

REPORT NO. DOT-TSC-OST-71-12

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# AN AIRPORT AIRSIDE SYSTEM MODEL

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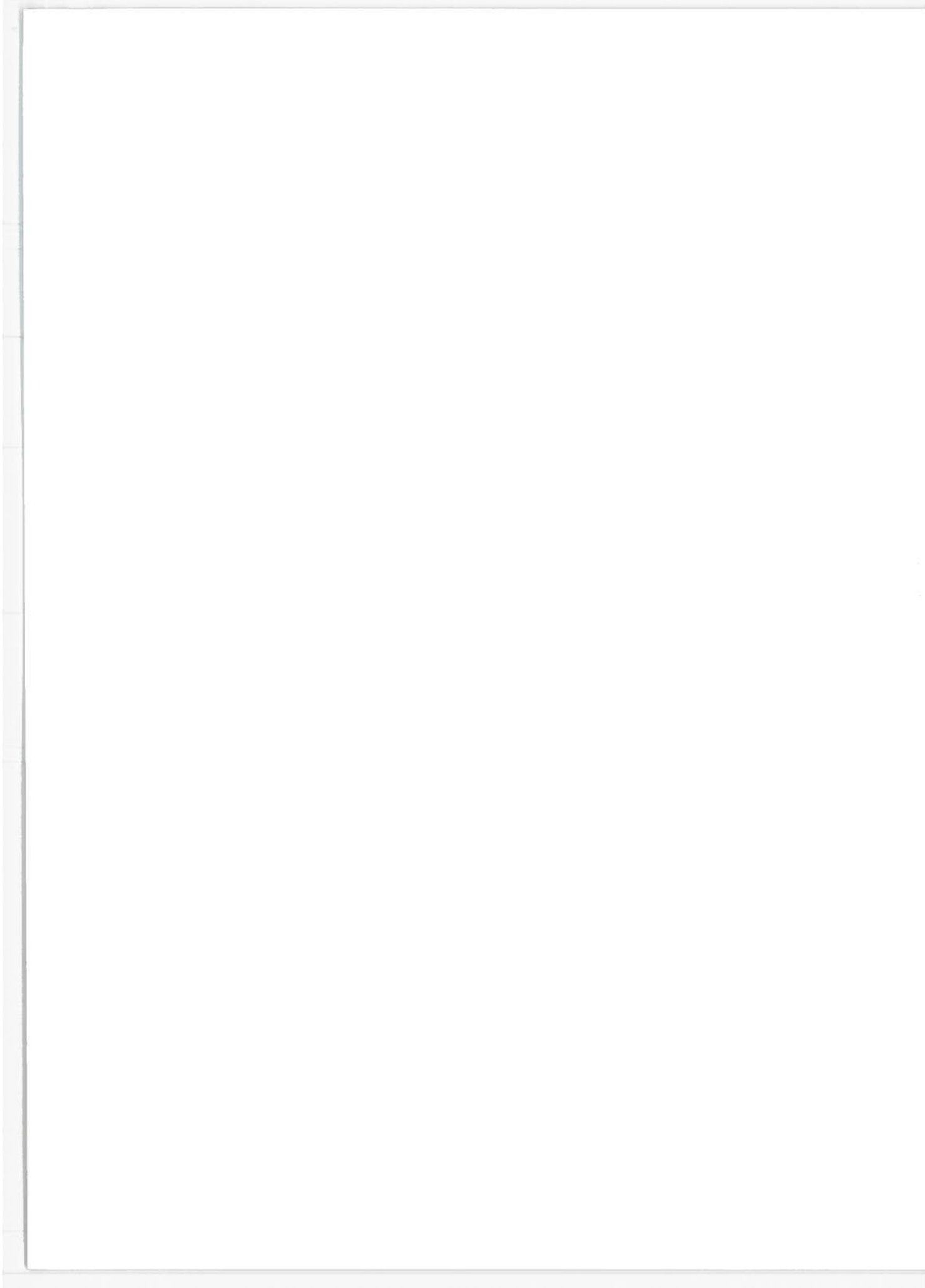


JUNE 1971  
TECHNICAL REPORT

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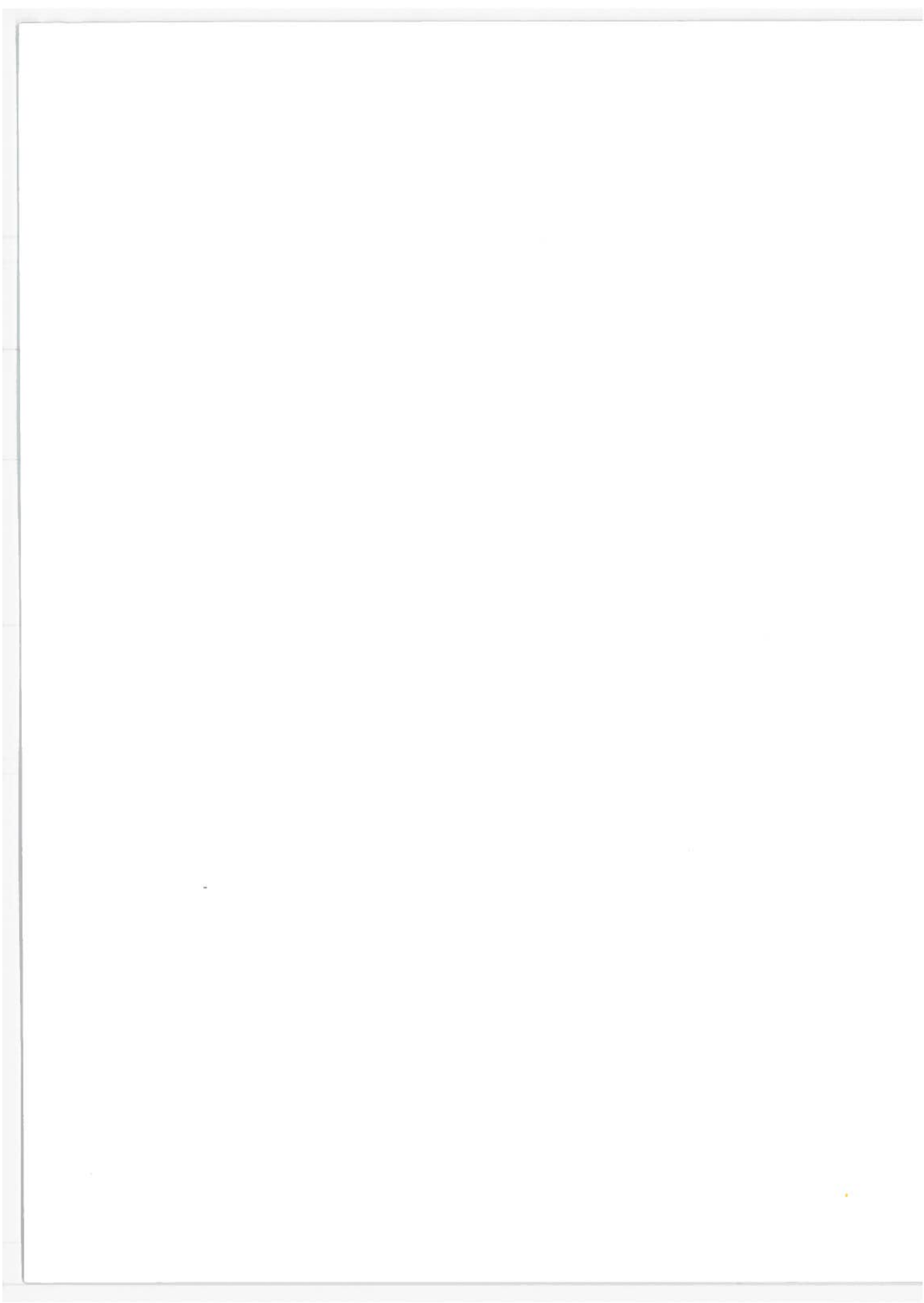
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## INTRODUCTION

An Airport Airside System model, simulating the airport control system from the terminal gate to the point of handoff to the enroute controller, has been developed for use in analyzing system performance in response to a variety of operating rules, control procedures, runway and taxiway configurations, and distributions of aircraft types. The model consists of an Input Package for defining the data and parameters, an Output Package to compute performance measures and to handle graphics displays, Arrival and Departure Packages to move planes through the system, and Local and Radar Controller Simulation Packages (both having arrival and departure portions) to control the movements of aircraft.

The model exists in two forms: batch and interactive. Both allow the user to analyze a problem quickly and easily. Experience with the model will provide insight into both its strengths and weaknesses and, more importantly, point the way to future upgrading of the model in the direction of a closer approximation to the real world. The interactive version of the model utilizes a computer graphics system which provides the user with a natural and easy means for setting up the problem, watching the system in action, changing parameters, and gathering performance statistics.

### OPERATION OF THE MODEL

The model permits the user to enter any desired airport surface configuration, consisting of a set of runways and taxiways. All altitude levels can be used by aircraft flying in the system, and standard vertical and horizontal separation criteria for aircraft are incorporated.

For simplicity, this first model is restricted to aircraft operating under Instrument Flight Rules (IFR). Furthermore, all flights in the system conform to schedules (which are defined by the user for each type of aircraft). Multiple flights may be scheduled for departure at the same time on one runway. These flights are then sequenced according to the characteristics of the runway and aircraft being used, taking into consideration the number of incoming flights and the rules governing aircraft separation in the terminal area. Any pattern may be used and the only restriction is that handoff points conform to Standard Instrument Departure (SID) routes.

Arriving aircraft enter the airport area through a simulated handoff to a radar controller and are then stacked



for later processing if necessary or, if traffic load permits, are immediately directed into a controlled pattern for landing and taxiing along prescribed routes to specified gates. Departing aircraft leave gates under ground control, take off under local control, and proceed under radar control up to the point of simulated handoff to enroute control. Flights are continuously updated while in progress and search logic in the Radar Controller simulation detects projected, or actual, violations of the separation rules. Automatic conflict resolution is an option in the model.

Standard air traffic controller functions exist, including communications between aircraft and controllers, as well as, provisions for altering flight paths because of potential conflicts. A list of potential conflicts (a potential conflict is a situation where two aircraft are less than five miles apart and closing) requiring controller attention is generated, and any potential conflict which would be apparent to the controller can be resolved automatically, if desired.

Measures of system performance are calculated while the model is in operation. These include controller workload, arrival rate, departure rate, queue size, etc. The system in action will be portrayed on interactive graphics displays in a form which is both realistic and readily understandable. In particular, areas of congestion or potential hazard can be immediately seen. Moreover, the model will be designed to be useable by people without computer programming experience.

## **APPLICATIONS OF THE MODEL**

The model can be used to analyze the effect of various airport runway configurations, traffic patterns, aircraft mixes, etc., on airport capacity. For instance, the batch version of the model has already been used to evaluate the effect of intermixing STOL and conventional (CTOL) aircraft in the traffic pattern of a typical airport. Realistic operational parameters provided by the Aircraft Division, SRDS, were used in this study, including STOL and CTOL aircraft characteristics, runway geometry for a particular airport, aircraft glide slope angles, and offset approach configurations. The performance measures used were arrival rate, departure rate, and number of conflicts.

Another major application is the analysis of acceptance rate, wherein airport arrival rate can be adjusted in accordance with controller work load. The model user can enter any acceptance rate algorithm he desires and evaluate its effect on airport operations (i.e. arrivals and departures).

A conflict analysis can be performed in which various measures of conflict potential are tested. Several thresholds (which depend on aircraft spacing and relative velocity) are possible and are available as options in the model. A vehicle access control system (VACS) simulator is being incorporated in the model for use in studying airport surface traffic control problems.

The above is not an exhaustive list of applications for the initial model. It is, rather, a representative list of typical problems which could be solved. We expect that other similar applications will suggest themselves and that these can be handled either directly, or by making minor modifications to the present model.

### LIMITATIONS OF THE MODEL

The current model does not include all features of a real world Airport Airside System. The missing features are not omitted because of any inherent difficulty in programming them. Rather, their omission serves to reduce the complexity of the model. It would be a simple matter to later add any desired feature.

Specifically, VFR flights and emergencies are excluded from the system since they neither comprise a significant proportion of the scheduled air carrier traffic, nor does the ATC system exert as much influence on them as on IFR flights.

Also, while provisions exist for simulating hardware in detail, these have not been implemented in the present model. Furthermore, there is no intent to incorporate these features until a specific problem requires them.

### ORGANIZATION OF THIS REPORT

This report is divided into three sections, one for each major function of the model, namely: Input/Output, Controller Actions, and Aircraft Movement and Communications. In addition, a complete listing of the simulation programs in FORTRAN IV is included in the Appendix. Figure 1 is a flow diagram of the model in which the portions constituting each of its three major functions are surrounded by dashed lines; the modules within each portion are shown as boxes labeled with a numeric code; and the flow of information is indicated by lines and arrows. Note that the Input and Output portions are replicated in the Arrival and Departure portions of the model. The gross organization of the model is as follows:

Major Functions	Portions
Input/Output	Input
	Output
Controller Actions	Radar Controller
	Local Controller
Aircraft Movement and Communications	Aircraft Arrival
	Aircraft Departure

Each section begins with a block diagram showing the inputs and outputs of all the modules contained in the portion of the model being described.

