TOTAL CONVEYOR TO A MINING MATERNA MATE 264.85 257.50 2655.00 95.60 .00 12.50 .00 .00 13.00 .00 25.50 .15 1.00 .15 .00 .00 .00 .00 .00 .00 .50 262.26 247.50 4102.50 92.00 .00 26.50 .00 .00 8.00 .00 28.50 .15 I.DO .15 .00 .00 .00 1.CO .00 .50 259.86 195.60 4297.50 83.60 .00 22.00 .00 .00 15.00 .00 37.00 .15 1.00 .15 .00 .00 .00 1.00 .00 257.65 47.50 4345.00 4I.CO .JO 76.00 .00 .UO 3.00 .00 79.0C .IS 1.00 .IS .00 .CO .00 1.00 .00 .50 257.38 86.00 4425.00 56.00 .U0 .00 .00 .00 16.50 .00 16.50 .15 1.00 .15 1.00 .80 .00 1.00 .00 .50

Appendix A-2. Average Weekly Progress Data

PROGRESS AND PRODUCTION

LAY AREA RAPIG TRANSIT CISTFICT Contract Number 100031 Mel Tunnel - 24th to Fanuall Striet San Francisco, California

					D0=1	NHOURS -	HOURS,	/wi£EK			FEL.	ATIVE	FREQU	ENCY THC W		ILT	PE 0	URING	
				_====	======						====					====			
STATION AT STADT				HICLO	EXCAN	CONVEYOR	HUCH	MT 57		TOTAL LOWN	,	11	111	1 1	v	47		v 1 T 1	RUNNING
CF SEEP		LATE	WECH	JHICLU	EGUIP	CONVETOR	TRANS		ACHIN	HOURS	*			1.	•	*1	***	****	#AICR+
	=======				======						====					====:			
263.63	2 L . U D	20.00	32.Lu	1.50	.00	.CU	.00	5.00	•00	6.50	.00	1.00	.00	•96	.LO	•€0	1.00	.00	•20
300.63	32.50	52.50	34.(Ű	2.00	2.00	-00	• 00	2.5C	.30	6.50	.03	1.00	•00	. Cu	0ن.	•00	1.00	•00	+20
200+30	122.50	175.00	76.00	• - 0	34,50	. C C	•00	5.00	5.00	44.50	•00	1.00	•00	• 00	•00	•00	1.00	.00	•20
259.08	166.00	335.úE	89.00	3.00	27.00	. C D	.00	1.00	.00	31.00	.00	1.00	.00	.ou	.00	•00	1.00	•00	.20
257.26	220.00	555.00	113.00	4 .∪C	• 30	.00	•00	1.50	1.50	7.00	•50	.50	•00	. 96	•C0	.CO	1.00	-00	.20
295.06	237.50	792.50	102.00	• 0	•00	• 120	.00	18.50	• 36	18.50	• 50	-50	•20	.00	.00	• 00	1.00	•00	.26
292.70	371.00	1162.51	112.00	•00	1.50	• 30	•00	5.00	1+50	8.00	• 50	02.	.20	.00	•00	• 00	1.00	•00	-20
289.00	187.50	1350+00	60.0	• 30	2.00	.00	.CO	13.50	2.30	17.50	•10	1.90	•10	• 00	• 00	• 00	1.00	•00	•20
287.13	137.50	1487.50	63.00	• ປຽ	•00	۵٦.	•00	14.50	•50	15.00	•10	1.00	•10	•00	-00	•00	1.00	• 00	•20
285.75	27.50	1515.50	10.00	•00	2.00	.00	.00	08.00	• JC	110.00	•10	1.00	-10	.00	.00	•00	1.00	• 00	•20
265.48	186.00	1695.00	84.(0	1.00	.00	14.00	13.00	7.50	•00	35.56	•10	1.00	•10	• 00	• 60	•00	1.00	•00	-20
283.68	175.00	1870.00	93.00	•00	16.00	•00	• 20	11.00	•00	27.00	.10	1.00	.10	.00	• 00	• 30	1.00	• 00	•20
261.93	65.00	1935.00	59.00	• 10	\$7.00	•00	.60	4.00	•30	61.30	-10	1.00	•35	.00	•00		1.00		
280.96	22.50	1987.50	ن 2.8 و 2	.00	96.00	• 0 0	• UG	4.50	• JO	92 . 5U	.10	1 .00	.35	• 30	.00	•00	1.00	•00	
260.75	175.00	2162.55	66.CO	•ü0	40.50	12.50	• 00	1.00	•00	54.00	.10	1.00	•35	•00	• 60		1.00		
279.00	332.50	2495.00	104.00	• 20	6.00	.00	•C0	10.50	• JO	16.50	.10	1.00	• 3 5	•00	.00	• 00	1.00	•00	•20
275 + 67	82.50	2577.50	56.00	0u.	58.00	- C O	•00	5.50	•00	63.50	•10	1.00	•35	•00	.00	• C O	1.00	•00	•20
274.85	210.00	2787.50	101.00	00•	\$.CO	•00	- 00	10.00	•00	19.00	•10	1.00	• 3 5	.00	• 00	.00	1.00	_	
272 .75	292.50	3 68 6 . 0 5	94.CO	•JD	6.00	•00	• CO	20.00	•50	26 • 50		1.00	•15	•00	•00		1.00		
269.83	205.00	3285.60	95.0	•00	14.50	.00	.00	9.50	.50	24.50			-15			.00	1.00	•00	-20
	LT AND G	CLAY				EMENTED G				EY TO V									
11 - CL/	AY AND S	SANU			V1 - PE	EAT AND T	PASH		(D = 0R¥		•75	= RUN	NING	WATER				

11 - CLAY AND SAND VI - PLAI AND IPASH D = DINY - /5 = NUNNING W 111 - SANG AND GRAVCL VIII - CONESIVE GROUND .25 = NOIST I = FLOODED 1V - COBBLES AND BOULDERS VIII - RUNNING GROUND .5D = WET

FAY ARCA RAPID TRANSIT DISTRICT (GNTRACT NUMBER IMDD31 PL TUNNEL - 24TH TO RANEALL STRLET SAN FRANCISCO, CALIFORNIA

PROGRESS AND PRODUCTION

					00 SM	HOURS -		WECK			RELA	T 1VE	FREOL	THE	OF SC	1L T	Y PE 0	URING	
STATION #1 START CF bCEK	TUNNSL RATE FT/ok	CUMUL. FCET TO DATE		SHIELO	EXCAV Equif	CONVEYOR	MUCF TRANS		ADMEN	TOTAL LOWN HOURS	1	11	111	IV	٧	¥1	¥ I I	VIII	RUNNING BATER+
267.78	230.00	3510.00	92.ED	•u0	21.00	.00	.UO	6.00	•\$c	27.50	• 10	1.00	.10	•00	.00	•00	1.00	.00	•20
265 .28	285.00	3795.00	95.CU	• -0	7.00	.00	• C O	16.50	1.50	25.00	-10	1.00	1.0	1.00	•80	+00	1.00		•50
262 • 42	325.00	4120.00	164.00	• 10	7.50	.00	• 00	8.5C	• 30	16.00	•15	1.00	•15	.03	•00	•CO	1.00	.00	•\$ U
259.17	160.00	4280+00	106.00	•uC	7.CO	•00	•C0	5.50	.00	12.50	•15	1.00	.15	.00	•00	.00	1.00	•00	.50
257.58	110.00	4390.00	101.00	•00	.00	•00	• 60	11.00	•0C	11.00	•15	1.00	-15	1.00	•8C	.00	1.00	.00	.50

CAY AREA RAPID TRANSIT DISTRICT Contract number 140003 Frikl tunnels Eerkeley, california

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							AUSE							THE					
STATION										TOTAL	===:					=====	=====	====	
AT START		FEET TO DATE	HRS IN NEEK		EXCAV	CONVEYOR	TRANS		ADMIN	L-O⊫N HOURS	I	II	111	ΙV	۷	VI	VII	/111 /	RUNNING WATER+
											=====								
1224.92	20.00	28.02	76 .0	4.30	.00	. 00	.00	8.00	.90	12.00	.00	٥2.	.50	.06	•00	•60	I.00	•CO	۰00
1224.72	62.00	9J.00	120.ro	• - 0	.00	.00	•60	.00	•9C	•00	•60	.50	.50	.60	0ن.	•CO	1.00	.00	•00
1224.10	73.00	163.00	118.00	• .0	.00	.00	•00	2.00	.00	2.00	• 60	•20	.50	.00	.00	.00	1.00	.00	•00
1223.37	49.00	212.00	111.00	•00	.00	.00	3.60	1.00	5.00	9.00	.00	.50	•50	+00	. GC	.00	1.00	.00	.00
1222.88	52.00		114.00	3.00	.00	.00	.00	.00	3.00	6.00	.00	.50	.50	.00	.00		1.00	.00	+00
							1.00							•00	+0C		1.00	.00	
1222.36			119-00	•00	•00	•00		•00	.00	1.00	•00	•50	•50						.00
1221.00			60 . 00	34.30	.00	•00	•00	3.00	3.00	40.00	.00	.50	.50	•00	• CO		1.00	•00	.00
1221-33	76.00	443.00	118.00	•)0	. OC	.00	• 00	2.00	•.00	2.00	•00	-50	.50	.00	•00	.00	1.00	.00	°0.0
1220.57	86.00	529.00	126.00	• 30	.00	.00	•00	•00	•00	•00	-00	-20	۰ 5 D	•06	.00	.00	1.00	•00	•00
1219.71	\$7.00	616.00	116.00	2.0	•00	.06	•Cû	٥٥.	.00	2.00	•00	°•20	•50	•00	.uó	.00	1.00	.00	.00
1213.84	96.00	712.00	111.00	2.00	•00	•00	4.00	3.00	.00	9.00	. CO	•20	.50	•00	.60	.00	1.00	.00	۰00
1217.88	59.00	771.00	78.00	2.30	.00	.00	.ú0	.00	.00	2.00	•60	•50	.50	.00	•00	.00	1.00	.00	.00
1217.29	91.00	862.00	117.00	2.00	.00	.00	.00	1.00	.00	3.00	•00	•5 O	.50	.00	-00	.00	1.00	.00	.00
1216.38	82.00	944.ED	113.00	0 ن. 5	• O C	.00	1.00	1.00	.00	7.50	•CO	.50	.50	•06	•00	.00	1.00	.00	۰00
1215.56		1016.00		20.00	.00	.00	1.00	.00	.00	21.00	.00	•30	•00	.50	.00	.00	1.00	•00	•00
1214.84		1099.00		1.00	.00	•00	.00	.00	.00	1.00	.00	•00	•00	.50	.00		1.00	.00	.00
				2.00	.00	•00	.00	.00	.00	2.00	•00	•00	•00	•50 •50	•00 •00		1.00	.00	-00
1214.01		1157.00	94.00																
1213.43		1225.00	96.00	• 70	.00	•00	.60	.00	•00	•00	•00	•00	•00	•50	•00		1.00	+00	.00
1212.74	65.00	1290.00	120.00	• 30	•00	-00	.00	•00	.00	•00	.00	-00	•00	1.00	1.00	.00	1.00	•00	•00
1212.09	84.00	1374.00	119.00	• JO	•00	.00	1.00	•00	•00	1.00	•00	.00	•00	1.00	1.00	•00	1.00	•00	•00
FEY FOR	SOIL TYP				v - cc	MENTEO G			* K	EY TO V	ALUES	FOR	RUNNI	NG =	TER				
II - CL	AY AND S	AND		v	I - PE	AT AND T	RASH		G	= 061					HATER				
III - SA 1v - CO		ARAVEL				HESIVE G NNING GR				5 = MOI		1	= FLC	10050					
									• >	0 = WE1									
			LF 3	• • • •			0040		• 3	U - 861									
				•••			0000		• 3	U - 464									
(A.Y. A DE A	04016							SS AN	•• • • • • • • • • • • • • • • • • • •										
' AY AREA CONTRACT	NUNPER	TRANSIT						SS AN											
	NUMPER	TR AN S1 T 18005 3						SS AN											
CONTRACT	NUMPER	TR AN S1 T 18005 3					PROGRE					ATIVE	FPEDI	DENCY	OF SC	:1L T	YPE D	URING	
CONTRACT	NUMPER	TR AN S1 T 18005 3		т	DG wh	HOURS -	PROGRE HOURS/ AUSE	WEEK	0 PRODU		ΓEL			THE 1	OF SC				
CONTRACT HRVAL TU EERHELEY STATION	NUMPER INNELS (, CALIF) Tunnel	TRANSIT 1ROO53 CRN1A CUMUL.	GISTFIC' Proc		00 wh	1HOURS - 84 (PROGRE HOURS/ AUSE	WEE K	0 PRODU 	TOTAL	KEL.			THE 1	EEX	====:			POLINIC
CONTRACT FRIGL TU EERFELEY STATION AT START CF BEEK	TUNNELS TUNNELS TUNNEL FATE FT/WK	TRANSIT 1ROOE3 GRN1A CUMUL. FEET TG LATE	GISTRIC PROC HRS IN WEEK	т ======= .H1ELG	DG WA	HOURS - 84 C	PROGRE HOURS/ AUSE EEEEEE R MUCK TRANS	WEEK	O PRODU Almin	TOTAL DOWN HOURS	КЕL. ==== 1	====== 11	 111	THE 1 	V	v 1	vII 1	 VIII -	RUANING VATER+
CONTRACT KR/RL TU EERHELEY STATION AT START CF WEEK	TUNNELS TUNNELS TUNNEL TUNNEL FT/44 TUNNEL	TRANSIT IROOS3 CRNIA CUMUL- FEET TC LATE	GISTFIC PROC HRS IN WEEK		CGWN Excay Equip	HOURS - 8 Y C 	HOURS/ AUSE MUCK TRANS	WEEK ====== misc	0 PRODU Almin	TOTAL DOWN Hours	κει. ==== Ι	II	111 	THE 1	V	v 1	vII (WATER+
CONTRACT KR/RL TU EERFELEY STATION AT START CF BEEK ======= 12I1+25	TUNNELS TUNNELS TUNNEL RATE FT/28 5 65-60	TRANSIT 1R0053 GRN1A EEET TC LATE 1459-00	GISTRIC PROC HRS IN WEEK ==================================	т литеге 	CG & M E XCA V E QU I P & OC	HOURS - 8 Y (PROGRE HOURS/ CAUSE RUSE TRANS TRANS	WEEK HISC +30	0 PRODU 	TOTAL DOWN HOURS 1.00	κει ==== Ι =====	11 	.00	THE 1 IV IV	V V 1.00	v 1 	vII 1.00	•00	*****
CONTRACT KR/RL TU EERHELEY STATION AT START CF WEEK	TUNNELS TUNNELS TUNNEL RATE FT/28 5 65-60	TRANSIT IROOS3 CRNIA CUMUL- FEET TC LATE	GISTRIC PROC HRS IN WEEK ==================================		CGWN Excay Equip	HOURS - 8 Y C 	HOURS/ AUSE MUCK TRANS	WEEK ====== misc	0 PRODU Almin	TOTAL DOWN Hours	κει. ==== Ι	II	.00	THE 1	V V 1.00	v 1 	vII (WATER+
CONTRACT KR/RL TU EERFELEY STATION AT START CF BEEK ======= 12I1+25	TUNNELS TUNNELS TUNNEL RATE FT/24 5 55-60 5 15-06	TRANSIT 1R0053 GRN1A EEET TC LATE 1459-00	GISTFIC PROC HRS 1N WEEK ==================================	т литеге 	CG & M E XCA V E QU I P & OC	HOURS - 8 Y (PROGRE HOURS/ CAUSE RUSE TRANS TRANS	WEEK HISC +30	0 PRODU 	TOTAL DOWN HOURS 1.00	κει ==== Ι =====	11 	111 -00 •00	THE 1 IV IV	¥EEX V I-00 1.00	v1 ===== .00 .60	vII 1.00	•00	*****
CONTRACT KR/RL TU EERKELEY STATION AT START CF MEEX 1211-25 1210.40 1210.25	TUNNELS TUNNELS TUNNEL RATE FT/JX 6 65-00 5 5-00	TRANSIT IRODE3 GRAIA FEETTC LATE 1459-00 1474-00	GISTFIC PROC HRS 1N WEEK 119.00 120.00		CG WA E XCA V E QU I P • OC • OC	.00 .00	PROGRE HOURS/ AUSE TRANS 1.00 .00	WEEK HISC 	0 PRODU ALMIN 0 00.	TOTAL 00NN HOURS 1.00 .90	€ E L . ==== I .00 .00	II II 00. 00. 00.	111 -00 •00	IV IV 1.00 1.00	¥EEX V I-00 1.00	v1 - CO - CO - CO	vII 1.00	•00 •00	**************************************
CONTRACT KR/RL TU EERKELEY STATION AT START CF MEEX 1211-25 1210.40 1210.25	TOANELS (, CALIF(RATE FT/28 6 65-60 1 15-00 5 5-00 1 119-00	CUMUL. FEET TC LATE 1459-00 1479-00	PROC HRS 1N WEEK 119.CO 120.CU 115.CO	0.0 01.0 00.0	CG W E XCA V E QU I P OC OC 00 00	140085 - 8 4 0 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	HOURS AUSE MUCK TRANS 1.00 .00	WEEK ======= HISC -30 .00 .00	0 PRODU ALMIN .00 .00	TOTAL OOWN HOURS 1.00 .00 5.00	κει. ===: Σ =00 •00 •00	II -00 -00 -00 -00 -00	111 111 000 000 000	THE 1 IV 1.00 1.00 1.00	V I -00 1 -00 1 -00	v1 •00 •60 •00	vII 1.00 1.00 1.00	IIIV IIIV 00. 00.	•00
CONTRACT 47/6L TU EERVELEY 51411 ON 41 51411 (F EER 1211-25 1210.90 1210-25 1224.93 1223.24	TUANELS (, CALIF(RATE F7748 6 65.00 5 15.00 6 119.00 1 74.00	TRANSIT 1R0053 C4N1A EUMUL. FEET TC LATC 1459.00 1474.00 1479.00 1598.00	CISTRIC PROC HRS 1N WEEK 119-C0 12C-C0 12C-C0 12C-C0 12C-C0 78-C0	JH1ELG .J0 .J0 .J0 .J0	CG WN E & CA Y E & O I P - O C - O C - O O - O O	HOURS	PROGRE HOURS/ CAUSE TRANS TRANS 1.00 .00 .00 4.L0	WEEK HISC 	ALMIN .00 .00 .00	TOTAL UOWN HOUNS 1.00 .00 5.00 2.00	€ E L . = = = = = I = = = = = . GO . GO 1. OO	II -00 -00 -30 1-06 1-00	111 111 000 000 000 000	IV IV 1.00 1.00 1.00 1.00	V I -00 1 -00 1 -00 -00 -00 -00	v1 -00 -00 -00 -00 -00	vII 1.00 1.00 1.00 1.00	•00 •00 •00 •00	• PO • PO • DO • OO • OO
CONTRACT RAFAL 10 EERPELEY STATION AT START CF BEEX 1211-25 1210.40 1210.25 1224.43 1223.24	NUREER JNNELS , CALIF(RATE F1748 5 65.00 15.00 119.00 119.00 174.00 136.07	TRANSIT 1R0053 CUMUL. FEETTC LATC 1459.00 1474.00 1479.00 1596.00 1672.00	PROC HRS 1N WEEK 119.CO 120.00 115.CO 78.CO 115.20		CG WN E XCA V E CO IP • OC • OC • OC • OC • UO • OD	HOURS - 84 C 84 C CONVE YOR 00 00 00 00 00 00 00 00	PROGRE HOURS/ LAUSE TRANS TRANS 1.00 .00 .00 4.L0 2.00 1.60	WEE K HISC 	ALMIN .00 .00 .00 .00 .00	TOTAL DOWN HOUNS 1.000 .000 5.000 2.000 1.000	FEL. 1 .00 .00 1.00 1.00 1.00	II -00 -00 -00 1.00 1.00 1.00	1111 100 000 000 000 000 000 000	THE 1 IV 1.00 1.00 1.00 1.00 .00	V V I -00 1 .00 1 .00 .00 .00	v1 .00 .00 .00 .00 .00	VII 1.00 1.00 1.00 1.00 1.00 1.00 1.00	viii .00 .00 .00 .00 .00 .00	• TO • TO • TO • OO • OO • OO • OO
CONTRACT RAFAL 10 STATION AT START CF BER 1211-25 1210.40 1210.25 1222.50 1221.12	NUMBER JNNELS CALIF RATE FT/AK 5 6 5 6 7 6 7 6 7 6 7	TRANSIT 1R0053 C4N1A FEETTC LATC 1459-00 1474-00 1479-00 1598-00 1672-00 1672-00 1672-00 1943-00	PROC HRS 1N WEEX 119.00 120.00 115.00 78.00 115.00 115.00 115.00		E XCA Y E XCA Y E QU IP - 00 - 00 - 00 - 00 - 00	HOURS - 84 C 84 C 2000 00 00 00 00 00 00 00 00 00 00	PROGRE HOURS/ AUSE TRANS TRANS 1.00 .00 .00 4.L0 2.00 1.60 8.90	чеек ====== +30 +00 +00 1.00 -00 -00	ALMIN ALMIN .00 .00 .00 .00 .00 .00 .00 .0	TOTAL OOMN HOURS 1.00 .00 5.00 2.50 1.00 8.00	KEL. 	II .00 .00 .00 1.00 1.00 1.00 I.00	111 00. 00. 00. 00. 00. 00. 00. 00.	IV IV 1.00 1.00 1.00 .00 .00 .00	V I -00 1 .00 .00 .00 .00	v1 •00 •00 •00 •00 •00 •00 •00	vII 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	viii .00 .00 .00 .00 .00 .00	.00 .00 .00 .00 .00 .00 .00 .00
CONTRACT RAFAL 10 STATION AT START CF BER 1211-25 1210.40 1210.25 1222.50 1221.12 1219.79	<pre>NUMPER TUNNELS TONNELS F, CALIF F, CALIF F, CAL F, CALIF F, C</pre>	TRANSIT 1R0053 C4N1A FEETTC LATC 1459-00 1474-00 1479-00 1672-00 1672-00 1672-00 1672-00 2659-00	PROC HRS 1N WEEX 119.00 120.00 115.00 78.00 115.00 115.00 115.00 115.00 103.00		CGwh EXCAY EQUIP .0C .0C .00 .00 .00 .00 .00		PROGRE HOURS/ AUSE TRANS 1.00 .00 .00 4.10 2.00 1.00 8.70 17.00	HISC 	ALFIN ALFIN -30 -00 -00 -00 -00 -00 -00 -00	TOTAL OOMN HOURS 1-00 -00 5.00 2.50 1.00 8.00	KEL. I .00 .00 1.00 1.00 1.00 1.00 1.00	II -00 +00 +00 1-06 1+00 1.00 I.00 I.00 I.00	111 11 00 00 00 00 00 00 00 00 00	THE 1 IV 1.00 1.20 1.20 0.00 0.00	V I -00 1 -00 -00 -00 -00 -00 -00	v1 -00 -00 -00 -00 -00 -00 -00 -00	VII 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	VIII -00 -00 -00 -00 -00 -00 -00 -00 -00	.00 .00 .00 .00 .00 .00 .00 .00 .00
CONTRACT KAPAGL 10 STATION AT START CF BER 1211-25 1210-80 1210-25 1224-43 1223-24 1222-50 1221-12 1219-79 1218-63	<pre>NUMPER INTELS TOMNELS RATE FT/JK 6 5.00 1 15.00 5 5.00 1 19.00 1 36.30 1 36.30 1 16.00 1 140.00</pre>	TRANSIT 1R0053 C4N1A FEETTC LATC 1459.00 1474.00 1479.00 1672.00 1672.00 1672.00 1672.00 2059.00 2199.00	PROC HRS 1N WEEX 119-C9 12C-C0 12C-C0 12C-C0 115-C0 78-C0 115-C0 112-C0 112-C0 112-C0 112-C0 112-C0 112-C0		CGLAN EAUTO - CC - CC - CC - CC - CC - CC - CC - C	C GNVE 8 - C C GNVE YOR 	PROGRE AUSS AUSS TRANS 1.00 .00 4.L0 2.00 1.60 8.70 2.00	WEEK HISC 	ALP 0 PROCU ALP 10 00 00 00 00 00 00 00 00 00 00 00	TOTAL DOWN HOURS 1.00 5.00 2.00 1.00 8.00 17.00 2.00	KEL. I .00 .00 1.00 1.00 1.00 1.00 1.00 1.00	II -00 .00 .00 1.00 1.00 I.00 I.00 I.00 1.00	111 11 00 00 00 00 00 00 00 00 00	THE 1 IV 1.00 1.00 .00 .00 .00 .00	V I -00 1 .00 1 .00 -00 -00 -00 -00 -00	1 v 1 v 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	v II v 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	VIII 00. 00. 00. 00. 00. 00. 00. 00.	4 TER - 00 - 00 - 00 - 00 - 00 - 00 - 00 - 00 - 00 - 00
CONTRACT KAPAGL 10 STATION AT START (F & EEX 1211-25 1224.43 1222.50 1221.22 1219.79 1210.63 1217.23	NUREER TONNELS RATE FT778 6 5.00 1 10.00 1 10.00 1 136.00 1 140.00 1 10.00	TRANSIT 1R0053 C4N1A FEETTC LATC 1459.00 1474.00 1479.00 1672.00 1672.00 1616.00 2659.00 2199.00 2329.00	PROC HRS 1N WEEK 119-C9 12C-C0 12C-C0 115-C0 115-C0 115-C0 112-C0 103-C0 112-C0 112-C0 112-C0 112-C0 112-C0		CGwh ExCAY EQUIP .0C .0C .00 .00 .00 .00 .00		PROGRE HOURS/ AUSE TRANS 1.00 .00 .00 4.10 2.00 1.00 1.00 1.00	HISC 	ALFIN ALFIN -30 -00 -00 -00 -00 -00 -00 -00	TOTAL DOWN HOURS 1.00 5.00 2.00 1.00 8.00 17.00 2.00	KEL. I .00 .00 1.00 1.00 1.00 1.00 1.00	II -00 .00 .00 1.00 1.00 I.00 I.00 I.00 1.00	111 11 00 00 00 00 00 00 00 00 00	THE 1 IV 1.00 1.20 1.20 0.00 0.00	V I -00 1 -00 -00 -00 -00 -00 -00	1 v 1 v 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	VII 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	VIII -00 -00 -00 -00 -00 -00 -00 -00 -00	.00 .00 .00 .00 .00 .00 .00 .00 .00
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CONTRACT CONTRACT CONTRACT STATION 41 STATION 41 START 1211-25 1210-40 1210-25 1224-43 1223-24 1222-50 1221-12 1219-79 1218-63 1217-23 1215-54 1214-60	NUMBER TONNELS r, CALIF RATE F1738 65.00 110.00 110.00 133.00 140.00 130.00 130.00 140.00 39.00 94.00	TP AN SI T 1R0053 C4 N1A FEE T TC LATT 1459.00 1474.00 1474.00 1598.00 1672.00 1672.00 1672.00 2659.00 2199.00 2329.00 2368.00 2462.00	PROC HRS 1N WEEX 119.CO 12C.CO 12C.CO 115.CO 115.CO 112.CO 112.CO 112.CO 117.CO 116.CO	JH1ELG - J0 - J0 - J0 - J0 - J0 - J0 - J0 - J0	EXCAY EXCAY EQUIP .00 .00 .00 .00 .00 .00 .00 .00 .00 .0	000 000 000 000 000 000 000 000 000 00	PROGRE HOURS/LAUSE 1.405 1.405 1.405 1.405 1.405 2.405 1.400 1.60 2.00 1.60 2.00 7.60 51.60 1.00 4.00	WEEK HISC -00 -00 -00 -00 -00 -00 -00 -00 -00 -0	00. 00. 00. 00. 00. 00. 00. 00. 00. 00.	TOTAL UONN HOURS 1.00 5.00 2.00 1.00 8.00 17.00 2.00 6.00 51.00 3.00 3.00	FEL. I - 00 - 00 - 00 1 - 00 1 - 00 1 - 00 - 00 - 00 - 00 - 00 - 00	II .00 .00 .00 1.00 1.00 1.00 I.00 I.00 I.00 I.00 .00 .00	00. 00. 00. 00. 00. 00. 00. 00. 00. 00.	IV IV I.000 I.000 .000 .000 .000 .000 .0	V 1.00 1.00 1.00 .00 .00 .00 .00	1 v 00. 00. 00. 00. 00. 01. 00. 00. 00. 00.	VII 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	000. 000. 000. 000. 000. 000. 000. 000	4 ATÈR• - ∩0 - ∩0 - 00 -
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CONTRACT CONTRACT CONTRACT STATION AT STATION AT STATE 1211-25 1210.40 1210.25 1224.43 1223.24 1222.50 1221.12 1219.79 1218.63 1215.93 1215.54 1213.76 1213.76 1211.76 1211.76	NUREER INTELS (, CALIF(RATE F1748 6 65.00 1 15.00 1 10.00 1 00.00 1 0	CUMUL. FEET TC LATC LATC 1459.00 1474.00 1598.00 1672.00 1672.00 1816.00 2659.00 2199.00 2329.00 2368.00 2462.00 2546.00 2650.00 2746.00 2810.00	PROC HBS IN WEEX 119.CO 12C.CO 12C.CO 12C.CO 115.CO 115.CO 112.CO 112.CO 112.CO 112.CO 112.CO 117.CO 116.CO 120.00 77.00 116.CO		CGLAN EXCAV EQUIP -000 -000 -000 -000 -000 -000 -000 -0	C CUVE YOR C CUVE YOR C CUVE YOR C CUVE YOR C CO C CO C CO C CO C CO C CO C CO C	PROGRE HOURS/LAUSE LAUSE TRANS 1.00 .00 4.10 2.00 1.00 4.10 2.00 1.00 5.1.00 1.00 4.00 .00 .00	WEEK HISC .00 .00 .00 .00 .00 .00 .00 .00 1.00 .00	000 0000 000 000 000 000 000 000 000 00	TOTAL ONN HOURS HOURS 1.00 .00 5.00 2.00 1.00 8.00 17.00 2.00 51.00 3.00 1.00 4.00 1.00 4.00 1.00 4.00 1.00 4.00 1.00 4.00 1.00 0.00 1.00 0.0	FEL 	11 00 00 00 00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 0.00 .00	111 00. 00. 00. 00. 00. 00. 00. 00. 00.	IV IV I.00 I.00 I.00 .00 .00 .00 .00 I.00 I	V V V 1.00 1.00 .00 .00 .00 .00 .00 .00 .00	1 v 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	VII 1.00 1	 VIII 00 	4 ATÉR 0 - 00 -

EAY AREA RAPIO TRANSIT OISTRICT CONTRACT NUMBER ISOCII TR TUNNEL SAN FRANCISCO, CALIFORNIA

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STATION AT START CF WEEM	TUNNEL RATE FT/wK	CUMUL. FEET TO CATE	HRS 1N WEEF	SHIELO	E XCAV EQU1P	CUNVE YOR	MUCK TRANS	M1 SC	AUMIN	TOTAL DOWN HOURS	1	11	111		v				RUNNIN
6286.52	47.43	47.43	63.08	.50	.00		.50	.00	.00	1.00		1.00	.00		.00			.50	.50
8333.95	147.30	194.73	114.84	• JO	-00		1.75	1.83	- 00	3.58	.00	1.00	.00	. 00	.00	.co	1.00	.00	•00
8481.45	167.34	362.07	112.76	1.15	1.25	.50	.50	.00	.00	3.46	• 00	1.00	•00	.00	. CO	.00	1.00	.00	•13
6648.79	204.78	566.85	115.59	1.32	1.50	.67	.00	• 2 5	.00	3.74	• 60	1.00	•00	.00	• CO	•00	• 90	•00	•29
8853.57	129.89	696.74	99.44	8.93	5.56	• 2 5	• 42	3.38	•00	18.56	.00	1.00	.00	.00	.00	• CO	• 00	1.00	•33
6983.48	192.22	888.96	99.37	5.59	8.67	1.42	.25	.50	.00	16.43	•00	1.00	• U C	.30	•00	•00	.40	.60	.00
9175.76	227.27	1116.23	102.36	.50	2 • 2 9	1 - 2 5	8 • 67	.30	•00	12.92	• 00	1.00	.00	.00	• 00	• 00	1.00	.00	•00
\$462.97	237.15	1353.38	168.40	•00	6.59	75	2.02	.83	.00	10.19	•60	1.00	•00	• 00	.00	. 0 0	1.00	.00	.00
9640-12	109.83	1463.21	118.66	• JO	•00	.00	.00	•00	.00	.00	.00	1.00	•00	.00	• 00	.00	. 45	• 5 5	•10
9749 •95	52.28	1515.49	97.62	7.41	3.17	.00	•00	4.67	.00	15.25	• oò	1.00	.00	.00	.00	.00	.00	1.00	•00
9802.23	34.99	1550.48	103.95	1.17	•00	•00	• 00	•00	. 30	1.17	.00	1.00	+00	•00	•00	•00	•00	1.00	.00

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FAY AREA KAPIO TRANSIT DISTRICT Contract Number 150611 TL TUNNEL San Francisco, California

