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| 73-15 | FUKD SYSTEM | |
| v.9 | Earl E. Jamison | |



JANUARY 1974 FINAL REPORT

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Prepared for

DEPARTMENT OF TRANSPORTATION URBAN MASS TRANSPORTATION ADMINISTRATION OFFICE OF RESEARCH, DEVELOPMENT AND DEMONSTRATIONS Washington DC 20590

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| | | | Technical Report Documentation Page | | | |
|---|---------------------|---------------------------------|---------------------------------------|--|--|--|
| 1. Report No. | 2. Government Acces | sion No. | 3. Recipient's Catalog No. | | | |
| UMTA-MA-06-0031-73,IX | | 18 | | | | |
| 4. Title and Subtitle | ····· | | 5. Repart Date | | | |
| ELECTROMAGNETIC ENVIRONMENT MEASUREMENTS OF PRT SYSTEMS AT "TRANSPO®72" V. 9. | | January 1974 | | | | |
| | | 6. Performing Organization Code | | | | |
| VOLUME IX - FORD SISIEM | | | 8. Performing Orgonization Report No. | | | |
| 7. Author's) Earl E. Jamison | | | DOT-TSC-UMTA-73-15, IX | | | |
| 9. Performing Organization Name and Address | | | 10. Work Unit No. (TRAIS) | | | |
| Westgate Research Park | | 11. Cantract or Grant No. | | | | |
| McLean VA 22101* | | | DOT-TSC-375, 9 | | | |
| 12 Security Assess News and Address | | | 13. Type of Report and Period Covered | | | |
| Department of Transport | ation | | Final Report | | | |
| Urban Mass Transportati | on Adminis | tartion | Jan - Sep 1972 | | | |
| Office of Research, Dev | elopment an | nd Demon. | 14. Sponsoring Agency Code | | | |
| 15. Supplementary Notes | - d | 5. | | | | |
| *under con | tract to De | epartment of | Transportation, | | | |
| Transportation System | s Center, H | Cendall Squar | re, Cambridge MA 02142 | | | |
| 16. Abstract | | | | | | |
| Inis report covers the measurements of the broadband conducted noise present on the A.C. power lines feeding the Personalized Rapid Transit (PRT) systems at Dulles Airport with each system operating individually. The purpose of the measurement effort was to evaluate the electrical environment existing on each of the PRT "hot" and neutral A.C. power lines and to assess the effect of each system on the power line with all other PRT systems turned off. The measurements obtained during this test will be used for a comparison with data obtained with no PRT systems operating and with all four PRT systems operating simultaneously. MAR. 2.8 1374 INDEALY | | | | | | |
| 17. Key Words | | 18. Distribution Stater | nent | | | |
| Broadband, Conducted, A.C. Power Line, Individual Operation, Personalized Rapid Transit Document is available to the Public THROUGH THE NATIONAL TECHNICAL INFORMATION SERVICE, SPRINGFIELD. VIRGINIA 22151. | | | | | | |
| 19. Security Clossif. (of this report) | 20. Security Clas | sif. (af this page) | 21. No. of Poges 22. Price | | | |
| Unclassifed Unclassified | | 30 | | | | |
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PREFACE

The work described in this report was performed as part of a test program conducted to evaluate the Safety and Performance characteristics of the four Personalized Rapid Transit Systems (PRT) on display at Transpo $^{\textcircled{R}}$ 72. Sponsored by the U.S. Department of Transportation, Transpo $^{\textcircled{R}}$ 72 was the first United States International Transportation Exposition and was intended to demonstrate to the general public new technologies in transportation.

The PRT demonstration program was the responsibility of the Urban Mass Transportation Administration (UMTA) and was conducted to provide detailed engineering test data in addition to providing mature candidates for an Urban demonstration.