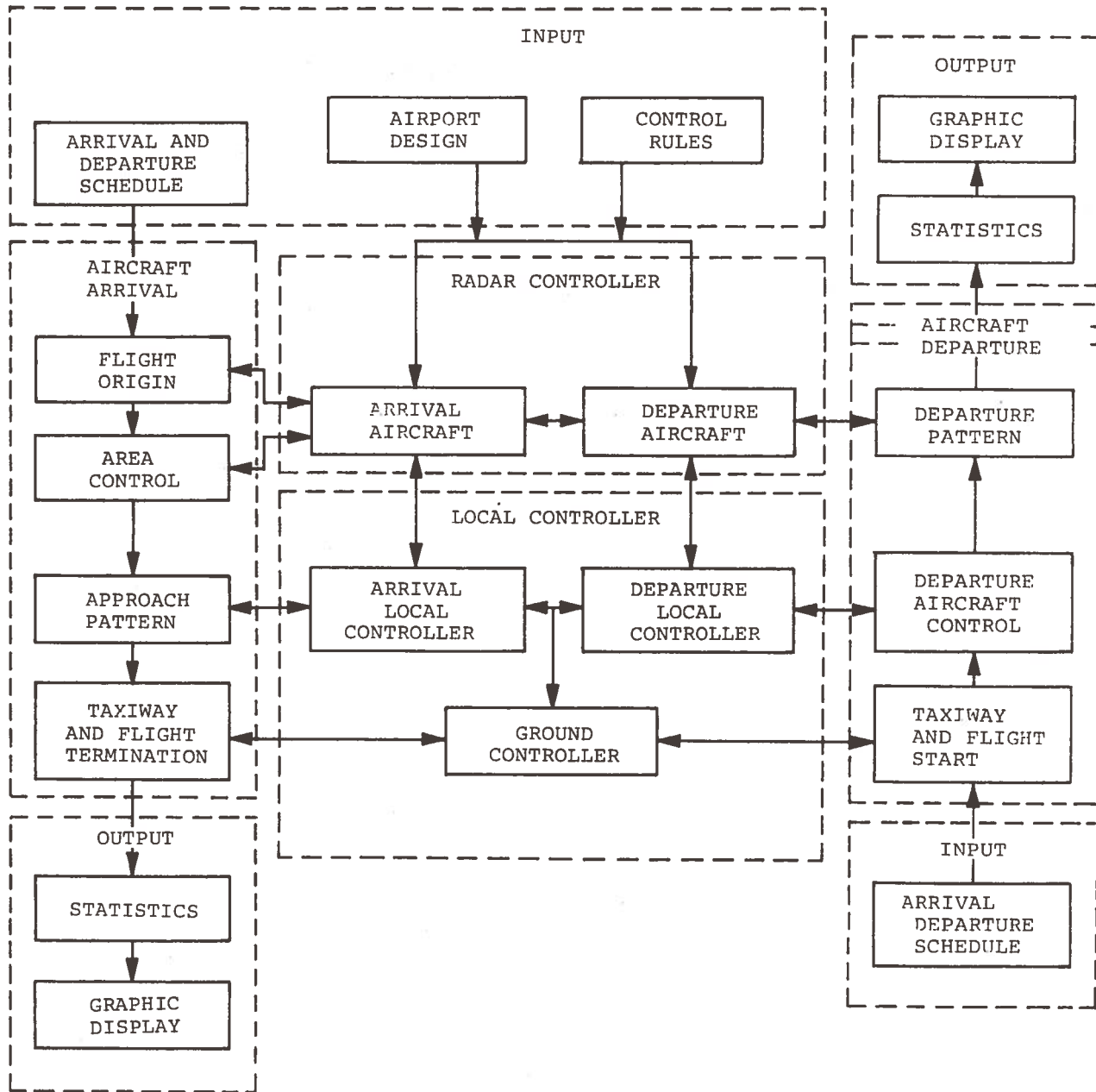


Figure 1. Airport Airside Model

## INPUT

The input portion of the model (Figure 2) contains all the parameters which specify the airport design, control rules, arrival schedules, and departure schedules. For ease in actual operation the parameters are divided into two groups: those which are infrequently changed and hence are built into the program; those which are frequently changed and thus are entered as input each time a new problem is simulated. However, any variable can be readily transferred from one group to the other.

Among the built-in parameters are SID, STARS, holding patterns, ATC rules and controller workload maximums. Among the input parameters are runway and taxiway location, handoff points, and aircraft characteristics, (i.e. turn rate, climb rate, acceleration, decent rate, and wake separation).

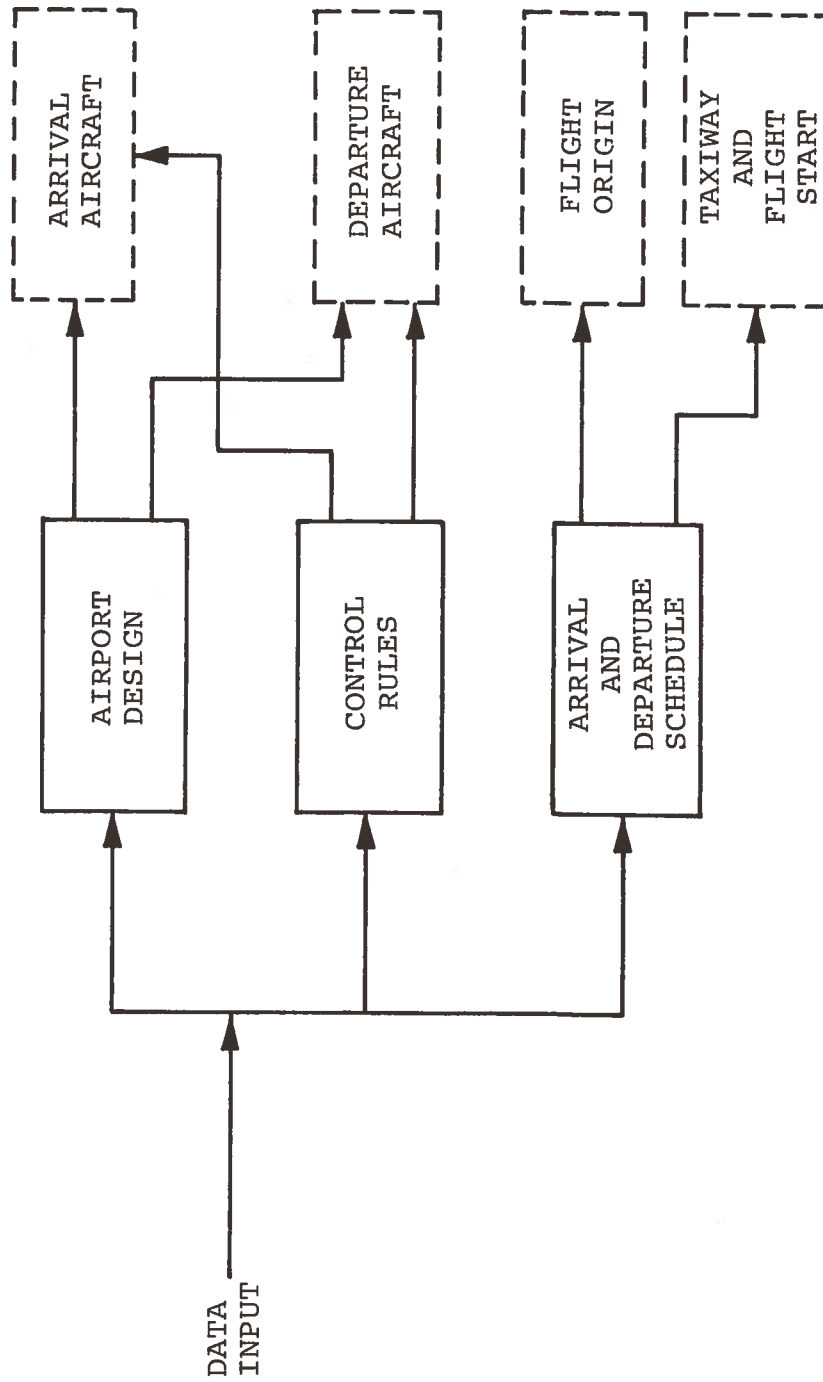


Figure 2. Input

## **AIRPORT DESIGN MODULE**

The airport design consists of the boundaries where handoffs are made between the enroute controller and the airport controllers; the runway locations and lengths; the traffic distribution for each type of aircraft (i.e. numbers of conventional aircraft, STOL aircraft, or VSTOL aircraft); and the positions of outer markers.

## **CONTROL RULES MODULE**

The Control Rules Module sets both the altitude at the outer marker and the glide path angle for each runway. Within each area a vector direction is defined for all points in the area below the holding pattern; the number of aircraft approaching a runway is set; a holding altitude is established and the holding pattern is protected. Maximum controller workload is an input which controls acceptance rate.

The spacing criteria for aircraft is three miles and one thousand feet altitude. A conflict is defined as a violation of these spacing criteria. (This is in conformance with F.A.A. rules). In addition, provisions are made for inputting standard instrument departures (SID) together with the requirement that the handoff of a departing aircraft can only occur when that aircraft is near or on a SID and outside the airport area.

## **ARRIVAL AND DEPARTURE SCHEDULE MODULE**

This arrival part of this module allows the user to input an arrival schedule for aircraft by type (CTOL, STOL, VSTOL). In the current model, arrivals of each aircraft type are equally spaced with no randomness.

The departure schedule delivers aircraft to the runway line up in a similar manner. However, the actual takeoff depends upon the air traffic control situation.

## OUTPUT

The output portion of the program has not been fully specified since each user may require different information depending upon his purpose. The program affords the user the flexibility of specifying what statistics will be collected and to select the output format (i.e. either a printout, a C.R.T. display, or both). The current user choices are specified below.

### STATISTICS MODULE

During the operation of the program a variety of statistics are calculated. For each operating runway a count of operations is made. (The counter is incremented for arrivals when the aircraft first occupies the runway, whereas for departures the counter is incremented when the runway is cleared.)

In order to evaluate controller workload, the following statistics are gathered. First, a count of vectors issued by the simulated controller is made. (A vector is assumed to be issued whenever the logic of the program requires a turn or an altitude change.) A second count is conflict minutes. (For each interval of simulation time a count of pairs of aircraft in conflict is made. This count is multiplied by the simulation interval, and the product is added to the counter.) A third count is the conflict minutes per mile. (At each interval of simulation time the simulation interval is multiplied by the sum of the inverse of the separations, and the product is added to the counter.) This count has the advantage over a straight time count in that it weighs conflict according to their seriousness as shown by separation.

A count of the line up for each runway at each time interval is made to give a measure of departure delay. A count of stack size at each time interval is made to measure arrival delay.

### GRAPHICS OUTPUT

The graphics output consists of two airport displays: one planer and one vertical. Both displays show the runways as well as all aircraft currently in the system. (At the user's option, an identification code can be displayed next to each aircraft.) Also, a table of statistics can be displayed on the planer view. To assist in coordination of the two views any group of aircraft can be made to blink, or become invisible, on both displays.



## RADAR CONTROLLER

The Radar Controller portion of the model (Figure 3) is divided into two modules: the Arrival and Departure Aircraft Modules. The first controls arriving aircraft from the airport boundary until the aircraft is assigned to a runway and is handed off to the Arrival Local Controller. The second handles departing aircraft from the point where they are received by handoff from the Departure Local Controller up to the point where they are handed off to an enroute controller at the airport boundary. Both modules use a common conflict resolution routine since conflicts checking is done for all aircraft.

### ARRIVAL AIRCRAFT MODULE

As each aircraft arrives, it is assigned to a runway which handles that type of aircraft and which has the smallest queue. If the assigned number for a given runway exceeds a specified limit (i.e., a variable, but presently set at five aircraft), the aircraft is placed in a holding pattern. (Each such pattern has a minimum holding altitude of 5000 feet and is allocated four fixes. For convenience, the model handles all aircraft in each holding pattern.) The number of aircraft in the holding pattern determines the altitude of the next arrival. Four oval holding patterns, each twenty miles long, are distributed around the airport. Aircraft enter these patterns on a first come first serve basis. The only exception is STOL aircraft which may have a separate holding pattern when the STOL runway is in operation.

If there is no holding required (or if an aircraft is being removed from the holding pattern for landing), the aircraft is assigned a vector bringing it to an initial approach altitude (currently 2200 feet for the first arrival runway and 3200 feet for a parallel runway). The aircraft is then vectored to a prescribed point for handoff to the Arrival Local Controller. The primary path is a function of the aircraft turn rate and descent rate.

A list of all pairs of aircraft and their altitudes is generated. Those pairs within three miles separation and one thousand feet altitude are classified as conflicts requiring priority attention. (Other separation distances can be designated as potential conflicts if desired.) The user has the option of moving aircraft on SID or STARS and merely recording conflicts, or he may choose to utilize an automatic conflict resolution program (available in the current model) which acts

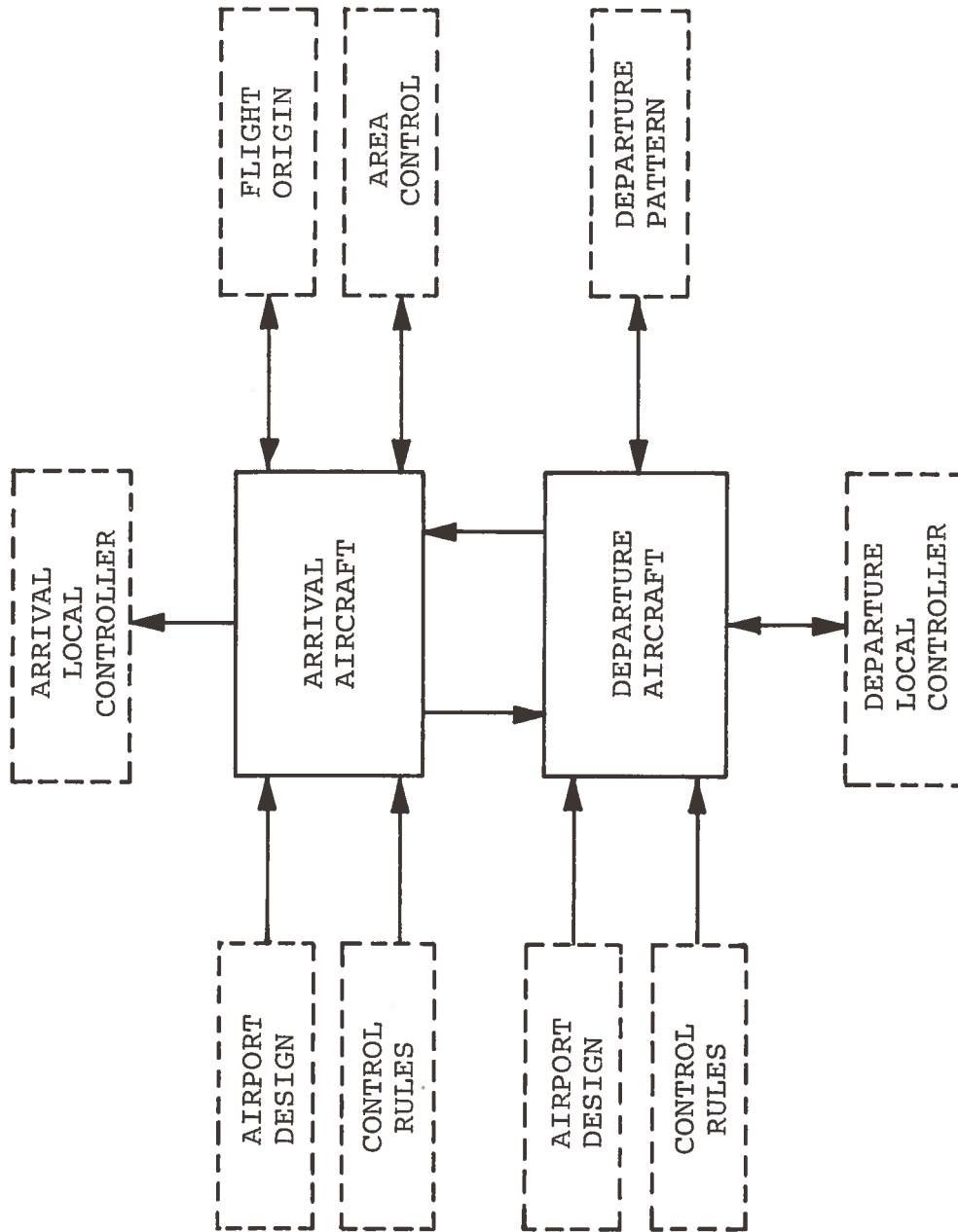


Figure 3. Radar Controller

to resolve potential and actual conflicts. A potential conflict is defined as two aircraft less than five miles apart whose point of closest approach is a conflict. (However, aircraft on a localizer path are not considered to be in potential conflict.) In the event of a potential conflict the current rules are:

1. If two aircraft are not co-altitude, then the aircraft are assigned altitudes to maintain altitude separation or to increase altitude separation.
2. Aircraft at the same altitude are turned from their current course to increase separation at the point of closest approach.