					HOURS - 8 Y C	AUSE						FPE 00	THE W	EEK				
STATION TUNNE AT START RATE CF DEEK FT/J	FLET TO	HRS IN BEEK	SHIELO	EOUIP	CONVEYOR	TRAN5		AUMIN	TO TAL DOWN HOURS	1	11	111		۷				RUNN 1NG
48264.02 44.	16 44.76	97.85	د		.00	1.40	3.00	.00	4.40								.80	
48230.03 92.5	9 137.34	112.67	4 + 6 7	•00	.00	• 60	2.16	.00	6.83	•00	1.00	.00	.00	. 34	•C0	•60		.00
48421.36 172.2	7 309.61	114.59	.io	.00	• 10	1.91	.00	.00	1.91	.00	1.00	.00	.00	.35	.00	1.00	•00	.00
48593.63 159.8	2 469.43	93.00	•00	• 5 6	.50	.00	.00	.00	1.00	+ OC	1.00	.00	. 30	.00	.00	1.00	.00	.00
46753.45 159.8	8 629.31	93.58	1.25	.00	.50	• 00	•00	.00	1.75	• 00	1.00	.00	.00	• 60	.ro	• 90	•10	•10
48913.33 197.	826+68	111.70	• 38	Z.25	3.42	.83	.00	.00	6.88	.00	1.00	-00	•00	•00	• CO	•90	• 02	.08
49113.19 227.3	6 1054.04	102.59	2.42	• 5 G	4.33	7.66	• 00	• 0 0	14.91	.00	1.00	.00	.30	•00	•00	1.00	.00	•00
49340.55 227.2	7 1281.41	105.10	3.16	5.43	2.16	2.27	. 38	.00	13.40	.00	1.00	•00	• 20	• 00	•00	. 80	.10	.\$0
49567.92 169.9	5 1451.36	92.24	5.55	2.5C	2.25	13.67	2.09	.00	26.06	.60	1.00	•00	• 00	.00	•00	.60	+13	+50
49737.87 64.9	3 1516.29	116.50	• JO	.00	.00	• 00	1.00	.00	1.00	•00	ī.oc	.00	.00	~,00°	.00	00	1.00	-15
49802.80 35.0	0 1551.29	75.66	0ئ.	.00	.00	• 00	2.92	.00	2.92	- 00	1.00	•00	•00	•00	•00	•00	1.00	•0Ű

PROCRESS AND PRODUCTION

PROCRESS AND PRODUCTION

(AY ARFA RAPIO TRANSIT DISTRICT CONTRACT NUMMER ISCOII SR TUNKEL SAN FRANCISCO, CALIFORMIA

						. У 900Ни С ¥ 0	CAUSE	WEEK			PEL.			THE W		DIL T	YPE 0	URING	
STATION #1 START CF wEEK	TUNNEL RATE FT/WK	CUMUL. FEET TO DATE		SHIELO	EXCAV EQUIP	CONVEYOR	TRANS		ADMIN	TOTAL DOWN Heurs	I	11	111	IV	v	٧ï	VI1	VIII	PUNN1NG WATER#
46284.00	42+51)	42.50	55.42	.33	•00	.co	20.00	1.50	.00	21.83	.00	1.00	•00	• 00	• 5 C	.00	1.00	•00	•00
48328.87	122.63	165.10	112.08	.ບໍລິ	.00	•00	3.17	2.91	۰۵۵	6.38	•00	1.00	•00	• 0C •	.50	•00	.70	•20	.31
48451.47	47.53	212.63	44.24	.33	•00	.00	.59	.67	.30	1.59	•00	1.00	•00	• C C	.50	•00	1.00	.00	.12
48499.00	112.40	325.03	84-,83	•00	2.67	.50	6.33	.67	.00	10.17	.00	I.CC	•00	.00	• 50	00.	•70	.20	.00
48611.40	164.88	489.91	113.08	.75	.00	.50	4 - 42	•00	•0n	5 + 6 7	•00	1.00	•00	. 00	.60	.GO	.70	•10	• C O
4677 6. 28	164.84	654.75	106.01	1.75	4.50	.00	I.94	1.08	.00	9.27	.00	1.00	•00	.00	•40	٥٦،	.30	.70	.00
46541.12	184.57	839.32	100.83	2.58	5.50	.00	5.92	• 00	. OC	14.00	.00	1.00	•00	. O C	•5C	• 00	• 5 0	.70	.00
49125.69	192.29	1031.61	91.23	1.ċ3	•00	• C O	26.36	• 00	.00	28.69	.00	1.00	.00	. 10	.60	0٩.	1.00	.00	.00
49317.98	204.73	1236.34	117.00	• 4 2	• C D	•00	۰00	•00	• O C	.42	• 00	I.00	+00	+00	•48	•00	•96	•00	•00
49522.71	179.41	1415.75	95.42	•00	•00	.00	.00	.00	.00	.00	.00	I.00	۰00	.00	•50	.00	1.00	.00	.00
49702.12	137.19	1552.94	84.C8	• 50	•00	.00	.25	12.25	.00	12.50	• CO	1.00	•00	•00	.60	٥٩.	1.00	۰00	+00

 PEY FOR SOIL TYPES
 *KEY TO VALUES FOR RUNNING WATER

 I - SILT AND CLAY
 Y - CEMENTED GROUND

 II - CLAY AND SAND
 VI - PEAT AND TRASH

 D = DRY
 *75 = RUNNING WATER

 II - SLAMD AND GRAVEL
 VII - COMESIVE GROUND

 IV - COBBLES AND BCULDERS
 VIII - FUNNING GROUND

EAY AREA RAPID TRANSIT GISTRICT CCNTRACT NUMBER ISODII SL TUNNEL SAN FRANCISCO, CALIFORNIA

						HOURS - By C	AUSE				-		FREQU	THE W	EEN					
AT STAPT	FIZAK	LAIT	HRS IN WEEK	SHIELO	EXCAV EQU1P	CONVEYOR	MUCK TRANS	MISC	ADMIN	TOTAL LOWN HOURS	1	11	111		v				UNNING SATER*	
		=======================================		=======						=======	22223									
48277.05	29.93	29.93	109.33	•u0	•00	.00	.10	.00	00 و	.00	• 80	1.00	0 0 •	•00	.00	•00	I.00	.00	•00	
48306.98	79.66	109.53	116.16	•>0	•00	+ 0.0	• 00	• 00	.00	•50	04.	1.000	• E G	. 90	•00	° 70	•00	1.00	• C O	
45366.64	99.92	209.45	112.17	.JO	1.00	.50	1.50	1 • 2 5	2.5P	6.75	• 00	1.00	•00	٥Ο،	.00	.00	.00	I.00	.50	
48486.56	117.50	326.95	112.42	• 30	•00	•75	• 00	•50	2.25	3.50	.00	1.00	•00	•00	•00	.00	• O C	1.00	.50	
46604+06	59.98	386.93	57.67	.00	.00	2.50	۰00	5.50	.00	8.00	•00	1.00	۰00	.00	۰۵۵	.00	•00	1.00	•00	
46664.04	138.90	525 + 83	108.50	1 • 25	•50	6.75	.00	.25	10.	8.75	• 00	1.00	۰00	•00	•00	• 00	.00	I • 0C	.00	
46862.94	113.40	639.23	81.17	1.58	4+50	3.33	• 00	•00	.00	9.4I	•00	1.00	.00	.00	•00	•00	1.00	٥٥.	.00	
46516.34	157.48	796°72	105.58	•50	•5C	2.00	2.00	.75	•00	5.75	. UD	1.00	.00	•00	•00	.00	1.00	.00	÷25	
49073.83	54.89	851.61	88.90	• 00	2.00	2.00	• 00	•00	۰00	4.00	.00	1.00	۰00	• 00	•00	•00	1.00	۰00	•00	
49128.72	129.64	981.25	92.08	2.10	19.83	2.16	.00	1 • 3 3	.00	25.42	• 00	1.00	۰00	.00	.00	• ÖÖ	1.00	•00	•00	-
49258.36	134.84	1116.09	98.42	.33	21.75	• 0 0	.LO	.00	.00	22.08	• 00	1.00	۰00	.00	•00	•CO	•00	1.00	۰00	
49393.20	179.65	1295.74	112.09	4.16	2 • 25	•00	• CO	.00	۰00	6.41	۰00	I.0C	.00	.00	•00	•00	1.00	•00	۰00	
۹9572 .85	162.12	1457.86	83.95	9.83	.50	1.50	16.56	• S C	.00	28.89	•00	1.00	۰00	۵0.	• 0 [`] 0	•00	1.00	.00	-•00 -	
49734.97	107.33	1565.19	74.83	• J D	.00	1.50	• 00	3.83	.00	5.33	•CO	1.00	۰00	•00	•00	.00	1.00	.00	۰00	

PROGRESS AND PRODUCTION

PROGRESS AND PRODUCTION

EAY AREA RAPIÙ TRANSIT Contract number isdoïia Sr tunnel - market sireet San Francisco, california

						NHOURS - By C	AUSE						FREQU	THE N	EEK	-		-	
STATION AT START CF WEEK	FT/ak	LATE	HES IN		EQUIP	CONVE YOR	T R AN S			TOTAL DOWN Hours		11	111	IV	v	٧I	V1 I	v1 I 1	RUNNING WATER*
		27.46			•00			.00				1.00	.00	•00	.4C	.00	.60	.38	.30
1332.06	67.50	94.96	110.25	1.25	.00	•00	3.25	3.00	• 20	7.5C	•60	1.00	•00	. 90	.00	.co	• 50	•40	.70
51262.08	42.50	137.46	52.34	7.83	.00	.00	•00	2.50	•00	10.33	•00	1.10	•00	•00	.00	•00	•20	•20	•75
£1219.58	52.78	190-24	74.67	2.00	.00	.00	• 33	• 90	.00	2.33	• 60	1.00	•00	.00	1.00	.00	1.00	•00	.34
51166 .8 L	87.22	277.46	106.69	4.24	•00	• 0 0	3.50	1.08	•33	9.15	.00	1.00		.00	.00	.00	•30	+90	•32
51079.58	107.50	384.96	100-64	8.99	.00	1.67	2.95	2.42	1.25	17.28	• u0	1.00	.00	.00	• 30	•00	•50	• 30	.34
50972.06	92.50	477.46	76.25	. 83	•00	•00	1.83	2.75	•00	5.41	•C0	1.00	.00	•0C	•Sa	•00	1.00	.00	•20
50879.58	97.50	564.96	73.26	.92	.00	.00	2.17	4.25	•00	7.34	• 00	I.00	•00	•90	1.00	•00	1.00	.00	.00
50792.08	122.50	687.46	5•52ء	.00	.00	1.33	2.25	5.58	.00	9.16	• CO	I.00	•00	•00	• 30	•00	•70	•00	•20
50669.58	22.50	709.96	37.75	• 30	•00	•00	. 00	11.75	•90	11.75	•60	1.00	•00	•00	•5Ō	• 00	.70	.00	10 -

KEY FOR SOLL TYPES		*KEY TO VALUES FOR RUNNING WATER
1 - SILT AND DEAY	V - CEMENTED GROUND	
II - CLAY AND SAND	VI - PEAT AND TRASH	C = DRY .75 = RUNNING WATER
1II - SANC AND GRAVEL	VII - COHESIVE GROUND	.25 = MOIST I = FLOODED
IV - COBBLES AND BOULDERS	VIII - RUNNING CROUND	.50 = WET

PROCPESS AND PRODUCTION

TAY AREA RAPID TRANSIT DISTRICT CONTRACT NUMBER ISOD'IA IL TUNNEL - MARKET STREET IAN FRANCISCO, CALIFORNIA

DOWNHOURS - HOURS/WEFK RELATIVE FPEOUENCY OF SCIL TYPE OURING PY CAUSE STATION TUNNEL CUMUL. PEOC AT START RATE FEFT TC HRS IN SHIELD EXCAV CONVEYOR MUCK MISC ADMIN TOWN 1 11 111 1V V VI VII VIII RUNNING CF WEEK FIJWK LATE -EEM EQUIP TRANS HOURS HOURS 1342.00 52.42 85.00 112.36 1.00 .00 .00 2.17 1.00 .00 4.17 .00 1.00 .00 .00 .50 .00 .80 .10 .40 51269.58 67.50 I52.5C 94.C8 1.15 .C0 .00 16.38 .25 .0C 17.78 .00 1.00 .CO .00 .3C .CO .70 .20 .75 51222.08 67.50 220.00 96.44 6.80 .00 .00 7.25 3.09 .00 17.14 .00 1.00 .00 .00 .00 .00 .90 .10 .25 .00 2.50 .00 .00 3.58 .00 1.00 .C0 .0C .20 .00 1.00 .00 .20 51154.58 60.00 280.00 78.36 1.08 .00 \$1094.58 7C.00 350.00 79.50 1.00 .0C .00 1.08 .00 .0C 2.08 .C0 1.0C .00 .00 .00 .00 .00 .00 .15 .10 .00 2.25 1.75 .00 6.32 .00 1.00 .00 .00 .00 1.00 .00 .00 50917.08 107.50 564.70 110.10 2.32 .00 \$C809.58 125.00 689.70 103.49 3.58 .00 .00 4.68 3.22 .00 11.68 .00 I.00 .00 .00 .50 .00 1.00 .D0 .00 \$C664.56 40.00 729.70 49.46 .00 .00 .00 .75 6.26 .0C 7.0I .00 1.00 .00 .00 .50 .C0 I.00 .D0 •C0

3740.00 276.00 3625.00 37.00

4016.00 228.00 3853.00 31.00

4244.00 376.00 4229.00 45.00

4620.00 216.00 4445.00 22.00

4836.00 280.00 4725.00 34.00

5116.00 152.00 4877.00 23.50

5268.00 300.00 5177.00 37.00

5568.00 304.00 5481.00 37.00

5872.00 400.00 5881.00 45.00

6272.00 286.00 6167.00 33.50

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						HOURS - 84 C	AUSE							THE V	OF SC WEEK				
ACITATS	TUNNEL									TOTAL									
CF LEK	Fî∕aK	LATE	₩EE⊬		EwUIP	CONVEYOR	TEANS	5	ADMIN	DOWN HOURS	I	11	III	IV	۷	VI			WATER*
							======					====	= = = = = = =			= = = = = =	=====		======
432 °CC	24.00	24.00	25.50	0L •	• C C	8.00	. U D	* D C	00.	6 • 70	1.00	•30	•0C	• 33	• üD	.00	•00	1.00	1.00
456.00	14=00	36.00	16.00	0	.00	4.00	• 60	24.00	. JC	28+00	I • 00	.0J	• C O	• D U	•00	•03•	•00	1.00	1.00
470.00	92.00	130+00	44.00	•ũD	6.00	• O O	• CO	•00	.00	6.00	1.UO	.00	•00	•00	۰UD	•00	•00	•75	1.00
562.0	66.00	210.00	25.LU	Oi.	4.55	- 0 D	- 00	20.00	00 ه	24.00	I.00	• O D	.00	1.00	.00	.00	1.00	•00	•00
642.00	4.00	214.00	3 °C D	• JO	5.00	- C D	•00	.00	.00	5.00	1.00	+00	•00	1.0.0	- OC	00•	1.00	٥0 ه	۰00
646.00	26.00	242.00	14.00	₀JC	32.00	4=00	• OQ	-00	- O O	36.00	1.00	۰۰۵	.00	1.00	۰00	•-C 0	•00	1.00	-00
674.00	23=00	265.00	16 •CO	•30	4.00	.00	.00	. U D	• 00	4.00	1.00	•06	•00	۰۵0	•00	•00	1.00	.00	۰00
657.CC	19.00	284.0C	10.00	.00	.00	•00	• 00	6.00	•00	8.00	1.00	.00	.00	-00	۰00	۰00	1 • 0 0	۰00	.00
714.00	74.00	358.00	30.00	•00	4.00	16.00	• 60	.uD	.00	20.00	1.00	•30	•00	. 4 L	۰۵۵	.00	1.00	.00	•C0
788.CC	52.00	410.00	18.00	• J D	6.00	15.00	• 60	•00	.00	21.00	1.00	•00	• O C	1.00	۰00	.00	1.00	•00	.00
840.00	160.00	590.0C	40.CO	• UD	•00	8.00	.00	.00	•00	6.00	1.00	.36	.00	1.00	.00	.00	1.00	•00	۰00
1020.00	116.00	706-00	25.50	.00	16.00	10.50	.00	2.50	.00	23.00	1.00	.00	• C O	1.06	۰00	•00	1.00	۰00	•00
1136.00	132.00	838.00	28.CD	.30	13.00	.00	•00	5.00	.00	18.00	1.00	.00	.00	1.00	.00	• CO	1.00	.20	°20
1229.00	256+00	1094.00	38.CO	•00	2.00	6.50	.00	3.50	•00	12.00	1.00	•0C	+00	•2í	-00	•00	- 80	.00	.00
1465.00			38.00	. 30	.00	.00	• 00	12.00	.00	12.00	.90	.10	.00	• 0.0	.00	.00	1.00	.00	.00
1753+00	104-00	1466-00	16.50	a.(D	17.00	5.50	.00	5.00	.00	27.50	.00	.20	-80	1.00	•00	.00	1.00	• 0 Ó	+00
1857.00		1510+00	12.00	.00	.00	6.50	•00		23.00	29.50			1.00		.00	•00	.00	•00	.00
1961.00		1530+00	12.00	.00	.00	4.00	• 00	- 00	-00	4.00			1.00	.00	•00	.00		1.00	*00
1921.00		1586.00	41. <u>€</u> 0	•00	2.50	• 0 0	•U0	6.00	.00	8.50	÷ 00			•20	• 00	•00	• 00	•50	.00
1977.00		1668.00	33.00	0u+	8.00	•00	.00	5.00	•00	13.00	.00		1.00		• 00	.00	.00	.50	.00
FEY FOR 5	LT ANG C	CLAY				MENTED GI				EY TO N				ING #A					
11 - CL/ 111 - SAP	ND AND D	GRAVEL		V 1	11 - CO	AT AND TH HESIVE OF	OUND) = OR1 25 = HOI	Y IST	.75 1	= RUM = FLC		WATER				
IA - CO8	BULES AN	ND BOULDE	RS	VII	11 - RU	NNING GRI	0 0 0 0		- 5	50 = w£1	T								
						F	ROGRE	SS AN	D PRODU	CTION									
LPPER SAL CONTRACT CHICAJO,	NUMBER	68-404-2	S																
						HOURS - P By C/	USE					,		THE W	OF SO				
STATION AT START	TUNNEL		PROD			CONVEYOR			ADMIN	TO TAL Lown	I	11	111	IV	v				UNNING
	FTZWK	LATE	⊌EE M		EQUIP		TR ANS			HOURS	-								WATER*
2659.00			 38.5J		.00	5.50	.00	6.00		11.50	.00		1.60		.00	•00	.70	.00	.00
									00.00										
2213.00			37.00	0U+	•00	• C O	• 00		10.00	13.00	.50	•20	.50	•2ú	- 00		1.00	.00	•00
2393.00		2075.00	34.00	1.30	.00	.00		11.00	2 • 00	14.00	-80	.00		1.00	°00	.00	.00	.50	•00
2466.00			41 •CO	4.00	• U D	2.00	• 00	1.00	.00	7.00	- 4 🛛	•10	•6 D	•10	.00	,00	•00	.50	.00
2630.00		2274.00	19.00	22°00	3.00	• C O	• 00	•00	.00	25.00	.40	·10	۰6 D	.16	.00	.00	+00	• 50	•00
2665.00		2338=00	23.00	* 70	۰۵۵	• D O	.00	2.00	19.00	21.00	1.00	•90	•00	• 00	.00	۰00	•00	1.00	°C 0
2729.90	175.00	2513.00	31.00	6.00	6+00	- 0 0	-00	2.00	•00	16=00	1.00	00ء	•00	.00	•00	۰00	•00	1.00	.00
2904.00	320.00	2833.00	45.CO	• 90	• C O	.00	•00.	5.00	•00	5.00	1.00	۰O0	•4 J	•4Û	03.	• 00	.50	.00	.00
3224.00	208.00	3 C4 1 . 0 C	25.00	. D.D	6.00	•00	•00	5.00	•00	11.00	1.00	.00	•00	1.00	•00	۰00	1.00	° 00	00.
3432 = 00	308-00	3349.00	39.00	.00	.00	3.00	• 00	•00	8 • 0 Ū	11.00	ū8.	•00	•20	.00	.00	.00	1.00	00 -	.00

Appendix A-2. (Continued)

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.co 10.00 .uo 13.00 .90 .10 .00 1.00 .co .00 .00 1.00

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₀00 ₀20 ₀25 ₀00

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•70 •90 •00 •10 •00 •00

•L0 6+00 10+00 16+00 +80 +00 +20 +00 +00 +00 -50 +50

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•CO 1.00 4.00 .00 5.00 1.00 .00 .00 .00 .00 .00 1.00 .00

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LPPER SALT GREEK #1 CONTRACT NUMPEP 60-404-25 CHICAGC, ILLINOIS

						HOURS - 1 BY C	AUSE	WEEK			FEL A	3V L T		ENCY THE W		IL T	YPE 0	UR I NG	
STATION AT START CF LEEK	TUNNEL RATE FT/#K	CUMUL. FEET TO LATE	HRS IN WEEK		EOUIP	CONVEYOR	TRANS		ADMIN	TOTAL COWN HOURS	I	11	111	•	v				RUNNING WATER*
6558.00	178.00	6345.CC		 J		.00		19.00		19.00				.00	-				
6736 .DC	100.00	6445.DC	30.00	•00	3.00	•00	• 60	12.00	5.00	20.00	•00	•00	1.00	.00	• GO	.00	• 00	1.00	•60
6836.00	46+00	6493.00	25+00	3+J0	7.00	•00	• OG	13.00	.00	23.00	•00	.00	1.00	.00	•00	•CO	•00	1.00	•60
6864 .DU	26.00	6519.UC	17.00	•00	12.60	.00	•00	7.00	8.00	27.00	•00	.00	1.00	•20	•00	•00	•00	1.00	•00
6910.00	46.00	6565.00	26.00	٥د.	•00	12.00	•00	8.00	•00	20.00	•00	•00	1.00	. OL	.00	.co	•00	1.00	+00
6956.00	98.00	6 66 3 • 00	33.00	• 39	•00	3.00	.00	4.00	8.00	15.00	• 00	•00	1.00	•00	•00	•00	•00	1.00	•00
7054 .00	162.00	6825.00	36.00	.00	•00	۵0.	• 00	12.00	•00	12.06	•00	•00	1.00	.00	.00	•00	• 00	1.00	•00
7216.00	246.00	7073.00	44.CO	•00	•00	•00	.00	6.00	•00	6.00	۰Ö0	• 00	1.00	•00	•00	.00	1.00	•00	•00

FEY FOR SOIL TYPES		*KEY TO VALUES FOR RUNNING WATER
I - SILT AND CLAY	V - CEMENTED GROUND	
II - CLAY AND SAND	VI - PEAT AND TRAS!.	O = ORY .75 = RUNNING WATER
III - SAND AND GRAVEL	VII - COMESIVE GROUND	.25 = MOIST 1 = FLOODED
IV - COBBLES AND BOULDERS	VIII - RUNNING GROUND	+50 = WET

PROGRESS AND PRODUCTION

LPPER SALT CREEK #2 CONTRACT NUMBER 66-405-25 CHICAGO, ILLINOIS

						HOURS -		/WEEK		-				UFNCY The W	EEK				
STATION AT START CF WEER	TUNNEL RATE FT/#K	CUMUL. FEET TO LATE		SHIELO	EXCAV	CONVEYOR	HUCK TRANS		AUMIN	TOTAL LOWN FOURS	I	11	111		v	۷I	VII	VIII	RUNNING WATER+
75.00	46+00	46.00	40.00	•00	.00	.00	.00	•00	.00	•00	1.00		•00	• 20	•00		1.00		.00
27.00	23.00	69.00	17.00	• JC •	.00	•00	•00	•00	• 30	.00	1.00	.00	.00	.00	.00	.00	1.00	•00	•00
75+00	103.00	172.00	30.60	0L.	.00	B.00	• 00	8.UO	•00	16.00	1.00	•00	•00	•00	.00	.00	1.00	•00	•00
173.00	213.00	385.00	41.00	•ú0	5+00	.00	• 60	.00	•00	5.00	1.00	.00	•00	• 90	•00	.00	1.06	•00	•00
751.DU	578.00	963.00	55.60	• u D	6.00	•00	• 00	2.00	•00	8.00	1•GO	•00	•00	.2ü	.00	.00	1.00	• 00	•00
969 .O O	159.30	1122.00	14.00	- 00	6.00	• 9 0	.00	18.00	.00	26.90	1.00	•0C	•00	•00	•00	•00	1.00	.00	.00
1129.00	549.00	1671.00	41.CO	•00	•00	.00	• 00	26.00	•00	26.00	1.00	1.00	1.00	1.00	•00	•00	1.00	• 00	•50
1665.00	218.00	1689.00	16.00	• JO	•00	.00	• 00	9.50	18.50	28.00	1.00	.00	•50	.50	•00	•00	1.00	.00	.00
1963.00	495.00	2 384 - 00	36.00	•00	.00	•00	•00	6.00	11.00	17.00	1.00	•00	•00	.10	•00	•00	1.00	.00	
2466.00	622.00	3006.00	51.00	.00	.00	.00	• 00	9.00	.00	9.00	.00	1.00	.10	•20	.00	.00	1.00	•00	•00
3028.00	104.00	3110.00	5.00	.00	13.00	•00	•00	•00	.00	I3.00	• 00	•50	•00	.00	•00	•00	1.00	.00	.00
3132.00	576.00	3660.00	39.00	0 د •	•00	•00	0، •	5.00	• 00	5.00	• 00	•50	.00	.00	•60	•00	1.00	.00	•Ó0
3710-00	411.00	≈091.00	31.00	.00	• 00	•00	.00	10.00	T.00	17.00	1 • 00	•00	•00	• 30	•00	.00	1.00	.00	.00
4129.00	513.00	4604.00	35.00	•UD	•00	•00	•00	8.00	.00	8.00	1.00	•00	.00	•00	•00	•00	1.00	۰ 0 0	•00
4650∘00	368.00	4972.00	25.00	•00	.00	.00	.00	8.00	7.00	15.00	1.00	•00	•00	•70	•00	.00	.00	.00	•00
5303.00	341.00	5 31 3 • 00	24.00	•u0	•00	.00	• CO	10.00	.00	10.00	1.00	.00	•00	~ 00	.00	•00	• 00	•00	•80

UPPER SALT CPEEK #3 Contract number 68-406-25 CH1CAGO, 1LLIND15

				DOW	NHDURS - 8y c		WEEK			REL	T1VE	FRED	UENCY The W		ILT	YPE O	UR 1 NG	
										= = = =	======	====	======		====		=====	
AT STATION TU AT START R OF WEEK FT	ATE FEET T		SHIELO	EXCAV Equip	CONVEYOR	MUCK		AOMIN	TOTAL ODWN HOURS	I	11	111	1 V	٧	۷1	V11	VIII	RUNN1NG WATER*
														=====	=====			
4681.00 20	0.00 20.0	0 10.00	•00	6.00	•00	•00	24.00	*00	30.00	1.00	•00	•00	۰00	۰00	•00	1.00	۰00	.00
4701.00 84	+.00 104.0	0 28.00	•00	•00	8 • 0 0	٥٥ .	3.00	1.00	12.00	1.00	•00	.00	1.00	•00	•00	1.00	۰00	.00
4785.00 164	+.00 268.0	0 30.00	•00	2.00	.00	• 00	8.00	.00	10.00	1.00	.00	•00	۰50	۰00	+00	•00	•00	•00
4949.00 120	0.00 388.0	23.00	.00	15.00	.00	•00	2.00	•00	17.00	1.00	۰00	•00	1.00	۰00	•00	1.00	۰00	۰۵۵
5069.00 130	8.00 526.0	31.00	.00	•00	•00	•00	9.00	•00	9.00	1.00	٥٥.	•00	1.00	•00	•00	1.00	•00	•00
5207.00 15	2.00 678.0	22.00	•00	•00	•00	•60	1.00	.00	1.00	1.00	.00	.00	.40	•00	•00	1.00	•00	•00
5359.00 164	.00 842.0	31.00	•00	•00	.00	.00	1.00	8.00	9.00	1.00	.00	•00	•20	•00	•00	•00	•00	•00
5523.00 268	8.00 1110.0	36.00	*00	•00	• 00	• 00	3 • 00	1.00	4 • 0 0	1.00	•00	•00	۰70	•00	•00	1.00	•00	•00
5791.00 120	0.00 1230.0	0 14.00	•00	•00	•00	•00	2.00	24.00	26.00	•20	1.00	.00	۰4O	•00	۰00	•00	•00	۰00
62.00 IO	7.00 1337.0	D 13.00	+00	•00	•00	• 00	27.00	.00	27.00	۰50	•00	•50	٥٥ ،	۰00	.00	.00	.00	.00
169.00 80	0.00 I417.0	17.00	•00	7.00	16.00	•00	•00	•00	23.00	. 90	۰00	•10	۰00	۰00	•00	1.00	•00	•00
249.00 164	.00 1581.0	30.50	.00	•00	5.50	•00	4 • 00	۰00	9.50	1.00	٥0.	.00	.00	•00	•00	1.00	•00	۰00
413.00 200	0.00 1781.0	29.00	•00	•00	•00	•00	8.00	.00	8.00	1.00	٥٥.	۰00	۰00	÷00	٥٥٥	1.00	.00	۰۵۰
613.00 III	2.00 1893.0	D 20.00	•00	•00	4 +00	•00	2.00	6.00	12.00	I.00	.00	•00	•00	•00	•00	1.00	•00	۰00
725.00 260	0.00 2153.0	29.00	•00	•00	•00	•00	3.00	•00	3.00	1.00	00 ه	•00	٥0 ه	۰00	۰00	1.00	•00	•00
985.00 324	.00 2477.0	40.00	۰00	•00	•00	.00	.00	.00	•00	1.00	۰00	۰00	•00	•00	•00	1.00	.00	•00
1309.00 252	2.00 2729.0	27.00	•00	•00	.00	۰00	5.00	8.00	13.00	1.00	۰00	•00	۰00	•00	.00	1.00	•00	۰00
1561.00 300	0.00 3029.0	34.50	۰00	۰00	•00	• 0 0	5.50	.00	5.50	1.00	•00	•20	۰00	.00	.00	.80	.00	۰00
1861.00 280	.00 3309.0	31.00	۰00	.00	1.00	۰00	.00	8.00	9.00	1.00	۰00	•16	•00	•00	•00	.96	•00	+00
2141.00 376	•00 3685•0	38.00	+00	1.00	1.00	.00	۰00	۰00	2.00	1.00	.00	•00	۰00	•00	•00	1.00	۰00	۰00
KEY FOR SDIL I - SILT / II - CLAY / III - SANO / IV - COPBLE	NO CLAY NO SAND NO GRAVEL	DERS	v tv	/I - PE II - CO	EMENTED G EAT AND TI DHESIVE G UNNING GR	R A S H ROUND		0 • 2	EY TO = OR 5 = MOI 50 = WEI	r I S T	.75		NING					

PROGRESS AND PRODUCTION

UPPER_SALT_CREEK #3 CONTRACT_NUMBER_68-406-25 CHICAGO, ILLINOIS

					0081	HOURS - 87 C		WEEK			REL/	T1VE	FREQU	ENCY THE W		IL T	YPE O	UR1NG	
				======	=======		======	=====:			====	=====		=====	=====	= = = = :	= = = = = =	=====	:
STATION	TUNNEL	CUMUL.	PRDO							TOTAL									
AT START				SHIELO		CONVEYOR			AOMIN	DOMN	1	11	I 1 I	1 V	٧	ΥI	AII	VIII	RUNNING
OF WEEK	FT/WK	DATE	WEEK		EQUIP		TRANS			HOURS									WATER*
								=====											
2517 00	212 00	3897.00	20.00	.00	.00	3.00	• 00		12 00	16.00	1 00	0.0	.00	0.0	0.0	00	1 00	. 00	.00
2517.00	212.00	3697.00	24.00	•00	•00	3 • 00	•00	۰UU	12.00	10.00	1.00	.00	.00	.00	.00	.00	1.00		
2729.00	400-00	4297.00	37.00	.00	.00	3.00	.00	.00	.00	3.00	I.00	.00	.00	.00	• 00	.00	1.00	.00	.00
3129.00	288.00	4585.00	38.50	•00	۰00	.00	.00	1.50	.00	1.50	1.00	.00	.00	.00	.00	.00	1.00	.00	.00
3417.00	141.00	4726.00	24.00	•00	۰00	•00	.00	۰00	16.00	16.00	1.00	۰00	•00	•00	-00	•00	1.00	٥٥ .	•00
3558.00	80.00	4806.00	15.00	4.00	٥0.	•00	• 00	5.00	16.00	25.00	• 50	•20	•00	۰00	•00	•00	1.00	.00	•00
																			•00
36.38.00	168.00	4974.00	32.00	00 ه	•00	•00	•00	8.00	•00	8.00	1.00	s 50	•00	•00	• 00	• UU	1.00	• 0 0	•00
3804.00	292.00	5266.00	37.00	.00	.00	.00		3.00	.00	3.00	1.00	. 00	.00	- 00	. 00	-00	1.00	.00	.00
5000.00	2 /2 000	3200+00	57.00		*00	.00	-00	3:00	-00	0.00	1.00								100
4098-00	316.00	5582.00	36.50	.00	.00	.00	- 00	3.50	- 00	3,50	1.00	.00	.00	.00	+00	•00	1.00	.00	.00
						500		2330		2000									
4414.00	256.00	5838.00	31.00	۰00	.00	۹.00	.00	5.00	.00	9.00	1.00	.15	.15	.00	• 00	.00	1.00	.00	•00

PROGRESS AND PRODUCTION

SASHINGTON METROPOLITAN AREA TRANSIT AUTHORITY Compact Number 10021 Framertagon outboung Sashington, D.C.

