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NOISE REDUCTION RETROFIT FOR A "NEW LOOK" FLXIBLE TRANSIT BUS Service Bulletin

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TRI-COUNTY METROPOLITAN TRANSPORTATION DISTRICT OF OREGON 4012 S.E. Seventeenth Avenue Portland OR 97202

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PREFACE

This document is an instruction: how to apply a noise treatment to a contemporary city transit bus without extensive_structural alteration. Specifically addressed is the Flxible[®] Model 111DC-D061 with a Detroit Diesel 8V-71N engine; however, the concepts and much of the hardware described here are transferable to similar buses.

The information is of interest primarily to transit bus operators wanting to reduce noise by practical means, and to government agencies, manufacturers, and planners concerned with reducing the noise of buses in service at a moderate cost.

Acoustic benefits and performance side-effects are given.

One beneficial side-effect (because of turbocharging) is reduced harmful exhaust emissions. Another, because of smaller injectors and reduced exhaust back pressure, is fuel conservation.

Acknowledgment is made of the special contributions made by Gary Brentano and Richard Woods of the Tri-County Metropolitan Transportation District of Oregon (Tri-Met) who managed the project.

The work has been directed by the U.S. Department of Transportation: James Campbell for the Urban Mass Transportation Administration and Robert L. Mason for the Transportation Systems Center.

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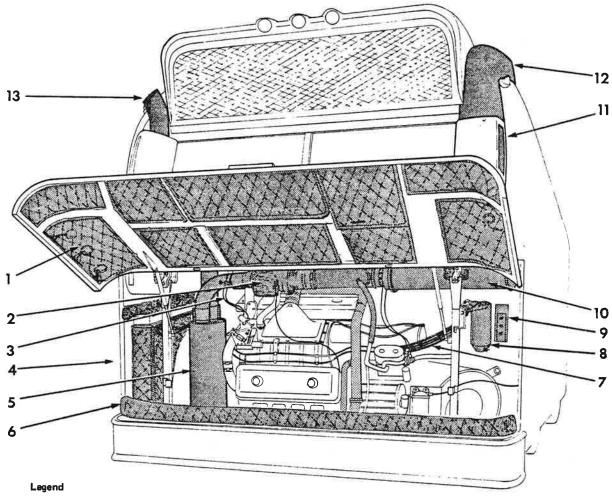
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INTRODUCTION

Owing to the general rise in prices for new vehicles, an operator might choose to extend the life of existing buses by renovation and remodeling instead of purchasing modern replacements. Noise treatments might well be included in such a program. Since fleets ordinarily consist of look-alikes having many small differences, this Instruction is designed to be of greatest utility by thoroughly documenting one good way to treat a typical bus. Highlights of the treatment are depicted in Figure 1. With this information, an experienced person can adapt the treatment to other bus models and expect similar results.

This approach unavoidably entails being specific about one set of suppliers and tradenames. There are a number of other products of equivalent quality and effectiveness. Regrettably, they cannot all be mentioned.



- Engine compartment padding
- Jacketed turbocharger
- Air dryer line
- Enlarged grille
- Jacketed muffler, relocated
- Door stop
- Relocated fuel lines
- 8 Relocated fuel filters, removed bypass oil filter
- 9 Relocated switch box
- 10 Larger air cleaner
- 11 Blanked inlet
- 12 Snorkle
- 13 5" exhaust stack

FIGURE 1 NOISE TREATED BUS

This, then, is an instruction for applying a noise treatment to a Flxible Model 111DC-D061 contemporary transit bus powered by a Detroit Diesel 8V-71N engine. Basically, the engine is retrofitted with a turbocharger, requiring new intake and exhaust systems, and the engine compartment is lined with antinoise padding. There are no major structural alterations or seriously adverse side-effects. The intent is to make these changes when the engine is due for an overhaul and will be dismounted.

BASELINE CONFIGURATION

The engineering work that led to this Instruction was done by Tri-Met in Portland, Oregon. Table 1 lists the important characteristics of the bus before it was modified.

TABLE 1.

BASELINE BUS CHARACTERISTICS

Coach Make Flxible
Coach Model 111DC-D061
Built October, 1972

Engine Make Detroit Diesel 8V-71N

Engine Model 7087-4523

City transit type

43° layover

clockwise rotation as viewed from flywheel

Injectors 71C5
Fuel #1 Diesel
Transmission Allison VS2-8

Length 35' 8"
Width 102"

Width 102"
Seats 42
Weight 22,560 lbs.

Axle Ratio 6 1/7 : 1

Axie Ratio 6 1//:1Tires Firestone 12.5 x 22.5 bias ply, 100 psi.

Air Conditioner Roof-mounted condenser

Exhaust System 4" tubing with EIP Aspirator

Muffler Nelson T-120323-F

Air Cleaner Donaldson EBA 13-0026

Pre-separator Donaldson PVH 000885
Fan Schwitzer L71 911024 (28" dia, 8-blades)

Radiator Core 1,048 in², 11 fins/inch, 222 tubes in 4 rows

Shroud 30" dia, sheet metal

Fan Drive GMC Torus

Engine Speed at Stall 1,250 rpm 1st Upshift Engine Speed 1,800 rpm at full throttle

1st Upshift Road Speed 22 mph

PRELIMINARY FIXES

Tri-Met's buses are relatively quiet to begin with when compared to those of many other transit systems. Other operators may be able to bring their bus noise down by doing what Tri-Met has already done and by paying attention to critical repair items.

- 1. Derate the engine by using the smallest available injectors: 71C5 (equivalent to 50 mm). This will reduce full throttle engine and exhaust noise. It is not practical to reduce noise by downsetting the overspeed governor. The transmission automatically upshifts before the engine speed exceeds 1,800 rpm. Downsets to lesser speeds would overly inhibit the bus's performance. Tri-Met uses small injectors and #1 Diesel to reduce exhaust smoke. Diesel #1 can slightly reduce full throttle engine and exhaust noise since it has about 4% less heat value per gallon.
- 2. Have a modulated speed fan drive such as the standard GMC Torus hydraulic clutch or the Schwitzer Viscous clutch. This minimizes average fan noise. An on-off fan clutch is not as satisfactory, but is better than a fixed drive. Tri-Met uses automatic fan drives for improved fuel economy.
- 3. Prevent unnecessary exhaust noise by making sure there are no exhaust leaks between the engine and the muffler outlet and that the muffler is adequate. Joints frequently break open because there is extensive stress caused by intermotion between the engine and the muffler. Provide an intermediate flexible tube section to relieve stress.
- 4. Keep the air side of the radiator core clean. Make sure the lower part of the fan shroud is not left off. Keep the fan centered in the shroud. These items minimize average fan speed, and thus fan noise, where there is an automatic fan drive. Also, the parasitic fan load on the engine is lessened, releasing more power to the wheels and reducing fuel consumption.
- 5. Adjust the transmission first upshift speed to the low end of its range: 22 mph. This reduces peak overall noise.
- 6. Keep bellypans in place. To reduce maintenance cost, Tri-Met does not use these optional engine compartment floors. However, operators who choose to use them can expect reduced engine noise generally and reduced fan noise on the right side. Although louvered sheet metal bellypans are not as acoustically effective as they could be, they are of some benefit.
- 7. Replace the 3 sets of synthetic *rubber engine mounts* when they fail, especially the donut-shaped mounts where the engine cradle connects to the chassis. If this is not done, engine vibration will telegraph more strongly into the bus body and the fan will move off-center in the shroud.
- 8. Repair body rattles. Keep in good working order the various handles and hold-downs to compartment doors. Tri-Met favors the spring-loaded struts that facilitate the opening and closing of the rear engine compartment door.

TURBOCHARGER CONVERSION

A turbocharger will reduce both engine noise and exhaust noise. Engine noise is reduced due to softening of the abrupt increase in the rate of cylinder pressure rise at the onset of ignition during the compression stroke. Exhaust noise is reduced since the drive turbine reflects and scatters the impinging sound waves.

The original motivation behind supercharging engines by means of an exhaust turbine (turbocharger) was to increase power output without increasing engine size. (The 8V-71TAC is rated as high as 350 hp with 75 mm injectors.) Figure 1 shows a turbocharged 8V-71 city coach engine. Turbocharging also compensates for rarified air at higher altitudes.

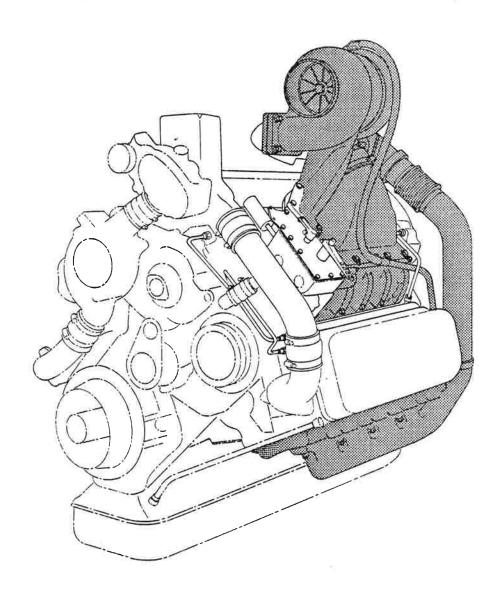


FIGURE 2.

TURBOCHARGED DETROIT DIESEL CITY COACH 8V-71

The turbocharger captures escaping energy from the exhaust pipe and returns it to the engine in the form of denser intake air. This enables more fuel to be burned and thereby more power to be produced.

The effect can be intensified with an "aftercooler" which cools the compressed intake air, making it even more dense. An aftercooler retrofit was not attempted. Making room for the aftercooler in the vee of the block requires more engine modification than it is worth.

Turbocharging reduces harmful gaseous exhaust emissions and can slightly improve fuel efficiency. Practically all diesel engines manufactured in the U.S. will be turbocharged in the future to satisfy clean air regulations.

Although turbocharging provides more air, thus allowing more fuel to be burned, it is inconsistent with noise control to increase fuel input along with a turbocharger retrofit. Consequently, injector size is kept the same or reduced if possible.

To plan a turbocharger conversion, the bus operator should review the information in Table 2 with his local engine dealer.

TABLE 2.

COMPARISON OF KEY ENGINE HARDWARE
WHEN CONVERTING AN 8V-71N INTO AN 8V-71T

Item	8V-71N	8V-71T
¹ Engine Model	7087-4523	² 7087-4620 Modified
³ Compression Ratio	18.7 : 1	17 : 1
4 Cylinder Kit	Naturally Aspirated City Coach Engine	Automotive Turbocharged with Crosshead Piston
Valves & Valve Inserts	Inconel X	⁵ Nimonic 90
⁶ Blower Drive Ratio	2.05 : 1	1.95 : 1
⁷ Blower Seals	Lip	Ring
⁸ Throttle Delay	.454"	.345"
Injectors	71C5	71C5
⁸ Injector Timing	1.484"	1.496"
9 Turbocharger	None	TV-8101 5101513 A/R 1.60
Exhaust Manifold, Crossover Pipes, and Blower Inlet	N Type	Turbo Type

Notes to Table 2

- 1 These model numbers apply to a Flxible city coach with a 43° layover.
- Model 7087-4620 applies to an 8V-71TAC which comes with an aftercooler. We are deleting the aftercooler. There is no model designation for a city coach 8V-71T (turbocharged without aftercooler).
- 3 Compression ratio is reduced to prevent overstressing the engine since the manufacturer anticipates more fuel, more cylinder pressure (BMEP), and more power. We are not adding more fuel and taking more power, but we change the pistons anyway because their improvements, including their improved piston rings, will extend engine life.
- ⁴ Since we do not use an aftercooler, we can use the same design N-engine cylinder liners which have shorter intake port slots.
- ⁵ Built to withstand higher temperatures of turbocharged engines.
- ⁶ Scavenging blower is slowed to the minimum to save parasitic power loss. The blower is still needed to purge spent gases of combustion during situations when the turbocharger is lagging and not up to speed.
- 7 Improved seal needed to withstand higher air box pressures.
- Reducing compression ratio tends to make the engine harder to start. Compensating adjustment is made to injector timing. If hard starting is still a problem in adverse weather, an ether cup installed on the dirty side of the air cleaner is recommended. With turbocharging, there is a tendency for a puff of smoke to occur at the onset of full throttle acceleration. Adjustment of the throttle delay corrects this.
- Tri-Met chose the TV-7101 (A/R = 1.23) turbocharger, Part Number 510509 which is designed for the 1978 8V-71TAC "California" engine. This is a more "active" turbo. Since we wanted significant supercharging at our customary low power levels, we selected this optional model. The TV-8101 is usually supplied with an 8V-71T, but is better matched with the highway truck application where engine load is higher.

The engine should have die-cast aluminum valve covers and a block-mounted crankcase breather pad.

Table 3 lists the changes in engine operating characteristics caused by turbocharger conversion.

After the engine is reassembled and checked for proper operation, check the turbocharger's functioning by measuring the pressure in the air box while the engine is under full throttle. Rather than rely on the idiosyncrasies of a chassis dynamometer, a simple, repeatable test is to drive the bus up a steady grade at full throttle, accelerating slowly, and note the air box pressure 100 rpm before top speed is reached. Pressures up to 50 inches of mercury can be expected. This baseline reading can be used later for verification if the turbocharger's performance is suspected of having fallen off.