#### **DEPARTURE AIRCRAFT MODULE**

An aircraft is handed off from the Departure Local Controller and issued vectors until it is five miles away from the airport. At this point the program routes the aircraft along a standard instrument departure (SID). Handoff from the model occurs when an aircraft is more than thirty miles from the airport center and on, or near, a SID path.

## LOCAL CONTROLLER

The Local Controller portion of the model (Figure 4) encompasses three controller functions. The first is the Ground Controller which monitors runway assignments and determines when a runway is available. This controller also monitors the landing and departure queues, and assigns aircraft in the queues to runways. The second function is the Arrival Local Controller which controls arriving aircraft from the time they are handed off from the Arrival Aircraft Module until they enter the taxiway. The third controller function is the Departure Local Controller which controls departing aircraft from the time they enter the runway line-up until they are airborne and handed off to the Departure Aircraft Module.

### GROUND CONTROLLER MODULE

The Ground Controller Module controls departing aircraft from the gate until they are in the runway line-up on the taxiway. Arriving aircraft are controlled from runway touchdown until the time they arrive at the gate.

The procedure for departing aircraft is to check the departure schedule at each step to determine if an aircraft departure is scheduled. If none is scheduled, the program proceeds to the next step. If a departure is scheduled, the aircraft is assigned to the departure runway handling that type of aircraft which has the smallest queue. Thus, it is possible to specify that STOL aircraft use STOL runways, and other similar restrictions.

Next, the Ground Control Module vectors ground aircraft to their runway queue, allowing them to cross available runways. (A runway is available if no arriving aircraft is within the two miles of landing on that runway, or a dependent runway, and if no other departing aircraft has been given takeoff clearance.)

Departure and arrival runways are designated. In cases where parallel runways are used, one is designated for departure and one for arrival, and assignments are made to each runway on a first come first served basis. When a single runway is used for both departure and arrival, arrivals are given preference, and the ratio of arrivals to departures is a function of mean waiting time and maximum waiting time for aircraft in the arrival queue. The exact function is an input. In this version of the program there are no provisions for emergency landings.

## AIRCRAFT ARRIVAL

The Aircraft Arrival portion of the model (Figure 5) is divided into four modules. The Flight Origin module simulates handoffs from the enroute controller to the Area Control module. In turn, the Area Control module assigns controllers and resets controller rules if the area has special rules. The Approach Pattern module handles aircraft motion and communication in response to the Arrival Local Controller. The Taxiway and Flight Termination module moves the aircraft from the landing point to the gate.

### FLIGHT ORIGIN MODULE

The Flight Origin module regulates controller workload by limiting acceptance rate (i.e., number of aircraft per controller). It checks the arrival schedule, and if an arrival is scheduled, it sets up a point of handoff and the velocity, descent rate, and bearing.

### AREA CONTROL MODULE

The Area Control module simulates the aircraft response to the vectors generated in the Arrival Aircraft module. The aircraft position is updated using the latest vector as a basis and then correcting for wind error and aircraft characteristics. The wind error in this program is a random number of limited magnitude (set by the user) which is added to the position. The aircraft characteristics which limit response to a vector are maximum climb rate, maximum descent rate, maximum and minimum velocity and maximum turn rate.

The module simulates communications between aircraft and controller by adding random errors to the position and velocity data before transmitting this information to the controller by voice, radar, or transponder mode C.

### APPROACH PATTERN MODULE

The Approach Pattern module governs aircraft response to vectors from the Arrival Local Controller module and handles communications with that module. The major difference between this module and the Area Control module is in the rules applied (i.e., communications are more frequent, radar is more accurate, and for each aircraft type there are rules covering altitude in relation to speed).

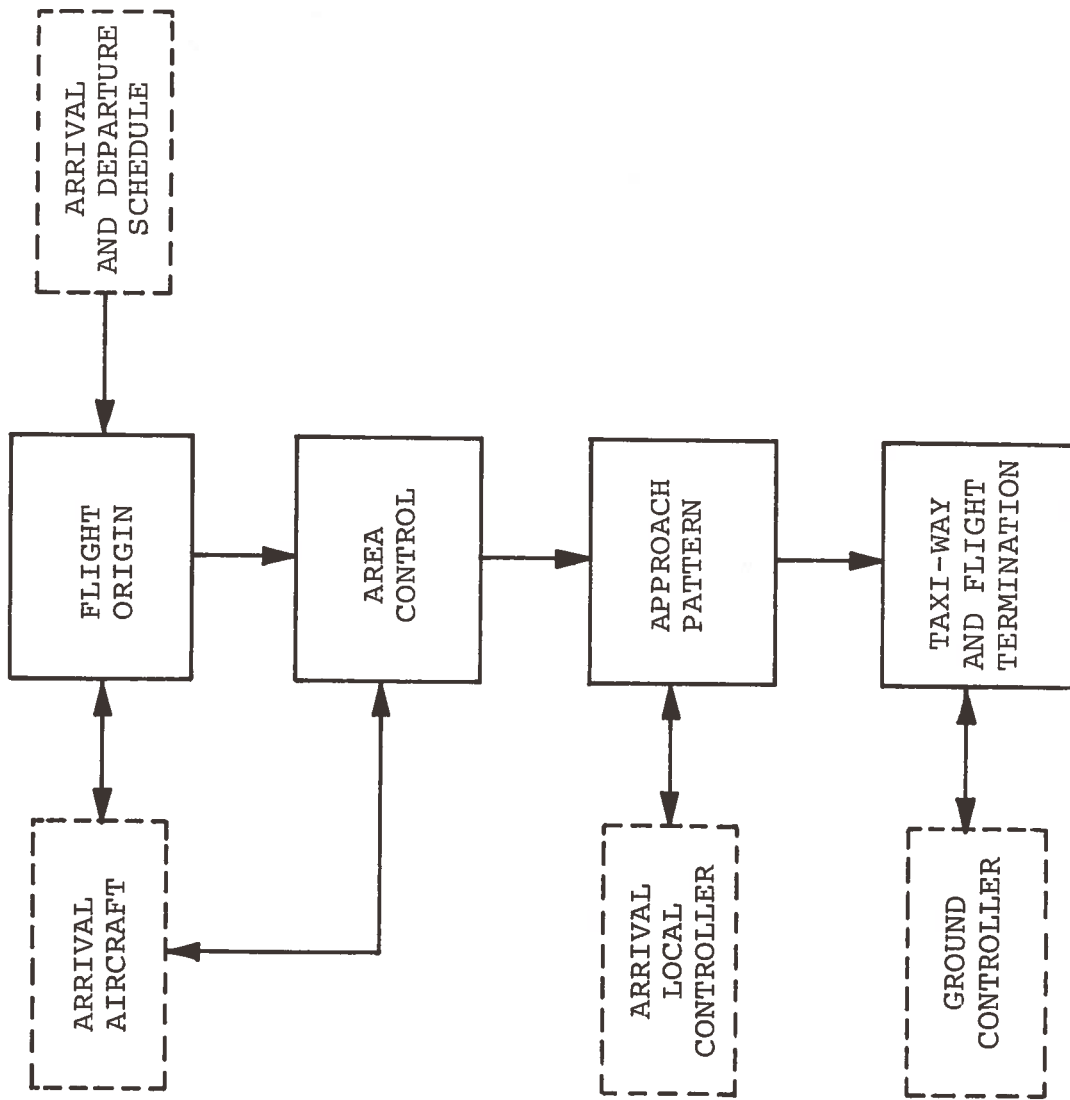


Figure 5. Aircraft Arrival

## TAXIWAY AND FLIGHT TERMINATION MODULE

The Taxiway and Flight Termination module receives a gate assignment from the Ground Controller module. It then simulates the aircraft following a taxiway map, moving from node to node towards its gate. The aircraft are processed on a first come first served basis and each is moved in such a manner that no two aircraft cross the same intersection at the same time. Aircraft move at 15 to 20 knots and are separated by no less than one plane length at all times. The prevailing rule is see and be seen.

## AIRCRAFT DEPARTURE

The Aircraft Departure portion of the model contains three modules which execute aircraft operations (i.e., communications and aircraft movements). The Taxiway and Flight Start module processes aircraft movement from gate to taxiway line up. The Departure Local Control module processes aircraft movement from clearance to take-off until the runway is available for the next aircraft. The Departure Pattern module processes aircraft motion from this point until it leaves the airport area.

### TAXIWAY AND FLIGHT START MODULE

This module contains a list of departing aircraft. When the schedule calls for a departure, the aircraft is assigned to a gate, and the Ground Controller module is called upon to assign the aircraft to a runway. The Taxiway and Flight Start module then moves the aircraft along a fixed path to the runway, resolving conflicts between crossing aircraft on a first come first served basis. When an aircraft is about to cross a runway the aircraft is stopped and a message transmitted to the Ground Controller module which transmits either a wait order or a runway clear order. After receiving a runway clear order the aircraft crosses the runway and proceeds to the end of the runway line-up.

### DEPARTURE AIRCRAFT CONTROL MODULE

This module receives a "runway cleared for departure" message from the Departure Local Controller module. It then brings the first aircraft onto the runway. The Departure Local Controller module is notified; it clears the aircraft for take-off; introduces a time delay to simulate take-off; and sets the aircraft take-off velocity and climb angle. The module then records position and transmits it through a radar simulator to the Departure Local Controller module. It also transmits, on request, data by voice communication. It receives vectors from the Departure Local Control module and executes them as fast as the aircraft characteristics permit. Finally, aircraft position is updated at regular intervals by this module.

### DEPARTURE PATTERN MODULE

This module models aircraft motion under a departure radar controller. It provides voice communication and radar blips to the Departure Aircraft module. It receives vectors from the Departure Aircraft module and models aircraft response to these vectors. Its principal algorithm checks vectors against aircraft capability and acts accordingly.



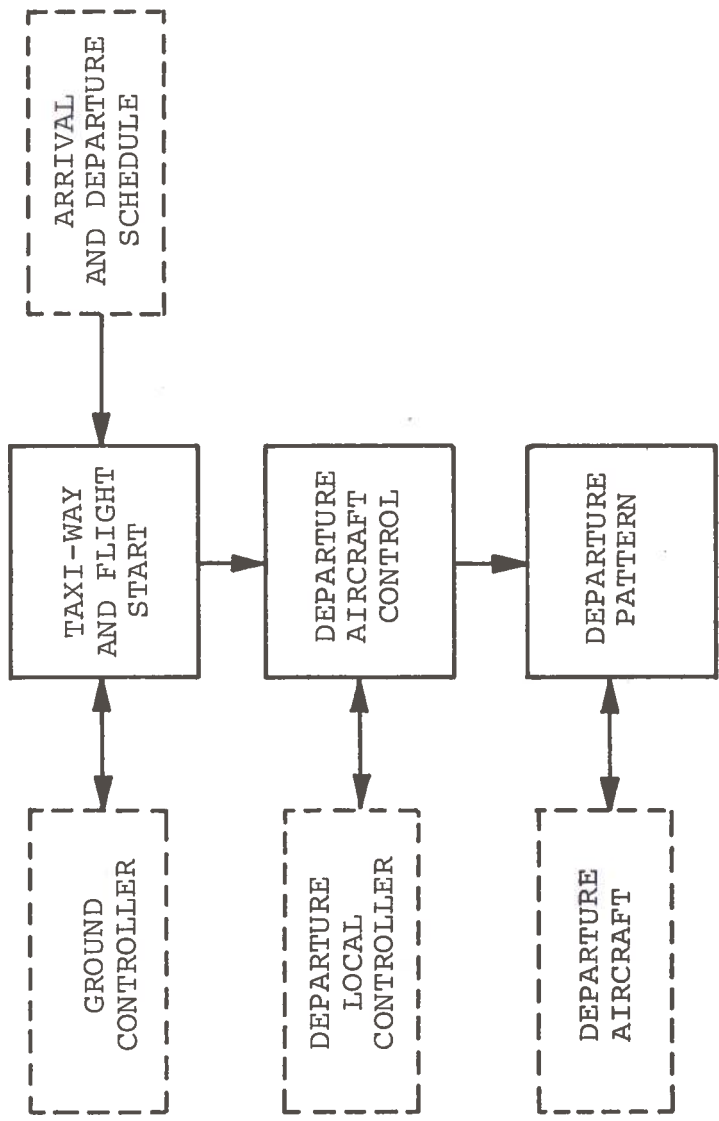


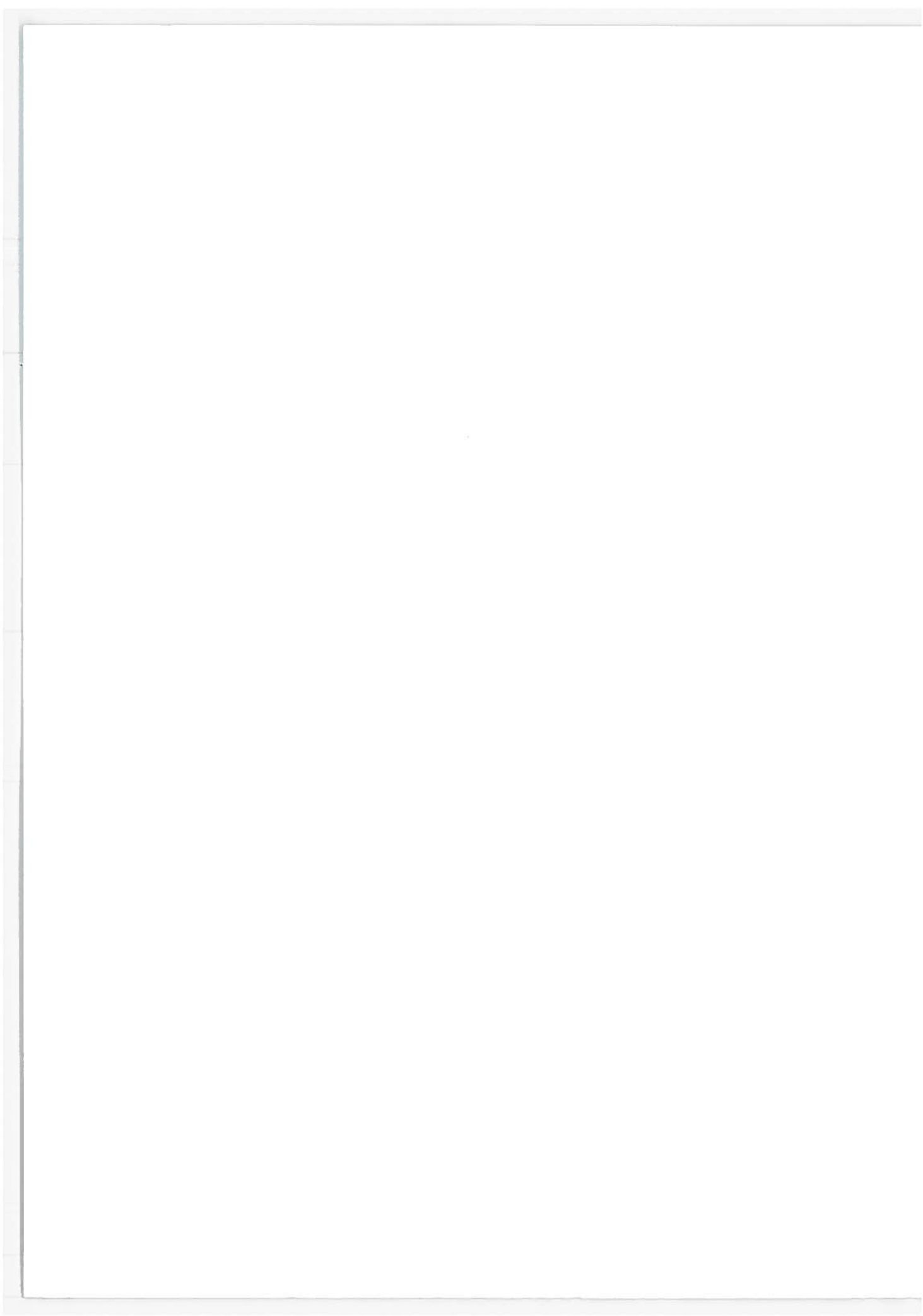
Figure 6. Aircraft Departure

It also adds an error to the aircraft bearing and velocity set by the pilot in response to the departure radar controller's direction. These are generated from a random distribution with a maximum value set at a fixed percent of the actual value. However, the distribution used can be changed by the user. The wind correction is set by moving the aircraft position by adding random numbers to the aircraft position. The maximum random number is set by the user.