						140005 - 1 Ry C		WEFK						THE W					
STATION /T STAPT CF SEEM		CUMUL. FEET TO GATE	HRS IN WEEF	SHIELD	EXCAV EQUIP	CONVE YOR	TRANS			TOTAL DOWN HOURS	1	11	111	1 V	v	¥1	V11	V111	RUNNING WATER+
7050.57	67.02	67.OC	76.49	•60	.00	.00	. 33	9.68	•00	10.01	1.00	1.00	•00	•00	•00	•00	1.00	•00	•00
6963.57	46.19	113.19	27.28	• 50	3.00	.70	•00	2.52	•00	6.72	1.00	1.00	•00	•00	•00	•00	1.00	.00	•00
6927.38	174.89	288.08	83.68	.58	•26	2.42	1.42	3.57	• 2 5	8.82	•00	1.00	.00	•00	•00	•00	.00	.00	.00
6762.49	51.42	339.50	21.65	•90	.00	•00	•25	5.10	.00	5.35	•C0	.00	1.00	1.00	.00	.00	•00	1.00	1.00
6711.07	213.94	553.44	69.83	1.50	.75	.00	•25	1.17	•30	3.67	1.00	•00	1.00	1.00	.00	.co	1.00	•00	.00
6497.13	54.37	607+81	23.34	•30	•00	• 3 3	1.00	1.50	•25	3.16	1.00	•00	1.00	1.00	.00	•00	1.00	1.00	.00
6442.76	2.47	616.28	7.25	•00	.00	• 2 5	•00	•00	.00	•25	1.00	1.00	•00	.90	.00	.no	1.00	1.00	+00
6440.79	91.74	702.02	37.15	4.00	.00	1.10	•00	6.00	•25	11.35	1.00	1.00	1.00	1.00	•00	•co	1.00	•00	.00
6348.55	133.57	835.57	77.55	3.20	3.00	.00	•00	10.75	•09	16.95	1.00	.00	1.00	1.00	•00	•00	1.00	1.00	•00
6214.98	261.95	1097.52	97.42	•00	•00	•20	1.00	9.08	•se	10.58	1.60	.00	1.00	1.00	•00	•00	1.00	.00	1.00
5953.03	293.27	1390.79	95.76	5.33	•25	.50	. 33	8.08	۰2۴	14.74	1.00	.00	1.00	1.00	•00	•00	1.00	•00	1.00
5659.76	17.47	1408.25	16.92	•00	•00	•00	.00	.33	.25	.58	1.00	•00	1.00	1.00	•00	•00	1.00	.00	•00

PROGRESS AND PRODUCTION

WASHINGTON METROPOLITAN AREA TRANSII AUTHORITY Contract Number IF0021 FZA PENIAGON INBOUND WASHINGTON, D.C.

DOWNHOURS - HOURS/WEEK RELATIVE FREDUENCY OF SOLL TYPE OURING 87 CAUSE THE WEEK 7141.90 7.50 7.50 9.50 .00 -00 - 00 .00 .00 .00 7134.40 6.80 19.30 8.28 .00 .22 1.00 .00 .00 .00 1.22 1.00 1.00 •00 .00 .00 .00 1.00 .00 .00 7127.60 29.96 39.26 38.11 .22 .67 • 0 **0** •00 .00 .00 .89 1.00 1.00 .00 .00 •00 .00 1.00 .0C • 00 2102-68 2.42 41.68 R.40 1.60 .00 - 00 .00 -00 .00 1.60 1.00 1.00 .00 .00 .00 .00 1.00 .00 1.00 7100.22 17.21 58.89 28.50 11.50 2.00 2.30 .00 9.00 .00 19.80 1.00 1.00 .00 • 00 .00 1.00 .00 .00 .00 7083.01 39.45 98.34 38.20 .00 .00 .00 .00 2.80 .00 2.80 1.00 1.00 .00 .00 -00 .00 1.00 .00 1.00 7043.56 61.96 160.30 38.00 .00 .00 .00 •00 4.50 .00 4.50 1.00 1.00 .00 .00 .00 .00 1.00 .06 1.00 6981-60 38-30 198-60 22.70 -00 1.90 . 00 .00 .90 .00 2.80 1.00 1.00 .00 .00 .00 .00 1.00 .00 1.00 6943.30 49.63 248.23 26.68 9.60 - 00 .00 .00 2.20 .00 6.80 1.00 1.00 .00 •00 +00 -00 1.00 .00 1.00 6893.67 41.07 ZRV.30 38.60 1.00 .00 1.00 .30 .10 .00 2.40 1.00 1.00 .00 .00 .00 .00 1.00 .00 1.00 6852-60 47.14 336.44 38.92 .75 .92 .00 .00 8.91 .00 6.5R 1.00 1.00 .00 .00 • 00 .00 1.00 .06 1.00 6805.46 146.66 483.10 79.95 2.75 .00 1.25 .00 16.80 .25 21.05 .00 1.00 .00 .00 .00 .00 .00 .00 1.00 6658.80 189.84 672.94 72.42 1.30 .00 .50 .53 1.75 .00 4.08 .00 1.00 1.00 .00 .00 .00 .00 .00 1.00 6468.96 167.03 839.97 72.05 5.70 1.00 \$.00 .00 5.25 .00 16.95 .00 1.00 1.00 1.00 .00 .00 .00 1.00 1.00 6301.93 69.22 909.19 44.55 -00 <u>_ nn</u> - 00 •00 4.75 .20 9.95 .00 1.00 1.00 1.00 .00 .00 .00 1.00 1.00 6232.71 104.07 1013.26 61.77 .00 .20 1.33 .00 8.20 - 00 9.73 1.00 1.00 1.00 1.00 .00 .00 1.00 1.00 1.00 6128.64 27.17 1040.43 17.50 .00 .00 .00 • 0 0 1.00 .00 1.00 1.00 .00 1.00 1.00 .00 .00 1.00 1.00 1.00 6101.47 2.51 1042.94 6.50 .00 .00 .50 .00 2.00 .00 6098.96 106.37 1149.31 63.03 1.80 .00 8.00 2.75 19.42 5992.59 170.31 1319.62 84.90 1.20 1.00 3.05 2.35 1.80 .20 KEY FOR SOIL TYPES 1 - SILT AND CLAY 11 - CLAY AND SAND 111 - SAND AND GRAVEL 117 - COBBLES AND BOULDERS WEY TO VALUES FOR RUNNING WATER V - CEMENTED GROUND VI - PEAT AND TRASH VII - COMESIVE GROUND III - RUNNING GROUND 0 = DRV •25 = H0157 •50 = WET -75 = RUNNING WATER 1 = FLODOED VIII

WASHINGTON METROPOLITAN AREA TRANSIT AUTHORITY CONTRACT NUMBER 1F0021 F2A PENTAGON INBOUND WASHINGTON, 0.CC.

	DDWNMOURS - HOURS/WEEK By Cause	RELATIVE FREQUENCY OF SOIL TYPE OURING THE WEEK
STATION TUNNEL CUMUL. PROD AT START RATE FEET TO HRS IN OF WEEK FT/WK DATE WEEK	SHIELO EXCAN CONVEYOR MUCK MISC ADMIN EQUIP TRANS	TOTAL OTAL TI III IA A AI AII AIII KUMMING Down I II III IA A AI AII AIII KUMMING Hours
583Z.28 191.52 IS11.14 89.40	≈••70 2•90 2•00 •50 •80 •20	1I.10 I.00 I.00 1.00 I.00 .00 .00 1.00 .00

PROGRESS AND PRODUCTION

PROGRESS AND PRODUCTION CONTRACT NUMBER IF0021 F2A BRANCH ROUTE GUIFOUND VACHINGTON, C.C.

		_=====		HOURS - J By C	USE							ENCY THE W	EEK				
CF .EEK FT/#K L	ET TC HRS 1 ATE DEEF		E UU1P	CONVEYOR	TRANS	_		TOTAL LOWN FOURS	1	11 ======	111		v =====				RUNN1NG 64 TER*
8665.69 69.89	69.89 54.08	۵۱۰۰۵	.00	.00	.60	1.92	.50	Z.42	• 20	•50	.30	•00	•00	• 00	•20	.00	.00
8535.86 136.63 Z	06.52 73.6	.20	5.50	2.83	1.42	9.08	•90	18.83	• 1 Ū	•5 0	.30	.10	.00	.00	.10	.00	.00
8399.17 27.32 2	33.04 33.08	∪ن. ا	.00	.4Z	- 17	.33	• 5 P	1.42	00 ه	.70	•20	-10	.00	00.	.00	•00	.00
8371.85 19.92 2	53.76 16.50	• -30	•00	•00	• CO	.00	.00	• 00	• 10	.70	• 2 O	.00	• C O	.00	•1C	۰00	•00
8351.93 202.84 4	56+60 62.00	1.50	.33	4.25	1 • 6 7	3.75	•5C	12.00	•00	.8C	•20	.00	.00	.00	•00	• 90	•00
6149.09 154.17 6	10-77 48-61	4.30	•00	.33	. ĻC	1.50	.00	5.83	.10	•60	•20	. CL	٥0 .	.10	÷10	• 00	.00
7994.92 265.54 8	76.31 87.42	.63	.00	1.00	• C O	4.00	•75	6.58	.00	.5C	.30	•1G	•00	.10	•00	•00	۰00
7729.38 178.93 10	55.24 66.47	2.53	•00	15.92	• GC	5.58	.00	24.03	۰00	.7C	-20	.10	.00	•00	.00	•00	.00
7550.45 311.93 13	67.17 96.CC	1.50	4.17	Z. C8	• 00	4.75	۰00	12.50	•00	.60	•3C	.19	•00	.00	•00	. OC	•00
7238.52 280.90 16	48.07 87.58	00	.75	• O C	• 41	•75	•5C	Z .41	0، •	02.	•30	• 2 C	. Ö.Ö	• CO	• O O	•00	•00
6924.85 269.76 19	17.83 62.2	, .75	۰00	3.50	1.33	.17	.00	5.75	00 ء	.8 O	•20	•00	+00	03،	+00	۰00	۰00
6655.09 324.66 22	42.49 65.84	••0	1.00	1.08	4.08	3.25	°25	9.66	• û0	.70	»20	•1C	٥٥ ه	•C0	•00	.00	.00
6330.43 324.53 25	67.02 70.58	•00	1.17	•00	.42	1.33	۰00	2.92	+ CO	.5C	• 3 O	•20	۰00	• 00	•00	.00	۰00
6005.90 244.58 28	11.60 75.84	5.33	• 5 0	.00	2.83	7.50	₀5C	16.66	.40	.40	.10	.10	•00	٥0.	۰40»	٥0 ه	۰00
5761.32 52.20 28	63.80 42.25	5 - 17	3,58	.00	• 4 Z	1.58	·•50	11.25	.60	10	•20	•10	•00	.00	.60	•00	•00
5769.12 74.40 29	38.20 31.25	5.00	3.00	.00	• 50	5.25	.00	13.75	.90	•30	•10	•00	۰00	.00	• 90	.00	•00

KEY FOR SOIL IYPES		*KEY TO VALUES FOR RUNNING WATER
1 - SILT AND CLAY	V - CEMENTEO GROUNO	
11 - CLAY AND SAND	VI - PEAT AND TRASH	G = ORY .75 = RUNNING WATER
111 - SANO ANO GRAVEL	V11 - COHESIVE GROUND	.25 = MO1ST 1 = FLOODED
IV - COBBLES AND BOULDERS	VI11 - RUNNING GROUND	.50 = WET

VASHINGTON HETROPOLITAN AREA TRANSIT AUTHORITY Contract number ifocol F2a branch Route ingund Vashington, S.C.

				EEK	THE W							AUSE	NHOURS - Ev C						
UNNING WATER#	VIII	V11	V I	۷	IV	111	11	1	TOTAL COWN HOURS	ACHIN	MISC	MUCK TRANS	CONVE YOR	EXCAV	SHIELO	HRS IN	CA TE		STATION AT START CF week
•00	.00				1.00				2.58	.oc	1.58			• 00	• - 0	14.92			6613.53
•00	.00	.20	.00	•00	•26	•50	1.00	• 30	10.59	•00	8•4Z	.00	2.17	.00	.00	75.91	102-04	84.73	8596+22
•00	•00	• 40	.00	.00	.00	-30	•6 D	.50	8.91	.25	2.58	4.68	2.00	.00	.00	26.09	139.31	37.27	8457.94
.00	• 00	• 7 3	•00	*CO	.5ĩ	•4C	•5 C	1.00	13.00	•25	4.25	Z • 58	4.67	.00	1.25	65.5J	327.55	188.24	6420.67
•00	.00	. 80	• 30	•00	•20	-30	.40	.80	12.24	.50	2.75	. 91	. 25	1.83	6.00	66 • 25	522.16	194.61	8232.43
•00	.00	• 8 0	.30	.00	.90	.40	•20	•8J	8.08	•00	7.SC	. 33	.00	.25	•90	55.42	687.04	164.88	8037.82
.00	.20	.70	.10	•:0	.50	.50	•20	•70	7.67	•5 c	2.92	.75	3.50	.00	•JD	103.83	993.97	306.93	7872.94
•00	.00	• 5 0	• CO	•00	•7C	•60	.40	.50	9.17	•5C	7.67	•00	1.00	.00	•00	99.33	1261.46	287.49	7566.01
.00	• 00	• 30	.00	.00	•8 C	.80	•60	• 30	10.75	•5 ⁿ	8.58	1.67	.00	.00	.00	97.75	1581.61	300.15	7278.52
•10	.00	• 20	•C0	•CO	.10	.50	•6 C	.20	8.18	1.50	4 • 9 3	• 75	1.00	• 00	•00	64 •E Z	1679.66	98.05	6978.37
-20	•40	•40	•00	•00	.Zű	•60	.70	.40	10.67	1.25	6.00	•00	• 4 2	3.00	•00	89.83	1915.98	236.32	6860.32
.50	•OC	.40	•00	+ CO	• 4 C	•60	.70	•40	11.58	•00	9.08	1.00	1.50	•00	•ů0	96.92	2139.52	223.54	£644 • 00
.60	.00	.40	.co	•c0	.30	.50	. 6 0	•40	7.51	• ÔÖ	3.92	2.17	1.42	.00	•~0	82.49	2391.57	252.05	£426.12
1.00	.60	.10	.00	.00	•80	•60	•90	• 10	12.42	.00	7.67	2.00	1.17	.00	1.58	80.58	2560.64	169.37	6174.07
•50	.00	.70	•00	•00	.90	.80	•40	• 70	4.34	.00	3.67	.00	.00	•00	.67	38.16	2595.38	34.74	6005.00
	.00	. 80	÷00	.00	•90	.80	•30	•90	14.68	•0C	11.17	- 58	.75	•00	2.18	119.07	2645.01	249.63	5970 .26
.00	.00	1.00	.00	•00	.90	.30	•00	1.00	1.83	.25	1.25	•00	.33	•00	•00	51.17	2934.87	89.66	5720.63

KLY FOR SOIL TYPES		*KEY TO VALUES FOR RUNNING WATER
I - SILT AND CLAY	V - CEMENTED GROUND	
11 - CLAY AND SAND	V1 - PEAT AND TRASH	D = DRY .75 = RUNNING WATER
111 - SAND AND GRAVEL	VII - COHESIVE GROUNC	.25 = MOIST 1 = FLOODED
IV - COBBLES AND BOULDERS	VIII - RUNNING GROUND	.50 = WET

PROGRESS ANL PRODUCTION

SASHINGTON METROPELITAN AREA TRANSIT AUTHORITY Centract Number 167012 Fig North Outbound Machineton, J.C.

					00w	NHOURS - 8 y C	AUSE	WEEK ======				T 1VE		ENCY The W	EEK			UR I NG	
STATION AT START CF meek		CUMUL . FEET TO CATE		SHIELD	EXCAV EGU1P	C GNVE YOR	MUCK TRANS			TOTAL COWN POURS	1	11	111		v				RUNNING WATER+
			=============																
1352.00	18.00	16.05	39.00	• JO	•OU	•00	.00	.00	•00	•00	.50	-10	•40	.00	•00	•00	• 5 0	.00	.00
1334.00	21.00	39.00	38.90	• 20	.00	• 00	3•0ô	3.00	•00	6.36	.50	.10	•40	•00	•00	•00	• 5 0	.00	.00
1313.00	101.00	140.00	74.30	•00	.00	.00	1.00	.67	•00	1.67	•\$0	-10	•40	.30	•00	•00	.50	.00	.00
1212.00	142.30	282.00	79.40	9.65	.00	- C D	.00	•00	6.92	16.57	.30	•20	.*0	-1C	•C0	•00	• 30	• • • • •	.00
1070.00	84.00	366.00	74.80	9.33	.00	.00	.60	8.33	•00	17.66	.40	•30	•30	• 9C	.00	• 00	. 40	•20	•20
986.00	52.00	918.00	41.30	• UD	•00	.00	• 60	2.17	•00	2.17	•8C	-00	-10	•0c	•00	.10	• 8 0	•20	•00
934 •CU	82.00	500.00	77.80	1.50	•OC	•00	•00	6.67	.00	8.17	•80	•0Ċ	•2 C	• 0,0	•00	•¢0	-80	•10	•00
852.00	105.00	605.00	95 +80	5.25	•00	.00	.00	2.50	•00	7.75	.70	•00	•30	.00	•00	.00	• 70	•10	.10
747.00	31.00	636.00	49.70	2.42	•CO	• 0 0	• 00	9.92	.00	12.34	•70	•2 O	•00	• 10	• 00	.10	• 70	.10	•00
716 .00	73.00	709.00	62.60	0 ن ہ	•00	. O Ó	.00	3.91	•00·	3.91	.70	. Ī0	•20	• Ö Ő	•cð	.00	. 70	.10	.10
643.00	24.00	733.00	41.80	0 ئى م	•00	+00	• 00	7.67	•50	8.17	.40	•00	•6 C	• O C	•00	•00	• 4 (•10	.00
619.00	67.00	800.00	48.30	7.08	.60	.00	•00	1.67	•00°	8.75	÷6 0	°•10	.30	•DŰ	.00	.00	. 60	10	.00
552 .00	74.00	874.00	49.10	1.50	.00	.00	5.50	.92	•00	7 .92		10	.30	.00	•00	•00	- 61	t in	.00
478 - CO	76.00	950.00	45.40	1.17	•00	.00	•00	3.08	7.33	11.58	.50	•20	.30	•30	03.	.00	. 50	-10	.00
402.00	25.00	975.00	19+00	• 00	•00	.00	.00	•00	.00	•00	• 50	•10	+40	•00	•00	•00	• 50	•10	.00

PROGRESS ANU PRODUCTION

WASHINGTON METROPOLITAN AREA TRANSIT AUTHORITY Contract Number 1f0012 f16 North Incound Machinetion, 0.c.

						HOURS -	AUSE					A T 1 V E		THE ¥	EEA				
STATION AI START CF NEEP	TUNNEL RATE FT/JK	EATE	HRS IN WELF		EQUIP	CONVEYOR	TRANS			TOTAL LOWN Hours	I	II	111		v	٧I			RUNNING WATER#
1353.00	32.00	32.00	55.00	±00	- G O	.00	.00	1.06	• JC	1.00	.50	•CC	⇒ 4 D	+10	.00	•00	•50	• NC	1.00
1326.00	143.00	175.00	65.6ü	• 0	.CO	.CU	• 6 0	6.42	۰۵0	6.42	.50	•IO	-40	.1ú	.00	.00	.50	.00	.50
1163.00	109.00	284.00	77.20	.UO	.00	.00	.00	3.33	. UD	3.33	.50	•0C•	.49	•10	.00	.00	.50	+GU	1 =00
1074.00	69.00	353.00	49.10	• JO	• C D	.06	۰00	ь.58	.83	7.41	+10	* 2 C	.70	a 0.6	•00	•CG	.10	.20	.Su
1045.00	81.00	434.00	58.50	6.25	.CC	.00	• 00	1.75	• JC	8.00	• CO	₀8C	•00	.00	•00	.10	•00	.10	1.00
924 .CJ	32.00	466.00	64.80	ů۵.	* 0 0	•00	.GU	11.20	.JO	11.20	• CO	•9C	•00	.30	00 -	01.	.00	-10	1.00
892.00	55.00	521.00	61.50	1.25	.00	-00	• 00	3.90	2 • 5 8	7 • 7 3	•C0	I.00	.CO	.00	•00	• C O	.00	•50	۰5 O
837.00	81.00	692.00	62 •20	1.00	• 60	. C O	.60	2.15	.00	3.75	• UO	1.00	• G O	•00	•00	• 00	.00	.20	.10
756.00	136.00	738.00	92.20	2.50	+00	.00	.75	• 0 O	•00	3.25	.CO	1.00	+ O O	.00	.00	۰00	+ O C	+10	• 0 0
620.00	112.00	856.00	66.70	3.60	+ O C	= 0 O	.00	.00	.00	3.8U	. [:] 00	1.00	•00	.0L	• C O	.00	.00	.0ú	00.
508.00	98.00	946.00	58.10	• JD	• C O	.00	.60	4.65	1.75	6.40	•20	°50	- UN	. 00	•00	• C G	. 2 C	.10	۰ O O
410.00	27.00	975.00	24.50	• U O	.00	• O O	• C D	- OD	3.00	3.00	•2U	نا 6 ه	•20	.00	.00	٥٦.	°50	.10	• G O

PROGRESS ANU PRODUCTION

WASHINGTON METROPOLITAN AREA TRANSIT AUTHORITY CONTRACT NUMBER 1FOG12 F1P SOUTH OUTGOUNG MASHINGTON, DaCo

GOWNHOURS - HOURS/WEEK RELATIVE FREDUENCY OF SCIL TYPE DURING THE WEEN E Y CAUSL STATION TUNNEL CUHUL. PROF AT START RATE FEET TO HRS IN "HIELD EXCAV CONVEYOR HUCK MISC AGMIN OF LEEV FIJKK CATL WEEF ELUIP TRANS TOTAL LOLN I 11 III IV V VI VII VIII PUNNING EGUIP ATER The second 3973.00 7 . 50 7.5" 6.60 . 92 .00 .00 .60 8.00 9.42 .50 • 00 ·00 1·00 ·00 ·00 .00 .00 .00 .00 3965.50 19.00 26.50 25.20 1.57 .00 .00 .00 13.25 × **D**O 14.82 .10 .00 .90 • 00 .00 .00 .10 .00 .00 3946.50 16.00 42.50 18.50 • J0 .00 .00 1.50 4.00 .00 5.50 •20 .00 00. 03. .00 .00 .20 .00 .00 79.00 31.00 3930.50 36.50 •00 +00 .00 .00 2.00 .00 2.00 .30 .00 .70 .00 .00 .00 .30 .00 .20 8.50 3894-06 56-00 135.UC 51.50 .00 .00 3 - 00 1.00 .00 12.50 «60 .00 .40 .00 - 00 .00 .50 .00 ۰00 3838.00 60.00 195.00 57.40 12.30 -60 • 6 6 .00 7.80 . JO 20.10 •6J •90 ۰۹0 • 00 .00 .50 .00 .00 "ÔO 3778.00 82.00 277.00 61.40 7.00 .00 • 0 0 • 2.00 7.10 .00 16.10 .80 .20 .20 .00 .00 •00 •00 . 80 . 00 3696.00 76.00 353.00 78.60 19-60 .33 5.00 .00 .00 .00 24.93 .70 .00 .30 .00 .00 .00 .70 .00 .20 3620.00 66.00 419.00 59.70 .33 .60 .00 .00 +00 11-50 • **n** n 11.83 .00 .40 .00 .00 .00 • 6 O .00 .00 3554 .CO 11.50 430.50 10.00 6.00 .00 .00 .00 2.30 .00 8.30 .60 ۰Ô۵ . 40 .00 .ú0 - 00 . 60 - da -0'T 3542.50 16.50 449.UD 25.70 • L O 3.00 .00 • 00 .00 .00 3.00 .50 .00 .50 .00 .00 • 00 .50 .00 .00 3524.00 61.00 510.0C 62.10 .67 4.65 .00 .58 1.50 .00 7.40 .60 .00 .30 .10 .00 .00 .60 • 00 .00 3463.00 69.00 579.00 68.70 7.83 .00 -00 . UD 1.00 .00 8.83 . 70 ٥٥. .20 • i 0 • GÖ .00 .70 60 .40 3394.00 17.00 596.00 16.IO 6.50 .00 .00 .00 .90 -ô0 7.40 .70 .00 .30 .00 .00 • 70 ۰00 .60 .00 3377.00 35.50 631.50 53.70 5.25 .00 .00 3.58 .00 8.83 •00 .70 .00 .30 .00 +00 .00 .70 .00 .00 3341,50 72.50 704.00 65.50 1.25 11.00 ÷00 • 00 7.75 •00 20.00 .00 .30 .60 • Ö O .10 .00 .60 .00 -50 3269.00 100.50 804.50 77.70 .00 1.00 . O O 8.83 -00 ۰00 • O O 9.83 • 60 .00 .30 .00 .IO .00 ۰60 1.00 3168.50 53.50 858.00 52.00 .00 2.50 .00 I4.50 1.00 .00 18.00 .60 .00 ₀2Ô .00 .20 .00 .60 .00 1.00 3115.00 101.50 959.50 68.50 6.33 2.50 .00 7.18 3.00 .00 19.01 .70 •20 .00 .00 ٠iō • C O .70 ۰00 -. 50 3013.50 125.50 1085.00 126.80 ۰U0 .00 .00 3.33 7.83 •00 11•16 •50 •30 •10 •10 •00 •00 •50 •00 - 0.0 KEY FOR SOIL TYPES *KEY TO VALUES FOR RUNNING WATER I - SILT AND CLAY II - CLAY AND SAND III - SAND AND GRAVEL IV - COBBLES AND BOULDERS V - CEMENTEO GROUNO VI - PEAT ANO TRASH VII - COMESIVE GROUNO VIII - RUNNING GROUNO 0 = 0RY -.75 = RUNNING WATER 1 = FL000E0 •25 = MOIST •50 = WET

VASHI16GTON HETROPCLITAF AREA TRANSIT AUTHORITY CONTRACT NUMBER IFOUI2 FIE SOUTH OUTBOUNG ASSHINGTON, D.C.

					C0w	HOURS - By C		WEEK			FELA	T 1 V E		ENCY		11 1	YPE O	URING	
STATION AT START CF DEEM				JHIELO	E XCA V EGUIP	CONVE YOR	MUCK TRANS	MISC	A0M1N	TOTAL LOWN HOURS	1	11	111	IV	v	VI-	v11	v111	RUNNING
2868.00	124.00	1209.0(86.70	3.JO	8.50	.00	1.75	3.00	•00	16.25	.50	.30	.10	•1c	•00	.00	.50	.00	•c0
2764 .00	97.00	1306.30	66.50	2.00	2.00	•00	2.50	3.00	•00	9.5U	•50	•30	•20	.03	•00	.00	. 50	.00	I.00
2667.00	96.00	1404.00	68.70	14.50	.00	.00	• 50	2.33	•00	17.33	•50	•10	•30	.10	•00	•00	.50	• 00	1.00
2570,00	125.50	1529.50	83.40	5 • 4 2	1.00	.00	•00	5.67	٥٥.	12.09	•50	•10	• 30	.10	•00	•00	• 5 0	.00	1.00
2444 • 50	129.50	1659.UC	84.70	• u D	2.25	.00	03•	6.60	•J0	10.85	.40	•20	.20	•2C	•c0	•00	. 40	•00	•50

 KEY FOR SOIL TYPES
 •KEY TO VALUES FOR RUNNING LATER

 I - SILT AND CLAY
 V - CLMENTED GROUND

 II - CLAY AND SAND
 VI - PEAT AND TRASH

 O = DRY
 .75 = RUNNING WATER

 III - SAND AND GRAVEL
 VII - COMESIVE GROUND

 IV - COBBLES AND BOULDERS
 VIII - RUNNING GROUND

							PROGRE	SS AND	PRODU	CTION									
KASHINGTO CONTRACT FI8 SOUTH	NUMBER I INDOU	1FC012 10	AREA TR	RANS1T	AUTHORI	τ γ													
LASHINGTO	JN, U.C	•																	
						HOURS - 8 Y C	AUSE	WLEK				T] V E		ENCY THE & =====	EEK		PE QU		
	TUNNEL	CUMUL.	PRO							TOTAL									
STATION #T START	RATE			SHIELO	EXCAV	CONVE YOR	MUCK	M1 SC	AUMIN	LOWN	1	11	111	1 V	۷	VI	VII V	111 6	RUNNING WATER®
CF WEEK	ET/WK	CATE	nEE⊬		EOUIP		TRANS			HOURS									
*********	======				******														
3971.0C	72.00	72.00	64.00	•00	•00	.00	.00	7.50	•00	7.50	.50	.10	•20	• Z C	• CO	•00	.50	•20	•00
3899.00	67.00	139.00	73.90	•00	•00	•00	18.42	5.73	.00	24.15	•50	•00	•30	•20	.00	•00	.50	.86	.00
3832.00	113.00	252.00	82.00	0ن.	.00	.00	•00	5.50	•00	5.50	• 70	•00	•20	• 1 C	•00	•00	. 70	•50	•00
3719.00	146.00	398.00	76.10	• 58	.00	•00	•00	6.00	1.33	9.91	•70	•10	•20	.06	•00	•00	.70	•10	•00
3573.00	176.00	568.CO	85.60	•ú0	• • • •	.00	•00	1.92	•00	1.92	•6.)	.00	.20	• 0 C	.00	•00	.80	•00	•00
3463.00	93.00	661.00	54.40	•50	•25	•50	•OV	1.33	•0 C	2.08	•70	•3C	•00	• 30	.00	•00	.70	.00	1.00
3310.00	141.00	802.00	83.CU	• 20	• 5 0	•00	1.50	3.00	•00	5.00	. 60	.30	•00	•00	- 10	•00	.60	•00	
3169.00	162.00	964.00	89.20	2.83	.50	•00	•00	1.00	•00	4.33	•50	.40	•10	•00	•00	•00	.60	•00	1.00
3007.00	150.00	1114.00	97.00	• UO	•00	•00	•00	2.00	•00	2.00		.20	•10	•00	• 00	•00	.70	•00	.50
2857.00	133.00	1247.00	91.00	1.00	.00	• 00	•00	.00	.00	1.00		.30					.50		
2724.00	129.00	1376.00	80.30	1.50	•25	•00	1.10	.83	•00	3.68	.50	•20			+00	•00	• 5 C		.50
2595.00	109.00	1485.00	73.40	6.33	•00	•00	2.00	.75	5.00	14.08	• 50	.10	.30	•10	•00	•00	.50		•40
2486 .00	97.00	1582.00	70.30	3.17	•00	•00	5.00	3.50	•00	11.67	•50	-20			•00	•00	•\$0	•00	
2389.00	72.00	1654.00	62.30	1 • 17	.00	.00	2.00	1.00	•00	4.17	.50	.20	.20	.10	•00	•00	• 50	•00	•40

PROGRESS AND PRODUCTION

WASHINGTON METPOPOLITAN AREA TRANSIT AUTHORINY CONTRACT NUMPER 100091 0-9 South Inpound WASHINGTON, O.C.

					001	HOURS - By C	AUSE				REL	TIVE		ENCY THE W		IL T	rpe o	URING	
AT STAPT	TUNNEL RATE FT/WK	CUMUL. FEET TO DATE	PROO HRS IN WEEK	SHIELD	EXCAV	CON VE Y DR	MUCK TRANS		AOMIN	TOTAL ODWN HOURS	1	11	111	IV	v	v I	v11	viii F	UNNING WATER+
22168.00	28.00	28.00	94.75	.00	.00	•00	1.00	• 00	.25	1.25	1.00	•00	•00	• 00	• 00	.00	1.00	•00	•00
22140.00	84.90	112.90	105.00	•00	4.00	.60	.00	8.00	.00	12.00	1.00	.00	.00	•00	•00	.00	1.00	.00	-00
22079.00	105.00	217.90	111.33	• CO	4.17	•00	2.00	2.00	•00	8.17	.80	•00	.00	•00	•20	•00	.80	.00	+00
21974.00	83.00	300.90	106.00	1.00	4.00	.00	11.00	8.00	+00	24.03	• 90	.00	•00	•00	.10	.00	• 90	.00	.00
21891.00	78.00	378.90	93.00	•00	•00	•00	14.00	.00	•00	14.00	1.00	.00	•00	.00	•00	•00	1.00	•10	• 30
21813.00	123.00	501.90	110.00	• 00	•00	• 00	21.00	4.00	+00	25.00	1.00	•00	•00	•00	• 00	•00	1.00	•00	• 30
21690.00	106.00	607.90	110.00	7.50	5.50	.00	2.00	5.00	.00	20.00	1.00	.00	.00	•00	•00	•00	1.00	•00	.10
21584.00	92.00	699.90	107.00	•00	•00	-00	•00	8.75	.00	8.75	1.00	•00	.00	•00	• 00	•00	1.00	•00	•00
21492.00	25.00	724.90	30.00	• 00	•00	.00	8.00	.00	•00	8.00	1.00	•00	.00	•00	• 00	•00	1.00	•00	•00

KEY	FOR SOIL TYPES	
I	- SILT AND CLAY	V - CEMENTED GROUND
11	- CLAY AND SAND	VI - PEAT AND TRASH
111	- SAND AND GRAVEL	VII - COHESIVE GROUND
IV	- COPELES AND EDULDERS	VIII - RUNNING GROUND

*KEY TO VALUES FOR RUNNING WATER

0	Ξ	ORY	.75	Ξ	RUNNING	MATER
.25	z	MOIST	1	Ξ	FLOODED	
.50	Ξ	WET				

Appendix A-3

Rate of advance calculations vs. measured rate for each data set of each tunnel.