With turbochargers, one must guard against any exhaust gas leakage past manifold gaskets, joints, or through cracks in the exhaust system upstream from the power turbine. This will weaken their propulsion. Also, it is important not to let air cleaner filter elements load up with dirt past the allowable restriction limits.

TABLE 3.

CHANGES TO ENGINE OPERATION

DUE TO TURBOCHARGER CONVERSION

(Relevant to 2,000 rpm, full throttle, and #1 Diesel)

	<u>Item</u>	Units	8V-71N	8V-71T
1	Allowable exhaust back pressure	"Hg	6	3
1	Allowable intake restriction	"H ₂ O	25	20
2	Air Flow	CFM	830	1,030
3	Water Flow	GPM	123	123
4	Heat Rejection to Coolant	BTU/min	6,322	7,040
5	Output	BHP	218	220
6	Fuel Efficiency	lbs/BHP-hr	.394	.402
	Peak Torque	ft-lbs	660	740
		rpm	1,200	1,200
	Exhaust emissions NO ₂	PPM	1,150	980
	HC	PPM	153	111
	СО	PPM	140	154

¹ Sensitivity of turbocharger to aspiration restriction is reflected in more stringent limits set by the engine manufacturer.

ENGINE COMPARTMENT PADDING

The engine compartment is padded with a $1\frac{1}{2}$ inch thick material that is soft, rugged, and easily bent. It consists of a 10 oz/ft^2 lead septum sandwiched between two blankets of glass fiber. The composite is protected by a lightweight waterproof aluminized glass cloth. The lead serves as a sound barrier and the glass fiber blankets reduce echoing. It can be steamcleaned and is incombustible.

After cutting to size with ordinary hand shears (die cut in mass production), the fabricator binds the edges by stapling on an aluminized glass cloth edging tape (AGE) as shown in Figure 3. The pads can be held in place with mechanical fasteners, but we use a quick-drying adhesive especially compounded for the purpose.

² Reflects supercharging effect of turbocharger.

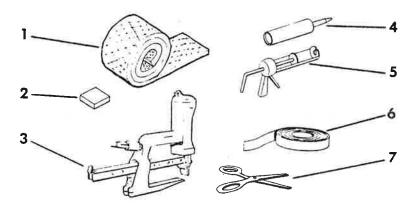
³ No change to water pump.

⁴ Heavier load on cooling system due to higher cylinder temperatures.

⁵ Same injectors, same fuel, same horsepower at rated speed.

⁶ No significant change to BSFC when converting an 8V-71N to an 8V-71T, but state-of-the art turbocharged diesels do have improved fuel efficiency.

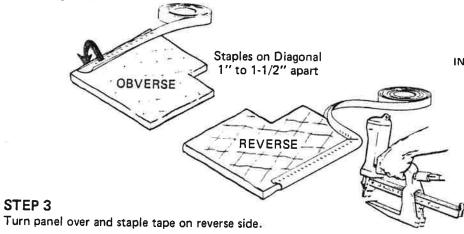
STEP 1 Gather tools, materials, and cut panels to size



STEP 2

Staple tape along edge, then roll tape over staples and

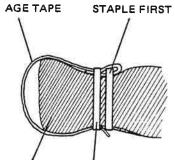
around edge of panel



Legend

- 1 Insul-Quilt, type 6
 2 1/2" x 5/8" Staples
 3 Bostitch pneumatic stapler
 4 Insul-Coustic adhesive
 5 Cartridge gun
 6 3" AGE tape

- 7 Shears



INSUL-QUILT STAPLE SECOND

DETAIL SECTION

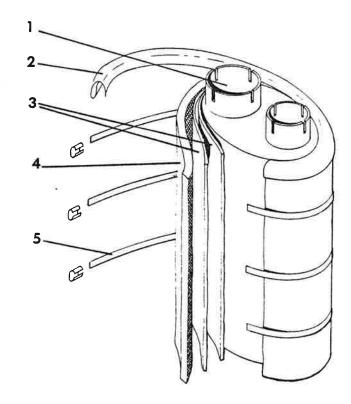
FIGURE 3 ANTI-NOISE PADDING FABRICATION TECHNIQUE

The padding is placed on all flat areas or single curvature surfaces that are not subject to removal for routine service operations.

Figure 4 illustrates the muffler jacket. It is lined with two layers of ceramic cloth for thermal protection and held in place with 1 wide steel bands applied by the strapping apparatus ordinarily found in Shipping Departments. This jacket stops muffler shell noise, reduces echoing of fan and engine noise, and protects maintenance personnel from accidental burns.

Legend

- 1 10" x 15" Oval Muffler
- **Edging Taper**
- 3 Two Layers Ceramic Cloth Lining 26" x 44"
- 4 26" x 44" anti-noise pad 5 1/2" Steel Strap



REFER TO DWG: SK-A-10003A

FIGURE 4. MUFFLER JACKET

Figure 5 dimensions and locates the ten anti-noise pads that fit into the recesses of the rear door to the engine compartment. A single large pad would be simpler, but there is insufficient room between the high spots on the door and the high spots on the engine. Chafing would penetrate and harm the pad.

Before gluing pads to the door, remove lamp holders and attach crimped screw holders to the screw holes in the door. Lamps can thereafter be removed and serviced from the outer side of the door without requiring access to the nuts on the inside. Cut holes in the pads to let wiring run to lamps.

To seal the upper edge and right and left sides of the rear door, $1\ 3/8$ " OD sponge rubber tubing is split in half and glued flat side down to the niche in the door's edges.

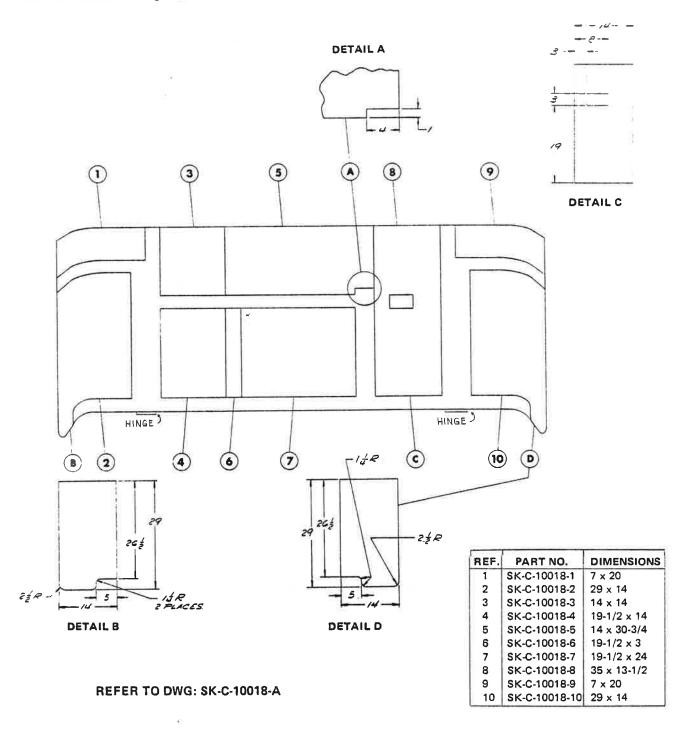


FIGURE 5. REAR DOOR PADDING

To seal the lower edge of the rear door, a door stop is fastened to the bumper so that it just touches the door padding when the door is fully closed. Figure 6 shows how an anti-noise pad is folded over a 4-piece aluminum angle, forming a seal with the door padding to reduce escaping noise.

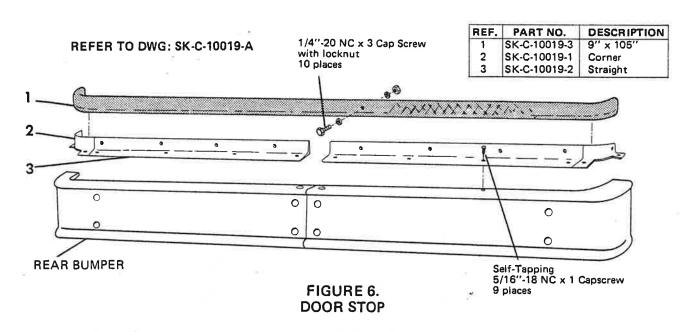
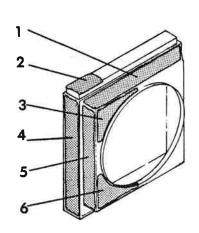
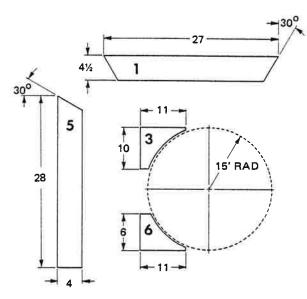


Figure 7 dimensions and locates the six pads that are glued to the radiator and shroud assembly.



REF.	PART NO.	DIMENSIONS
1	SK-B-10022-1	4½ x 27
2	SK-B-10022-2	6 x 9
3	SK-B-10022-3	10 x 22
4	SK-B-10022-4	6 x 25
5	SK-B-10022-5	4 x 28
6	SK-B-10022-6	6 x 11



REFER TO DWG: SK-C-10022A

FIGURE 7.
RADIATOR INSUL—QUILT TREATMENT

Anti-noise pads are put on the overhead and on the firewall of the engine compartment. The numerous mounting brackets, wire harness clips, and hose clamps are detached from these surfaces and reattached over the pads. These pads are depicted on Figure 8 along with the pads that attach to the right side of the engine compartment.

Finally, anti-noise pads are installed in the air conditioner compressor compartment on the left side of the bus and in the circuit breaker compartment on the right side just ahead of the engine compartment. Both door pads are glued in place. The compressor compartment floor is simply laid down.

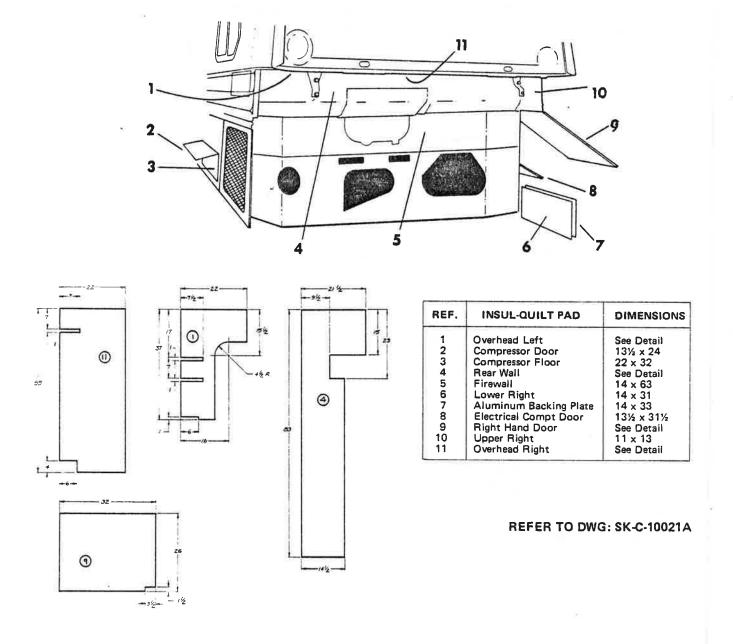


FIGURE 8. FIREWALL, ETC. PADDING

AIR INTAKE SYSTEM

A new air intake system is installed because the turbocharger displaces the original air cleaner and because the engine both draws in more air and is more sensitive to air intake restriction (Table 3). The main changes are:

	Before	After
Air Cleaner	Donaldson EBA 13-0024	Donaldson ECG 11-2000
Pre-cleaner	Donaldson PVH 000885	Removed
Inlet	Rear window cowl	Rooftop snorkle

The turbocharger requires that the air filter element must be serviced when intake restriction reaches 20 $^{\prime\prime} H_2O.$ If not, exhaust emissions will become unduly polluted.

The pre-cleaner is removed due to lack of space.

To compensate for the tendency toward shorter air filter service interval caused by the more demanding engine and the loss of the pre-cleaner, a larger air cleaner (80% more filter paper area) is used and the air is taken in from a cleaner source atop the bus roof facing forward.

The existing air intake system is removed and replaced with the system shown in Figure 9. The new filter element is easier to remove and replace. The rubber reducing elbow is protected from the hot exhaust pipes forming a wye before entering the turbocharger by insulating jackets covering the pipe elbows.

OIL FILTERS, ETC.

Originally, the exhaust manifolds emptied at the front of the engine into tubes that joined in a wye and led away to the muffler. After turbocharging, the exhaust manifolds empty toward the rear of the engine into tubes that sweep upward into a wye before entering the turbocharger. The left bank tube displaces the primary and secondary fuel oil filters bracketed above and behind the engine to its left.

Since there is no real need for the by-pass lubrication oil filter, it is removed. The space it occupied on the right side of the engine compartment where it was bracketed to the engine cradle hanger is now used for the fuel filters. Their new bracket, SK-B-10014, appears in its relative location in Figure 9. A new run of six hydraulic hoses connecting the fuel filters must be cut to length and installed.

The remote control engine-start switch box was originally mounted upon an angle clip in the upper right corner of the engine compartment. It is displaced by the new air cleaner location and dropped straight down to hang from the same angle clip by means of a new bracket, SK-B-10013, which also shows in its relative location in Figure 9.

The new air cleaner also displaces the small manifold which carries several oil pressure sending units, etc. Affected in the same way is the pressure switch that prevents the air conditioner compressor's drive from engaging at engine speeds above low idle. These items are moved downward on the firewall to a location below the new air cleaner.