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APPENDIX A  
Simulation Program Listings



\$JOB I13710 2 TCD ENGLANDER  
\$EXECUTE IRJOB  
\$IBJOB

001 020

\$IBFTC ONE

C OS04 AIRPORT CAPACITY JUNE 14,1971

C IDO ARE RUNWAY ASSIGNMENT POSITIVE ARRIVE, NEGATIVE DEPARTURE

COMMON/A/ISENSF

COMMON /M/MTRAN

COMMON /R/ IDO

COMMON/P/ XS,YS,ZS,T

COMMON/U/DI,TI

COMMON/B/COINT

COMMON/C/ZMAX,ZMIN,TMAX,TMIN

DIMENSION MTRAN(144)

DIMENSION IDIST(100),JDIST(100)

DIMENSION ZMAX(30),ZMIN(30),TMAX(30),TMIN(30)

DIMENSION PRI(4)

DIMENSION IDENT(4,30),JTYPE(4,30)

DIMENSION IDO(4),KS(4)

DIMENSION TOC(4),TC(4)

DIMENSION PH(4),XS(4),YS(4),ZS(4),S(4),TS(4),IS(4),T(4),V(4),P(4)

DIMENSION COUNT(10)

DIMENSION X(4,30),Y(4,30),Z(4,30),TT(4,30),VT(4,30),PT(4,30)

DIMENSION XA(4,30),YA(4,30),ZA(4,30),TD(4,30),VD(4,30),PD(4,30)

DIMENSION ISENSE(4)

DIMENSION CCOUN(5,9)

IID=0

996 CONTINUE

IF(IID.LE.0) GO TO 997

DO999 I=1,9

CCOUN(IID,I)=COUNT(I)

999 CONTINUE

MTRAN(1)= -9\*IID

K=1

DO 998 KK=1,IID

DO 998 LL=1,9

K=K+1

MTRAN(K)=CCOUN(KK,LL)

998 CONTINUE

CALL CPSXN(IWORD,MTRAN,JUNN)

997 CONTINUE

IID=IID+1

C N IS NUMBER OF RUNWAYS

CALL DATA(N)

PI=3.14159

KSIGN=0

JRXUA=1

DO 6 IJKU=1,144

MTRAN(IJKU)=0

6 CONTINUE

C CALL INNERT

C VEHICLE ACCESS

C\*\*\*\*\*

C\*\*\*\*\*

C\*\*\*\*\*

C\*\*\*\*\*

JUNK=0

209 FORMAT (6F10.5,2I5)

C OUTPUT CONTROL SECTION

```

LARBRT ST LOUIS SPECIAL
LAMBFR=-1
4001 CONTINUE
C TWRITE IS INNITIAL PRINTING OF PLANF TABLF
  TWRITE=0.0
C TLIST CONTROLS CONFLICT TABLE PRINTING
  TLIST=0.
C DTWRIT IS WRITING INTERVAL
  DTWRIT=10.
102 FORMAT(1X,F9.5,5F10.5)
C SET RESULTS COUNTERS TO INNITIAL VALUFS
  DO 462 I=1,10
    COUNT(I)=0.0
462 CONTINUE
C DT IS TIME INCRFMENT
  DT=0.01
C ITYPE IS THE NUMBER OF AIRCRAFT TYPES
  ITYPE=2
  NCLASS=2*ITYPE
  MTRAN(1)=N
C ISENSE ARE CONTROLS OF INTERACTIVE INPUT
  ISENSE(1)=0
  ISENSE(2)=0
  ISENSE(3)=0
  ISENSE(4)=0
  DO 300 J=1,N
    ISENSE(J)=1
300 CONTINUE
C M IS MAXIMUM NUMBER OF AIRCRAFT
  M=30
C TI IS PROBLEM TIME
  TI=-DT
C INPUT SECTION
C PH IS INTERRUNWAY PHASE SHIFT FOR ARRIVALS
  READ(5,102)(PH(IFF),IFF=1,NCLASS)
C S IS AIRCRAFT DISPLACEMET ON ARRIVAL IN AIRPORT AREA
  READ(5,102)(S(IFF),IFF=1,NCLASS)
C WRITE(6,102)(PH(IFF),IFF=1,NCLASS)
C WRITE(6,102)(S(IFF),IFF=1,NCLASS)
C TOC IS MINIMUM OCCUPANCY TIME
  TOC(1)=1.
  TOC(2)=1.
  TOC(3)=1.
  TOC(4)=1.
  DO 767 J=1,N
C INPUT NEW PLANE CHARACTERISTICS. POSITION, BEARING, VELOCITY, CLIMB
  READ(5,102)XS(J),YS(J),ZS(J),T(J),V(J),P(J)
C WRITE(6,102)XS(J),YS(J),ZS(J),T(J),V(J),P(J)
  V(J)=V(J)/60.
767 CONTINUE
C INPUT AIRCRAFT CHARACTERISTICS
C ZMAX MAXIMUM CLIMB RATE FT./HR.
C ZMIN MAXIMUM DECENT RATE
C PDMAX MAXIUM ACCENT ANGLE
C PDMIN MAXIUM DECENT ANGLE
C TMAX AND TMIN MAXIMUM TURN ANGLES.
  DO 127 IT=1,ITYPE
  READ(5,102) ZMAX(IT),ZMIN(IT),TMAX(IT)
C WRITE(6,102)ZMAX(IT),ZMIN(IT),TMAX(IT)

```

```

----- TMIN(IT)=-TMAX(IT)
127 CONTINUE
100 FORMAT(4I1)
-----
C INNNITIALIZE
DO1J=1,N
C IS IS AIRCRAFT ASSIGNED TO RUNWAY
IS(J)=0
C KS(J) IS QURUE COUNT
KS(J)=0
-----
C TC IS TIME RUNWAY OCCUPIED
TC(J)=0.
C TS(J) IS TIME SINCE LAST ARRIVAL
IS(J)=0.
DO 1I=1,M
C X,Y,Z IS AIRCRAFT POSITION
X(J,I)=0.
Y(J,I)=0.
Z(J,I)=0.
IDENT(J,I)=0
JTYPE(J,I)=J/3 +1
1 CONTINUE
-----
C INCREMENT PROBLEM TIME
7 TI= TI +DT
IF(TI.GT.30.) GO TO 996
C CALL VACS
C VEHICLE ACCESS
C *****
C *****
C *****
IF(TI.LT.TWRITE) GO TO 1101
C PRINT OUTPUT FOR PROBLEM INTERVAL
TWRITE=TWRITE+DTWRIT
C WRITE(6,902)(COUNT(L),L=1,9) ,KS(L),L=1,4)
C RESET INDEX OF ORDERLINESS
COUNT(7)=0.
902 FORMAT(9F10.4,4I5)
C LABERT ST LOUIS SPECIAL
1101 CONTINUE
IAIR=0
PRIOR=0.0
DO797 J=1,N
IAIR=IS(J)+IAIR
PRI(J)=(TI/S(J))-COUNT(J)
IF(IDO(J).GT.0) PRIOR=PRIOR+PRI(J)
797 CONTINUE
IF(JUNK.GT.2) MTRAN(1)=IAIR
ITRAN=1
DO 750 J=1,N
IIS=IS(J)
XIS=IIS
DO 502 I=1,IIS
505 FORMAT(5E20.8)
IXAIR=X(J,I)*1500./40.
IF(JUNK.LT.1) GO TO 502
JFIF=2000.
IFIF=-2000
IF(IXAIR.GT.JFIF.OR.IXAIR.LT.IFIF) MTRAN(1)=MTRAN(1)-
IF(IXAIR.GT.JFIF.OR.IXAIR.LT.IFIF) GO TO 502

```



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ITRAN=ITRAN+1
IF (ITRAN.GT.144)GO TO 502
MTRAN(ITRAN)=IXAIR
IYAIR=Y(J,I)*1500./40.
IF (IYAIR.GT.JFIF.OR.IYAIR.LT.IFIF) ITRAN=ITRAN-1
IF (IYAIR.GT.JFIF.OR.IYAIR.LT.IFIF) MTRAN(1)=MTRAN(1)-1
IF (IYAIR.GT.JFIF.OR.IYAIR.LT.IFIF) GO TO 502
ITRAN=ITRAN+1
IF (ITRAN.GT.144)GO TO 502
MTRAN(ITRAN)=IYAIR
IZAIR=Z(J,I)*3000./8000. -2000.
IF (IZAIR.GT.JFIF.OR.IZAIR.LT.IFIF) ITRAN=ITRAN-2
IF (IZAIR.GT.JFIF.OR.IZAIR.LT.IFIF) MTRAN(1)=MTRAN(1)-1
IF (IZAIR.GT.JFIF.OR.IZAIR.LT.IFIF) GO TO 502
ITRAN=ITRAN+1
IF (ITRAN.GT.144) GO TO 502
MTRAN(ITRAN)=I7AIR
ITRAN=ITRAN+1
IF (ITRAN.GT.144) GO TO 502
MTRAN(ITRAN)=IDENT(J,I)
502 CONTINUE
750 CONTINUE
IWORD=2*IAIR+1
IF (ISENSE(1).GT.0.OR.ISENSE(2).GT.0) IWORD=0
IF (ISENSE(3).GT.0.OR.ISENSE(4).GT.0) IWORD=0
IF (IWORD.LE.0) GO TO 10
JUNN=0
IWORD=144
8 FORMAT(1X,I10)
IF (MTRAN(1).LE.0) GO TO 298
CALL CPXSN(IWORD,MTRAN,JUNN)
C
C
C
C
298 CONTINUE
C*****
JUNK=5
10 CONTINUE
C WRITE(6,308)
NNJ=N -1
308 FORMAT(15H CONFLICT TABLE)
JRXUA=JRXUA+1
IF (JRXUA.GE.N) JRXUA=1
J=JRXUA
IIS=IS(J)
C FLOW CONTROL
IFLOW=10
IF (IIS.GT.IFLOW) S(J)=S(J)*1.10
IF (IIS.LE.0) S(J)=0.90*S(J)
IF (IIS.LT.1) GO TO 1103
C CONFLICT PARAMETERS
C DISTR ACTION POINT FOR CONTROLLER BASED ON PROJECT STUPID
DISTR=5.0
C DISTL MINIMUM SEPERATION
DISTL=3.0
C ZCON MINIMUM ALTITUDE
ZCON =800.
C ALTM MINIMUM ALTITUDE SEPERATION

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ALTM=900.
DO 301 K=J,M
LLS=IS(K)
IF(LLS.LT.1) GO TO 301
DO 302 I=1,LLS
IF(Z(J,I).LT.ZCON) GO TO 302
DO 303 L=1,LLS
IF(Z(K,L).LT.ZCON) GO TO 303
C PREVENT ARRIVAL DEPARTURE INTERACTION
ZCOM=3200.
IF(Z(J,I).LT.ZCOM.AND.IDO(J).NE.IDO(K)) GO TO 303
C AIRCRAFT UNDER LOCAL CONTROLLED
ZCOMM=2200.
IF(Z(J,I).LT.ZCOMM.AND.IDO(J).GT.0) GO TO 303
IF(Z(K,L).LT.ZCOMM.AND.IDO(K).GT.0) GO TO 303
IF(Z(K,L).LT.ZCOM.AND.IDO(J).NE.IDO(K)) GO TO 303
ALT=ABS(Z(J,I)-Z(K,L))
IF(ALT.GT.ALTM) GO TO 303
DIST =SQRT(((X(J,I)-X(K,L))**2)+(Y(J,I)-Y(K,L))**2))
IF(DIST.GT.DISTR) GO TO 303
C CHECK FOR POSITIVE RELATIVE VELOCITY
KDIST=20.*DIST
IF(KDIST.GT.100) KDIST=100
IF(KDIST.LT.1) KDIST=1
IDIST(KDIST)=IDENT(J,I)
JDIST(KDIST)=IDENT(K,L)
LDIST=KDIST-1
IF(LDIST.LE.0) GO TO 970
DO 982 IRS=1,LDIST
IF(IDENT(J,I).EQ.IDIST(IRS).AND.IDENT(K,L).EQ.JDIST(IRS))GO TO 970
982 CONTINUE
GO TO 303
307 FORMAT(4I5,2F10.5)
970 IF(K.EQ.J.AND.L.LE.I) GO TO 303
C COUNT(7) IS INDEX OF ORDERLINESS
XMU=IS(J)*IS(K)
XMU=XMU*(DIST**2)
IF(XMU.LT.1.E-05) XMU=1.E-05
COUNT(7)=COUNT(7)+(1./XMU)
C LABERT ST LOUIS SPECIAL
IF(LIST.GT.11) GO TO 1102
C WRITE(6,307) J,J,IDENT(J,I),IDENT(K,L),ALT,DIST
1102 CONTINUE
IF(DIST.GT.DISTL) GO TO 980
C COUNT(6) IS THE CONFLICT COUNTER
COUNT(6)=COUNT(6)+DT
IF(DIST.LT.1.E-05) DIST=1.E-05
COUNT(8)=COUNT(8)+(DT/DIST)
C LABERT ST LOUIS SPECIAL
GO TO 980
IF(LIST.GT.11) GO TO 980
C WRITE(6,307) J,IDENT(J,I),K,IDENT(K,L),ALT,DIST
C HORIZONTAL CONFLICT RESOLUTION MAKES THE AIRCRAFT PATHS MORE PARALLEL
C DELETE CONFLICT RESOLUTION THIS RUN
980 GO TO 303
C 980 IT=JTYPE(J,I)
COR=PI/2.
IF(COS(TD(J,I)).EQ.0.) GO TO 762
XDIF=((XA(J,I)-XA(K,L))/COS(TD(J,I)))