The calculation procedure includes the estimate of the learning curve exponent, equation (6.1), the intercept, equation (6.2) and their substitution in the RoA equation (6.3).

GAY AREA RAPIO TPANSIT OISTRICT CONTRACT NUMBEP IMCO31 MR TUNNEL - 24TH TO FANOALL STREET SAN FRANTISCO, CALIFORNIA

WEEK	CUMPLATIVE	DOWN HOURS CCRRECTION	501L CORRECTION	SHIELO CORRECTION	EXCAVATING ESUIPMENT CORRECTION	#EEK*5 =========== 1 N TE GRATION	5 HOUR5 5 SUMMATION	CUMULATIN TTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTT			. POURS
1	1 * .00	1.00	.75	9.93	1.50	30.15	26 • 22	30.15	26.22	8.00	5 = 0 ⁿ
2	47.50	1 • 1 2	.75	9.93	1.50	43+10	42+31	73.25	68=53	32+00	40.00
?	235+00	1.00	.75	9.93	1.50	145.82	141+14	219.07	209.67	110.00	150.00
4	737.50	1.03	.75	9.93	1.50	61.73	61.62	280.RD	271.28	41.00	191.00
5	557.50	1.02	•73	9.93	1.50	118.63	118.17	399.44	389.46	111+00	*02+06
6	68^.00	1.03	.73	9.93	1.50	63.49	63.43	462.91	452.89	56.00	353.00
7	825.00	1.01	.77	9.93	1+50	69.75	69.71	532.66	°22.60	54.00	412.00
ρ	1385.00	1.02	.77	9.93	1.50	118+20	118.37	650.R7	640.67	94.00	506.00
9	1377.50	1.00	.76	9.93	1.50	119.01	118.90	769.87	759.57	94.00	600.00
10	1502+50	1 • 1 2	.76	9.93	1 • 5 0	54+26	54.76	824+14	817.83	84.00	674+00
11	1657.50	1.15	.76	9.93	1.50	67.14	67.13	891.28	830.96	77.00	761+CC
12	1950.00	1 • C 4	.76	9.93	1.50	73.02	73.01	964.30	953.96	92.00	851.00
1 *	1960.00	1 + 38	.79	9.93	t.50	57.28	57.2P	1021.58	1011.24	5C.PO	901.00
14	2050.00	1 = 0.3	.79	9.93	1.50	34.30	34.30	1055.98	1045.54	112.00	1013.00
15	2300.00	1.05	_* 7 ۹	9.93	1.56	95.02	95+00	1150.90	1140.54	86.00	1099.00
16	2557.50	1.06	. 7 %	9.93	1.50	95.92	95.91	1246.82	1236.45	82.00	1101-00
17	2057.50	1.02	.79	9.93	1.50	104.19	104.17	1351.02	1346.62	95.00	1276.01
1 %	3102.50	1.05	.76	9.93	1.50	81.35	81.34	1432.36	1421.96	100.00	1376.00
19	3340.00	1.08	.76	9.93	1.5C	79.32	79.31	1511.68	1501.27	8 R . 33	1464.00
20	35,57.50	1.02	•9C	9.93	1.50	94.33	94.32	1606.01	1595+59	94.00	1558.00

PAY ARFA RAPIO TPANSIT DISTRICT CONTRACT NUMMER IMOD31 MR TUNNEL - 24TH TO RANDALL SIREET SAN FRANCISCO, CALIFORNIA

₩E E K	CUMULATIVE FEET	DOWN HOURS Correction	50ÎL Correction	SH1ELO CDRRECTION	EXCAVATING EDUIPMENT CORRECTION	WEEK*5 ========= INTEGRATION		CUMULATIV TITEGRATION			L HOUR5
21	385 .00	1.04	.76	9.93	1.50	79.16	79.17	1685.19	1674.76	95.00	1653.00
22	4107.50	1+07	.76	9.93	1.50	76.63	76.62	1761.81	1751.39	92.00	1745.00
23	4297.50	1.09	.76	9.93	1.50	60.75	60.74	1822.56	1812.13	83.00	1828.00
24	434*.00	2.16	.76	9.93	1.50	20.04	29.34	1851.60	1841.17	41.00	1869.00
25	4425.00	1.01	•78	9.93	1.50	23+28	23.28	1874.87	1864.45	56.00	1925.00

Appendix A-3. Rate of Advance Calculations.

RAY AREA RAPID TRANSIT DISTRICT CONTRACT NUMBER 1M0031 WL TUNNEL - 24TH TO PANDALL STREET SAN FRANCISCO, CALIFORNIA

WEEK	CUMULATIVF FEET	DOWN HOURS Correction	501L	SHIELO Correction	EXCAVATING EQUIPMENT CORRECTION	WEEK'S					L HOURS
		CORRECTION	CORRECTION	CONNECTION		INTEGRATION	SURRALIUN	INICORALIUN	504841104	*CENS	CONDENTIVE
1	20.00	1.04	. 75	9.93	1.50	39.25	34.45	39.25	34.45	32.00	32.00
7	52.50	1.08	.75	9.93	1.50	41.41	40.90	80.66	75.35	34.00	66.00
3	175.00	1.27	. 75	9.93	1.50	134.94	132.42	215.60	237.77	76.00	142.00
4	334.00	1.15	.75	9.93	1.50	125.79	125.35	341.40	332.82	89.00	231.00
5	55°.00	1.02	.73	9.93	1.50	128.52	128.06	469.92	460.87	113.00	344.CC
6	797.50	1.00	.77	9.93	1.50	127.47	127.24	597.39	58A.11	102.00	446.00
7	1167.50	1.01	. 77	9.93	1.50	180.39	180.71	777.78	768.11	112.00	558.00
۵	1359.00	1.02	.76	9.93	1.50	84.87	84.94	862.65	852.96	60.00	618.00
9	1487.50	1.01	.76	9.93	1.50	59.31	59.31	921.96	912.20	63.00	6º1.00
10	1515.50	1.09	.76	9.93	1.50	12.85	12.52	934.81	924.66	10.00	691.00
11	1695.30	1.06	.76	9.93	1.50	78.86	79.37	1013.67	1003.95	84.00	775.00
17	1.70.00	1.07	.76	9.93	1.50	75.65	75.64	1089.32	1079.59	93.00	A68.GC
13	1935+00	1.66	.79	9.93	1.50	44.84	44.84	1134.16	1124.43	59.00	•27.00
14	1987.50	3.49	.79	9.93	1.50	75.62	32.34	1209.78	1156.77	28.00	955.00
15	2157.53	1.71	.79	9.93	1.50	86.20	86.70	1295.94	1242.97	66.00	1021.00
16	2495.00	1.02	.79	9.93	1.50	132.86	132.82	1428.95	1375.79	104.00	1125.00
17	2577.50	1.53	.79	9.93	1.50	48.61	48.61	1477.45	1424.40	56.00	1181.00
19	2787.53	1.04	.79	9.93	1.50	82.31	92.30	1559.76	1506.70	101.00	1282.00
19	308^.00	1.02	.76	9.93	1.50	105.01	105.30	1664.78	1611.70	94.00	1376.00
20	3285.00	1.06	.76	9.93	1.50	74.81	74.81	1739.59	1686.5C	95.00	1471.00

PAY AREA RAPID TRANSIT DISTRICT CONTRACT NUMBER 1M0031 ML TUNNEL - 24TH TO RANDALL STREET SAN FRANCISCO, CALIFORNIA

WEEK	CUNULATIVE FEET	DOWN HOURS Correction	50IL Corrfction	SHIELD Correction	EXCAVATING Equipment Correction	WEEK'S		CUMULATIV			AL HOURS CUMULATIVE
21	3510.00	1.00	.76	9.93	1.50	81.68	83.50	1821.26	1770.01	92.00	1563.00
2 2	3795.00	1.03	.90	9.93	1.50	115.00	114.99	1936.27	1885.00	95.00	1659.00
2 3	4120.00	1.02	.76	9.93	1.50	107.42	107.41	2043.68	1992.40	104.00	1762.00
24	4280.00	1.04	.76	9.93	1.50	52.48	52.88	2096.56	2045.26	108.00	1870.00
25	4397.00	1.00	• 7 8	9.93	1.50	35.78	35.78	2132.34	2081.06	101.00	1971.00

PAY AREA RAPID TRANSIT DISTRICT Contract number 1r0053 Pr/RL Tunnels Gerkeley, California

	CUMPLATIVE	DOWN HOURS	SOIL	SHIELD	EXCAVALING ECUIPHENT	WEEK*5	HOURS	CUMULATIV	HOUPS	A U T J A	L HOURS
WEEX			CORRECTION	CORRECTION	CORRECTION	INTEGRATION	SUMMATION	INTEGRATION	SUMMATION	WEEKS	CUMULAT 1VE
1	29.00	1.09	• 8 8	10.77	. 9.2	153.23	91.99	153.23	91.99	76.00	76.00
Z	90.00	1.00	• P 8	10.77	. 8 2	198.67	195.58	351,90	287.58	120.00	196.00
3	16 7.00	1.00	.88	10.77	• 8 2	191.87	191.04	543.78	478.61	119.00	314.00
4	212.00	1+13	• ¤ 6	10.77	• 8 2	131.75	131.63	675.52	610.25	111.00	425.CO
5	254.00	1.39	.88	10.77	• ⁸ 2	127.02	126.94	802.55	737.19	114.00	539.DD
6	320.00	1.31	.88	10.77	• 8 2	120.11	120.05	922.65	857.24	119.00	658.C7
7	367.00	1.39	.A8	10.77	• 8 2	133.41	133.38	1056.06	990.62	80.00	7 ° 8 • C C
۹	847.CO	1.00	. 8.8	10.77	.82	149.42	149.36	1205.49	1139.97	118.00	856.00
9	529.00	1.00	• A 8	10.77	. 8 2	161.53	161.46	1367.01	1301.44	120.00	976.00
10	614.00	1.21	. A 8	10.77	. 8 2	158.79	158.75	1525.81	1460.18	114.00	1094+00
11	710.00	1.03		10.77	. 8 ž	171.58	171.53	1697 • 39	1631.71	111.00	1205.00
1,2	771.20	1.02	• ^e 8	10.77	• 8 Z	101.58	101.57	1798.97	1733.29	7 . 00	1263.00
13	867.00	1.01	• ° 8	10.77	• 8 2	152+14	152.11	1951.10	1885.40	117.00	_1400+00
14	×40.00	1.74	• A E	10.77	.82	136.96	136.95	2088.06	2022+35	113.00	1513.00
1 %	1014.00	1.14	. P C	10.77	. e 2	110.18	119.17	2206.24	214C.52	99.00	1612.00
15	1090.00	1.01	. B D	10.77	• P 2	117.97	117.96	2324.21	2258.47	119.00	1731.00
17	1157.00	1.02	• 9.0	10.77	• 9 2	82.06	82.36	2406+27	234C•53	94.00	1825.00
1 Բ	1225.00	1.30	• R C	10.77	• P Z	93.28	94.65	2499.55	2435.19	96.00	1921.00
19	1297.00	1.00	. 90	10.77	.82	99.46	99.46	2599.01	2534.64	120.00	2041.00
z٦	1374.00	1.00	.90	10.77	. 8 2	127.35	127.34	2726.35	2661.98	119.00	2160.00

PAY AREA RAPID TPANSIT DISTRICT CONTPACT NUMBER IRODES RR/RL TJMNEL! BERKELEY, CALIFORNIA

			SCIL	SHIELO	EXCAVATING EQUIPMENT	WFEK'S	HOURS	CUMULATIV	E HOURS	ACTUA	L HOURS
WEEK	CUMULATIVE FEET	CORRECTION		CORRECTION		INTEGRATION	SUMMATION	INTEGRATION	SUMMATION	WEEKS	CUMULATIVE
21	1459.00	1.00	.90	10.77	• 9 2	126.92	126.91	2853.27	2788.90	119.00	2279.00
22	1474.00	1.00	.90	10.77	. 8 2	22.10	22.10	2875.37	2811.00	120.00	2309.00
23	1479.00	1.00	.90	10.77	• 8 2	7.35	7.35	2882.72	2818.35	120.00	2519+00
24	1599.00	1.01	.66	10.77	• R 2	127.85	127.94	3010.58	2946.19	115.00	2634+00
2 5	1677.00	1.01	.66	10.77	• 8 2	78,10	78.10	3088.68	3024.29	7 8 . 0 0	2712.00
26	1810.00	1.00	.66	10.77	• 8 2	142.29	142.28	3230.97	3166.57	119.00	2871.00
27	1947.00	1.72	.66	10.77	.82	137.47	137.47	3368.44	3304+03	112.00	2943.00
29	2059.00	1.36	+66	10.77	• 8 2	121.87	121.96	3490.31	3425.90	103.00	3046.00
29	2199.00	1.01	.66	16.77	• 8 2	137.76	137.76	3628.07	3563.65	118.00	3164.00
30	2329.00	1.02	+66	10.77	• 8 2	128.00	128.00	3756.08	3691.65	112.00	3276.00
31	2369.00	1.41	.66	10.77	• 8 2	52.45	52.45	3909.53	3744.10	69.00	3345.00
32	2467.00	1.01	.90	10,77	.82	123.73	123.73	3937.26	3867.83	117.00	3462.00
33	2546.00	1.02	. ° 0	10.77	.82	110.58	110.58	4042.83	3978.40	116.00	3578.00
34	2657.00	1.00	.90	10.77	• 8.2	133 • 15	133.15	4175.99	4111.55	110.00	3697+00
35	2746.00	1.00	• 9 0	10.77	.82	121.74	121.73	4297.72	4233.29	120.00	3817.00
36	2810.00	1.31	• 9 0	10.77	. 8 2	105.17	105.17	9402.89	4338.45	77.00	3894.00
37	2889.00	1.01	.90	10.77	• B 2	98.27	98.27	4501-16	4436.73	118.00	4012.00
3 P	2903.00	1.00	• • 0	10.77	+ 8 2	18.69	18.69	4519.86	4455.42	120.00	4132.00

DAY ANEA RAPIO TRANSIT OTSTRICT CONIRACT NUMBER ISCOII TR TUNNEL SAN FRANCISCO, CALIFORNIA

	CUMPLATIVE	DOWN HOURS	501L	SHIELO	EXCAVATING EQUIPMENT	WEE**5	FOURS	CUMULATIV	HOURS	ACTU	L HOURS
WEEK		CORRECTION		CORRECTION	CORRECTION	INTEGRATION	SUMMATICN	INTEGRATION	SUMMATICN	WEEKS	CUMULATIVE
1	47.43	1.01	.73	9.11	1.09	77.98	66 • 1 2	77.98	66.12	63.38	63.08
2	194.73	1.01	• 7 5	9 • 1 1	1.09	128.04	124.20	206 • C 2	190.32	114.84	177.92
3	367.07	1.01	.75	9.11	1.49	149.09	148.11	355.11	338.42	112.76	290.68
4	564.85	1.01	•76	9.11	1.49	155.81	155.27	510.93	493.69	115.59	406.27
5	696.74	1.07	.75	9.11	1 • 6 3	102.73	102.66	613.66	596.35	99.44	505.71
6	P60.09	1.06	•73	9.11	1.49	123.71	123.58	737.37	719.93	99.37	605.08
7	1114+23	1.03	. 75	9.11	1.49	135.36	135.24	872 • 74	\$55.17	102.36	707.44
9	1357.38	1,03	.75	9.11	1.49	132.08	132.30	1004.82	987.17	108.40	815.84
Ŷ	146 3 . 21	1.00	•73	9.11	1.49	55.59	55.59	1060.41	1042.76	118.66	934.50
10	151 * . 49	1.12	• 7 5	9.11	1.63	32.69	32.69	1093.11	1075.45	97.62	1032.17
11	1557.48	1.02	• 7 5	9 • 1 1	1.63	34.54	34.54	1127.65	1169.99	103.95	1176+07

PAY AREA RAPIO TPANSIT DISTRICT CONTRACT NUMBER 150011 TL TUNNEL SAN FRANCISCO, CELIFORMIA

WEEK	CUMPLATIVE FEET	DOWN HOURS Correction	SOIL CORRECTION	SHIELO CORRECTION	EXCAVATING EQUIPMENT CORRECTION	WEEK'S ========= 1ntegration	HOURS	CUMULATIV			L HOUR5 ======= Cumulative
1	44.76	1.01	.77	9.59	• 8 2	71.71	62.23	71.71	62.23	97.85	97.85
2	137.34	1.03	•79	9.59	.82	90.46	88.86	162.17	151.10	112.67	210.52
3	330.61	1.00	.81	9.59	• 8 2	129.36	128.10	291.53	279.19	114.59	325.11
4	469.43	1.00	.75	9.59	1.49	170.18	169.73	461.71	448.92	93.00	418.11
5	527.31	1.91	.74	9.59	1.45	152.60	152.00	614 • 31	601.32	93.58	511.69
6	824.68	1.02	.76	9.59	1.49	175.88	178.57	793.19	779.99	111.70	623.39
7	1054.04	1.03	.75	9.59	1.49	191.68	191.51	984.98	971.50	102.59	725.98
8	1281.41	1.03	.75	9.59	1.49	161.42	181.31	1166.29	1152.81	105.10	P31+C9
9	1451.36	1.07	.77	9.59	1.11	139.24	138.21	1304.54	1291.02	92.24	923.32
10	1516.29	1.00	.75	9.59	1.49	46.47	46.47	1351.01	1337.49	116.50	1039.82
11	1551.29	1.00	.75	9.59	1.49	43.51	43.51	1394.52	1381.00	75.66	1115.48

PAY AREA RAPIO TRANSIT CISTRICT Contract number 150011 SR Tusnël San Frajëisco, california

WEEK	CUNULATIVE FEET	OOWN HOURS Correction	501L CORRECTION	5H1ELD. Correction	EXCAVATING EQUIPMENT CORRECTION		HOURS	CUMULATIN		******	L HOURS CUMULATIVE
1	42.50	1.17	.83	9.59	1.09	83.56	73.02	83.56	73.02	55.42	55.42
2	16 . 10	1.00	.83	9.59	1.09	117.81	115.02	201.36	188.04	113.08	168.50
3	212.63	1.01	. 83	9.59	1.09	38.1P	38.14	239.54	226.18	44.24	212.74
a	325.03	1.04	.92	9.59	1.49	114.96	114.65	354.50	34C+84	84.83	297.57
5	480.91	1.01	.86	9.59	1.49	151.06	150.58	505.56	491.52	113.08	410.65
6	654.75	1.03	• R C	9.59	1.49	130.14	129.98	635.70	621.50	108.81	519.46
7	830.32	1.04	.79	9.59	1.49	134.80	134.67	770.50	756.17	100.83	620.29
4	1031.61	1.06	.85	9.59	1.49	143.36	143.27	913.86	899.44	91.23	711.52
9	1234.34	1.00	.83	9.59	1.49	134.26	134.19	1048.12	1033.63	117.00	828.52
10	1415.75	1.00	.83	9.59	1.49	112.59	112.55	1160.70	1146 • 19	95.42	923.94
11	1552.94	1.00	.85	9.59	1.54	153.42	153.40	1314.12	1299.58	84.08	1008.02

PAY AREA WAPIO TRAMSIT DISTRICT Contract Number 150011 SL TUNNEL SAN FRANCISCO, CALIFORNIA

	CUMULATIVE	DOWN HOURS	SOIL	541610	EXCAVATING EQUIPMENT	WEEK*S HOURS		CUMULATIV	E HOURS	ACTUAL HOURS	
WEEN		CORRECTION		CORRECTION	CORRECTION	INTEGRATION	SUPMATION	INTEGRATION	SUMMATION	WEEKS	CUMULAT1VE
1	20.93	1.00	• 75	e.71	1.49	75+73	63.91	75.73	63.81	109.33	109+33
2	109.53	1.00	.75	8 • 7 1	1.49	105.35	102.53	181.09	166.44	116.16	225.49
3	200.45	1.04	.75	8 • 7 1	1.49	102+64	101.48	283.72	268.31	112.17	337+66
4	326.95	1.02	.75	8.71	1.49	99.36	99.00	383. ⁰⁸	367.32	112.42	450.CP
5	386.93	1.02	.75	8 . 71	1.49	45.81	45.79	420.89	413+10	57.67	507.75
6	525.03	1.03	.75	e • 7 1	1.49	98+81	98.64	527.70	511.74	108.50	616.25
7	639.23	1.05	.75	8.71	1.49	76.11	76.36	603.81	587.80	81.17	697.42
e	796.72	1.01	.75	8 • 7 1	1.49	95.24	95.15	699.05	687.96	105+58	803+00
9	951.61	1.04	.75	8.71	1.49	32 + 62	32.62	731.68	715.58	88.90	891.90
10	981.25	1.14	.75	8.71	1.49	81.11	81.28	P12.79	796.66	92+08	983.98
11	1116.09	1 • 1 3	.75	8.71	1.49	80 • 22	80.20	893.02	876.86	98.42	1082+40
12	1295.74	1.02	.75	8.71	1.49	92.22	92.18	985+23	969.04	112.09	1194.49
13	1457.86	1.08	.75	P • 71	1 • 2 6	76.52	76.50	1061.75	104°+54	83.95	1278.44
14	1565.19	1.01	.75	8.71	1.49	88 • 11	88.10	1149.86	1133.64	74.83	1353.27

SAY AREA RAPIO TRANSIT DISTRICT CONTRACT NUMBEP ISODSIA SL TUNNEL - MARKET STREET SAN FRANCISCO, CALIFORNIA

WEEK	CUMULATTVE FEET	ODWN HOURS Correction	501L CORRECTION	5HIELO CORRECTION	EXCAVATING EQUIPMENT CORRECTION		HOURS	CUMULATIV			CUMULATIVE
1	8 - 00	1.02	۰ ^p 3	8.71	1 • 1 7	279.96	130.39	279.96	130.39	112.36	112.36
z	157.50	1.10	• e D	8.71	1 • 1 7	138 + C 3	137.19	417.99	267.58	94.08	206+44
3	220.00	1.09	.79	8 . 71	1 • 1 7	116.65	116.37	534.64	383.94	96.44	302 • P.P
4	280.00	1.03	.79	8.71	1 • 1 7	e7.49	87.40	622.13	471.34	78.16	391.24
5	350.00	1.01	.75	F • 71	1.17	89.23	89.15	711.36	560.49	79,50	460.74
6	45*.20	1 = 0 3	.76	8.71	1 • 1 7	129.00	128.83	84C.36	680.72	106.03	566.77
7	564.70	1.02	. 75	8.71	1.17	117.41	117.32	957.78	806.64	110.10	676.87
ч	53°.70	1 + 9 3	.83	8 - 71	1.17	142.61	142.51	1100 - 39	940.15	107.49	789.36
9	720.70	1.01	• R 3	8 - 71	1.17	75+17	75.17	1175.57	1024.22	49.46	129.82

EAY AKEA RAPIO TRANSIT CONTRACT NUMPER 1500518 SR TUNNEL - MARKFT STREET SAN FRANCISCO, CALIFORNIA

WEEK	CUMIILATIVE FEET	DOWN HOURS Correction	501L CORRECTION	SHIELD CORRECTION	EXCAVATING EQUIPMENT Correction		HOURS	CUMULATIV			L HOUR5 ====== CU¤ULAT1VE
1	27.46	1.00	• e D	6 + 5 4	1.09	67.74	43.51	67.74	43.51	66.00	66.00
2	94.96	1.03	.74	6.84	1.09	00.86	78.73	148.60	122.24	110.25	176.25
3	137.46	1.09	. 81	8.84	1.09	45.76	45.64	194.36	167.88	52.34	228.59
4	190.24	1 • 0 2	.80	8 . 8 4	1.63	78.21	78.95	272.57	245.93	74.67	303.26
5	777.46	1.04	.77	8.84	1.63	100.33	100.36	372 - 90	345.99	106.69	409.95
e	384.96	1.07	.81	8 . 8 4	1.63	118.09	117.94	490.99	463.03	100.64	510.59
7	477.46	1.01	• A 3	8.84	1.63	90.29	90.71	581.28	554.04	78,25	508.84
٩	564.96	1.02	. 89	8.84	1.63	86.15	86.1C	667.43	64C.14	73.26	662.10
ç	687.46	1.01	.93	6.64	1 • 6 3	104.97	104.09	772.40	745.03	105.52	767+62
10	750.96	1+01	• 8.6	6.84	1.63	33.65	33.65	806.05	770.68	37.75	805.37

UPPE9 SALT CYEEK #1 CONTRACT NUMPER 68-404-25 CHICAGA, ILLINDIS

WEEK	CU411673VF FEF7	OOWN HOURS Correction	SOIL CORRECTION	SHIELO CORRECTION	EXCAVATING EQUIPMENT CORRECTION	WEEK'S INTEGRATION		CUMULATIV			L HOURS ======= Cumulative
1	24+00	1.13	.12	6+92	1.50	28.59	23.99	20.59	23.99	25.50	25+SC
ĉ	34.00	1.77	.75	6.92	1.50	10.27	10+23	36 • 80	34.22	16.00	41.50
۲	130.00	1+05	•77	6.92	1.50	49.84	48.60	88.70	62.62	44.00	P5+50
4	710.00	1.04	•67	6.92	1.50	28.58	28.46	117.28	111.28	25.00	110.50
Ľ	214.00	1.99	.67	6.92	1.50	2.46	2.46	119.74	113.74	3.00	113.50
6	242.00	1.92	.67	6.97	1.50	16.58	16.58	136.32	130+32	14.00	127+50
7	204000	1.27	.75	6.92	1.50	9.82	9.92	146.14	140.14	10.00	144.50
4	284.00	1.01	.75	6.92	1.50	6.70	6.30	152.44	146.44	10.00	155+50
9	*5*•30	1 • 1 3	.71	6.92	1.50	24.42	24.46	176.02	170.89	37.00	1**.55
10	41^.00	1.20	.67	6 • 92	1.50	16.22	16.21	193.13	167.10	1 • .00	273.51
11	590+CO	1.05	.67	6.92	1.50	43.63	43.52	236.76	230+65	40.00	243.50
12	204.00	1.11	.67	6.92	1.50	27.93	27.92	264.70	258.54	25.50	10.695
1 7	°3°•CO	1.08	.64	6.92	1.50	2P.14	28.13	292.84	286.66	28.00	202.00
14	1094.00	1.02	.75	6 • 92	1.50	55.60	55.53	349.44	342.19	38+CC	335.00
15	1*5*•"0	1.00	.75	6.97	1.50	52.89	52.94	401.32	395.03	38.00	373.00
16	1464.00	1.15	• A 5	6.97	1.50	25.60	25+59	426.02	426.63	16.50	189.50
17	1510.00	1.62	.92	6.92	1.50	16.21	16.21	443.14	436.84	15.00	471.50
18	1530.00	1.78	.89	6.92	1.50	4.73	4.73	447.86	441.57	12.00	413.50
19	1584.00	1.04	1.05	6 • 9 2	1.50	14.91	14.91	462.77	456.47	41.50	455.00
27	156 * + 00	1.08	.96	6.92	1.50	20.45	20.95	487.22	476.92	33.00	488.00

UPPER SALT CREEK #1 CONIGACT NUMPEG 66-404-25 CHICAGO, ILLINDIS

WEEK	CUMULATIVE	DOWN HOURS CCR9ECTION	SOIL CORPECTION	SHIELD CORRECTION	EXCAVATING EQUIPMENT COPRECTION	NFEK*S		CUPULATIV			L HOURS
21	1427.00	1.02	.94	6.92	1.50	34.34	34.33	517.56	511.25	38.50	526.50
2 2	200-00	1.06	• 9.2	6.92	1.50	35.65	35.55	553.21	546.90	37.00	563.50
23	2075.00	1.04	.76	6.92	1.50	12.79	12.79	566.00	559.69	34.00	597.50
24	2230.00	1.02	. 93	6.92	1.50	33.95	33.95	599.95	593.64	41.00	638.50
25	2274.00	1.36	• 9 3	6.92	1.50	9.54	9.59	609.49	603.18	19.00	657.50
54	2335.00	1.31	.75	6.92	1.50	13.51	13.51	623.00	616.69	23.00	680.50
27	2513.00	1.05	• 7 5	6.97	1.50	29.20	29.19	652.19	e44.86	31.00	711.50
29	2933.00	1.00	. 82	6.92	1.50	53.49	53.48	705.68	699.36	45.00	756.50
29	3741.00	1.02	•67	6.92	1.50	27.98	27.98	733.67	727.34	25.00	741.50
30	3349.00	1.03	• • [6.92	1.50	46.90	48.90	782.57	776.23	39.00	P20.50
31	3652.00	1.01	. 6 6	6.92	1.50	34.29	34 . 28	816.85	810.51	37.00	857.50
32	3*5*+00	1.05	.74	6.92	1.50	32.18	32+18	949.03	842.68	31.00	888.50
33	4729.00	1.00	.78	6.92	1+50	51.83	51.02	900.°t	894.51	45+00	933.50
34	4445.00	1.05	.7E	6.92	1+5 C	30 • 6 9	30.69	931.55	925.20	\$5.00	955.50
	4725.00	1.90	• 90	6.92	1.50	42.91	42.91	974.47	96 R • 1 1	34.00	989.50
	4977.00	1.08	.93	6.92	1.50	25.59	25.59	1000.06	997.70	23.50	1013.00
	517".00	1.01	.75	6.92	1.50	37.68	37.68	1037.74	1031.38	37.00	1050.00
	5481.00	1.04	.75	6.92	1.50	38.33	38.32	1076.07	1069.70	37.00	1087.00
	5887.00	1.00	.75	6.92	1.0	47.65	97.64	1123.71	1117.35	95.00	1132.00
40	6167.00	1+04	.84	6 • 92	1.50	38.71	38.71	1162.93	1156.06	33.50	1165.50

UPPER SALT CREEK #1 CONTRACT NUMBER 68-404-25 CHICAGO, 1LL14015

WEEK	CJMULATIVE FEET	DOWN HOURS Correction	SC1L CORRECTION	SH1ELD CORRECTION	EXCAVATING EQUIPMENT CORRECTION	WEEK''S		CUMULATIN TTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTT		========	L HOURS TITITI CUMULATIVE
41	634 . CO	1.00	1+72	6.92	1.50	27.8F	27.48	1190.30	1183.93	31.00	1106.50
42	6445.00	1.78	1.02	6.92	1.50	16.71	16.71	1207.01	1200+64	30.00	1226.50
43	645°.CC	1.14	1.02	6.92	1.50	8.46	8.46	1215.47	1209+10	25.00	1251.50
44	6519.00	1.70	• 9 9	6 • 92	1.50	6.59	6.59	1222.05	1215.6F	17.00	1268.50
45	6565.00	1.09	1.02	6.92	1.50	7.72	7.72	1229.77	1223.40	26.00	1294.50
44	6667.00	1.10	1.02	6 • 92	τ.\$0	16.49	16.49	1246.26	1239.89	33.00	1327.50
47	6°2°.00	1.00	1.02	6 • 92	1.50	24.72	24.72	1270.98	1264.61	36.00	1363.50
4.8	7077.00	1.00	1.02	6.92	1. 6 0	37.41	37.41	1308.39	1302.02	44.00	1407+50

HPPER SALT CREEK #2 Contract NUMBER 68-405+25 Chicago, 11114015

NEEK	CUMPLATIVE FEE1	OO⊌∿ HOURS Correction	SOIL CORRECTION	SHIELD CORRECTION	EXCAVATING EQUIPMENT CORRECTION	WEEK'S		CUMULATIV			HOURS
1	44.00	1.00	.75	6 • 2 9	1.63	23.46	19.63	23.48	19.63	40.00	40.00
2	6°+00	1.00	• 7 ^c	6.29	1.63	7.22	7.19	30.70	26.83	17.00	57.00
٦	172.00	1.03	.75	6 + 2 9	1.63	26.24	25.85	56.04	\$7.68	3(.00	•7.00
4	365.00	1.92	•75	6 . 2 9	1.50	36 • P 1	36.38	93.75	89.06	41.00	129+00
5	°67+00	1.01	•73	6.29	1 + S C	71.18	70.12	164.93	159.19	55.00	193.00
6	1127.00	1.04	. 75	6.29	1.0	17.76	17.75	182.69	176.94	14.00	197.00
7	1671.00	1.00	.69	6 . 29	1.50	49.21	49.36	231,90	226.01	41.00	2 7 8 + 0 0
8	1089.00	1.09	. 7 7	6.29	1.50	21.85	21.95	253.75	247.85	16.00	254.00
9	2384+00	1.02	.74	6.29	1.5C	41.89	41.05	295.65	289.70	36.00	290.00
10	3004.00	1.00	. 7 5	6.29	1.50	47.95	47.90	343.59	337.60	\$1.00	341+00
11	3110.00	1.10	.79	6.29	1.50	9.00	9.70	352.60	346.60	5.00	346,00
12	3480.00	1.00	.79	6.29	1 + 5 0	43.27	43.75	395.87	389.85	39.00	385.00
13	4091.00	1.02	•72	6.29	1.50	27.02	27.41	423.29	417.27	31.00	416+00
14	4534.00	1.00	.75	6 - 2 9	1.50	33.89	33.98	457.17	451.14	35.00	451+00
15	4972.00	1.02	• ª C	6 • 2 9	1 • S G	25.46	25.45	482.63	476.60	25.00	476.00
14	5*1*+00	1.00	• P 8	6.29	1.50	24.78	24.78	507.41	501.38	24.00	f00.00