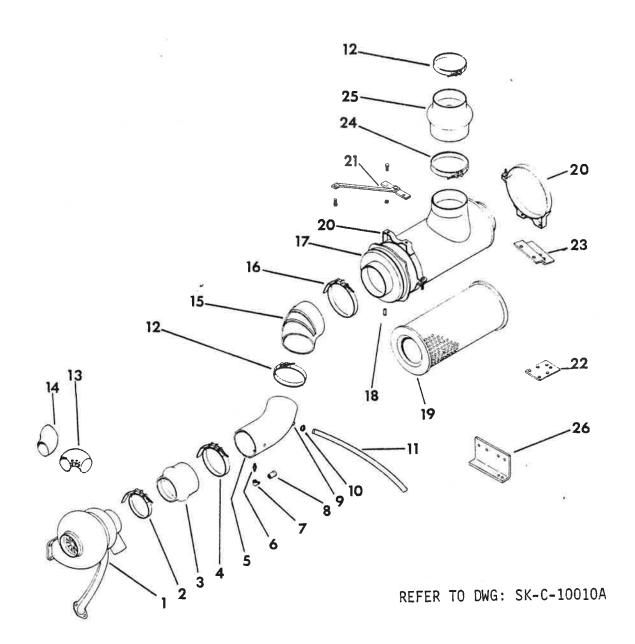


FIGURE 9. AIR INTAKE SYSTEM

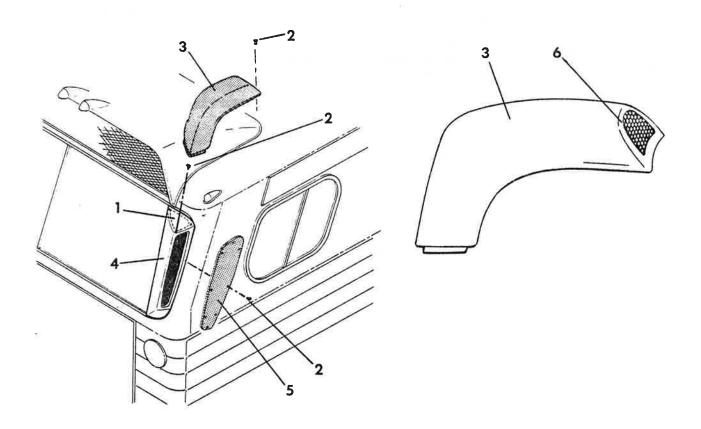
LEGEND FOR FIGURE 9.

Reference	Description	Quantity
1	Turbocharger	1
	5½" Latch-type Band Clamp	ī
3	6-to-5 Reducer	ī
4	6½" Latch-type Band Clamp	ī
2 3 4 5 6 7	45° Elbow, 6" OD	1
6	Safety Filter	1
7	1/8" NPT Street Ell	1
8 9	Restriction Indicator	1
	1/8" NPT Pipe Plug	1
10	1" DIA Worm Screw Hose Clamp	1
11	1" ID Reinforced Rubber Hose	≃18"
12	6½" Band Clamp ,~	2
13	Left Sweep Elbow Jacket	1
14	Right Sweep Elbow Jacket	1
15	7-to-6 Reducing 45° Elbow	1 2 1 *1 2 1 1
16	7½" Latch-type Band Clamp	1
17	Air Cleaner	2
18	1/4" OD x 1" Copper Drain Tube	1
19	Replacement Element	*1
20	Mounting Band	2
21	Air Cleaner Strap	1
22	Switch Box Bracket	1
23	Air Cleaner Support	1 1
24	7½" Band Clamp	1
25	7-to-6 Reducer	1
26	Fuel Filter Bracket	1

^{*}Included in Air Cleaner

AIR INTAKE SNORKLE

The air intake snorkle is installed in accordance with Figure 10. The template, SK-A-10020, is used to cut an opening in the top of the existing air intake cowl. The snorkle inserts into this hole and is held in place by screws. Another screw attaches the inlet end of the snorkle to the roof of the bus. The existing screen is removed from the cowl and the old inlet is closed by the plasic blank, SK-B-10016.



Legend

- 1 Snorkle Template SK-A-10020
- 2 Sheet Metal Screws
- 3 Holloway Snorkle SK-A-10017-A
- 4 Existing Intake Cowl
- 5 Intake Cowl Blank SK-B-10016 6 SS Wire Screen SK-A-10017-2

REFER TO DWGS:

SK-A-10016 SK-A-10017-A

SK-A-10020

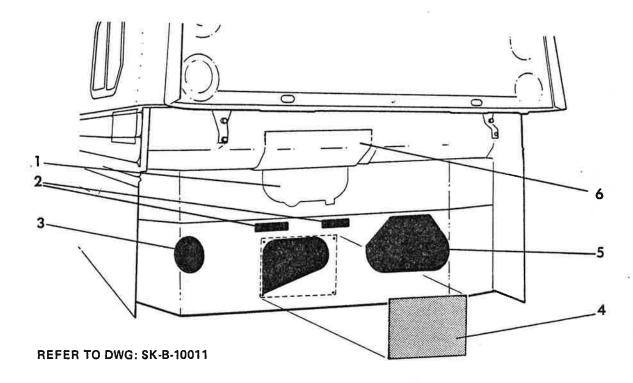
FIGURE 10. HOLLOWAY SNORKLE INSTALLATION

EXHAUST SYSTEM

A new exhaust system is installed in order to provide the reduced back pressure required by the turbocharger (Table 3). The main changes are:

	Before	After
Tube size to muffler	4" diameter	4" diameter
Exhaust muffler	Nelson T-12023-F	Donaldson WOM12-083, modified
Tube size to stack	4" diameter	5" diameter
Exhaust aspirator	EIP Kit	Removed

The original exhaust tubing and muffler system from engine to outlet is removed. Their old passageway through the center of the firewall is covered with a steel plate as shown in Figure 11. Retaining screws pass through the firewall from front to rear and engage the cover plate on the rear side of the firewall.



Legend

- Access panel, seldom used and now covered by anti-noise padding
- 2 Plumbing passage
- 3 Freon compressor drive shaft passage
- 4 Newly fabricated exhaust pipe passage blank (SK-B-10011)
- 5 Drive line passage
- 6 Rear seat access hatch

FIGURE 11. EXHAUST PIPE PASSAGE COVER

Figure 12 depicts the new exhaust system. It features a new, smaller oval-shaped muffler. The muffler is relocated to the space between the engine and radiator formerly occupied by the "aspirator", a component of the so-called "Environmental Improvement Kit." The function of the aspirator was not replaced because it served no useful purpose to begin with.

The new muffler's body acts as a partial barrier to engine compartment noise emitting through the radiator opening. To compensate for its interference with access to the front of the engine, the muffler is bottom-mounted and jointed with v-band clamps to facilitate quick removal.

The plastic cowl located to the left of the rear window whose purpose is to conceal the stack is trimmed to fit the larger 5" diameter stack. A flexible tube section in the stack relieves stresses in the exhaust tubing produced by the relative motion between the engine and the chassis.

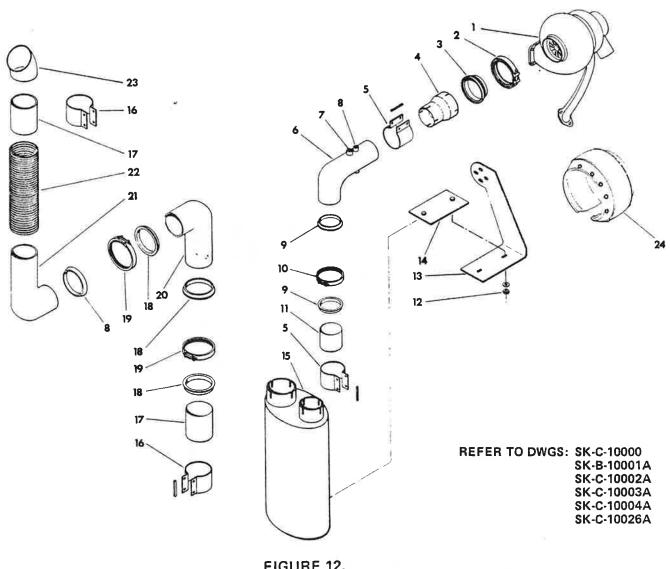


FIGURE 12. EXHAUST SYSTEM

LEGEND FOR FIGURE 12.

Reference	Description	Quantity
1	Turbocharger	1
2	V-band Clamp	1
3	Turbocharger Flange	1
4	5-to-4 ID-OD Reducer	1
5	4" Diameter Band Clamp	2
3 4 5 6 7	4" OD, 16 GA, MS Tube, 90° Elbow Ass'y	1
7	1/8" NPT Pipe Plug	1
8	1/4" NPT Pipe Plug	1
8 9	4" ID Pipe Flange	2
10	4" DIA V-band Coupling	1 1 2 1 2
11	4" OD x 4", 16 GA, MS Tube	
12	5/16"-18NC Nut & Washer	2 ea.
13	Muffler Hanger	1
14	Muffler Mounting Plate Ass'y	1
15	Muffler	1
16	5" Diameter Band Clamp	2
17	5" OD x 6", 16 GA, MS Tube	1 2 2
18	5" ID Pipe Flange	
19	5" DIA V-band Coupling	4 2
20	5" OD, 16 GA, MS Tube, 90° Elbow, 12 3/16 Long	
21	5" OD, 16 GA, MS Tube, 90° Elbow, 13 7/8" Long	ī
22	5" ID x 18", SS Flex Tube	ī
23	5" OD, 16 GA, SS Tube, 45° Elbow	ī
24	Turbocharger Blanket	î
- ¬	ful boolia, get branker	-

AIR DRYER HISS

The air dryer is a safety device, yet it sounds dangerous. Located just downstream from the compressor, it removes condensate from the newly compressed air before the air reaches the valves, chambers, and reservoirs of the air brake system where freezing might cause blockage. Each time the compressor replenishes the air storage tanks, the same signal that unloads the compressor opens the dryer's sump valve, allowing the pent up air within to blow the collected condensate down onto the street below. This causes a loud, prolonged hissing noise. Often this will occur about a half-block after the bus pulls away from a boarding station. Since it sounds like something dramatic is happening with the airbrakes, it scares people, creating an unnecessary sense of alarm and annoyance.

Figure 13 shows a harmless way to silence the air dryer. Simply run a line from the sump to the exhaust pipe upstream of the muffler where there is a fitting provided. Any condensate, oil carryover, or other debris in the air dump is safely dissipated in the hot exhaust gas.

REF. DESCRIPTION		
1	Air Dryer	
2	Adapter	
3	1/4 NPT Male Elbow	
4	Brass Insert	
2 3 4 5 6	3/8" OD Nylon Tube	
6	Union Elbow	
7	3/8" OD Copper Tube	
8	90° Elbow	
9	1/4" NPT Male Connector	

REFER TO DWG: SK-A-10008-A

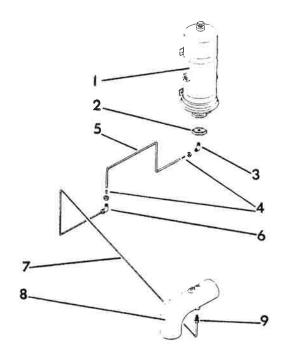


FIGURE 13.
AIR DRYER SILENCING

RADIATOR GRILLE

The turbocharger removes heat from the exhaust gas. Most of this missing heat is transferred to the engine's cooling system. The cooling load is increased 11%. To offset this extra load, the radiator grille is rebuilt, giving a 45% larger net area. This results in a 12% increase in air flow at the same fan speed which, in turn, results in a 7% greater heat rejection from the same radiator without a rise in coolant temperature. The end result is a slight reduction in the cooling system's capacity. However, the cooling system has surplus capacity in our buses to prevent overheating of the engine in any environmental condition, provided that it is kept in reasonably good working order. Therefore, rather than take the next step, which would be to replace the existing 4-tube row radiator core with a 5-row core, it is better to pay attention to routine service items such as:

- 1. Steamclean air side of radiator and keep clean.
- 2. Do not discard any part of the fan shroud.
- 3. Keep fan centered in shroud.
- 4. Keep fan drive thermostat valve working.

Figure 14 shows how the existing grille is salvaged and rebuilt.

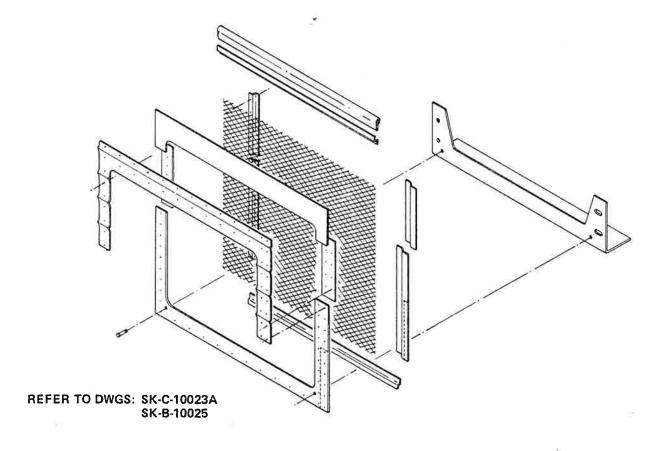
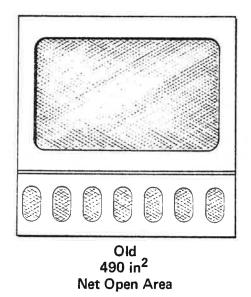
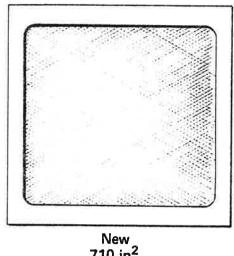


FIGURE 14.
REWORKED RADIATOR GRILLE

Figure 15 compares the old grille with the new grille.