POWER LINE CONDUCTED NOISE MEASUREMENTS FORD SYSTEM - TRANSPO®'72

1. INTRODUCTION

The technical report presents the data obtained in the performance of tests for power line conducted noise at the personal rapid transit (PRT) system of FORD at TRANSPO[®] '72, Dulles Airport, Washington, D. C. This report covers one of the four tests defined under Item 5 of Contract DOT-TSC-375, and as performed by National Scientific Laboratories, Inc.

Item 5 calls for the performance of conducted noise measurements on PRT a.c. power lines in the frequency range from d.c. to at least 10 KHz, with one PRT system on. The objective of the tests was to gather operational data for each of the PRT systems. Such data will enable characterization of the noise increase attributable to system operations, when considered in comparison with the ambient data collected and documented* previously by NSL.

The measurements reported in this document were made during the forenoon of August 2, 1972.

^{*} Technical Report, Item 4, Ambient Power Line Conducted Noise Survey, PRT Systems, March 1972, Contract No. DOT-TSC-375, Department of Transportation, Transportation Systems Center, 55 Broadway, Cambridge, Massachusetts 02142.

2. METHOD OF MEASUREMENT

2.1 Instruments

All measurements were made using test set-ups and instruments as nearly identical as possible to those used during ambient testing. The power line conducted measurements were performed using a Fairchild Model EMC-10 Interference Analyzer. This device is a battery-operated calibrated RFI/EMI meter, which, when operated as a narrowband tunable device, covers the frequency range of d.c. to 50 KHz. The receiver has an internal calibration source and incorporates a meter circuit of such design that signal levels are expressed in decibels on a linear scale. In addition, the receiver incorporates circuitry providing buffered voltage outputs in proportion to meter indication and tuned frequency. A Hewlett Packard Model 3005B X-Y Plotter was driven from the receiver.

Some observations were made at frequencies above 50 KHz through the use of a Hewlett Packard Model 8552/8553A spectrum analyzer. Data was recorded photographically with a Hewlett Packard Model 198A oscilloscope camera. The analyzer is an extremely versatile instrument in that it has numerous frequency scan and bandwidth settings throughout the frequency spectrum of a few cycles up to 100 MHz.

Signals were obtained from the power lines by means of a Fairchild Model PCL-10 Current Probe. This device is a clampon current transformer which provides an output voltage in

proportion to the current on the conductor which passes through its aperture. This probe has a specified transfer-admittance characteristic which is a function of frequency.

2.2 Power Line Arrangement

The power provided to the PRT site via an underground feeder is 480 v.a.c., three phase (\emptyset). The feeder lines enter commercial switchgear in the Ford building and are coded as follows:

| Phase | <u>Color Code</u> |
|--------------|-------------------|
| | |
| A | Orange |
| В | Brown |
| C (Grounded) | Yellow |

The current probe was attached at the point where the feeders enter the switchgear which is the same point as used when making the ambient tests described in report Item 4.

2.3 Measurement Technique

Each of the three power conductors were tested by scanning two frequency ranges, d.c. to 1 KHz using a 5 Hz bandwidth, and 1 KHz to 50 KHz using a 50 Hz bandwidth. Two recordings have been made for each frequency range, on each of the three power lines. The scanning time per recording averaged four to six minutes.

These recordings are reproduced in the Appendix as the upper half of pages A-2 through A-13. The recordings are

presented in order of phase rather than the order in which they were produced. The dB scale refers to the level at the instrument input connector. Some of the charts have two amplitude scales. Located somewhere along the bottom of the chart is an upside down letter "Y" which denotes the point of changeover from the scale on the left side to the scale on the right side.

The spectrum analyzer was used to record data in the frequency range up to 1 MHz, particularly in the area of 150 KHz to 250 KHz wherein the vehicle and computer communicate.

3. INTERPRETATION OF DATA

The amplitude/frequency charts produced during the tests are reproduced in the upper half of each page of Appendix A-2 through A-13. The lower chart on each page is a plot of approximately one level in each major frequency increment of the chart directly above it. Peaks were selected whenever available. A correction factor for the current probe (current probe amplitude response is non-linear with frequency) has been included in the levels plotted in the lower chart.