UPPER SALT CREEK #3 Contract numper 68-406-25 Chicago, Illindis

WEEK	CUMULATIVE FEET	DOWN HOURS Correction	SOIL COPRECTION	SHIELD CORRECTION	E XCAVATING E CUIPMENT CORRECTION	WEEK'S		CUMULATIVE		*******	CUMULATIVE
1	2~.00	1.20	.75	5.77	1.63	22.59	19.15	27.59	19.15	10.00	10.00
7	134.00	1.05	.67	5.77	1.50	32.94	31.66	55.53	50.82	29.00	*8.00
3	26 . 00	1.01	• A 2	5.77	1.53	53.20	52.42	108.73	103.23	30.00	68.00
4	76°.CO	1.10	.67	5.77	1.50	27.82	27.76	136.55	130.99	23.00	91.00
¢,	526.00	1.00	.67	5.77	1.50	26.15	26.11	162.70	157.10	31.00	172.00
t	67	1.00	.71	5.77	1.50	28.00	27.97	190.70	18 7	22.00	144.00
7	842+00	1.05	• * 5	5.77	1.50	35.24	35.21	225.95	220.28	31.00	175.00
F	1110.00	1.00	.64	5.77	1.50	41.03	43.97	266.97	261.25	36.00	211.00
9	1230.00	1.21	• 9 0	5+77	1.50	24.28	24.27	291.25	285.53	14+00	225.00
10	1737.00	1.01	1.02	6.92	1.50	26.90	26.99	318+15	312.42	13.00	238.00
11	1417.00	1.15	.78	6.92	1. • 0	17.03	17.23	335.10	329.45	17.00	255.00
12	1561.00	1.01	.75	6.92	1.50	29.54	29.73	364.22	358.48	30.50	245.50
13	1781.00	1.00	.75	6.9?	1.56	33.70	33.69	397.92	397.18	29.00	314.50
14	1997.00	1.07	.75	6.92	1.50	19.62	19.51	417.54	411.79	20.00	334.50
15	2157.00	1.00	.75	6.92	1.50	41.24	41.73	458.78	453.02	29.00	*63.50
16	2477.00	1.00	.75	6.92	1.00	49.20	49.18	567.98	502.21	40.00	403.50
17	2720.00	1.03	.75	6.92	1.50	38.09	38.39	546.07	540.29	27.00	4 TO . 5C
15	3029.00	1.00	••0	6.92	1.50	45.49	45.4P	591.56	FR6.77	34.50	445.00
19	3309.00	1.03	.78	6.92	1.50	41.30	41.70	632.87	627.07	31.00	496.00
20	3655.00	1.00	.75	6.92	1.50	50.16	50.15	683.03	677.22	38.00	534.00

UPPER SALT CPEEN #7 Contract numper f8-466-2* Chicago, illinois

CUMULATIVE	DOWN HOURS	N HOURS SOIL	SHIELD	EXCAVATING EQUIPHENT	WEEK'S	HOURS	CUMULATIV	HOURS	ACTU	AL HOURS	
WEEK		CCRRECTION		CORRECTION	CORRECTION	INTEGRATION	SUMMATION	INTEGRATION	SUMMAT10N	WEEKS	CUMULATIVE
21	3457.00	1.07	.75	6.92	1.50	29.40	29.40	712.43	706.62	24.00	558.00
22	4297.00	1.50	• 7 *	f • 92	1.50	50.70	50.70	763.13	757.32	37.00	595.00
23	4565.00	1.00	.75	6.92	1.50	35.47	35.46	798.60	797.78	30.50	633+50
24	4726.00	1.12	.75	6.92	1.50	19.15	19.15	817.75	811.93	24.00	657.50
25	4PCF.C0	1.23	•73	6.92	1.50	11.62	11.62	829.37	823.55	15.00	672.50
26	4974.00	1.00	• 71	6.92	1.50	19.10	19.10	848.47	842.65	32.00	704.50
27	5764.00	1.00	• 7 5	6.92	1.50	34.36	34.35	882.92	877.00	37.00	
28	5567.00	1.00	•75	6.92	1.50	36.50	36.50	919.32	913.50	36.50	
29	5938.00	1.01	.76	6.92	1.50	29.50	29.50	948.F2	947.00	31.00	500.003

VASHINGTON METROPOLITAN AREA TRANSIT AUTHORITY CONTRACT NUMBER IF0021 F2A PLNTAGON OUTBOUNO VASHINGTON, 0.CC.

WEEK	CUMULATIVE FLET	DOWN HOURS Correction	SOIL CORRECTION	SHIELD CORRECTION	EXCAVATING EQUIPMENT CORRECTION		HOURS	CUMULATIV 			HOURS CUMULATIVE
1	67.00	1.01	.66	10.40	1.36	94.67	84.01	94.67	84.01	78.49	78.49
2	113.19	I.06	.66	10.40	1.36	47.66	47.49	142.34	131.51	27.28	175.77
3	280.08	1.02	.88	10.40	1.36	187.64	185.59	329.98	317.09	83.68	189.44
4	339+50	1.00	.90	10.40	1.36	49.62	49.60	379.60	366.73	21.65	211+10
۴	57.44	1.01	• 7 9	10.40	1.36	165.88	165.36	545.48	532+06	69.93	290.91
6	607.01	1.02	.68	10.40	1.36	34.01	34+00	579.49	566.06	23.34	104+27
7	617.28	1.04	.57	10.40	1.36	1.30	1.70	580.79	567.36	7.25	211+52
٩	7002	1.03	.69	10.40	1.76	57.54	57.52	630.73	124.85	37.15	348.67
ş	834.57	1.03	•65	10.40	1.36	78.98	76.96	717.31	707.84	77.55	426.22
10	1097.52	1.10	.79	10.40	1.36	165.66	165.49	882.97	860.33	97.42	523+64
11	1390.79	1.01	.79	10.40	1.36	175.15	175.72	1050.12	1044.75	95.76	119.41
12	140 * . 25	1.02	.79	10+40	1.36	10+14	10.14	1068.25	1054.50	16.02	636.37

WASHINGTON HETROPOLITAN AREA TRANSIT AUTHORITY CONTRACT NUMREP 1F0021 F2A PEMTAGON INDUNO WASHINGTON, O.C.

WEEN	CUMULATIVE FEET	DDWN HOURS Correction	SOIL Correction	SH1ELD CORRECTION	EXCAVATING E OU 1PMENT CORRECTION		HOURS	CUMULATIVI 			L HOUPS CUMULATIVE
1	7.50	1.00	•66	10.40	1.36	20.98	16.59	20+98	18.59	9.50	9.50
2	14.30	1.01	.66	10.40	1.36	13.00	12.93	33.98	31+51	9.28	17.79
3	36.26	1.03	.66	10.40	1.36	38.52	38.03	72.50	69.54	38.11	55.89
4	41.68	1.30	.66	10.40	1 + 3 6	4.20	4.20	76.70	73.73	8.40	64.29
5	58.89	1.09	.66	10.40	1.36	23.69	23.65	100.39	97.39	28.50	92.79
6	99.34	1.00	.66	10.40	1.36	44.47	44.31	144.86	141.70	34.20	130.99
7	165.30	1.00	-66	10.40	1.36	61.33	61.13	206.19	202.93	38.00	168.99
8	198.60	1.04	.66	10.40	1.36	36.95	36.03	242.24	238.86	22.7C	191.69
9	24 0 . 2 3	1.05	.66	10.40	1.36	44.39	44.36	286.63	263+22	26.68	218.37
10	289.30	1.03	.66	10+40	1.36	34.27	34.26	120.89	317.48	38.60	256.97
I 1	334.44	1.03	.66	10+40	1.36	37+83	37.82	358.72	355.29	38.42	295.39
I 2	48 *.10	1 • 0 2	.88	10.40	1.36	144.87	144.62	503.60	499.91	79.95	375.34
13	677.94	1.01	1.04	10.40	1.36	201+14	200.94	704.73	700.75	72.42	447.76
14	830.97	1.03	. 79	10.40	1.36	128.92	120.04	833.65	829.58	72.05	519+81
15	900.19	1.01	.79	10.40	1.*6	49.95	49.94	883.60	879.52	44.55	564.36
16	1017.26	1.01	.59	10.40	1.36	55.29	55.28	930.09	934.80	61.77	626.1?
17	1040.43	1.00	•68	10.40	1.36	16.08	16.08	954.97	950.88	17.50	643.63
18	1047.94	1.06	.68	10.40	1 • 3 6	1.57	1.57	956.54	952+46	6.50	650.13
1 ¢	1140.31	1.05	.6P	10.40	1.36	65.04	65.03	1021.58	1017.49	63.03	713.16
20	1319.62	1.02	. 5 9.	10,40	1.36	85.84	85.41	1107.42	1103.30	84.90	798.C6
21	1511.14	1.03	.69	10.40	1.36	109.53	109.50	1216.95	1212.80	89.40	887.46

WASHINGTON WETPOPOLITAN AREA TRANSIT AUTHOPITY Contract Numer IfCO21 F24 Klamph Route Outpound Washingion, D.C.

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	CUMPLATIVE	OOWN HOURS	5011	SHIFLO	EXCAVATING EDUIPMENT		HOUP5	CUMULATIV			L HOUR5
#65x	"EET	CORRECTION	CORRECTION	COPRECTION	CORRECTION	INTEGRATION	20MMAILTON	INIEGRALION	SUMMATION	WEEKS	CUMULATIVE
1	67.89	1.01	. 92	10.40	I.36	99.25	86.70	99.25	£6.70	54.08	54.08
2	204.52	1.05	•93	10.40	1.76	123.72	121.74	722.97	20 . 45	73.67	127.75
۲	237.44	1.03	. 9 3	10.40	1.36	20.91	26.91	243.AP	229.35	33.08	160.83
ú	253.76	1.00	.91	10.40	1.36	14.09	14.08	257.97	243.44	16.50	177.33
5	454.60	1.02	•93	10.40	1.36	136.04	135.36	394.01	378.79	62.00	2 39 . 3 3
6	610.77	1.01	.92	10+40	1.36	89.R7	89.76	483.08	46 . 55	49.67	248.00
7	876.31	1.01	.97	10.40	1.76	147.89	147.40	631.77	616.16	87.42	375.42
٩	1055.24	1.04	.93	10.4D	1.36	91.65	91.60	723.47	707.76	66.47	441.89
9	1367.17	1.72	.96	10.40	1.36	150.93	150.78	874.34	858.53	96.00	537.89
10	164°.07	1.03	.96	10.40	1.36	129.21	129.14	1003+56	987.48	۶7.58	625.47
I 1	1017.83	1.06	.93	10.40	1.36	119.79	118.74	1122.33	1106.41	62.25	6 - 7 . 72
17	2247.49	1.02	.93	10.40	1.36	131.12	131.07	1253.45	1237.48	65.84	753.56
1 ?	2567.02	1.00	.96	10.40	1.36	127.40	127.36	1380.25	1364.85	72.58	824.14
14	2811.60	1.02	• P 2	10.40	1.36	81.30	P1.29	1462.14	1446.13	75.84	809.98
15	2861.80	1.12	• • *	10.40	1.36	1°.98	18.98	1461.12	1465.11	42.25	942.23
16	2939.20	1.07	.79	10.40	1.36	24.27	24.27	1505.39	1489.38	31.25	973.48

WASHINSTON METROPOLITAN ARFA IRANSIT AUTHOPITY Contraci Numero ifoo?i F2a Rranch Poute Inbouno WaShington, D.C.

WEEK	CUMULAIIVE FEET	OCEN HOURS COFRECTION	501L Correction	5HIELO Correction	EXCAVATING EQUIPMENT CORRECTION	WEEK*5		CUPULATIVE			UL HOURS
1	17.31	1.02	. 9 2	10.40	1.36	45.09	39.48	45.09	39.46	14.92	14.92
2	137.04	1.01	.86	10.40	I.36	107.94	104.02	153.04	143.51	75.91	°0.63
۲	130.31	1.07	.84	10.40	1.36	3 . 9 3	35.07	191.96	102.38	26.09	116.92
4	227.55	1+92	•72	10.40	1.36	137.31	135.91	329.27	318.29	85.50	202.42
5	52 .16	1.03	.76	10.40	1.36	125.45	125.95	454.72	447.34	86.25	288.67
6	687.C4	1.00	.76	10.40	1.36	95.76	95.65	550.48	539.00	55.42	344.00
7	997.97	1.01	.77	10.40	1.36	161.62	161.30	712.10	700.29	103.83	447.92
4	1711.46	1.00	+ ⁰ 1	10.40	1.36	146.51	I46.37	858.61	P46.66	99.33	547.25
9	1581.61	1.00	.86	10.40	1.36	151+29	151.19	1009.90	997.86	97.75	£45.0C
10	1679.66	1.02	• 9 0	10.40	1.36	51.14	51.14	1061.03	1048.99	64.82	709.62
11	1915,96	1.02	.79	10.40	1.36	105.08	105.06	1166.12	1154.05	89.83	799.65
12	213". 42	1.01	. 83	10.40	1.36	99.58	99.57	1265.70	1253.61	96.92	896.57
13	2391.57	1.01	• A 2	10.40	1.36	107.44	107.42	1373.14	1361.03	82.49	979.06
14	256 64	1.01	.78	10.40	1.36	66.98	66.9R	1440.12	1420+01	80.58	1059.64
I 5	2555.78	1.01	.7t	10.40	1.36	13+63	13.63	1453.74	1441.63	38.16	1697.80
16	2045.01	1.01	.76	10.40	1.36	94.06	94.05	1547.81	1535.68	119.07	1216.87
Ι7	2934.87	1.00	.72	10.40	1.36	31.20	31.20	1579.01	1566.89	51.17	1268+04

washington hetropolitan area transit authority contract numper ifcold for outpound washington, $0.\varepsilon$

bEFK	CUMULATIVE FEET	DC®N POURS COFRECTION	SOIL CORRECTION	SHIELO CORRECTION	EXCAVATING EQUIPMENT CORRECTION	₩ F E K * S =========== 1 N T E G R A T 1 O N		CUPULATIVE	=======	=======	L HCURS ======= CU≃ULATIVE
1	1	1.00	. 90	12.19	.68	32.94	30.42	32 . 94	30+42	39.00	39.00
2	39.00	1.06	.90	12.19	.68	30.20	30.04	63.14	60.45	38.90	77.90
?	140.00	1.00	200	12.19	.68	111.96	110.44	175.10	170.89	74.30	152.20
4	282.00	1.09	.93	12.19	.68	146.89	146.24	321.99	317.13	79.40	231.60
5	366.00	1.06	.85	12.19	.68	70.97	70.92	392.96	388.05	74.80	306.40
ŧ.	418.00	1.00	.77	12 + 1 9	.68	36.56	36.55	429.52	424.61	41.30	347.70
7	500.00	1 • 🛙 1	.80	12.19	•68	58.84	58+83	48P.36	483.43	77.80	425.50
ß	60".00	1.03	. 84	12.19	÷6 8	77.01	76.98	565.37	560.42	95.80	521.30
9	636.00	1.04	.76	12.19	• 6 8	20+41	20+41	585.79	587.83	44.70	566.00
10	709.00	1.00	• ^A 1	12.19	.68	49.46	48.45	634.25	629.28	62.60	628.60
11	737.CU	1.03	.9+	12.19	.68	19.13	19.13	653.38	648.41	41.80	670.40
12	P07.00	1.05	.85	12.19	.68	47.68	47.68	701.06	696.09	48.30	718.70
13	A74.00	1.04	.85	12.19	.68	51.14	51.14	752.20	747.23	49.10	767.8C
14	\$57.00	1.11	.85	12.19	.68	55.68	55.68	PG7.88	P02+91	4 ° . 4 0	A13.20
15	975.00	1.00	.68	12.19	.68	16.92	16.92	R24.80	619.83	19.00	₽32+2C

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VASHINSTON HETROPOLITAN AREA TRANSIT AUTHORITY
CONTRACT NUMPER IFOOI2
FIB NORTH INFOUND
VASHINGTON, C.C.
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WEEK	CUMULATIVE FEET	OCWN HOURS Correction	SOIL CORRECTION	SHIELO CORRECTION	EXCAVATING EQUIPMENT CORFECTION	WEEK'S ======= INTEGRATION		CUMULATIVE ========= INTEGRATION		= = = = = = = =	L HOURS ====== Cumulative
1	32.00	1.00	.90	12.19	.68	56.76	51.1.8	56 • 76	51.18	55.00	55.00
2	175.00	1.00	.89	12.19	+6.8	149.66	145.56	206.42	196.74	65.60	120.60
?	284.00	1.00	.90	12.19	.75	IC3.57	103.29	309.99	300.03	77.20	197.80
4	35*.^0	1.02	1 • 0 2	12.19	.75	69.13	69.39	379+12	369+13	49.10	246.90
ĉ	430.00	1.04	.87	12.19	.75	68.06	65.32	447.18	437.15	58.50	306+40
6	466.00	1 + 0 1	.87	12.19	.75	25.04	25.04	472.22	462.18	64.80	376.20
7	52T+CO	1.76	• P C	12.19	.75	40.98	40.97	513.19	503.15	61.50	431.70
9	602.00	1.01	. 8 4	12.19	.75	5 A . 54	58.53	571.73	561.68	82.20	513.90
9	739.00	1.01	• 8 6	12 • 1 9	.75	96.34	96.29	668.07	657.97	92.20	6.06+10
10	s50.00	1.02	• 96	12.19	.75	78.29	78.27	746.26	736.24	67.70	666.80
11	°49.00	1.02	• P 1	12.19	.75	61.84	61.83	808+20	798.07	58.10	724.90
12	075.00	1.12	.87	12.19	.75	19.66	19.66	827.86	817.73	24.50	749.40

WASHINGTON NETROPOLITAN ARFA TRANSIT AUTHORITY CONTRACT NUMERO IFGOI2 FIG SOUTH OUTEOUND WASHINGTON, D.C.

	CUMPLATIVE	DCan HOURS	5011	SHIELC	EXCAVATING EGUIPHENT	WFE # * 5	HOURS	CU-ULATIVE	HOURS	ACTUA	HOUR5
WEEK		CCRRECTION		CORRECTION	CORRECTION	INTEGRITION	SUMMAT10N	INTEGRATION	SUPPETION	WEEKS	CUMULATIVE
1	7.50	1 • 1 2	1.19	12.19	.68	23.70	21.99	23.70	21.99	6.60	6.60
2	24.50	1.05	1.13	12.19	•68	37.98	37.51	61.69	50.50	25.20	31.00
3	47.50	1.04	1.07	12.19	.68	26.27	26.22	87.96	65.72	18.50	50.30
4	79.00	1.00	.98	12.19	•68	47.92	47.76	135.88	133.48	31.60	81.3C
5	135+00	1.10	. 9 I	12.19	.68	66.94	66.77	202.81	200.24	\$1.50	132.80
ŧ	195.00	1.10	.91	12.19	•68	66.26	66.18	269.07	266.42	57.40	190.20
7	277.00	1.05	.82	12.19	.68	73.58	73.50	342.65	339.92	61.40	251.60
8	35 *. CO	1.13		12.19	.68	72.25	72.21	414.90	412.13	78.60	330.20
9	419.00	1.01	.90	12.19	+66	56.45	56.44	471.35	468.57	59.70	389.90
10	437+50	1.16	.90	12.19	•68	11.13	11.13	482.49	479.70	10.00	399.90
11	440.00	1.18	.94	12.19	.68	18.89	16.99	501.38	498.59	25.70	425.60
12	510.00	1.07	• • 6	12.19	.68	51.El	51.50	552.89	55C+10	62.10	487.70
13	577.00	1.06	.75	12 • 1 9	+68	48.44	48.43	601.33	598.53	68.7C	556.4C
14	596.00	1.18	. 77	12.19	.68	13.60	13.60	614.93	612.13	16.10	572.50
۱ د	631.50	1.11	. 86	12.19	.68	29.45	29.48	644.41	641.61	53.70	626.20
16	734.03	1.13	.90	12.19	•68	63.22	63.21	707.63	704.93	65.50	691.70
17	P04.50	1.01	.90	12.19	•68	76.73	76.72	784.36	781.54	77.70	769.40
1.0	۰Se+40	1.14	•90	12.19	•68	45.34	45.33	829.69	P26.88	52.00	821.40
19	950.50	1.06	.79	12.19	.66	76.59	70.58	900.29	897.46	68.50	P99.90
20	1095.00	1.01	. 81	12.19	•68	81.71	81.70	982.00	979.16	126.80	1016.75

WASHINGTON WETROPOLITAN AREA TRANSIT AUTHORITY COVTRACT NUMBER IFODI2 FIA SLUTH CUTADUNO WASHINGTON, O.C.

VEEN	CUNVLATIVE FEET	OOWN HOURS Correction	501L COPRECTION	5H1ELO CORRECTION	EXCAVATING EDUIPMENT CORRECTION	WEEK*5		CUMULATIV			AL HOURS
21	1200.00	1.07	• 8 1	12.19	.68	83.85	83.84	1065.84	1063.00	86.30	1103.00
22	1704.00	1.04	. P4	12.19	. 68	64.79	64.78	1130.63	1127.78	66.50	1169.50
5.	1454.00	1.78	. 97	12.19	+68	69.28	69.28	1199.91	1197.06	69.73	1238+20
24	1520.50	1 • 0 3	.87	12.19	.68	83.70	83.70	1283.62	1280.76	63.40	1321.67
25	1655.00	1.02	.85	12.19	•68	82.01	82.00	1365.62	1367.76	84.70	1476.30

WAYMINGTON RETPOPOLITAN AREA TEANSIT AUTHORITY Contract Number 160612 F19 South Infound Ashington, D.C.

	CUMULATIVE	DOWN HOURS	SCIL	SHIELO	EXCAVATING EGUIPMENT	WEEK'S	HOURS	CUPULATIV	E HOUPS	ACTUA	LHOURS
WEEK			CORRECTION	CORRECTION	CORRECTION	INTEGRATION	SUMMATION	INTEGRATION	SUMMATICN	WEEKS	CUMULATIVE
1	77.00	1.00	• * 1	12.19	.68	93.73	86.90	93.73	86.90	64.CO	64.00
7	130.00	1.10	. 77	12.19	.68	69.37	69.11	163.11	156.01	73.90	1 7 . 90
3	2500	1.00	.76	12.19	. 6 8	93.54	93.29	256.69	249.30	62.00	219.90
4	394.00	1.01	.81	12.19	.68	116.91	118.68	*75.59	367.98	76.13	296.00
4	560.00	1.00	• ^p 2	12.19	.68	129.02	128.88	504.62	496.86	85.6C	391.60
6	661.00	1.01	.76	12.19	.66	63.11	63.10	567.73	~59. 96	54.40	476.00
7	807.00	1.01	• B Č	12.19	.66	97.54	97.50	665.26	657.46	87.00	519.00
e	964.00	1.01	. R G	12.19	.6.8	108.43	108.39	773.69	765.85	89.20	6 18.20
9	1114.00	1.00	. 70	12.19	.68	95.60	95.5A	P69.29	861.44	97.00	775.20
10	1247.00	1.00	• R 1	12.19	. 4 8	84.71	84.70	954.01	946.14	91.00	7°6.20
11	1376-00	1.01	• 9.1	12.19	.68	81.19	81.18	1035.20	1027.32	80.30	876.5C
12	148 - • 00	1.09	• 87	12.10	• F P	77.08	77.98	1113.10	110 .30	73.40	949.92
13	1 * 8 *.00	1.04	. 94	12.19	. + 6	63.13	63.1?	1176.31	I168.43	7:.30	1020.20
14	1654.00	1.92	.84	12.19	.68	45.61	45.51	1221.92	1214.04	62.30	1082.50

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WASHINGION HETROPOLITAN AREA TRANSII AUTHORITY
CONTPACI NUMBER 100001
C-9 SOUTH INBOUND
WASHINGION, O.C.
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WEEK	CUMPLATIVE FEET	OOWN HOURS Correction	SOIL CORRECTION	SH1ELO CORRECTION	EXCAVATINE ECUIPMENT CORRECTION		S HOURS	CUMULATIV		=======	L HOURS CUMULATIVE
1	2°.00	1.02	.75	11.40	• 8 ž	72.81	65.98	72.81	65.08	94.75	94.75
2	112.90	1.04	. 7 5	11.40	.82	143.36	143.61	216.17	206.49	105.00	199.75
3	217.90	1.04	• 8 2	I1.40	• 8 2	157.47	156.71	373.65	363.20	111.33	311.08
4	307.90	1.09	.79	11.40	. 8 2	112.70	112.57	486.35	475.77	106.00	417.00
5	37 . 90	1.07	.74	11.43	. 92	91.17	91.11	577.51	566.F8	97.00	10.08
6	501.90	1.07	.75	11.40	• 9 2	137.93	137.90	715.44	704.68	110.00	F20+08
7	637.90	1.08	.75	11.40	.82	114.77	114.72	830.21	819.41	110.00	7 °C.CP
8	590.90	1.00	• 7 5	11.40	• B 2	88.42	88.40	918.63	937.81	107.00	F 77.DF
ç	724.90	1.12	.75	11.40	• B 2	26.40	26.40	945.04	934.21	30.00	°67.LF

Appendix A-3 (continued)

A-55 / A-56

Appendix A-4

Total downtime hours for each data set of each tunnel are calculated from equation (6.4).

~	A	Y		A	4	ε	A		ĸ	٨ د	1	Q		7	۰,	8	s	1	1		0	1	5	тн	1	с	τ	
С	0	N	ī	R	۵	С	1		N	U١	18	Ε	R		1 1	10	0	3	1									
w	R		T	υ	N	N	Ε	ι		-	Z	4	Ţ	н	1	10		R	۵	N	D	A	L	L.	5	1	REE	T.
s	A	Ν		F	R	٨	N	r	1	s (: 0	١.		С	A L	. 1	F	0	R	Ņ	1	A						

	CUMULATIVE	SOIL	CUIPMENT/ DISTANCE		ULATED HOURS		ACTUAL Down Hours	
ыΕΕΚ	FEET		CORRECTION		CUMULATIVE	WEEK *5	CUMULATIVE	
1	15.00	2.21	22.18	3.31	3.31	•00	• 30	
2	47.50	2 • 21	22.15	7.16	10.46	7.50	7.50	
3	735+00	2 • 2 1	21.98	40.97	51.43	10.50	18.00	
4	₹32.50	2 + 2 1	21.65	20.99	72+42	79.00	97.00	
5	5 2.50	2 • 4 2	21.17	50.70	123.12	9.00	106.00	
6	00.084	2 • 4 2	20.54	28.50	151.62	22.00	128.00	
7	P25+00	2 + 8 5	19.97	37.20	188.82	66.50	194.50	
8	1085.00	2.85	19+04	63.62	252.44	26.00	220.50	
ç,	1777.50	2 • 6 1	17.68	60.85	313.29	26.50	247.00	
10	1 * 0 2 • 50	2.61	16.62	24.45	337.73	36.00	283.00	
11	1457.50	2.6I	15.91	29.02	366.75	43+00	326.00	
12	1 • 50 • 00	2.61	15.05	34.08	400.84	30.00	356.00	
13	1960.00	3.21	14.32	22.80	423.64	69+50	425.50	
14	2050.00	3 . 2 1	13.85	18.05	441.68	8.00	433.50	
15	2 300 + 10	3 • 2 1	13.09	47.38	489.06	33.50	467.00	
16	2557.50	3 - 2 1	12.04	44.89	533.95	36.00	505.00	
17	2 * 5 7 . 50	3 . 2 1	11.02	47.88	581.84	25+00	530.00	
18	3102.50	2 + 8 4	10.18	31 • 92	613.76	20.00	550.00	
19	3740+00	2.84	9.55	29.03	642.79	31.50	581.50	
20	3597.50	7.47	9.03	78.17	720.95	26.50	600.00	

GAY AREA RAPID TRANSIT DISTRICT CONTRACI NUMBER IMOD31 MR TUNNEL - 24TH TO RANDALL STREET SAN FRANCISCO, CALIFORNIA

WEEK	CUMHLAI1VF FEET	SOIL	OUIPMENT/ DISTANCE CORRECTION	DOWN	ULATEO HOURS CUMULAIIVE	00 9 1	CTUAL HOURS CUMULATIVE
21	3955.70	2.84	8.61	28.40	749.35	25.50	633.50
22	4102.50	2.64	8.34	26.43	775.78	28.50	662.00
2 र	4 797.50	2 + 8 4	8.22	20.52	796.30	37.00	699.00
24	4745.00	2 . 84	8.20	4.98	801.28	79.00	778.00
25	4425+03	3.85	8.20	11.38	812+66	16.50	794.50

Appendix A-4. Calculation of Downtime Hours.