New 710 in² Net Open Area

FIGURE 15. OLD AND NEW GRILLES

A grille having a still greater open area does not result in a further increase in air flow. This is because the "bottleneck" lies elsewhere. The net open area of the radiator core is $720 \, \text{in}^2$ and the area of the shroud opening is $710 \, \text{in}^2$. The next step in improving air flow would be either to redesign the fan-shroud interaction or increase the size of the radiator, shroud, and fan.

ESTIMATED COST

It is estimated that the cost of applying the treatment is about \$6,000 per bus. Most of this amount is associated with turbocharging the engine. In making this estimate, itemized in Table 4, it is assumed that:

Only one or a few buses will be treated at a time.

Workmen are unrehearsed, but supervised and well motivated.

No special tooling is built up.

Common tools, parts, materials, and outside fabricators are available.

Prices are at the 1979 level.

Shop labor and overhead rate is \$20 per man-hour.

Purchases are below levels deserving quantity discounts.

In the interest of economy, the engine is turbocharged at the same time it is undergoing an overhaul. The net cost of rebuilding the engine into an 8V-71T over the cost of restoring it to an 8V-71N is used.

TABLE 4.
COST ESTIMATE

SHOP LABOR	Build Up	Install	Total
Overhaul to 8V-71T	42	8	50
Overhaul to 8V-71N	³ 32	8	40
Net to turbocharge	10	ō	10
Anti-noise padding	$7\frac{1}{2}$	5½	13
Air intake system	$\frac{1}{4}$	21/4	2½
Oil filters, etc.	1	2½	3½
Air intake snorkle	1/2	1	$1^{\frac{1}{2}}$
Exhaust system	2½	6½	9
Air dryer line		2	2
Radiator grille	31 ²	12	4
Total man-hours	25½	$2\overline{0^{\frac{1}{4}}}$	45½

COSTS	Purchased Parts	Build Up Labor	Outside Fabricate	Install _Labor	Total
Overhaul to 8V-71T	\$7,200	\$840	\$ 0	\$160	\$8,400
Overhaul to 8V-71N	4,800	640	0	160	5,800
Net to turbocharge	2,400	200	ō	0	2,600
Anti-noise padding	611	150	0	110	871
Air intake system	514	5	50	45	614
Oil filters, etc.	40	20	0	50	110
Air intake snorkle	12	10	600	20	642
Exhaust system	578	50	210	130	968
Air dryer line	20	0	0	40	60
Radiator grille		_70	0	10	_100
Total cost	\$4,195	\$505	\$860	\$405	\$5,965

ACOUSTICS

Sound is vibration in air...pressure waves. Noise is unwanted sound.

The human ear is an extremely sensitive and delicate organ. A young person can detect a sound whose air pressure is only one two-ten thousandths of a millionth of an atmosphere. The ear can momentarily function even when exposed to sound pressure 10 million times this threshold.

Sound is measured with a sound level meter and is usually expressed in terms of A-weighted decibels. The sound level meter consists of a microphone, an amplifying electronic network, and a readout. Too many digits would be involved if sound were expressed in plain pressure units, so decibels are used to make the numbers simpler. A decibel is 20 times the logarithm (power of ten) of the ratio of the measured sound pressure to a reference sound pressure. The reference is the threshold of human hearing. A sound having a thousand times the pressure of the human threshold would have a decibel rating of 60 dB. A-weighting means that the signal is sent through a filter that downgrades low frequency sound corresponding to the response of the human ear.

One does not use simple arithmetic with decibels. For example, 80 dBA plus 80 dBA does not equal 160 dBA. As a matter of fact, every time sound pressure doubles, the sound level increases by 3 dBA. 80 + 80 = 83 dBA.

If one sound is 10 dBA louder than another, the lesser is masked out. That is, the sound level of the two together is not detectably greater than the greater sound. When a particular noise source is 10 dBA less than the overall noise, then it is unimportant.

Distance has a predictable effect on sound level. Each time one doubles the distance to a sound source radiating from a point in an echo-free space, the sound level drops by 6 dBA.

Juries won't agree that there is a difference in level when sounds less than 3 dBA are compared. A sound 10 dBA less than another seems half as loud.

When trying to stop noise by putting a box around the source, one should keep these things in mind:

- 1. A lot of noise comes through a small hole. An air leak is usually a noise leak too.
- 2. Kill "live" panels (they ping when you strike them) by stiffening them or by gluing something heavy to them.
- 3. The walls of the box have to be relatively heavy. Usually a pound or two per square foot is enough.
- 4. Some kind of sound absorptive lining inside of the box is good because it reduces echoes inside. If it becomes less noisy inside the box, it will become less noisy outside the box too.
- 5. If you can't put a complete box around the source, at least try to put barriers to cut off line-of-sight noise. That is better than leaving open holes.

A bus is a chorus of individual noises. These can be grouped as engine compartment noise, fan noise, exhaust outlet noise, muffler and exhaust pipe shell noise, and tire and body noise.

Engine noise is both sensitive to speed and power. It has a harsh, unpleasant quality. It is the most difficult noise source to treat and is therefore usually the dominant source after the overall bus has been treated. It can be helped by the engine manufacturer through smoothing of the onset of combustion, by stiffening the block, and by curing "hot spots." But, this takes a long time and is expensive. Other treatments are turbocharging and encapsulation.

The fan makes a whirring sound, coming from where the blade tips chop the air. It is steeply sensitive to fan speed, so a modulating speed drive is better for noise control than an on-off drive. At least sometimes you will hear the fan if it has an on-off drive, but you might never be bothered by fan noise with a modulating speed drive. Nothing much can be done to cure fan noise except to slow the fan down. This is more easily done at the factory through the use of larger radiators than in the field.

Exhaust outlet noise is more mellow and musical. Most uninitiated believe they are hearing exhaust noise and blame the muffler when a loud bus goes by. It might well be a break in the exhaust piping upstream of the muffler, or more often just plain engine noise they are hearing. Exhaust noise is relatively easy to treat. All one needs is a proper muffler. With turbocharged engines, there is a need for low back pressure. This leads to the problem of finding room for the adequate muffler. To have low back pressure and good silencing, a muffler can't be kept small.

Muffler and exhaust pipe shell noises might be revealed as treatment of the louder engine, exhaust, and fan noises progresses. Common practice is to double the skin of the muffler body when used with naturally aspirated engines. The need is less with turbocharged engines. Pipe shell noise does not ordinarily require treatment, but there might be significant noise radiating from flexible tube sections.

Tire noise is unimportant at speeds below 40 mph for the ordinary bus. Even after treatment, tire noise is masked out at speeds below 30 mph. Body noise can be a nuisance if there are loose doors and windows.

Noise radiates in all directions from a bus of the type we treat here, but not evenly. Less noise radiates forward because the bus body is a barrier to engine noise in the rear. The bus is noisier on the left side than on the right, not because the exhaust stack is on that side, but because the radiator opening is there... an open door to noise from the engine compartment. Fortunately, the boarding passengers are exposed to right side noise which is quieter and easier to treat than left side noise.

We believe the operator of a city transit bus should judge a treatment by its effect on the ordinary noise a bus makes most of the time; not on the maximum noise it makes only once in awhile. A treatment that reduces the one does not necessarily reduce the other. Consequently, we believe it is better to evaluate the bus with its fan drive in the "as-is" condition and not artificially locked up. We use the following criteria:

Exterior Noise.

Average of right side and left side peak sound level during a 50-foot full acceleration pass-by through first upshift.

Interior Noise.

Average of rear seat and driver's seat peak sound level during full acceleration through first upshift.

By these criteria, the results of treating a bus in accordance with this Retrofit Instruction are:

	As-Is Average Exterior Rating*	As-Is Average Interior Rating*
Baseline (Typical Tri-Met)	79½ dBA	79½ dBA
After Treatment	75½ dBA	76½ dBA
Reduction	4 dBA	3 dBA

*Rounded to the nearest ½ dBA

An acoustically effective bellypan would make possible a further reduction to the average exterior rating of at least 3dBA, but this has not been reduced for practical hardware.

A more detailed breakdown by side and source is given in Table 4. This enables comparison with other standards such as the U.S. EPA proposed rule for regulating manufacturers of buses. The EPA rule is "worst-case" oriented. It considers only the "fan-on" condition and the louder side or end. The proposed levels are:

	Exterior	<u>Interior</u>
First year	83 dBA	86 dBA
Fifth year	80 dBA	83 dBA
Seventh year	77 dBA	80 dBA

TABLE 5.

NOISE SOURCE DIAGNOSIS BEFORE AND AFTER TREATMENT Measured by EPA 50-foot Acceleration Pass-by Test (Rounded to Nearest ½ dBA)

BASELINE

E:	EXTERIOR		LEFT	RIGHT
	SOURCE	ENGINE SHELL EXHAUST TIRES	79 73 66 58	77½ 70 65 58
-2	0, -	FAN ON FAN AS-IS	77 71	76½ 70½
	OVERALL	FAN ON FAN AS-IS FAN OFF	*82 80 80	81 79 78½
II	NTERI	IOR	REAR	FRONT
		FAN ON FAN AS-IS	*83½ 83	77½ 76

TREATED

E	EXTERIOR		LEFT	RIGHT
SOURCE		ENGINE SHELL EXHAUST TIRES	74½ NIL 65 58	73½ NIL 64 58
	01	FAN ON FAN AS-IS	77½ 71	73 65
	OVERALL	FAN ON FAN AS-IS FAN OFF	*79½ 76½ 75	76½ 74½ 74
II	NTER	OR	REAR	FRONT
20/41		FAN ON FAN AS-IS	*80½	74½ 73

^{*}Comparable to EPA Rating

EFFECTS ON PERFORMANCE

Table 5 quantifies the side-effects of the noise control treatment on various aspects of bus performance. It complements the data presented in Table 3. In general, emissions and aspiration are improved, delivered power and fuel economy are unchanged or slightly improved, cooling system capacity is affordably decreased. Predicted aggregate maintenance costs are not measurably changed.

TABLE 6.

PERFORMANCE BENCHMARKS BEFORE AND AFTER TREATMENT

(#1 Diesel Fuel)

	UNITS	BASELINE	TREATED
POWER OUTPUT			
Terminal Speed on 4% Grade	mph	45½	46
Acceleration on Flat 1200-foot Time	sec	8.7	8.8
² Engine Dynamometer Full throttle, 2,000 rpm	внр	218	220
FUEL MILEAGE			
Average Mission	mpg	³ 4.22	44.40
COOLING SYSTEM			
Full Speed on 4% Grade Fan Delivery, 1,500 rpm	5°F ATB CFM	134° 10,500	127½° 12,000
ASPIRATION (Full Power, 2,000 rpm)			
Exhaust Back Pressure Exhaust Temperature Intake Restriction	"Hg °F "H ₂ O	5.6 810° 7	2.1 560° 11

¹ Full throttle from a standing start.

 $^{^{2}}$ Data supplied by engine manufacturer.

^{3 2-}year fleet average.

^{4 5}½ months in-service average.

⁵ The ambient air temperature at which the coolant would theoretically warm up to the boiling point of water, 212°F.

ABBREVIATIONS

AGE Aluminized Glass Edging Tape AL, ALUM Aluminum Air-to-Boil Temperature ATB One-millionth of an atmosphere of pressure µbar Bolt Circle B.C. Brake Horsepower BHP BMEP " Brake Mean Effective Pressure Brake Specific Fuel Consumption BSFC British Thermal Unit BTU Cubic Feet per Minute CFM CO Carbon Monoxide dBA A-weighted decibel referenced to .0002 µbar Diameter DIA, dia DWG Drawing EIP Environmental Improvement Package °F Degree Fahrenheit Flexible Flex ft² Square Foot GA Gage GPM Gallons per Minute HC Hydrocarbons "Hq Inches of Mercury Inches of Water "H2O hr Hour Inside Diameter ID in^2 Square Inches Installation INST. Left Bank L.B. lbs Pounds min Minute Millimeter mm Miles per Gallon pqm mph Miles per Hour M.S. Mild Steel MTG Mounting National Coarse Thread NC NO_2 Nitrous Oxide NPT National Pipe Thread OD Outside Diameter Ounce oz Parts per Million PPM Pounds per Square Inch psi Radius R, RAD REF Reference R.B. Right Bank Revolutions per Minute rpm Second sec

Stainless Steel

Typical

S.S.

TYP

APPENDIX A.

PURCHASE LIST

Notes:

- 1. Parts for turbocharge rebuild to be negotiated with local Detroit Diesel dealer.
- 2. Common fasteners not called out.