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TCOS=COS(TD(K,L))/COS(TD(J,I))
762 TDX=TD(K,L)-COR-TD(J,I)
IF(YA(J,I).GT.YA(K,L)) TDX=-TDX
IF(XDIF.GT.0.) TDX=0.0
IF(TCOS.GT.0.) GO TO 802
TDX=0.0
IF(COS(TD(J,I)).LT.0..AND.XA(J,I).LT.XA(K,L)) GO TO 802
IF(COS(TD(J,I)).GT.0..AND.XA(J,I).GT.XA(K,L)) GO TO 802
IF(YA(K,L).EQ.YA(J,I)) YA(J,I)=YA(J,I)+1.E-05
COR=((YA(K,L)-YA(J,I))/ABS((YA(K,L)-YA(J,I))))*COR
IF(COS(TD(K,L)).LT.0.) COR=-COR
TDX=COR
802 CONTINUE
TXX=TMAX(IT)*DT
TNN=TMIN(IT)*DT
IF(TDX.GT.PI) TDX=TDX-2.*PI
PIJ=-PI
IF(TDX.LT.PIJ) TDX=2.*PI-TDX
IF(TDX.GT.TXX) TDX=TXX
IF(TDX.LT.TNN) TDX=TNN
TD(J,I)=TD(J,I)+TDX
IT=JTYPE(K,L)
COR=PI/2.
IF(COS(TD(J,I)).EQ.0.OR.COS(TD(K,L)).EQ.0.) GO TO 9999
XDIF=((XA(K,L)-XA(J,I))/COS(TD(K,L)))
TCOS=COS(TD(K,L))/COS(TD(J,I))
9999 CONTINUE
TDX=TD(J,I)-COR-TD(K,L)
IF(YA(K,L).GT.YA(J,I)) TDX=-TDX
IF(XDIF.GT.0.) TDX=0.0
IF(TCOS.GT.0.) GO TO 803
TDX=0.0
IF(COS(TD(K,L)).LT.0..AND.XA(K,L).LT.XA(J,I)) GO TO 803
IF(COS(TD(K,L)).GT.0..AND.XA(K,L).GT.XA(J,I)) GO TO 803
IF(YA(J,I).EQ.YA(K,L)) GO TO 803
COR=((YA(J,I)-YA(K,L))/ABS((YA(K,L)-YA(J,I))))*COR
IF(COS(TD(J,I)).LT.0.) COR=-COR
TDX=COR
803 CONTINUE
TXX=TMAX(IT)*DT
TNN=TMIN(IT)*DT
IF(TDX.GT.PI) TDX=TDX-2.*PI
PIJ=-PI
IF(TDX.LT.PIJ) TDX=2.*PI-TDX
IF(TDX.GT.TXX) TDX=TXX
IF(TDX.LT.TNN) TDX=TNN
TD(K,L)=TD(K,L)+TDX
C VERTICAL CONFLICT RESOLUTION MAKES THE AIRCRAFT PATHS SLOW
C COALTITUDE APPROACH
C XEX IS MAXIMUM DECENT ANGLE FOR EMERGENCIES
XEX=2.*PI*DT/180.
EX=(ZA(J,I)-ZA(K,L))/ALTM
IF(EX.EQ.0.) EX=1./XEX
EX=1./EX
IF(EX.GT.XEX) EX=XEX
XEX=-XEX
IF(EX.LT.XEX) EX=XEX
PD(J,I)=PD(J,I)-EX
PD(K,L)=PD(K,L)+EX

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CALL VELO(TD(J,I),TT(J,I),VD(J,I),VT(J,I),PD(J,I),PT(J,I))
CALL VELO(TD(K,L),TT(K,L),VD(K,L),VT(K,L),PD(K,L),PT(K,L))
303 CONTINUE
302 CONTINUE
301 CONTINUE
IF(TLIST.GT.TI) GO TO 1103
TLIST=TLIST+0.1
1103 CONTINUE
103 DO2KJ=1,NCLASS
J=KJ
IF(NCLASS.GT.N) J=KJ-2
C CHECK FOR NEW PLANE ARRIVAL
C HAND OFF FROM ON ROUTE CONTROLLER
IF(TI.GT.PH(KJ)) TS(KJ)=TS(KJ)+DT
IF(TS(KJ).LT.S(KJ)) GO TO 2
TS(KJ)=0.
C VACS INSETRS
C *****
C *****
C *****
C IF(IDO(J).LT.0) CALL VACB(J,KT)
C IF(IDO(J).LT.0.AND KT.LT.0) GO TO 2
C UPDATE PLANE COUNTER FOR NEW ARRIVAL
IF(IDO(J).GT.0) IS(J)=IS(J)+1
IF(IS(J).GT.M) IS(J)=M
C SET COUNTER FOR NEW DEPARTURE QUEUE ENTRY
IF(IDO(J).LT.0) KS(J)=KS(J)+1
IF(IDO(J).GT.0) I=IS(J)
IF(IDO(J).LT.0) I=KS(J)+IS(J)
IF(I.GT.M) I=M
KSIGN=KSIGN+1
IF(KSIGN.GT.99) KSIGN=1
IDENT(J,I)=KSIGN
JTYPE(J,I)=KJ/2 +1
IF(JTYPE(J,I).GT.ITYPE) JTYPE(J,I)=ITYPE
C TRANSFER POSITION TO PILOT
104 CALL ARIVIT(J)
CALL POSIT(XS(J),X(J,I),YS(J),Y(J,I),ZS(J),Z(J,I))
C TRANSFER POSITION TO CONTROLLER VIA RADAR ETC.
CALL POSIT(XS(J),XA(J,I),YS(J),YA(J,I),ZS(J),ZA(J,I))
C TRANSMIT VELOCITY, BEARING, CLIMB TO PILOT VIA INSTRUMENTS
CALL VELO(T(J),TT(J,I),V(J),VT(J,I),P(J),PT(J,I))
C TRANSMIT MOTION DATA TO CONTROLLER VIA DATA LINK
CALL VELO(T(J),TD(J,I),V(J),VD(J,I),P(J),PD(J,I))
2 CONTINUE
12 FORMAT(1X,I10,I10)
11 FORMAT(1X,I10,F10.5)
J=1
375 CONTINUE
I=0
C CHECK FOR TAKEOFF
IF(IDO(J).LT.0) GO TO 205
17 IF(IS(J).LT.1) GO TO 3
I=I+1
13 FORMAT(1X,6F10.5)
XPI=2.*PI
IF(TT(J,I).GT.PI) TT(J,I)=TT(J,I)-XPI
PI=-PI
IF(TT(J,I).LT.PI) TT(J,I)=TT(J,I)+XPI

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        PI=3.14159
        CALL PLANE(X(J,I),Y(J,I),Z(J,I),TT(J,I),VT(J,I),PT(J,I))
C CONTROLLNR-ESTIMATES NEW POSITION AND UPDATES INSTRUCTIONS IF REQUIRED
C COUNT(10) CONTROLS STACKING OF EXCESS ARRIVAL AIRCRAFT
        COUNT(10)=I*IDO(J)
        CALL PLAND(XA(J,I),YA(J,I),ZA(J,I),TD(J,I),VD(J,I),PD(J,I),J,
1JTYPE(J,I),I)
C TRANSMIT POSITION TO CONTROLLER VIA RADAR ETC.
        CALL POSIT(X(J,I),XA(J,I),Y(J,I),YA(J,I),Z(J,I),ZA(J,I))
C CONTROLLER TRANSMITS DIRECTIONS TO PILOT
        CALL VELO(TD(J,I),TT(J,I),VD(J,I),VT(J,I),PD(J,I),PT(J,I))
C GO TO 200 FOR DEPARTING AIRCRAFT TAKE OFF ROUTINE
        IF(IDO(J).LT.0) GO TO 200
C ARRIVING AIRCRAFT LANDING ROUTINE
C INTER RUNWAY CONFLICT ARRIVAL CONTROL
        NDEP=-2
        JDEP=ISENSE(J)
        IF(ISENSE(J).LT.0)ISENSE(J)=0
        IF(JDEP.LT.NDEP) TS(J)=TS(J)-DT
C IF PLANE HAS NOT LANDED GO TO 5
        IF(Z(J,I).GT.0.) GO TO 5
C VAXC INSERT
C *****
C *****
C *****
C *****
C        CALL VACX(X(J,I),Y(J,I),J,IDENT(J,I))
C COMPUTE LANDING COUNTERS AND OCCUPANCY
C COUNT(5) IS DUAL OCCUPANCY COUNTER
        CALL DUAL(TC,J)
        IF(TC(J).LE.TI)TC(J)=0.
        IF(TC(J).GT.0.)COUNT(5)=COUNT(5)+1.
        TC(J)=TI + TOC(J)
C COUNT(J) IS NUMBER OF PLANES LANDED
        COUNT(J)=COUNT(J)+1.
C DELETE LANDED PLANE FROM CONTROLLER WORK LOAD
        ISJ=IS(J)
        ISI=I+1
        IF(ISI.GE.ISJ)GO TO 270
        DO 4 K=ISI,ISJ
        X(J,K-1)=X(J,K)
        Y(J,K-1)=Y(J,K)
        Z(J,K-1)=Z(J,K)
        TT(J,K-1)=TT(J,K)
        VT(J,K-1)=VT(J,K)
        PT(J,K-1)=PT(J,K)
        IDENT(J,K-1)=IDENT(J,K)
4 CONTINUE
270 CONTINUE
        IS(J)=IS(J)-1
        I=I-1
        IF(IS(J).GT.M) IS(J)=M
5 IF(I.LT.IS(J)) GO TO 17
        GO TO 3
C DEPARTURE ROUTINE
200 DMAX=40.
        XOI=0.0
        YOI=0.0
        DRUN=SQRT((((X(J,I)-XOI)**2)+((Y(J,I)-YOI)**2)))

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IF(DRUN.LT.DMAX)GO TO 5
C HAND OFF REQUIRED
XH=X(J,I)
YH=Y(J,I)
ZH=Z(J,I)
TH=TT(J,I)
VH=VT(J,I)
PHH=PT(J,I)
JDENT=IDENT(J,I)
II=IS(J)-1
IF(II.LT.I) GO TO 275
DO 204 K=I,II
X(J,K)=X(J,K+1)
Y(J,K)=Y(J,K+1)
Z(J,K)=Z(J,K+1)
TT(J,K)=TT(J,K+1)
VT(J,K)=VT(J,K+1)
PT(J,K)=PT(J,K+1)
IDENT(J,I)=IDENT(J,K+1)
204 CONTINUE
C REDUCE CONTROLLER LOAD
275 IS(J)=IS(J)-1
I=I-1
GO TO 5
C RUNWAY OCCUPIED
205 CALL DUAL(TC,J)
IF(TC(J).GT.TI) GO TO 17
TC(J)=0.0
C IF BACKUP IN LANDING SUSPEND TAKEOFFS
IF(IDO(J).LT.0.AND.PRIOR.GT.10.)GO TO 17
C NO AIRCRAFT READY FOR TAKEOFF GO TO 17
IF(KS(J).LE.0) GO TO 17
C CHECK FOR CONFLICT WITH DEPENDENT RUNWAY
NDEP=-2
JDEP=ISENSE(J)
IF(ISENSE(J).LT.0) ISENSE(J)=0
IF(JDEP.LT.NDEP) GO TO 17
C COUNT TAKEOFFS
COUNT(J)=COUNT(J)+1
TC(J)=TI+TOC(J)
C REDUCE QUEUE
KS(J)=KS(J)-1
C INCREASE CONTROLLER LOAD
IS(J)=IS(J)+1
IF(IS(J).GT.M)IS(J)=M
IIA=IS(J)
C VTAC IS TAKEOFF VELOCITY
C
C
C STOL CORRECTION
IF(J.LT.3) VTAC=140./60.
IF(J.GE.3) VTAC= 70./60.
C
C
C VD(J,IIA)=VTAC
VT(J,IIA)=VTAC
C
C
C STOL CORRECTION

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PDTAC=-3.*PI/180.
IF(J.GE.3) PDTAC=-8.*PI/180.
PI(J,IJA)=PDTAC
PD(J,IIA)=PDTAC
IF(KS(J).GT.0) TC(J)=TI+TOC(J)
4000 FORMAT(1X,20HERROR ISTEP ALTITUDE,E20.9,3I10)
GO TO 17
C 3 CONTINUE
3 J=J+1
IF(J.LE.N) GO TO 375
GO TO 7
END
$IBFTC TWO
SUBROUTINE STACK(ITC,XA,YA,ZA,TD)
DIMENSION XO(4),YO(4),RR(4)
PI=3.14159/2.
RR(1)=20.
RR(2)=20.
RR(3)=20.
RR(4)=20.
XO(1)=20.
XO(2)=0.
XO(3)=-20.
XO(4)=0.
YO(1)=0.
YO(2)=20.
YO(3)=-20.
YO(4)=0.
C KZM IS MINIMUM STACKING ALTITUDE
KZM=5000
CNAL IS AIRCRAFT PER ALTITUDE
NAL=4
KT=(ITC/NAL)-1
C ZA IS ASSIGNED STACKING ALTITUDE
ZA=KT*1000+KZM
C IT IS AIRCRAFT IN UNFILLED CIRCLE
IT=ITC-KT*NAL
IF(IT.GT.NAL) IT=NAL
XXA=XA-XO(IT)
YYA=YA-YO(IT)
ATD=ATAN2(XXA,YYA)
DIST=SQRT(((XA-XO(IT))**2)+((YA-YO(IT))**2))
ERR=DIST-RR(IT)
IF(ERR.GT.1.) TD=-ATD
IF(ERR.LT.1.) TD=ATD+PI
ERR=-ERR
IF(ERR.GT.1.) TD=ATD
RETURN
END
$IRFTC THRF
SUBROUTINE EXPECT(XA,YA,ZA,TD,VD,PD)
C THIS SUBROUTINE UPDATES POSITION
COMMON/U/DT,TI
COMMON/A/ISFNS
COMMON/B/COUNT
DIMENSION COUNT(10)
DIMENSION ISENSE(4)
C VH HORIZONTAL VFLOCITY
VH=VD*COS(PD)