BAY AREA RAPIO TRANSIT DISTRICT Contract Number 1m0031 ML Tunnel - 24th To Randall Street San Francisco, California

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	CUMULATIVE	5011	DU IPMENT/		JLATEO HOURS		TUAL
WEEX	FEET		CORRECTION		CUMULATIVE	WEEK 'S	CUMULATIVE
1	20.00	2.21	22.18	4.4]	4.41	F.50	6.50
7	52.50	2.21	22.15	7.16	11.57	6+50	13.00
3	175.00	2.21	22.03	26.83	38.39	44.50	57.50
4	735.00	2.21	21.72	34.56	72.95	31.00	A8.50
5	555.00	2.42	21.16	50.68	123.63	7.00	95.50
6	792.50	2.85	20.30	61.96	185.56	19.50	114.00
7	1162.50	2.85	18.94	90.02	275.60	8.00	122.00
8	1*50.00	2.61	17.55	38.73	314.33	17.50	139.50
9	1487.50	2.61	16.73	27.06	341.40	15.00	154.50
10	1515.50	2.61	16.31	5.28	346.67	110.00	264.50
11	1695.00	2.61	15.78	33.43	389.11	35.57	370.00
17	1 • 70 • 00	2.61	14.91	30.69	410.80	27.00	327.00
13	1 . 35 . 00	3.21	14.33	13.48	424.29	61.00	388+00
14	1067.50	3 . 21	13.98	4.55	420.84	92.50	480.50
15	2162.50	3.21	13.53	34 . 2 9	463.12	54.00	514.50
16	2495.00	3.21	12.44	59.89	523.02	16.50	551.00
17	2577.50	3.21	11.63	13.89	536.91	63.50	614.50
19	2 87.50	3.21	11.11	33.78	570.69	10.00	633.50
19	3780+00	2 • 8 4	10.31	38 • 6 1	669.29	26.50	660.00
20	3265.00	2.84	9.64	25.30	634.65	24.50	684.50

BAY AFFA RAPIO TRANSIT DISTRICT CONTRACT NUMBER IMODSI ML TUNNEL - 24TH TC PANDALL STPEET SAN FRANCISCO, CALIFORNIA

h eek	CUMULATIVE FEET	\$01L	EQUIPMENT/ DISTANCE CORRECTION	CALCULATEO DOWN HOURS WEEK'S CUMULATIV		ACTUAL OOWN HOURS WEEK*S CUMULATIN		
21	3*10.00	2.61	9.17	24.81	659.41	27.50	712.00	
22	3795.00	7.47	P.72	83.56	742.97	25.00	737.00	
23	4120.00	2.64	8.36	34.79	777.76	16.00	753+00	
24	4280.00	2 . 8 4	F . 2 2	16.83	794.59	12.50	765.50	
25	4790.00	3.85	8.20	15.69	e10.23	11.00	776.50	

PAY AREA RAPIO TRANSIT	OISTRICT
CONTRACT NUMBER 180053	
PRIRL TUNNELS	
BERKELEY, CALIFORNIA	

			EQUIPMENT/		ULATEO		TUAL HOUP5
₩ E E K	CUMILATIVE FEET	5°IL CORRECTION	OISTANCE CORRECTION		HDUR5 CUMULATIVE	WEEK *5	CUMULATIVE
1	28.00	2.34	2.44	.52	.52	12.00	12.00
2	90.00	2.38	2.44	1.62	2 • 1 4	.00	12.00
3	163.00	2.38	2.42	1.90	4.04	2.00	14.00
4	212.00	2.38	2.41	1 • 2 7	5 • 3 1	9.00	23+00
5	264.00	2.3°	2.40	1.34	6.65	6.00	29.00
6	20.00	2.39	2.38	1.43	8.08	1.00	30.00
7	*67.00	2.3P	2.37	1.19	9.27	40.00	70.00
я	443.00	2.30	2 + 3 4	1.91	11.18	2.00	72.00
ş	×29.00	2.38	2 • 3 1	2.14	13+32	• C D	72.00
10	616.00	2.38	2.28	2.13	15.45	2.00	74.00
11	712+60	2.30	2.24	2.31	17.75	9.00	83.00
12	771.00	2.38	2.20	1.40	19+15	2+00	۰،00
13	P62.00	2.38	2.17	2.12	21.27	1.00	P8.JO
14	044.00	2.38	2.12	1.87	23.14	7.00	95.30
15	1916.00	1.31	2.08	.88	24.02	21.00	116.00
16	1799.00	1.31	2.04	1.00	25.02	1.00	117.00
17	1157.00	1.31	2.90	•68	25.70	2.00	119.00
18	1725.00	1.31	1.97	. 0	26.50	• 0 0	119.00
19	1290+90	1.52	1.93	.86	27.36	.00	119.00
20	1774.00	1.52	1.89	1.09	28.45	1.00	120.00
2.0							

RAY AREA RAPIO TPANSIT DISTRICT Contract number 180053 pr/rl tunnels Berkeley, california

	CUMULATIVE		OUIPHENT/ 015tance		ULATEO HOURS	A C DOWN	TUAL
₩ E E K	FEET	501L CORPECTION	CORRECTION		CUMULATIVE	WEEK *5	CUMULATIVE
21	1459.00	1.52	1.84	1.07	29.52	1.00	
		1.52					121.00
2.2	1474.00	1.52	1.81	.19	29.71	•00	121.00
23	1479.00	1.52	1.81	.06	29.77	• O C	121.00
24	1 498.0G	5.20	1.77	4.94	34 + 71	5.00	126.00
25	1672.00	5.20	1.72	2.98	37.69	2.00	128.00
26	1010.00	5.20	1.66	5.37	43.06	1.00	129.00
27	1943.00	5.20	1.59	4.95	48.02	8.00	137.30
28	2759.00	5.20	1.53	4.15	52.16	17.00	154.00
29	2199.00	5.20	1.46	4.80	56.96	2.00	156.00
30	2 729.00	5.20	1.40	4.26	61.22	8.00	164.30
31	2 468.00	5 • 2 0	1.36	1.24	62.46	51.00	215.00
32	2462.00	1 • 5 2	1 • 3 3	.86	63.32	3.00	218.00
33	2546.00	1.52	1.29	.74	64.36	4.00	222.00
34	2650.00	1.52	1.26	.89	64.96	1.00	223+00
35	2746.00	1.52	1 • 2 2	.80	65.76	•00	223.00
36	2 * 10 . 00	1.52	1.19	• 5 2	66.28	43.00	266.00
37	2 986.00	1.52	1.16	• 6 2	66.90	2.00	26 A.00
3 M	2903.00	1.52	1.15	.12	67.01	.00	268.00

Appendix A-4 (continued)

PAY AREA RAPIO TOANSIT DISTRICT Contract numbeo isodii Tr tunnel San Francisco, california

	CUMPLATIVE SOIL		CUIPPENT/		ULATEO HOURS	ACTUAL DOWN HOURS		
NEEK	FEET	CORGECTION			CUMULATIVE	WEEK S		
1	47.43	4.17	89.94	16.96	16.96	1.00	1.00	
2	194.73	2.21	29.44	27.67	44.63	3.50	4.58	
3	\$67.97	2.21	30.10	10.70	55.33	3.40	7.96	
4	€66.AS	2.51	20.32	14.48	69.82	3.74	11.72	
ŕ	496.74	7.89	18.99	18.74	88.56	18.55	30.27	
6	°65.96	4.74	27.50	24.12	112.68	16.43	46.70	
7	1116-23	2 • 2 1	26.14	12.62	125.30	12.92	59.62	
Ą	1 3 5 3 . ! 8	2.21	24.54	12.36	137.66	10.10	69.81	
Q	1463.21	4.45	23.32	10.96	148.62	.00	69.81	
17	1 < 1 < • 4 9	7.89	16.18	6.03	154.65	15.25	85.06	
11	1 5 0 . 48	7.89	14.99	3.98	158.63	1.17	°6 • 2 3	

FAY AREA RAPIG TRANSIT DISTRICT Contract number 150011 TL TURNEL SAN FRANCISCO, CALIFORMIA

			GU 1PMENT/		ULATED	ACIUAL		
	CJMULATIVE	SOIL	CISTANCE		HOURS	DOWN	HOURS	
WEEK	FEFT	CORRECTION	CORRECTION	WEEK'S	CUMULATIVE	WEEK'S	CUMULATIVE	
1	44.76	7.89	12.80	20.37	20.37	4.40	4.40	
ş	137.34	3.67	12.75	19.53	39.90	6.83	11.23	
3	309.61	2.21	12.59	21.56	61.47	1.91	13.14	
4	469.43	2.21	6.33	10.06	71.53	1.00	14.14	
٢	629.31	2.51	6.17	11.14	82.67	1.75	15.89	
6	"26.F9	2.51	5.96	13.28	95.95	6.80	22.77	
7	1054.04	2.21	5.67	12.82	108.76	14.91	37.68	
٩	1751.41	2.94	۲.34	15.50	124.34	13.40	51.08	
ç	1451.36	3 . 6 7	4.69	13.19	137.53	26.06	77.14	
13	1-16.24	7.85	7.29	16.83	154.35	1.00	78.14	
11	1551+29	7.89	7.18	6.93	163.28	2+97	91.06	

FAY AREA HAPIO TRANSIT DISTRICT Coniract Numper iscoli Sr Tunnel San Francisco, California

		ECUIPMENT/		CALCULATED		ACTUAL DOWN HOUPS	
≓EE R	CUMPLATIVE FEET		CORRECTION		HOURS		CUPULATIVE
1	42.50	2.21	19.03	8.04	8.04	21.83	21.83
2	165.10	3 . 2 3	18.92	33.00	41.84	3.17	25.00
3	-12.63	2 • 2 1	10.78	8.87	50.71	1.59	26.59
4	325.03	3 • 2 3	6.44	10.55	£1.26	10.17	\$6.76
٩	×89.91	3.23	6.32	15.18	76.44	5.67	42.43
6	*54.75	5.30	6.15	24.58	101.02	9.27	51.70
7	P 39 . 32	4.17	5.94	20.60	121.62	14.00	65.70
8	1031.61	2.21	5.68	10.86	132.48	28.69	94.39
9	1236.34	2.26	5.39	11.26	143.74	. 4 2	94.81
10	1415.75	2 • 2 1	5 • 1 1	9.11	152.85	.00	94.81
11	1 5 2 . 94	2 • 2 1	9.24	5.79	158.63	12.50	107.31

BAY AREA RAPIO TRANSIT DISTRICT Contract number 150011 SL Tunnel San Francisco, california

			EQUIPMENT/ SOIL DISTANCE		CALCULATED DOWN HOURS		ACTUAL DOWN HOURS	
WEEK	CUMULATIVE FEET		CORRECTION		CUMULATIVE	NEEK'S	CUMULATIVE	
1	29.93	2.21	114.82	2.02	2.02	.00	•00	
2	109.53	7.89	114.43	19.13	21.15	.50	.50	
3	209.45	7.89	113.60	23.83	44.98	6.75	7.25	
4	326.95	7.89	112.31	27.70	72.68	3.50	10.75	
5	386.93	7.89	111.03	13.98	86.66	8.00	18.75	
6	525.83	7.89	109.39	31.89	118.55	8.75	27.50	
7	639.23	2 • 2 1	107.01	7.12	125.67	9.41	36.91	
8	796.72	2.21	104.16	9.63	135.30	5.75	42.66	
9	851.61	2 • 2 1	101.75	3.28	138.58	4.00	46.66	
10	981.25	2.21	99.54	7.57	146.15	25.42	72.08	
11	1116.09	7.89	96.25	27.24	173.40	22.08	94.16	
12	1295.74	2.21	92.20	9.72	183.12	6.41	100.57	
13	1457.86	2.21	131.41	12.50	195.62	28.89	129.46	
14	1565.19	2.21	84.17	5.30	200.93	5.33	134.79	

BAY AREA RAPIO TRANSIT DISTRICT Contract number 150051a 5L Tunnel - Market Street San Francisco, California

WEEK	CUMULATIVE Feet	50IL	EOUIPNENT/ D15tance Correction	0 O W N	ULATED Hours Cumulative		TUAL HOURS CUMULATIVE
1	85.00	2.85	130.53	5.18	5.18	3.67	3.67
2	152.50	3 • 2 3	129.95	7.55	12.73	17.78	21.45
3	220.00	2 • 5 1	129.16	5.81	18.54	17.14	38.59
4	280.00	2.21	128.29	4.52	23.06	3.58	42+17
5	350.00	2.21	127.28	5.23	28.29	2.08	44.25
6	457.20	2.51	125.71	8.98	37.27	10.17	54.42
7	564.70	2.21	123.56	7.80	45.07	6.32	6D • 7 4
8	689.70	2.21	120.95	8.87	53.94	11.68	72.42
9	729.70	2.21	118+94	2.79	56.74	7.01	79.43

FAY AREA RAPID TRANSIT Contract number 150051a SR Tunnel - Markft Street SAN FRANCISCO, CALIFORNIA

NEEK	CUMULATIVE FEET	SCIL	EQUIPMENT/ DISTANCE CORRECTION	DOWN	ULATED HOURS CUMULATIVE	DOWN	TUAL HOURS CUMULATIVE
1	27.46	3.67	31 9 . 7 3	7.03	7.03	.00	.00
2	94.96	4.17	318.85	23.89	30.92	7.50	7.50
3	137 - 46	6 • 1 2	317.56	21.96	52.88	10.33	17-83
4	190.24	2.21	73.02	2.26	55.1,4	2.33	2D.16
ŕ	>77.4 6	5 • 3 8	72.50	9.06	64.20	9.15	29.31
6	² 84 • 96	4.17	71.64	8.55	72.75	17.28	46.59
7	477.46	2.21	70.62	3.83	76.58	5.42	52.01
۴	564.96	2.21	69.58	3.57	80.15	7.34	59.35
9	687.46	3 . 2 ?	68.24	7.19	87.34	9.17	68.52
10	709.96	3.23	67.25	1.30	88.65	11.75	80.27

UPPER SALT CREEK N1 CD%TRACT NUMRER 68-4C4-25 CH1CAGC, 1LLINO15

	CUNILATIVE	STIL E	DI STANCE		ULATED HOURS	DOWN I	
WEEK	FEET	CORRECTION	CORRECTION	WEEK*5	CUMULATIVE	WEEK'S	CUPULATIVE
1	24.00	10.46	4.26	4.81	4.81	8.00	9.00
2	38.00	9.46	4.25	2.54	7 . 3 5	26.00	36.00
3	130.00	9.46	4.24	16.62	23.97	6.00	42.00
4	210.00	3.58	4 • 2 1	5.44	29.41	24.00	66.00
¢	714.00	3.58	4.10	.27	29.68	5.00	71.00
6	242.00	12.82	4.18	6.76	36.44	36.00	107.00
7	265.00	2.65	4.17	1.14	37.58	12.00	119.00
8	284.00	2.65	4.16	.94	38.53	A.0C	127.00
9	*58+00	2.99	4.14	4.12	42.65	20.00	147.00
10	410.CO	3.50	4.10	3.44	46.09	21.00	168.00
11	€90+CO	3.58	4.03	11.70	57.79	8.00	176.00
17	07.86*	3.59	۲.92	7.34	65.12	27.00	100.00
13	638.00	3.58	2.82	8 • 1 4	73.27	18.00	217.00
14	1194.00	3.63	3.65	15.25	88.52	12.00	229.30
1 c	1762.00	2.60	3.40	10.66	99.18	12.00	241.00
16	1466.00	3.38	3.22	5.10	104.25	27.50	268.50
17	1410+00	29+37	3.14	18.31	122.58	29.50	298.00
16	1530.00	21.68	3.11	6.08	128.66	4.00	302.00
19	1 86.00	9.78	3.08	7.59	136.26	F.50	310.50
zo	1668.00	12.47	3.01	13.67	150.13	13.00	323.50

UPPER SALT CREEK #1 CONTPACT NUMMER 68-404-25 CHICAGC, 1LL1NC15

			OU IPHENT/		ULATED		TUAL
WEEK	CUMULATIVE FEET	SCIL CORRECTION	DISTANCE CORRECTION		HOUR5 CUMULATIVE	WEEK *5	CUMULATIVE
21	1 * 2 2 . 00	5.11	2.90	10.26	160.40	11.50	335.00
22	2002.00	3.17	2.74	7.06	167.46	13.00	348.00
27	2075.60	12.75	2.63	11.03	178.49	19.00	362.00
24	2~39.00	10.26	2.53	19.17	197.66	7.00	369.00
25	2774.00	10.26	2.45	3.96	201.62	25.00	394.00
26	2*38.00	9.46	2.41	6.56	208.18	21.00	415.00
27	2 * 1 * • 00	9.46	2+31	17.26	225.44	16.00	431.00
2 د	2 * 3 3 • 00	7.67	2.14	24.28	249.72	5.00	436.00
23	3041.00	3.58	1.98	6.64	256.36	11.00	4*7.00
30	3749.00	2.63	1.85	6.74	263.10	11.00	458.00
31	3425.00	12.59	1.73	27.02	290.12	13.00	471.00
32	3 - 5 3 - 00	2.55	1.65	4.32	294.44	19.00	490.00
33	4729.00	2.64	1.59	7.12	301.56	.00	490.00
34	4445.00	4.99	1.57	7.62	309.18	16.00	506.00
35	4725.00	10.15	1.59	20.35	329.53	6.00	512.00
34.	4 • 7 7 . (2)	9.41	1.63	10.49	340.02	14.50	526.50
37	5177.00	2.65	1.70	6.08	346.11	11.00	537.50
3 h	5461.00	2 • 6 5	1.86	6.74	352.85	13.00	550.50
39	5 8 8 1 . 00	2.65	2.17	10.34	363.18	5.00	555.50
4 ^	6167.0	9.46	2.66	32.45	395.64	16.50	572.00

UPPER SALT CREEK #1 Contract number 68-404-25 Chicago, illinois

	CUMPLATIVE	SDIL	DUIPMENT/ DISTANCE		HOURS	ACTUAL DOWN HOURS	
WEEK	FEET	CORRECTION	CORRECTION	WEEK*S	CUMULATIVE	₩EEK *S	CUMULATIVE
41	6745.00	9.21	3+17	23.37	419.01	19.00	501.00
42	6445.00	9.21	3.56	14.77	433.77	20.00	611.00
43	6493.00	9.21	3 • 8 1	7.58	441.35	23.00	634.00
44	6=10*00	9.78	3.94	4.52	445.87	27.00	661.00
45	6*65.00	9 • 2 1	4.08	7.78	453.65	20.00	6 R 1 + D D
46	6663.00	9 • 2 1	4.38	17.81	471.46	15.00	696.00
47	6 P 2 5 + 00	9 • 2 1	5.02	33.75	505+21	12.00	708.00
48	7073.00	2.57	6.36	18.30	523.51	6.00	714.00

UPPER SALT CREEK #2 CDNTPACT NUMBER 68-405-25 CHICAGO, ILLINOIS

	CUMULATIVE	EQUIPMENT/ SOIL DISTANCE		CALCULATED DDWN HOURS		ACTUAL DOWN HOURS	
ж E S N	FEET	CORPECTION					CUMULATIVE
1	46.00	2.65	+ 3.1	+17	+17	.00	•00
2	69.00	2.65	.31	• C 8	• 2 5	• 0 0	•00
3	172.00	2.65	+ ? 1	•36	.63	16.00	16.00
4	°65.00	2.6"	4.40	11.16	11.79	5.00	21.00
5	°63.00	2.81	4 • 1 2	30.16	41.96	P . D D	29.00
	1122.00	2 • 6 5	3 • 78	7.16	49.12	26 • D C	55.00
7	1671.00	16 • 1 4	3 • 4 2	136.42	185.54	26.00	81.00
£	1080.00	4.66	3.03	13.86	199.40	28.00	109.00
9	2784.00	2.73	2.69	16.36	215.76	17.00	126.00
10	3-06.00	2.55	2 . 2 5	16.04	231.80	9.00	135.00
11	3110.00	1.57	2.02	1.49	233.29	13.00	148.00
12	3680.00	1.57	1.96	7.52	240.81	5.00	153.00
13	4~91.00	2.90	1 • 7 1	9.18	249.99	17.00	170.00
14	4604.00	2.65	1.66	10.17	260.16	6 ° C C	176.00
1 °	4972.00	11.70	1.72	33.34	293.50	15.00	193.00
16	5717.00	9.46	1. * * 5	26.93	320.42	10.00	203.00

UPPER SALT CREEK #3 Contract Number 68-406-25 Chicago, 11110015

	CUMU 47105		EDU IPMENT/ DI STANCE		ULATEC HOURS		TUAL
WEEK	CUMPLATIVE FEET	SOIL CCRPECTION	COPRECTION		CUMULATIVE	WEEK *5	CUMULATIVE
1	20.00	2.65	• 3 P	.09	.09	30.00	30.00
2	104.00	3.58	5.52	7.49	7.58	12.00	42.00
3	268+00	11.01	2.21	26.CB	33.66	10.00	52.00
4	₹88.00	3 • 5 8	5.38	10.42	44.05	17.00	69.00
5	526.00	3.58	5.28	11.76	55+84	9.00	78.00
6	674.00	2.99	5.14	10.52	66.36	1.00	79.00
7	°42.00	10.05	4.98	36.99	103.34	9.00	88.00
8	1110.00	3.27	4.73	18.69	122.04	4.00	92.00
a	1236.00	10.58	4.49	25.69	147.73	26.00	118.00
1 C	1 7 3 7 . 00	9.33	3.34	15.05	162.77	27.00	145.00
11	1417.00	2.64	3+25	3 • 0 9	165+87	23.00	163.00
12	1 6 8 1 . 00	2.65	3 • 1 3	6.12	171.99	9.50	177.50
13	1781.00	2.65	2.96	7.05	179.04	8.00	185.50
14	1993.00	2.65	2.81	3.75	182.79	12.00	197.50
15	2153.00	2 • 6 5	2.64	8.19	190.99	3.00	200.50
16	2477.00	2.65	2.40	9.27	200.25	•	200.50
17	2729.00	2.65	2.19	6.57	206.82	13.00	213.50
18	3-29.00	4.03	2.01	10.95	217.77	5.50	219.00
19	3709.00	3.18	1.96	7.45	225.22	9.00	228.00
20	3485.00	2.65	1.72	7.72	232.94	2.00	230.00

UPPER SALT CREEK 83 Contract numeer 68-406~25 Chicago, Illino15

CUMPLATIVE		ÉDUIPHENT/ 501L 01STANCE		CALCULATED DOWN HOURS		ACTUAL Odwn Hours	
WEEK	FEET	CORRECTION	CORRECTION	WEEK * 5	CUMULATIVE	WEEK'S	CUMULATIVE
21	3 * 97.00	2.65	1.64	4.14	237.08	16.00	296.00
22	4297.00	2.65	1.59	7.56	244.64	3.00	249.00
23	4665.00	2.65	1.58	5.41	250.05	1.50	250.50
24	4726.00	2.65	1.60	2.69	252.74	16.00	266.50
25	4 * 06 . 00	2.42	1.62	1.41	254.15	25.00	291.50
24	4°74.t0	3.24	1.65	4.05	258.20	8.00	299.50
27	5~66.CD	2.65	1.74	6.06	264.27	3.00	302.50
2 A	5-82.00	2.65	1.93	7.26	271.53	3.50	306.00
2 4	5°38.00	3.31	2.20	8.42	279.95	9.00	315.00

Appendix A-4 (continued)

A-66

WASHINSTON HETROPOLITAN AFFA TRANSIT AUTHORITY CONTRACT NUMEER IFOO21 F2A PENTAGON OUTPOUNO WASHINGTON, O.C.

	CUMPLATIVE	EDUIPMENT/ IVE 501L DISTANCE		CALCULATED Down Hours		ACTUAL Down Hours	
VEEK	FEET		CORRECTION	HEEK*5	CUMULATIVE		CUMULATIVE
1	67.00	5.20	1.65	2.59	2.59	10.01	10.01
2	113.19	5.20	1.65	1.78	4.37	6.72	16.73
2	288.08	7.89	1.63	10.13	14.50	8 + 8 2	25.55
4	*39.50	12.47	1.61	4.65	19.14	5.35	30.90
ē.	s53.44	6 + 2 I	1.56	12.49	31.63	*.67	34.57
6	407.81	8.21	1.54	3.10	34.73	3.16	37.73
7	f10.28	5.20	1.53	.09	34.82	• 2 5	37.98
۵	702.02	16.14	1.52	10 • 1 3	44.95	11.35	49.33
9	*35.57	8.21	1.48	7.33	52.28	16.95	66.28
10	1 797 . 52	8 • 2 1	1.42	13.72	66.01	10.58	76.86
11	1 790.79	6.21	1.31	14.25	80 • 26	14.74	91.60
12	1408.25	8 • 2 1	1.25	. 81	81.07	.58	92+18

WASHINGTON METROPOLITAN AREA TRANSIT AUTHORITY CONTRACT NUMBER IF0021 F2A PENTAGON INEOUND WASHINGTON, D.C.

	CUMPLATIVE	501L	OU 1PMENT/ D1 STANCE		HOURS	AC Down	TUAL
₩Е£К	FEET		CORRECTION		CUMULATIVE	WEEK*5	CUMULATIVE
1	7.50	5.20	1.65	.29	.29	.00	.00
	14.30					.00	.00
2		5.20	1.65	.26	•55		
3	39.26	5.20	1.65	.96	1.52	.89	.89
4	41.68	5.20	1.65	•09	1.61	1.60	2.49
5	58.99	5.20	1.65	.66	2.27	3 • 0 0	5.49
۴	9P.34	5.20	1.65	1.52	3.79	2.80	8.29
7	160.30	5.20	1.64	2.38	6.17	4.50	12.79
p	198.60	5.20	1.63	1.46	7.63	2.80	15.59
9	248.23	5.20	1.63	1.89	9.52	6.82	22.41
1 0	286.30	5 • 2 0	1 • 6 2	1.55	11.07	2.40	24.81
11	736.44	5.20	1.61	1.77	12.85	6.58	31.39
1.7	483.10	7.89	1.59	8 • 2 7	21.12	21.05	~ Z . 4 4
13	672.94	18.09	1.54	23.85	44.97	4 • 🖯 P	56.52
14	139.07	24.50	1.40	27.43	72.40	16.95	73.47
15	009+19	24.50	1.45	11.06	83.47	4.95	78.42
16	1 " 1 3 • 26	16.14	1.42	10.72	94.19	9.73	88 • 15
17	1 ~ 4 0 + 4 3	8.21	1.39	1.40	95.59	1.00	89.15
1 9	1~42.94	8.21	1.79	• 1 3	95.72	2.50	91.65
19	1149.31	6.21	1 • 3 7	5.39	101+11	32 • 4 7	124.12
ΣC	1*19.62	16.14	1 • 3 2	16.30	117.41	9.60	133.72
21	1511+14	16.14	1.25	17.38	134.79	11+10	144.82

WASHINGTON METROPOLITAN AREA TRANSIT AUTHORITY Contract Number 1f0021 F2A Brangth Route Outround Washington, D.C.

	CUMULATIVE	SOIL	EQUIPMENT/ DISTANCE		ULATEO		TUAL
NEEN	FEET		CORRECTION		CUMULATIVE	WEEK'S	
1	65.89	6 • 6 4	1 • 6 5	3.45	3.45	2.42	2.42
2	°C6+52	7.14	1.64	7.20	10.65	18.83	21.25
3	733.84	7.84	1.63	1.57	12.22	1.42	22.67
4	753.76	7.3C	1.62	1.06	13.28	•00	22.67
م	454.60	8.14	1.60	11.89	25.18	12.00	34.67
6	610.77	6 + 8 2	1.55	7.36	32.54	5.83	۹0.50
7	°76.31	7.44	1.49	13.28	45.82	6. " R	47.38
8	1755+24	7.84	1.42	8.95	54.77	24+03	71.11
9	1 76 7 . 17	7.96	1.32	14.84	69.61	12.50	83.61
10	1648.07	7.67	1.21	11.78	81.39	20.92	104.53
11	1 0 1 7 . 8 3	6.14	1.11	10.99	92.38	46+25	144.78
17	2742.44	7.84	1.01	11.55	103.93	17.66	162.44
1 7	2567.02	7.67	.90	10.15	114.08	2.92	165.36
14	2°11.60	4.99	.83	4.54	119.62	16.66	182.02
15	2°63.80	4.07	.79	.76	119.37	11.2 "	193.27
16	2938.20	3.00	.76	•7F	120.15	13.75	207.02

WASHINGTON METROPOLITAN AFFA TPANSIT AUTHORITY CONTRACT NUMREP 1FCO21 F2A BRANTH ROUTE INFOUND WASHINGTON, D.C.

	CUMPLATIVE	SOIL	LOU 1PHENT/ 01 STANCE		ULATEO HOURS		TUAL
WEEK	FEET		CORRECTION	WEEK *S	CUMULATIVE	DOWN WEEK*S	HOURS CUMULATIVE
1	17.31	24.50	1.65	3.16	3.16	2.58	2.58
2	102.04	12.72	1.65	8.01	11.17	10.59	13.17
3	139.31	7.12	1.64	1.96	13.13	R.91	22.08
4	*27.55	8.81	1.62	12.13	25.26	13.00	35.08
5	522.16	5.13	1.58	7.12	32.39	12.25	47.33
6	687.C4	5.18	1.53	5.90	38.29	P + 0 A	55.41
7	993.97	6.05	1.46	12.21	50.49	7.67	63.08
2	1781.46	8.69	1.35	15.23	65.72	9.17	72.25
9	1581.61	13.16	1.24	22.10	87.82	10.75	83.00
10	1679.66	9.90	1.17	5.10	92.92	8.18	91.18
11	1915.98	9 • 5 3	1.11	11.22	104+14	10.67	101.85
12	2139.52	10.13	1.02	10.45	114.59	11.58	113.43
13	2 7 9 1 . 5 7	9.67	• 95	10.40	124.99	7.51	120.94
14	2*60.64	14.84	.88	9.99	134.98	12.42	133.36
15	2595.38	10.02	. 8 6	1.34	136.33	4.34	137 .70
1+	2545.01	9.70	• R 2	9.01	145.34	13.93	151+63
17	2934.97	4.46	• 7 8	1.40	146.74	1.83	153.46

WASHINGTON HETROPOLITAN AREA TRANSIT AUTHORITY CONTRACT NUMRER IF0012 F13 NOPTH OUTBOUND WASHINGTON, D.C.

			CUIPMENT/		ULATED		TUAL
WEEK	CUMULATIVE FEET	SOIL CORRECTION	O15TANCE CORRECTION		HOURS CUMULATIVE		CUMULATIVE
1	18.00	4.86	4.33	1.71	1.71	.00	•00
2	39.00	4.86	4.33	1.99	3.70	6.10	6.10
3	140.00	4.86	4.31	9.53	13.23	1.70	7.80
4	282.00	5.83	4.26	15.89	29.12	16.60	24.40
s	766.00	5.34	4.21	8.50	37.62	17.70	42.10
6	418.00	3.12	4.17	3.05	40.67	2.20	44,30
7	<00.00×	3.39	4.13	5 • 1 7	45.84	8.20	\$2.50
8	605.00	3.85	4.06	7.38	53.23	7.70	60.20
9	F36.00	3.43	4.01	1.92	55.15	12.30	72.50
10	769.00	3.79	3.97	4.94	60.09	3.90	76.40
11	733.00	5.59	3.93	2.37	62.46	8 • 2 0	84.60
17	°00.00	4.29	3.89	S + C 3	67.49	8.70	93.30
13	974.00	4.20	3.83	S • 47	72.97	7.90	101.20
14	°\$0.00	4.78	3.76	6.16	79.13	11.60	112.80
15	.75.00	4.86	3.71	2.03	81.16	.00	112.80

WASHINGTON HETPOPOLITAN AREA TRANSIT AUTHORITY Contract Number 1f0012 F19 North Inbound Washington, O.C.

			CUIPMENT/		ULATEO		TUAL
VEEK	CUMULATIVE FEET	SOIL	OISTANCE CORRECTION		HOUR5 CUMULATIVE		CUMULATIVE
BCC N				PLLN 3	CONCERNIC		00.0004.110
1	32.00	4.68	۹,33	2.92	2 • 92	1.00	1.00
2	175.00	5.01	4.31	13.90	16.82	6.40	7.4C
3	784.00	4.68	1.90	4.36	21.18	3.30	10.70
4	*53,00	7.88	1.88	4.60	25.78	7.40	18.10
s	434.00	6 • 8 9	1.86	4.67	30.45	8.00	26.10
6	466.00	7.38	1.84	1.96	32.40	11.20	37.30
7	×21.00	7.89	1.83	3.57	35.98	7.70	45.00
R	F02.00	7.89	1.81	\$ • 2 0	41.18	3.80	48.80
9	738.CO	7.89	1.77	8.55	49.73	3.30	\$2.10
10	°\$0.00	7.89	1.72	6.86	56.58	3,80	55.90
11	948.30	6 • 3 4	1.68	4.70	61.29	6.4E	62.30
12	\$75.CO	6.54	1.65	1.32	62.60	3 • 0 0	65.30

WASHINGTON METROPOLITAN AREA TRANSIT AUTHORITY Covtract Number 1f0012 Fir South Outbound WASHINGTON, D.C.

	CUMULATIVE	5011	QUIPMENT/		ULATED HOURS		TUAL
MEEK	FEET		CORRECTION		CUMULATIVE	WEEK'S	CUMULATIVE
1	7.50	9.21	4.33	1.35	1.35	9.40	9.40
÷	26.50	8 • 1 3	4.33	3.01	4.36	14.80	24.20
3	42.50	7.17	4.33	2 . 2 4	6.60	5.50	29.70
4	79.00	6.33	4.32	4.50	11.09	2.00	31.70
Ĕ	135.00	4.95	4 • 31	5.37	16.47	12.50	44.20
۴	195.00	4.95	4.28	5.73	22.20	20.10	64.30
7	277.00	3.39	4.25	5,33	27.53	16.10	A0.40
A	*53.00	3.85	4.21	5.55	33.08	24.90	105.30
9	010.CO	4.36	4.17	5.40	38.48	11.80	117.10
17	430.50	4.36	4.15	.94	39.41	6.00	123.10
11	449.00	4.93	4.14	1.70	41.11	5.30	128.40
17	°10.00	4 • 1 3	4.11	4.67	45.78	7.40	135.80
13	*79.CO	3.65	4.07	9.61	50.39	6.90	144.60
34	596.DD	3.85	4.03	1.19	51.58	7.40	152.00
15	631.50	3.05	4.01	2.47	54.05	8.80	160.80
1 e	704.00	4.01	3.97	5.20	59.25	20.00	140.80
17	PC4.5C	4 - 0 1	3.90	7.08	66.33	9.80	190.60
18	•58.00	3.69	3.83	3.41	69.73	18.00	208.60
1¢	°5°.50	3.43	3.76	5.90	75.64	19.00	227.60
20	1005.00	4.47	3.66	9.24	84.88	11.20	234.80

SASHINGTON HETPOPOLITAN AREA TPANSIT AUTHORITY Contract Number Ifooi2 Fis South Outpound Mashington, C.C.

WEEK	CUMULATIVE FLET	501L	EGUIPHENT/ Distance Correction	OOWN	ULATED HOURS CUMULATIVE		TUÁL HOURS CUMULÁTIVE
21	1209.00	4.47	3.54	8.83	93.71	16.20	255.00
2 2	1 * 6 . 00	4.71	3 • 4 3	7.06	100.77	9.50	264.50
2 ?	1404+00	4 - 6 1	7+33	6.78	107.55	17.30	2A1.80
24	1 * 2 9 . 50	4.61	3.22	8.39	115.94	12.10	293.90
25	1659.00	4.88	3.09	8.81	124.75	10.80	304.70

WASHINGTON METPOPOLITAN AREA TRANSIT AUTHORITY CONTPACT NUMBER IFCOI2 FIR SCUIM INMOUND WASHINGTON, D.C.

	CUMPLATIVE	501L	CUIPMENT/ DISIANCE		ULATED HOURS		TUAL
WEER			CORRECTION				CUMULATIVE
1	72.00	4.37	4.33	6.14	6.14	7.50	7.50
2	139.00	4.44	4.31	5.77	11.91	24.10	31.60
?	752.00	3.65	4 • 2 7	7 • 9 3	19.84	5.50	37.IC
4	796.00	3.79	4.21	10.48	30.32	°.9[47.00
د	569.00	3.39	4 • 1 1	10.68	4I.01	1.97	48.90
6	461.00	3.67	4.01	6 • 1 7	47.16	2.1C	51.00
7	F02.00	3.87	1.02	9.53	56.71	5+00	56.00
9	°64.CC	4.08	3.79	11.29	67.99	4.30	60.30
9	1114.CC	3.73	3.64	9.17	77.17	2.00	62.30
10	1247.00	4.47	3.50	9.38	86.55	1.00	63.30
11	1776.00	4.31	3.37	8.45	95.00	3.70	67.00
12	1465.00	4.61	3.26	7.37	102 • 37	14.10	81.10
12	1562.00	4.54	3.15	6.26	10F.63	11.70	92+80
14	1454.00	4.54	3.07	4.52	113.15	4.20	97.00

WASHINGION WETROPOLITAN AREA TPANSIT AUTHORITY CONTRACT NUMBER 10:001 C-9 SOUTH INEOUNO -ASHINGION, O.C.