Quantity	Brand or Manufacturer	Size or Part Number	Description	Where Us
1 1 1 1 2 1	Aeroquip Aeroquip Aeroquip Aeroquip Aeroquip Aeroquip Aeroquip	55083-650-2 MB9460-S-100-N-750 55083-750-2 MB9360-S-075-N-550 MB9460-S-100-N-650 MLJ 8750-500S MLJ 8750-400S	6½" Band Clamp 7½" Latch Band Clamp 7½" Band Clamp 5½" Latch Band Clamp 6½" Latch Band Clamp 5" Servicemaster 4" Servicemaster	SK-C-10(SK-C-10(
1	Bostitch Bostitch	P50-5B SB-5019-5/8"	Pnuematic Stapler S.S. Staples	IC Pads
40" x 88"	Carborundum	Grade FW35	Flexweave 1000 Cloth	SK-A-100
1	Detroit Diesel Detroit Diesel	5101814 5132650	Turbocharger Flange V-Band Clamp	SK-C-10(SK-C-10(
2	Donaldson	17061	5" Sealclamp	SK-C-10(
2 1 1 1 1 1 1 2	Donaldson Donaldson Donaldson Donaldson Donaldson Donaldson Donaldson Donaldson Donaldson	KYX00-4482 5080B79 21067 23013 P10-0089 RBX00-2278 ECG11-2000 P00-4079	4" Sealclamp WOM12-83, Modified 4-5 ID-OD Reducer 6" OD 45° Elbow Safety Filter Restriction Indicate Air Cleaner Mounting Band	SK-C-10(SK-C-10(SK-C-10(SK-C-10(SK-C-10(SK-C-10(SK-C-10(SK-C-10(
18" Long	Federal	R200S	5" ID S.S. Flex Tube	SK-C-100
1 1 1	HITCO HITCO	298S27644 298S27664 298S27663	Turbo-Charger Blkt. L.B. Elbow Blanket R.B. Elbow Blanket	SK-C-100 SK-C-100 SK-C-100
1	Holloway	SK-A-10017A	Snorkle	Sk-A-10(
1 1 1	Huntington Huntington Huntington	60R50 70R60 45HL70R60	6-5 Rubber Reducer 7-6 Rubber Reducer 7-6 Reducer 45°Elbow	SK-C-10(SK-C-10(SK-C-10(
1 25' Roll 1 Roll 6	Insul-Coustic Insul-Coustic Insul-Coustic	Type 6, 10 oz/ft ² 3" Wide x 400 Yards IC 998	48" Wide Insul-Quilt AGE Tape Adhesive Cartridge	IC Pads IC Pads IC Pads

APPENDIX A.

PURCHASE LIST CONTINUED

	Brand or	Size or		
Quantity	Manufacturer	Part Number	Description	Where Used
15" x 38"	Local Supply	3/16" Thick	M.S. Plate	SK-C-10000 SK-B-10001A
20" x 28"	Local Supply	1/8" Thick	M.S. Plate	SK-A-10011 SK-B-10012 SK-A-10013 SK-B-10014
3" x 15" 14" x 36" 26" x 32" 6' 31" x 33" 1" Long 6' 10' 2" Long 6" x 24" 2' 1	Local Supply	1/4" Thick 5/32" Thick 1/8" Thick 1/8" x 3" x 3" 1" x 2" Diamond 1" OD x .065" Wall 1/4" OD SAE J844B, Type 1 SAE J844B, Type 3 2" Hexagonal 1/8" Thick 1" OD 5" OD, 16 GA 1/8" NPT	M.S. Plate M.S. Plate Alum Sheet Alum Angle M.S. Expanded Mesh M.S. Tube Copper Tube 3/8" OD Copper Tube 3/8" OD Nylon Brass Bar Polypropylene Sheet Haircell Black Rein Rubber Hose S.S. 45° Elbow Pipe Coupling	SK-C-10015A SK-C-10023A SK-C-10021A SK-C-10019A SK-C-10023A SK-A-10009A SK-A-10008A SK-A-10008A SK-A-10007 SK-B-10016 SK-C-10010A SK-C-10002A SK-C-10005A
1	Local Supply	1/4" NPT	Pipe Coupling	SK-C-10009A SK-C-10005A
3	Local Supply	1/8" NPT	Pipe Plug	SK-C-10005A SK-C-10009A SK-C-10010A
1	Local Supply Local Supply	1/4" NPT 1" DIA	Pipe Plug Worm Hose Clamp	SK-C-10005A SK-C-10010A
1 1 1 2 1 12" x 12"	Parker Parker Parker Parker Parker Western Wire	2202P-2-2 269CA-6-4 165CA-6 63PT-6-62 68CA-44	1/8" NPT Street Ell 1/4" NPT Male Elbow Union Elbow Brass Insert 1/4" NPT Male Conn.	SK-C-10010A SK-A-10008A SK-A-10008A SK-A-10008A SK-A-10008A
14 X 12"	western wire	16 GA, 4 Mesh	T304 S.S. Screen	SK-A-10017A

APPENDIX A.

SPECIALTY SUPPLIERS

HITCO Insulation Products 2302 Marietta Blvd, N.W. Atlanta, Georgia 30318 (404) 355 1205

Insul-Coustic Jernee Mill Road Sayreville, New Jersey 08872 (201) 257 6674

Huntington Rubber Co. 6800 S.W. Macadam Blvd. Portland, Oregon 97219 (503) 246 5411

Holloway Product Development 14023 N.W. Science Park Drive Portland, Oregon 97229 (503) 643 7338

Carborundum Co. Insulation Division P.O. Box 808 Niagra Falls, N.Y. 14302 (716) 278 6221

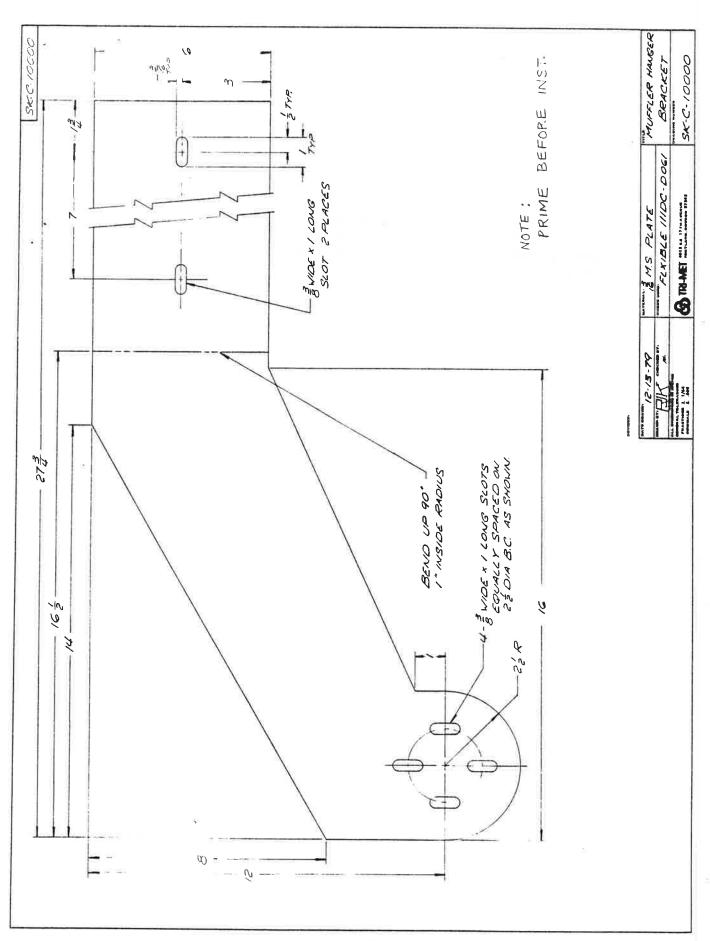
Donaldson Co., Inc. 1400 W. 94th St. Minneapolis, Minnesota 55440

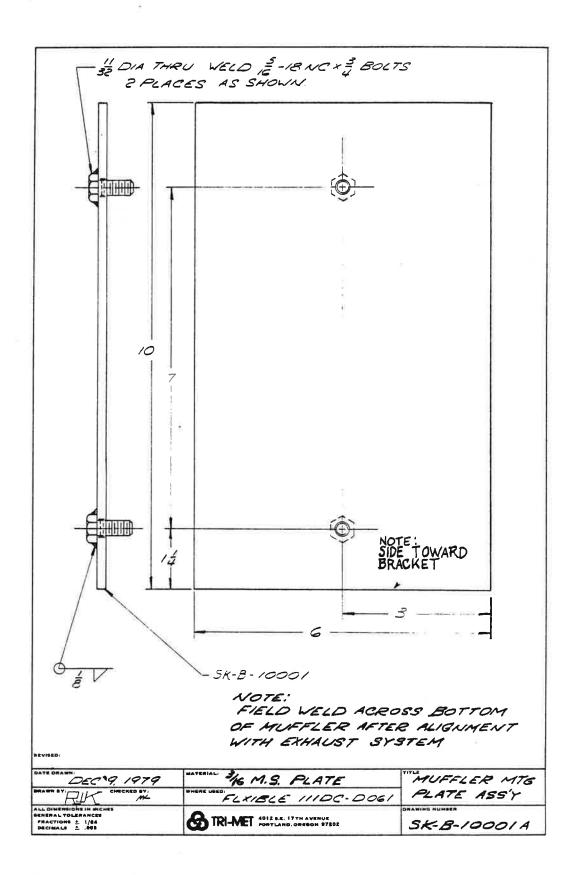
Western Wire Works 4025 N.W. Express Portland, Oregon 97210 (503) 222 1644

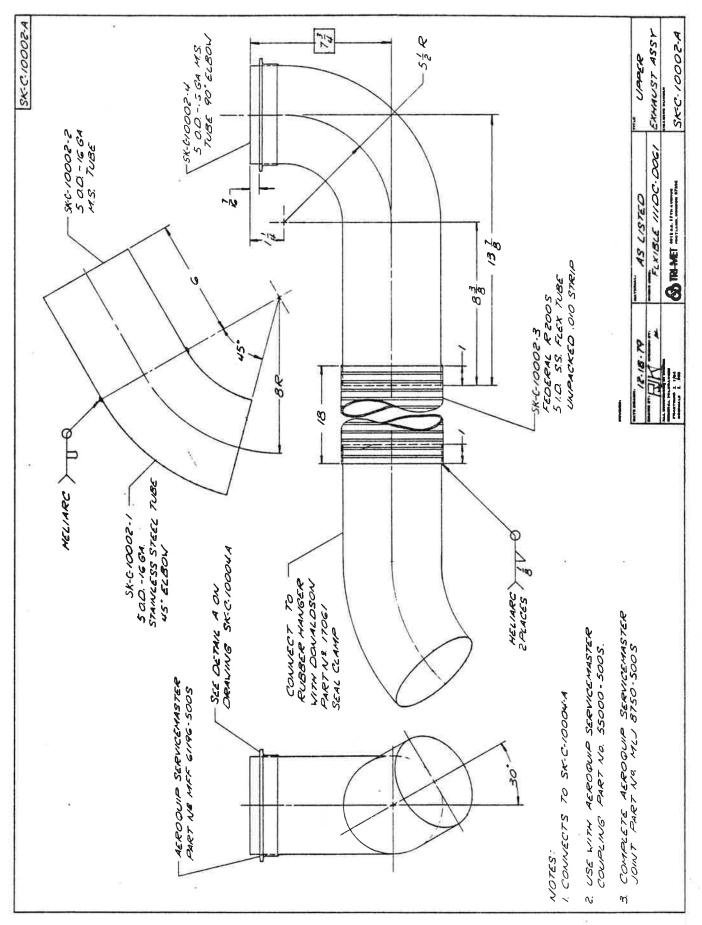
APPENDIX B.