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XA=XA+(VH*DT*COS(TD))
YA=YA+(VH*DT*SIN(TD))
ZA=ZA/5280.
ZA=ZA-(VD*DT*SIN(PD))
ZA=ZA*5280.
RETURN
END
$IBFTC FOUR
SUBROUTINE PLANF(X,Y,Z,T,V,P)
C THIS SUBROUTINE UPDATES AIRCRAFT POSITION
COMMON/A/ISENSF
COMMON/B/COUNT
DIMENSION COUNT(10)
DIMENSION ISENSF(4)
C SUBROUTINE ERROR INPUTS WIND AND OTHER ERRORS TO VELOCITY AND HEADING
CALL ERROR(V,P,T)
C SUBROUTINE EXPECT GENERATES NEW POSITION
CALL EXPECT(X,Y,Z,T,V,P)
RETURN
END
$IBFTC FIVE
SUBROUTINE ERROR(V,R,T)
C THIS SUBROUTINE INPUTS ERROR
COMMON/A/ISENSF
COMMON/B/COUNT
DIMENSION COUNT(10)
DIMENSION ISENSE(4)
C VE MAXIMUM VELOCITY ERROR
VE=0.1
C TE MAXIMUM BEARING ERROR
TE=0.01
C RANDOM GENERATING FUNCTION FOR VELOCITY ERROR. ANOTHER DISTRIBUTION MAY BE
C SUBSTITUTED FOR THIS OR ANY OTHER GENERATING FUNCTION.
P=RAN(JX)
S=RAN(JX)
IF(S.GT.0.5) P=-P
V=V+VE*P
C RANDOMLY GENERATED BEARING ERROR.
P=RAN(JX)
S=RAN(JX)
IF(S.GT.0.5) P=-P
T=T+TE*P
C RANDOMLY GENERATED CLIMB ERROR.
P=RAN(JX)
S=RAN(JX)
IF(S.GT.0.5) P=-P
R=R+TE*P
RETURN
END
$IBFTC SIX
SUBROUTINE RUNWAY(J,XA,YA,ZA,TD,VD,PD)
C THIS SUBROUTINE SETS RUWAY CRITERIA COMMON TO ALL RUNWAYS.
COMMON/R/IDO
COMMON/P/ XS,YS,ZS,T
COMMON /M/MTRAN
COMMON/A/ISENSF
COMMON/B/COUNT
DIMENSION IDO(4)
DIMENSION XS(4),YS(4),ZS(4),T(4)

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        DIMENSION MTRAN(144)
        DIMENSION COUNT(10)
        DIMENSION ISENSE(4)


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C CALL SPECIFIC RUNWAY TO SET RUNWAY SPECIFIC CRITERIA.
  GO TO (1,2,3,4),J
    1 CALL RUNONE(PD,VD,XA,YA,ZA,TD)
      GO TO 10
    2 CALL RUNTWO(PD,VD,XA,YA,ZA,TD)
      GO TO 10
    3 CALL RUNTHR(PD,VD,XA,YA,ZA,TD)
      GO TO 10
    4 CALL RUNFOU(PD,VD,XA,YA,ZA,TD)
      GO TO 10
  10 IF(VD.LT.0.) RETURN
C VELOCITY CONTROL IN AIRPORT AREA MAY BE EXPANDED
  DISTR=4.0
  ALTM=900.
C VDAIR RESET FOR STOL AIRCRAFT
C
C STOL CORRECTION
  VDAIR=280.
  IF(J.GT.2) VDAIR=140.
  DISTO=3.0
C INTRA RUNWAY AIRCRAFT SPACING
  IF(J.NE.J0) GO TO 20
  ALT=ABS(7A-7A0)
  ZA0=7A
  IF(ALT.GT.ALTM) GO TO 20
  DIST=SQRT(((XA-XA0)**2)+((YA-YA0)**2))
  DTA=-1.
  TEMP= VD*COS(PD)*COS(TD)
  IF(XA0.GT.XA.AND.TEMP.GT.0.) DTA=1.
  IF(XA0.LT.XA.AND.TEMP.LT.0.) DTA=1.
  TEMP= VD*COS(PD)*SIN(TD)
  DTY=-1.
  IF(YA0.GT.YA.AND.TEMP.GT.0.) DTY=-1.
  IF(YA0.LT.YA.AND.TEMP.LT.0.) DTY=-1.
  DTA=DTA/DTY
  XA0=XA
  YA0=YA
  VD=60.*VD
  IF(DIST.LT.DISTO.AND.DTA.GE.0.) VD=VD-20.
  IF(DIST.LT.DISTO.AND.DTA.LE.0.) VD=VD+20.
  IF(DIST.GT.DISTB.AND.VD.LT.VDAIR) VD=VD+20.
  VDAIRX=VDAIR+40.
  IF(VD.GT.VDAIRX) VD=VD-20.
  IF(VD.LT.140.) VD=140.
  VD=VD/60.
  20 JO=J
  RETURN
  END
$IBFTC SEVEN
  SUBROUTINE RUNONE(PD,VD,XA,YA,ZA,TD)
C THIS SUBROUTINE SETS CRITERIA FOR RUNWAY ONE.
  COMMON /R/ IDO
  COMMON /A/ ISENSE
  COMMON /B/ COUNT
  COMMON /P/ XS,YS,ZS,T
  COMMON /M/ MTRAN
  DIMENSION XS(4),YS(4),ZS(4),T(4)

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DIMENSION IDO(4)
DIMENSION MTRAN(144)
DIMENSION ISENSE(4)
DIMENSION COUNT(10)
102 FORMAT (6F10.5)
JRUN=IDO(1)
TDU=TD
IF (ISENSF(1).LT.1) GO TO 103
CALL INPUT(XRS,YRS,THETA,THETB,DAP,DDI,ERROR,JRUN,RLFN,WAKE)
ISENSF(1)=0
C INPUT RUNWAY GEOMETRY AND ACCEPTABLE ERROR
C XAM,YAM IS THE APPROACH OUTER MARKER
C DAP IS APPROACH DISTANCE
C RLEN IS RUNWAY LENGTH
C DDI IS THE DEPARTURE OUTER MARKER DISTANCE
C THETA ANGLE OF RUNWAY WITH NORTH
C ERROR ACCEPTABLE DEVIATION IN APPROACH.
C ST. LOUIS LAMBERT FIELD RUNWAY 12R
C WRITE(6,102)XRS,YRS,DAP,RLFN,DDI,THETA,ERROR
YMIN=YRS
YMAX=YRS
XMIN=XRS
XMAX=XRS
XAM=XRS +DAP*SIN(THETB)
YAM=YRS +DAP*COS(THETB)
IF(XAM.GT.XMAX) XMAX=XAM
IF(XAM.LT.XMIN) XMIN=XAM
IF(YAM.GT.YMAX) YMAX=YAM
IF(YAM.LT.YMIN) YMIN=YAM
XRE=XAM-(RLEN+DAP)*SIN(THETA)
YRE=YAM-(RLEN+DAP)*COS(THETA)
IF(XRE.LT.XMIN) XMIN=XRE
IF(XRE.GT.XMAX) XMAX=XRE
IF(YRE.LT.YMIN) YMIN=YRE
IF(YRE.GT.YMAX) YMAX=YRE
XDM=XAM-(RELEN+DAP+DDI)*SIN(THETA)
YDM=YAM-(RELEN+DAP+DDI)*COS(THETA)
IF(XDM.GT.XMAX) XMAX=XDM
IF(XDM.LT.XMIN) XMIN=XDM
IF(YDM.LT.YMIN) YMIN=YDM
IF(YDM.GT.YMAX) YMAX=YDM
YAB=(YRS+YRE)/2.
IYA=YRS*1500./40.
IXA=XRS*1500./40.
JXA=XRE*1500./40.
JYA=YRE*1500./40.
MTRAN(2)=IXA
MTRAN(3)=IYA
MTRAN(4)=JXA
MTRAN(5)=JYA
103 PI=3.14159
C JRUN NEGATIVE IS DEPARTURE CODE
IF(JRUN.GT.0) GO TO 7
C DEPARTURE PATTERN
I(1)=THETA+PI
XS(1)=XRE
YS(1)=YRE
ZS(1)=0.
DP=SQRT(((XA-XRE)**2)+((YA-YRE)**2))

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CALL INTCON(XAM,YAM,JRIN,DP,IAB)
IF(YA.GT.YMAX) TD=PI/2.
IF(YA.LT.YMIN) TD=-PI/2.
XPFL=XA/XAM
IF(XPFL.GF.1.) TD=-PI/2.
IF(XPFL.LT.1.) TD=PI/2.
IF(ZA.LT.800.) TD=THETA+PI
VD=60.*VD
IF(ZA.LT.800..AND.VD.LT.140.) VD=VD+20.
IF(ZA.LT.800.) VD=-VD
VD=VD/60.
CALL SID(XA,YA,ZA,TD,PD,YDM,XDM,JRIN)
RETURN
C VH HORIZONTAL VELOCITY
7 VH=VD*COS(PD)
C APPROACH PATTERN
C DISM IS MINIMUM TURN DISTANCE
DISM=10.
C DIST IS DISTANCE TO APPROACH MARKER
DIST=SQRT(((XA-XAM)**2)+((YA-YAM)**2))
IF(DIST.LT.DISM) GO TO 20
YCA=ARS(YA-YAM)
XCA=ARS(XA-XAM)
IF(YCA.LT.DISM.OR.XCA.LT.DISM) GO TO 20
C COMPUTE DESIRED VECTOR
IF(YA.GT.YMAX.AND.XA.GT.XMAX)TD=-PI/2.
IF(YA.GT.YMAX.AND.XA.LT.XMIN)TD=-PI/2.
IF(YA.LT.YMAX.AND.XA.LT.XMIN)TD= PI/2.
IF(YA.LT.YMAX.AND.XA.GT.XMAX)TD= PI/2.
YCA=ARS(YA-YMAX)
IF(YCA.LT..05.AND.XA.GT.XMAX) TD=PI
IF(YCA.LT..05.AND.XA.LT.XMIN) TD=0.
IF(XA.LT.XMIN.OR.XA.GT.XMAX) RETURN
IF(ANGLE.GT.0.) TD=0.
IF(ANGLE.LT.0.) TD=PI
IF(YA.LT.YMIN.OR.YA.GT.YMAX) RETURN
C COMPUTE ANGLE TO OUTER MARKER
20 SINTD=(YA-YAM)/DIST
ATD=ARSIN(SINTD)
IF(ATD.GT.0..AND.XA.LT.XAM)ATD =ATD+PI/2.
IF(ATD.LT.0..AND.XA.LT.XAM)ATD =ATD-PI/2.
PII=-PI/2.
IF(THETA.GT.0..AND.ATD.GT.PII) TD=ATD+PI
IF(THETA.GT.0..AND.ATD.GT.PII) RETURN
IF(ATD.GT.0..AND.THETA.LT.0.) TD=ATD+PI
IF(ATD.GT.0..AND.THETA.LT.0.) RETURN
IF(ATD.LT.PII.AND.THETA.LT.0.) TD=ATD+PI
IF(ATD.LT.PII.AND.THETA.LT.0.) RETURN
C IF ABORTING SET DECFNT RATE TO ZERO
PD=0.
IF(YA.LT.YAB.AND.THETA.LT.0.) TD=-PI/2.
IF(YA.LT.YAB.AND.THETA.GT.0.) TD= PI/2.
IF(YA.LT.YAB) RETURN
C ENTERING APPROACH PATH TURN
C CORRECT APPROACH ANGLE TO RUNWAY END
DP=SQRT(((XA-XPS)**2)+((YA-YRS)**2))
C CHECK FOR CONFLICT WITH DEPENDENT RUNWAY
CALL INTCON(XAM,YAM,JRIN,DP,IAB)
IF(DP.FQ.0.) DP=1.F-05

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SINTD=(YA-YRS)/DP
TD=ARSIN(SINTD)
IF(XA.LT.XRS) TD=TD+PI/2.
TD=TD+PI
C COMPUTE DECENT RATE
ZA=7A/5280.
TANPD=ZA/DP
ZA=5280.*ZA
PD=ATAN(TANPD)
PDMAX=3.*PI/180.
IF(PD.GT.PDMAX) PD =PDMAX
VD=60.*VD
IF(VD.GT.130.) VD=VD-20.
VD=-VD/60.
RETURN
END
$IBFTC EIGHT
SUBROUTINE RUNTWO(PD,VD,XA,YA,ZA,TD)
C THIS SUBROUTINE SETS CRITERIA FOR RUNWAY TWO
COMMON /R/ IDO
COMMON /A/ ISFNSF
COMMON /B/ COUNT
COMMON /P/ XS,YS,ZS,T
COMMON /M/ MTRAN
DIMENSION XS(4),YS(4),ZS(4),T(4)
DIMENSION IDO(4)
DIMENSION MTRAN(144)
DIMENSION ISENSE(4)
DIMENSION COUNT(10)
102 FORMAT (5F10.5)
TDU=TD
IF(ISFNSF(2).LT.1) GO TO 103
JRUN=2*IDO(2)
CALL INPUT(XRS,YRS,THETA,THETB,DAP,DDI,ERROR,JRUN,RLEN,WAKE)
ISENSE(2)=0
C INPUT RUNWAY GEOMETRY AND ACCEPTABLE ERROR
C XAM,YAM IS THE APPROACH OUTER MARKER
C DAP IS APPROACH DISTANCE
C RLEN IS RUNWAY LENGTH
C DDI IS THE DEPARTURE OUTER MARKER DISTANCE
C THETA ANGLE OF RUNWAY WITH NORTH
C ERROR ACCEPTABLE DEVIATION IN APPROACH.
C ST. LOUIS LAMBERT FIELD RUNWAY 12R
C ST. LOUIS LAMBERT FIELD RUNWAY 12L
C WRITE(6,102)XRS,YRS,DAP,RLEN,DDI,THETA,ERROR
YMIN=YRS
YMAX=YRS
XMIN=XRS
XMAX=XRS
XAM=XRS +DAP*SIN(THETB)
YAM=YRS +DAP*COS(THETB)
IF(XAM.GT.XMAX) XMAX=XAM
IF(XAM.LT. XMIN) XMIN=XAM
IF(YAM.GT.YMAX) YMAX=YAM
IF(YAM.LT. YMIN) YMIN=YAM
XRE=XAM-(RLEN+DAP)*SIN(THETA)
YRE=YAM-(RLEN+DAP)*COS(THETA)
IF(XRE.LT.XMIN) XMIN=XRE
IF(XPF.GT.XMAX) XMAX=XRF