WEEK	CUMPLATIVE FEET	SOIL	EDU 1PMENT/ (·I STANCE	0.0 ¥ N	ULATEO HOURS		TUAL HOURS
	- 2 2 1	CORRECTION	CORRECTION	WEEK *S	CUMULATIVE	WEEK'S	
1	28.CG	2.65	8.00	2.67	2.67	1.25	1.25
7	112.90	2 • 6 5	7.97	8.67	10.74	12.00	13.25
ŗ	217.90	2 • 8 8	7.91	10.76	21.50	8.17	21+42
٩	100.90	2.76	7.84	8.08	29.58	24.00	45.42
5	378.90	2.65	7.76	7.21	36.79	14.00	59+42
6	501.90	2.65	7.64	11.20	47.99	25.00	R4.42
7	467.90	2.65	7.50	9.47	57.46	20.00	104+42
ġ	K86°00	2 • 6 °.	7.36	8.06	65.53	۶.00	112.42
9	724.90	2.65	7.27	2 • 16	67.69	8.00	120.42

Appendix A-4 (continued)

A-71/A-72

Appendix A-5

The calculated rate of advance data of Appendix A-3 is combined with the downtime estimates of Appendix A-4 to give an estimate of the total tunneling shift hours for each data set of each tunnel. The percent error of the tunnel's cumulative hours relative to the reported hours is shown.

BAY AREA RAPIO TRANSIT DISTRICT FONTRACT NUMPER IMOD31 MR TUNNEL - 24TH TO RANDALL STREET SAN FRANCISCO, CALIFORNIA

8AY AREA RAPID TRANSIT DISTRICT CONTRACT NUMBE® IMDO31 ML TUNNEL - 24TH TO RANDALL STREET SAN FRANCISCO, CALIFORNIA

WEEK	CUPULATIV CALCUL INTEGRATION	ATEO	CUMULATIN Hours- Actual	1 DIF	FERENCE DN SUMMATION	WEEK	CUMULATIV CALCUL INTEGRATION	ATED	CUMULATIN HOURS- Actual	% OIFF	ERENCE In Summation
1	33.46	29.53	8.00	-318.24	-269.10	1	43.66	38.86	38.50	-13+40	94
2	A 3.72	78.99	47.50	-76.24	-66.30	2	92.23	86.91	79.00	-16.75	-10+02
3	270.50	261.10	168.00	-61.01	-55.42	٦	254.00	246.16	199.50	-27.32	-23.39
4	353.22	343.70	288.00	-22+65	-19+34	4	414.34	405.76	319.50	-29.69	-27.00
5	522.56	512.58	409.00	-2P+0P	-25.63	5	593.55	s84.50	439.50	-35.05	-32.99
6	614.53	604.51	486.00	-26.45	-24 + 38	6	782.97	773.69	560.00	-39.82	-38.16
7	721.48	711.42	606.50	-18.96	-17.30	7	1053.30	1043.72	680.00	-54.91	-53.49
ė	903+30	893.10	726.50	-24 . 34	-22.93	8	1176.98	1167.29	757.50	-55.38	-54+10
9	1093.16	1072.86	847.00	-27.88	-26.67	9	1263.36	1253.66	835.50	-5I • 21	-50.05
10	1161.87	1151.56	967.00	-20.15	-19.09	10	1281.48	1271.56	955.50	-34.12	-33.08
11	1256.03	1247.71	1067.00	-15.73	-14.76	11	1393.77	1364.06	1075.00	-29.65	~2*.75
12	1365.13	1354.80	1207.00	-13.10	-12 +7 5	12	1500.12	1490.39	1195.00	-25.53	-24.72
13	1445.22	1434.88	1326.50	-8.95	- * . 1 7	13	1558.45	1548.72	1315.00	~18.51	-17.77
14	1497.56	1487.23	1446.50	-3 • 5 3	-2.82	14	1638.62	1585+61	1435.50	-14.15	=1.7 + 4.6
1 د	1639.96	1629+61	1566.00	-4 .72	-4.De	15	1759.11	1706.09	1555.50	-13.09	-9.68
16	1780.78	1770+40	1686.00	-5.62	-* • 0 1	16	1951.86	1898.81	1676.00	-16-46	-13.29
17	1972.85	1922.46	1906.00	-7.02	-6.45	17	2014.36	1961.31	1798.50	-12.19	-9.23
16	2046.12	2035+72	1926+00	-6.24	- ^c . 7 c	10	2130-45	2077.36	1915.50	-11.22	- 6 . 4 5
19	2154.47	2144.06	2045.50	-5 • 3 3	-4 • 8 2	19	7274.07	2220.99	2036.00	-11.69	-9.09
2 D	2326+95	2316.54	2166.00	-7.43	-6.95	2.0	2374.19	2721+10	2155.50	-10+15	-7.68
21	2434+53	2424.11	2286.50	-6.47	-6.02	21	2420.67	2429.42	2275.00	-9.04	-6.79
22	2537.60	2527.17	2407.00	-5.43	-4.99	22	°679.24	2627.97	2395.00	-11.87	-9.73
23	7618.86	260 ^A .43	2527+00	- 3 • 6 4	~ 3 • 2 2	23	7821.44	2770.16	2515.00	-12.18	-10.15
24	7652.8P	2642.45	2647.00	22	• I 7	24	2891.15	2839.97	2635.50	-9.70	-7.75
25	7697.54	2677.11	2719.50	1.18	1.56	25	7942.57	2891.29	2747.50	-7.10	- ° • 2 3

Appendix A-5. Total Estimated Shift Hours and Percentage of Error.

GAY AREA RAPIO TRANSIT DISTRICT Contract number irooss Rr/Rl tumnels Rerkeley, california

WEEK	CUMULATIVE HOURS Calculated Integration Summation		CUMULATIVE Hours- Actual			
1	153.76	92.52	88.00	-74.72	-* • 1 3	
z	354.05	289.72	208.00	-70.21	-39.29	
3	547.82	482.65	328.00	-67.92	-47.15	
4	680.83	615.55	448.00	-51.97	-37.40	
5	859.19	743.84	568.00	-42.46	-30.96	
6	930.73	865.32	688.00	-35.28	-25.77	
7	1065.33	999.89	808.00	-31.85	-23.75	
9	1216.67	1151.16	929.00	-31.11	-24.05	
9	1380.33	1314.76	1048.00	-31.71	-25.45	
10	1541.25	1975.63	1168.00	-31.96	-26 . 34	
11	1715.14	1649.47	1288.00	-33.16	-29.06	
12	1618.12	1752.44	1364.00	-32.90	-29.10	
13	1972.37	1966.67	1488.00	-32.55	-28.14	
14	2111.20	2045.48	1608.00	-31.29	- 27 . 21	
15	2230.26	2164.54	1728.00	-29.07	-25.26	
16	2349.27	2283.49	1848.00	-27.12	-23.57	
17	7431.97	2366.23	1944.00	-25.10	-21.72	
18	7526·04	2461.69	2040.00	-23.83	-20.67	
19	2626.37	2562.00	2160.00	-21.59	-18.61	
20	754.80	2690.43	2280.0C	-20.82	-18.00	
21	2882.79	2919.42	2400.00	-20.12	-17.43	
22	2905.04	2840.70	2520.00	-15.28	-12.73	
23	2912.49	2848.12	2640.00	-10.32	-7.88	
24	3045.29	2980.90	2760.00	-10.34	- 8 . 0 0	
25	*126.37	3061.98	2840.00	-10.08	-7.82	
26	3274.03	3209.63	2960.00	-10.61	-8.43	
27	7416.46	3352.05	3080.00	-10.92	-8.83	
28	7542.47	3478.06	3200+00	-10.70	- 9.69	
29	36P5+03	3620.61	3320.00	-10.99	-9.05	
30	3817.29	3752.87	3440.00	-10.97	-9.09	
31	3670.99	3806.56	3560.00	-8.74	- 4 . 9 3	
32	3995.57	3931.14	3680.00	-8.58	-6.82	
33	4106.90	4042.47	3800.00	-8.08	-6 • 38	
34	4240.94	4176.51	3920.00	-8.19	-6.54	
35	9363.48	4299.04	4040.00	-8.01	-6.91	
36	9469.17	4404.73	4160.00	-7.43	-5 - 8 8	
37	4568.06	4503.62	4280.00	-6.73	- 5 + 2 2	
38	4586.87	4 * 2 2 . 4 3	4400.00	-4.25	-2.78	

MAY AREA RAPIO TRANSIT DISTRICT CONTRACT NUMBER 150011 TR TUNNEL SAN FRANTISCO, CALIFORNIA

BEEK	CUMULATIV CALCUL 1915GRA7109		CUMULATIV HOURS- Actual	E % DIFFE INTEGRATION	
1	94.94	83.08	64.08	-48.16	-29.65
2	250.66	234.95	182.50	- 37.35	-28.74
3	110.44	393.75	298.66	-37.43	-31.84
4	580.74	563.51	417.99	-38.94	-34.81
5	702.22	684.91	535.98	-31.02	-27.79
6	850.06	832.62	651.78	-30.42	-27.75
7	998.04	980.48	767.06	-30.11	-27.82
c	1142.48	1124.83	885.65	-29.00	-27.01
9	1209.03	1191.37	1004.31	-20.38	-18.63
10	1247.76	1230.10	1117.18	-11.69	-10.11
11	1286.28	1268.62	1222.30	-5.23	-3,79

GAY AREA RAPIO TRANSIT DISTRICT Contract number 157011 TL TUNNEL San Francisco, california

	CUMULATIV	E HOURS	CUMULATIV			
	CALCUL	A T E O	HOUR5-	% OIFFE	IFFERENCE	
WEEK	INTEGRATION		ACTUAL	INTEGRATION	SUMMATION	
1	92.09	82.61	102.25	9.94	19.21	
2	202.08	191.00	221.75	8.87	13.87	
3	353.30	340.66	338.25	-4.36	71	
4	533.24	520.45	432.25	-23.36	-20.40	
5	696.98	683.99	527.58	-32.11	-29.65	
6	889.14	P75.94	646.16	-37.60	-35.56	
7	1093.64	1080.26	763.66	-43.2I	-41.46	
8	1290.64	1277.15	882.16	-46.30	-44.78	
9	1442.07	1428.55	1000.46	-44.14	-42.79	
10	1505.37	1491.05	1117.96	-34.65	-33.44	
11	1557.81	1544.28	1196.54	-30.19	-29.06	

PAY AREA RAPIO TRANSIT DISTRICT Contract number Isodii Sr Tunnel San Francisco, California

	CUMULATIVE HOURS CALCULATED		CUMULATIVE Hours- & Difference		
WEEK	INTEGRATION	SUMMATION	ACTUAL		N SUMMATION
1	91.60	81.06	77.25	-18.57	-4.93
2	243.20	229.88	193.50	-25.69	-14.80
3	290.26	276.90	239.33	-21.28	-15.70
4	415.76	402.10	334.33	-24.36	-20.27
5	582.00	567.96	453.00	-28.45	-25.36
6	736.77	722.52	571.16	-28.99	-26.50
7	892.12	877.79	685.99	-30.05	-27.96
8	1046+34	1031.92	805.91	-29.83	-28.04
٩	1191.86	1177.37	923.33	-29.08	-27.51
10	1313.55	1299.03	1018.75	-28.94	-27.51
11	1472.75	1458.22	1115.33	-32.05	-30.74

Appendix A-5 (continued)

A-76

EAY AREA RAPIO TPANSIT OISTRICT Contract numper 150011 SL TUNNEL SAN FRANCISCO, CALIFORNIA

UPPER SALT CREEK B1 Contract Number 68-404-25 Chicago, illinois

	CUMULATIVE HOURS CALCULATED		CUMULATIV HOURS-	RENCE	
WEEK	INTEGRATION	SUMMATION	ACTUAL	1NTEGRATION	SUMMATION
1	77.75	65.82	109.33	28.89	39.80
2	202.23	187.58	225.99	10.51	17.00
3	328.71	313.30	344.91	4.70	9.16
4	455.76	439.99	460.03	1.10	4.52
ė	515.55	499.76	526.50	2.08	5.08
6	646.25	630.29	643.75	~0.39	2.09
7	729.48	713.47	734.73	0.66	2.84
6	834.35	818.26	845.66	1.34	3.24
9	870.26	854.16	938.56	7.28	8.99
10	951.38	935.24	1056.06	9.91	11.44
11	1066.42	1050.26	1176.56	9.36	10.73
12	1168.36	1152.16	1295.06	9.78	11.03
13	1257.38	1241.16	1407.90	10.69	11.84
14	1350.79	1334.57	1488.06	9.22	10.31

-BY AREA RAPIO TRANSIT DISTRICT CONTRACT NUMBER ISCOSIA SL TUNNEL - MAPKFT STRFET SAN FRANCISCO, CALIFORNIA

	C ALC!!L		CUMULATIV HOUPS-	E % DIFFE	RENCE
₩8.5 K	INTEGRATION	SUMMATION	ACTUAL	INTEGRATION	
1	285.14	135.57	116.03	-145.75	-16.84
2	430.72	280.31	227.89	-89.00	-23.00
٦	553.18	402.48	341.47	-62.00	-17.87
4	645.19	494.40	427.41	-52.38	-16.77
r	739.65	588.78	504.09	-46.47	~16.59
4	877.63	726.59	621.19	-41.28	-16.97
7	1002.85	851.71	737.61	-35.96	-15.47
~	1154.33	1003.09	P52.78	-35.36	-17.63
9	1232.30	1081.06	909.29	-35.53	-18.90

PAY AREA RAPID TPANSIT Coutract Number Iscoria SR Tunnel - Magkey Street San Francisco, Califernta

CUPULATIVE HOURS

нЕЕК	CALCUL	ATED	CUMULATIV HOURS- ACTUAL	ERENCF N SUPMATION	
1	74.76	50.54	66.00	-13.27	23.42
2	179.52	153.15	183.75	2.30	16.65
7	247.24	220.76	246.42	-0.33	10.44
4	327.71	301.06	323.42	-1.33	6.91
¢	437.10	410.19	439.26	0.49	6.62
1.	563.74	536.58	557.16	-1.18	3.70
,	657.86	630.61	640.85	-2.65	1.60
ы	747.58	720.29	721.45	-3.62	0.16
9	859.73	832.36	A 36 - 14	2 32	0.45
10	894.70	867.33	P8".64	-1.02	2.07

VEEK	CUMULATIV Calcul Integration		CUMULATIV HOURS- ACTUAL	% OIFF	ERENCE N SUMMATION
1	33.41	28.91	33.50	. 28	19.01
2	46.21	41.57	77.50	40.37	46.36
3	112.67	106+80	127.50	11.63	16.24
4	146.69	140.69	176.50	16.89	20+29
5	149.42	143.42	184.50	19.02	22.27
6	172.76	166.76	234.50	26.33	28.89
7	183.73	177.72	264.50	30.54	32.81
6	190.96	184.96	282.50	32.40	34 + 5 3
9	219.56	213.54	.32.50	33.97	35.78
10	239.22	233.19	371.50	35 • 6 1	37.23
11	294.56	288.42	419.50	29.78	31.25
1,2	329.83	323.67	469.00	29.52	30.84
13	366.11	359.93	514+00	28.77	29.97
14	436.96	430.71	564.00	22.53	23.63
15	500.50	494.2I	614.00	18.48	19.51
16	531+20	524.91	658.00	19.27	20.23
17	565.72	559.43	699.50	19.13	20.03
1 P	576.53	570.23	715.50	19.42	20.30
19	599.63	692.73	765.50	21.75	22.57
2 ^	633.34	627.05	PI1.50	21.95	22.73
21	677.96	671.66	861.50	21.31	22+04
22	720.67	714.36	911.50	20.94	21.63
2 *	744.48	735.18	959.50	22.41	23.07
24	797.61	791.30	1007.50	20.83	21.46
25	811.11	804.80	1051.50	22.86	27.46
26	831.IR	°24.º7	1095.50	24.13	24.70
27	877.64	F71+32	1142.50	23.18	27.74
26	955.47	949.08	1192.50	19.88	20+41
29	990.03	983.70	1229.50	19.41	19.93
30	1045.67	1039.33	1278.50	I8.21	10.71
31	1106.97	1100+63	1328.50	16.68	17.15
32	T143.47	1137.13	1379.50	17.05	17.51
33	1202.43	1196.07	1423.50	15.53	15.98
34	T240.73	1234.38	1461.50	15.11	I¢.54
35	1304.00	1297.64	1501.50	13.15	13.58
36	1340.0P	1333.72	1539.50	12.95	1 * • 3 7
37	1383.85	1377.48	1587.50	12.83	13+23
3.8	1428.91	1422.55	1637.50	12.74	13.13
39	3486.90	1465.53	1687.50	11.89	12 . 27
4 C	1558.06	1551.69	1737.50	10.33	10.69
41	1609.31	1602.94	1787.50	9.97	10.33
42	1640.78	1634.41	1837.50	10.71	11.05
43	1656.82	1650.45	1885.50	12 • 13	12 • 4 7
44	1667.92	1661.55	1929.50	13.56	13.89
45	1683.42	1677.05	1975.50	14.78	15+11
46	1717.72	1711.35	202*.50	15.11	15.43
47	1776.19	1769.82	2071.50	14 - 26	14.56
49	1831.90	1025.52	2121.50	13.65	13.95

UPPER SALT CREEK #2 CONTRACT NUMPER 68-405-25 CH1C4G0, ILLINDIS

	CALCUL		CUMULATIV	E ¥ DIFFEI	RENCE
WEEK	INTFGRATION		ACTUAL		
1	23.65	19.20	40.00	40.87	50.50
2	30.95	27.08	57.00	45.70	57.49
3	57.57	53.31	103.00	44.10	48.24
4	105.54	100.86	149.00	29.16	32.31
ŝ	206.88	201.14	212.00	2.41	· • 1 2
6	231.81	226.06	252.00	8 • 0 1	10.29
7	417.44	411.55	319.00	-30.86	-29.01
8	453.15	447.25	363.00	-24.84	-23-21
9	511.41	505.47	416.00	-22.94	-21.51
10	575.39	569.40	476.00	-2C.88	-19.62
11	585.89	579.89	494.00	-16.60	-17.39
1 2	636.68	630.67	538+00	-18+34	-17.22
13	673.28	667.26	586.00	-14.89	-13.87
19	717.33	711.30	629.00	-14.04	-17.08
15	776.13	776.09	669.00	-16.01	-1*+11
16	827.84	821.80	703.00	-17.76	-16.90
CONTR	SALT CREEK PACT NUMPER 6 NGDy ILLINDIS	8-4C6-25			

VASHINGTON HETPOPOLITAN AREA TRANSIT AUTHORITY CONTRACT NUMREP IFOO21 F2A PENTAGON DUTROUNC WASHINGTON, P.C.

CUMULATIVE HOURS		CUMULATIVE						
		CALCUL	ATED	HOUPS-	1 01FFF	1 DIFFERENCE		
۲	EEK	INTEGRATION	SUMMATION	ACTUAL	INTEGRATION			
	1	97.26	86.60	88+50	-9.90	7.14		
	2	146.70	135.07	122.50	-19.76	-10+92		
	3	344.49	331.59	215.00	-60.22	-54.23		
	4	398.74	385.84	242.00	-64.77	-59.44		
	٢	577.12	563.69	315.40	-82.92	-79.67		
	6	614.22	600.79	342.00	-79.60	-75.67		
	7	615.61	602.18	349.50	-76.14	-77.30		
	s	683.28	669.83	398.00	-71.68	-68.30		
	9	769.59	756.12	492.50	-56.26	-53.53		
	េ	946.97	935.34	600.50	-58.03	-55.76		
	11	1138.37	1124.61	711.OC	-60.11	-58.17		
	12	1149.32	1135.56	728.50	-57.77	-588		

WASHINGTON HETROPOLITAN APEA TRANSIT AUTHORITY CONTRACT NUMBER 1FCO21 F2A PENTRON INPOUND WASHINSTON, D.C.

						WASH	INSTON, D.C.	CURU			
WEEK	CUMULATI CALCU INTEGRATION	LATED	CUMULATTI HOUPS- ACTUAL	\$ 01F	FERENCF ON SUMMATION	WEFK		VE HOURS LATED	CUMULATI Hours-	1 01F	FERENCE
1	22.68	19.24	40.00	43.3C	51.89			50-641104	ACTUAL	INTEGRATI	ON SUMMATION
2	63.11	58.40	80.0C	21+11	27.00	1	21.27	18.87	9.50	-123.93	-98.68
2	142.39	136.89	120.00	-18.66	-14.08	2	34.53	32.06	17.78	-94.22	-8C.33
4	190.63	175.07	160.00	-12+89	-9.42	ŗ	74.0?	71.06	56+78	-30.36	-25.14
5	218.54	212.93	200.00	-9.27		4	78.31	75.34	66.78	-17.26	-12.82
ь	257.06	251.42			-6.97	5	102.66	99.66	98.28	-4.46	-1.41
7	329.20		223.00	-15.27	-12.75	6	146.65	145.49	139.28	-6.73	-4.46
		323.13	263.00	-25.21	-23.05	7	212.36	209.00	181.78	-16.82	-14.98
8	389+01	161.29	303.00	-28.39	-26.50	e	249.87	246.49	207.28		
9	4 78.98	433.26	343.00	-27.98	-26.31	9	296.15	292.74		-20.55	-10.92
10	480.92	475.19	383.00	-25.57	-24.07	10	331.97		240.78	-23.00	-21.58
11	501.05	₩95.32	423.00	-16.45	-17.1C	11		32 . 55	281.78	-17.81	-16.60
12	536.21	53C+47	463.00	-15.81	-14.57		71.57 د	364.14	326 • 78	-13.71	-12.66
13	576.96	× 71.22	500.00	-15.39	-14.24	12	524.72	\$21.03	427.78	-22.66	-21.80
14	60C+33	594.58	532.00	-12.84	-11.76	13	749.71	745.72	504.28	-48.67	-47.88
15	649.77	644.01	564.00	-15+21	-14.19	14	906.36	901.99	593.28	-52.72	-52.03
16	708.27	702.46	604.00	-17.26	-16.30	1 4	967.37	962.99	642.78	-50.45	-49.62
17	752.89	747.11	644.00	-16.91		16	1033.04	1024.99	714.28	-44.63	- 44 . 06
1.9	609.33	503.54			-16.01	17	1050.56	1046.48	732.78	-43.37	-42.81
19	658.00		684.00	-10.32	-17.48	18	1052.26	1048.16	741.78	-41.86	-41.31
		F52-29	724.00	-18.52	-17.72	19	1122+69	1118.59	837.28	-34.09	-33.60
20	\$15.97	°10.16	764.00	-19 + 89	-19.13	20	1224.83	1220.71	931.78		
ē 1	949.51	°43.70	804.00	-18.10	-17.38	21	1351.74			-31.45	-31.01
22	1007.70	1001.96	844.00	-19.40	-10.72		1551.74	1347.59	1032.28	-30.95	-30.55
23	1548.65	1042.83	884.00	-18.63	-17.97						
24	1070.49	1064.67	924.00	-15.85	-15.22						
25	1063.57	1077.70	964.00	-12.40	-11.79						
26	106.67	1100.05	1004.00	-10.23	-9.65						
27	1147.09	1141.27	1044.00	-9.87							
2 F	1190.05	1185.03	1064.00		-9.32						
29	1226.77	1222.94		-9.86	- • • 32						
		1222.94	1124.00	-9.32	-8 •8 C						

WASHINGTON METROPOLITAN AREA TRANSIT AUTHORITY CONTRACT NUMBER IFUO21 F2A BRAYN ROUTE OUTBOUND WASHINGTON, D.C.

WASHINGTON METPOPOLITAN AREA TRANSIT AUTHORITY CONTRACT NUMEER IFCC12 FIB NOPIH PUTECUNO WASHINGTON, C.C.

WEEN	CUPULATIV CALCUL INTEGRATION	ATED	CUMULATIVE HDU95- ACTUAL	3 DIFFEF INTEGRATION	
1	102.71	90.16	56.50	- 61 . 78	-59.57
2	233.62	219.10	149.00	-56.80	-47.C5
3	256.10	241.58	183+50	-39.57	-31.65
4	271.25	256 + 72	200.00	-35 • 6 2	-28.36
¢	419+18	403.97	274.00	-52.99	-47.43
6	516.42	501.09	328.50	-57.21	-52.54
7	677.59	661.98	422.50	-60.3 0	-56.68
8	778.19	762.53	513.00	-51.69	-48.64
9	943.95	928.14	621.50	-5I.88	-49.34
10	1084.94	1069.07	730.0C	-48.62	-46.45
11	1214 • 71	1198.79	832.50	-45.91	~44.00
12	1357.38	1341+41	916.00	-46 +19	-46.44
13	1494.92	1478.92	989.5C	-51.08	-49.46
- 1.4	1580.76	1564.75	1082.00	-46 +10	-44 • 6 2
15	1600.50	1584.49	1135.50	-4C •95	-39.54
1 ^	1625.54	1609.53	1180.50	-37.70	-36.34

	CUMULATIVE HOUPS CALOULATED		CUMULATIVE HOURS- % DIFFERENCE		
WEEK	INTEGRATION			INTEGRATION	
1	34+65	3?+12	39.00	11.16	17+63
7	66.84	64.15	64.00	20.43	27.63
3	188.32	184+12	160.00	-17.70	-15.08
4	351+11	346.25	256.00	-37.15	-35+25
5	430.59	425.68	348.50	~23.55	-27+14
6	476.19	465.28	392.00	-19.95	-18.69
7	534 + 21	E29+26	478.00	~11.76	-10 +73
8	618.6C	613.64	581.50	-6.38	- 5 . 5 3
9	640.93	635.98	638.50	38	. 39
10	694.33	689.37	705+05	1.51	7.72
11	715 + 84	710.87	755 • C C	5 • 1 9	° • 8 4
12	768.56	763.59	812.00	5 • 3 5	5.96
1 3	825.17	820.20	869.00	5 • C 4	¢.62
14	887.01	882.C4	926.00	4 • 2 1	4.75
15	905.96	900.99	945.00	4 • 1 3	4.66

WASHINGION HETROPOLITAN AREA TRANSIT AUTHORITY CONTRACT NUMBER IFNO21 F2A BRAYCH ROUTE INBOUNO WASHINGION, O.C.

	CUMULATIV CALCUL INTEGRATION	ATEO	CUMULATI HOURS- ACTUAL	1 01F	FERENCE DN SUMMATION	CONT	INGTON METROP Ract Number 1 North Infound	FOC12	TRANSIT AU	THORITY	
WEER	INTERATION	20-MA110~	ACTUAL	INTEGRATI	DN SOMPALION		INSTAN. D.C.				
1	48.25	47 + 6 4	17.50	-175 • 73	-143.68						
2	164.20	154.67	104.00	-57.89	-48.72	HEEK	CUPULATIV CALCUL INTEGRATION	ATED	CUMULATI HOUPS- ACTUAL	1 01FF	FERENCE IN SUMMATION
3	205.09	195.50	139.00	-47.55	-40.65						
	354.53	747.55				1	55.62	54.10	56.00	-6.57	*•38
4	354+53	343.55	237.50	-49.28	-44.65	2	223.24	213.56	128.00	-74.40	-66.85
5	487.10	475.73	336.00	-44.97	-41.59						
6	588.77	577.28	399.50	-47.38	-44.50	3	331 • 17	321.21	20 A + 50	-58.83	-54.06
6	200.11	-11+20	399.50	-47.38	-44.70	4	404.90	394.90	265.00	-52.79	-49.02
7	762.59	750.79	511.00	-49.23	-46.93						
۶	\$24.33	912.38	619.50	-49.21	-47.28	5	477.62	467.59	331.50	-44 .08	-41.05
۴	924.37	412+36	614.50	-49.21	-47.28	6	504.62	494.59	407.50	-23.83	-21.37
9	1097.72	1985.67	728.00	-50.79	-49.13		_				
10	1153.96	1141.91	P01.00	-44.36	-42.56	7	549.17	539.13	476 •7C	-15 - 20	-13+10
10	1123.40	1141.91	-01-00	-44.05	-42.50	٩	612.91	602.86	562.70	-8.92	~7+14
11	1270.26	1258.19	961.50	-40.90	-30.57						-
12	1380.29	1368+20	1010.00	-36.66	-35.47	9	717.80	707.70	658.70	-9.05	~ 7 . 5 2
12	1360.29	1364+20	1010.00	-30.00	- 35 . 4 /	10	802.94	792.82	722.70	-11.10	-9.70
13	1498.13	1486.02	1100.00	-36 • 19	~ 3 K + C 9						
14	1575.10	1562.99	1193.00	-32.03	-31.0I	11	869.49	P59.36	787.20	~1C.45	- 0 . 1 7
14	12/2.10	1002.99	119.400	-32.03	-31+01	1 è	890.46	880.33	814.70	-9.30	06
15	1590.07	1577.96	123* •50	-28.7C	-27.72						
11	1693.15	1681.02	1368.50	-23.72	-22+84						
17	1725.75	1713.63	1421.50	-2I+40	-20.55						

WASHINGTON HETPOFOLITAN ARFA TFANSIT AUTHORITY CONTPACT NUMER IFOLIZ FIR SOUTH OUTBRUND WASHINGTON, C.C.

WASH:	INSTON, C.C.				
• E E K	CUMULATIVE CALCULA 19TEGRATION		CUMULATIVE HOURS- Actual	1 OIFFE INTEGRATION	
1	25.0*	23.34	16.00	-56.55	-45.85
2	66.04	63.86	56.00	-17.94	-14.03
3	94.56	92.32	80.00	-18.20	-15.40
4	146.97	144.57	113.00	-30.06	-27.94
5	219.28	216.71	177.00	-23.89	-22.44
٤	201.27	289.42	254.50	-14.45	-13.41
7	376.18	367.45	332.00	-11.50	-10.68
8	447.9R	445.21	435.50	-2.86	-2.23
٩	509.83	507.05	507.00	56	01
10	521.90	519.12	523.00	.21	.74
11	542.49	539.71	554.00	2.08	2.58
12	598.67	595.88	623.50	3.98	4.43
13	651.72	648.92	701.00	7.03	7.43
14	666.51	663.71	724.50	8.30	8.39
15	698.46	695.66	787.00	11.25	11.61
16	766.88	764.07	872.50	12.11	12.43
17	850.69	847.87	960.00	11.39	11.68
ء 1	809.43	896.61	1030.00	12.68	12.95
1 9	975.92	973.10	1117.50	12.67	17.92
20	1066.80	1064.04	1255.50	15.02	15.25
21	1159.56	1156.71	1358.00	14.6I	14.82
27	1231.40	1228.55	1430.00	14.13	14.33
23	1307.47	1304.61	1520.00	13.98	14.17
24	1399.56	1396.70	1615.50	13.37	13.54
2 4	1490.37	1487.51	1711.00	12.89	13.06

WASHINGTON WETROPOLITAN AREA TRANSIT AUTHOPITY Contract Number 1fCo12 fip South Infour WASHINGTON, D.C.

	CUPULATIV		CUMULATIV	E 1 01FFE	PENCE
WEEK	INTEGRATION		ACTUAL		
1	\$9.87	93.04	71.50	-39.68	-39.12
2	175.07	167.92	169.50	-3.26	.93
3	276.53	269.14	257.00	-7.60	-4.72
4	405.92	398.70	343.00	-18.34	-16.12
r	545.62	537.86	430.50	-26.74	-24.94
6	614.91	607.13	487.00	-24.26	-24.67
7	721.97	714+17	575.00	-25.56	-24.20
p	641.68	833.85	668.50	-25.91	-24.73
9	946.46	938.60	767.50	-23.32	-22.29
10	1043.56	1032.69	859.50	-21.07	-20.15
11	1130.19	1122.32	943.50	-19.79	-18.95
12	1215.55	1207.67	1031.00	-17.90	-17.14
13	1284.93	1277.05	1113.00	-15.45	-14.74
14	1335.07	1327.19	1179.50	-13.19	-12.52

►ASHINSTCN HETOOPOLITAN AREA TRANSIT AUTHORITY CONTRACT NUMPER 100091 D-9 South Infound ¥ASHINGTCN, 0.C.

	CUMULATIV		CUMULATIV		
	CALCUL	ATEP	HOURS-	1 0 IF F	ERENCE
WEEK	INTEGRATION	SUMMATION	ACTUAL	INTEGRATIO	N SUMMATION
1	75.4P	68.55	96.00	21.38	28.59
2	226.91	217.23	213.00	-6.53	-1.98
3	395.15	384.71	332.50	-18.84	-15.70
4	515.93	505.35	462.50	+11.55	-9.27
۴.	614.30	603.67	569.50	-7.87	-6.00
6	763.44	752.68	764.50	-8.37	-6 • 8 4
7	887.67	876.87	834.50	-6.37	-5.06
a	954.16	973.33	949.5C	-3.65	-2.*1
9	1012.73	1001.90	987.5C	-2.55	-1.46

Appendix A-6

The format of the keypunch cards used to record the weekly progress data from which the various equations were derived.

Variable meanings and values assigned are as follows. The dotted line represents the decimal point; the format is 7F10.5.

Variable No.