In the upper charts, noise peaks recorded in the top major amplitude division are out of the calibrated range of the instrumentation system. Thus, the levels plotted for peaks that enter the upper division are plotted as having an amplitude of the highest level indicated numerically on the chart for that particular frequency.

Notations are written on the charts which denote vehicle start and stop on the guideway as well as at the station. Also, vehicle entering and leaving the stations were noted, as were similar functions at the north end of the guideway.

Spectrograms on page A-14 show the conduction noise on ØA up to 1 MHz for two vehicle conditions. The current probe is linear for frequencies above 50 KHz, thus, each gradicule amplitude division is a 10 dB level change.

Attempts were made to locate the communication frequencies of 150 KHz (Control to Vehicle) and 225 KHz to 250 KHz FSK (Vehicle to Control). The 150 KHz carrier was evident at such time as the vehicle was not drawing motive power, but at no time were the FSK frequencies recognized. The spectrograms in pages A-15 to A-17 show the conduction signals for various vehicle situations; note the 150 KHz carrier. The various other spikes were not identified.

4. TIME LOG

Ford had only one vehicle running during the test period--0800 to 1200. The log of events is contained in the Appendix on pages A-18 to A-20.

APPENDIX

POWER LINE CONDUCTION

MEASUREMENTS DATA

This appendix contains data charts for tests No. 423 through 435 (432 omitted), and spectrograms 436, 438, 440 to 444. The charts are presented in order of phase--A, B and C-for ease of analysis, rather than in numerical order as the tests were performed. The spectrograms are also rearranged for analysis purposes. The time log of operational events is at the end of the Appendix.





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FREQ. SCAN = 100 kHz/DIV. TIME SCAN = 0.1 sec/DIV. For frequencies above 50 kHz, -40 dB gradicule scale is 95 dBµV/MHz

POWER LINE: ØA

Vehicle slow down before entering station.





500 kHz

No. 438

FREQ. SCAN = 100 kHz/DIV. TIME SCAN = 0.2 sec/DIV.

For frequencies above 50 kHz, -40 dB gradicule scale is 95 dBµV/MHz

Power Line: ØA

Vehicle parked in station.



f_c 150 kHz

f_c 150 kHz

FREQ. SCAN = 50 kHz/DIV. TIME SCAN = 0.1 sec/DIV.

For frequencies above 50 kHz, -40 dB gradicule line (center) is 95 dBµV/MHz

POWER LINE: ØA

Vehicle parked in South Station

No. 442

FREQ. SCAN = 50 kHz/DIV. TIME SCAN = 0.1 sec/DIV.

For frequencies above 50 kHz, -40 dB gradicule line (center) is 95 dBµV/MHz

POWER LINE: ØA

Vehicle stopped at North end of guideway.



FREQ. SCAN = 50 kHz/DIV. TIME SCAN = 0.1 SEC/DIV.

For frequencies above 50 kHz, -40 dB gradicule line (center) is 90 dBµ/MHz

POWER LINE: ØA

Vehicle stopped (unscheduled) on guideway





No. 443

FREQ. SCAN = 50 kHz/DIV. TIME SCAN = 0.1 SEC/DIV.

For frequencies above 50 kHz, -40 dB gradicule line (center) is 95 dBµV/MHz

POWER LINE: ØA

Vehicle travelling from North to South on guideway





f_c 150 kHz



FREQ. SCAN = 50 kHz/DIV. TIME SCAN = 0.5 SEC/DIV.

For frequencies above 50 kHz, -40 dB gradicule line (center) is 75 dBµV/MHz

POWER LINE: ØB

Vehicle parked on guideway during noon lunch hour.

No. 444 (Special)

Same as 444 above except:

TIME SCAN = 5 SEC/DIV., and Display Video Frequencies limited to 100 Hz.

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