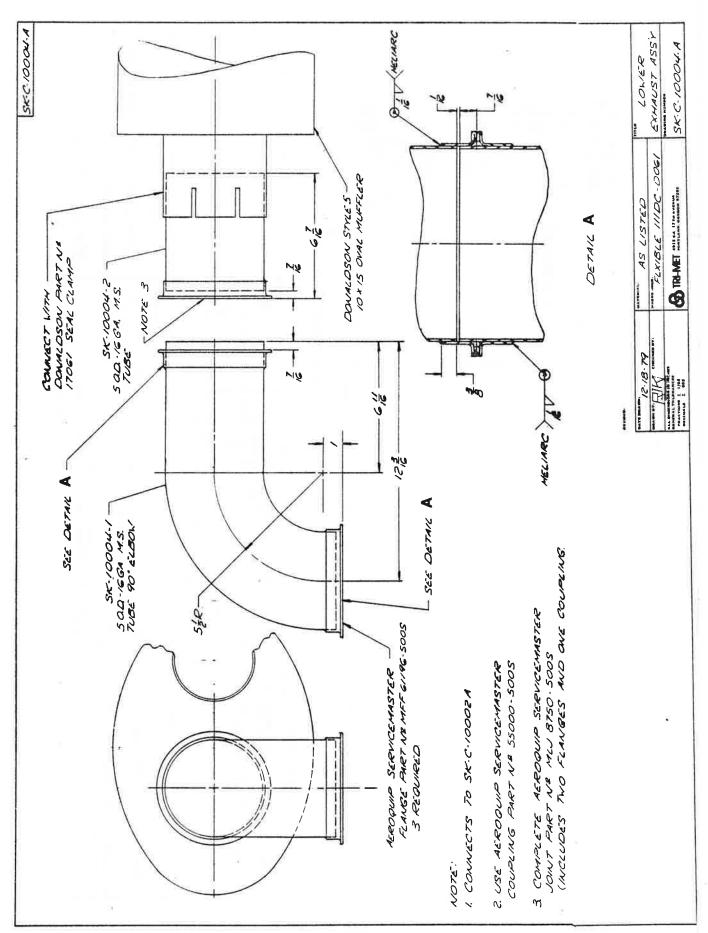
TRI-MET DRAWINGS

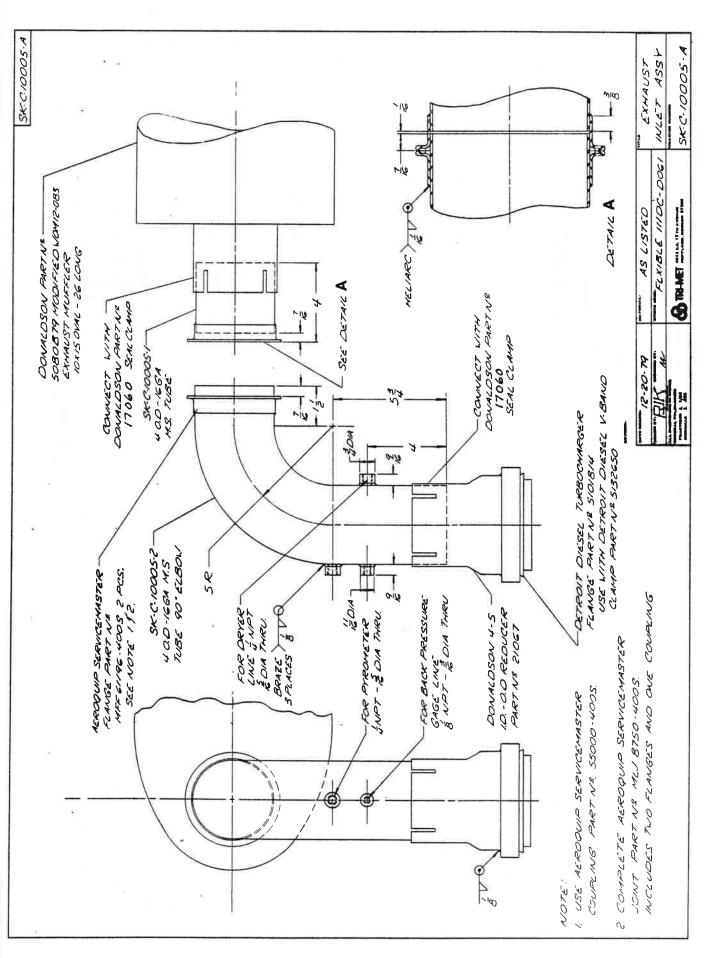
Number	Title
SK-C-10000	MUFFLER HANGER BRACKET
SK-B-10001A	MUFFLER MOUNTING PLATE ASS'Y
SK-C-10002A	UPPER EXHAUST ASS'Y
SK-A-10003A	MUFFLER JACKET ASS'Y
SK-C-10004A	LOWER EXHAUST ASS'Y
SK-C-10005A	EXHAUST INLET ASS'Y
SK-A-10007	DRYER ADAPTER
SK-A-10008A	DRYER AIR LINE INST
SK-C-10009A	INTAKE ELBOW ASS'Y
SK-C-10010A	INTAKE SYSTEM INST
SK-B-10011	FIREWALL BLANK
SK-B-10012	AIR CLEANER SUPPORT
SK-A-10013	SWITCH BOX BRACKET
SK-B-10014	FUEL FILTER BRACKET
SK-C-10015A	AIR CLEANER STRAP ASS'Y
SK-B-10016	INTAKE COWL BLANK
SK-A-10017A	HOLLOWAY SNORKLE ASS'Y-FLX
SK-C-10018A	REAR DOOR PADDING
SK-C-10019A	DOOR STOP
SK-A-10020	SNORKLE TEMPLATE
SK-C-10021A	FIREWALL PADDING
SK-C-10022A	RADIATOR PADDING
SK-C-10023A	REBUILT GRILLE
SK-A-10024A	SNORKLE INST
SK-B-10025	GRILLE SUPPORT
SK-C-10026A	EXHAUST SYSTEM INST