Description

1	The survey station at the beginning of the week's tunneling.
2	Lineal feet tunneled during the week.
3	Cumulative feet tunneled through the end of the week.
4	Tunneling hours during the week from Ring Logs.
5	Tunneling down hours in week due to shield and its ancillaries' failure.
6	Down hours in week due to excavating equipment; e.g., the rotating wheel and digger arm.
7	Down hours in week due to the conveyor belt.
8	Down hours in week due to muck transportation and/or the bringing in of necessary supplies; e.g., primary lining rings.
9	Down hours in week due to other work causes.
10	Down hours in week due to administrative decision; e.g., a shutdown for surveyor's alignment.
11	Total shift hours in week. Tunneling hours (4) plus down hours $(5 + 6 + 7 + 8 + 9 + 10) = total shift hours.$

Variable No.

Description

Note: In some cases, tunneling did not begin immediately at the beginning of the week's first shift and frequently shutdown earlier than the end of the week's last shift. Where this was known, the interim time was assigned to administrative down hours (10). Where actual week's beginning and end times were unknown, the week's total shift hours were computed between the time for the first shove and the last ring erection.

- 12 Fraction of the face as silt and clay +1.
- 13 Fraction of the face as clay and sand +1.
- 14 Fraction of the face as sand and gravel +1.
- 15 Fraction of the face as cobbles and boulders + 1.
- 16 Fraction of the face as cemented ground +1.
- 17 Fraction of the face as peat and trash + 1.
- 18 Fraction of the face as cohesive ground + 1.

Note: The sum of the fractions logged for variables 12, 13, 14, 15, and 17 should equal 1.

- 19 Average tunnel pressure during the week-psig.
- 20 A measure of the average wetness in the tunnel during the week. Refer to Section 4.2. The range is from 1.0 to 2.0.
- 21 Driver horsepower to cutting wheel or digger arms. These data were not complete and therefore the variable was not used in the equation derivations.
- 22 Total jacking potential of shield in short tons (2000 lb/ton). In some cases, the jacking potential was greater than the ring strength; a relief valve was installed in the hydraulic line to reduce the pressure. The reduced pressure is to be used in calculating the jacking potential tons.

Variable No.	Description
23	Outside diameter of shield - ft.
24	If a rotating wheel excavator is used = 2, otherwise = 1.
25	If an oscillating wheel excavator is used = 2, otherwise = 1. None of the tunnels investigated used this equipment.
26	If a digger arm excavator is used = 2, otherwise = 1.
27	If manual excavation is used = 2, otherwise = 1.
	Note: In some tunnels, intial excavation was manual (2 logged) until the digger arm could be brought to bear. Then, due to the limited radius of the arm, excavation was 50 percent manual (1.5 logged) and 50 percent digger arm (1.5 logged).
28	If a conveyor belt and train are used = 2, otherwise = 1.
29	If a conveyor belt and truck are used = 2, otherwise =1.
30	If a rubber tired mucking truck is used = 2, otherwise = 1.
31	Fraction of the face as non-cohesive ground + 1. (This variable was eliminated as being the converse of variable 18.)
32	Fraction of the face as running ground + 1.
33	If ribs and lagging primary lining is used = 2, otherwise = 1.
34	If concrete pipe lining is jacked into place = 2, otherwise = 1.
36	If it was the last week of tunneling = 1, otherwise = 0. This was an added variable, and it was not practical to redo all the data sets to add a 1 or a 2. A 1 was added to all data sets for just the last week. During the computer data processing, a 1 was added to all number 36 variables so that the 1/2 relation would hold.
38	The tunnel RoA intercept. See Section 5.2.
39	The hours/ft for the shove operation. See Section 4.4.
40	The hours/ft for the ring erection. See Section 4.4.

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Variable No.	Description
41	The hours/ft for the dead time. See Section 4.4.
	Note: The data for variables 39, 40, and 41 were only obtained for tunnels in which the original ring logs were used for tunneling advance rates.
42	The learning curve RoA exponent. See Section 5.2.

TT III	ECONOMI DATA PROCESSING	C FACTORS IN TUNN DOT STUDY	EL CONSTRUCTION	NERAL	100 NO. 11770-100	Tunnel No:
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IIIII	EC DATA PROCES		DOT STUDY KEYPUN	EL CONSTRUCTION CH CODING FORM-GE	NERAL	11770-100 Tunnel Location;	Tunnel No:
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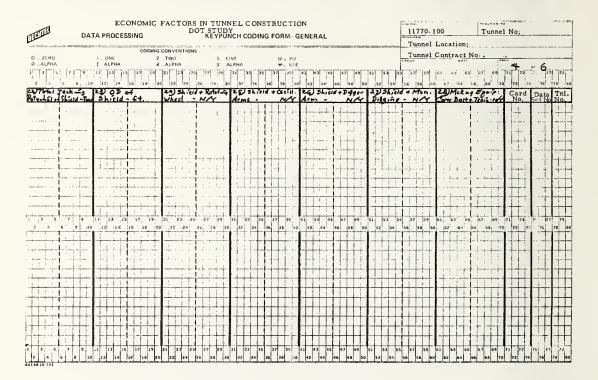
Appendix A-6 Keypunch Forms

فخلات	ECONO DATA PROCESSING	MIC FACTORS IN DOT	STUDY KEYPUNCH CODI	STRUCTION		11770-100	Tunnel No:
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PURSANAM NR.

ECONOMIC EACTORS IN TUNNEL CONSTRUCTION



Appendix A-6 (Continued)

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2(10) ALPIA 31 - 31 - 3 - 4 - 4 - 4 - 4		A PROC 1 ONE 1 ALPHAN 12 13 12 10 12 10	A 		CONVIN T(H) ALPHA 21 22 23 23 24 24 24 24 24 24 24 24 24 24 24 24 24	24 24 24 24 24 24 24 24 25 24	27 26 27 26 27 20 20 20 20 20 20 20 20 20 20 20 20 20	5 - F 29 - 20 - 30 	VE NCH 33 33 33 34		35 36 37 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	16 3 TR U(FDR U +	MG				49	50		7 7 1	11 TT TT COOL 3 57 56 57 57	770 anne anne 55		catio ntra 63	on; ct N 4 65 65		anne 	No;	74 d 50	76 Data 1 No 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Tr NG
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		A PROC 1 DRE 1 ALPHU 1 ALPHU 1 ALPHU 2 DR 2 DR	A 2 55 110 2 55 112 2 15 12 2 15 12 1 1 1 1 1 1 1 1 1 1 1 1 1 1	initial initial S S CODENIA S CODENIA S S <td>CONVIN TWIJ 23 33 32 32 32 32 32 32 32 32 32 32 32</td> <td></td> <td></td> <td>5 - F S - 29 129 29 30 30 30 30 30 30 30 30 30 30</td> <td>NCH</td> <td></td> <td></td> <td>6 3 R U(FDR </td> <td>M G</td> <td></td> <td></td> <td></td> <td>49</td> <td>50</td> <td></td> <td>7 7 1</td> <td>11 TT COOLE 3 57 56 57 56 57 56 57 56 57 56 57 56</td> <td>770 anne anne 55</td> <td>- 100 1 Lc 1 Cc 60 60 60</td> <td>catio ntra 63</td> <td>on; ct N 4 65 65</td> <td></td> <td>anne </td> <td>No;</td> <td>74 d 50</td> <td>76 Data 1 No 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1</td> <td>Tring</td>	CONVIN TWIJ 23 33 32 32 32 32 32 32 32 32 32 32 32			5 - F S - 29 129 29 30 30 30 30 30 30 30 30 30 30	NCH			6 3 R U(FDR 	M G				49	50		7 7 1	11 TT COOLE 3 57 56 57 56 57 56 57 56 57 56 57 56	770 anne anne 55	- 100 1 Lc 1 Cc 60 60 60	catio ntra 63	on; ct N 4 65 65		anne 	No;	74 d 50	76 Data 1 No 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Tring

Appendix A-6 (Continued)

Appendix B

MEXICO CITY TUNNEL DATA

In this appendix, the data submitted by the contractor who conducted the tunneling effort for the Mexico City deep sewer (Ingenieros Civiles Asociados, S.A.) are presented for reference. It is felt that the data herein may be of value either to support or lead to modification of the equations derived in this report. November 11, 1976

Bechtel Corporation Fifty Beal Street San Francisco, California 94119 U.S.A.

Attention: Mr. L.R. Damskey, Long Range Planning

In response to your wishes, we are sending you a report detailing the incidents during the period of excavation in one of the tunnels which we are drilling in the soils of Mexico City.

The adjoined information contains the details requested of us during your stay in this city and constitutes the complement to the data supplied earlier.

We would be grateful if, at the conclusion of your investigations, you would send us a copy of the final result of your studies.

Respectfully,

Engineer Manuel Salvoch Director

7. THE DRAINAGE PLAN

In this plot of land, it was necessary to proceed with a deep reduction of the level of the ground waters, in virtue of the fact that this level was localized at 10.0 m above the crown of the tunnel. Not to dewater this would have presented serious problems of piping in the sandy matter especially. The surface or deep-well type dewatering system covers 60 m ahead of and 40 m behind the face. It was made up of 15 shafts on the average and the capacity of the battery of pumps was 80 to 100 liters/each. The system remained installed and functioning for at least fifteen days previous to when the tunnel would pass through the corresponding zone and was maintained for the necessary time until the primary revetment of the concrete grout would be injected in its periphery.

In Figure B-1 is shown a plan of the line for lowering the level of the water by pump.

In Figure B-2 is presented a cross-section of a typical pump-shaft.

A. DESCRIPTION: CASE HISTORY DATA

1. PROJECT NAME: Federal District Deep Drainage

2. LOCATION: CENTRAL INTERCEPT TUNNEL: SHAFT AREA 11 -SHAFT 13; excavation with shield stage.

3. OWNER: Head Office of Hydraulic Works of the Department of D.F.

4. CONTRACTOR: TUNEL, S.A. de C.V.

5. DATES: START: 9/25/72 COMPLETE: 11/7/73

6. PROJECT SCOPE (INCLUDE ANY APPURTENANT STRUCTURES): The Federal District Deep Drainage System consists of a complex of tunnels which conduct by gravity the sewerage and rain waters from the Mexico Valley basin to a distant river in the state of Hidalgo. It is made up on two ancillary tunnels: the Central Intercept and the East Intercept, which unite in one major tunnel: the Central Emission tunnel (See plan I-2-5 annexed). The present report refers only to the stage of excavation with the shield, in alluvial soils in Mexico City, from the face of shaft 11 toward shaft 13 of the Central Intercept.

7. OWNER FURNISHED MATERIAL AND EQUIPMENT LIST Concrete grout Steel for reinforcement Type II cement Tubing for the conductance of compressed air Rails Metal frames for shoring Transformers for the electric current Electric energy

8. OTHER OWNER SUPPLIED ITEMS (e.g. INSURANCE) Materials laboratory

CASE HISTORY DATA - (CONT.)

B. DESIGN INFORMATION

1.	PLAN AND PROFILE ATTACHED:	YES	NO
2.	TYPICAL SECTION DRAWING ATTACHED:	YES	NO
3.	TEMPORARY LINING DETAILS ATTACHED:	YES	NO
4.	PERMANENT LINING DETAILS ATTACHED:	YES	NO
5.	GEOLOGICAL PROFILE ATTACHED:	YES	NO

6. VERBAL DESCRIPTION OF SOIL CONDITIONS: Alluvial soils characteristic of Mexico City in its section named the transition zone. In this zone there are in general on the surface clay deposits and organic silts, covering very compressible clay volcanic strata of variable thickness interspersed with beds of compact silty sand or clear sand, which rest upon stiff layers in which the predominating substance is sand or silt. The natural water content in the clay formations and in the sandy silt is, on the argillaceous average, 200% and 40% respectively, displaying cohesion (obtained by means of simple cohesion tests) of 0.4 kg/cm² for the former and 0.3 and 0.6 kg/cm² for the latter.

DEWATERING PLAN ATTACHED: YES NO
 GROUND WATER CONDITIONS DESCRIPTION: The normal level of

ground water in the excavation zone of the tunnel is 10 meters above the crown. With the system of well-shafts this was brought down to below the tunnel invert. In spite of this system, in some sites with sandy substance, the use of WELL POINTS became necessary on the periphery of the face of the tunnel in order to channel the water deposits and remove them by pumping through the tunnel to the surface.

9. SITE PREPARATION AND RESTORATION DESCRIPTION: On the surface the CONTRACTOR supplied the land areas required for the installation of the deep well pumping system, since the project was localized for an inundation of Mexico City. Also, in the access shafts he supplied an area for the installations; towers, mantle capstans, offices, workshops, and storage grounds.

10. UNDERPINNING DESCRIPTION

11. UTILITIES DESCRIPTION: The tunnel remains localized at an average depth of 30.0 m. As a result it passes much below the municipal service lines so that there would not be a problem of relocation of the installations.

C. CONSTRUCTION METHODS

DESCRIPTIONS: The entire length considered in the present report was excavated in normal atmospheric pressure conditions. It was carried out by means of an open face shield of 6.42 m external diameter and 6.40 m length, with remote control hydraulic operation. In the rear it has a thrust system made up of 26 hydraulic jacks at 200 ton capacity each, which operate by resting against the primary revetment. In the front the shield bears 17 jacks with a capacity of 120 tons each, whose function is to hold the wood strut which supports the face. By means of pneumatic hammers operating manually the material of the face is loosened and falls to a lower central compartment, whence it is removed by an EIMCO 40 H air mucker of 1 m2 capacity mounted above platforms above the track. Then the convoy is pulled by a locomotive up to the shaft through which the muck is lifted to the surface, and from there is transported to the storage beds in back loader trucks (See Fig. B-3).

TEMPORARY LINING:

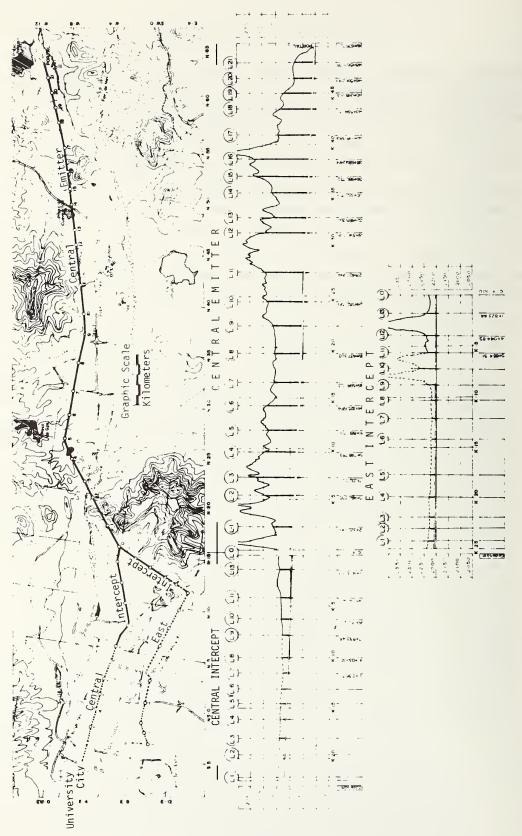
As the shield advances there is put into place the primary revetment, constituted of eleven segments of prefabricated reinforced concrete 1.50 m. long, 0.20 m. thick, and 0.75 cm. wide, which are connected with each other and with the preceding rings by means of screws and nuts, with which they reckon on the necessary cavities and ductile areas. In order to maintain the circular ring, it is propped up with tubular scaffolding equipped with machanical jacks for its adjustment. This support is maintained unit1 the zone is injected.

The segmented ring is set up with the aid of an eractor arm behind the shield's jacket, which has a thickness of 5 cm. Consequently, the advance of the shield leaves a void which is refilled immediately with gravel, applied with a small pneumatic conveyor.

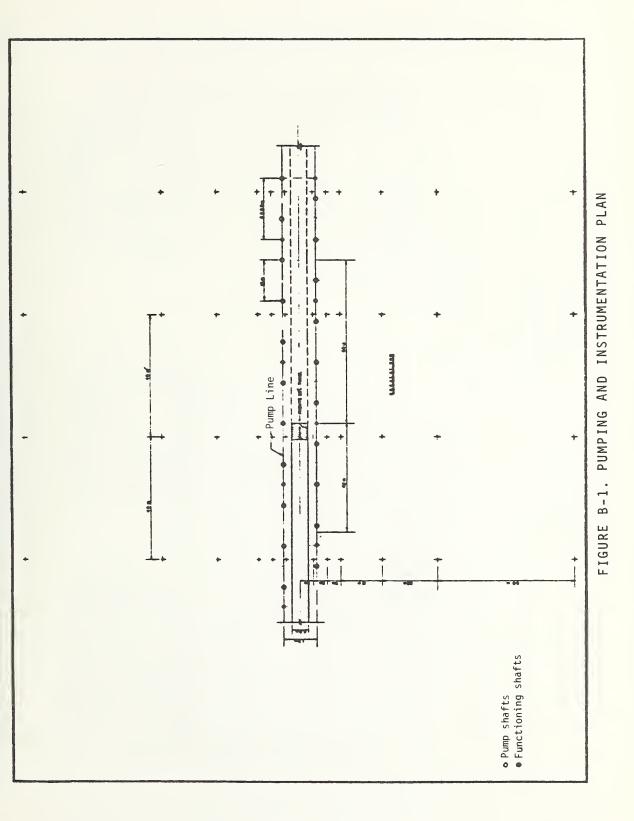
CASE HISTORY DATA - (CONT.)

Ten meters behind the shield there takes place the process of injection of the cement grout in its refill or consolidation stage, later to pass on to the impermeability stage.

FINAL LINING: The tunnel bears a definitive revetment of concrete filtered on the site, maintaining a final surface of 5.00 mts. diameter. To make this a metallic frame formed by 9 telescopic sections 7.32 m. long, each is utilized. See Fig. B-4. The concrete is produced on the surface, lowered down the tunnel by gravity, loaded onto transport carts (See Fig. B-5), carried to the face, unloaded with the transport belt, fed into pneumatic conveyors, pumped, and filtered (See Fig. B-6).



B **-** 8



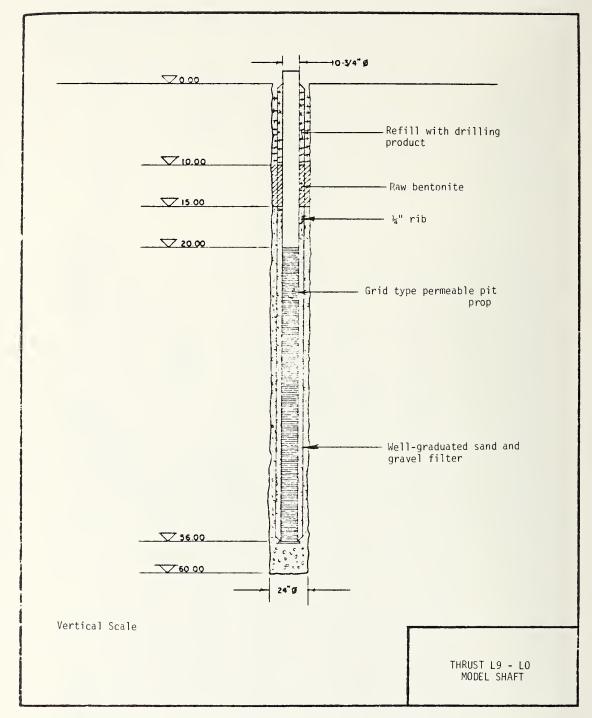
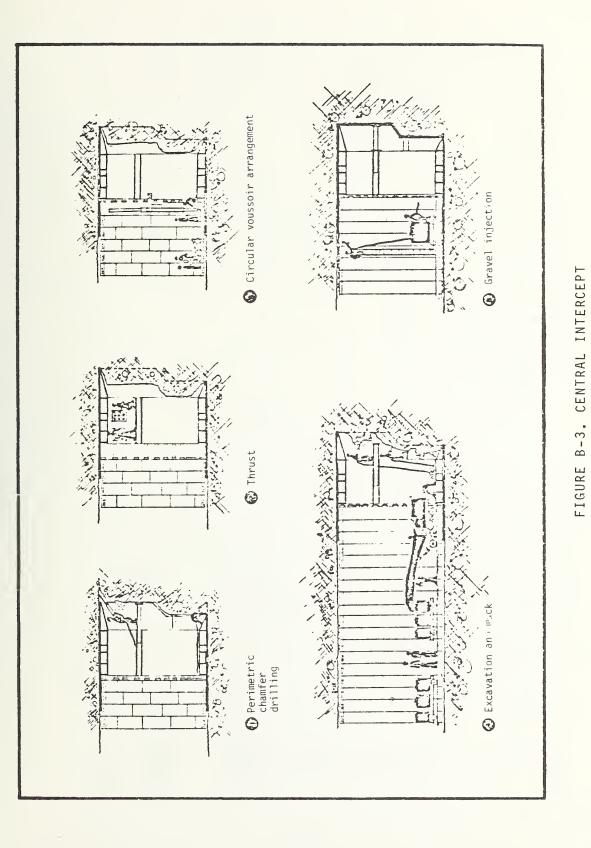
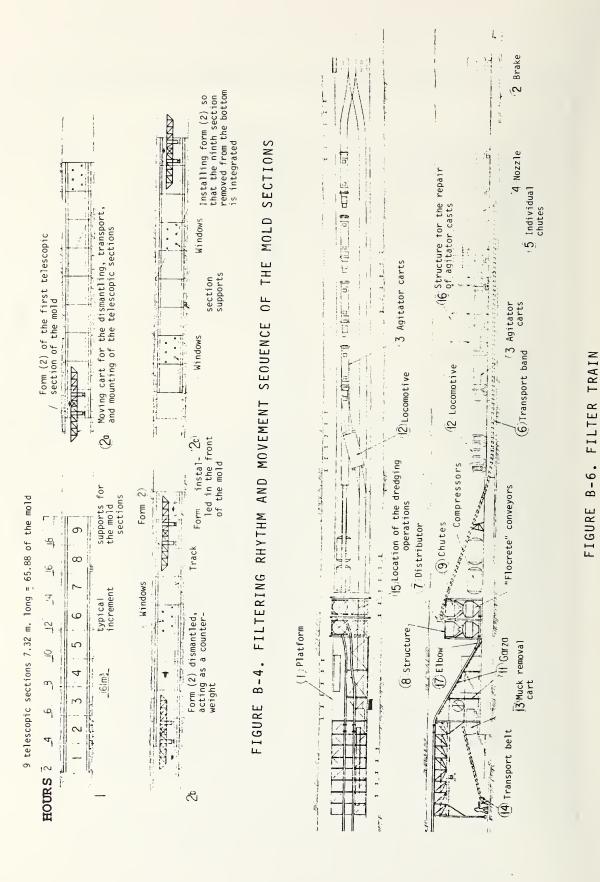


FIGURE B-2. CENTRAL INTERCEPT





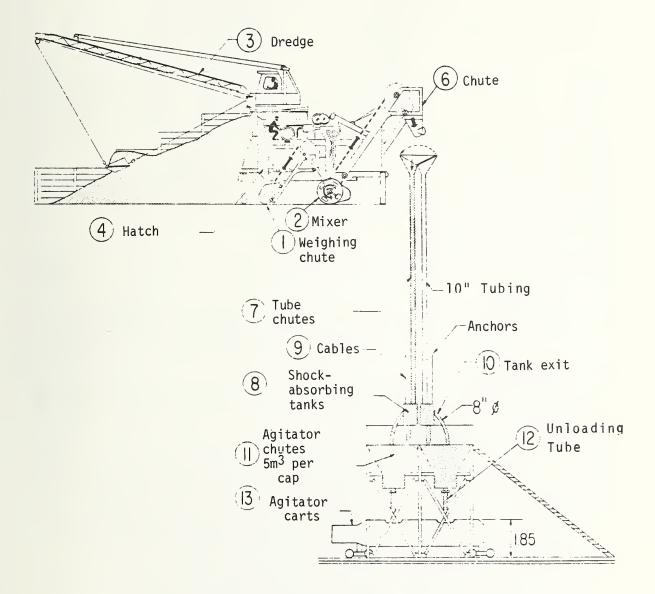


FIGURE B-5. PRODUCING AND UNLOADING OF THE CONCRETE

SHAFT FACE 11 - SHAFT 13 OF THE CENTRAL INTERCEPT

OBSERVATIONS					Installation of California switch and accomodation	into the track							Serious problems of creep- ing sands and increase of	the filtrations into the face will make it necessary to install MELL POINTS in	the face.	Sands in the face with creeping water	CTINCICI VehiloH	Holiday 1/1/73	Strong thrusts are noted in	the ground which deform the circle of voussoirs and	wnich are stopped by injec- ting the zone.	
Amount of water in the face (*)		2.00	1.75	1.75	1.75		1.75	1.75	1.75	1.75	1.75	2.00	2.00		2.00	2.00	2.00	2.00	2.00			
M E Lue to Due to neıther personnel nor equip- ment hr/wk		60	24	18								ω	104		84	92	108	88	100			
0 S T T T Break- down in the muck removal system	(hr/wk)				104		12															
Break- down in the shield (hr/wk)											24											
Effective excavation work time hours/wk		84	120	126	40		132	144	144	144	120	136	40		60	52	36	56	44			
Cumul- ative advance m/v:k	ł	11.25	34.00	57,61	65.11		90.61	117,61	146.86	180.61	208.78	236.53	244.03		255.28	265.03	271.78	282.28	290.53			
Advance m/wk		11.25	22.75	23.61	7.50		25.50	27.00	29.25	33.75	28.17	27.75	7.50	Y	11.25	9.75	6.75	10.50	8.25			
Chain	0+104.12	0+115.37	0+138.12	0+161.73	0+169.23		0+194.73	0+221.73	0+250.98	0+284.73	0+312.90	0+340.65	0+348.15		0+359.40	0+369.15	0+375.90	0+386.40	0+394.65			
Date	23-IX-72	30-IX-72	7-X-72	14-X-72	21-X-72		28-X-72	4 - X I - 7 2	11-XI-72	18-XI-72	25-XI-72	2-XII-72	9-XII-72		16-XII-72	23-XII-72	30-XII-72	6-`I-73	13-I-73			

OBSERVATIONS	Strong thrusts in the ground, cracking the voussoirs.	<u> </u>	H0110ay 2/5//3	The thrusts begin to be minor.				The shield of face 11-10 begins to operate so that from now on the same shaft services two faces.				Holidays 19, 20, 21/4/73		Holiday 5/1/73		Comparison of frame	progress; 0 + 768.46= 0 + 770.25.
Amount of water in the face (*)	2.00 2.00	2.00	1./5 1.75	1.75	1.75	1 °75	1.75	1.75	1.50	1.50	1.50	1.50	1.50	1.50	1.50	1.50	1.50
LE to Due to neither personnel nor equip- ment hr/wk	100 52	72	76 36	56	34	60	40	52	12		24	72	24	28	ω	8	4
<u>STTT</u> Break- down in the muck removal system	(hr/wk).																
Breakdown Breakdown in the shield (hr/wk)			12		30												
Effective excavation work time hours/wk	44 92	72	68 96	88	80	84	104	9 2	132	144	120	72	120	116	136	136	140
Cumul- ative advance m/wk	298.78 316.03	328.03	340°78 358.03	374.53	388.78	404.53	424 03	441。28	466.34	501.59	529°34	542.84	565.34	587.09	612.59	638.09	664.34
Advance m/wk	8.25 17.25	12.00	12.75 17.25	16.50	14.25	15.75	19.50	17.25	25.06	35.25	27.75	13.50	22.50	21.75	25.50	25.50	26.25
Chain	0+402.90 0+420.15		0+444.90 0+462.15	0+478。65	0+492.90	0+508.65	0+528.15	0+545.40	0+570.46	0+605.71	0+633.46	0+646.96	0+669.46	0+691.21	0+716.71	0+742。21	0+768.46
Date	20-1-73 27-1-73	3-11-73	10-11-73 17-11-73	24-11-73	3-111-73	10-III-73	17-III-73	24-III-73	31-III-73	7 - I V - 7 3	14-IV-73	21-IV-73	28-IV-73	5 - V - 7 3	12-V-73	19-V-73	26-V-73

SHAFT FACE 11 - SHAFT 13 OF THE CENTRAL INTERCEPT

	OBSERVATIONS															volume or water into the face 46 liters Exploratory and drainage boreholes are made in the								
Åmount of water in		1.50	1,50	1.50	1 ° 50	1.50	1.50	1.50	1.50	1.50	1.50	1.50	1 . 50	2.00	2.00	2.00	2.00	2 ° 0 0	2.00	1.75	1.75	1 .75	1.75	1.75
M E Due to	neither personnel nor equip- tment hr/wk	15	4		8	28	12				4		24	40	124	108	124	100	32	4	12			
D S T T T Break-	down 1n the muck removal svstem	(hr/wk)																						
Breakdown	in the shield (hr/wk)																							
Effective excavation	work time (hr/wk)	128	140	144	136	116	132	144	144	144	140	144	120	104	20	36	20	44	112	140	132	144	144	144
Cumul- ative	advance m/wk	688.34	714.59	741.59	767.09	788.84	813.59	840,59	869.09	899.09	926.84	958.34	983.09	1003.34	1007.09	1008.59	1012.34	1020.59	1041.59	1071.59	1097.84	1129.34	1162.34	1198.34
Advance	m/wk	24.00	26.25	27.00	25.50	21.75	24 ° 75	27.00	28.50	30.00	27.75	31.50	24.75	20.25	3°75	1 . 50	3.75	8.25	21.00	30°00	26.25	31.50	33.00	36°00
	Chain	0+794.25	0+820.50	0+847.50	0+873.00	0+894。75	0+919.50	0+946.50	0+975.00	1+005.00	1+032.75	1+064.25	1+089.00	1+109.25	1+113.00	1+114.50	1+118.25	1+126.50	1+147.50	1+177.50	1+203.75	1+235.25	1+268.25	1+304.25
	Date	2-VI-73	9-VI-73	16-VI-73	23-VI-73	30-VI-73	7-VII-73	14-VII-73	21-VII-73	28-VII-73	4-VIII-73	11-VIII-73	18-VIII-73	25-VIII-73	1-IX-73	8-IX-73	15-IX-73	22-IX-73	29-IX-73	6-X-73	13-X-73	20-X-73	27-X-73	3 - X I - 7 3

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OBSERVATIONS	Holiday 11/20/73 The tunnel is connected.
Am wa th	1.75 1.75 1.75 1.75 1.75
E Due to neither personnel nor equip- ment hr/wk	4
STTTM Break- down in the muck removal svstem	(hr/wk)
L O Breakdown in the shield (hr/wk)	
Effective excavation work time hours/wk	144 144 144 104 104
Cumul- ative advance m/wk	1233.59 1294.34 1333.34 1354.81 1354.81
Advance m/wƙ	35.25 33.00 27.75 39.00 21.47 21.47
Chain	1+372.50 1+372.50 1-400.25 1+439.25 1+460.72 1+460.72
Date	10-XI-73 17-XI-73 24-XI1-73 7-XII-73 7-XII-73

Appendix C

REFERENCES

- S.G. Vick, A Probabilistic Approach to Geology in Hard-Rock <u>Tunneling</u>, M.I.T. School of Engineering Report R75-11, June 1974.
- A. Sluz, <u>A Probabilistic Approach to Soft Ground Tunneling</u>, M.I.T. Thesis Submission, June 1975.
- 3) R.B. Peck, A.J. Hendron, Jr., and B. Mohraz, "State of the Art of Soft-Ground Tunneling," <u>Proceedings of the North</u> <u>American Rapid Excavation and Tunneling Conference</u>, Chicago, IL, June 5-7, 1972, p. 259-260.
- 4) L. Pietrzak and M. McJunkin, "Simulation as a Tunneling Research and Project Planning Tool," <u>Proceedings of the</u> <u>North American Rapid Excavation and Tunneling Conference</u>, San Francisco, California, June 1974, p. 176.
- 5) Ibid, p. 165.
- 6) R.W. Conway and A. Schultz, Jr., "The Manufacturing Progress Function," <u>Journal of Industrial Engineering</u>, Vol. X, January-February 1959, p. 39.

M. Gates and A. Scarpo, "Learning and Experience Curves," Journal of the Construction Division, ASCE, Vol. 58, March 1972, p. 79.

A. Vazsonyi, <u>Scientific Programming in Business and Industry</u>,J. Wiley, New York, N.Y. (1958) p. 382-395.

- W.B. Hirschmann, "Profit from the Learning Curve," <u>Harvard</u> <u>Business Review</u>, Vol. 42, January-February 1964, p. 116.
- 8) M.T. Tayyabkhan and T.C. Richardson, "Monte Carlo Techniques," Chemical Eng. Progress Vol. 61, January 1965, p. 78.

G.L. Smith, "Monte Carlo Simulation — A Tool for Combating Uncertainty in Economic Analysis,":presented at the 5th Annual Meeting, American Association of Cost Engineers, Philadelphia, PA, June 1966.

Appendix C (Continued)

9) A.E. Hoerl, "Application of Ridge Analysis to Regression Problems," <u>Chemical Eng. Progress</u>, Vol. 58, March, 1962, p. 54.

D.W. Marquardt and R.D. Snee, "Ridge Regression in Practice," The American Statistician, Vol. 29, February, 1975, p. 3.

 D.B. Hertz, "Risk Analysis in Capital Investment," <u>Harvard</u> Business Review, Vol. 42, January-February, 1964, p. 95.

Appendix D

REPORT OF INVENTIONS

No new inventions were developed during this study. Existing principles were applied to a problem in a new way, and a logic of problem-solution was developed.

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