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IF(YRF.LT.YMIN) YMIN=YRF
IF(YRF.GT.YMAX) YMAX=YRF
XDM=XAM-(RELEN+DAP+DDI)*SIN(THETA)
YDM=YAM-(RELEN+DAP+DDI)*COS(THETA)
IF(XDM.GT.XMAX) XMAX=XDM
IF(XDM.LT.XMIN) XMIN=XDM
IF(YDM.LT.YMIN) YMIN=YDM
IF(YDM.GT.YMAX) YMAX=YDM
YAB=(YRS+YRF)/2.
IXA=XRS*1500./40.
IYA=YRS*1500./40.
JXA=XRF*1500./40.
JYA=YRF*1500./40.
MTRAN(6)=IXA
MTRAN(7)=IYA
MTRAN(8)=JXA
MTRAN(9)=JYA
103 PI=3.14159
C JRUN NEGATIVE IS DEPARTURE CODF
IF(JRUN.GT.0) GO TO 7
C DEPARTURE PATTERN
T(2)=THETA+PI
XS(2)=XRF
YS(2)=YRF
ZS(2)=0.
DP=SQRT(((XA-XRE)**2)+((YA-YRE)**2))
CALL INTCON(XAM,YAM,JRUN,DP,IAB)
IF(YA.GT.YMAX) TD=PI/2.
IF(YA.LT.YMIN) TD=-PI/2.
XREL=XA/XAM
IF(XREL.GE.1.) TD=-PI/2.
IF(XREL.LT.1.) TD=PI/2.
IF(ZA.LT.800.) TD=THETA+PI
VD=60.*VD
IF(ZA.LT.800..AND.VD.LT.140.) VD=VD+20.
IF(ZA.LT.800.) VD=-VD
VD=VD/60.
CALL SID(XA,YA,ZA,TD,PD,YDM,XDM,JRUN)
RETURN
C VH HORIZONTAL VFLOCITY
7 VH=VD*COS(PD)
C APPROACH PATTERN
C DISM IS MINIMUM TURN DISTANCE
DISM=10.
C DIST IS DISTANCE TO APPROACH MARKER
DIST=SQRT(((XA-XAM)**2)+((YA-YAM)**2))
IF(DIST.LT.DISM) GO TO 20
YCA=ABS(YA-YAM)
XCA=ABS(XA-XAM)
IF(YCA.LT.DISM.OR.XCA.LT.DISM) GO TO 20
C COMPUTE DESIRED VECTOR
IF(YA.GT.YMAX.AND.XA.GT.XMAX) TD=-PI/2.
IF(YA.GT.YMAX.AND.XA.LT.XMIN) TD=-PI/2.
IF(YA.LT.YMAX.AND.XA.LT.XMIN) TD=PI/2.
IF(YA.LT.YMAX.AND.XA.GT.XMAX) TD=PI/2.
YCA=ABS(YA-YMAX)
IF(YCA.LT..05.AND.XA.GT.XMAX) TD=PI
IF(YCA.LT..05.AND.XA.LT.XMIN) TD=0.
IF(XA.LT.XMIN.OR.XA.GT.XMAX) RETURN

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      IF (ANGLE.GT.0.) TD=0.
      IF (ANGLE.LT.0.) TD=PI
      IF (YA.LT.YMIN.OR.YA.GT.YMAX) RETURN
C COMPUTE ANGLE TO OUTER MARKER
      20 SINTD=(YA-YAM)/DIST
      ATD=ARSIN(SINTD)
      IF (ATD.GT.0..AND.XA.LT.XAM) ATD =ATD+PI/2.
      IF (ATD.LT.0..AND.XA.LT.XAM) ATD =ATD-PI/2.
      PII=-PI/2.
      IF (THETA.GT.0..AND.ATD.GT.PII) TD=ATD+PI
      IF (THETA.GT.0..AND.ATD.GT.PII) RETURN
      IF (ATD.GT.0..AND.THETA.LT.0.) TD=ATD+PI
      IF (ATD.GT.0..AND.THETA.LT.0.) RETURN
      IF (ATD.LT.PII.AND.THETA.LT.0.) TD=ATD+PI
      IF (ATD.LT.PII.AND.THETA.LT.0.) RETURN
C IF ABORTING SET DECENT RATE TO ZERO
      PD=0.
      IF (YA.LT.YAR.AND.THETA.GT.0.) TD= PI/2.
      IF (YA.LT.YAR.AND.THETA.LT.0.) TD=-PI/2.
      IF (YA.LT.YAR) RETURN
C ENTERING APPROACH PATH TURN
C CORRECT APPROACH ANGLE TO RUNWAY END
      DP=SQRT(((XA-XRS)**2)+((YA-YRS)**2))
C CHECK FOR CONFLICT WITH DEPENDENT RUNWAY
      CALL INTCON(XAM,YAM,JRUN,DP,IAB)
      IF (DP.EQ.0.) DP=1.F-05
      SINTD=(YA-YRS)/DP
      TD=ARSIN(SINTD)
      IF (XA.LT.XRS) TD=TD+PI/2.
      TD=TD+PI
C COMPUTE DECENT RATE
      7A=7A/5280.
      TANPD=7A/DP
      ZA=5280.*ZA
      PD=ATAN(TANPD)
      PDMAX=3.*PI/180.
      IF (PD.GT.PDMAX) PD =PDMAX
      VD=60.*VD
      IF (VD.GT.130.) VD=VD-20.
      VD=-VD/60.
      RETURN
      END
$IBFTC NINE
      SUBROUTINE RUNTHR(PD,VD,XA,YA,ZA,TD)
C THIS SUBROUTINE SETS CRITERIA FOR RUNWAY THREE
      COMMON /R/ IDO
      COMMON /M/MTRAN
      COMMON /A/ISFNSF
      COMMON /B/COUNT
      COMMON /P/ XS,YS,ZS,T
      DIMENSION MTRAN(144)
      DIMENSION IDO(4)
      DIMENSION XS(4),YS(4),ZS(4),T(4)
      DIMENSION ISENSE(4)
      DIMENSION COUNT(10)
      102 FORMAT (6F10.5)
      TDU=TD
      IF (ISFNSF(3).LT.1) GO TO 103
      JRUN=3*IDO(3)

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      CALL INPUT(XRS,YRS,THETA,THETB,DAP,DDI,ERROR,JRUN,RLEN,WAKE)
      ISENSE(3)=0
C INPUT RUNWAY GEOMETRY AND ACCEPTABLE ERROR
C XAM,YAM IS THE APPROACH OUTER MARKER
C DAP IS APPROACH DISTANCE
C RLEN IS RUNWAY LENGTH
C DDI IS THE DEPARTURE OUTER MARKER DISTANCE
C THETA ANGLE OF RUNWAY WITH NORTH
C ERROR ACCEPTABLE DEVIATION IN APPROACH.
C ST. LOUIS LAMBERT FIELD RUNWAY STOL LAND
C STOL RUNWAY MUST BE A MINIMUM OF 2500. FEET FROM OTHER
C RUNWAYS DUE TO WAKE TURBULENCE
      XRS=0.0-WAKE*COS(THETA)
      YRS=YRS+WAKE*SIN(THETA)
      DCR=8000./5280.
      XRS=XRS-DCR*SIN(THETA)
      YRS=YRS-DCR*COS(THETA)
C WRITE(6,102)XRS,YRS,DAP,RLEN,DDI,THETA,ERROR
      YMIN=YRS
      YMAX=YRS
      XMIN=XRS
      XMAX=XRS
      XAM=XRS +DAP*SIN(THETB)
      YAM=YRS +DAP*COS(THETB)
      IF(XAM.GT.XMAX) XMAX=XAM
      IF(XAM.LT.XMIN) XMIN=XAM
      IF(YAM.GT.YMAX) YMAX=YAM
      IF(YAM.LT.YMIN) YMIN=YAM
      XRE=XRS -(RLEN)*SIN(THETA)
      YRE=YRS -(RLEN)*COS(THETA)
      IF(XRE.LT.XMIN) XMIN=XRE
      IF(XRE.GT.XMAX) XMAX=XRE
      IF(YRE.LT.YMIN) YMIN=YRE
      IF(YRE.GT.YMAX) YMAX=YRE
      XDM=XRS-(RLEN+DDI)*SIN(THETA)
      YDM=YRS-(RLEN+DDI)*COS(THETA)
      IF(XDM.GT.XMAX) XMAX=XDM
      IF(XDM.LT.XMIN) XMIN=XDM
      IF(YDM.LT.YMIN) YMIN=YDM
      IF(YDM.GT.YMAX) YMAX=YDM
      YAB=(YRS+YRE)/2.
      IXA=XRS*1500./40.
      IYA=YRS*1500./40.
      JXA=XRE*1500./40.
      JYA=YRE*1500./40.
      MTRAN(14)=IXA
      MTRAN(15)=IYA
      MTRAN(16)=JXA
      MTRAN(17)=JYA
      103 PI=3.14159
C JRUN NEGATIVE IS DEPARTURE CODE
      IF(JRUN.GT.0) GO TO 7
C DEPARTURE PATTERN
      ZS(3)=0.
      YS(3)=YRF
      XS(3)=XRF
      T(3)=THETA+PI
      DP=SQRT(((XA-XRE)**2)+((YA-YRE)**2))
      CALL INTCON(XAM,YAM,JRUN,DP,IAB)

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IF(YA.GT.YMAX) TD=PI/2.
IF(YA.LT.YMIN) TD=-PI/2.
XREL=XA/XAM
IF(XREL.GE.1.) TD=-PI/2.
IF(XRFL.LT.1.) TD=PI/2.
IF(ZA.LT.800.) TD=THETA+PI
VD=60.*VD
IF(ZA.LT.800..AND.VD.LT.140.) VD=VD+20.
IF(ZA.LT.800.) VD=-VD
VD=VD/60.
      CALL SID(XA,YA,ZA,TD,PD,YDM,XDM,JRUN)
RETURN
C VH HORIZONTAL VFLOCITY
  7 VH=VD*COS(PD)
C APPROACH PATTERN
C DISM IS MINIMUM TURN DISTANCE
  DISM=10.
C DIST IS DISTANCE TO APPROACH MARKER
  DIST=SQRT(((XA-XAM)**2)+((YA-YAM)**2))
  IF(DIST.LT.DISM) GO TO 20
  YCA=ARS(YA-YAM)
  XCA=ARS(XA-XAM)
  IF(YCA.LT.DISM.OR.XCA.LT.DISM) GO TO 20
C COMPUTE DESIRED VECTOR
  IF(YA.GT.YMAX.AND.XA.GT.XMAX)TD=-PI/2.
  IF(YA.GT.YMAX.AND.XA.LT.XMIN)TD=-PI/2.
  IF(YA.LT.YMAX.AND.XA.LT.XMIN)TD= PI/2.
  IF(YA.LT.YMAX.AND.XA.GT.XMAX)TD= PI/2.
  YCA=ARS(YA-YMAX)
  IF(YCA.LT..05.AND.XA.GT.XMAX) TD=PI
  IF(YCA.LT..05.AND.XA.LT.XMIN) TD=0.
  IF(XA.LT.XMIN.OR.XA.GT.XMAX) RETURN
  IF(ANGLE.GT.0.) TD=0.
  IF(ANGLE.LT.0.) TD=PI
  IF(YA.LT.YMIN.OR.YA.GT.YMAX) RETURN
C COMPUTE ANGLE TO OUTER MARKER
  20 SINTD=(YA-YAM)/DIST
  ATD=ARSIN(SINTD)
  IF(ATD.GT.0..AND.XA.LT.XAM)ATD =ATD+PI/2.
  IF(ATD.LT.0..AND.XA.LT.XAM)ATD =ATD-PI/2.
  PII=-PI/2.
  IF(THETA.GT.0..AND.ATD.GT.PII) TD=ATD+PI
  IF(THETA.GT.0..AND.ATD.GT.PII) RETURN
  IF(ATD.GT.0..AND.THETA.LT.0.) TD=ATD+PI
  IF(ATD.GT.0..AND.THETA.LT.0.) RETURN
  IF(ATD.LT.PII.AND.THETA.LT.0.) TD=ATD+PI
  IF(ATD.LT.PII.AND.THETA.LT.0.) RETURN
C IF ABORTING SET DECENT RATE TO ZERO
  PD=0.
  IF(YA.LT.YAB.AND.THETA.LT.0.) TD=-PI/2.
  IF(YA.LT.YAB.AND.THETA.GT.0.) TD= PI/2.
  IF(YA.LT.YAB) RETURN
C ENTERING APPROACH PATH TURN
C CORRECT APPROACH ANGLE TO RUNWAY END
  DP=SQRT(((XA-XRS)**2)+((YA-YRS)**2))
C CHECK FOR CONFLICT WITH DEPENDENT RUNWAY
  CALL INTCON(XAM,YAM,JRUN,DP,IAB)
  IF(DP.EQ.0.) DP=1.E-05
  SINTD=(YA-YRS)/DP

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      TD=AR SIN(SINTD)
      IF(XA.LT.XRS) TD=TD+PI/2.
      TD=TD+PI
C COMPUTE DECENT RATE
      ZA=ZA/5280.
      TANPD=ZA/DP
      ZA=5280.*ZA
      PD=ATAN(TANPD)
      PDMAX=8.*PI/180.
      IF(PD.GT.PDMAX) PD =PDMAX
C RUNWAY APPROACH VELOCITY CONTROL
      VD=60.*VD
      IF(VD.GT. 65.) VD=VD-20.
      VD=-VD/60.
      RETURN
      END
$IBFTC TEN
      SUBROUTINE RUNFOU(PD,VD,XA,YA,ZA,TD)
C THIS SUBROUTINE SETS CRITERIA FOR RUNWAY FOUR.
      COMMON /P/ IDO
      COMMON /M/MTRAN
      COMMON /A/ISENSF
      COMMON /R/COUNT
      COMMON /P/ XS,YS,ZS,T
      DIMENSION MTRAN(144)
      DIMENSION XS(4),YS(4),ZS(4),T(4)
      DIMENSION ISENSE(4)
      DIMENSION COUNT(10)
      DIMENSION IDO(4)
      102 FORMAT (6F10.5)
      TDU=TD
      IF(ISENSF(4).LT.1) GO TO 103
      JRUN=4*IDO(4)
      CALL INPUT(XRS,YRS,THETA,THETB,DAP,DDI,ERROR,JRUN,RLEN,WAKE)
      ISENSE(4)=0
C INPUT RUNWAY GEOMETRY AND ACCEPTABLE ERROR
C XAM,YAM IS THE APPROACH OUTER MARKER
C DAP IS APPROACH DISTANCE
C RLEN IS RUNWAY LENGTH
C DDI IS THE DEPARTURE OUTER MARKER DISTANCE
C THETA ANGLE OF RUNWAY WITH NORTH
C ERROR ACCEPTABLE DEVIATION IN APPROACH.
C ST. LOUIS LAMBERT FIFLD RUNWAY STOL DEPAT
C STOL RUNWAY MUST BE A MINIMUM OF 2500. FEET FROM OTHER
C RUNWAYS DUE TO WAKE TURBULENCE
      XRS=0.0-WAKE*COS(THETA)
      YRS=YRS+WAKE*SIN(THETA)
      DCR=8000./5280.
      XRS=XRS-DCR*SIN(THETA)
      YRS=YRS-DCR*COS(THETA)
C WRITE(6,102)XRS,YRS,DAP,RLEN,DDI,THETA,ERROR
      YMIN=YRS
      YMAX=YRS
      XMIN=XRS
      XMAX=XRS
      XAM=XRS +DAP*SIN(THETA)
      YAM=YRS +DAP*COS(THETA)
      IF(XAM.GT.XMAX) XMAX=XAM
      IF(XAM.LT.XMIN) XMIN=XAM