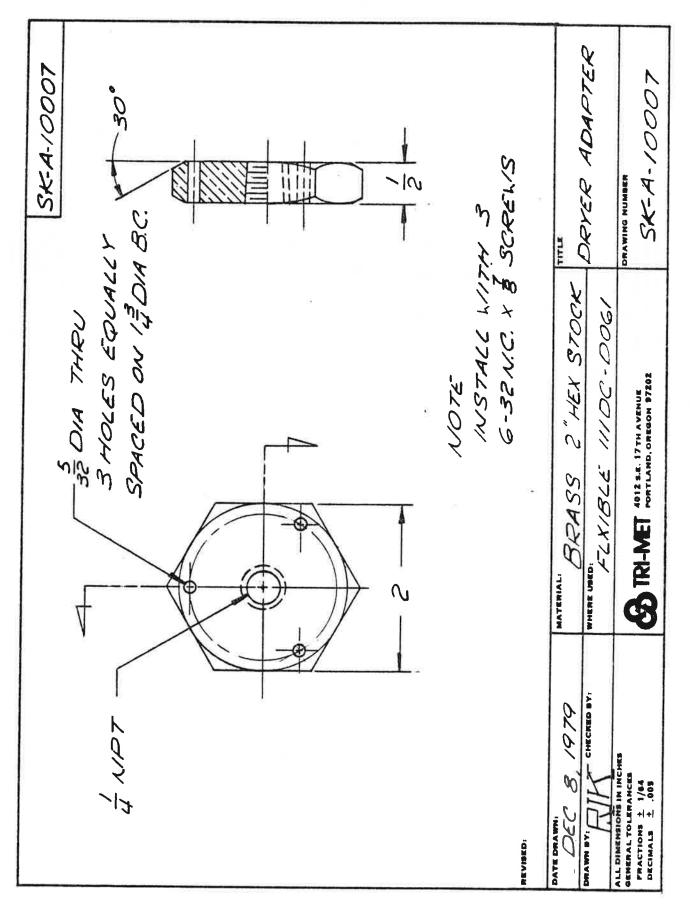


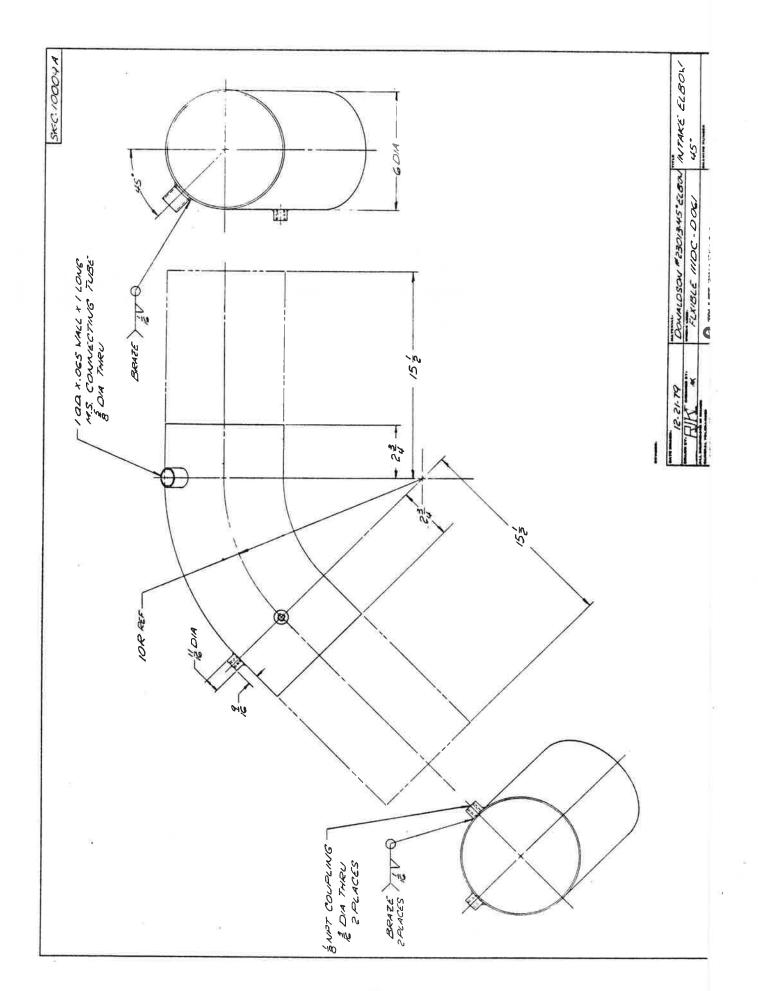


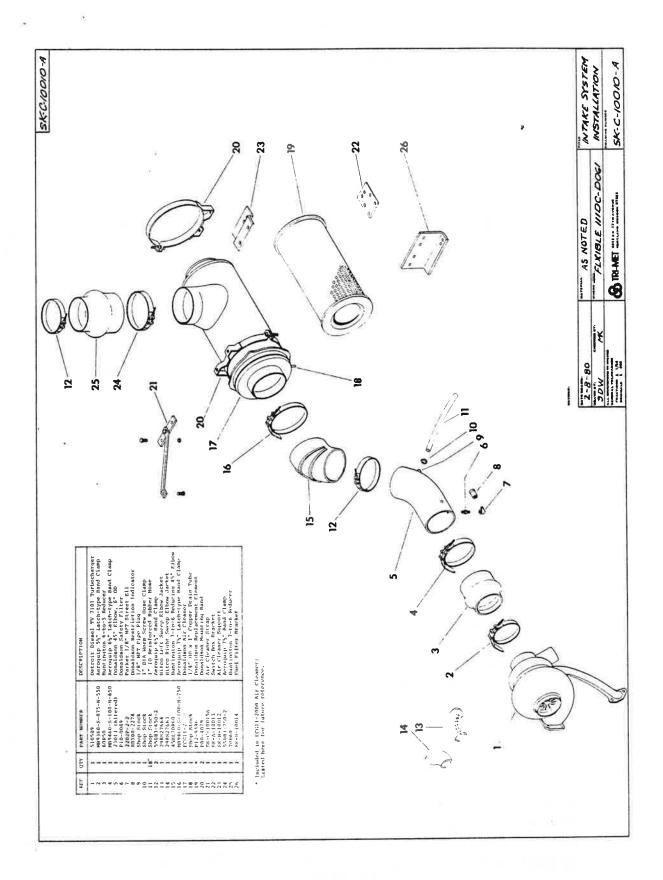


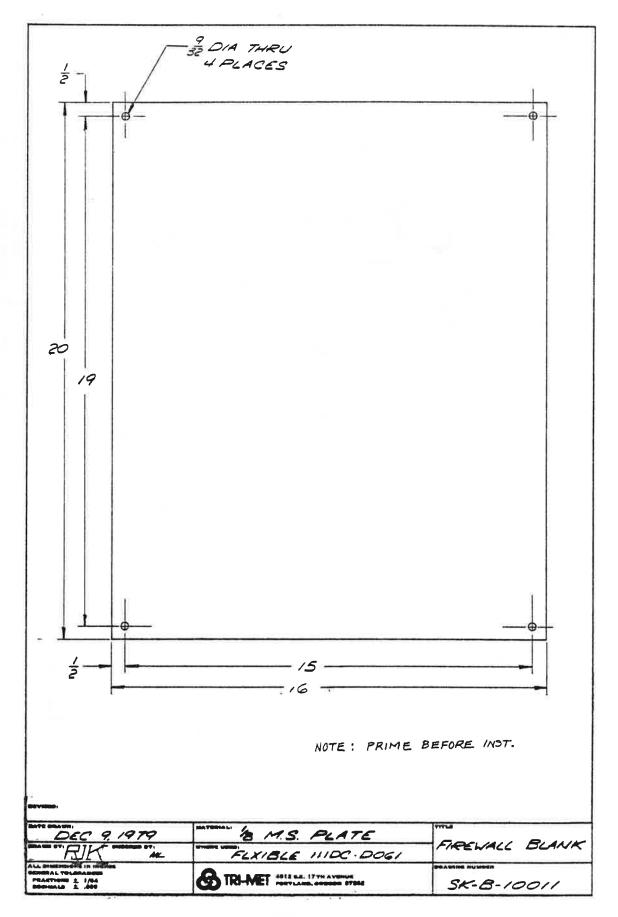


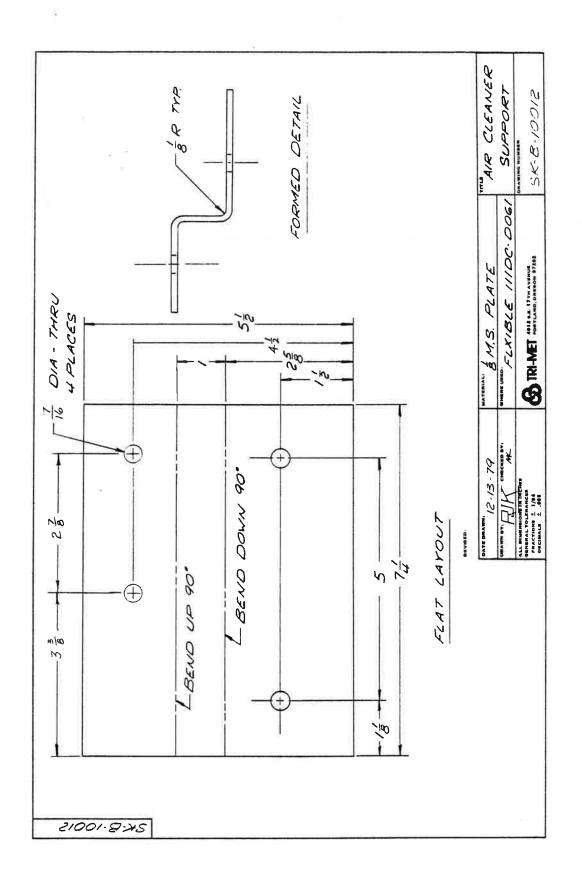


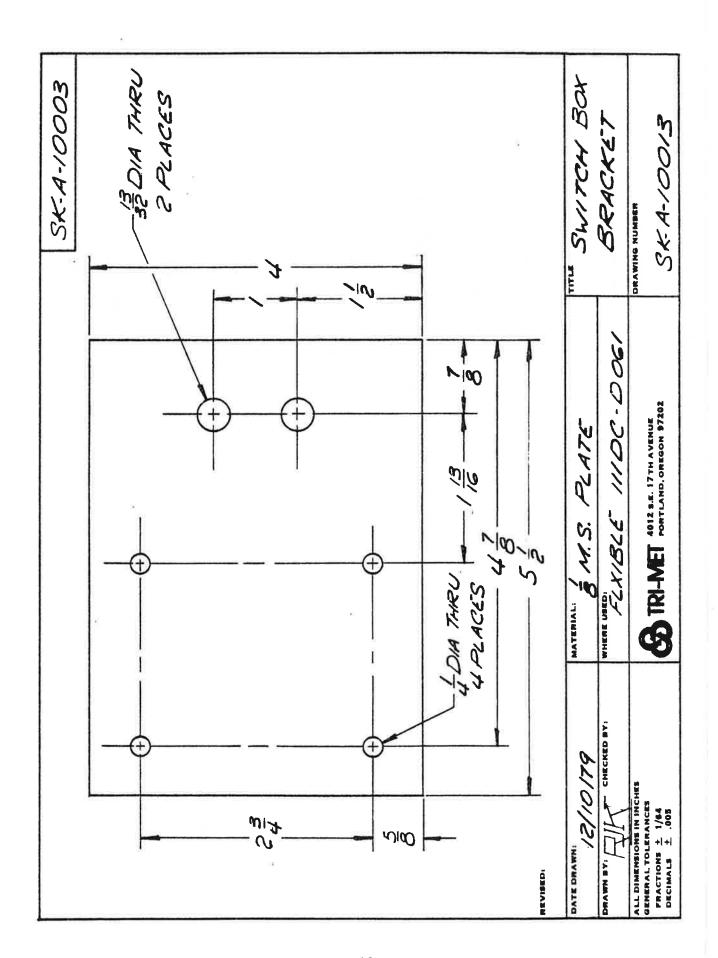


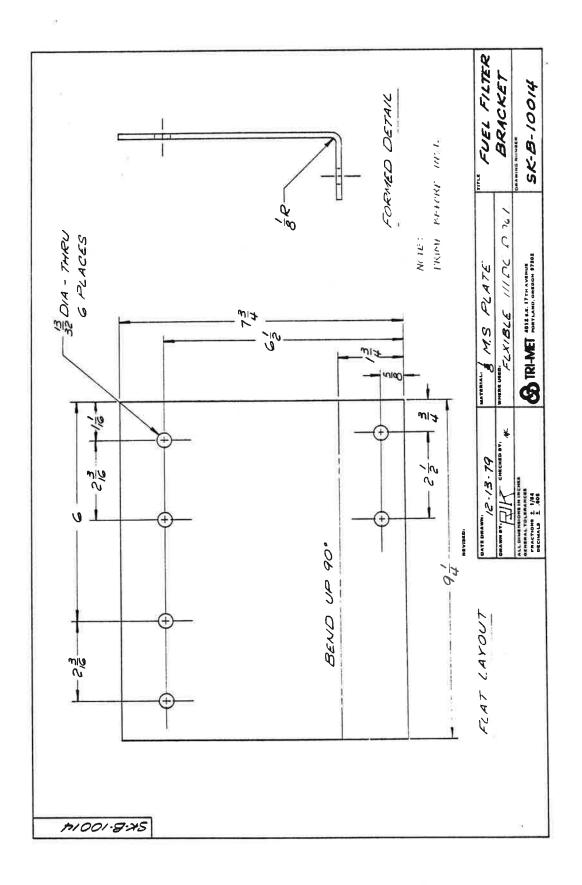


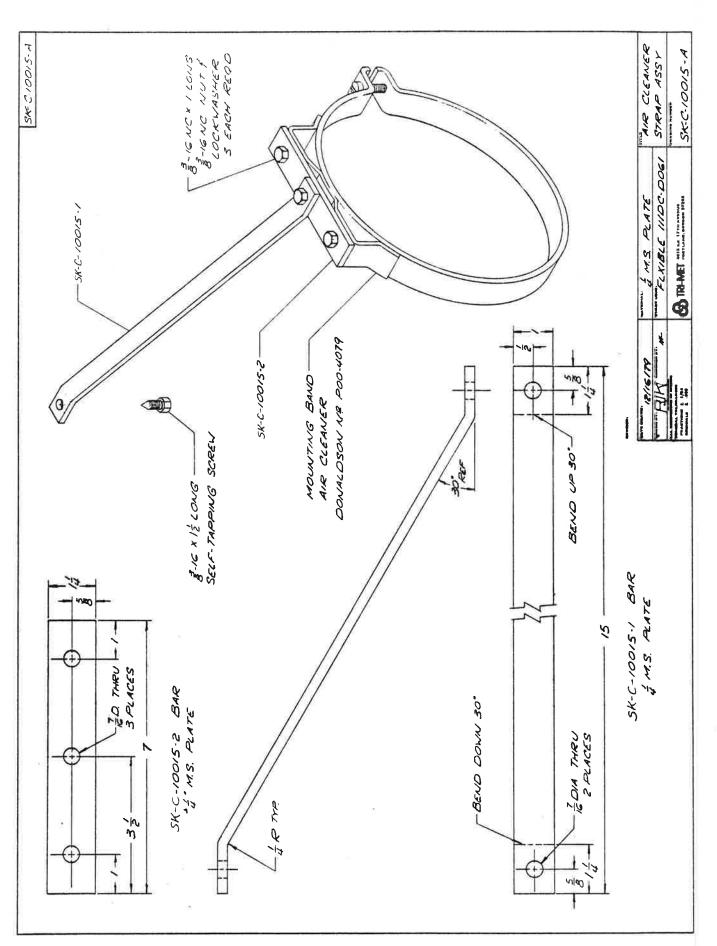


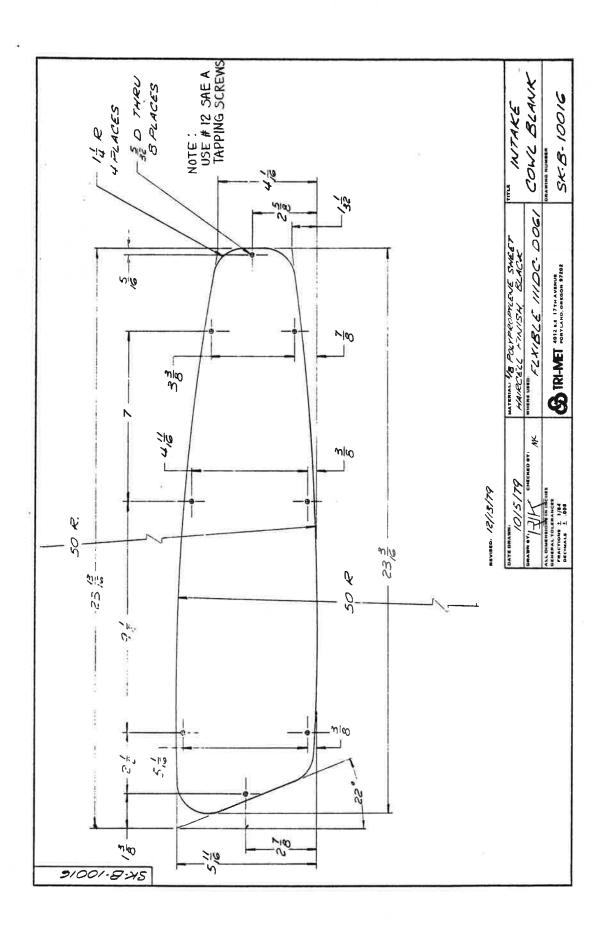




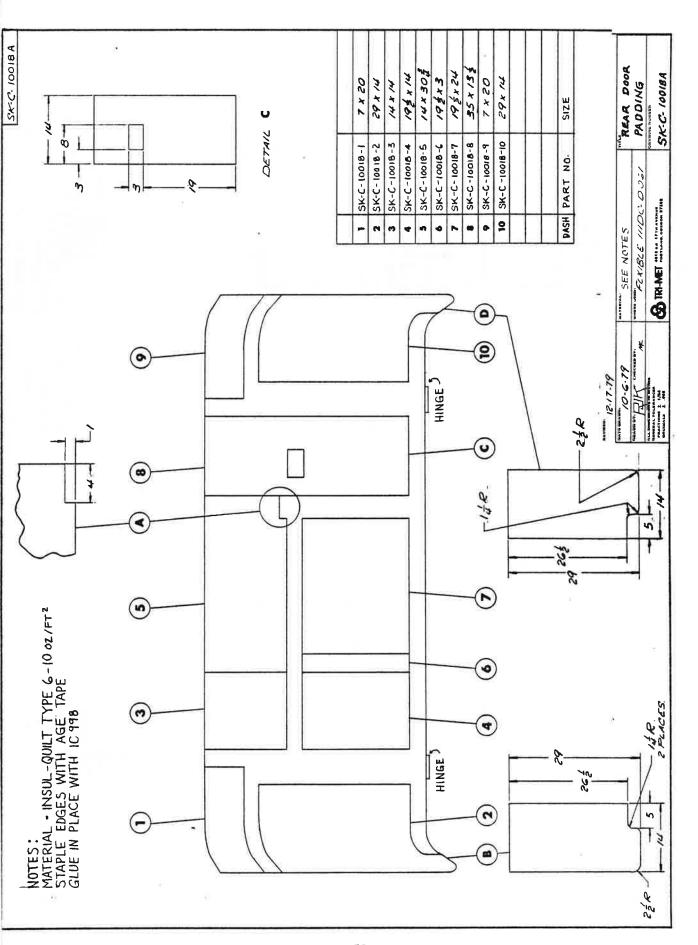


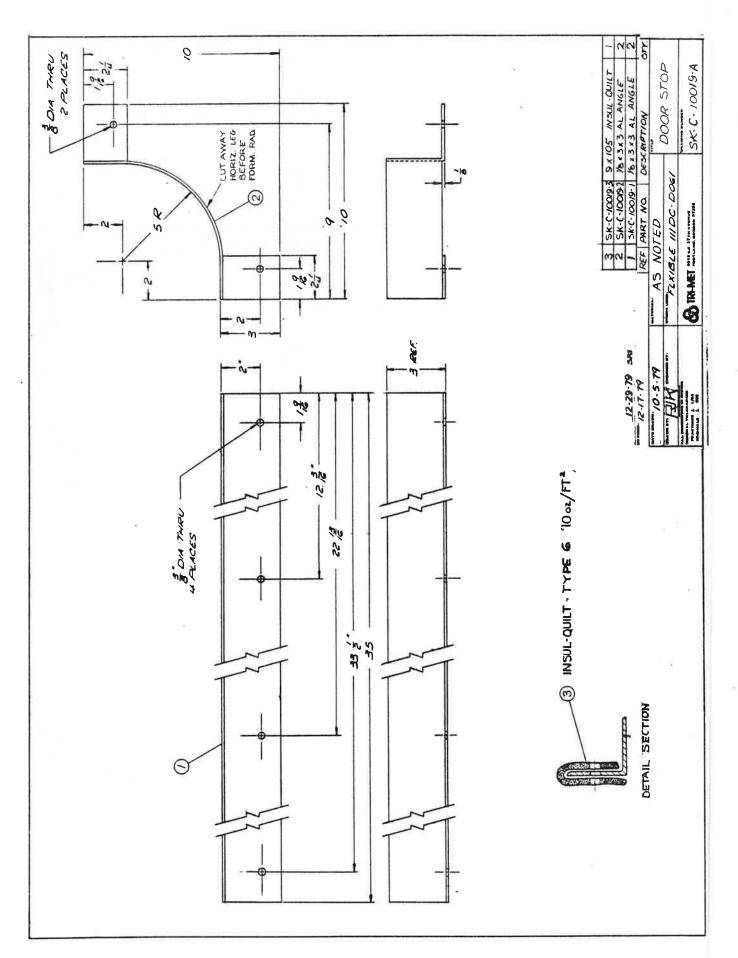


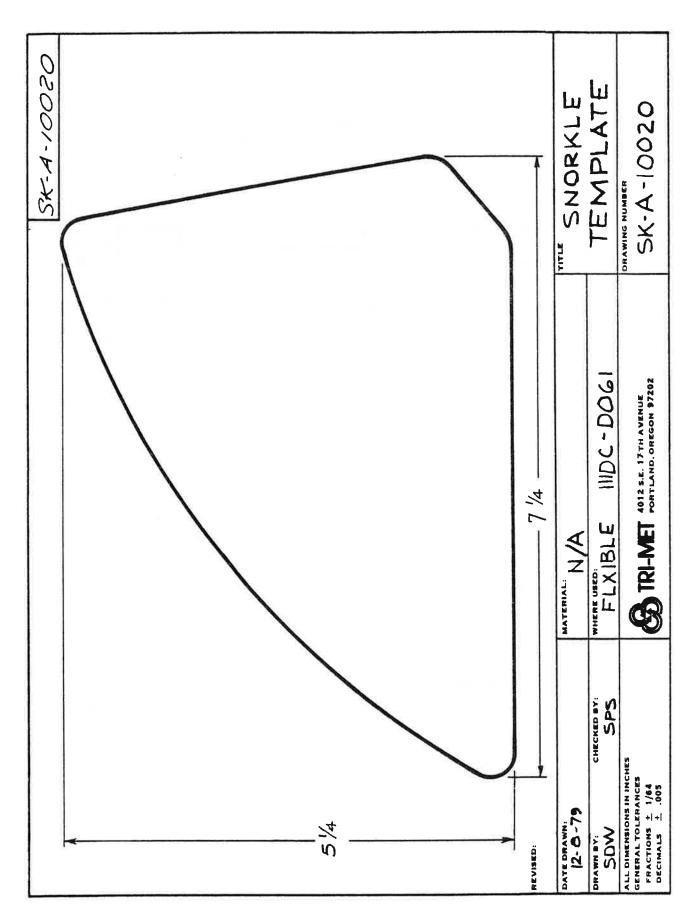


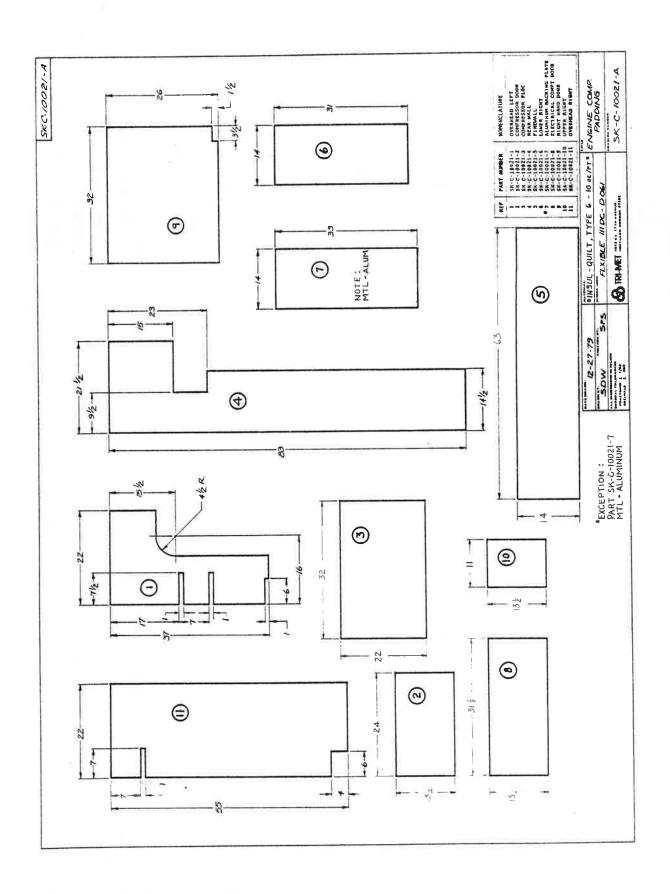


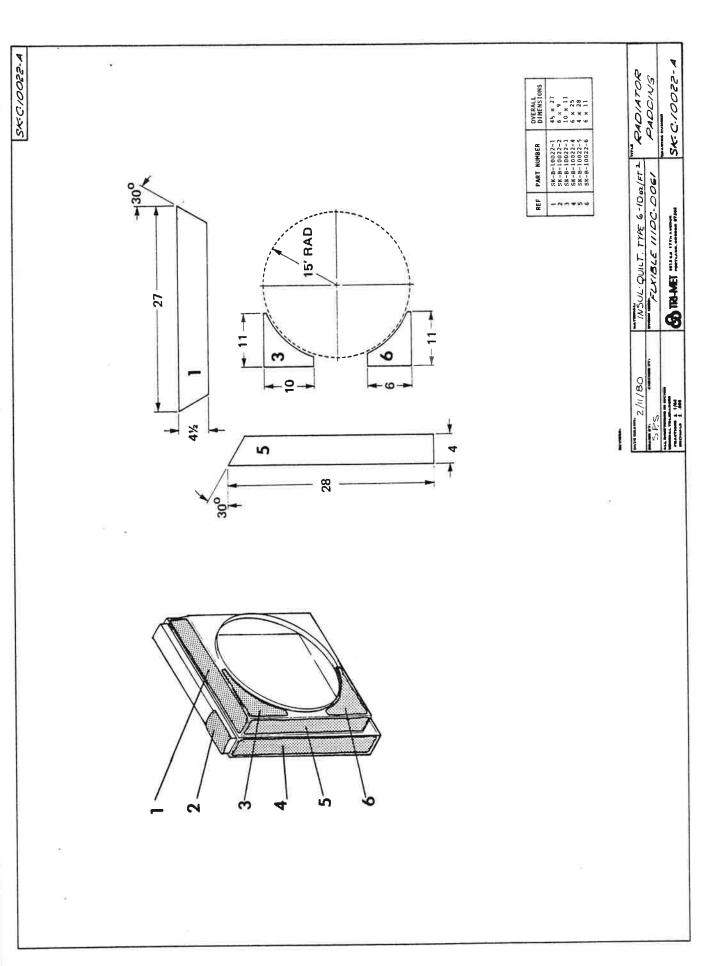
	SK-A-10017-A	7.A
		\$ 5 P. C.
	2 SK-A-10017-2 SS WIRE SCRN	RE SCRN
	I SK-A-10017-1 FIBERGLASS	SLASS
REVISED:	REF PART NO. MATERIAL	IAL
DATE DRAWN: JAN 7, 1979	45 NOTED	>
DRAWN BY: CHECKED BY:	WHERE USED: SNORKLE FLXIBLE HIDC - DOG!	
INCHES ICES 64 05	TRI-NET 4012 S.E. 17TH AVENUE SK-A-10017-A	4

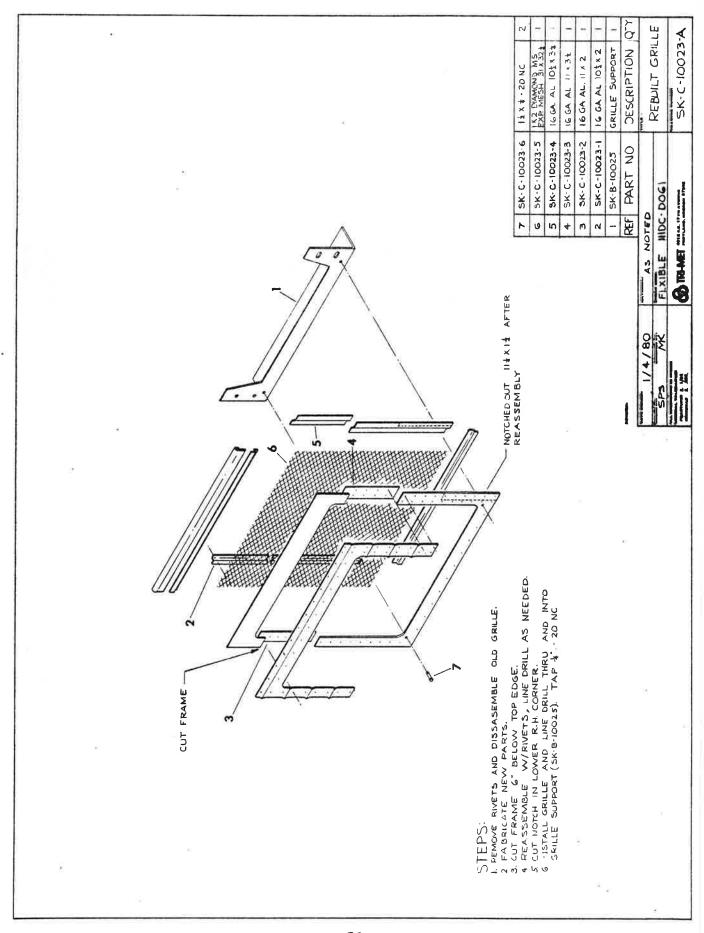


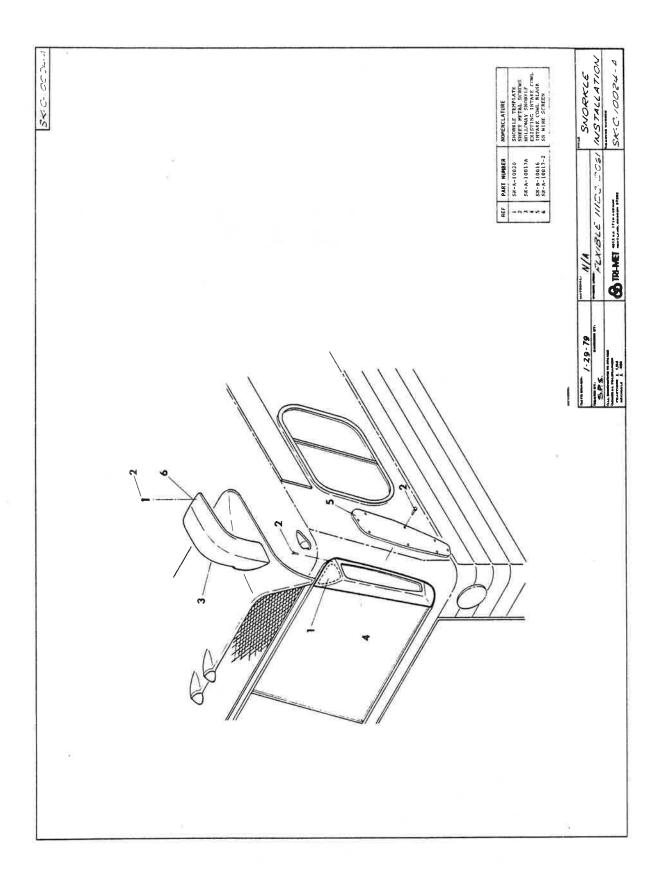


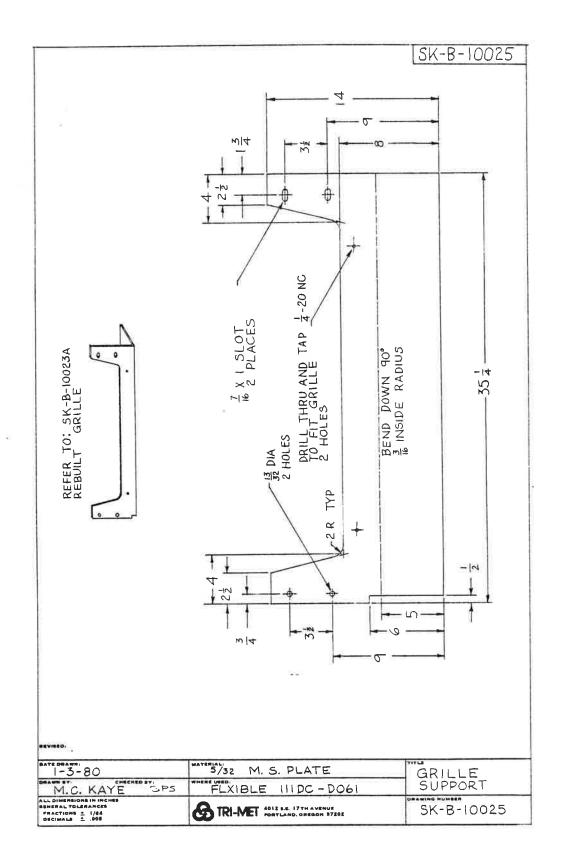


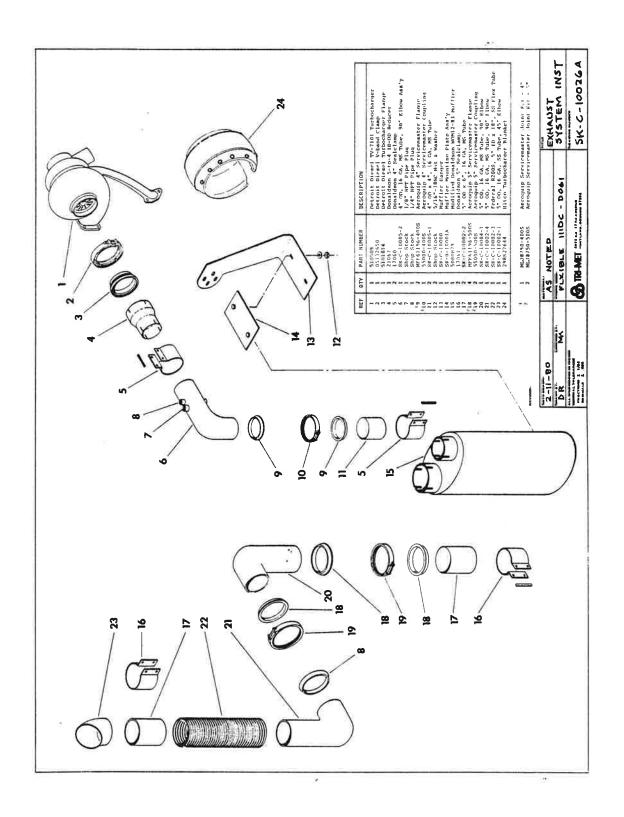












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