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IF(YAM.GT.YMAX) YMAX=YAM
IF(YAM.LT.YMIN) YMIN=YAM
YRE=YRS -(RLEN)*COS(THETA)
XRE=XRS -(RLEN)*SIN(THETA)
IF(XRE.LT.XMIN) XMIN=XRE
IF(XRE.GT.XMAX) XMAX=XRE
IF(YRF.LT.YMIN) YMIN=YRF
IF(YRF.GT.YMAX) YMAX=YRF
XDM=XRS-(RLFN+DDI)*SIN(THETA)
YDM=YRS-(RLFN+DDI)*COS(THETA)
IF(XDM.GT.XMAX) XMAX=XDM
IF(XDM.LT.XMIN) XMIN=XDM
IF(YDM.LT.YMIN) YMIN=YDM
IF(YDM.GT.YMAX) YMAX=YDM
YAB=(YRS+YRF)/2.
IXA=XRS*1500./40.
IYA=YRS*1500./40.
JXA=XRE*1500./40.
JYA=YRE*1500./40.
MTRAN(10)=IXA
MTRAN(11)=IYA
MTRAN(12)=JXA
MTRAN(13)=JYA
103 PI=3.14159
C JRUN NEGATIVE IS DEPARTURE CODE
IF(JRUN.GT.0) GO TO 7
C DEPARTURE PATTERN
ZS(4)=0.
YS(4)=YRF
XS(4)=XRE
T(4)=THETA+PI
DP=SQRT(((XA-XRE)**2)+((YA-YRE)**2))
CALL INTCON(XAM,YAM,JRUN,DP,IAB)
IF(YA.GT.YMAX) TD=PI/2.
IF(YA.LT.YMIN) TD=-PI/2.
XREL=XA/XAM
IF(XREL.GE.1.) TD=-PI/2.
IF(XREL.LT.1.) TD=PI/2.
IF(ZA.LT.800.) TD=THETA+PI
VD=60.*VD
IF(ZA.LT.800..AND.VD.LT.140.) VD=VD+20.
IF(ZA.LT.800.) VD=-VD
VD=VD/60.
CALL SID(XA,YA,ZA,TD,PD,YDM,XDM,JRUN)
RETURN
C VH HORIZONTAL VELOCITY
Z VH=VD*COS(PD)
C APPROACH PATTERN
C DISM IS MINIMUM TURN DISTANCE
DISM=10.
C DIST IS DISTANCE TO APPROACH MARKER
DIST=SQRT(((XA-XAM)**2)+((YA-YAM)**2))
IF(DIST.LT.DISM) GO TO 20
YCA=ABS(YA-YAM)
XCA=ABS(XA-XAM)
IF(YCA.LT.DISM.OR.XCA.LT.DISM) GO TO 20
C COMPUTE DESIRED VECTOR
IF(YA.GT.YMAX.AND.XA.GT.XMAX)TD=-PI/2.
IF(YA.GT.YMAX.AND.XA.LT.XMIN)TD=-PI/2.

```

```

COMMON/A/ISENSE
COMMON/B/COUNT
DIMENSION COUNT(10) ,ISENSE(4)
DIMENSION IDO(4),JDO(4),XXO(4),YYO(4) ,ICON(4,4)
DCON=1.0
DPM=2.0
DPN=3.0
J=IAPS(JRIN)
XXO(J)=XAO
YYO(J)=YAO
DO 7 I=1,4
IF(ISENSE(I).GT.0) GO TO 7
IF(I.EQ.J) GO TO 7
DIST=SQRT(((XXO(J)-XXO(I))**2)+((YYO(J)-YYO(I))**2))
IF(DIST.GT.DCON) GO TO 7
ICON(J,I)=I
ICON(I,J)=J
7 CONTINUE
5 DO 14 I=1,4
K=ICON(J,I)
IF(K.NE.I) GO TO 14
IDO(K)=0
IF(DP.LT.DPN.AND.JRUN.LT.0) IDO(K)=-1
IF(DP.LT.DPM.AND.JRUN.GT.0) IDO(K)=-1
IF(IDO(K).LT.0) ISENSE(I)=-4
14 CONTINUE
RETURN
END

```

-----  
\$IRFTC SIXT

```

SUBROUTINE ARIVIT(J)
COMMON /R/ IDO
COMMON/P/ XS,YS,ZS,T
DIMENSION XS(4),YS(4),ZS(4),T(4)
DIMENSION IDO(4)
IF(IDO(J).LT.0) RETURN
PI=3.14159
PIJ=-PI
DISTBO=30.
X=XS(J)
Y=YS(J)
D=SQRT((X**2)+(Y**2))
IF(D.EQ.0.) D=1.E-05
U=Y/D
IF(U.GT.1.0.OR.U.LT.-1.0) U=1.0
U=ARCSIN(U)
U=U+(X+Y)/DISTBO
10 IF(U.GT.PI) U=U-PI
IF(U.LT.PIJ)U=U-PIJ
IF(U.LT.PI.AND.U.GT.PIJ) GO TO 5
GO TO 10
5 X =DISTBO*SIN(U)
Y =DISTBO*COS(U)
XS(J)=X
YS(J)=Y
T(J)=U+PI
RETURN
END

```

-----  
\$IRFTC SEVENT

```

SUBROUTINE SID(XA,YA,ZA,TD,PD,YDM,XDM,JRUN)

```

```

DIMENSION TU(6,6),DU(6),ZU(6,5)
PI=3.14159
DU(1)=2.0
DU(2)=10.
DU(3)=15.
DU(4)=20.
DU(5)=40.
DO 27 K=1,5
TU(K,1)=PI
DO 29 L=2,5
TU(K,L)=TU(K,L-1) -PI/2.
29 CONTINUE
27 CONTINUE
DO 51 K=1,5
DO 52 L=1,5
ZU(K,L)=1000.+1500.*(L-1)
52 CONTINUE
51 CONTINUE
J=IARS(JRUN)
C ZMIN IS MINIMUM TURN ALTITUDE
ZMIN=800.
C DMIN IS MINIMUM TURN DISTANCE FROM RUNWAY END
DMIN=2.0
DIST=((XA-XDM)**2)+((YA-YDM)**2)
C IF MINIMUMS NOT MET RETURN
IF(ZA.LT.ZMIN.OR.DIST.LT.DMIN) RETURN
DIST=SQRT((XA**2)+(YA**2))
DO 7 I=1,5
JP=I+1
IF(DIST.LT.DU(I)) GO TO 9
7 CONTINUE
RETURN
9 IF (DIST.LE.0.) DIST=1.E-05
TK=YA/DIST
TV=ARSIN(TK)
IF(TK.GT.0..AND.XA.LT.0.) TV=TV+PI
IF(TK.LT.0..AND.XA.LT.0.) TV=TV-PI
TD=TU(J,JR)
PD=0.
IF(ZA.LT.ZU(JR,J)) PD=-3.*PI/180.
IF(J.GT.2) PD=(8./3.)*PD
RETURN
END
$IBFTC EIGHTT
SUBROUTINE DUAL(TC,J)
DIMENSION IC(4),TC(4)
IC(1)=1
IC(2)=2
IC(3)=4
IC(4)=3
K=IC(J)
IF(TC(J).GT.TC(K)) TC(K)=TC(J)
IF(TC(K).GT.TC(J)) TC(J)=TC(K)
RFTUPN
END
$IRFTC NINFT
SUBROUTINE PLAND( XA,YA,ZA,TD,VD,PD,J,IT,I)
C THIS SUBROUTINE GENERATES CONTROLLER EXPECTATION OF PLANE POSITION.
COMMON/R/ IDO

```

```

COMMON/A/ISENSE
COMMON/B/COUNT
COMMON/U/DT, TI
COMMON/C/ZMAX, ZMIN, TMAX, TMIN
COMMON/P/ XS, YS, ZS, T
COMMON /M/MTRAN
DIMENSION IDO(4)
DIMENSION XS(4), YS(4), ZS(4), T(4)
DIMENSION MTRAN(144)
DIMENSION ICN(4)
DIMENSION ZMAX(30), ZMIN(30), TMAX(30), TMIN(30)
DIMENSION COUNT(10)
DIMENSION ISENSE(4)
DIMENSION ZAI(4)
DIMENSION ZAA(4,30), TDA(4,30)
102 FORMAT (6F10.5)
C ICN CONTROLS THE MAXIMUM NUMBER OF AIRCRAFT ASSIGNED TO RUNWAY APPROACH
  ICN(1)=5
  ICN(2)=5
  ICN(3)=5
  ICN(4)=5
C ZAI ALTITUDES ASSIGNED TO VARIOUS BEARINGS.
103 ZAI(2)=2200.
  ZAI(4)=3200.
  ZAI(1)=2200.
  ZAI(3)=3200.
  PI=3.14159
C STORE BEARING AND ALTITUDE
  TDX=TD
  7AX=7A
C RUNWAY UPDATES CONTROLLER INSTRUCTIONS BASED ON POSITION DATA.
  IC=COUNT(10)
C NO ARRIVALS
  IU=IABS(IC)
C RESET STACKING COUNTER
  IF(IU.EQ.1.AND.J.EQ.1) ITC=1
  IF(IC.LT.0) GO TO 10
  IC=IARS(IC)
C IF EXCESS AIRCRAFT STACK THEM
  IF(IC.LT.ICN(J)) GO TO 10
  CALL STACK(ITC, XA, YA, ZA, TD)
  ITC=ITC+1
  GO TO 900
10 CALL RUNWAY(J, XA, YA, ZA, TD, VD, PD)
C A NEGATIVE VD MEANS IN APPROACH CONTROLLER SECTOR
  IF(VD.LT.0.) GO TO 15
C EACH RUNWAY HAS A SPECIFIED ALTITUDE
  ZA=ZAI(J)
C COMPUTE DESIRED CLIMB. ZD
C CONTROLLER WORK LOAD COUNT
900 ERZ=ABS(ZA-ZAA(J,I))
  ETD=ABS(TD-TDA(J,I))
C IF A VECTOR CHANGE OCCURRED ADD TO THE COUNT(9)
  IF(ERZ.GT.100..OR.ETD.GT.0.15) COUNT(9)=COUNT(9)+1.
  ZAA(J,I)=ZA
  TDA(J,I)=TD
  ZD=(ZA-ZAX)/5280.
C COMPUTE MAXIMUM CLIMB ZP MAXIMUM DECENT ZC
  ZP=ZMAX(IT)*DT/5280.

```

```

ZC=ZMIN(IT)*DT/5280.
VDA=VD*DT
IF(VDA.EQ.0.) VDA=1.F-05
IF(ZP.GT.VDA) 7P=VDA
VDA=-VDA
IF(ZC.LT.VDA) 7C=VDA
C COMPUTE DESIRED CLIMB ANGLE
C IF CLIMB EXCEEDS AIRCRAFT CAPABILITY DECREASE EXPECTATIONS.
IF(ZD.GT.ZP) ZD=ZP
IF(ZD.LT.ZC) ZD=ZC
SINPD=ZD/VDA
PD=ARSIN(SINPD)
PDMIN=-3.*PI/180.
PDMAX= 3.*PI/180.
IF(J.GT.2) PDMIN=-8.*PI/180.
IF(J.GT.2) PDMAX=8.*PI/180.
IF(PD.LT.PDMIN) PD=PDMIN
IF(PD.GT.PDMAX) PD=PDMAX
C TC IS DESIRED TURN
TC=TD-TDX
IF(TC.GT.PI )TC=TC-2.*PI
PIX=-PI
IF(TC.LT.PIX) TC=2.*PI+TC
C IF DESIRED TURN EXCEEDS AIRCRAFT CAPABILITY REDUCE EXPECTATIONS
TXX=DT*TMAX(IT)
TNN=DT*TMIN(IT)
IF(TC.GT.TXX )TC=TXX
IF(TC.LT.TNN ) TC=TNN
C UPDATE EXPECTED BEARING.
TD=TDX+TC
C UPDATE EXPECTED POSITION.
15 VD=ABS(VD)
CALL EXPECT(XA,YA,ZA,TD,VD,PD)
RETURN
END
$IRFTC TWENTY
SUBROUTINE DATA(N)
COMMON /LU/ WAK
COMMON /LU/XA,YA,TTA,TTB,DA,DD,ER,RL
COMMON /R/ IDO
DIMENSION IDO(4)
DIMENSION XA(4),YA(4),TTA(4),TTB(4),DA(4),DD(4),ER(4),RL(4)
READ(5,29)
C WRITE(6,29)
29 FORMAT(1X,'TEST RUN')
READ(5,10) N ,WAK
WAKE=WAK
C WRITE(6,12)N ,WAKE
WAKE=WAKE/5280.
IF(N.GT.4) N=4
10 FORMAT(I10,F10.5)
12 FORMAT(I10,F10.5)
25 FORMAT(4I10)
READ(5,25) (IDO(K),K=1,N)
DO 20 I=1,N
READ(5,11) XA(I),YA(I),TTA(I),TTB(I),DA(I),DD(I),ER(I) ,RL(I)
C WRITE(6,11)XA(I),YA(I),TTA(I),TTB(I),DA(I),DD(I),ER(I) ,RL(I)
XA(I)=XA(I)/5280.
YA(I)=YA(I)/5280.

```

```
RL(I)=RL(I)/5280.  
11 FORMAT(1X,F9.5,7F10.5)  
20 CONTINUE
```

```
RETURN
```

```
$IBFTC TTWO
```

```
SUBROUTINE INPUT(XRS,YRS,THETA,THETB,DAP,DDI,ERROR,K,RLFN,WAKE)  
COMMON/LU/XA,YA,TTA,TTB,DA,DD,ER,RL  
DIMENSION XA(4),YA(4),TTA(4),TTB(4),DA(4),DD(4),ER(4),RL(4)  
J=IABS(K)
```

```
XRS=XA(J)
```

```
YRS=YA(J)
```

```
THETA =TTA(J)
```

```
THETB=TTB(J)
```

```
DAP=DA(J)
```

```
DDI=DD(J)
```

```
ERROR=ER(J)
```

```
RLFN=RL(J)
```

```
RETURN
```

```
END
```

```
$IBFTC TONE
```

```
SUBROUTINE CPXSN(IWORD,MTRAN,JUNN)
```

```
DIMENSION MTRAN(144)
```

```
12 FORMAT(10I10)
```

```
WRITE(12,12) (MTRAN(I),I=1,144)
```

```
RETURN
```

```
END
```

```
$DATA
```

```
' END OF FILE CARD  
' END OF FILE CARD
```